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Evaluation of Energy Storage Technologies for Damping Control

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Evaluation of Energy Storage Technologies for Damping Control

Wednesday, October 24, 2012

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Acknowledgements

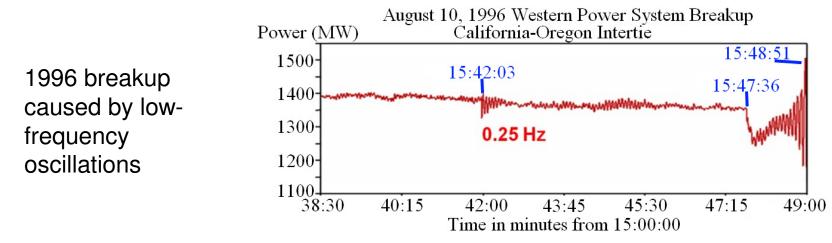


 The work was performed under funding from the DOE Energy Storage Program managed by Dr. Imre Gyuk of the DOE Office of Electricity.

Energy Storage Controls for Grid Stability



- Power systems are susceptible to low frequency oscillations caused by generators separated by long transmission lines that oscillate against each other
- These oscillations are not as well damped as higher frequency "local" oscillations
- Energy storage-based damping controllers can mitigate these oscillations



Energy Storage Controls for Grid Stability

- There are several low frequency oscillation modes in the Western Electricity Coordinating Council (WECC) region¹
 - "North-South" mode nominally near 0.25 Hz;
 - "Alberta-BC" mode nominally near 0.4 Hz;
 - "BC" mode nominally near 0.6 Hz; and,
 - "Montana" mode nominally near 0.8 Hz.
- Researchers at Montana Tech and Bonneville Power Administration (BPA) have investigated damping controls for the WECC
- This project builds on their results

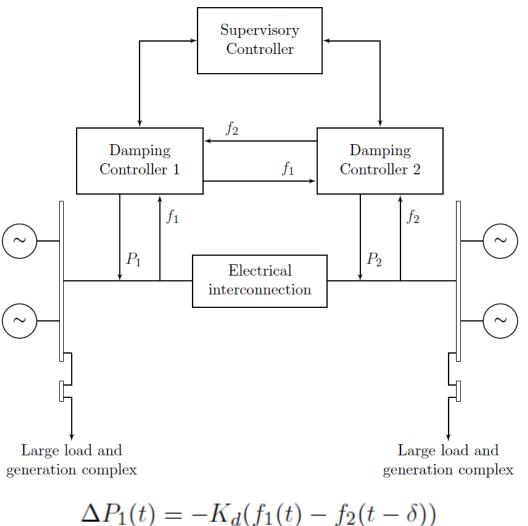
¹D. Trudnowski, "Baseline Damping Estimates," Report to Bonneville Power Administration, September 2008.





Damping control basics





$$\Delta P_2(t) = -K_d(f_2(t) - f_1(t - \delta))$$

5

Project Goals

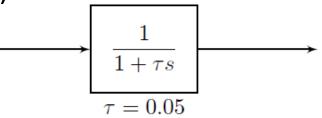


- Assess storage technologies for the damping control application
 - Develop high fidelity models
 - Perform PSLF simulations to validate performance
- Develop safeguards for the supervisory control system to insure that it can never destabilize the grid
- Develop a pilot project to be deployed in 2013

Damping Control Performance Requirements



- A typical damping control node must meet the following performance requirements:
 - Output power +/- 10MW per device, ~10 total devices
 - Bandwidth to track a P_{command} signal in the 0.25-1Hz range (real power modulation)
 - Minimal latency
- Previous simulation results from BPA and Montana Tech have shown acceptable performance with a first order system model¹ (bandwidth ~ 3.2 Hz)



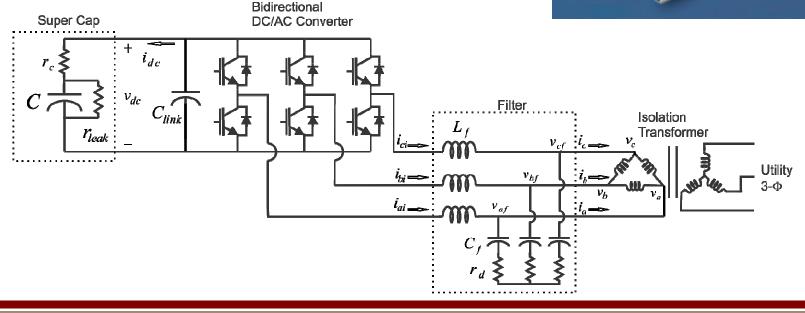
¹Dan Trudnowski, "Analytical Assessment of Proposed Controls," Report to Bonneville Power Administration under contract number 37508, September 2008.

