

5-25-2016

# Hydrodynamic study of a circulating fluidized bed used for biomass gasification between 20 °c and 900 °c

Sébastien Pecate

*Université de Toulouse, INPT, Laboratoire de Génie Chimique de Toulouse, 4 allée Émile Monso, 31432 Toulouse Cedex 4 - BP 84234, sebastien.pecate@ensiacet.fr*

Mehrdji HEMATI

*Université de Toulouse, INPT, Laboratoire de Génie Chimique de Toulouse, 4 allée Émile Monso, 31432 Toulouse Cedex 4 - BP 84234*

Mathieu MORIN

*Université de Toulouse, INPT, Laboratoire de Génie Chimique de Toulouse, 4 allée Émile Monso, 31432 Toulouse Cedex 4 - BP 84234*

Yilmaz KARA

*Centre de Recherche et d'Innovation Gaz et Energies Nouvelles (CRIGEN), 361 avenue du Président Wilson – BP33 – 93211 Saint Denis la Plaine CEDEX Groupe ENGIE*

Sylvie VALIN

*CEA, LITEN, 17 rue des Martyrs F-38054 Grenoble cedex 9, France*

Follow this and additional works at: [http://dc.engconfintl.org/fluidization\\_xv](http://dc.engconfintl.org/fluidization_xv)

 Part of the [Chemical Engineering Commons](#)

---

## Recommended Citation

Sébastien Pecate, Mehrdji HEMATI, Mathieu MORIN, Yilmaz KARA, and Sylvie VALIN, "Hydrodynamic study of a circulating fluidized bed used for biomass gasification between 20 °c and 900 °c" in "Fluidization XV", Jamal Chaouki, Ecole Polytechnique de Montreal, Canada Franco Berruti, Wewstern University, Canada Xiaotao Bi, UBC, Canada Ray Cocco, PSRI Inc. USA Eds, ECI Symposium Series, (2016). [http://dc.engconfintl.org/fluidization\\_xv/134](http://dc.engconfintl.org/fluidization_xv/134)

This Abstract and Presentation is brought to you for free and open access by the Proceedings at ECI Digital Archives. It has been accepted for inclusion in Fluidization XV by an authorized administrator of ECI Digital Archives. For more information, please contact [franco@bepress.com](mailto:franco@bepress.com).

# BIOMASS GASIFICATION IN A CIRCULATING FLUIDIZED BED: HYDRODYNAMIC STUDY BETWEEN 20 °C AND 950 °C

Sébastien Pécate, Mathieu Morin, Mehrdji Hemati

# GAYA PROJECT OBJECTIVES

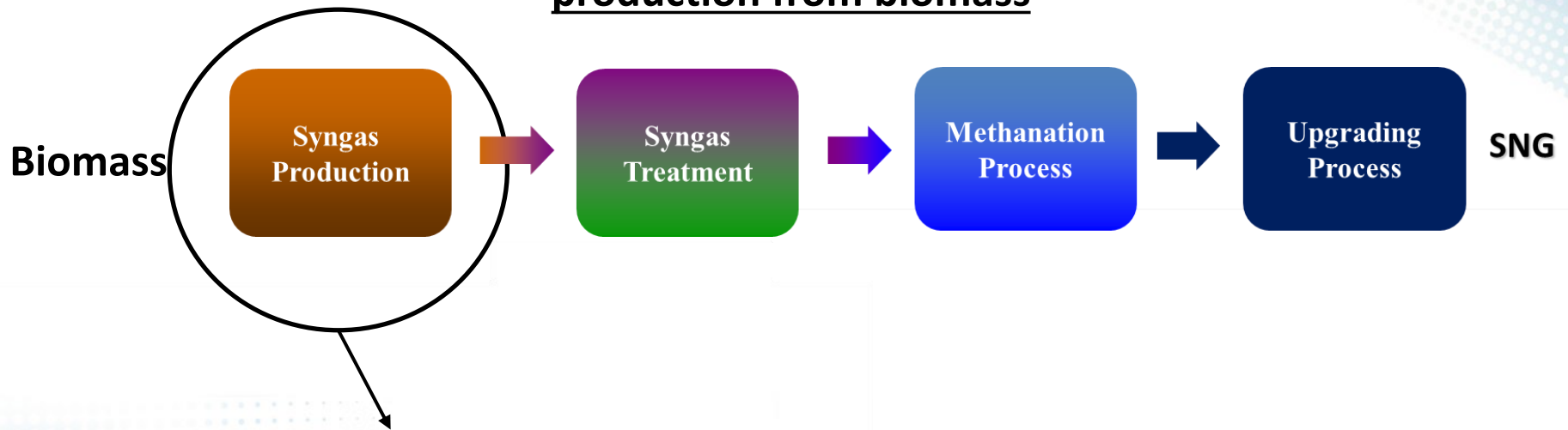
Building of an industrial process for the Synthetic Natural Gas (SNG)  
production from biomass





# GAYA PROJECT OBJECTIVES

## Building of an industrial process for the Synthetic Natural Gas (SNG) production from biomass

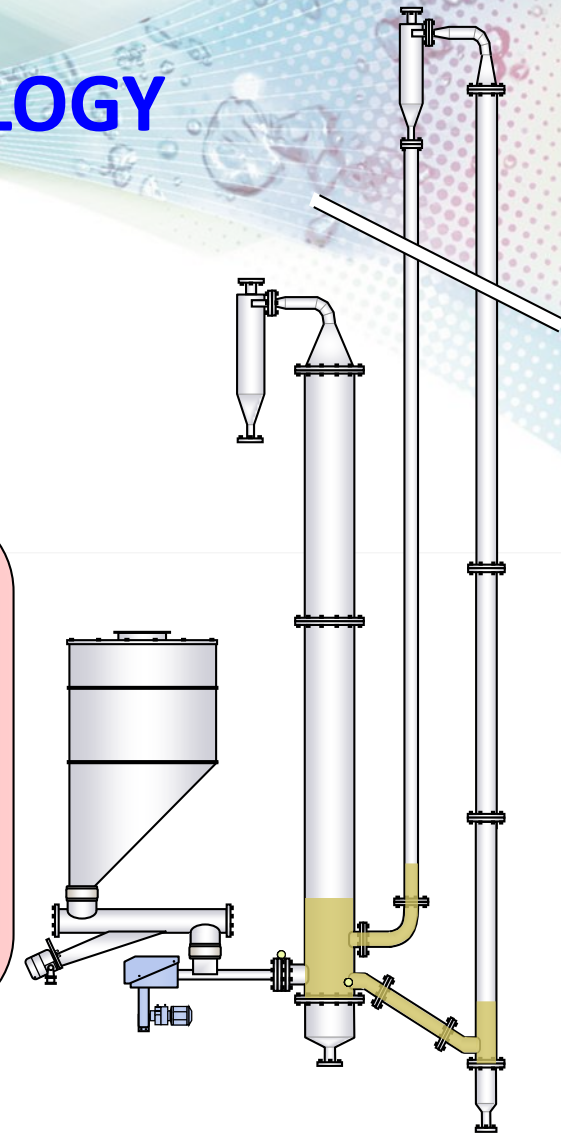
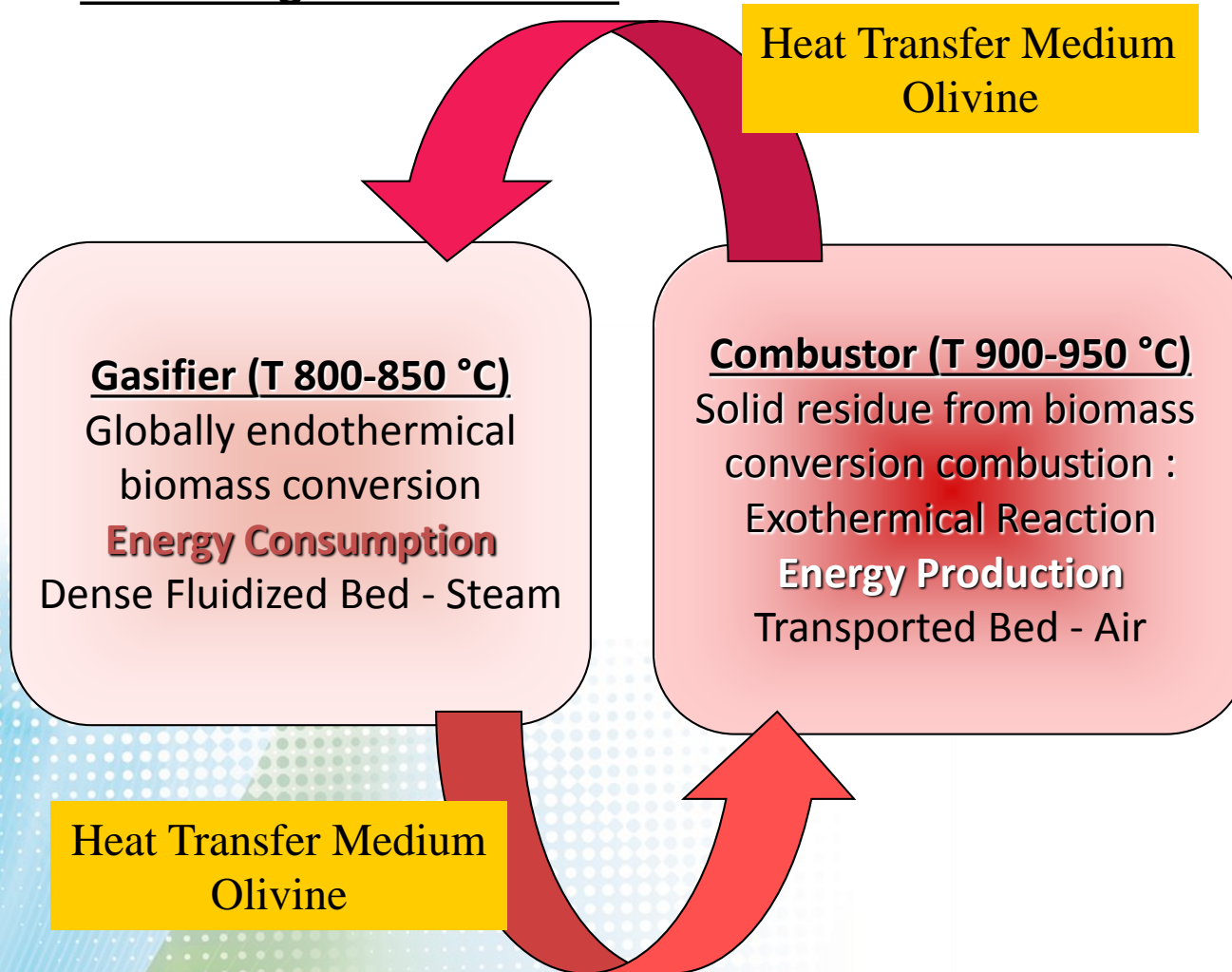


