



PRELIMINARY STUDY OF GASIFICATION WITH STEAM / ENRICHED AIR MIXTURES OF SEWAGE SLUDGE AND OF THE CHAR OBTAINED IN ITS PYROLYSIS PROCESS

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Bioenergy III: Present and New Perspectives on Biorefineries
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OUTLINE

1. INTRODUCTION AND OBJECTIVES
2. MATERIALS AND METHODS
 - Materials
 - Experimental plant
3. RESULTS
 - Effect of H₂O/O₂ molar ratio used as gasifying agent
 - Effect of temperature
4. CONCLUSIONS AND FUTURE WORKS

OUTLINE

1. INTRODUCTION AND OBJECTIVES

2. MATERIALS AND METHODS

- ❑ Materials
- ❑ Experimental plant

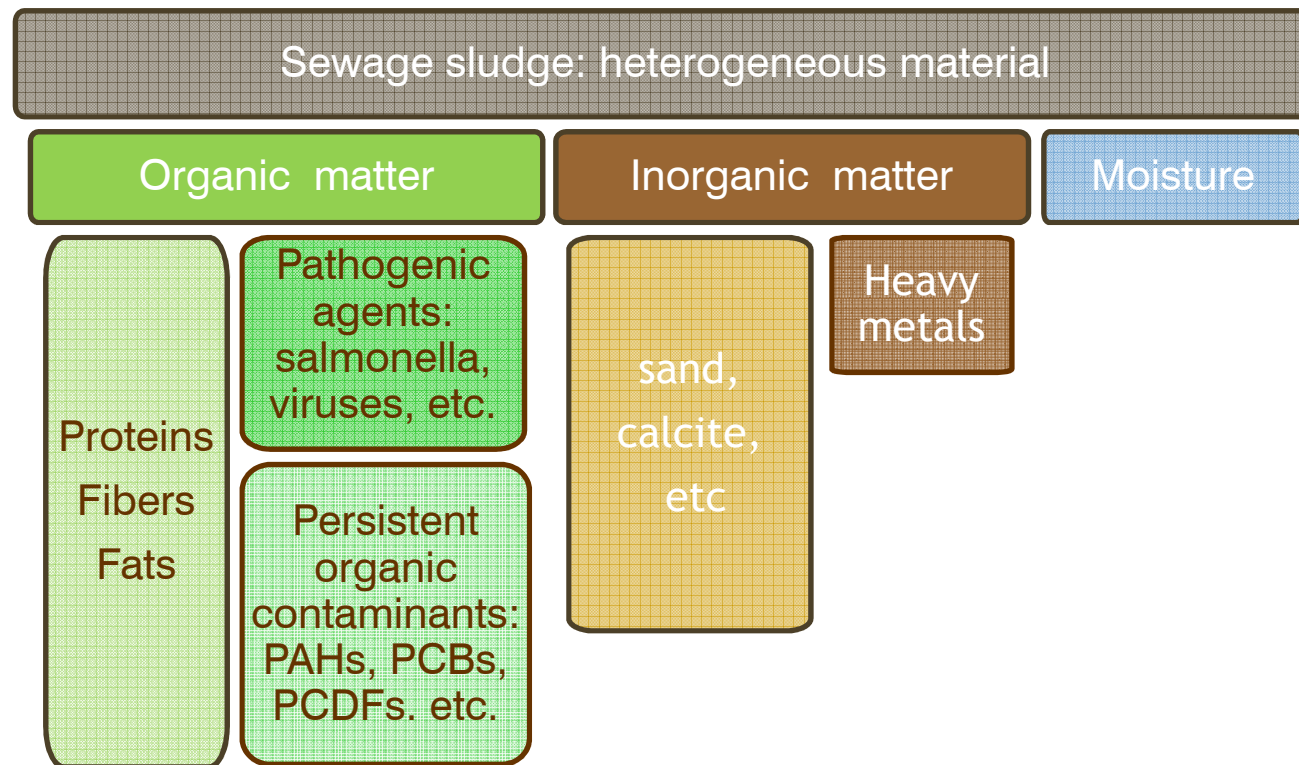
3. RESULTS

- ❑ Effect of H₂O/O₂ molar ratio used as gasifying agent
- ❑ Effect of temperature