Ultra Capacitor System



- High fidelity (13th order) model based on a Maxwell Technologies ultra-capacitor
 - 125V Heavy Transportation Module
 - 1,000,000 charge/discharge cycles
 - 63F, 125V
 - Model accurate to ~10% power dissipated across the ESR

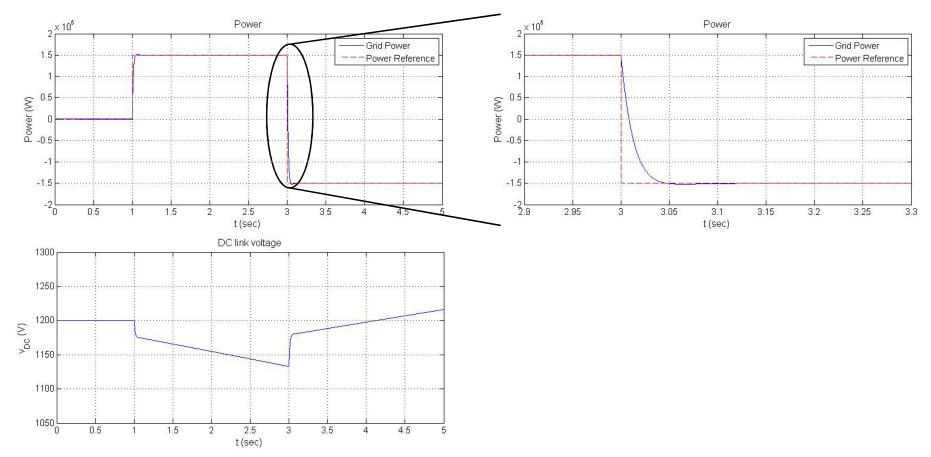




Ultra Capacitor System



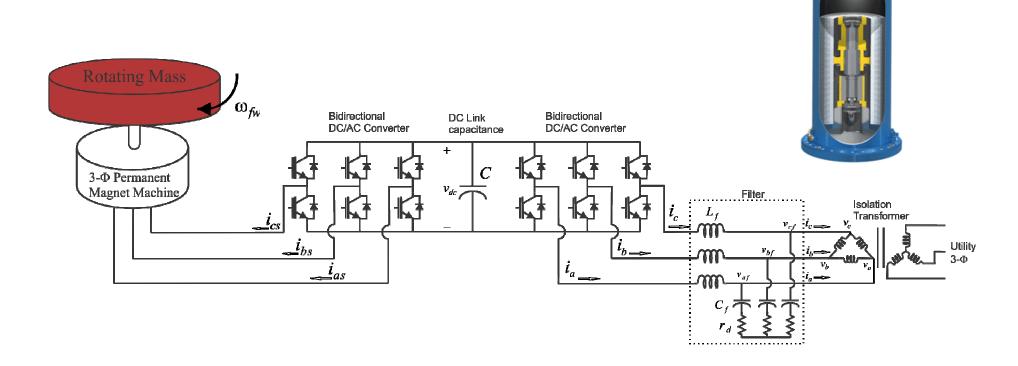
 Detailed state-space models are used to simulated system with steps in power reference: 10 series-connected 63F caps