**LGC Objective : Understanding of the hydrodynamic, thermal and reactive phenomena occurring in the syngas production pilot plant**

Technology : CFB ✓

# EMPLOYED TECHNOLOGY

## Circulating Fluidized Bed :



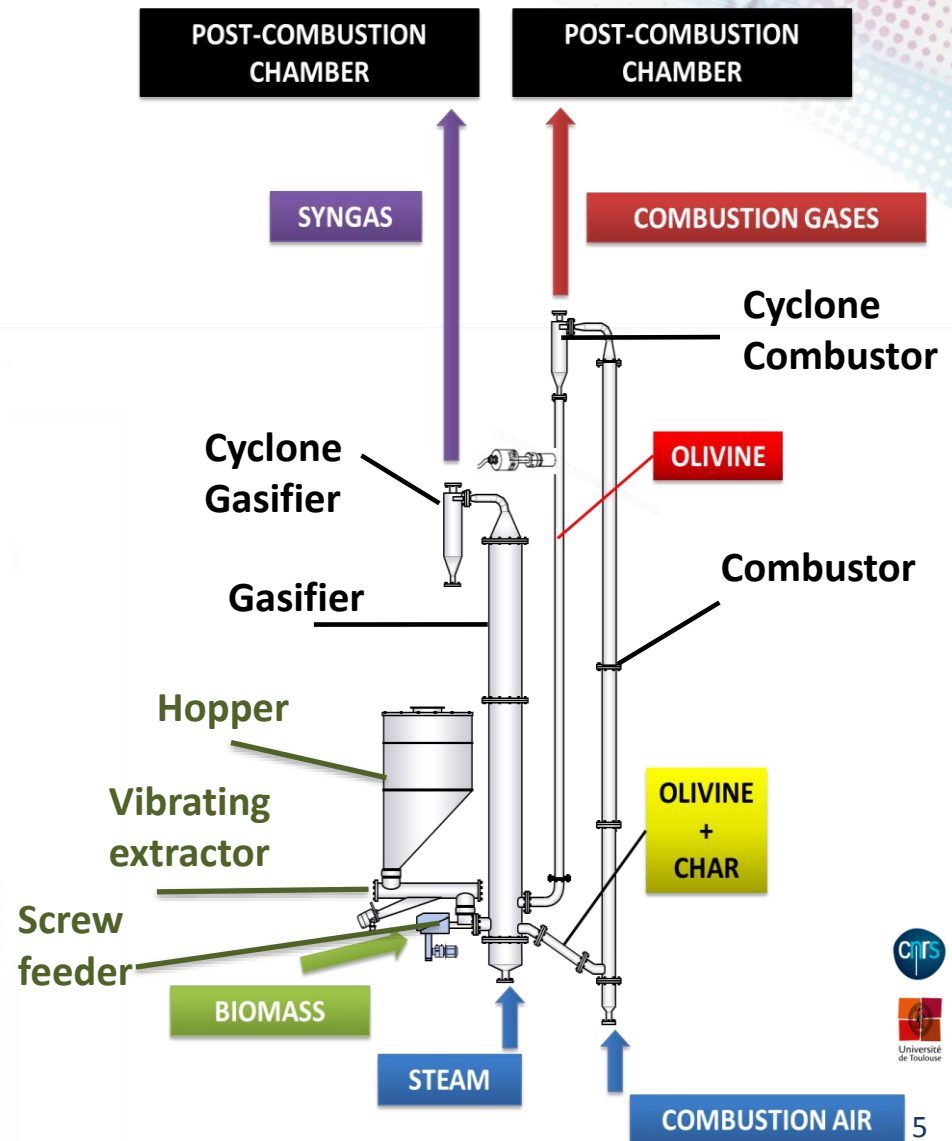
# EXPERIMENTAL SETUP

- Circulating fluidized bed designed and built-up at the LGC Toulouse

## Biomass Feeding

### Gasifier / Combustor : Reactive zones

- Electric furnaces 15 and 6 kW :
- ✓ Startup of the installation
- ✓ Carrying of hot hydrodynamic tests
- Post-combustion chamber at the outlet
- ✓ Burning all combustible gas





# EXPERIMENTAL SETUP

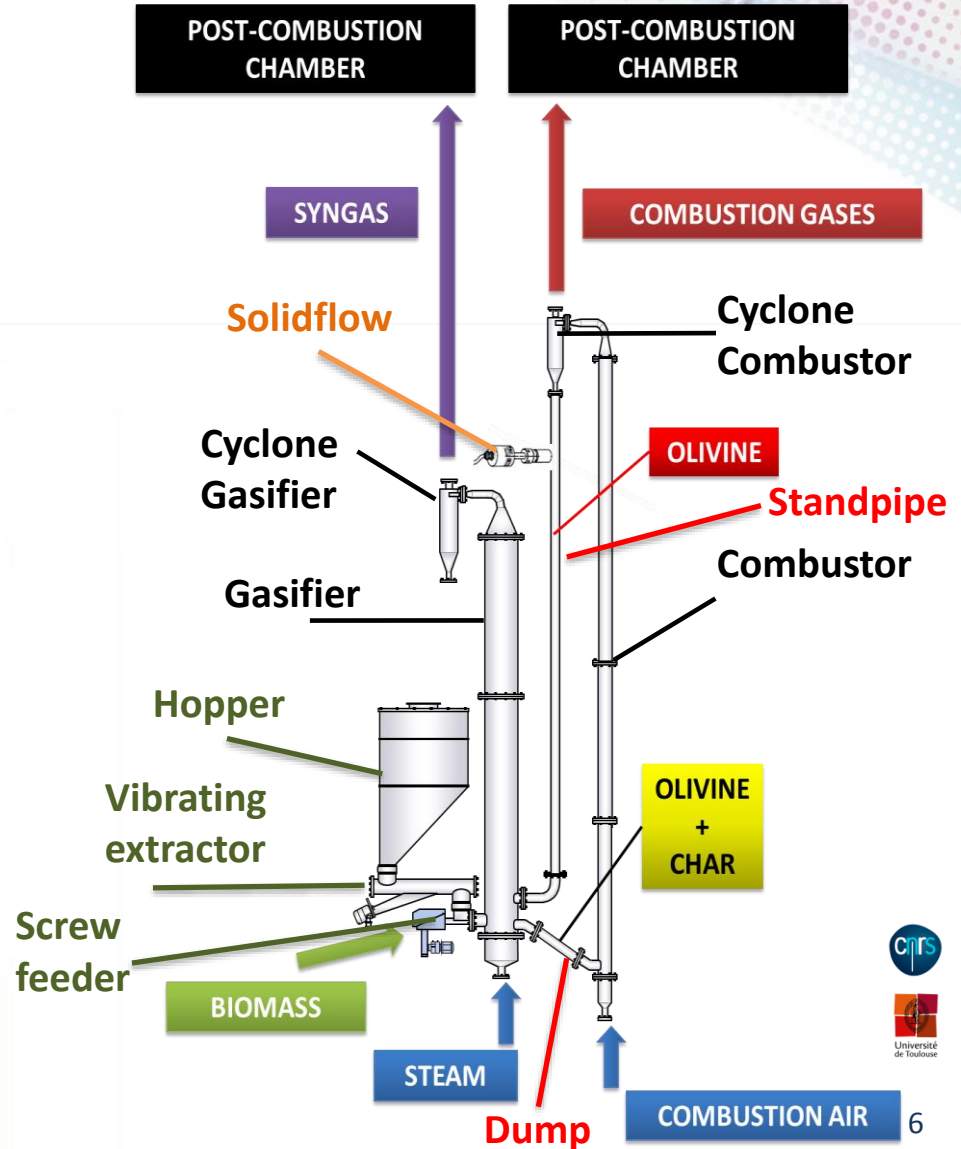
- Circulating fluidized bed designed and built-up at the LGC Toulouse

