

UNIVERSITY OF BIRMINGHAM

Research at Birmingham

Development of a fluid-structure interaction model to simulate mitral valve malcoaptation

Hassani, Kamran; Karimi, Alireza; Dehghani, Ali; Golpaygani, Ali Tavakoli; Abdi, Hamed; Espino, Daniel

DOI:

[10.1177/0267659118811045](https://doi.org/10.1177/0267659118811045)

License:

None: All rights reserved

Document Version

Peer reviewed version

Citation for published version (Harvard):

Hassani, K, Karimi, A, Dehghani, A, Golpaygani, AT, Abdi, H & Espino, D 2018, 'Development of a fluid-structure interaction model to simulate mitral valve malcoaptation', *Perfusion*. <https://doi.org/10.1177/0267659118811045>

[Link to publication on Research at Birmingham portal](#)

Publisher Rights Statement:

Checked for eligibility 06/11/2018

This is the Author Accepted Manuscript of an article published in *Perfusion*.
<https://doi.org/10.1177/0267659118811045>

General rights

Unless a licence is specified above, all rights (including copyright and moral rights) in this document are retained by the authors and/or the copyright holders. The express permission of the copyright holder must be obtained for any use of this material other than for purposes permitted by law.

- Users may freely distribute the URL that is used to identify this publication.
- Users may download and/or print one copy of the publication from the University of Birmingham research portal for the purpose of private study or non-commercial research.
- User may use extracts from the document in line with the concept of 'fair dealing' under the Copyright, Designs and Patents Act 1988 (?)
- Users may not further distribute the material nor use it for the purposes of commercial gain.

Where a licence is displayed above, please note the terms and conditions of the licence govern your use of this document.

When citing, please reference the published version.

Take down policy

While the University of Birmingham exercises care and attention in making items available there are rare occasions when an item has been uploaded in error or has been deemed to be commercially or otherwise sensitive.

If you believe that this is the case for this document, please contact UBIRA@lists.bham.ac.uk providing details and we will remove access to the work immediately and investigate.

Development of a fluid-structure interaction model to simulate mitral valve malcoaptation

Kamran Hassani^{1*} , Alireza Karimi², Ali Dehghani¹, Ali Tavakoli Golpaygani³, Hamed Abdi¹, and Daniel M. Espino⁴

¹ *Department of Biomedical Engineering, Science and Research Branch, Islamic Azad University, Tehran, Iran*

² *Department of Mechanical Engineering, Kyushu University, 744 Motoooka, Nishi-ku, Fukuoka 819-0395, Japan*

³ *Department of Biomedical Engineering, Standard Research Institute, Karaj, Iran.*

⁴ *Department of Mechanical Engineering, University of Birmingham, Birmingham B15 2TT, United Kingdom*

* *Corresponding author at:* Department of Biomedical Engineering, Science and Research Branch, Islamic Azad University, Hesarak, Daneshgha Square, Tehran, Iran.

E-mail address: k.hasani@srbiau.ac.ir (K. Hassani).

1 **Abstract**

2 Mitral regurgitation (MR) is a condition in which the mitral valve does not prevent the reversal of
3 blood flow from the left ventricle in to the left atrium. This study aimed at numerically developing
4 a model to mimic MR and poor leaflet coaptation and also comparing the performance of a normal
5 mitral valve to that of the MR conditions at different gap junctions of 1, 3, and 5 mm between the
6 anterior and posterior leaflets. The results revealed no blood-flow to the left ventricle when a gap
7 between the leaflets was 0 mm. However, MR increased this blood-flow with increases in the
8 velocity and pressure within the atrium. The pressure within the aorta did not vary meaningfully
9 though (ranging from 22 kPa for a ‘healthy’ model to 25 kPa for severe MRD). The findings from
10 this study have implications not only for understanding the changes in pressure and velocity as a
11 result of the MR in the ventricle, atrium, or aorta, but also for the development of a computational
12 model suitable for clinical translation when diagnosing and determining treatment for MR.

13

14 **Keywords:** blood flow; fluid-structure interaction; left atrium; left ventricle; Mitral
15 regurgitation.

