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# Radiation damage in the LHCb vertex locator

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ABSTRACT: The LHCb Vertex Locator (VELO) is a silicon strip detector designed to reconstruct charged particle trajectories and vertices produced at the LHCb interaction region. During the first two years of data collection, the 84 VELO sensors have been exposed to a range of fluences up to a maximum value of approximately  $45 \times 10^{12}$  1 MeV neutron equivalent (1 MeV n<sub>eq</sub>). At the operational sensor temperature of approximately  $-7^{\circ}$ C, the average rate of sensor current increase is  $18 \mu A$  per fb<sup>-1</sup>, in excellent agreement with predictions. The silicon effective bandgap has been determined using current versus temperature scan data after irradiation, with an average value of  $E_g = 1.16 \pm 0.03 \pm 0.04 \,\text{eV}$  obtained. The first observation of  $n^+$ -on-n sensor type inversion at the LHC has been made, occurring at a fluence of around  $15\times10^{12}$  of 1 MeV n<sub>eq</sub>. The only  $n^+$ -on-p sensors in use at the LHC have also been studied. With an initial fluence of approximately  $3 \times 10^{12}$  1 MeV n<sub>eq</sub>, a decrease in the Effective Depletion Voltage (EDV) of around 25 V is observed. Following this initial decrease, the EDV increases at a comparable rate to the type inverted  $n^+$ -on-*n* type sensors, with rates of  $(1.43 \pm 0.16) \times 10^{-12} \text{ V} / 1 \text{ MeV } n_{eq}$  and  $(1.35 \pm 0.25) \times 10^{-12} \text{ V} / 1 \text{ MeV} n_{eq}$  measured for  $n^+$ -on-p and  $n^+$ -on-n type sensors, respectively. A reduction in the charge collection efficiency due to an unexpected effect involving the second metal layer readout lines is observed.

KEYWORDS: Radiation damage evaluation methods; Particle detectors

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## 1 Introduction

The VErtex LOcator (VELO) is a silicon strip detector positioned around the proton-proton interaction region at the LHCb [1] experiment. To obtain the precision vertexing required for heavyflavour physics, the closest active silicon sensor region is located 8.2 mm from the beam axis, while the silicon edge is located at a distance of 7 mm. For the luminosity delivered by the LHC in 2010 and 2011, the VELO was exposed to higher particle fluences than any other silicon detector at the LHC. Careful monitoring of radiation damage to the sensors is essential to ensure the quality of data for LHCb physics analyses and to provide information relevant to the eventual detector replacement and upgrade.

During proton injection and energy ramping the LHC beams are wider and less stable than the beams used for data taking. To prevent damage to the silicon sensors, the VELO consists of two halves retractable by 29 mm in the horizontal plane. Each half contains 42 half-disc shaped silicon-strip sensors. When the beams are in a stable orbit, the two VELO halves are closed such that the colliding beams are surrounded by the silicon sensors. Half of the sensors have strips orientated in an approximately radial direction ( $\phi$ -type) and the other half perpendicular to this (Rtype), as shown in figure 1. A detector module consists of an R-type and a  $\phi$ -type sensor glued to a common support in a back-to-back configuration. Track coordinates are measured using the charge collected by the two sensors in a module. All but two of the VELO sensors are oxygenated  $n^+$ -on-nsensors, consisting of an n-type implant on a n-type bulk with a backplane  $p^+$ -type implant. Two



**Figure 1**. A schematic representation of an R-type and a  $\phi$ -type sensor, with the routing lines orientated perpendicular and parallel to the silicon strips, respectively.

**Table 1**. The VELO sensor design parameters. The sensor position along the beam axis is given relative to the beam interaction region.

Parameter	Value
Silicon thickness	300 µm
Strip pitch	$40-120\mu m$
Strip width	$11 - 38  \mu m$
Routing line width	$\sim 11\mu m$
Inner silicon edge to beam axis	7 mm
Radial distance of active strips from beam axis	8.2–42 mm
Sensor position along beam-axis	-300 to $750$ mm
Oxygen enhancement	$> 1  \mathrm{x}  10^{17}  \mathrm{cm}^{-3}$

oxygenated  $n^+$ -on-*p* silicon sensors are installed at one end of the VELO, intended to be a test of one of the leading LHC silicon-upgrade candidates in an operational environment. A summary of the silicon sensor properties is given in table 1.

