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# The Next Steps for Ultra-High Temperature Ceramics

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# The Next Steps for UHTC Materials

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Ultra-High Temperature Ceramics for Extreme Environment Applications II

May 14, 2012

Hernstein, Austria

## Background

Why UHTCs?

Current research & development focus

Systems Needs/Designers Phobias – are UHTCs getting a bad reputation?

How to integrate into structure?

Catastrophic Failure

Long-term applications - oxidation

What needs to be done?

New Processing Technologies

Testing in Relevant Environments

## Why UHTCs?

What does a UHTC need to do:

- Carry engineering load at RT - ✓
- Carry load at high use temperature
- Respond to thermally generated stresses (coatings)
- Survive thermochemical environment - ✓

High Melting Temperature is a major criteria, but not the only one  
Melting temperature of oxide phases formed  
Potential eutectic formation

Thermal Stress –  $R' = \sigma k / (\alpha E)$

Increasing strength helps, but only to certain extent

Applications are not just function of temperature

- **Materials needs for long flight time reusable vehicles are different that those for expendable weapons systems**

In many aerospace systems, designers will add weight and complexity by using metals and active fuel cooling to avoid using advanced ceramics and composites.

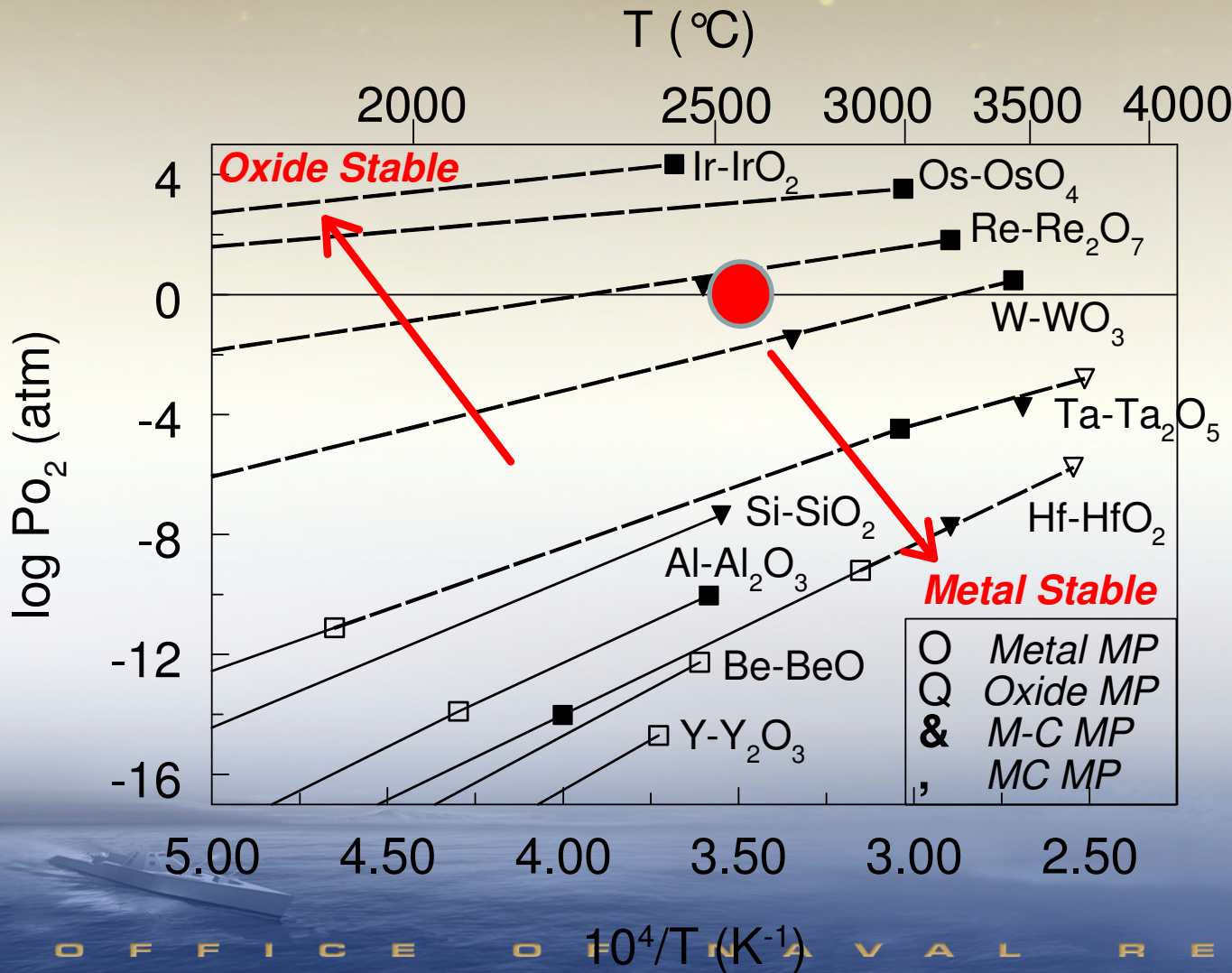
- Direct function of the conservatism engrained in industry and the system integrator being contracted to build a system and not demonstrate a materials technology
- Unfamiliarity with designing with brittle materials - safety factor.
- Advantages of weight savings and uncooled temperature capability not high enough to overcome risk aversion

Using monolithic ceramics and CMC requires a different design approach, not just dropping in a ceramic part to replace a metallic component

- Rocket nozzle examples – learning how to use a brittle material in a highly transient heating environment

Need for subscale materials/component testing in realistic environments is imperative

**Onus is on US to develop materials that will be used by designers**

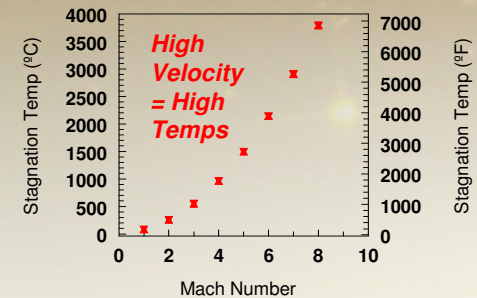


- Metallurgical Thermo tools employed
- Lines divide stability regions of metal vs condensed metal oxide
- Each element shown is best representative of Group (eg., Ta-Nb-V)
- Each element is also representative of compounds (HfC, HfN, HfB<sub>2</sub>, HfO<sub>2</sub>, etc.)
- So what ????
- How is this useful ????

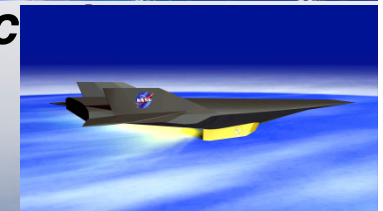
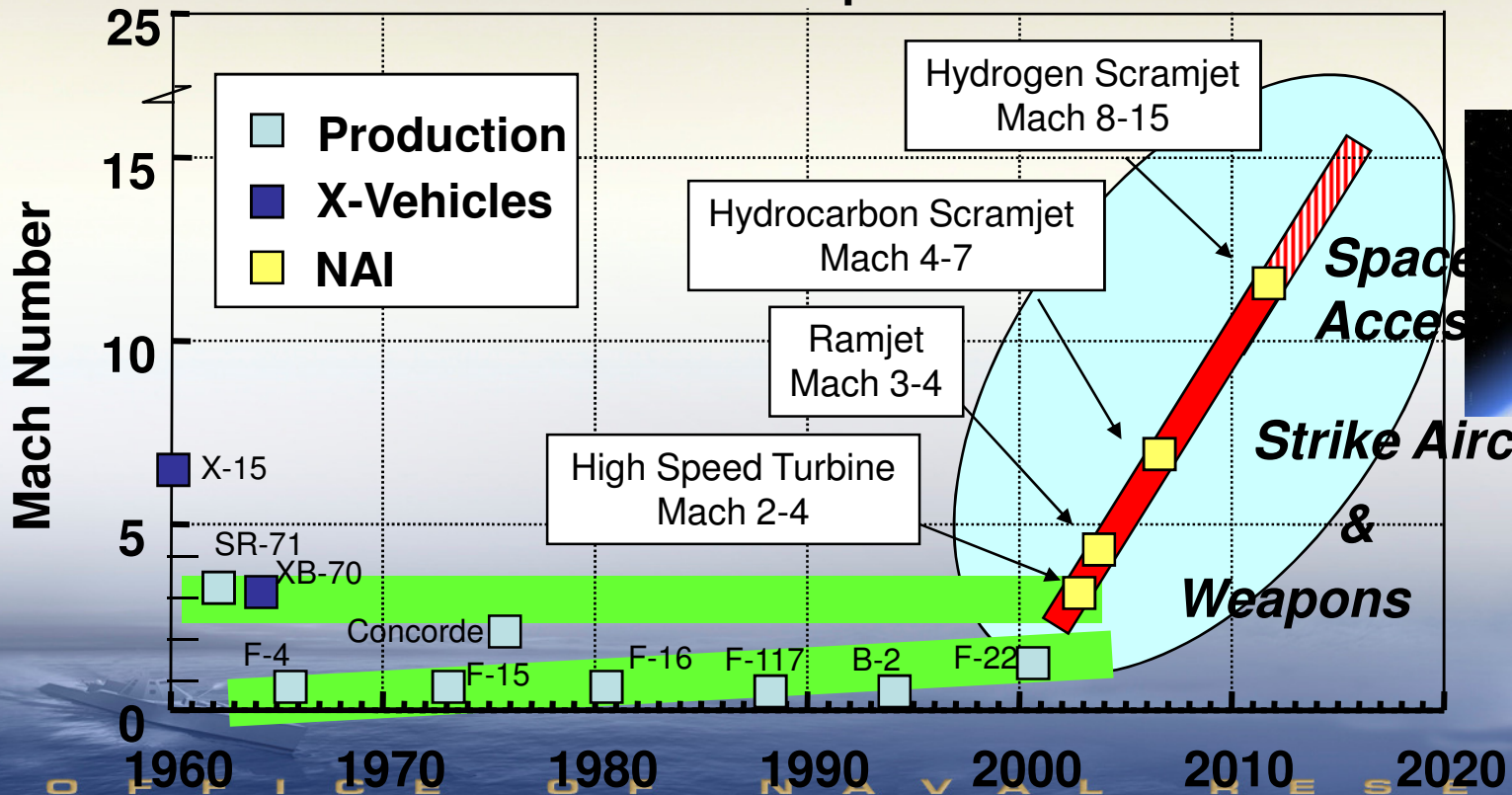
# Current research vs future directions