1 **Introduction**

2 Mitral regurgitation (MR) is a condition in which the leaflets of the mitral valve do not prevent
3 backflow of the blood from the left ventricle to the left atrium [1],[2],[3]. This is often due to poor
4 closure, or coaptation, between its leaflets; known as mal-coaptation. Thus, if MR is severe, the
5 pressure of the left atrium increases leading to symptoms such as dyspnea, fatigue, orthopnea, and
6 pulmonary edema [4]. Although annular dilation, and its subsequent effect on coaptation, has been
7 assessed *in vitro* [5], there is limited understanding of the effect of the specific mode of mal-
8 coaptation on the subsequent hemodynamic characteristics of the blood flow during MR between
9 the left atrium, left ventricle, and the aorta. MR can be studied clinically, but it does not offer the
10 possibility to assess variables associated with mal-coaptation independently to assess how they
11 contribute to subsequent hemodynamics during MR. Computational modelling, and in particular,
12 transient Fluid-Structure Interaction (FSI) [6] offers the potential to determine the mechanisms
13 linking altered mechanics and coaptation between mitral valve leaflets, with the resulting
14 pathophysiological hemodynamics.

15 There is an extensive range of computational modelling of the mitral valve within the literature.
16 For instance, Wenk *et al.* [7] proposed a finite element (FE) model for the left ventricle with MR
17 using magnetic resonance imaging (MRI) data from sheep. Stevanella *et al.* [8] presented a patient-
18 specific structural FE model of the mitral valve to assess mitral annuloplasty procedures. A three-
19 dimensional FE model of the mitral valve has also proposed to assess the nonlinear mechanical
20 performance of the anterior and posterior leaflets during the diastole and systole [9]. Surgical repair
21 of the mitral valve has been assessed too [10], along with the effect of collagen concentration
22 within the mitral valve leaflets [11]. More recently, there has been a focus on combining
23 Computational Fluid Dynamics (CFD) with end-diastolic geometry and time-dependent

1 deformation of the left ventricle cavity [12], as well as MR flow [13]. CFD has also been used to
2 assess insufficiency through the mitral valve Sonntag *et al.* [14]. However, regardless of the depth
3 of literature, currently no such studies have determined a mechanical pathway which links the
4 specific pathophysiological hemodynamic characteristics during MR to the altered leaflet
5 mechanics which result in mal-coaptation. Even an initial step of assessing the influence of a gap
6 between the two mitral leaflets has not been assessed; despite the clinical importance of such
7 studies, and their potential to be used to propose novel repair strategies, both the computational
8 and experimental literature is very much limited [15].

9 This study was aimed at developing a transient FSI model of the mitral valve able to predict
10 mal-coaptation. The model geometry is based on subject-specific MRI data. For this initial
11 development, a two-dimensional (2D) model has been used. While three-dimensional models are
12 of value [16], the timescales associated with solving 2D models at present more closely match
13 clinical timeframes [17]. This initial model has focused on hemodynamic assessment of blood flow
14 through the left atrium, left ventricle, and the aorta, during mal-coaptation of the anterior and
15 posterior mitral valve leaflets due to gap sizes of 1, 3, and 5 mm.

16

17 **Materials and methods**

18 An MRI scan (Siemens, Germany, 1.5 Tesla) of a mitral valve was obtained from a 60-year-old
19 male. Ethical approval was obtained from Tehran Modarres Hospital. The mitral valve scanned
20 had normal coaptation. From this scan, distinct MR cases were simulated using a 2D model (**Fig.**
21 **1**).

22 Four cases were simulated. The first model included tightly coapting anterior and posterior leaflets
23 so that no MR occurred across the mitral valve (Case A). The second model included a 1 mm gap

1 between the leaflets, and was considered as a mild MR model (Case B). The third model included
2 a 3 mm gap between the leaflets, representing fully developed MR (Case C). The last model
3 included a 5 mm gap, simulating severe MR (Case D). Left atrial and ventricular systolic pressures
4 were applied as boundary conditions [18],[19] where the blood velocity (flow rate if considered
5 over the cross-sectional area of the aorta) was applied as a further boundary condition [20]. As the
6 mitral valve is closed during systole, the leaflets were assumed to be fixed in position. This
7 boundary condition would mimic the mitral valve leaflets following the initial elongation of
8 chordae tendineae; consistent with previous studies [21].