Flywheel System



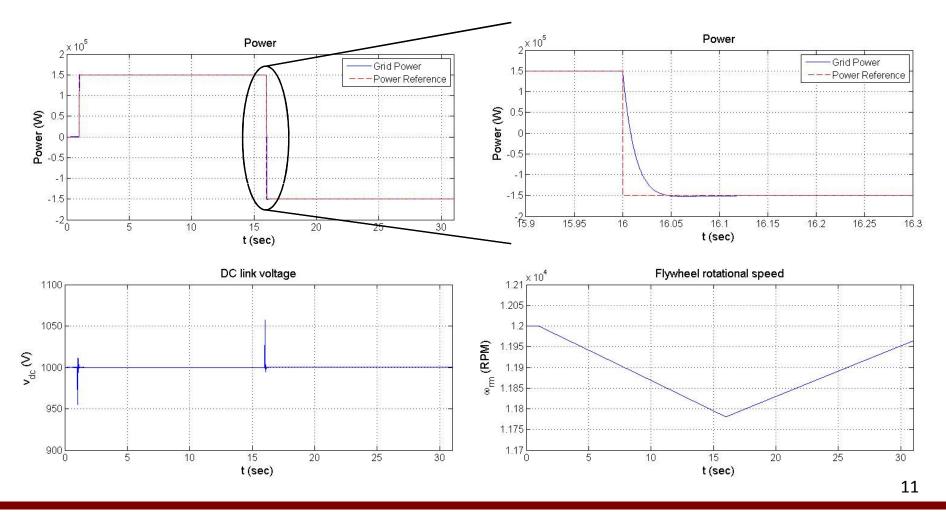
- High fidelity (21st order) model based on a Beacon flywheel (Smart Energy 25 Flywheel) and Sandia custom control
 - Parameters derived from published performance data



Flywheel System



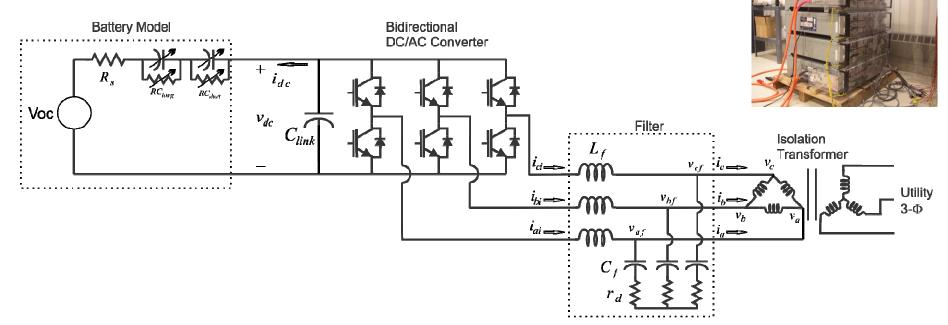
 Detailed state-space models are used to simulated system with steps in power reference



Battery System



High fidelity (15th order) model with polarization and over 60 parameters based on a carbon enhanced valve regulated lead acid battery from East Penn Manufacturing¹

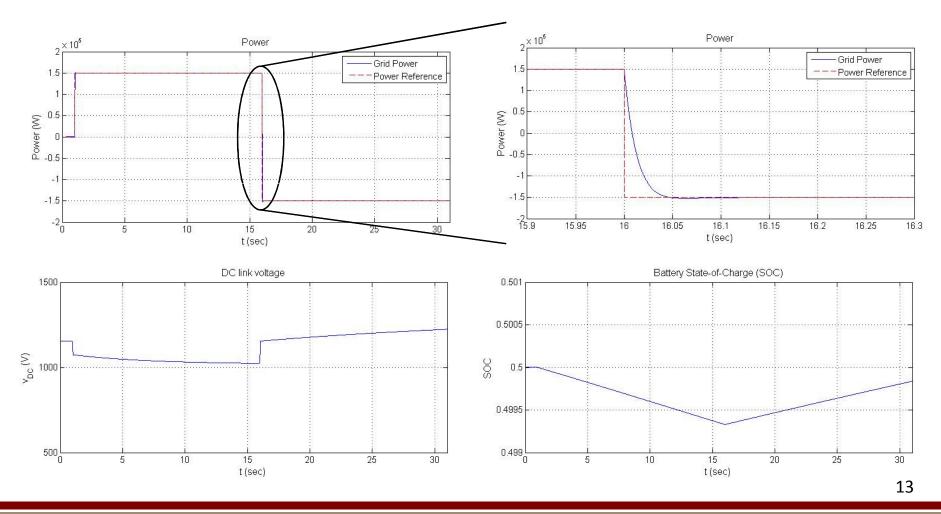


¹D. Fregosi, S. Bhattacharya, and S. Atcitty, "Empirical Battery Model Characterizing a Utility-scale Carbon-enhanced VRLA Battery", 2011 IEEE Energy Conversion Congress and Exposition (ECCE), September 17-22, 2011, pages 3541-3548.