Each  $n^+$  implant is read out via a capacitively coupled *first metal layer* running along its length. The R-type strips and inner  $\phi$ -type strips do not extend to the outer region of the sensor. Therefore each strip is connected via a metal routing line to the edge of the sensor where the readout electronics are located. The routing lines are referred to as the *second metal layer* and are insulated from the bulk silicon and first metal layer by  $3.8 \pm 0.3 \,\mu\text{m}$  of SiO<sub>2</sub>. For R-type sensors, the routing lines are positioned perpendicular to the sensor strips, whilst for the  $\phi$ -type they are positioned directly above and parallel to the strips.

This paper presents studies of radiation damage in the VELO sensors using data collected during 2010 and 2011. Section 2 describes studies of sensor currents as a function of voltage and temperature. In section 3 the effects of radiation are monitored by measuring the charge collection efficiency and noise as a function of bias voltage. An unexpected decrease in clustering efficiency due to an effect involving the second metal layer is described in section 4. The results from the various studies are summarised in section 5.



**Figure 2**. Currents measured in the VELO for each sensor as a function of time (bottom). The luminosity delivered to LHCb and the average sensor temperature is shown over the same time scale (middle and top). Increases in the delivered luminosity are matched by increases in the sensor currents. The mean measured current agrees well with the prediction from simulation, which is described in section 2.4. The mean measured value excludes sensors that are surface-current dominated.

#### 2 Current evolution

The leakage current in a silicon sensor varies linearly with fluence for a wide range of silicon substrates [2]. This predictability provides a simple and accurate method of relating sensor currents to the amount of particle fluence accumulated by a sensor. This section presents an analysis of sensor currents in order to monitor radiation damage in the VELO.

#### 2.1 Interpretation of sensor current measurements

Each VELO sensor is biased through a high-voltage connection to the backplane, and a common ground connection to the bias line and innermost guard ring on the strip side. Therefore a single current is measured, corresponding to the current drawn by the entire sensor. The raw measured currents are shown as a function of time in figure 2, for sensors operated at the nominal bias voltage of 150 V and at a mean temperature of approximately  $-7^{\circ}$ C. The temperature is measured with thermistors positioned on the readout hybrid near the silicon on each side of the module. The difference betwen the average thermistor temperature and the silicon temperature was measured in vacuum during production with a thermal camera as  $3.2 \pm 1.6^{\circ}$ C [3]. During the early running period, the majority of the sensors had small currents, with a few exceptions that had currents of up to 40 µA. With sensor irradiation the bulk currents have increased. The spread of the measured currents is partly due to the difference in the sensor positions relative to the interaction point, but is dominated by variations in the sensor temperatures. The occasional dips in the currents are related to short annealing periods in which the cooling systems were switched off.

The measured currents contain contributions from two dominant sources, generically referred to as *bulk* and *surface* currents. The bulk currents vary exponentially with temperature and have a



Figure 3. The current versus temperature for two VELO sensors operated at the nominal 150 V bias. Before irradiation there is a small exponential component for the sensor shown in figure **a**), while that shown in figure **b**) is dominated by the non-temperature dependent surface current contribution. After irradiation, a large exponential component is seen for both sensors. These sensors are now bulk current dominated and the surface current has largely been annealed.

precisely predicted relationship with fluence. Surface currents arise due to irregularities introduced during sensor production such as process errors, scratches, guard rings and non-uniformities in the cut edges. Some of these contributions may have an exponential dependence on temperature [4], however the surface currents measured in VELO sensors are predominantly characterised by an Ohmic increase in current with bias voltage. In the majority of sensors the Ohmic surface current is seen to anneal with particle fluence. An analysis of VELO sensor currents as a function of bias voltage (IV scan) is described in detail in ref. [5].

For the VELO sensors the pre-irradiation exponential contribution is very small and is assumed to consist of a mixture of bulk and surface currents. The relative contribution of bulk and surface current is identified by measuring the current as a function of temperature (IT scan), as shown in figure 3. This method is described in detail in ref. [3].

#### 2.2 The effective band gap

In the temperature range of interest, the bulk current is expected to scale according to,

$$I(T) \propto T^2 \exp\left(-\frac{E_g}{2kT}\right),$$
 (2.1)

where T is the temperature in Kelvin and k is the Boltzmann constant. The constant  $E_g$  is related to the bandgap energy and an effective value of 1.21 eV is assumed for the temperature range of interest [6]. Using this function the sensor currents can be normalised to a common temperature. In addition, the current variation as a function of temperature can be fitted to measure  $E_g$  in the VELO sensors. A summary of the results obtained from several IT scans is presented in table 2. The statistical uncertainty quoted is the width of a Gaussian fitted to the distribution of the measured

Delivered luminosity	Bias voltage	$E_g$
$[fb^{-1}]$	[V]	[ eV ]
0.48	100	$1.17 \pm 0.07 \pm 0.04$
0.48	150	$1.18 \pm 0.05 \pm 0.04$
0.82	150	$1.14 \pm 0.06 \pm 0.04$
1.20	150	$1.15 \pm 0.04 \pm 0.04$

**Table 2**. The effective band gap,  $E_g$ , measured following various amounts of delivered luminosity. The first uncertainty is statistical and the second is systematic.

values from all sensors. The largest source of systematic uncertainty is related to the accuracy with which sensor temperatures are known, and the choice of the temperature fitting range [3].