9 Blood flow was assumed to be laminar, incompressible, and Newtonian; a suitable
10 approximation under large-scale flow as occurs within the heart [22]. The viscosity of blood was
11 taken to be 5.5 mPa/s with density of 1056 kg/m³ [23], [24]. Anterior and posterior mitral leaflets
12 were assumed to behave as linear elastic materials (with a Young's modulus of 1 and 2 MPa,
13 respectively). The density and Poisson's ratio of the leaflets applied to the model were 1060 kg/m³
14 and 0.488, respectively [25], [26].

15 Triangular elements were used to generate the mesh. The mesh density analyses have been
16 conducted to select the appropriate mesh size (stress was assessed with mesh density). The number
17 of elements used in the model was 3309. The simulation time was set to run for 0.45 s, i.e. only
18 systole was modelled [27].

19 FSI was used to perform transient, and simultaneous simulations of the mitral valve.
20 Simulations were performed using Comsol Multiphysics (Comsol Multiphysics, Stockholm,
21 Sweden). The formulation employed led to the following physical restraints/coupling to enable
22 interaction between simulation of fluid flow and structural deformation: a) the deformation of the
23 contact points of the fluid (blood) and solid (Leaflet) were coupled (i.e. rate of change of solid

1 boundary displacement is matched by the velocity of blood); b) the planar force of the fluid in the
2 contact point of the fluid and solid acts as the planar force of the solid (i.e. the loading condition
3 applied to the leaflets); and c) a no slip condition is applied to the fluid boundary [28].
4

5 **Results**

6 Velocity contours at 0.2 s (during systole) are provided **Fig. 2** for all four cases. For the ‘healthy’
7 model (Case A), MR was not possible [29] and a vortex ensued behind the leaflets. When MR was
8 simulated (Cases B-D), the blood volume and the velocity increased due to an increasing gap
9 between the leaflets. The result is blood-flow into the atrium (**Fig. 2**). For mild MR (Case B), the
10 leakage rate was low (around 2.5 m/s). However, blood-flow velocity reached 5 m/s for Cases C
11 and D. For severe MR (Case D), the velocity was such that a large vortex ensued within the left
12 ventricular cavity.

13 The velocity of blood within the left atrium is provided in **Fig. 3**. For Case A, this velocity was
14 zero. For MR, blood flow increased to peak values of 0.81, 1.63, and 2.42 m/s for Cases B, C, and
15 D, respectively. This trend continued from the time at which these peaks occurred up to the end of
16 the simulation.

17 The time-dependency of left atrial blood pressure is provided in **Fig. 4**. For Case A, these
18 pressures were in agreement with experimental data [30]. For Case B, similar trends were predicted
19 for time-dependent pressures, but a small alteration in the maximum (0.3 Kpa) and minimum (1.9
20 Kpa) pressures did occur. However, for Cases C and D, an abnormal pressure trend was predicted.
21 This abnormal pressure was related to the rate of systolic ventriculo-atrial blood-flow; in essence,
22 the velocity of MR. Peak pressures for Cases C and D were 2.12 and 2.90 kPa, respectively.

1 Time-dependent ventricular pressure adjacent to the mitral valve is provided in **Fig. 5**. There is
2 an increased pressure during early systole (to 5 kPa) for both cases C and D. For Case D this
3 pressure peaked at 7.80 kPa. The graphs predicted that the increased size of the gap, C and D cases,
4 led to a ventricular pressure increase of 5 to 7 kPa comparing to normal situation, Case A.

5 This model has made predictions of altered MR hemodynamics and a potential relationship to
6 left atrial pressure – this might have implications for LV and LA remodeling. Also, there may be
7 some comparisons to literature (e.g. clinical / experimental).

8 Time-dependent aortic pressure is displayed in **Fig 6**. No meaningful differences in pressure
9 were predicted for aortic blood-flow. These values ranged from peak pressures 22 kPa for a
10 ‘healthy’ model (Case A) to 25 kPa for severe MR (Case D. Fig 7 represents the pressure contours
11 at 0.2 s (during systole) for all cases.