Biomass Feeding

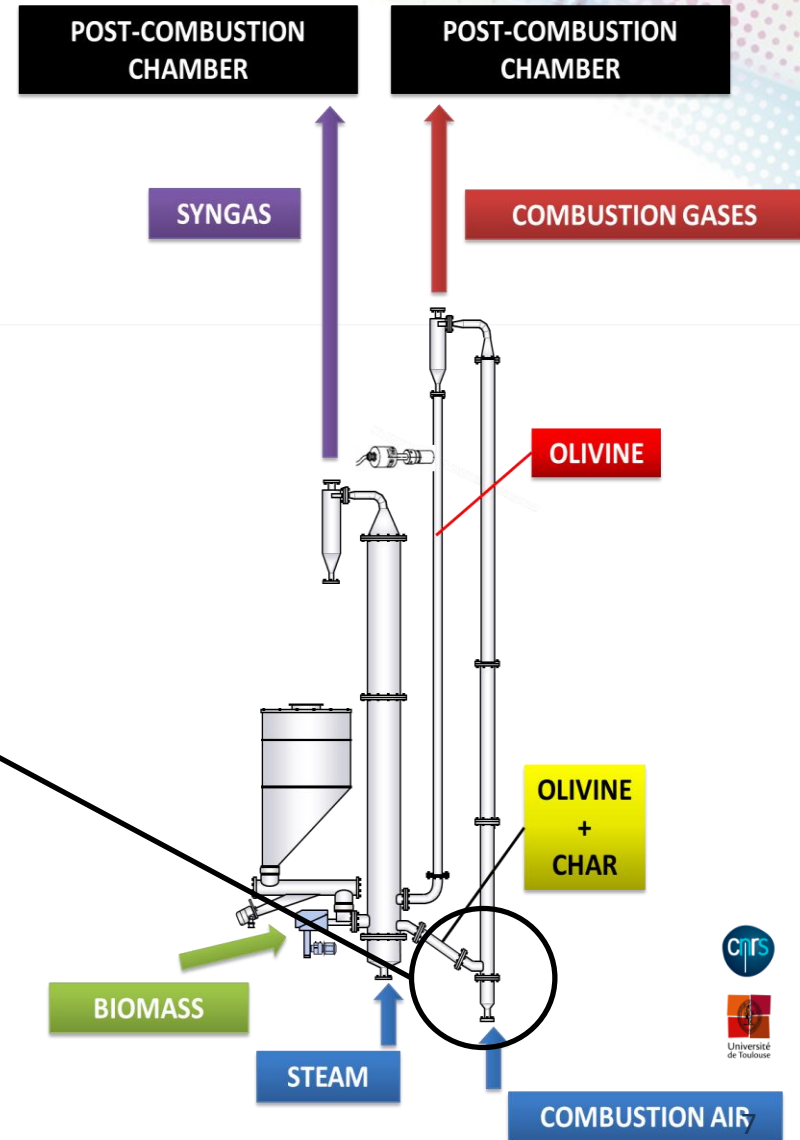
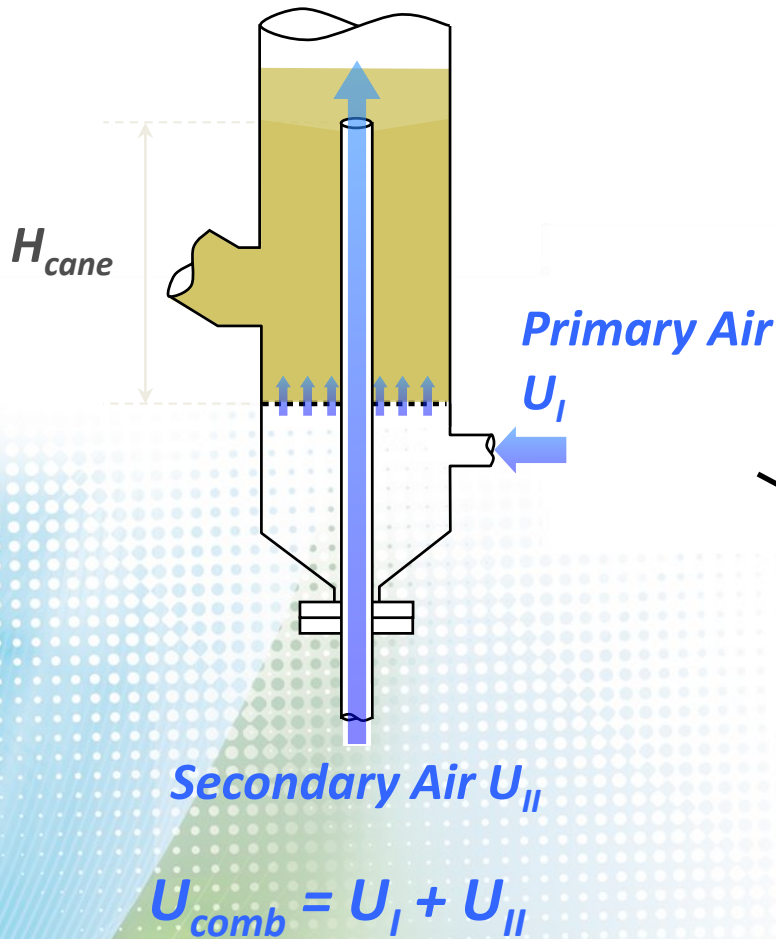
Gasifier / Combustor : Reactive zones

Standpipe / Dump : Solid circulation

Solidflow : Circulating solid mass flow rate measurement

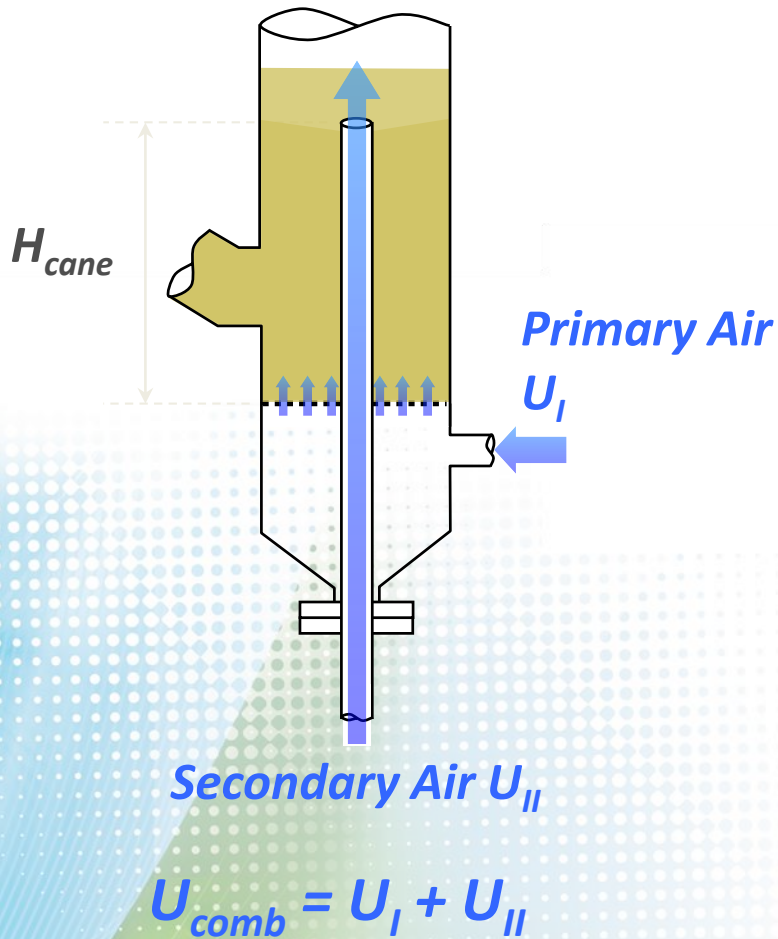


# AIR FEEDING IN THE COMBUSTOR





# AIR FEEDING IN THE COMBUSTOR



## ✓ Secondary Air injection cane height

$H_{cane}$

- Sets the dense fluidized bed height
- 15 cm

# INDUSTRIAL DEVELOPMENT ISSUES

Design/simulation of industrial CFB biomass gasifiers



Dense fluidized bed hydrodynamic properties ( $U_{mf}$ ,  $\varepsilon_{mf}$ ,  $\varepsilon$ )