- Increase strength - SPS (engineers don't like lack of toughness)
- Increase thermal conductivity ( $\text{HfB}_2$  is already very high)
- Decrease modulus (graphite second phases, but eutectic issue)
- Decrease thermal expansion (intrinsic property)
- Design around thermal stresses – rocket nozzles (ONR & AFRL)
- **Understand and improve oxidation behavior – why SiC?**
- **Develop UHTC-matrix composites – hot pressing, SPS, HIP, all produce bulk monolithic materials.**
  - Modulus/CTE mismatch w/ C fibers a problem
  - Current polymeric precursors - expensive and air sensitive
  - Organometallics
  - Melt infiltration – refractory alloys reactive with fibers
  - Densification/conversion of matrix
  - Alternative Processing routes (CVC, in-situ reinforcement, cermets)

**High Operational Velocities**  
 ⇒ **High Temps & Heating Rates**



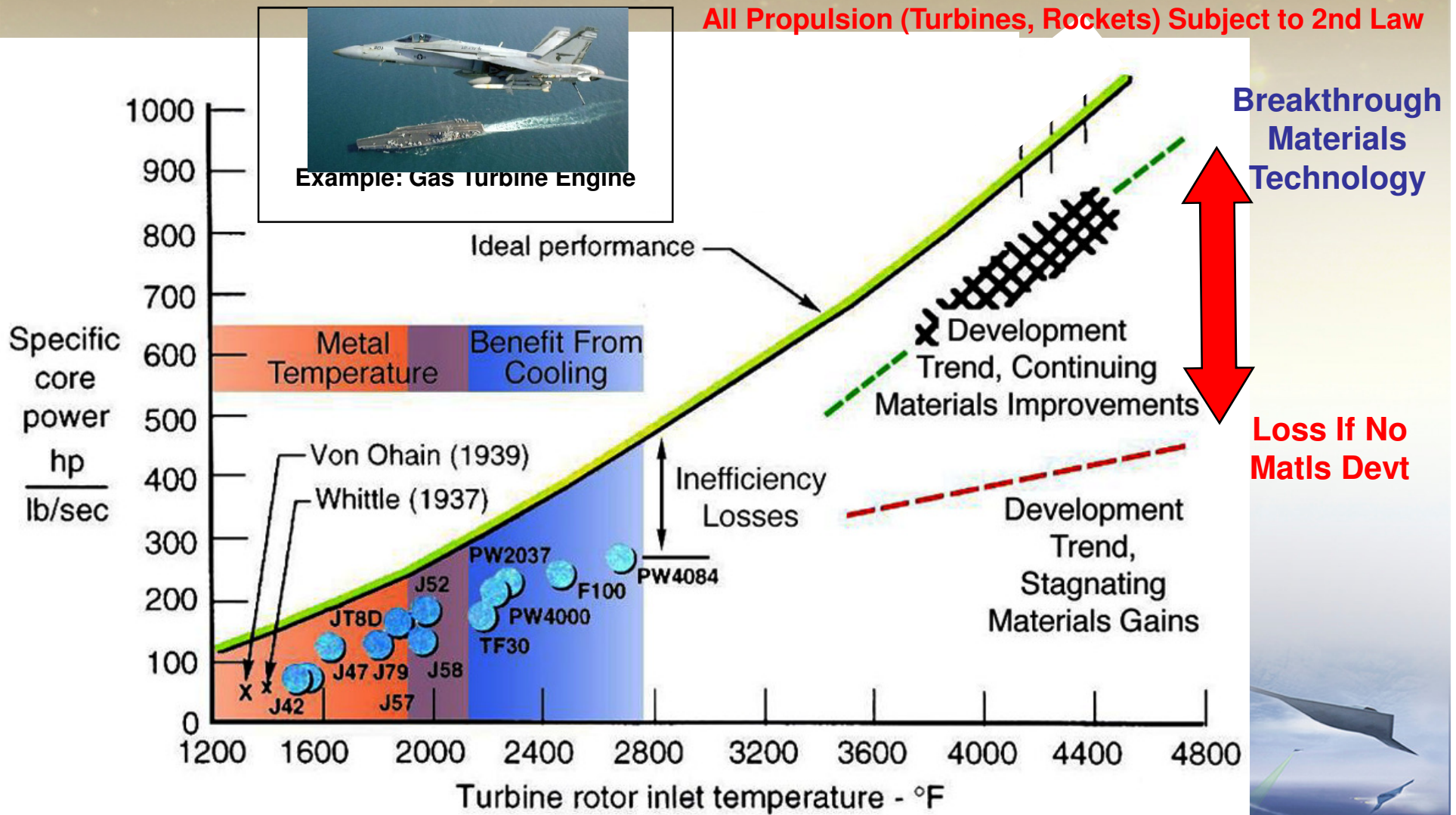
**NAI : One Mach Number per Year to 2012**