12 **Discussions**

13 We have presented a model which has made predictions of altered MR hemodynamics and a
14 potential relationship to left atrial pressure. This might have implications for left ventricle and left
15 atrium remodeling. Comparison of four MR models showed different hemodynamic
16 characteristics based on the size of the gap between leaflets. The blood jet generated small vortexes
17 in mild and severe MRs.

18 Looking to the pressure contours, we found out that the absence of mitral regurgitation in model-
19 A leads to an increase of systolic pressure in the left ventricle. The results is in agreement with
20 Lassila et al [31] findings. On the other hand, Thomas et al [32] showed that peak ejection
21 velocity was seen to increase due to MR severity. This is also in agreement with our findings.

22 During the ventricular systolic phase the left ventricle contradiction, the rate of blood flow from
23 the mitral is very low or zero [33]. The leaflet close mechanism depends on the distance of ring

1 vortexes of each ventricle during systole [34]. These vortexes could not be modeled in the
2 commercial FE software. Therefore, the leaflets were considered as fixed components. This
3 assumption allowed the mitral valve was closed during systole and the blood flow showed no effect
4 on the leaflets. The limitation of this study was that we considered a fixed left ventricle wall which
5 could not mimic the ventricle failing to reproduce the necessary pressures during severe MR.
6 We believe that this is the first model which assesses mal-coaptation and its relationship with MR:
7 increasing MR velocity, left atrium pressure and other hemodynamic parameters. We also
8 hypothesize that the reduced aortic flow may not be due directly to MR but to increased difficulty
9 of the heart to pump blood. Although the obtained results were clinically shown but our work is
10 the first to link actual changes in coaptation to specific hemodynamic factors including pressure
11 and velocity. The success of this study opened the way for further development in to a clinical
12 tool. On the other hand, there were several limitations in our study which should be considered for
13 further studies. The inclusion of myocardium as well as endocardium and the influence of these
14 structures should be investigated therefore another fluid structure interaction model is required to
15 show these structures responses and the flow inside the left ventricle. Dynamic motion of leaflets
16 should also evaluated. It is also suggested to make more accurate anatomically model using three
17 dimensional echocardiography or new MRI sets.

18
19

20 **Conclusions**

21 An FSI model of the left side of the heart has been produced, from an MRI scan to study mitral
22 valve mal-coaptation. Increased mal-coaptation resulted in increased left atrial pressure, which
23 would presumably lead to enlargement (as seen clinically). A bigger gap between the leaflets led

1 to a large vortex within the left ventricle and higher blood velocity in the atrium. The pressure
2 adjacent to the mitral valve also increased with increased mal-coaptation. These findings have
3 implications not only for understanding alterations in pressure and velocity as a result of the MR
4 in the ventricle, atrium, or aorta, but also for providing a comprehensive numerical model suitable
5 for clinical translation. We believe that this model, along with improved version, is a powerful tool
6 for future clinical scenarios as it could capture the presence of MR. However, the model should be
7 improved in number of ways as mentioned before.

8

9 **Compliance with Ethical Standards**

10 **Funding:** None.

11 **Conflict of Interest:** None.

12 **Ethical approval:** Ethical approval was provided under the permission of Modarres Hospital,
13 Tehran, Iran.