Battery System



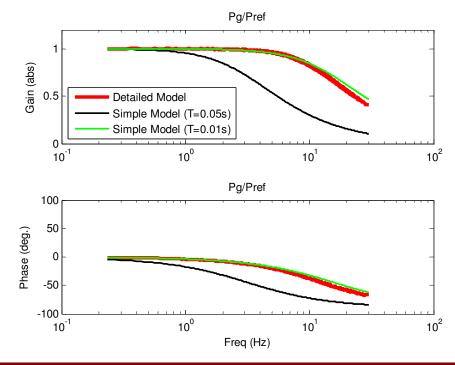
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Performance Validation

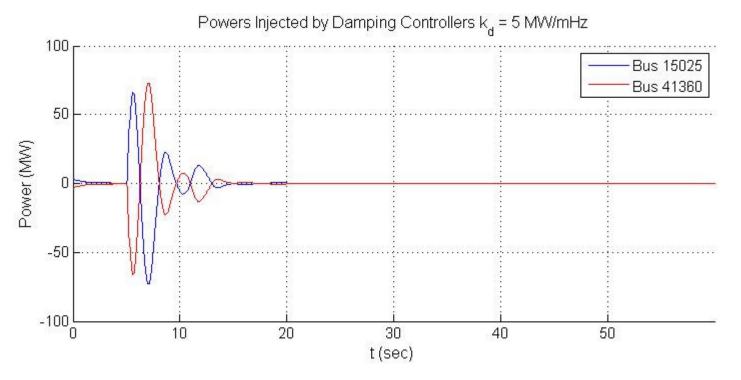


- Dynamics are dominated by the control system design (PI of currents in the qd reference frame)
- First order model accurately approximates the higher order system model
- All designs exceed the bandwidth requirements of 3.2 Hz



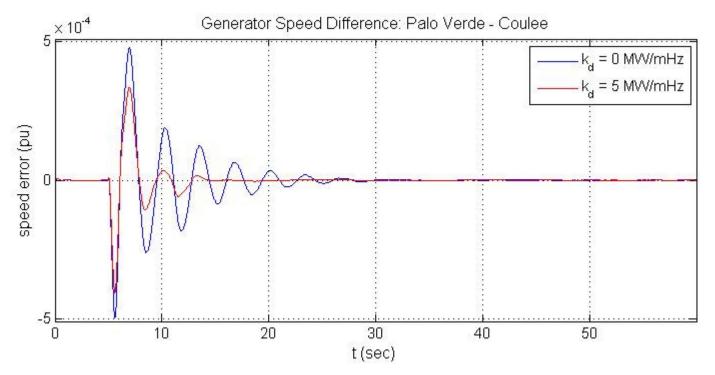


- 2017 Heavy Summer Base Case
 - PSLF simulation of line fault between CBK500 and CHAPRI
 - Ultra-Capacitor based damping control nodes at Palo Verde Coulee
 - Power Rating +/- 100 MW with $K_d = 5$ MW/mHz



