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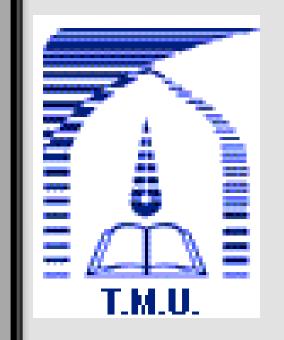
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Bonding characteristics of glass seal/metallic interconnect for SOFC applications: Comparative study on chemical and mechanical properties of the interface

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Introduction:

Glass and glass-ceramics have been extensively used as seal material in planar solid oxide fuel cell (SOFC) stack. The main objective of the present work was to investigate the joining properties of a silicate based glass-ceramic as seal material with two different ferritic stainless alloys as interconnect, i.e. SS430 and Crofer 22APU.

For a straight-forward approach to evaluate sealing materials, sandwiched samples will allow interfacial situation of a glass-ceramic material. A convenient method for determining the interfacial fracture energies is double cantilever beam (DCB) test. The method allows to measure the crack-growth resistance of these materials to be able to use fracture mechanics design methods. Stable crack growth is necessary to get reliable and unambiguous fracture toughness data. If the fracture toughness values are determined from test configurations that do not allow stable crack growth, then the measurement may be related more to crack initiation than crack growth. In such cases, the calculated value of the fracture toughness may depend on the geometry of the machined notch.

Tasks:

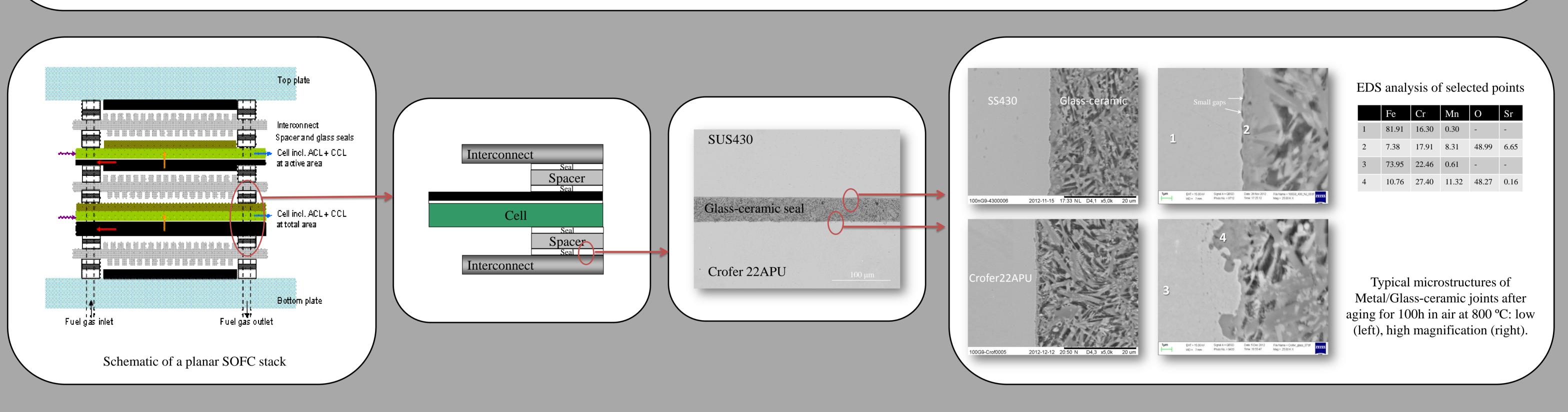
 \blacktriangleright A glass was synthesized with the nominal composition of 30–50 mol%SiO₂, 0–10 mol%B₂O₃, 5-15 mol% Al₂O₃, 25-50 mol% SrO, 0-25 mol% CaO, and 3 mol% (8.16 wt.%) Y₂O₃. ≻Joint samples of metal/glass/metal were prepared at 850° C for 0.5 h under air and then cooled down to 800° C and aged for 100h. ≻Chemical characterization was conducted on glass/metal interfaces by SEM+EDS. ≻Mechanical characterization was conducted by double cantilever beam (DCB) and nanoindentation testing (NIT) methods.