1 **References**

- 2 [1] Smith PK, Puskas JD, Ascheim DD, Voisine P, Gelijns AC, Moskowitz AJ, Hung JW, Parides
3 MK, Ailawadi G, Perrault LP. Surgical treatment of moderate ischemic mitral regurgitation. *N Engl*
4 *J Med* 2014;371(23) : 2178-2188.
- 5 [2] Glower DD, Kar S, Trento A, Lim DS, Bajwa T, Quesada R, Whitlow PL, Rinaldi MJ,
6 Grayburn P, Mack MJ. Percutaneous mitral valve repair for mitral regurgitation in high-risk
7 patients: results of the EVEREST II study. *J Am Coll Cardiol* 2014; 64(2) : 172-181.
- 8 [3] Al-Atabi M, Espino DM, Hukins DW. Computer and experimental modelling of blood flow
9 through the mitral valve of the heart. *JBSE* 2010; 5(1):78-84.
- 10 [4] Anwar AM, Folkert J, Soliman OI. Clinical Recognition of Tricuspid Valve Disease. *Practical*
11 *Manual of Tricuspid Valve Diseases*, Springer ;2018. Chapter 3.
- 12 [5] Espino DM, Shepherd DE, Buchan KG. Effect of mitral valve geometry on valve competence.
13 *Heart vessels* 2007; 22(2): 109-115.
- 14 [6] Espino DM, Shepherd DE, Hukins DW. Transient large strain contact modelling: A
15 comparison of contact techniques for simultaneous fluid–structure interaction. *Eur. J. Mech.*
16 *B/Fluids* 2015; 51: 54-60.
- 17 [7] J.F. Wenk, Z. Zhang, G. Cheng, D. Malhotra, G. Acevedo-Bolton, M. Burger, T. Suzuki, D.A.
18 Saloner, A.W. Wallace, J.M. Guccione, M.B. Ratcliffe, First Finite Element Model of the Left
19 Ventricle With Mitral Valve: Insights Into Ischemic Mitral Regurgitation, *The Annals of Thoracic*
20 *Surgery* 89(5) (2010) 1546-1553.
- 21 [8] Stevanella M, Maffessanti F, Conti CA, Votta E, Arnoldi A, Lombardi M, Parodi O, Caiani
22 EG, Redaelli A. Mitral Valve Patient-Specific Finite Element Modeling from Cardiac MRI:
23 Application to an Annuloplasty Procedure. *Cardiovasc Eng Technol* 2011; 2(2): 66-76.

- 1 [9] Prot V, Haaverstad R, Skallerud B. Finite element analysis of the mitral apparatus: annulus
2 shape effect and chordal force distribution. *Biomech Model Mechanobiol* 2009; 8(1): 43-55.
- 3 [10] Votta E, Maisano F, Soncini M, Redaelli A, Montevecchi FM, Alfieri O. 3-D computational
4 analysis of the stress distribution on the leaflets after edge-to-edge repair of mitral regurgitation. *J*
5 *Heart Valve Dis* 2002;11(6): 810-822.
- 6 [11] Kunzelman KS, Quick DW, Cochran RP. Altered collagen concentration in mitral valve
7 leaflets: biochemical and finite element analysis. *Ann Thorac Surg* 1998; 66(6):198-205.
- 8 [12] Lassila T, Malossi C, Stevanella M, Votta E, Redaelli A, Deparis S. Simulation of left
9 ventricle fluid dynamics with mitral regurgitation from magnetic resonance images with fictitious
10 elastic structure regularization, arXiv:1707.03998 [physics.med-ph] ;2017.
- 11 [13] Wang Y, Quaini A, Čanić S, Vukicevic M, Little SH. 3D experimental and computational
12 analysis of eccentric mitral regurgitant jets in a mock imaging heart chamber. *Cardiovasc Eng*
13 *Technol* 2017;8(4):419-438.
- 14 [14] Sonntag SJ, Li W, Becker M, Kaestner W, Büsen MR, Marx N, Merhof D, Steinseifer U.
15 Combined computational and experimental approach to improve the assessment of mitral
16 regurgitation by echocardiography. *J Bioeng* 2014;42(5): 971-985.
- 17 [15] Al-Atabi M, Espino DM, Hukins DW, Buchan KG. Biomechanical assessment of surgical
18 repair of the mitral valve. *Proc Inst Mech Eng H* 2012; 226(4): 275-287.
- 19 [16] Bahraseman HG, Hassani K, Khosravi A, Navidbakhsh M, Espino DM, Kazemi-Saleh D,
20 Fatourae N. Estimation of maximum intraventricular pressure: a three-dimensional fluid–
21 structure interaction model. *Biomed Eng Online* 2013;12(122).
- 22 [17] Bahraseman HG, Languri EM, Yahyapourjalaly N, Espino DM .Fluid-structure interaction
23 modeling of aortic valve stenosis at different heart rates. *Acta Bioeng Biomech* 2016;18 (3):11-20.