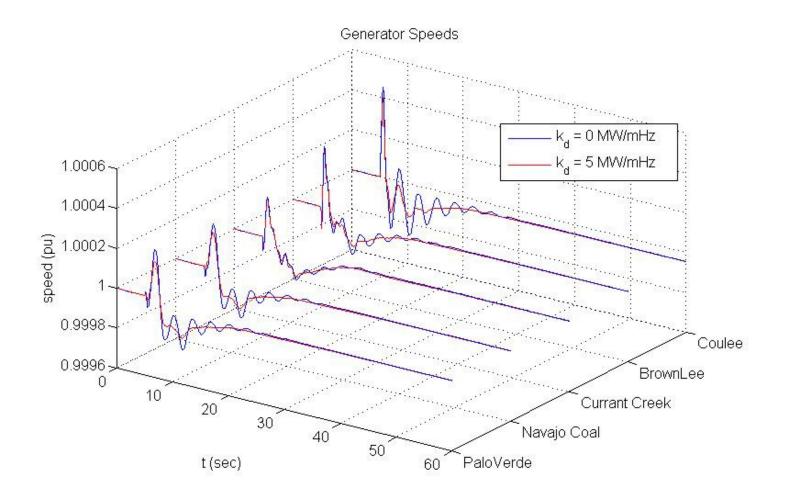


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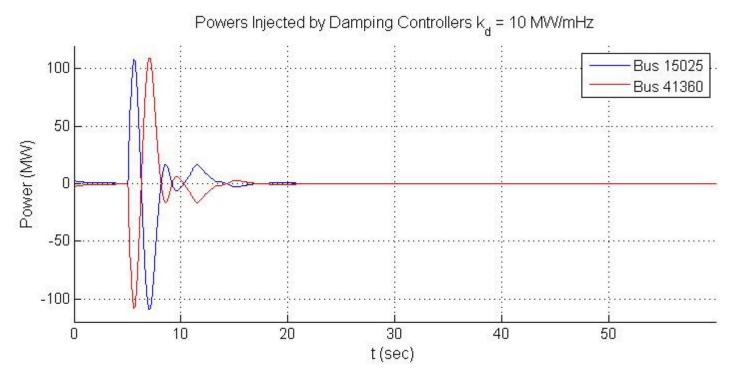
Benefit is seen by several generators in the system



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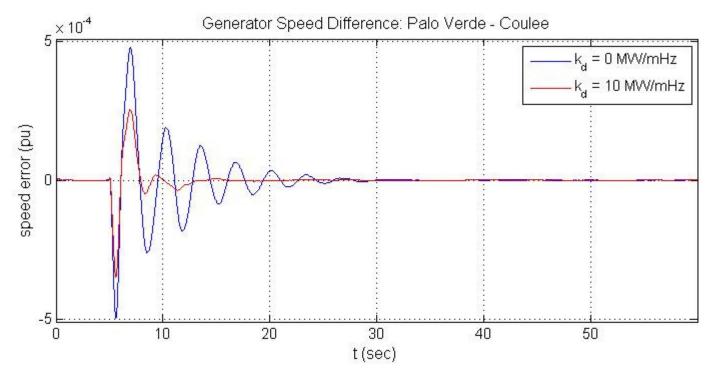


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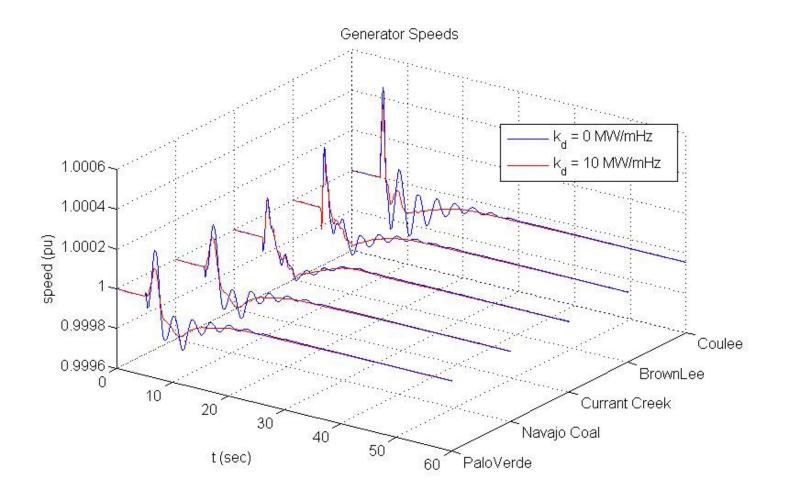