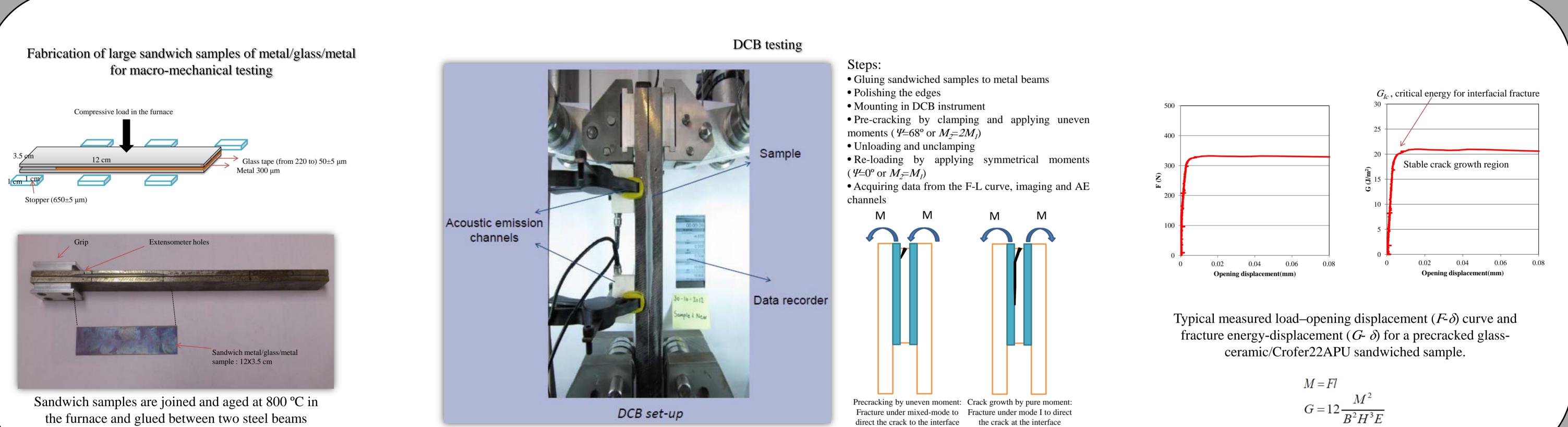
Thermal properties of the sealing glass

$T_g \pm 3$ (°C) from dilatometry	T _S (°C)	CTE (X10 ⁻⁶ K ⁻¹)
695	738	10.0

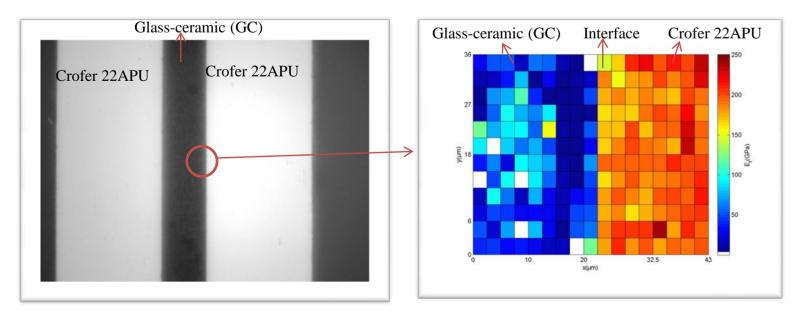
Aim:

≻Correlating between chemical and mechanical properties of seal/interconnect interfaces is the main topic of this research.





Fabrication of small sandwich samples of metal/glass/metal for microscopy and nano-mechanical testing



Optical micrograph of Crofer22APU/glass-ceramic/Crofer22APU (left) and reduced elastic modulus map for the selected area



Interphases

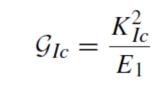
Fracture surface to XRD, including glass + metal strip (SS430 or Crofer22APU)

The XRD peaks revealed the main crystalline compounds formed from the bulk glass are Ca₄Y₆O(SiO₄)₆, Y₂Si₂O₇, SrAl₂Si₂O₈, CaSiO₃, (Ca-Sr)SiO₃, SrSiO₃.