- 1 [18] Burriesci G, Howard I, Patterson E. Influence of anisotropy on the mechanical behaviour of
2 bioprosthetic heart valves. *J Med Eng Technol* 1999; 23(6): 203-215.
- 3 [19] Burriesci G, Marincola FC, Zervides C. Design of a novel polymeric heart valve. *J Med Eng*
4 *Technol* 2010; 34(1): 7-22.
- 5 [20] Hall JE. *Guyton and Hall textbook of medical physiology*. Philadelphia: Saunders Elsevier;
6 2011.
- 7 [21] Espino DM, Shepherd DE, Hukins DW. Evaluation of a transient, simultaneous, arbitrary
8 Lagrange–Euler based multi-physics method for simulating the mitral heart valve. *Comput*
9 *Methods Biomech Biomed Eng* 2014;17(4): 450-458.
- 10 [22] Carty G, Chatpun S, Espino DM. Modeling blood flow through intracranial aneurysms: a
11 comparison of Newtonian and non-Newtonian viscosity. *J Med Biol Eng* 2016;36(3): 396-409.
- 12 [23] Karimi A, Navidbakhsh M, Razaghi R, Haghpanahi M. A computational fluid-structure
13 interaction model for plaque vulnerability assessment in atherosclerotic human coronary arteries.
14 *J. Appl. Phys* 2014;115(14).
- 15 [24] Karimi A, Navidbakhsh M, Razaghi R. Plaque and arterial vulnerability investigation in a
16 three-layer atherosclerotic human coronary artery using computational fluid-structure interaction
17 method. *J. Appl. Phys* 2014;116(6).
- 18 [25] Astorino M, Gerbeau JF, Pantz O, Traoré KF. Fluid–structure interaction and multi-body
19 contact: application to aortic valves. *Comput Methods Appl Mech Eng* 2009;198(45):3603-3612.
- 20 [26] Baccani B, Domenichini F, Pedrizzetti G. Vortex dynamics in a model left ventricle during
21 filling. *Eur. J. Mech. B/Fluids* 2002; 21(5):527-543.

- 1 [27] Oncel D, Oncel G, Tastan A. Effectiveness of dual-source CT coronary angiography for the
2 evaluation of coronary artery disease in patients with atrial fibrillation: initial experience.
3 *Radiology* 2007; 245(3): 703-711.
- 4 [28] Tang D, Pedro J, Yang C, Zuo H, Huang X, Rathod RH, Gooty V, Tang A, Wu Z, Billiar KL.
5 Patient-specific MRI-based right ventricle models using different zero-load diastole and systole
6 geometries for better cardiac stress and strain calculations and pulmonary valve replacement
7 surgical outcome predictions. *PLoS ONE* 2016; 11(9).
- 8 [29] Elbaz MS, Van der Geest RJ, Calkoen EE, De Roos A, Lelieveldt BP, Roest AA, Westenberg
9 JJ. Assessment of viscous energy loss and the association with three-dimensional vortex ring
10 formation in left ventricular inflow: In vivo evaluation using four-dimensional flow MRI. *Magn*
11 *Reson Med* 2017;77(2): 794-805.
- 12 [30] Suito H, Takizawa K, Huynh VQ, Sze D, Ueda T, Tezduyar TE. A geometrical-characteristics
13 study in patient-specific FSI analysis of blood flow in the thoracic aorta. *Advances in*
14 *Computational Fluid-Structure Interaction and Flow Simulation*, Springer 2016, pp. 379-386.
- 15 [31] Lassila T, Malossi C, Stevanella M, Votta E, Redaelli A, Deparis S. Simulation of left
16 ventricle fluid dynamics with mitral regurgitation from magnetic resonance images with fictitious
17 elastic structure regularization. *arXiv:1707.03998 [physics.med-ph]*.
- 18 [32] Thomas L, Foster E, Schiller NB. Peak Mitral Inflow Velocity Predicts Mitral Regurgitation
19 Severity. *J Am Coll Cardiol* 1998;31(1).
- 20 [33] Konishi T, Funayama N, Yamamoto T, Hotta D, Kikuchi K, Ohori K, Nishihara H, Tanaka
21 S. Severe mitral regurgitation due to mitral leaflet aneurysm diagnosed by three-dimensional
22 transesophageal echocardiography: a case report. *BMC Cardiovasc Disord* 2016;16(1): 234.

1 [34] Vaziri SM, Larson MG, Lauer MS, Benjamin EJ, Levy D. Influence of blood pressure on left
2 atrial size. *J Hypertens* 1995;25(6): 1155-1160.

3