The weighted average of the measured values is  $E_g = 1.16 \pm 0.03 \pm 0.04 \text{ eV}$ , which is statistically compatible with the expected value of 1.21 eV from the literature [6]. Recent studies [6] have shown that discrepancies can occur due to sensor self-heating, in which case  $E_g$  is measured to be systematically high. In addition, dependencies of  $E_g$  on the sensor bias voltage have been observed. However, the VELO sensors used for these measurements were cooled and sufficiently biased at 150 V, such that these effects should not significantly influence the result. This is supported by the consistency of the cross-check measurement made at 100 V.

#### 2.3 Fluence determination

With a good understanding of the annealing conditions, changes in current can be related to the particle fluence incident on a sensor. The expected change in leakage current at room temperature is given by the relation,

$$\Delta I = \alpha \phi V_{Si},\tag{2.2}$$

where  $\alpha$  is the leakage current damage constant [2] in units A cm<sup>-1</sup>,  $\phi$  is the fluence in units of number of particles per cm<sup>2</sup>, and  $V_{Si}$  is the silicon volume in cm<sup>3</sup>. The leakage current damage constant has been shown to evolve in time, t, with the temperature T(t) following an Arrhenius relation,

$$\alpha(t) \propto \exp\left(-\frac{E_I^*}{kT(t)}\right),$$
(2.3)

where  $E_I^*$  is the activation energy for which a value of  $1.30 \pm 0.14 \text{ eV}$  has been derived from a fit [2]. In order to estimate the appropriate value of  $\alpha$  for our data, we proceed as follows. The sensor temperatures are recorded for each minute of operation and corrected to an equivalent time at 21 °C. The delivered integrated luminosity,  $\mathcal{L}$ , is folded with this equivalent time to produce an effective value of  $\alpha \phi$  to be used in eq. 2.2. This procedure [3] yields a value for  $\alpha \mathcal{L}$  of  $4.8 \times 10^{-17} \text{ A fb}^{-1} \text{ cm}^{-1}$  at the total delivered luminosity of  $1.2 \text{ fb}^{-1}$ , corresponding to an effective value for  $\alpha$  of  $6 \times 10^{-17} \text{ A cm}^{-1}$ .

Fluences simulated with GEANT4 in the LHCb detector are folded with particle damage factors using the NIEL scaling hypothesis [7]. The damage caused by high energy particles in the bulk material is parameterised as proportional to a displacement damage cross section, *D*. A displacement damage cross section of 95 MeV mb for 1 MeV neutrons,  $D_n(1 \text{ MeV})$ , is assumed and each particle, *i*, is assigned an energy-dependent hardness factor,  $k_i$ ,

$$k_i(E) = D_i(E)/D_n(1 \,\mathrm{MeV}), \qquad (2.4)$$

which can be used to estimate the damage in the material. The total damage is expressed as a multiple of the expected damage of a 1 MeV neutron (referred to as 1 MeV neutron equivalent, or 1 MeV  $n_{eq}$ ). This technique has been shown to be highly effective for describing the evolution of the leakage current. For this analysis, every particle in the simulation that is incident on a VELO sensor is assigned a displacement damage cross-section, or cross-section per silicon atom, using as reference a set of tabulated values from ref. [8].

The fluence varies with the geometric location of the sensors in the VELO, as shown for simulated events in figure 4. It decreases with radial distance from the beam with an approximate  $1/r^{1.75}$  dependence. The effect of the position along the beam-pipe (*z*-direction) and angle of the particle with respect to the the silicon sensor are also both significant and are taken into account in the calculation of the fluence incident on a sensor. The predicted fluence is assigned an uncertainty of ~8% which is dominated by uncertainties due to particles with no available displacement damage data. The average measured current increase for the sensors at the operational temperature of approximately  $-7^{\circ}C$  (and including several annealing periods) is ~18 µA per fb<sup>-1</sup>.