4. CONCLUSIONS AND FUTURE WORKS



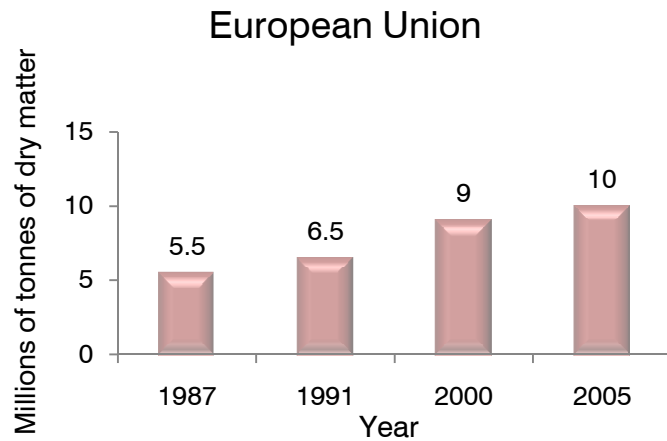
Sewage sludge is the waste produced during the purification of the wastewater in the wastewater treatment plants.



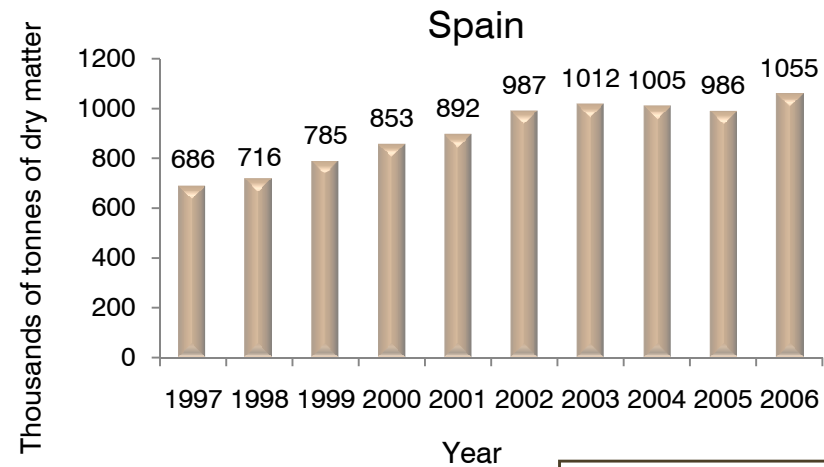
Strict legislation (Directive 91/271/ECC)



↑ sewage sludge generation

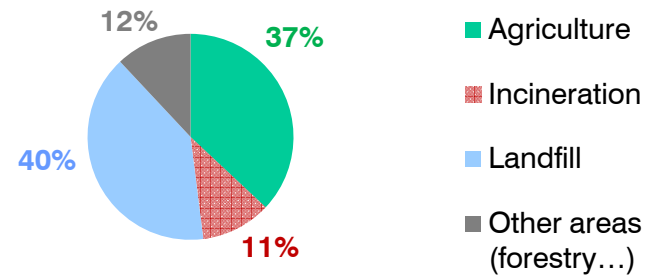


Source: Eurostat



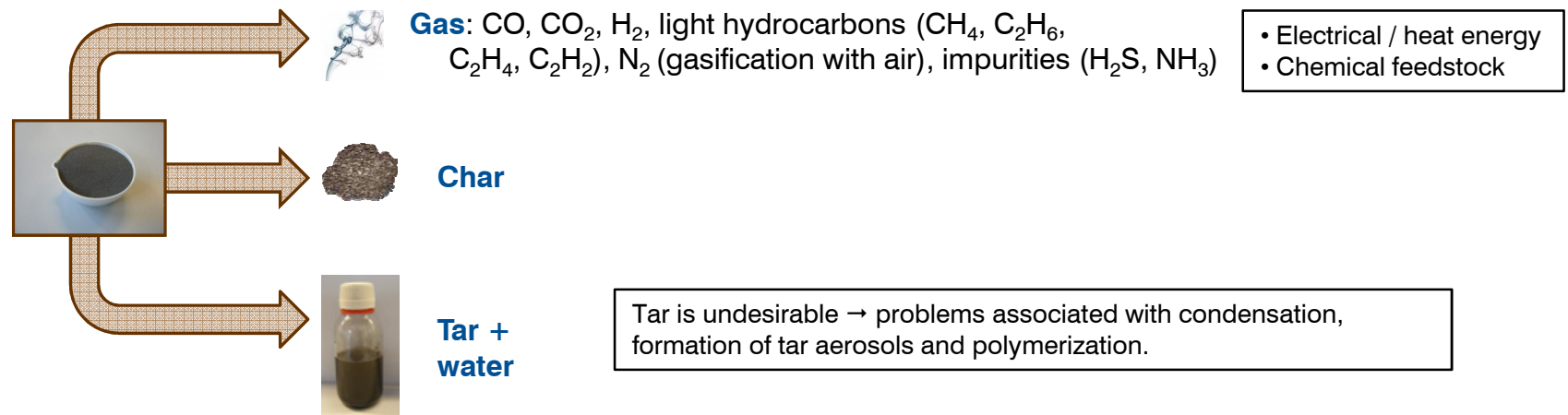
Source: PNIR 2008-2015

Sewage sludge management ways in European Union (2008)