## Higher Operating Temps Yield Higher Engine Performance

All Propulsion (Turbines, Rockets) Subject to 2nd Law



**High speed = High T**

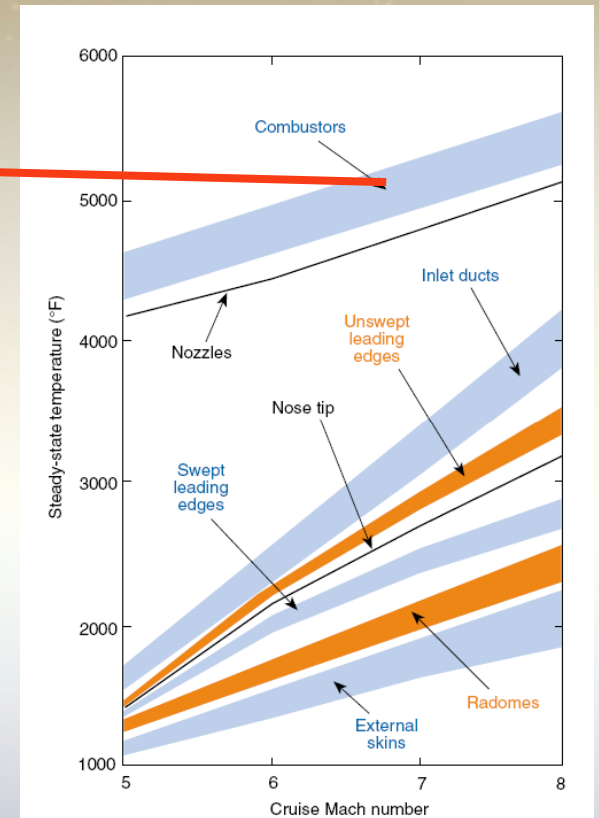
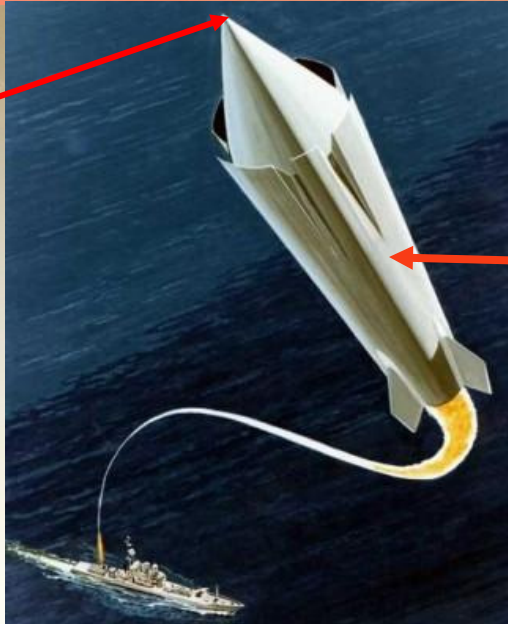
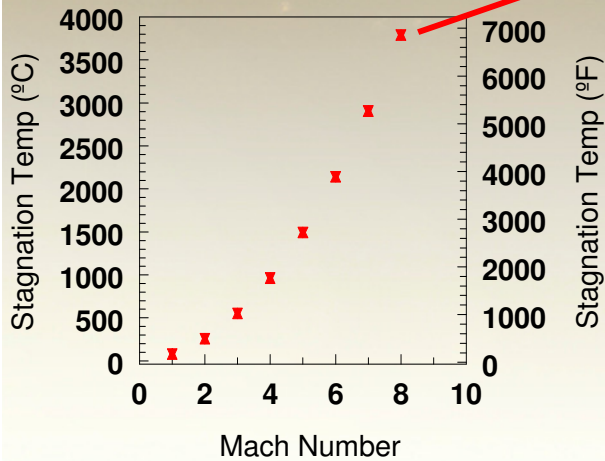
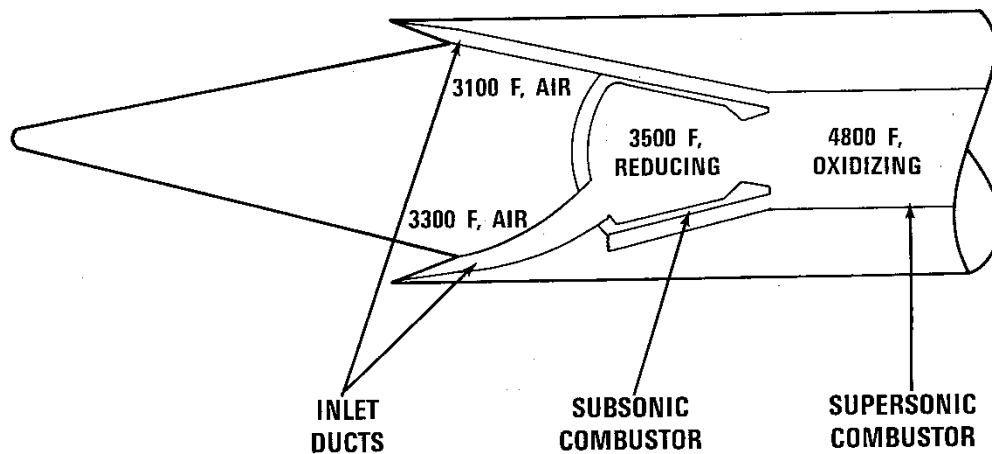
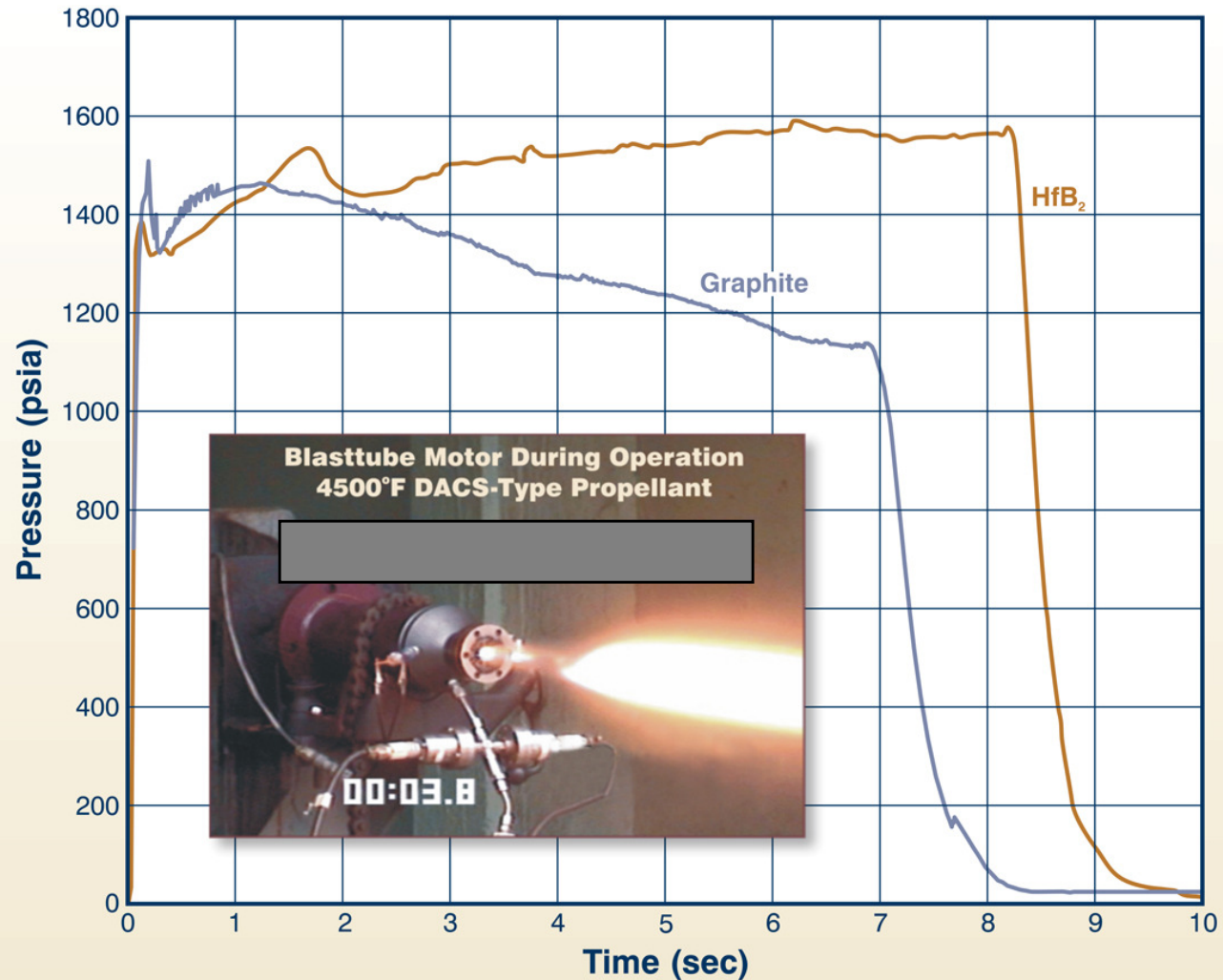


Figure 5. Steady-state temperature versus cruise Mach number for critical components at an 80,000-ft altitude.