#### 2.4 Predicted currents

With the relationship between integrated luminosity and damaging fluence established, the expected change in leakage current due to radiation damage can be predicted. The integrated luminosity is taken from the LHCb online measurement. Predictions are shown to agree with the measured currents, as shown in figure 5. The predictions have an associated uncertainty of approximately 10%, estimated by adding the uncertainties for the integrated luminosity (5%), the annealing factor (3%) and the damaging fluence prediction (8%) in quadrature. The predicted leakage current is on average within 5% of the measured current.

## **3** Depletion voltage studies

The depletion voltage, defined as the reverse bias voltage required to fully deplete a sensor, has been monitored as a function of the delivered luminosity. For fluences delivered to the VELO within the first few years of operation, the change in depletion voltage for an  $n^+$ -on-n type sensor should be accurately described by the Hamburg model [9], where the parameter values given in [10] have been used. The effective doping of the n-bulk changes over time due to radiation-induced defects. Dominant mechanisms are expected to be the inactivation of phosphorous dopants in combination with the introduction of acceptors. This leads to an initial decrease in the depletion voltage of the  $n^+$ -on-n sensors to a value close to 0V. The n-type bulk inverts and becomes p-type, after which further irradiation leads to an increase in depletion voltage. Eventually, the bias voltage required to obtain sufficient charge from a sensor will cause electrical breakdown in the silicon or exceed the 500 V hardware limit, thus limiting the useful lifetime of the silicon detector. For an



**Figure 4.** a) The fluence from  $1 \text{ fb}^{-1}$  of integrated luminosity versus radius for two VELO sensors, as seen in simulated proton-proton collisions at a 7 TeV centre-of-mass energy. **Top b**) In each sensor, the fluence as a function of radius is fitted with the function  $Ar^k$ . The fitted exponent, k, is shown as a function of the sensor *z*-coordinate, where *z* is the distance along the beam-axis that a sensor is from the interaction region. The distribution of the fluence across the sensor is seen to become flatter with increasing distance from the interaction region. **Bottom b**) The fluence at the innermost radius of the sensor against the sensor *z*-coordinate.



**Figure 5**. The leakage current against sensor *z*-coordinate after  $1.20 \text{ fb}^{-1}$  of integrated luminosity, normalised to  $0^{\circ}$ C. The data are in agreement with predictions, represented by the shaded region. The two VELO halves are referred to as the A and C sides of the VELO.

oxygenated  $n^+$ -on-p type sensor irradiated with charged hadrons there are expected to be competing mechanisms. The detailed and complex role of oxygen is discussed in [11].

Following manufacture the depletion voltage of each VELO sensor was measured by comparing the capacitance (C) at different bias voltages (V) [12]. It is not possible to implement this technique after VELO installation and so alternative methods are used to extract information on the depletion voltage. This section presents results from two such studies: Charge Collection Efficiency and noise scan studies.

#### 3.1 Charge collection efficiency

The amount of charge collected by an under-depleted silicon strip increases with the bias voltage applied. When the sensor is fully depleted, any further increase in bias voltage will not increase the amount of charge collected (given a sufficient signal collection time and before radiation induced charge trapping effects become significant). The relationship between the Charge Collection Efficiency (CCE) and the applied bias voltage has been exploited to measure a property of the sensor analogous to the depletion voltage, referred to as the Effective Depletion Voltage (EDV).

#### 3.1.1 Effective depletion voltage determination

The nominal operational voltage of the VELO sensors is 150V. For the CCE analysis, collision data is recorded with every fifth module operated at a voltage ranging between 0 and 150V. The remaining modules are maintained at 150V. Sensors with variable voltage are referred to as *test* sensors. The test sensors are removed from the reconstruction algorithms such that only hits from the 150V operated sensors are used to reconstruct particle tracks. A track is extrapolated to a coordinate on the test sensor and the set of five strips nearest to this coordinate are searched for deposited charge. This provides unbiased information on the amount of charge deposited by the particle as a function of bias voltage. At each bias voltage the pedestal-subtracted ADC distribution is fitted using a Gaussian convoluted with a Landau function. This is used to determine the Most Probable Value (MPV) of the ADC distribution. At large bias voltages the MPV of the ADC distribution reaches a plateau. The MPV of a Landau function for a fit to an unirradiated Phi sensor is 37.1 ADC counts [13], this is expected to correspond to approximately 23,400 electrons [14–16].

The EDV is defined as the voltage at which the MPV of a sensor is equal to 80% of the plateau ADC value, as shown in figure 6. The threshold of 80% was chosen as it gives closest agreement with depletion voltages determined from pre-irradiation CV measurements [12]. For unirradiated sensors, the difference in the values obtained using the CV method and the EDV method is less than 10 V.