Thermochemical processes as a way of sewage sludge management

➤ **Gasification** is the thermal process during which carbonaceous content of sewage sludge is converted to a gaseous fuel by heating in a gasification medium such as air, oxygen or steam.



➤ **Pyrolysis** is the thermal decomposition of a material in an inert atmosphere.

Char is the main byproduct in flash pyrolysis → it still has carbonaceous content → raw material for gasification process.

OBJECTIVE OF THE WORK

Study the influence of some OPERATIONAL CONDITIONS:

- ✓ Raw material: sewage sludge and char obtained in sewage sludge pyrolysis.
- ✓ Gasification medium: mixtures of enriched air / steam ($\text{H}_2\text{O}/\text{O}_2$ molar ratio = 1 and 3).
- ✓ Temperature: 820°C and 850 - 860°C

on some RESPONSE VARIABLES of the gasification process:

- ✓ Distribution of products (mass yields of gasification products: gas, solid, tar, water)
- ✓ Gas composition and LHV_{gas}
- ✓ Carbon conversion efficiency
- ✓ Apparent thermal efficiency

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2. **MATERIALS AND METHODS**

- ❑ *Materials*
- ❑ *Experimental plant*

3. RESULTS

- ❑ Effect of H₂O/O₂ molar ratio used as gasifying agent
- ❑ Effect of temperature

4. CONCLUSIONS AND FUTURE WORKS

□ Materials

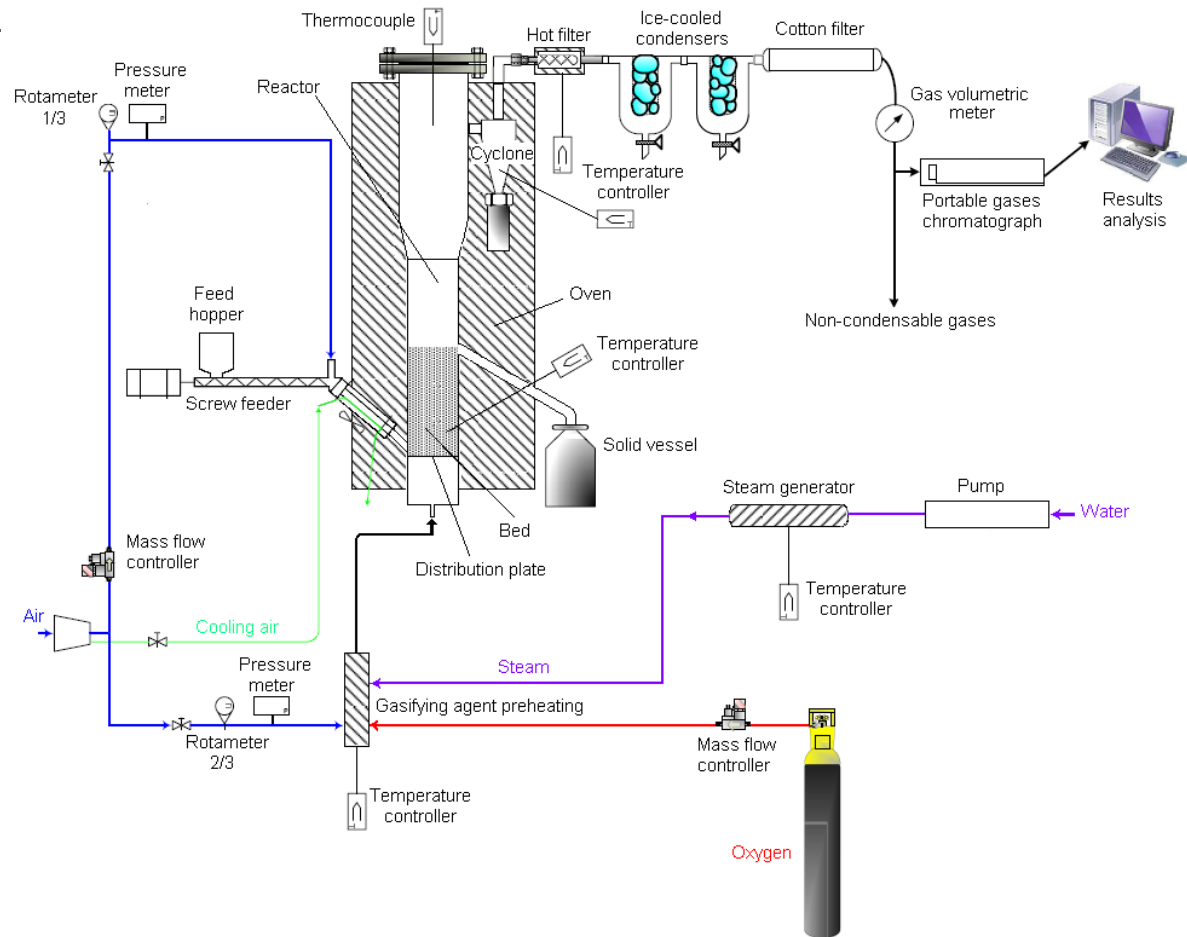
- Anaerobically digested and dried sewage sludge, supplied by a Spanish urban waste water treatment plant (it is ground and sieved to 250-500 μm).
- Char obtained from sewage sludge pyrolysis (530°C) in fluid bed.