Olivine particle size

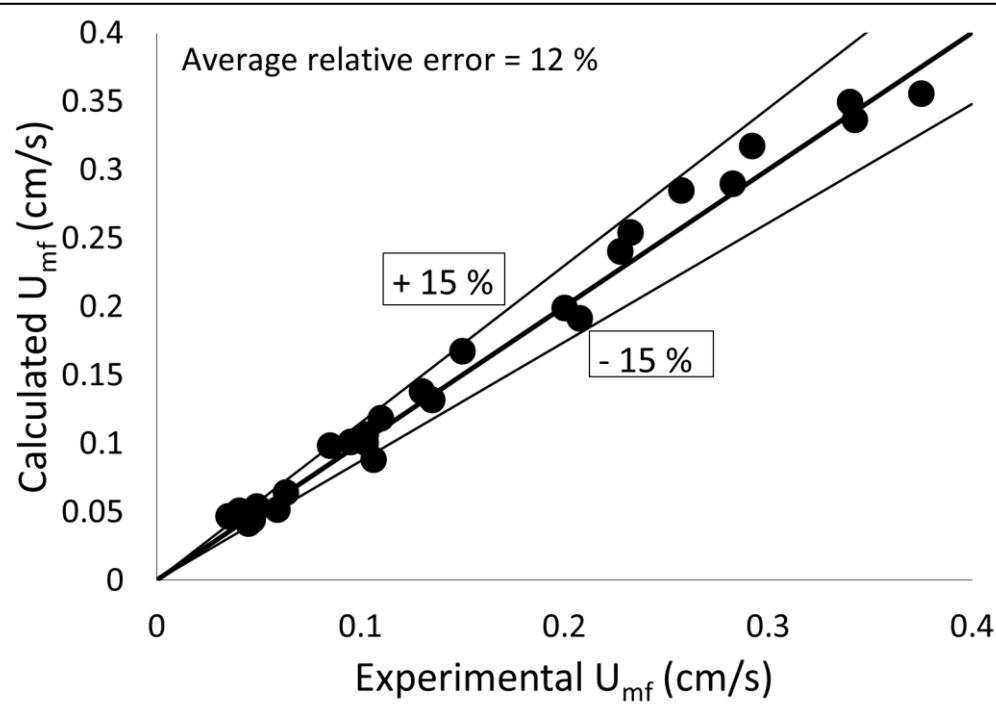
- [200 – 300  $\mu\text{m}$ ]  $d_{3/2} = 280 \mu\text{m}$
- [300 – 400  $\mu\text{m}$ ]  $d_{3/2} = 460 \mu\text{m}$
- [400 – 600  $\mu\text{m}$ ]  $d_{3/2} = 690 \mu\text{m}$

Temperature  
[20 – 950°C]

Gas nature  
Air / Steam

Proposition of correlations

## MINIMUM FLUIDIZATION VELOCITY



$U_{mf}$   when

• T 

• dp 

$U_{mf}$  (Steam)  $\Rightarrow$   $U_{mf}$  (air) :  
 $\rho$  et  $\mu$  (Steam)  $<$   $\rho$  et  $\mu$  (Air)

$$Re_{mf} = (20.32^2 + 0.031 \cdot Ar)^{0.5} - 20.32$$



## POROSITY / VOIDAGE

**Minimum fluidization porosity  $\epsilon_{mf}$  :**

No effect of bed temperature or particle size  
 $\Rightarrow \epsilon_{mf} = 0.55$

**Average porosity  $\epsilon$  :**

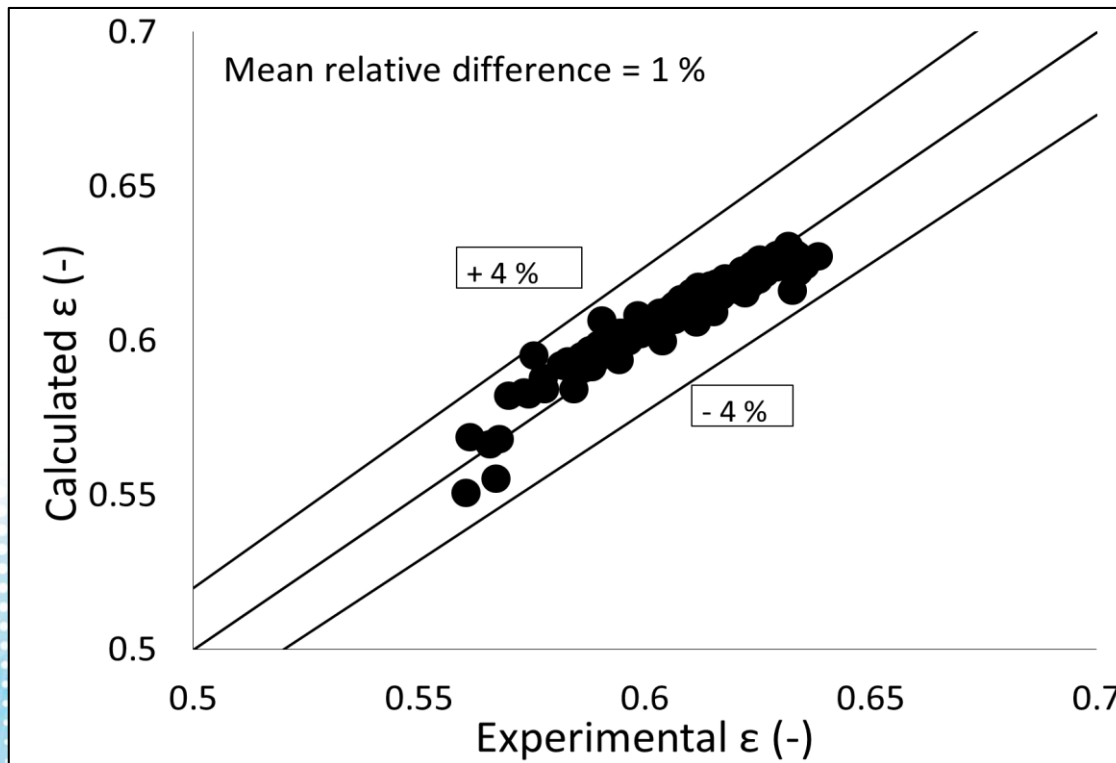
$\epsilon$   $\nearrow$  when

- $U - U_{mf}$   $\nearrow$

But independent of :

- bed temperature
- particle size

## POROSITY / VOIDAGE



$$\frac{\epsilon}{\epsilon_{mf}} = 1.0394 \cdot \left( \frac{U - U_{mf}}{U_{mf}} \right)^{0.026} \cdot Ar^{0.006}$$