Differences between the depletion voltage and EDV are expected near to sensor type-inversion. The depletion voltage is expected to decrease to a value of approximately 0 V, whereas the minimum EDV is dictated by the smallest potential difference required to collect charge from the silicon strips, which in turn depends on the shaping time of the electronics. When operated with a 25 ns signal shaping time, the smallest EDV that can be measured in the VELO sensors is approximately 20 V. The EDV is therefore not an accurate estimate of the depletion voltage below this value.



**Figure 6. a)** The pedestal subtracted ADC distributions for an R-type sensor at three example bias voltages. **b)** The MPV of the fit to the ADC distribution vs. bias voltage. The dashed lines represent the ADC that is 80% of the plateau value, and the corresponding EDV.

#### 3.1.2 Bulk radiation damage

Between April 2010 and October 2011 five dedicated CCE scans were taken, corresponding to delivered luminosities of 0, 0.04, 0.43, 0.80 and  $1.22 \,\text{fb}^{-1}$ . As the fluence delivered to the sensors varies significantly with sensor radius, each sensor is divided into 5 radial regions such that the fluence does not change by more than a factor of two across a region. The change in EDV with irradiation for a particular  $n^+$ -on-n type sensor is shown in figure 7(a). Initially the EDV is found to decrease with fluence across all radial regions, as predicted by the Hamburg model. The rate of decrease is greater in the inner radial regions of the sensor, consistent with expectations that these regions are exposed to higher fluence. The innermost region undergoes an increase in EDV between 0.80 and  $1.22 \,\text{fb}^{-1}$  of delivered luminosity, indicating that this part of the sensor has undergone type inversion. The  $n^+$ -on-p type sensors exhibit a decrease in EDV with initial fluence, as shown in figure 7(b). This effect has been previously observed, for instance in [17, 18]. A potential cause, given in [19], is the removal of substitutional boron due to silicon self-interstitials. The resulting boron interstitials then diffuse out, eventually forming a stable defect with oxygen.

The global change in EDV is determined by combining the data from many of the VELO sensors with the predicted fluence (see section 2.3), as shown in figure 8. Sensors are divided into categories based on their initial EDVs. The irradiation-induced change in the depletion voltage of  $n^+$ -on-n type sensors is modeled as a function of time, temperature and fluence by the Hamburg Model. It has three components: a short term annealing component, a stable damage component and a reverse annealing component. Taking into account the LHCb luminosity measurements and VELO sensor temperature readings, the Hamburg model predictions can be compared to data, as shown by the overlaid curves in figure 8. Good agreement is found for low fluences, and for higher fluences after type inversion. It is assumed that the sensors type invert at a fluence near to the EDV minimum. For all  $n^+$ -on-n type sensors this occurs at approximately the same fluence of  $(10-15) \times 10^{12} 1 \,\text{MeVn}_{eq}$ . The behaviour after inversion is found to be independent of the initial EDV of the sensor, with an approximately linear increase in EDV with further fluence. A



**Figure 7.** a) The EDV against sensor radius for an  $n^+$ -on-*n* type sensor for each of the CCE scans. The dashed line shows the mean EDV across all radius regions prior to sensor irradiation, where some  $0 \text{ fb}^{-1}$  data points are not present due to low statistics. b) A similar plot for the  $n^+$ -on-*p*,  $\phi$ -type sensor. The minimum EDV is ~40V, which is significantly higher than the minimum at ~20V observed for the  $n^+$ -on-*n* type sensor.



**Figure 8.** The EDV against fluence for VELO sensors of various initial EDV. The EDV from data is compared to depletion voltages predicted by the Hamburg model, with good agreement observed prior to, and after sensor type-inversion.

linear fit to the data gives a voltage increase with fluence of  $(1.35 \pm 0.25) \times 10^{-12} \text{ V}/1 \text{ MeV } n_{eq}$ . For the  $n^+$ -on-p type, the initial decrease in EDV occurred up to a fluence of approximately  $2 \times 10^{12} 1 \text{ MeV } n_{eq}$ . After this the EDV has increased with further fluence. The rate of increase is measured to be  $(1.43 \pm 0.16) \times 10^{-12} \text{ V}/1 \text{ MeV } n_{eq}$ , similar to that of the type inverted  $n^+$ -on-n type sensors.