	Sewage sludge	Char from sewage sludge pyrolysis
Ultimate analysis (wt. % as received)		
Moisture	6.6	1.7
Ash	41.3	74.2
Volatiles	46.1	15.0
Fixed carbon	6.0	9.1
Elemental analysis (wt. % as received)		
C	27.7	15.5
H	4.4	1.0
N	3.9	1.9
S	0.8	0.4
Lower Heating Value		
LHV (MJ/kg)	10.80	4.96

2. Materials and methods. Experimental plant

Experimental plant

- Fluidized bed reactor (atmospheric pressure)
- $u_f/u_{mf} \approx 6$
- Continuous feed of solids and continuous removal of ash



Operational conditions

- Gasifying agent → mixtures of steam and enriched air with different H_2O/O_2 molar ratios: 1 or 3.
- Gasifying agent ($H_2O + O_2$) to biomass ratio: 1.1 kg $H_2O + O_2$ /kg biomass *daf* (dry and ash free).
- Bed temperature: 820 or 860°C

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3. **RESULTS**

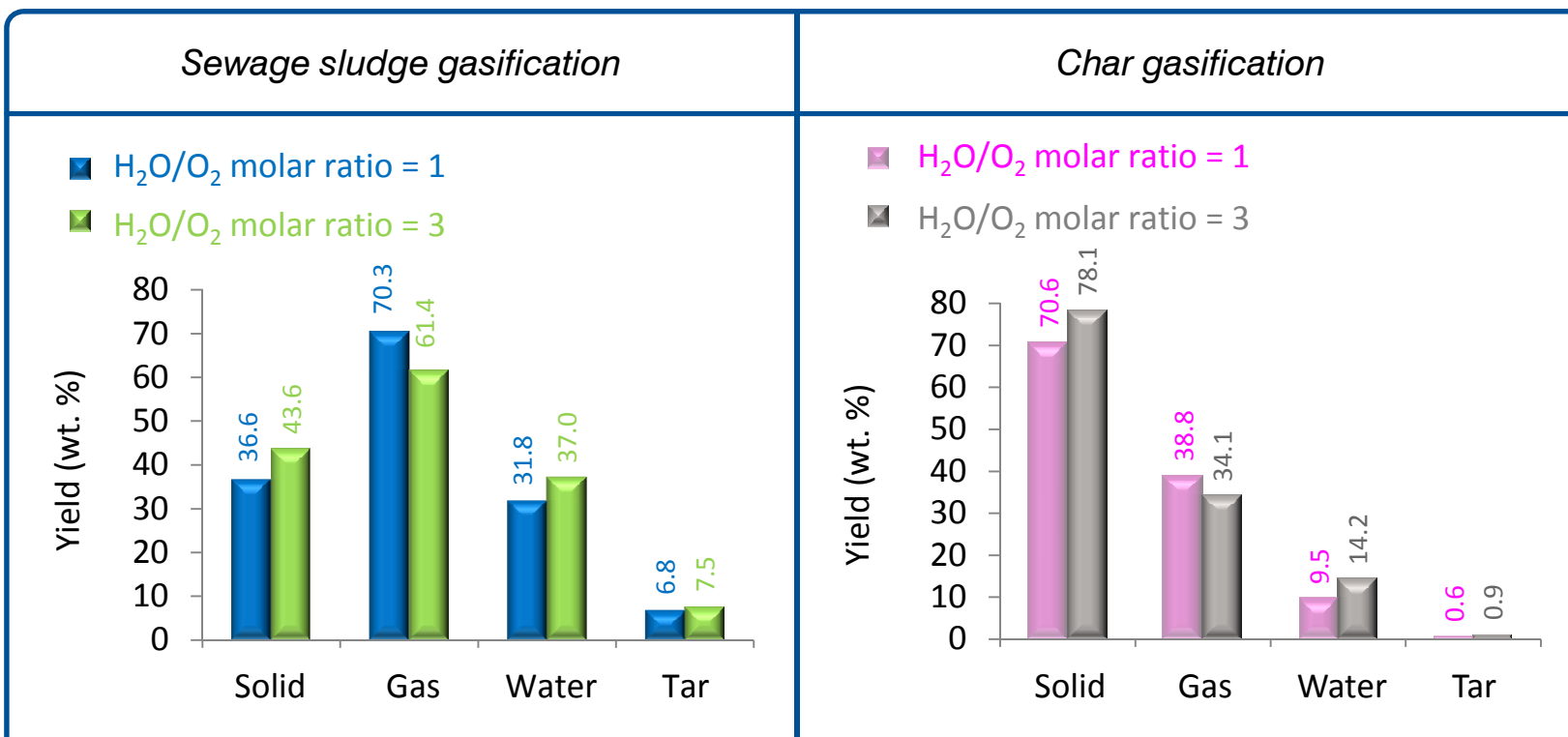
- ❑ *Effect of H_2O/O_2 molar ratio used as gasifying agent*
- ❑ *Effect of temperature*

4. CONCLUSIONS AND FUTURE WORKS

3. Results. Effect of H_2O/O_2 molar ratio used as gasifying agent

□ Effect of H_2O/O_2 molar ratio used as gasifying agent (I)