# INDUSTRIAL DEVELOPMENT ISSUES

I. Hydrodynamic study  
of the gasifier

Syngas production efficiency

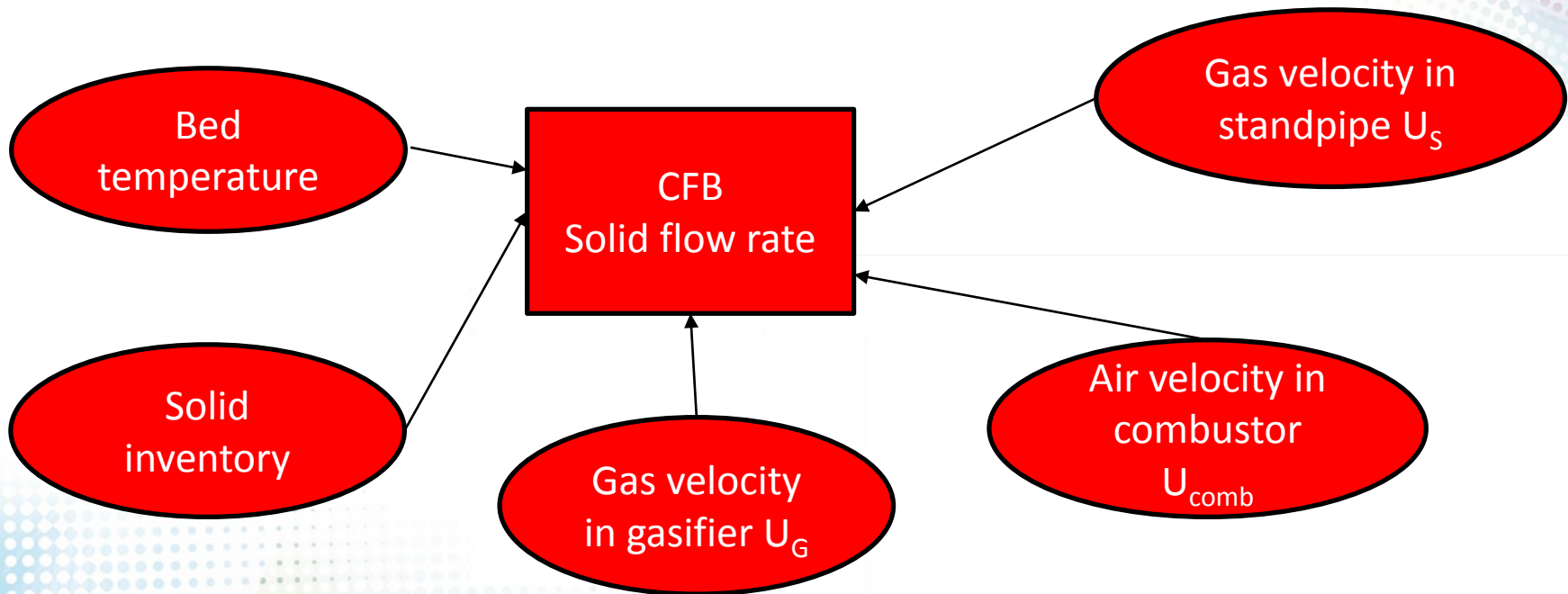
Gasifier / Combustor Relative  
temperature difference

Heat transfer medium circulation  
flow rate

Solid flow rate control  
parameters ?

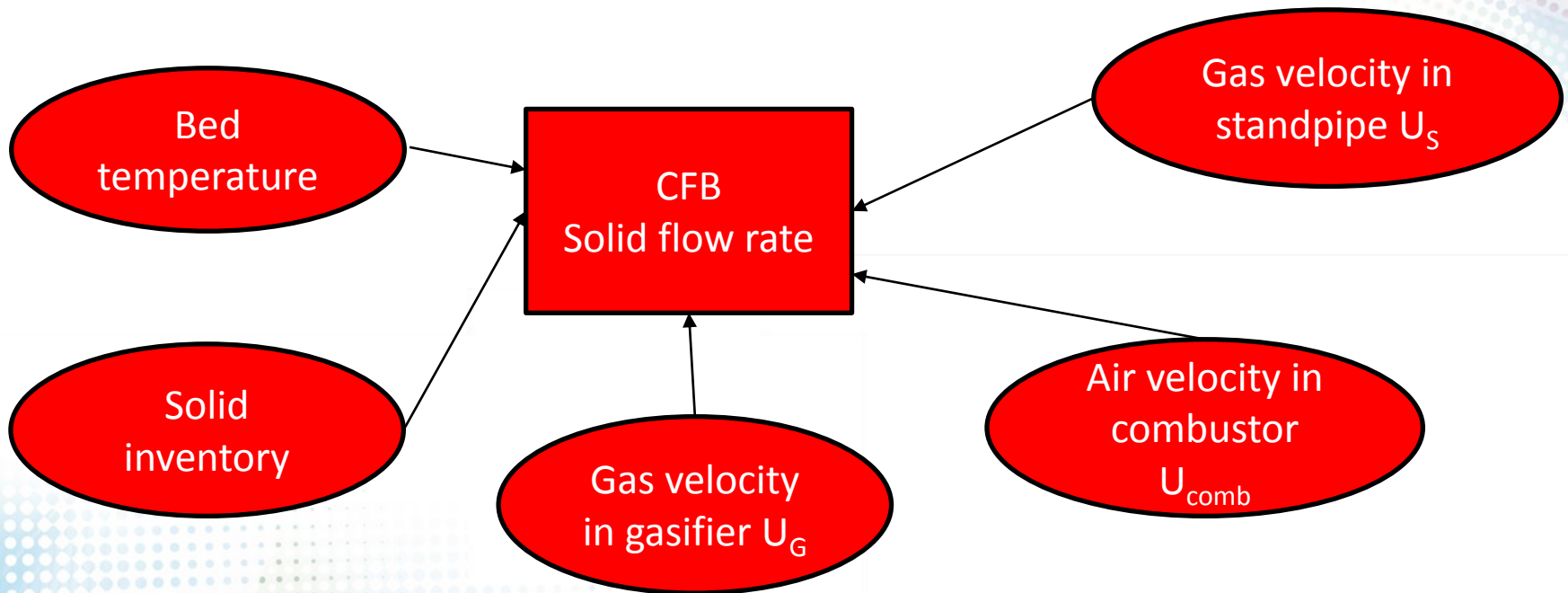


# II. HYDRODYNAMIC STUDY OF THE CFB



	T (°C)	$m_p$ (kg)	$U_G$ ( $U/U_{mf}$ )	$U_{comb}$ ( $U/U_t$ )	$U_s$ ( $U/U_{mf}$ )
Reference	500	35	4	2.4	8
Range	[20 – 850]	[35 – 60]	[1 – 8]	[0.4 – 3]	[1 – 8]

# II. HYDRODYNAMIC STUDY OF THE CFB

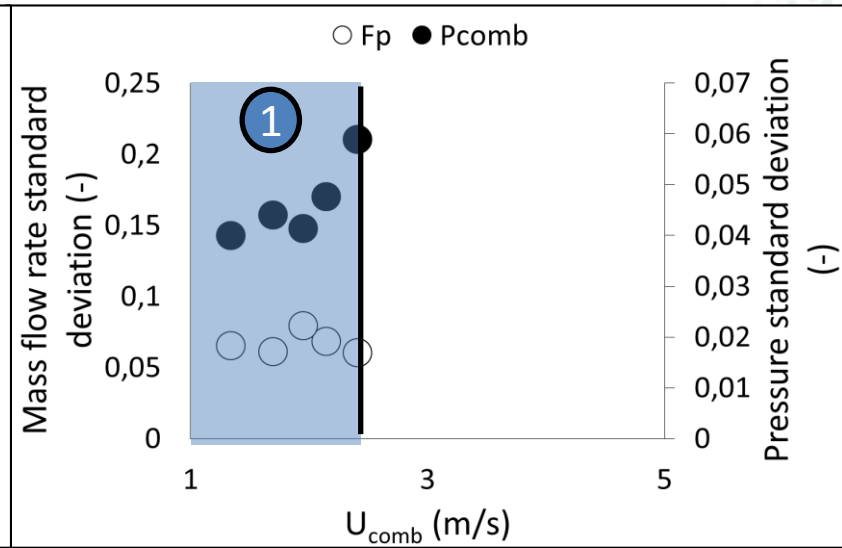
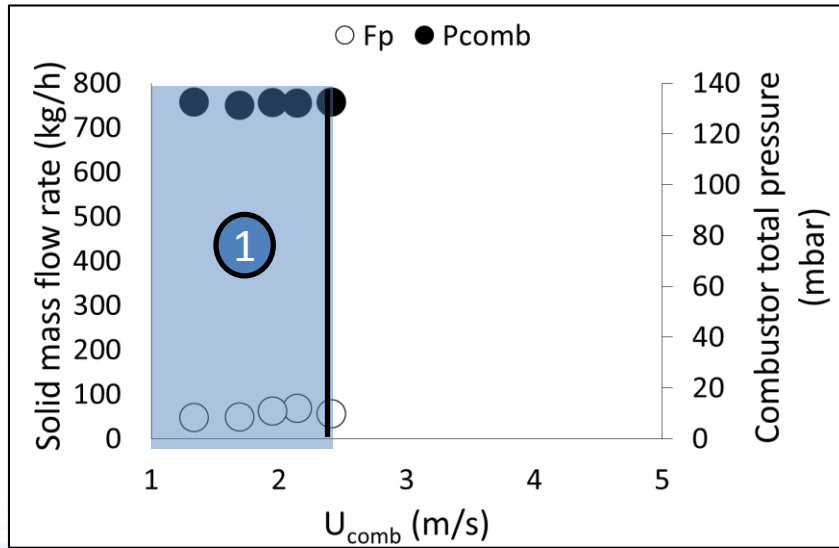