# Pressure-Time Traces of Graphite & HfB<sub>2</sub> Throats Showing Non-eroding Behavior of Ceramic Nozzle



### Small Nozzle Example

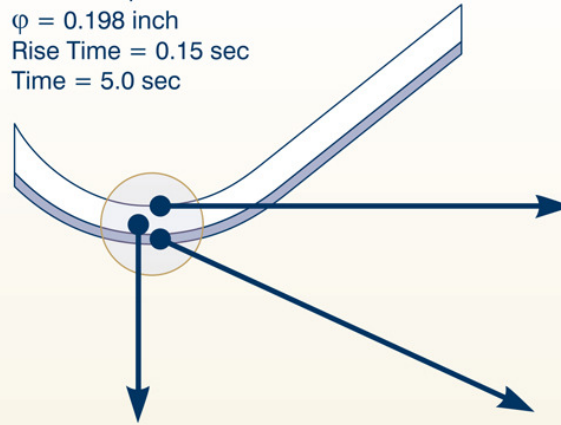
$T_o = 4400^\circ\text{F}$

$P_o = 1500 \text{ psi}$

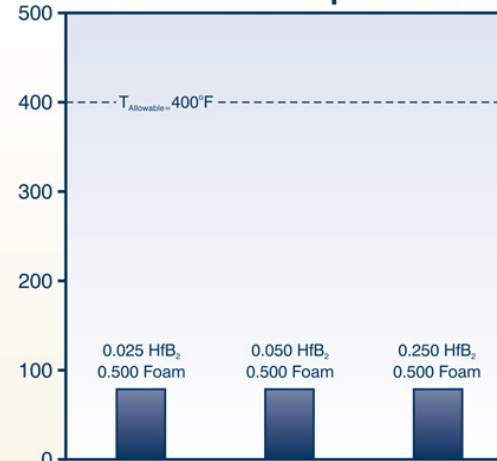
$\phi = 0.198 \text{ inch}$

Rise Time = 0.15 sec

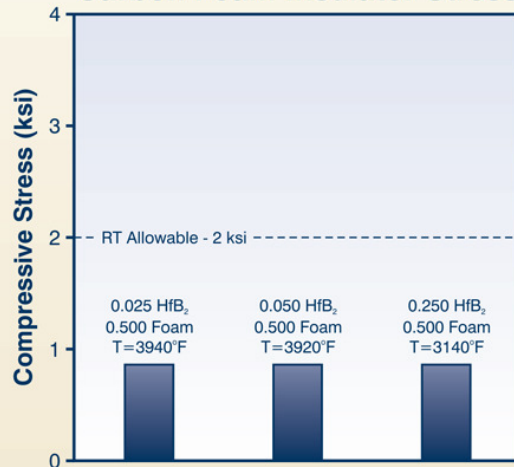
Time = 5.0 sec



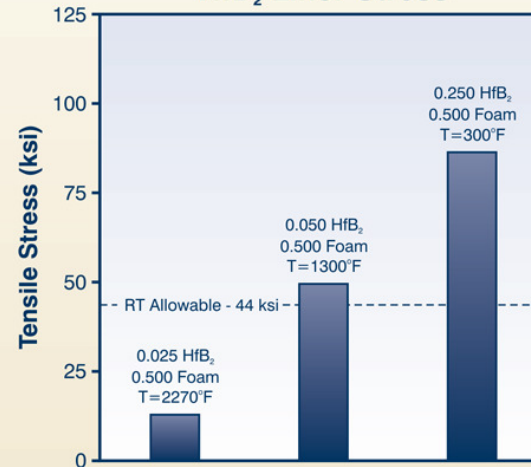
### Backface Temperature



### Carbon Foam Insulator Stress



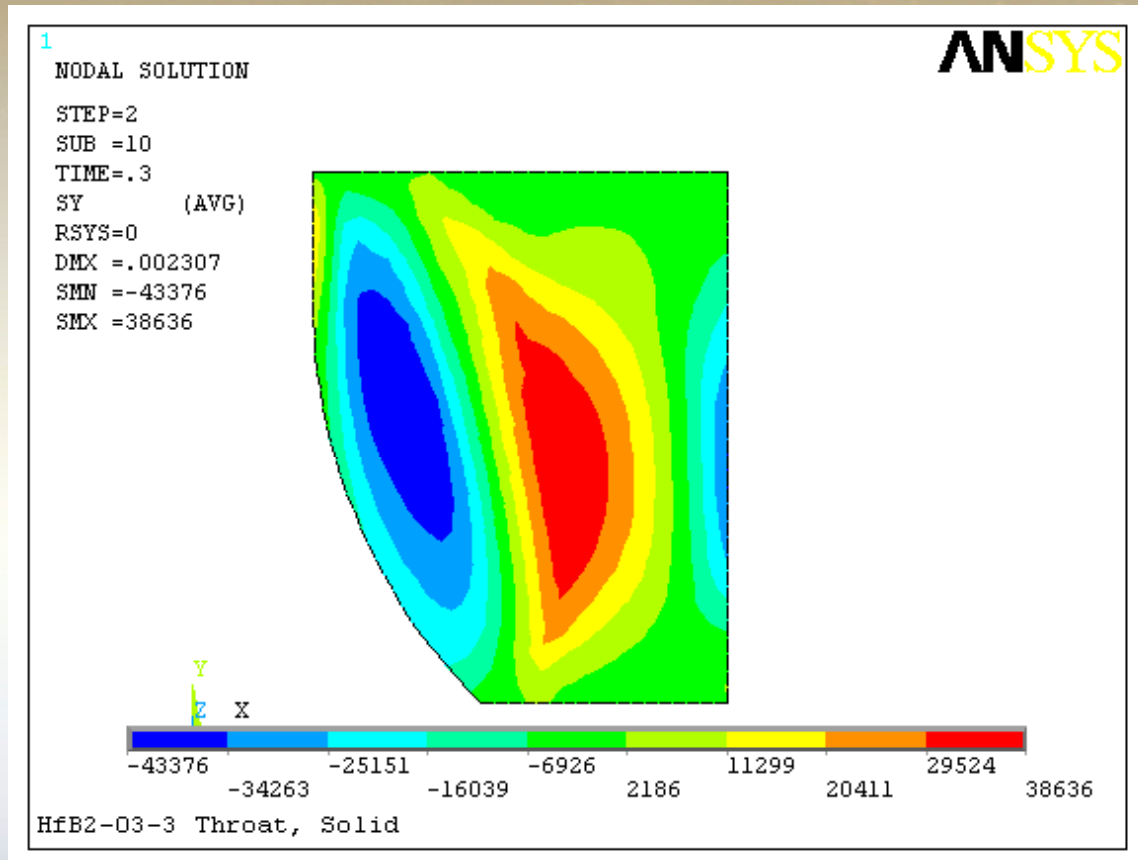
### HfB<sub>2</sub> Liner Stress



C-foam provides insulation and allows expansion of liner

# THERMALLY GENERATED STRESSES

## Solid HfB<sub>2</sub> Throat

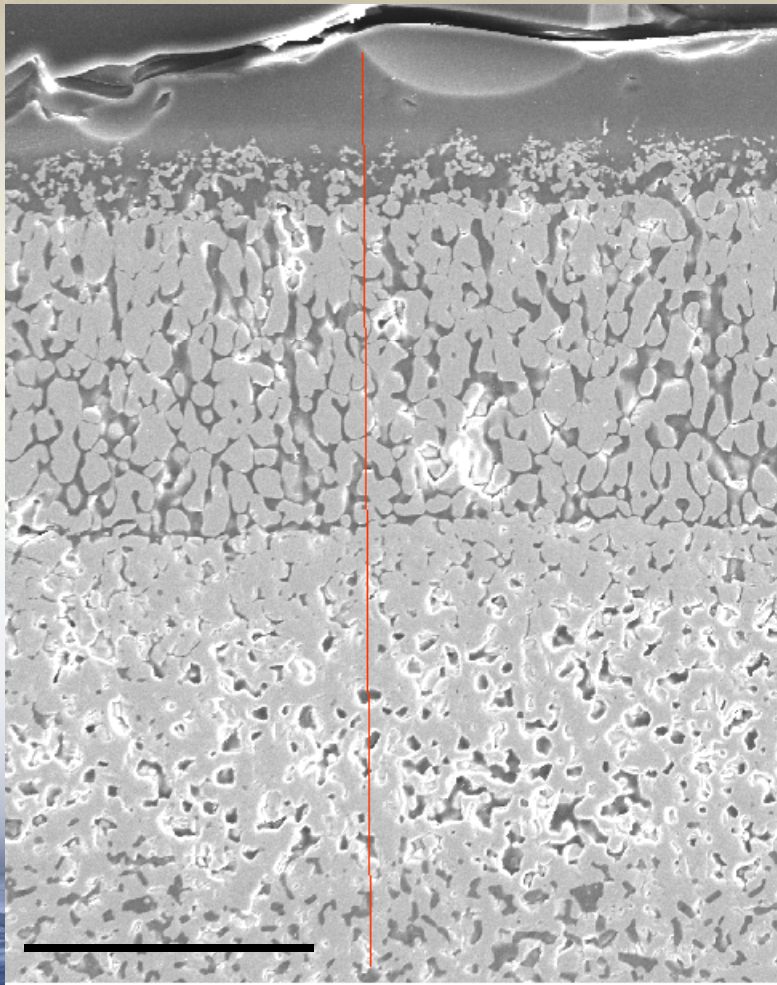


Similar Axial Stress Fields Have Been Observed  
In Previous Analysis Efforts

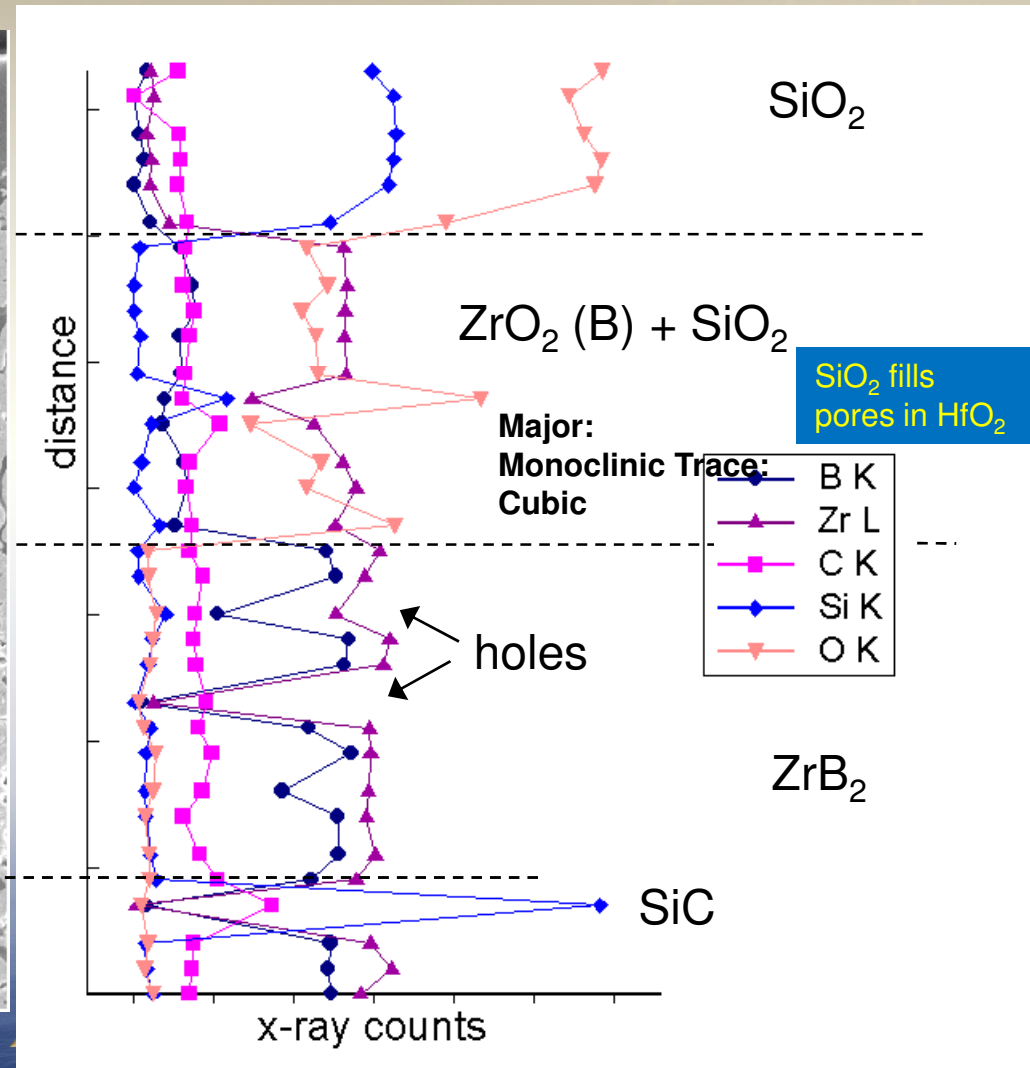
**Maybe the models are too conservative in  
predicting thermal stress failures?**

**(1627C not high enough!)**

Ref: Evaluation of Ultra High Temperature Ceramics for Propulsion Application
   
 S.R. Levine, et al., NASA Glenn Res. Ctr, ACerS PacRim Conf., Seattle, WA, 01 Nov 2002



100 μm

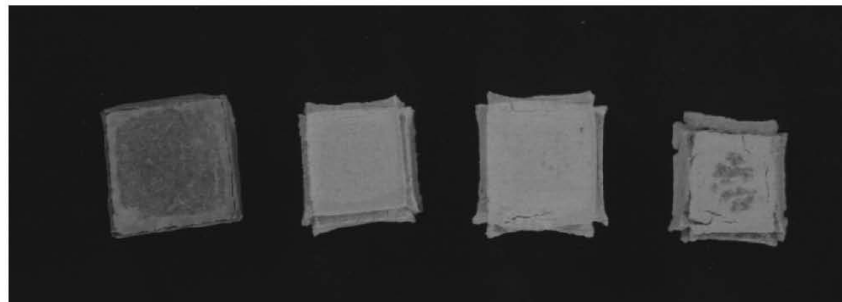
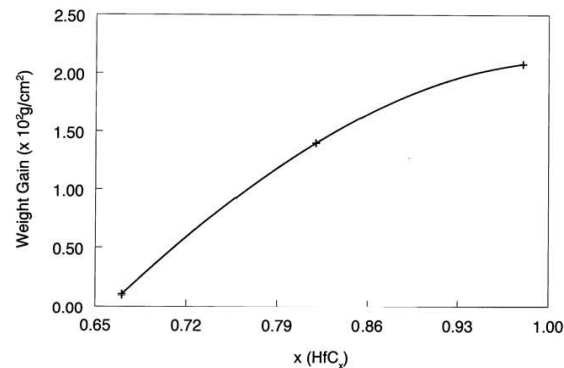
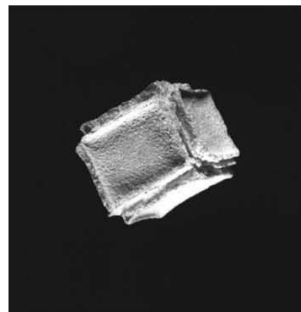