Temperature = 820°C

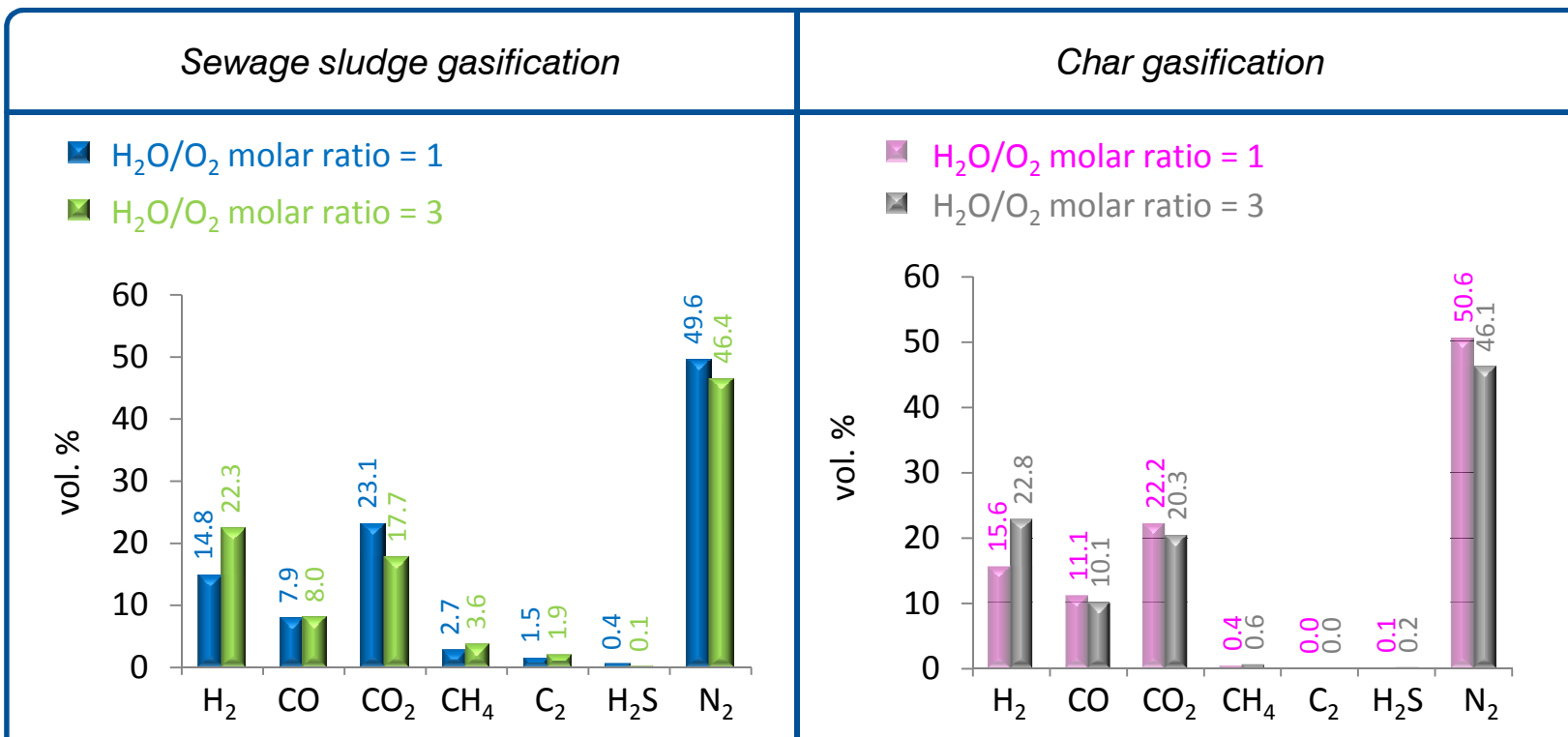


- ↑ steam proportion → ↓ gas yield; ↑ solid, water and tar yields.
- The main product obtained in sewage sludge gasification was the gaseous product, while solid was the main product in char gasification.

3. Results. Effect of H₂O/O₂ molar ratio used as gasifying agent

□ Effect of H₂O/O₂ molar ratio used as gasifying agent (II)

Temperature = 820°C



- ↑ steam proportion → ↑ H₂ and light hydrocarbons; ↓ CO₂.
- vol. % of CH₄ and C₂ were lower in the gas obtained in char gasification than in those obtained in sewage sludge gasification.

3. Results. Effect of H₂O/O₂ molar ratio used as gasifying agent

□ Effect of H₂O/O₂ molar ratio used as gasifying agent (III)

Temperature = 820°C

	Gas LHV (MJ/Nm ³)	Carbon conversion efficiency (%)	Apparent thermal efficiency (%)
Sewage sludge gasification			
H ₂ O/O ₂ molar ratio = 1	4.55	83.83	49.72
H ₂ O/O ₂ molar ratio = 3	5.87	75.67	64.30
Char gasification			
H ₂ O/O ₂ molar ratio = 1	3.25	76.18	42.85
H ₂ O/O ₂ molar ratio = 3	3.97	66.12	49.40

$$\text{Carbon conversion efficiency (\%)} = \frac{\text{kg C in gas produced}}{\text{kg C in biomass fed}} \times 100$$