The EDV of the  $n^+$ -on-p type sensors begins to increase having received significantly less

fluence than the  $n^+$ -on-n type sensors. If the comparable rate of EDV increase is maintained with further fluence then the  $n^+$ -on-p type sensors will reach an EDV of 500 V, the hardware limit of the VELO system, after receiving approximately  $35 \times 10^{12}$  1 MeV n<sub>eq</sub> less fluence than the  $n^+$ -on-n type sensors. It is expected that the  $n^+$ -on-n sensors will reach the 500 V limit following a fluence of approximately  $380 \times 10^{12}$  1 MeV n<sub>eq</sub>.

The amount of charge collected is expected to change with fluence due to radiation induced changes to the silicon, radiation charge trapping effects are discussed in for example [20]. For  $\phi$ -type sensors the MPV has decreased by approximately 4% in the most irradiated regions, having received a fluence of  $40 \times 10^{12}$  1 MeV n<sub>eq</sub>. However, an even larger reduction of approximately 8% is found in the inner regions of the R-type sensors, having received a comparable fluence. This is due to a charge loss mechanism related to the second metal layer of the R-type sensors, which is described in detail in section 4. The outer regions of the sensor are most significantly affected, with decreases of approximately 12% observed following a fluence of just  $2 \times 10^{12}$  1 MeV n<sub>eq</sub>.

#### 3.2 Noise scans

The CCE scan data described in section 3.1 requires proton beams, and so is collected at the expense of physics data. A second method has been developed to monitor radiation damage, using the relationship between the intrinsic electronic noise of the pre-amplifier and the capacitance of the sensor. Data scans for this study can be collected regularly as proton collisions are not required.

In undepleted silicon, several sources of input capacitance are identified, the most dominant of which is the inter-strip impedance. For  $n^+$ -on-*n* sensors before type inversion, the depletion region grows with increasing voltage from the backplane (the opposite side to the strips). When the sensor is fully depleted the space-charge reaches the strips and the inter-strip resistance increases by several orders of magnitude, resulting in a decrease in sensor noise [21, 22]. For  $n^+$ -on-*n* type sensors following type inversion and  $n^+$ -on-*p* type sensors, the depletion region grows from the strip side of the silicon. In this situation the strips are immediately isolated at the application of a bias voltage and the relationship between noise and voltage cannot be exploited to extract information related to the depletion voltage.

The intrinsic noise in VELO sensors is determined by subtracting the mean ADC value (or *pedestal*) and a common-mode noise term. Figure 9 shows the inverse of the intrinsic noise as a function of voltage for an  $n^+$ -on-n and  $n^+$ -on-p type sensor. For the  $n^+$ -on-p before and after irradiation, and  $n^+$ -on-n after irradiation (having type inverted) the distribution is flat, thus little information related to the sensor depletion voltages can be extracted. For the  $n^+$ -on-n type sensor prior to type inversion, an increase in voltage results in a decrease in noise until a plateau is reached when the sensor is fully depleted.

The noise scan data can be used to identify whether an  $n^+$ -on-n type sensor has undergone type inversion. Only R-type sensors are investigated as the strip orientation allows the identification of strips that have been subject to a specific fluence. Following a delivered luminosity of approximately  $0.80 \,\text{fb}^{-1}$ , 40 of the sensors are identified as having type-inverted in the first radial region (8–11 mm), while in the second region (11–16 mm) 21 sensors are identified. Similar information can be extracted from the CCE data, with a sensor region defined as type-inverted when the measured EDV has reached a minimum and subsequently begun to increase. Following the same luminosity, the CCE method identified 21 and 5 type-inverted sensors in the first and second



**Figure 9.** The inverse of the sensor noise against bias voltage for a particular  $n^+$ -on-n and  $n^+$ -on-p type sensor, for two values of integrated luminosities. The C-V scan measured initial depletion voltages are shown by the dashed lines.

radial regions, considerably fewer than the noise method. This discrepancy is understood by examination of figure 8, in which the minimum of the Hamburg model prediction and the point at which the EDVs begin to increase are separated by a fluence of approximately  $10 \times 10^{12}$  1 MeV n<sub>eq</sub>. The noise scan method is not subject to the same fluence lag. Following a delivered luminosity of  $1.2 \text{ fb}^{-1}$ , the CCE method identifies 39 and 21 sensors in the two radial regions. This is in good agreement with the noise method, with the same 39 and 21 sensors identified by each method.

## 4 Charge loss to the second metal layer

All physics analyses at LHCb rely on efficient track reconstruction using clusters from the VELO sensors. A cluster is defined as one or several adjacent strips with charge above a particular threshold [13]. The data samples described in section 3.1 are also used to measure the Cluster Finding Efficiency (CFE), by looking for the presence of a cluster at the track intercept on the test sensor. Before irradiation the mean CFE of the VELO sensors was greater than 99% [13]. After irradiation the CFE in many sensors decreased significantly, as shown in figure 10. The inefficiency is particularly prevalent at large sensor radii and for high bias voltages. The decrease in CFE does not appear to be proportional to the delivered luminosity, but instead exhibits a rapid drop between the 0.04 and 0.43 fb<sup>-1</sup> data scans.