# Borides are not the only UHTC Materials

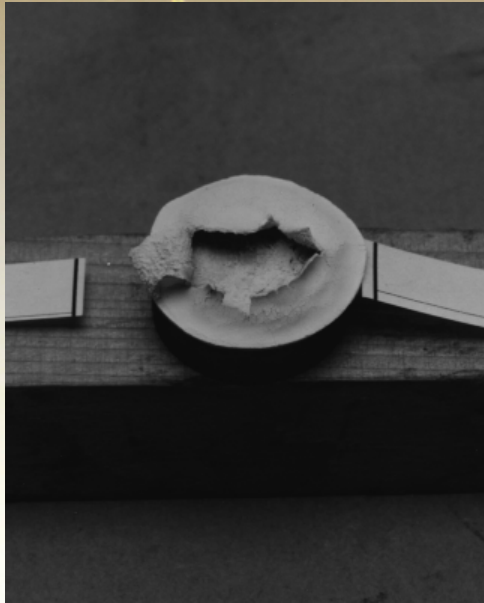
Boria has high Pv, SiC active oxidation, and  $\text{HfO}_2$  does not sinter below  $1800^\circ\text{C}$ , so oxidation behavior **improves** with temperature

## Furnace Testing of HfC – $1500^\circ\text{C}$

Pesting Issues at Low T – Sinterability of  $\text{HfO}_2$



# Arc-jet tests help understanding thermochemical environment

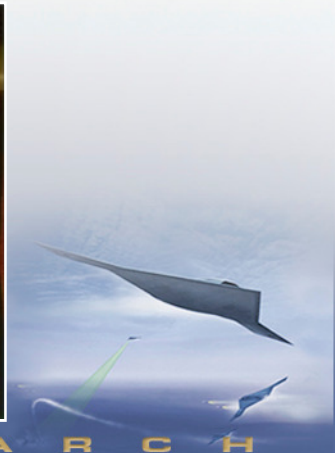
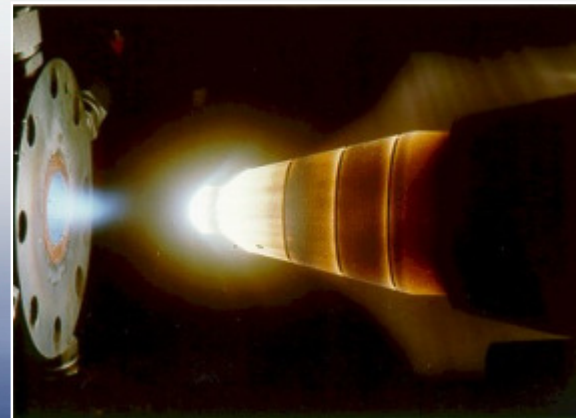


**HfN<sub>.75</sub>**



**HfN<sub>.95</sub>**

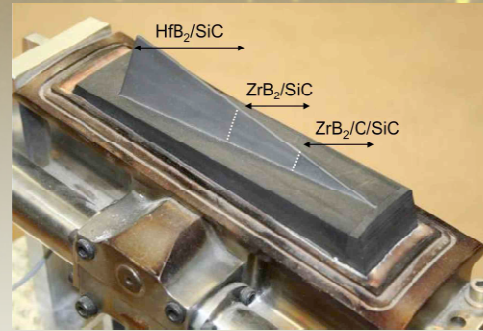
**But sample geometry (radius of curvature), enthalpy, catalycity, and pressure all affect performance**





# Relevant Testing Can be Enlightening – and Scary

- ◆ **SHARP-B2 UHTC flight test [Sannes, 9 and Johnson, 10]**
  - Very progressive & expensive
  - Failure attributed to UHTC processing



Pre-test



Post-test

Slide from D. Glass, NASA-Langley



- ◆ **ZrB<sub>2</sub>-SiC nose tip during arc-jet test [Marino, 11].**
  - Failure attributed to titanium screw [12].

Second assembly withstood two test at 3 MW/m<sup>2</sup> for 108 sec. Non-critical damage observed at base of UHTC tip. [Scatteia, 12]

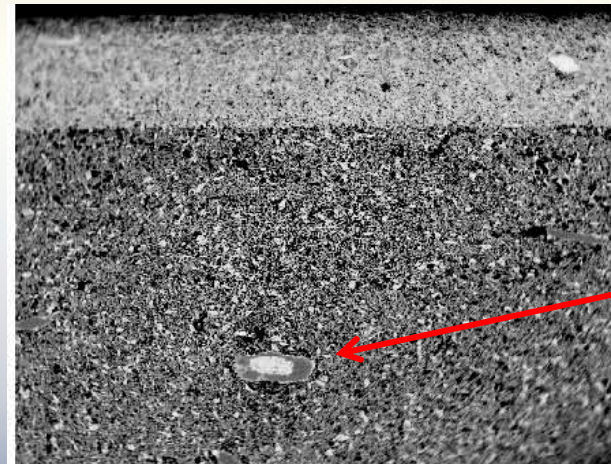
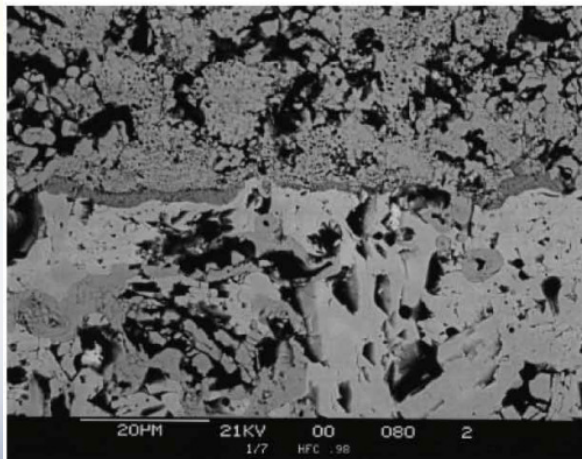
Affecting future of Italian UHTC work?

Even in constrained 1-D heating environment for oxidation testing, **low thermal shock resistance** and **low fracture toughness** of **monolithic ceramics** can result in catastrophic failure

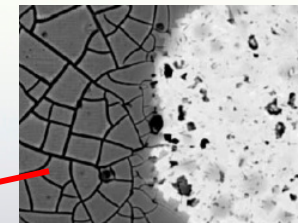
# Improve oxidation behavior

- Eliminate presence of Si - detrimental above 1700 °C
- Test in relevant environments
- Dopants to control oxygen diffusion through oxide scale
- Decrease porosity of scale
  - Substoichiometry & Doping – Wuchina & Opeka
  - Liquid phase sintering – Fahrenholtz & Hilmas

HfCxOy  
Interphase



WO<sub>3</sub>  
formation



Careful on effects on high-temperature strength

Hf, Ta: **Linear** Oxidation Kinetics at High Temperature (HT)

Hf-20Ta: **Parabolic** Kinetics to 2000°C with strongly adherent scale (Marnoch, 1965)

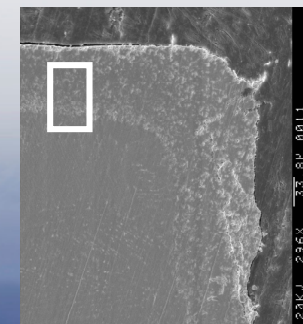
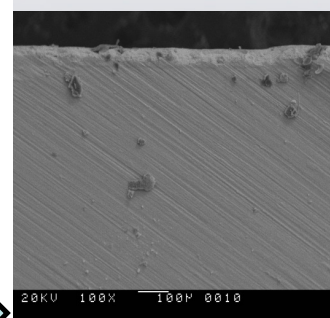
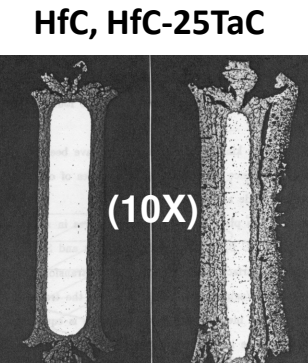
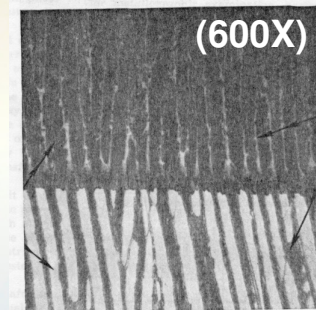
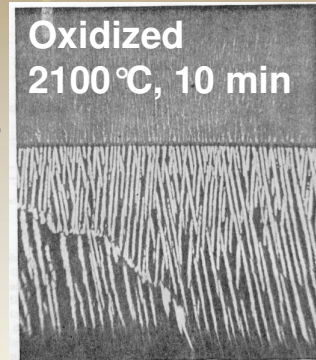
HfC-25TaC: **Linear** Kinetics at HT (Holcomb, 1988)

HfB<sub>2</sub>-20TaB<sub>2</sub>: **Linear** Kinetics at HT (Talmy, unpublished)

(Hf,Ta)N<sub>x</sub> Ceramics:  
Not Investigated To-Date;  
Initial Navy Expts Conducted with HfTa alloys

Hf20Ta:

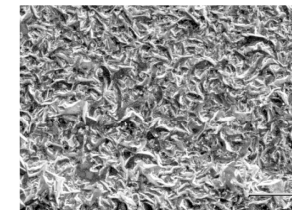
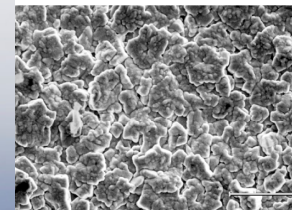
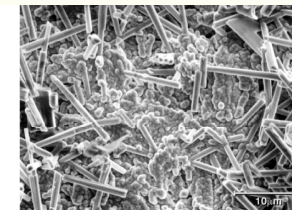
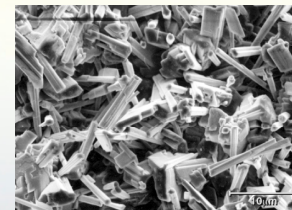
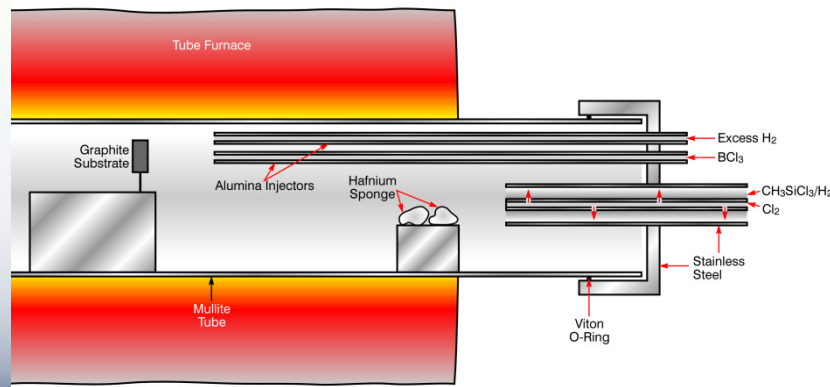
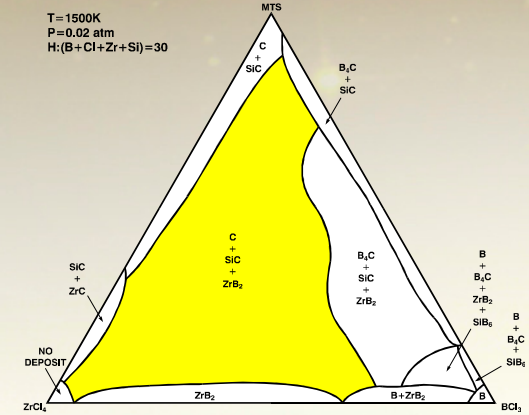
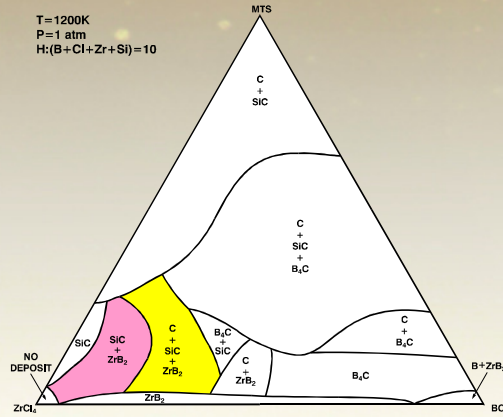
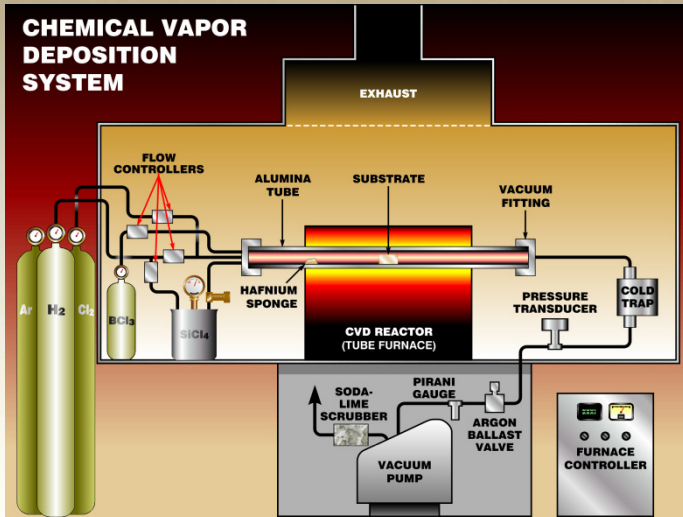
HfO<sub>2</sub> columnar morphology in alloy & oxide



Hf27Ta:

Oxidized at 1500C, 15 minutes; Oxide scale thickness ≈ 50 µm

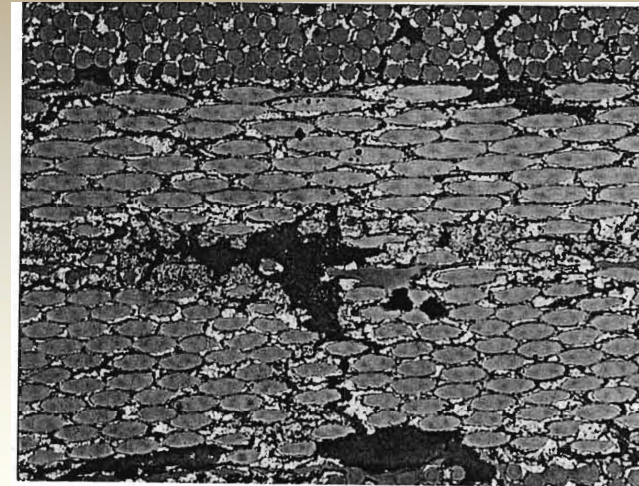
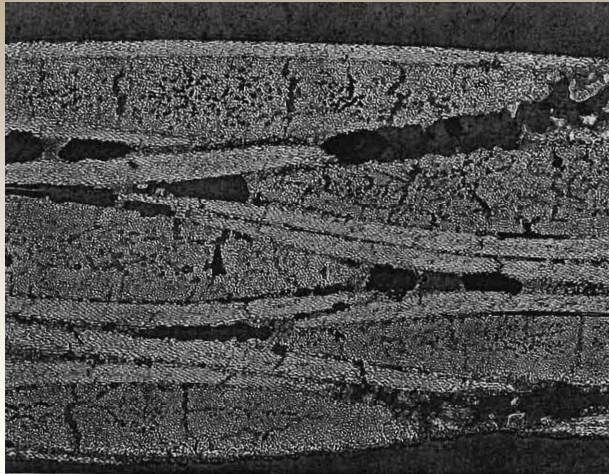
# Alternative Processing Techniques



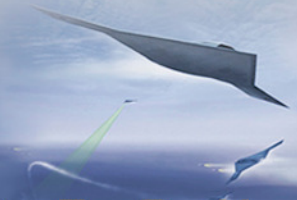
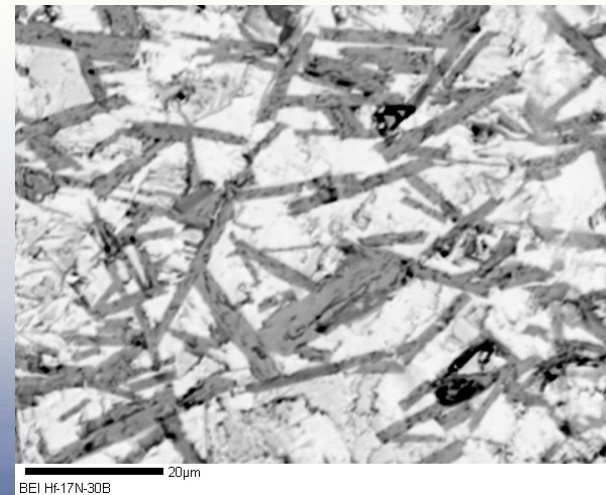
CVD not a panacea, but shows possibilities

# UHTC-matrix composite – ca 1997 and Hf-HfN-HfB<sub>2</sub> cermet

Hf acetate + C, CVI, C/C late stage PIP or gas infiltration, nano HfC



X-51 Inlet leading edge was follow-on to work initiated in late 1990s through SBIR



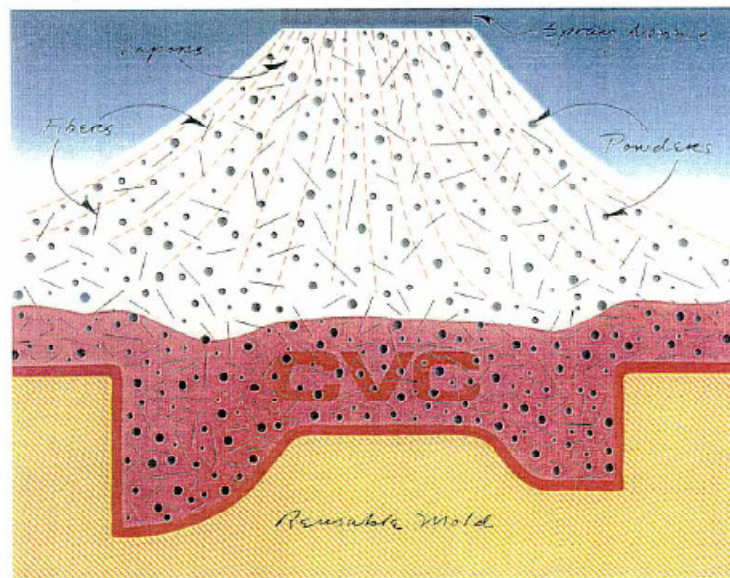
# Chemical Vapor Composites

## CVD with Particulate or fiber reinforcement



## Chemical Vapor Composites

Powders and fibers are mixed with reactant vapors and deposited on a reusable mold, producing a composite in the exact shape of the component



### LOW COST

- Single step
- High deposition rate
- Net shape

### HIGH QUALITY

- Strong – tough
- Lightweight
- High temperature

### VERSATILE

- Metal composites
- Ceramic composites
- Transition joints

4025-VB-1



# The Intersection of Basic Science and Engineering



Ab-initio calculations for discovery of new materials and correlation of chemical & physical models with materials by design approach for improving properties

High-fidelity analysis to understand multi-scale effects on macroscopic properties