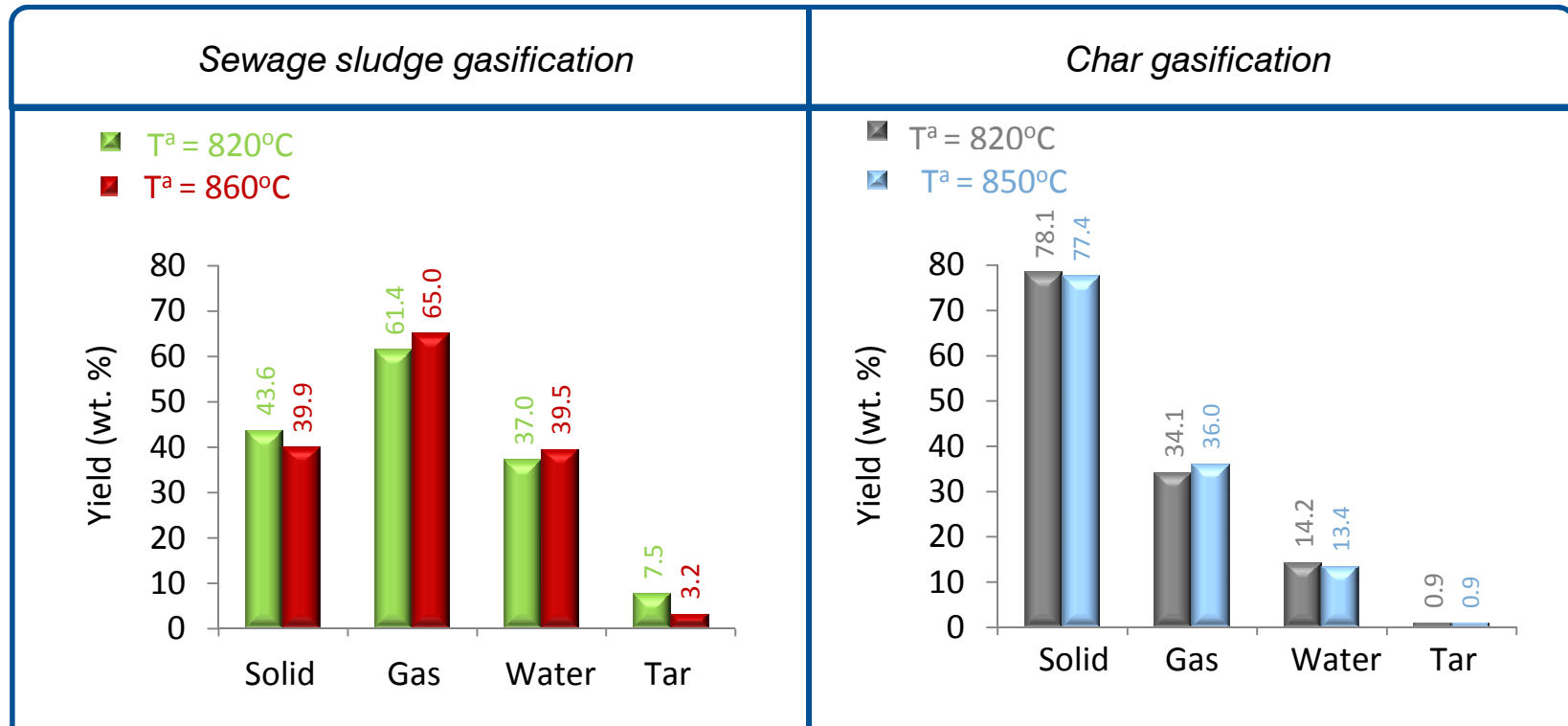
$$\text{Apparent thermal efficiency (\%)} = \frac{\text{Nm}^3 \text{ gas produced} \times \text{LHV}_{\text{gas}} \left(\frac{\text{MJ}}{\text{Nm}^3} \right)}{\text{kg biomass fed} \times \text{LHV}_{\text{biomass}} \left(\frac{\text{MJ}}{\text{kg}} \right)} \times 100$$

- ↑ steam proportion → ↑ LHV_{gas} (↑ vol. % of H₂, CH₄ and C₂); ↓ carbon conversion efficiency; ↑ apparent thermal efficiency.
- LHV_{gas}, carbon conversion efficiency and apparent thermal efficiency are lower in char gasification than in sewage sludge gasification.

3. Results. Effect of temperature

□ Effect of temperature (I)

