# ConocoPhillips

#### Aqueous Amine Absorption: Experimentation and Modeling

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## Motivation



Source: Energy Information Administration, 2005

- Reduce CO<sub>2</sub> capture costs
- Flue gas units will dwarf acid gas treaters
- Precise sizing requires accurate mass transfer data
- No existing data for aged solvents
- Packing requires rate-based modeling
- Significant energy savings in the regenerator

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#### **Aqueous Amine Absorption**



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#### **Capture Costs**



#### Wetted-Wall Column



#### **Mass Transfer with Chemical Reaction**



#### **Experimental Technique**



#### Gas Film Calibration and Benchmark

![](_page_7_Figure_1.jpeg)

<sup>\*</sup>Dugas, R., G. Rochelle, "Absorption and desorption rates of carbon dioxide with monoethanolamine and piperazine," *Energy Procedia*, 1163-1169, 2009.

![](_page_8_Picture_0.jpeg)

- Most designs based on fresh solvents
- Effect of degradation components unknown

 $k_l$  fresh (mol/s m² Pa) $k_l$  aged (mol/s m² Pa) $3.7 \times 10^{-6}$  $3.1 \times 10^{-6}$ 

![](_page_8_Picture_4.jpeg)

#### **Modeling Results**

• Non-equilibrium, Aspen Hysys model

 Model compares favorably to literature (30 wt.% MEA)

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CO <sub>2</sub> Capture (%)	90.1	90.1
Regen. Energy (MJ/kg CO <sub>2</sub> )	13.8	15.9
Solvent Circulation (L/s)	2638.9	2639.4
Absorber Packing Height (m)	15.0	15.0
Regenerator Packing Height (m)	10.0	10.0
Lean CO <sub>2</sub> Loading (mol CO <sub>2</sub> /mol alk.)	0.28	0.25
Rich CO <sub>2</sub> Loading (mol CO <sub>2</sub> /mol alk.)	0.48	0.46

![](_page_9_Picture_4.jpeg)

## **Conclusions and Future Work**

- Accurate experimental data required for proper design of CO<sub>2</sub> capture systems
- Kinetic information of aged systems needed to predict real performance
- Incorporate kinetic data into rate-based models

![](_page_10_Picture_4.jpeg)

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#### Acknowledgements

- Luminant Carbon Management Program
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![](_page_11_Picture_4.jpeg)

# **Questions?**

![](_page_12_Picture_1.jpeg)