Additional compound characterized at the interface of fractured samples, as interphases, include: MnCr₂O₄, $Ca_{3,11}Mn_{2,89}Si_6O_{18}, Mn_5O_{15}Si_5, Mn_4Sr_7O_{12}.$

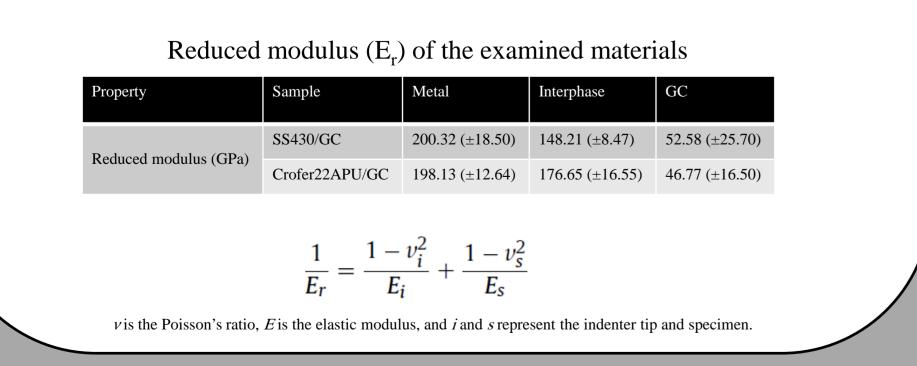
Fracture toughness of joint samples

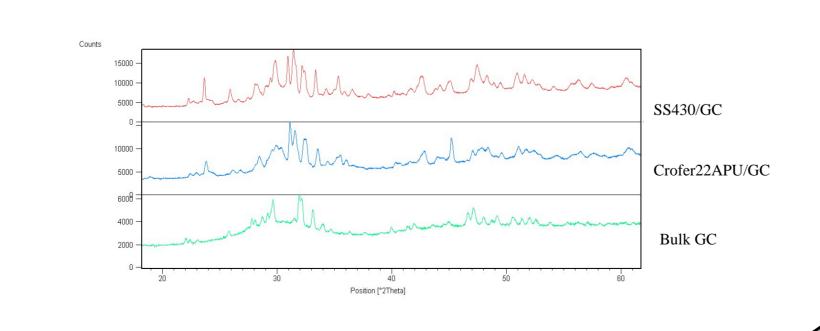
From the critical energy release rate, G_{Ic} , under elastic conditions, the critical plane stress Mode I stress intensity factor can be evaluated by [4]:



Fracture toughness values of the current work with the limited data reported in literature are compared:

K_{IC} of different metal/glass-ceramic after aging					
SS430/GC	Crofer22APU/GC	JS3 steel/Glass73*	JS3 steel/Glass25*		
1.43 (±0.14)	1.91 (±0.08)	$1.58(\pm 0.22)$	1.54 (±0.28)		





Summary:

✓A technique for evaluating the critical energy-release rate/fracture toughness of thin glassceramic layers and stainless steel metal strips is described.

 \checkmark The approach involves a new specimen geometry, in which a sandwich sample is glued onto thicker steel beams.

 \checkmark The advantages of the technique, stable crack growth, allows fracture energy and toughness of a desired joint materials to be evaluated.

✓ The fracture toughness for crack initiation was measured with a very good reproducibility.

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*Ref. [5]

Data of ref. [5] are for bimaterial notched specimens to determine the interfacial fracture energies and toughness of glass-ceramic sealants in planar SOFCs, corresponded to a given mode mixity, and the asdetermined fracture energies and toughness values are related to the materials used and the mode mixity realized. Changing the loading configuration or specimen type will affect the mode mixity value, and, as a consequence, the fracture energy and toughness will change.

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