H₂O/O₂ molar ratio = 3

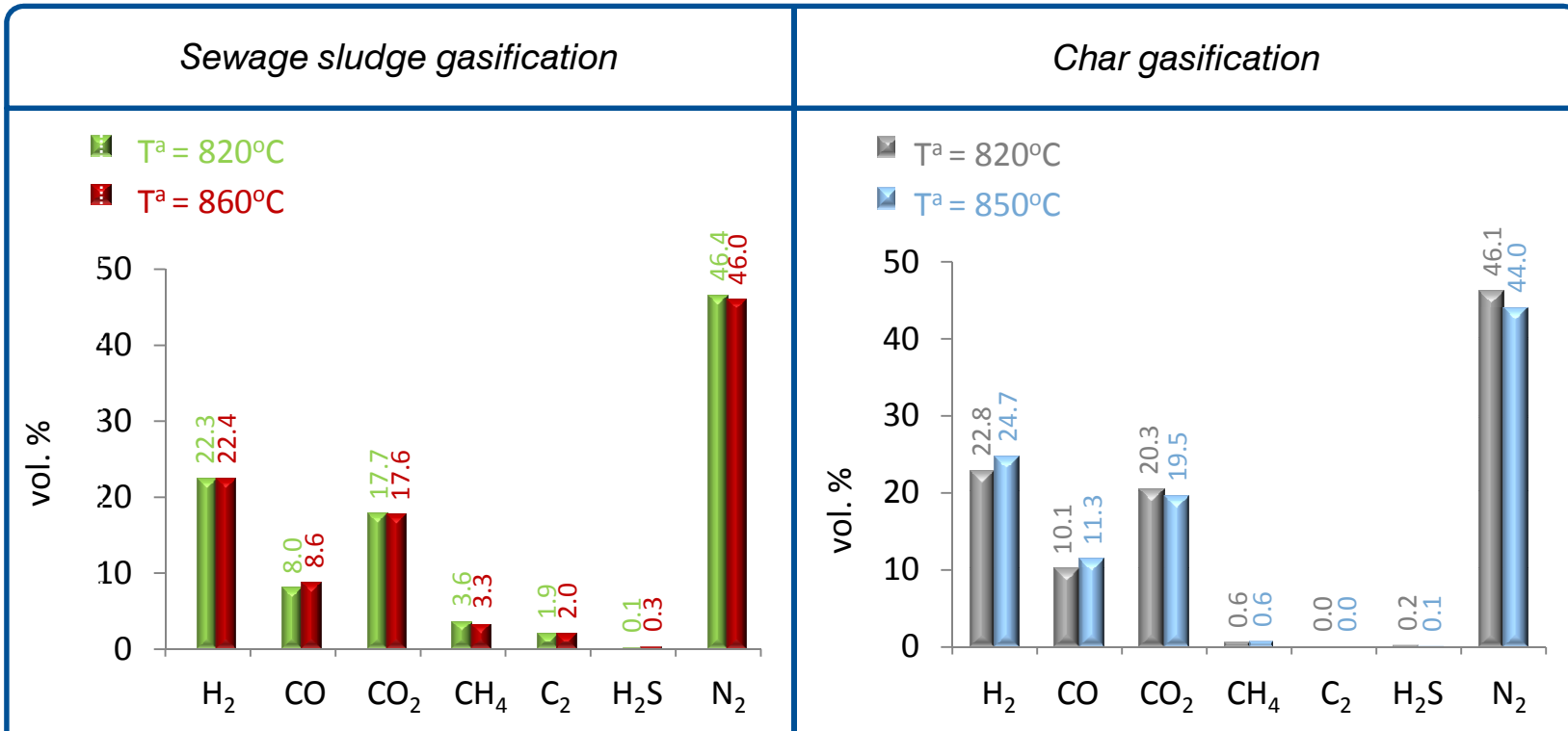


➤ ↑ temperature → ↑ gas yield; ↓ solid yield; ↓ tar yield in sewage sludge gasification, but this difference was not significant in char gasification.

3. Results. Effect of temperature

Effect of temperature (II)

H₂O/O₂ molar ratio = 3



➤ Gas composition was hardly influenced when temperature was increased in both sewage sludge and char gasification.

3. Results. Effect of temperature

□ Effect of temperature (III)

H₂O/O₂ molar ratio = 3

	Gas LHV (MJ/Nm ³)	Carbon conversion efficiency (%)	Apparent thermal efficiency (%)
<i>Sewage sludge gasification</i>			
T = 820°C	5.87	75.67	64.30
T = 860°C	5.88	79.96	67.50
<i>Char gasification</i>			
T = 820°C	3.97	66.12	49.40
T = 850°C	4.32	70.90	56.98

➤ ↑ temperature → LHV_{gas} was hardly influenced; ↑ carbon conversion efficiency; ↑ apparent thermal efficiency.

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CONCLUSIONS

- The $\text{H}_2\text{O}/\text{O}_2$ molar ratio used as gasifying agent had a significant effect on gasification process of both, sewage sludge and sludge derived char.
 - $\uparrow \text{H}_2\text{O}/\text{O}_2$ molar ratio \rightarrow \downarrow gas yield but $\uparrow \text{LHV}_{\text{gas}}$ and \uparrow apparent thermal efficiency; $\uparrow \text{H}_2$ formation.
 - $\uparrow \text{H}_2\text{O}/\text{O}_2$ molar ratio \rightarrow $\uparrow \text{H}_2/\text{CO}$ molar ratio in gas product (above 2).
- \uparrow temperature \rightarrow \uparrow gas yield; gas composition and LHV_{gas} were hardly influenced.
- Char gasification yielded a gas with a very low LHV, being the advantage the low tar content.

FUTURE WORKS

- To analyze the influence on tar composition
- To deepen into the gas cleaning process

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Thermo-Chemical
Processes Group



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Universidad de Zaragoza



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Química y Tecnologías
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