Chemical Vapor Infiltration

**Organnometallic Precursors**

Mean Free Path

Modulus Mismatch – fiber breakage

PIP Processing

**Pre ceramic Polymer Development**

Particulate Additions – filtration

Increase Yield & Reduce Cycles

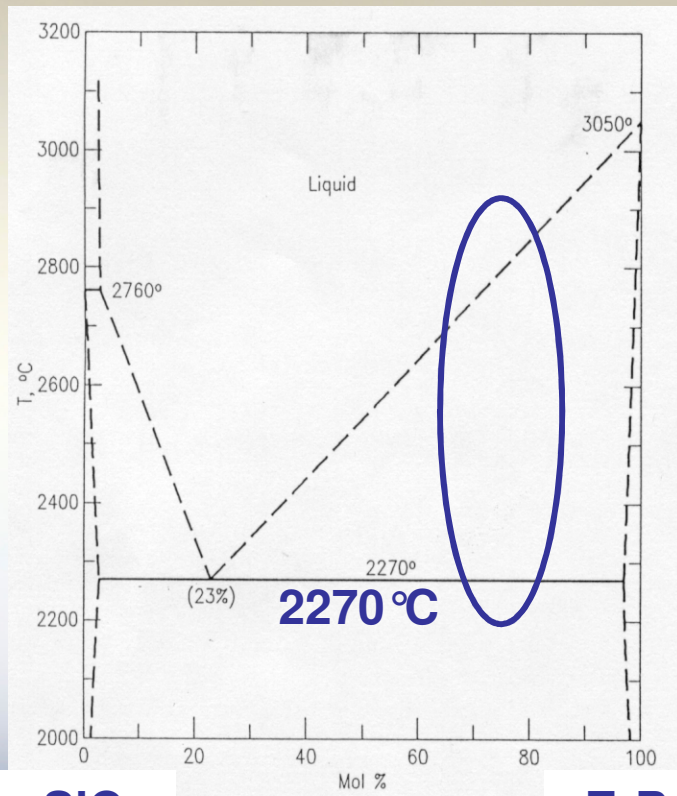
Other Techniques

Vapor Phase Conversion

UHTC fibers

SiC P C

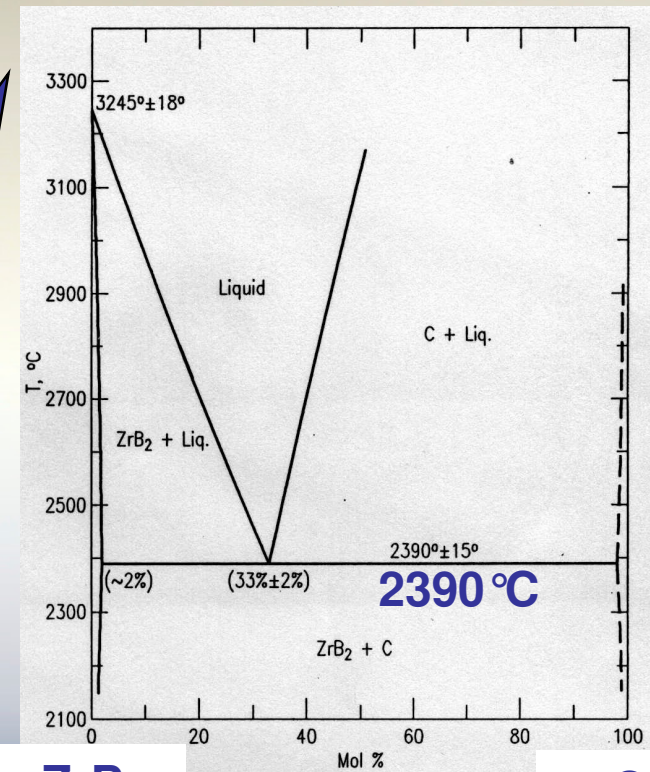
**Hard-Hard Ceramic Eutectic**



SiC

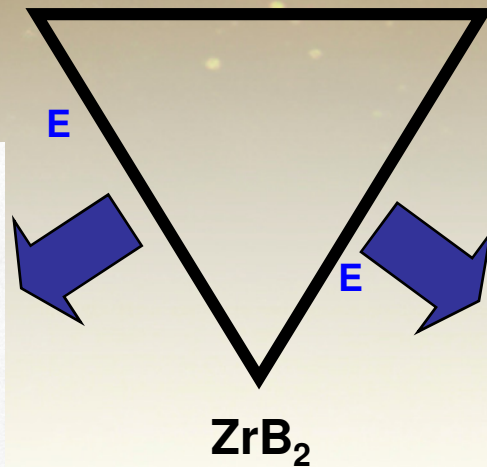
ZrB<sub>2</sub>

**Hard-Soft Ceramic Eutectic**



ZrB<sub>2</sub>

C



**Hypersonics  
Aerosurfaces:  
ZrB<sub>2</sub>-SiC (-C)  
HfB<sub>2</sub>-SiC (-C)**

*Microstructure and Property Differences Between  
Hard-Hard and Hard-Soft Ceramic Eutectics?*



## Microstructure and Properties of Ceramic-Metal Eutectics?

Eutectic Temps & Intersolubilities Vary Significantly:

HfC-W: 2890 °C,

HfN-W: 2800 °C ( $P_{N_2}$ -Dependent),

HfB<sub>2</sub>-W: 2280 °C

HfC-Ta: 2550 °C (large intersolubilities)

HfN-Ta: 2800 °C (some intersolubility)

HfB<sub>2</sub>-Ta: Reaction to (TaHf)B

Composition Control and Properties of “Metal” Phase a Major Issue for Cermet Eutectics

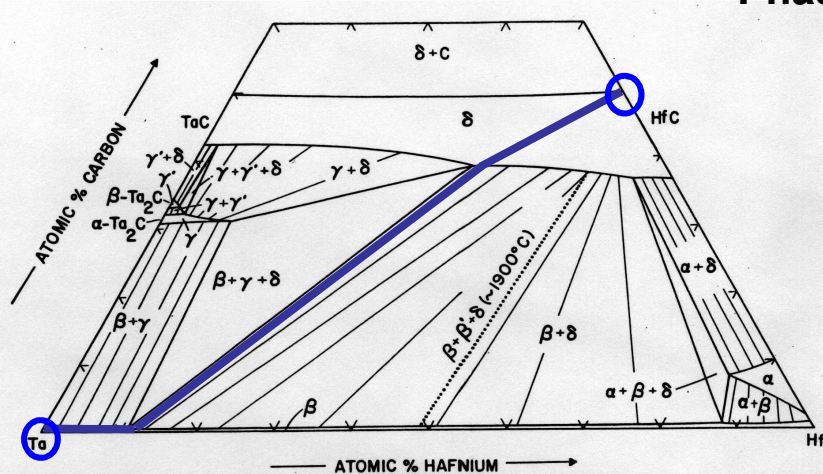
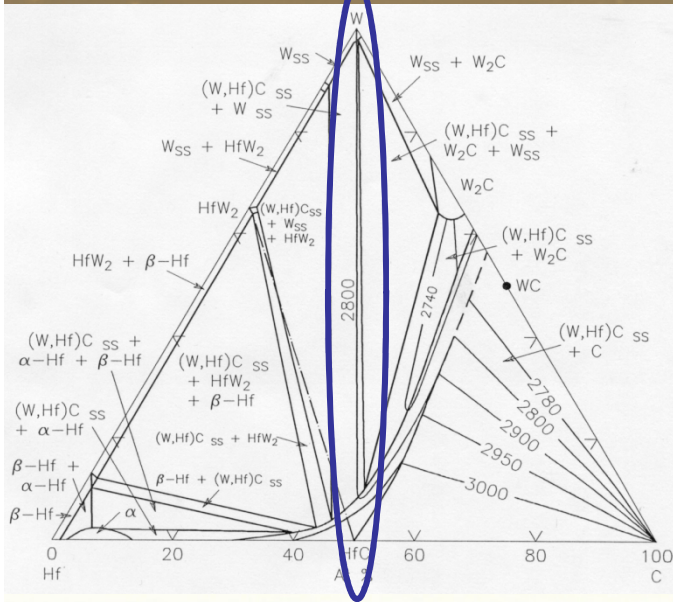