	T (°C)	$m_p$ (kg)	$U_G$ ( $U/U_{mf}$ )	$U_{comb}$ ( $U/U_t$ )	$U_s$ ( $U/U_{mf}$ )
Reference	500	35	4	2.4	8
Range	[20 – 850]	[35 – 60]	[1 – 8]	[0.4 – 3]	[1 – 8]

# II. HYDRODYNAMIC STUDY OF THE CFB

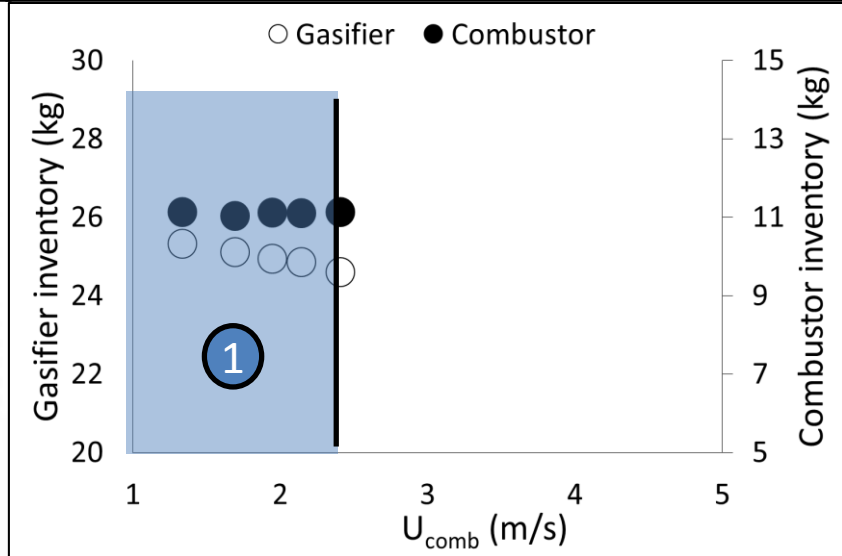
## EFFECT OF THE GAS VELOCITY $U_{comb}$ :

1 Dense fluidized bed



Three hydrodynamic regimes identified in the combustor :

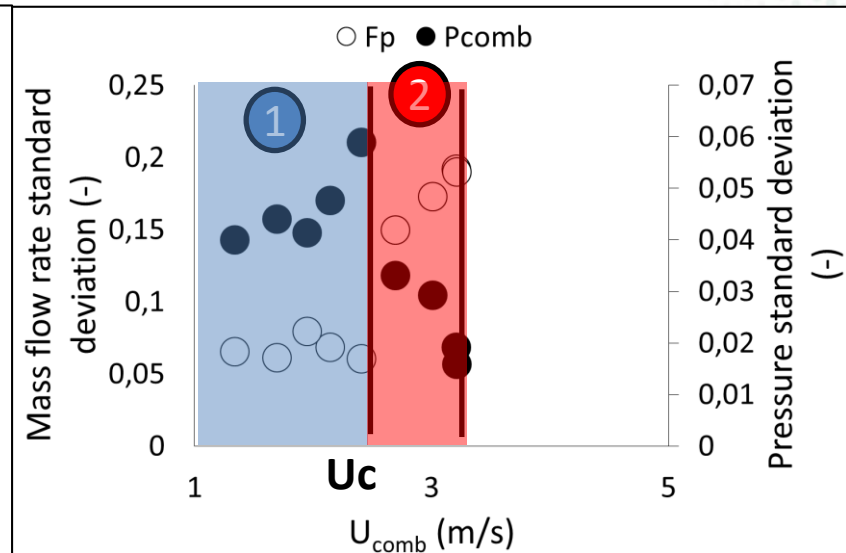
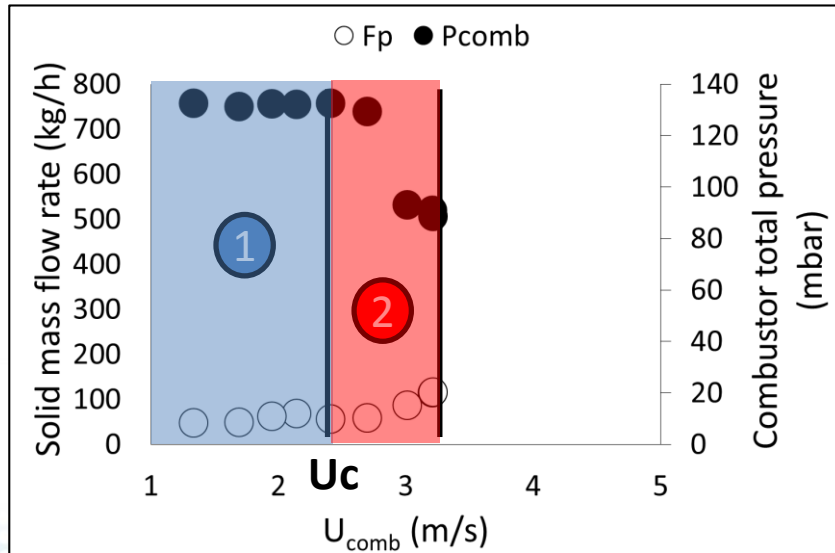
- 1) Dense fluidized bed regime





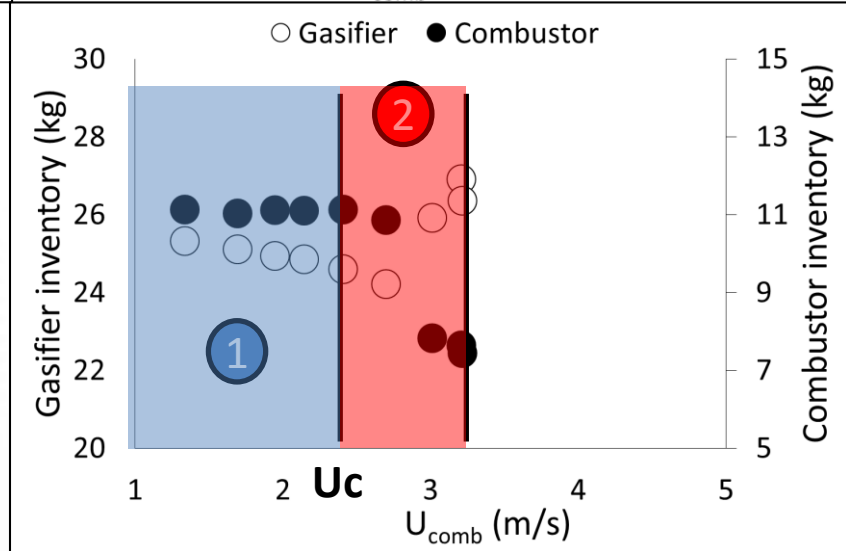
## EFFECT OF THE GAS VELOCITY $U_{comb}$ :

### 2 Turbulent bed



Three hydrodynamic regimes identified in the combustor :