To determine the source of this CFE decrease, a large sample of regular LHCb physics data has been used to measure the CFE for small spatial regions on a sensor at the nominal 150V bias. The result of this is shown in figure 11, displayed beside a diagram illustrating the layout of the second metal layer readout lines. There is a clear correspondence between the two figures, with high CFE measured in regions that are devoid of second metal layer lines. The relative orientation of the strips and routing lines in R-type sensors is shown in figure 12. In addition, a schematic cross-section of an R-type sensor is shown in figure 13. The routing lines from inner strips are seen to pass approximately perpendicularly over the outer strip implants.



**Figure 10**. The CFE for an R-type  $n^+$ -on-*n* sensor as a function of sensor radius for **a**) different amounts of delivered luminosity and **b**) several different bias voltages.



**Figure 11**. **a)** The layout of the second metal layer routing lines on an R-type sensor. The darker regions represent the presence of routing lines, and the lighter regions their absence. **b)** The CFE shown in small spatial regions of an R-type sensor.



**Figure 12**. A photograph of the innermost region of an R-type sensor. Strips run from the bottom-left to the top-right. Each strip is connected to a routing line orientated perpendicularly to the strip.



Figure 13. A schematic cross-section of a portion of an R-type sensor, showing the relative position of the two metal layers used to carry the readout signals in  $n^+$ -on-n type sensors. The  $n^+$  implants and strips (into the page) run perpendicularly to the routing lines (left to right). For clarity the routing line of just one strip is shown.



**Figure 14**. The CFE as a function of the distance between the particle intercept and the nearest routing line, for several bins of the distance between the particle intercept and closest strip edge.

Using the precision tracking of the VELO, it is possible to investigate the CFE loss as a function of the distance between a track intercept with a sensor, and the nearest strip and routing line. This is shown in figure 14. The CFE is improved for track intercepts that are near to the strip implants. Conversely, the CFE is reduced when a track intercept is far from a strip and near to a routing line. Similar effects have been observed in other experiments [23, 24].

The source of the CFE loss is hypothesised in terms of charge induction on the second metal layer. Prior to irradiation, ionised electrons will drift along the field lines, most of which terminate at the  $n^+$  implants. Hence the majority of the signal will be induced on the implants, which are strongly capacitively coupled to the readout strips. The drifting charge is expected to be collected well within the ~20 ns readout period of the electronics, and no signal is expected on neighbouring electrodes (with the exception of capacitive coupling and cross-talk effects, which are measured to be low). However, irradiation may cause modifications to the field line structure, such that not all field lines terminate on the implants. In addition, there may be charge trapping effects which delay the drift of charge, resulting in charge sampling before the electrons have reached the implants. In both of these situations there will be a net induced charge on nearby electrodes, such as the second metal layer routing lines. In figure 10(b) the CFE was seen to worsen with increasing bias voltage. This appears to disfavour the contribution due to trapping, as an increase in bias voltage should result in faster collection times. However, the bias voltage may also affect the field-line



**Figure 15.** For R-type sensors: **a)** The ADC spectrum of all clusters seen for three different integrated luminosities. The limit at 10 ADC counts is imposed by the clustering thresholds. **b)** The fraction of reconstructed clusters that are induced on routing lines as a function of the distance to the nearest routing line and strip. This is determined by examining the track intercept point and finding the nearest routing line. The deposited charge is attributed in the reconstructed on the inner strip associated with this routing line. One strip clusters with less than 35 ADC counts reconstructed on these inner strips are then identified.

structure. In reality, it is likely that the charge loss to the second metal layer is due to several competing mechanisms.

The CFE loss also exhibits a significant radial dependence, as was shown by figure 10. This can be understood by considering two competing mechanisms. The implant strip width and the fractional area covered by the strips increases with radius, resulting in reduced charge loss, due to greater strip shielding. However, the fractional area covered by the second metal layer also increases with radius, due to the greater density of lines, increasing the amount of pickup. The latter effect is dominant, hence the overall charge loss is greater at large sensor radii.

In addition to lowering the clustering efficiency, charge induced on a routing line can introduce a noise cluster. The cluster ADC distribution from R-type sensors has a peak associated to these low ADC noise clusters that has grown with fluence, as shown in figure 15(a). These noise clusters are predominantly single strip clusters located at small radius regions of R-type sensors. The fraction of the induced noise clusters increases when tracks traverse a sensor near to a routing line and far from a strip, as shown in figure 15(b).