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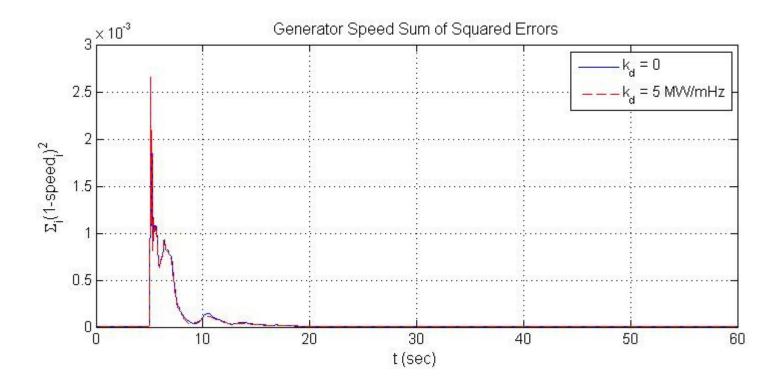


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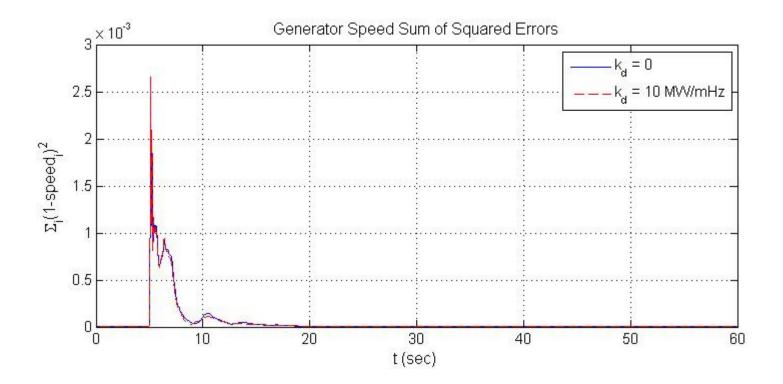


Inter-area damping does not appear to effect system frequency





Inter-area damping does not appear to effect system frequency





- The benefit of the gain K_d may be better quantified by applying Prony Analysis across a large data set to measure the damping benefit
 - Specifically, for some mode, we would like to know how much damping K_d adds to the system at that frequency:

$$d_{\rm i} = \overline{d}_{\rm i} + f_i(K_d)$$

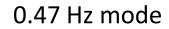
where i is the index of the mode

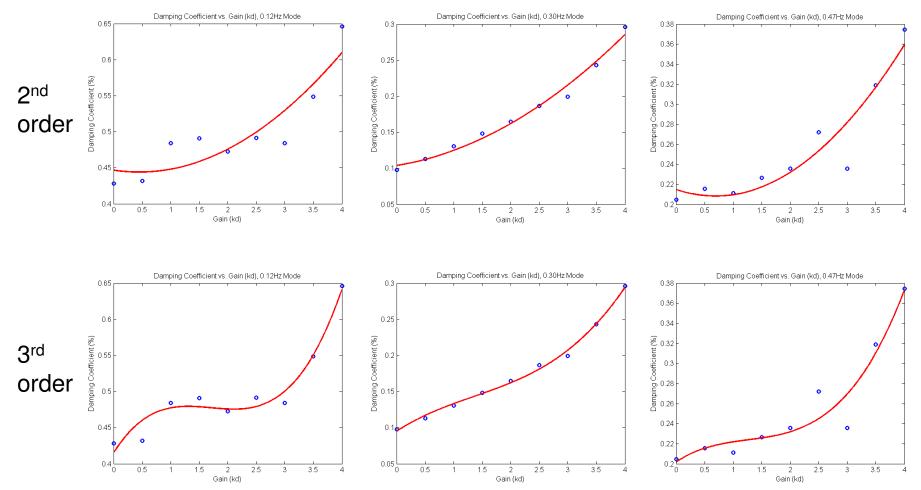
- The function f_i may be selected to give good agreement
 - Linear, quadratic, cubic ... etc



0.12 Hz mode

0.30 Hz mode





Stability Analysis

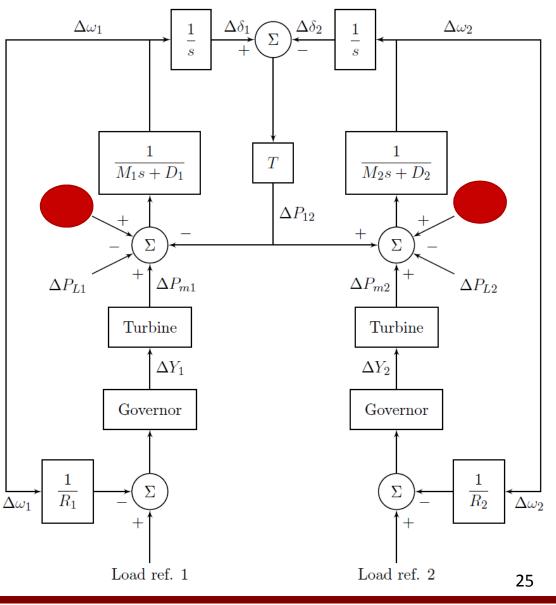


- Two-area model
- Damping controllers have the form:

 $\begin{aligned} P_{D1}(t) &= -K_d(\omega_1 - \omega_2(t - T_d)) \\ P_{D2}(t) &= -K_d(\omega_2 - \omega_1(t - T_d)) \end{aligned}$

$$P_{D1}(s) = -K_d(\omega_1(s) - \omega_2(s)e^{-sT_d})$$

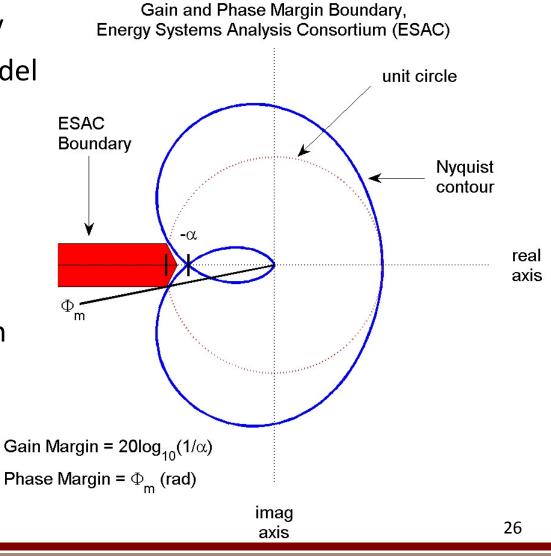
$$P_{D2}(s) = -K_d(\omega_2(s) - \omega_1(s)e^{-sT_d})$$



Stability Analysis



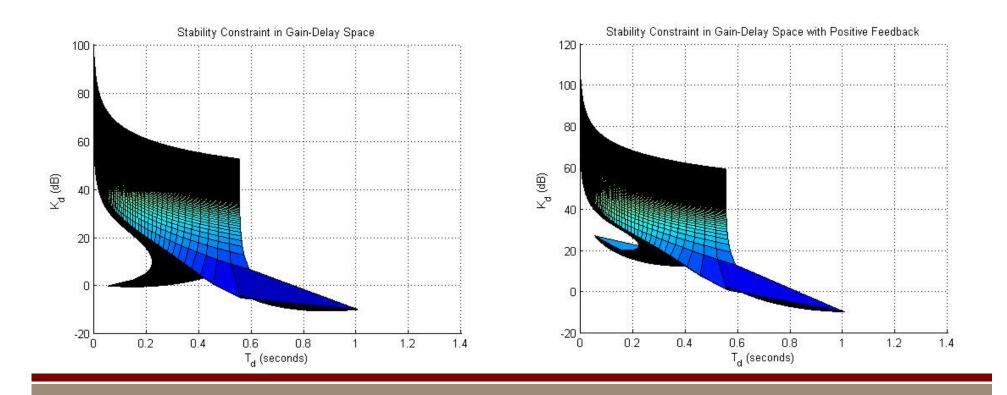
- Apply the Nyquist stability criterion to the two-area model
- Specify a relative stability margin
 - Gain margin
 - Phase margin
- ESAC Boundary
- Identify stability regions in (gain, delay) space



Stability Analysis - Results



- ESAC Boundary
 - 3 db gain margin
 - 9 degrees phase margin
- Unstable system (e.g. damping control required)



Accomplishments



- Developed high fidelity models for:
 - Ultra capacitor system
 - Flywheel system
 - Battery system
- Validated damping controller performance in PSLF using a WECC model
- Developed an analytical approach for supervisory control gain scheduling
- A Technology Innovation Proposal to Bonneville Power Administration was accepted for a follow-on demonstration project (co-funded by DOE)

Contact Information



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