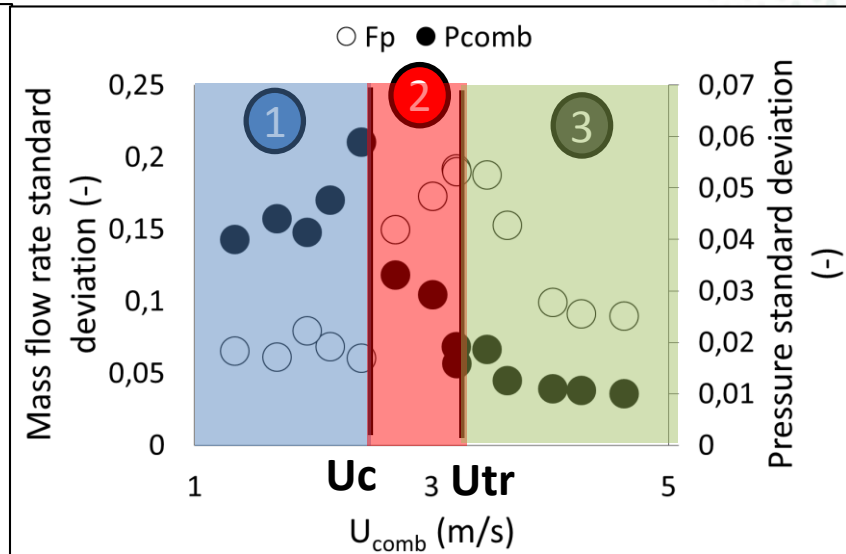
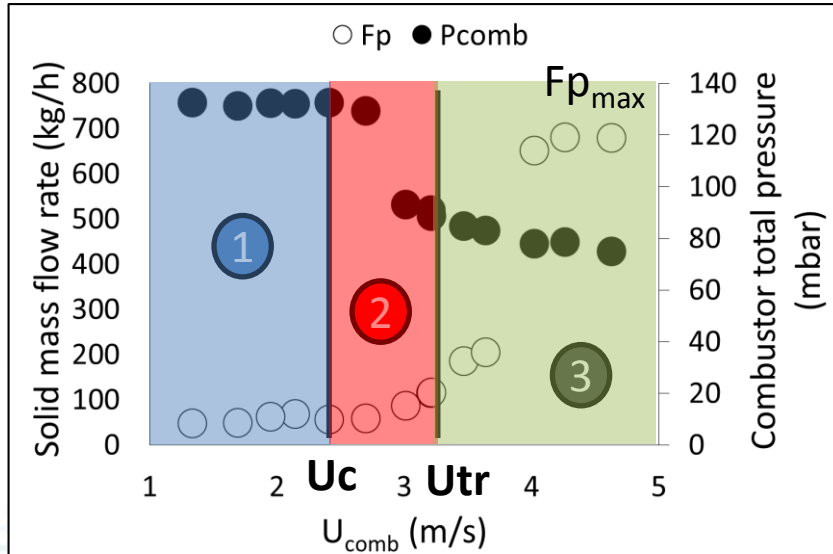
- 1) Dense fluidized bed regime
- 2) Turbulent (transition) bed regime



# II. HYDRODYNAMIC STUDY OF THE CFB

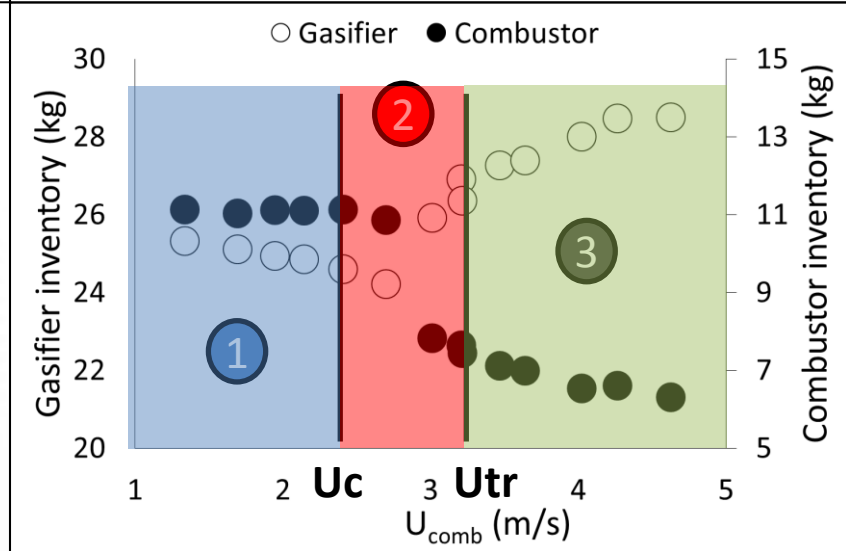
## EFFECT OF THE GAS VELOCITY $U_{comb}$ :

3 Transported bed



Three hydrodynamic regimes identified in the combustor :

- 1) Dense fluidized bed regime
- 2) Turbulent (transition) bed regime
- 3) Transported (circulating) bed regime

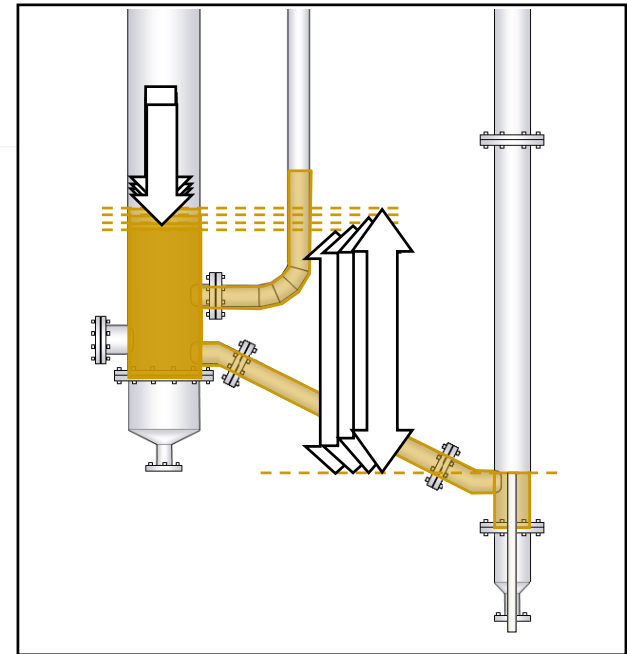


# II. HYDRODYNAMIC STUDY OF THE CFB

## EFFECT OF THE SOLID INVENTORY :

$$H_{\text{cane}} = 15 \text{ cm} = H_{\text{comb}}$$





➤ When  $m_p$    $H_{\text{Gasifier}}$  

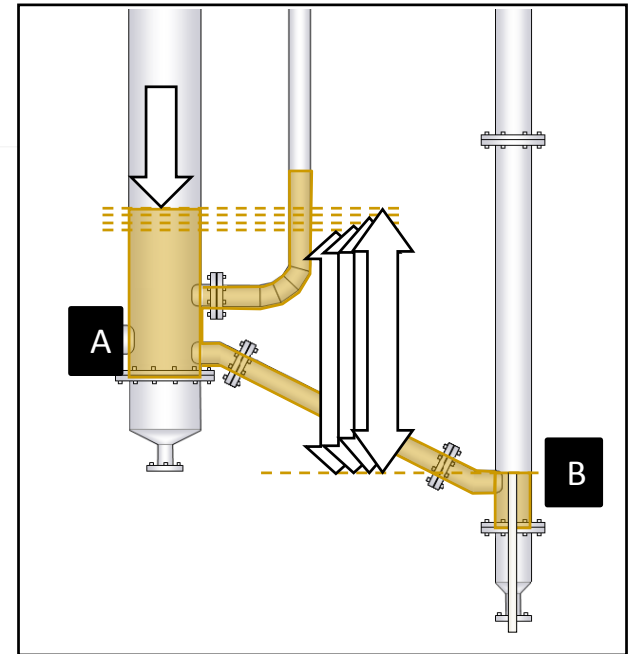




## EFFECT OF THE SOLID INVENTORY :

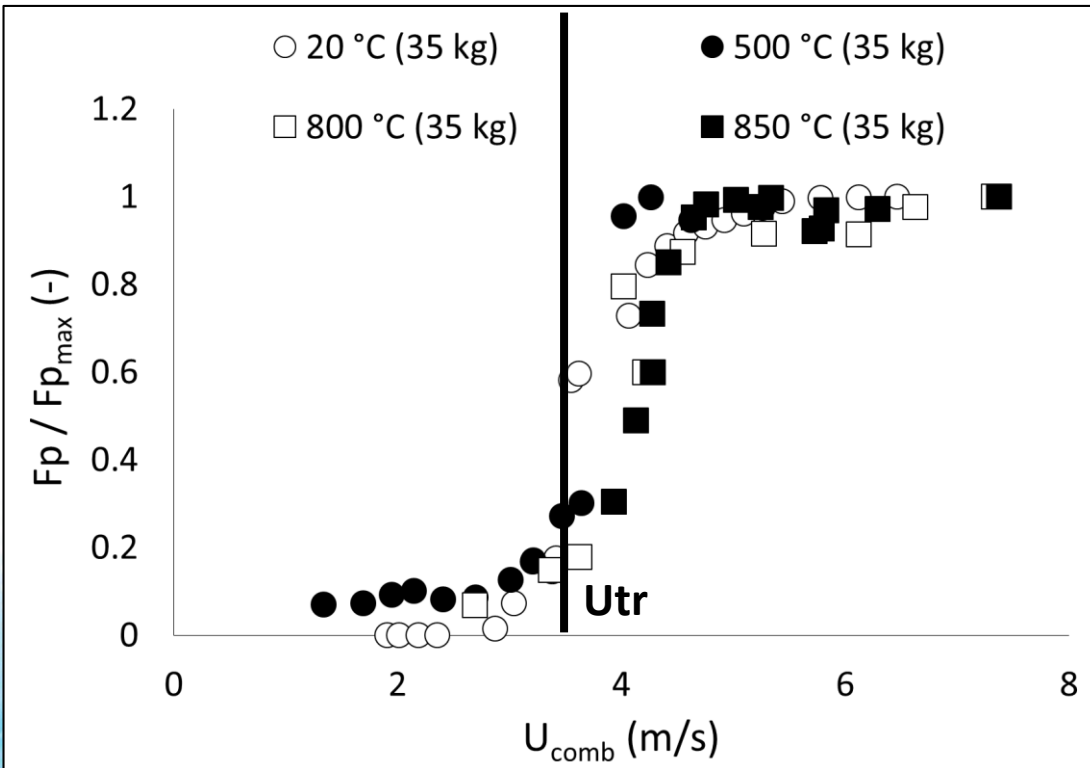
$$H_{\text{cane}} = 15 \text{ cm} = H_{\text{comb}}$$