Figure III.E.9.10. Isothermal Section of the Ta-Hf-C System at 2000°C

**Non-Aluminized Propulsion:**

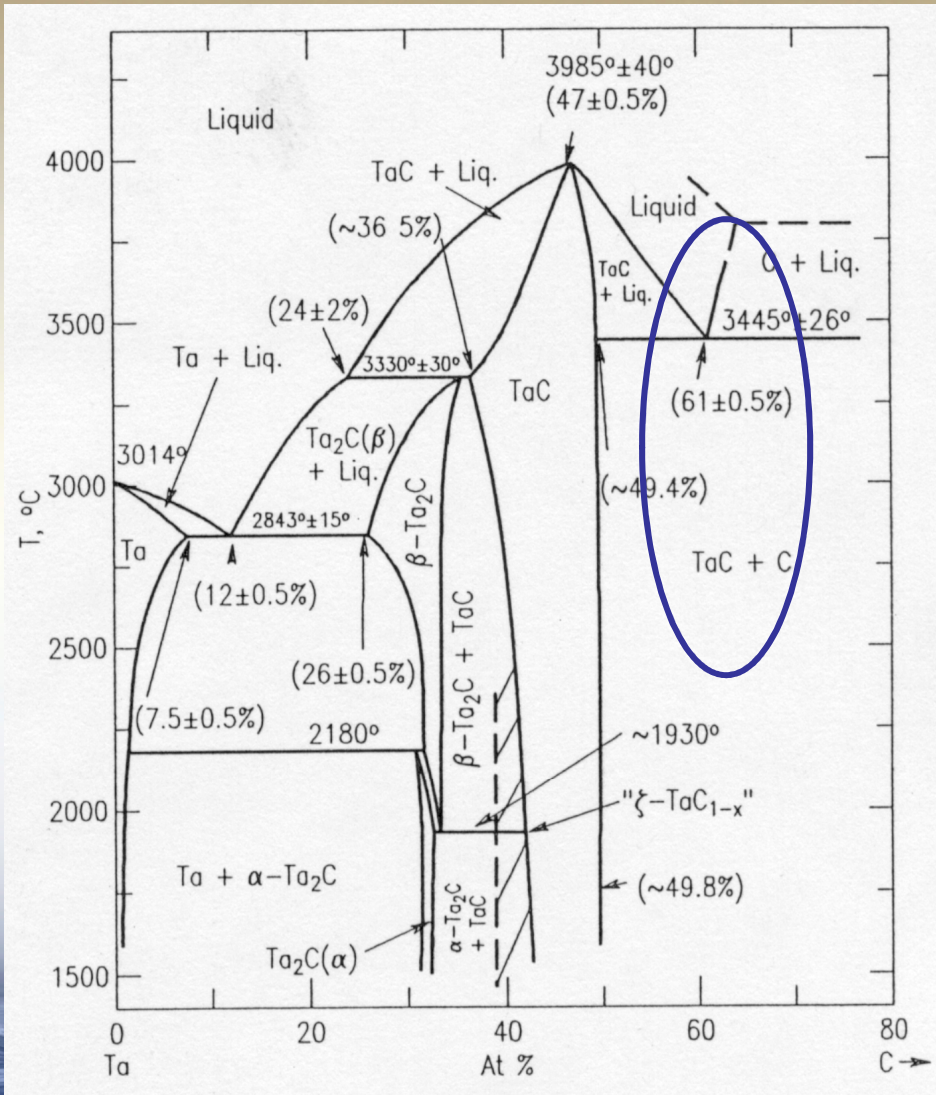
**HfC-W**

**HfN-W**

**HfC-Ta**

**HfN-Ta**

**(and ZrC, ZrN compositions)**



**Aluminized Boost Propulsion:**

**TaC-C**

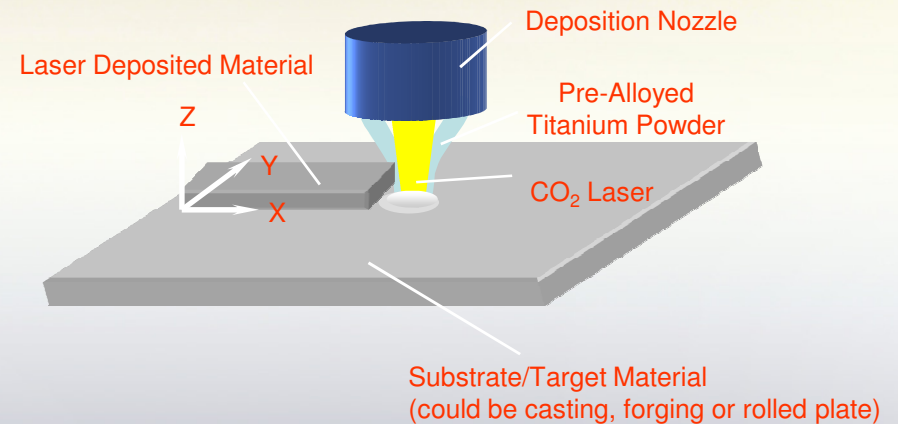
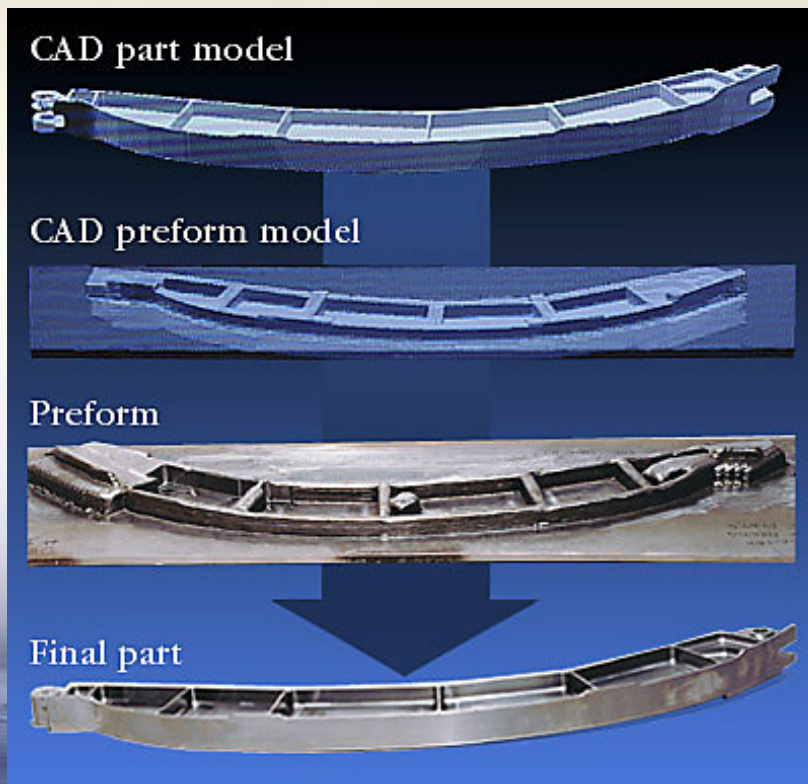
**Non-Aluminized Boost Propulsion:**

**HfC-C**

**HfN-BN**

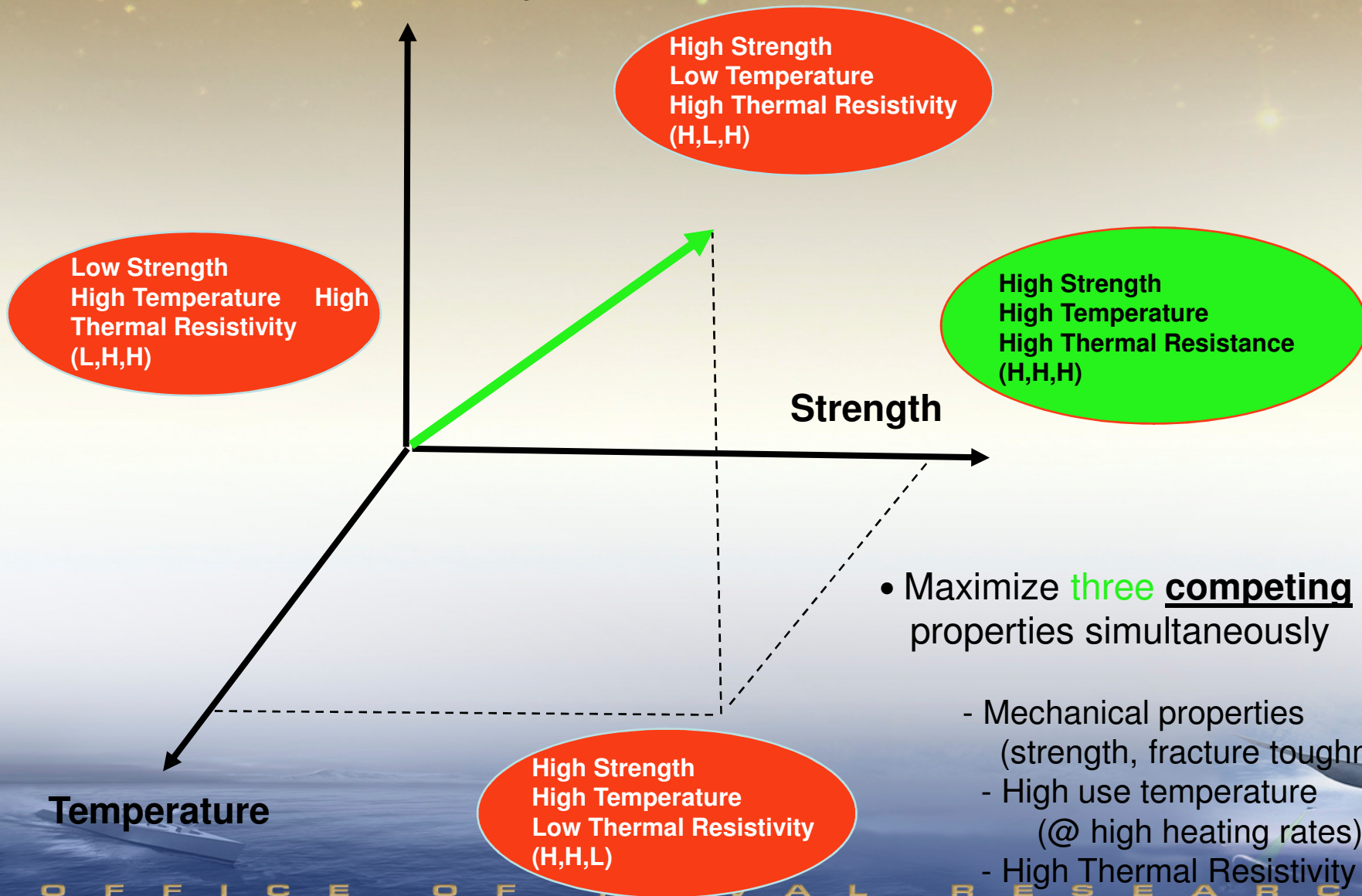
**HfB<sub>2</sub>-BN**

From CAD to part using laser or e-beam(?) metal deposition:  
*Metals were low-hanging fruit – Refractory Eutectic Ceramics and/or Coatings  
are a bit tougher*



# Structural Insulators: A Materials Challenge

Thermal Resistivity



UHTCs are necessary for future hypersonic flight/propulsion systems due to higher use temperatures

Oxidation must be understood and controlled

Monolithic Ceramics will not likely be used in flight hardware

- Flaw Sensitivity (Attachment issues)
- Thermal Shock failure

Current work – joining and reinforced UHTCs

Do good research, but think like an engineer, not a scientist!