The CFE decrease is not observed in  $\phi$ -type sensors as the routing lines from inner strips were intentionally placed directly above the outer strips to minimise pick-up. This is made possible by the  $\phi$ -type sensors strip orientation. The CFE loss could be partially recovered by lowering the cluster reconstruction thresholds. However this comes at the expense of a worse signal to back-ground ratio which leads to higher rates of fake tracks reconstructed from noise induced clusters.

The R-type  $n^+$ -on-p and  $n^+$ -on-n sensors have a similar CFE dependence on the strip and routing line distance, as shown in figure 16(a). Figure 16(b) shows the MPV of the collected charge distribution as a function of bias voltage for an  $n^+$ -on-n and an  $n^+$ -on-p type sensor. At 150 V, the MPV of the  $n^+$ -on-n and  $n^+$ -on-p are approximately equal, both before and after irradiation. For



**Figure 16.** a) The CFE as a function of the distance between the particle intercept and the nearest routing line and strip edge, compared for an  $n^+$ -on-n and  $n^+$ -on-p sensor. b) The MPV vs. bias voltage for an  $n^+$ -on-n and  $n^+$ -on-p sensor.



**Figure 17**. The MPV against bias voltage for an R-type  $n^+$ -on-*n* sensor at three values of delivered luminosity. The sensor region has been identified as having type inverted in the  $1.22 \,\text{fb}^{-1}$  scan, in which the MPV dependence on voltage is no longer present.

the  $n^+$ -on-*n* type sensor post irradiation, the MPV reaches a maximum at around 60V after which it is observed to decrease with increasing bias voltage. This decrease in MPV leads to a reduced CFE and is associated with the second metal layer effect. Therefore less charge is lost to the second metal layer when operating the  $n^+$ -on-*n* sensor at a voltage lower than the nominal 150V bias.

The  $n^+$ -on-p type sensor does not exhibit this same charge collection loss (and resulting CFE decrease) dependence on voltage. This may be due to the depletion region in the  $n^+$ -on-p type sensor growing from the strip side of the silicon instead of from the sensor backplane. This is supported by the observation that after type inversion, charge loss in  $n^+$ -on-n type sensors no longer depends on the bias voltage, as shown in figure 17.

#### 5 Summary

The effects of radiation damage have been observed in all of the LHCb VELO sensors. At the operational sensor temperature of approximately  $-7^{\circ}$ C, the average rate of sensor current increase is measured to be  $18 \,\mu\text{A}$  per fb<sup>-1</sup>, in agreement with expectations. The silicon effective bandgap has been determined using current versus temperature scan data collected at various levels of radiation, with an average value of  $E_g = 1.16 \pm 0.03 \pm 0.04 \,\text{eV}$  found.

Analysis of the Charge Collection Efficiency has proven an effective method for tracking the evolution of the sensor depletion voltages with fluence. Measurements of the Effective Depletion Voltage after sensor type inversion have been shown to agree well with the Hamburg model predictions. A method relating the sensor noise dependence on bias voltage was used to identify type-inverted sensors, and was found to be in good agreement with the Charge Collection Efficiency method.

A significant decrease in the Cluster Finding Efficiency in R-type sensors due to the second metal layer has been observed following a relatively small amount of particle fluence. In the worst affected sensor regions the Cluster Finding Efficiency decreased by over 5%. Despite this relatively large localised inefficiency, studies of the VELO tracking efficiencies show no degradation associated to this effect, within the errors of  $\pm 0.3\%$ . For the  $n^+$ -on-n type sensors before type inversion the magnitude of the charge loss is found to increase with sensor bias voltage. For type-inverted  $n^+$ -on-n type sensors and  $n^+$ -on-p type sensors, a voltage dependence is not observed. Radiation induced modifications to the field line structure and charge trapping effects are thought to be possible sources of this charge loss effect.

The two  $n^+$ -on-*p* sensors have been studied in detail, providing valuable information for upgraded detector designs. If the Effective Depletion Voltage were to continue increasing at the currently observed rate with further irradiation, then the  $n^+$ -on-*p* would reach the 500 V hardware limit having received approximately  $35 \times 10^{12} 1 \text{ MeV} n_{eq}$  less fluence than an equivalent  $n^+$ -on-*n* type sensor. This corresponds to approximately  $1 \text{ fb}^{-1}$  of integrated luminosity in the highest particle fluence region of the VELO.

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