- When  $m_p$    $H_{\text{Gasifier}}$  
- $\Delta P$  between A and B (driving force of the circulation) 
- $Fp_{\text{max}}$  

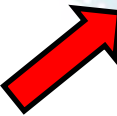


# II. HYDRODYNAMIC STUDY OF THE CFB

## EFFECT OF THE BED TEMPERATURE : 20-850 °C

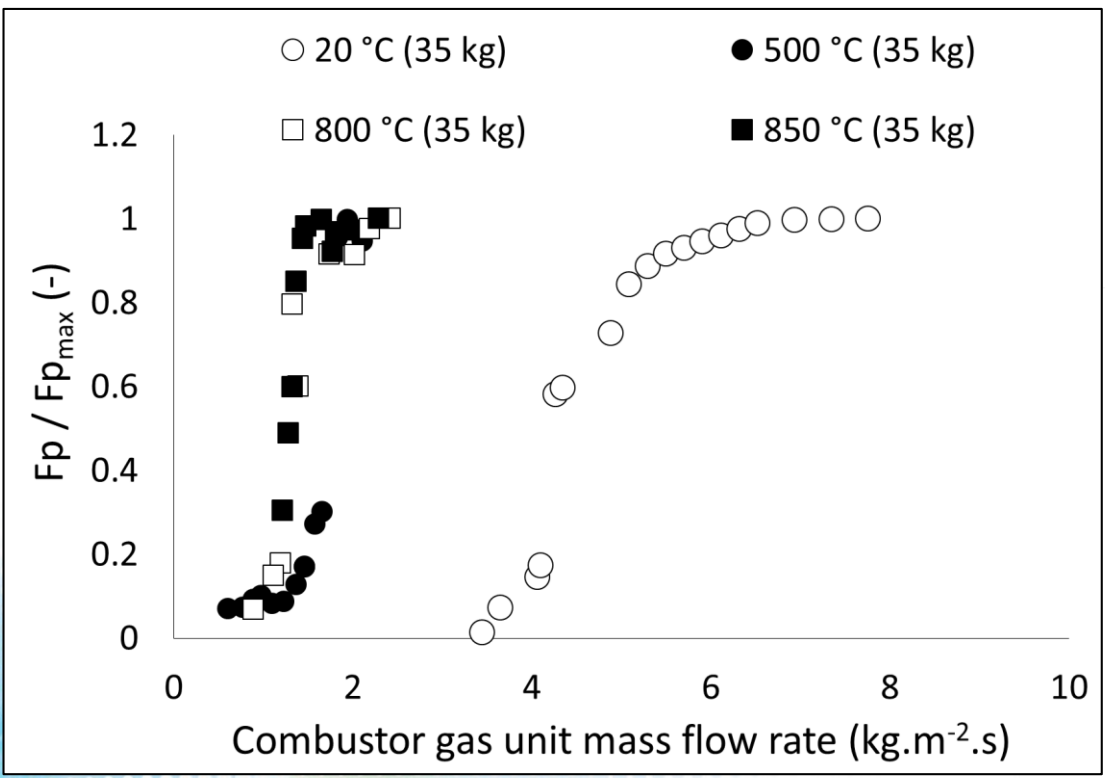


When bed temperature  
=> Low effect on  $U_{tr}$

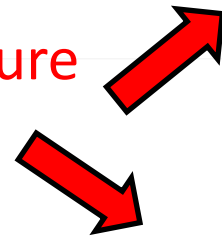


# II. HYDRODYNAMIC STUDY OF THE CFB

## EFFECT OF THE BED TEMPERATURE : 20-850 °C

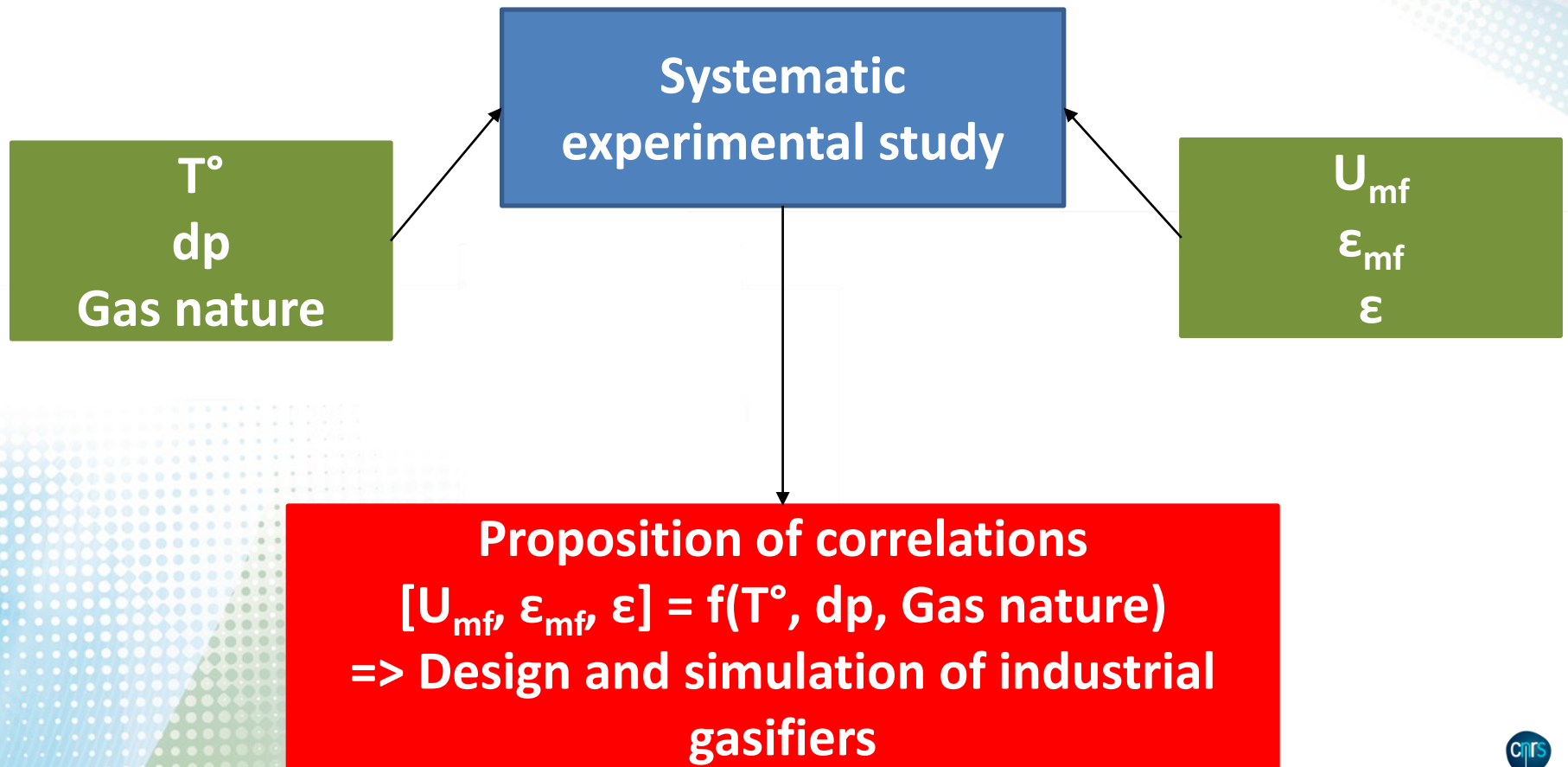


When bed temperature  
=> Air consumption



# CONCLUSION

- Dense fluidized bed tests (20 – 950 °C)





# CONCLUSION

- Circulating fluidized bed tests (20 – 850 °C)



Hydrodynamic regimes in the combustor :  
3 between dense fluidized bed and transported bed



3 key parameters : gas velocity  $U_{comb}$ , solid inventory and bed temperature

For  $U_{comb}$  and solid inventory

Circulating solid flow rate

For bed temperature

Air consumption

**Thank you for your  
attention**