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# Geometrical analysis of thread milling – Part 1: Evaluation of tool angles

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Abstract: Thread milling is a method which is increasingly used for machining thread. For this operation, a helical interpolation is required. Furthermore, the thread mill is a tool whose geometry is rather complex. Its envelope profile is linked to the thread profile and a single tooth of the thread mill is composed of three continuous cutting edges. The present study proposes a geometrical model and an analytical formulation to define the rake face and the cutting edge. Further, the calculations of cutting planes and cutting angles are explained. The analysis shows specific aspects of thread mills, in particular the fact that the flute angle may lead to a negative rake angle. This study is a contribution to cutting geometry aspect and constitutes a step for cutting force model in thread milling.

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## NOMENCLATURE

Subscripts and abbreviations:

m relative to the mill

r,  $\theta$ , z cylindrical coordinates

fce: front cutting edge

uce: upper cutting edge

lce: lower cutting edge

Referentials and parameters:

$R_0 = (o, \mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3)$  referential linked to the mill

$z_{ce}$ : altitude of a cutting edge point in the  $R_0$  referential

u: parameter

Metric thread dimensions:

D: nominal diameter of the internal thread

$D_1$ : minor diameter of the internal thread

$D_2$ : pitch diameter of the internal thread

H: fundamental triangle height

P: thread pitch (mm)

$\rho$ : angular thread pitch (mm/rad)

Mill dimensions:

$D_m$ : maximum diameter (mm)

$D_{2m}$ : pitch diameter (mm)

$k_m$ : reduction coefficient of the mill profile height

$\rho_{im}$ : pitch per radian of the helicoidal flute

Mill cutting angle:

$\gamma_{om}$ : orthogonal rake angle

$\lambda_{sm}$ : flute angle (or helix angle) on the  $D_m$  diameter

$\gamma_i$ : rake angle in  $P_i$  plane ( $i \in \{n, f, o, s\}$ )

$\lambda_s$ : cutting edge inclination angle

$\kappa_r$ : cutting edge angle

$P_r$ : tool reference plane

$P_s$ : tool cutting edge plane

$P_n$ : tool cutting edge normal plane

$P_f$ : tool working plane

$P_o$ : tool orthogonal plane

$\mathbf{TV}_{ce}(z_{ce})$ : tangential vector with respect to  $CE_1$

$\mathbf{TV}_{ce,Pr}(z_{ce})$ : tangential vector with respect to  $CE_1$  projected onto plane  $P_r$

$\mathbf{NV}_{RF}(z_{ce})$ : normal vector with respect to the rake face on the cutting edge point

1 **NV**<sub>P<sub>i</sub>(z<sub>ce</sub>)</sub>: normal vector with respect to the P<sub>i</sub> plane (i ∈ {n, f, o, s} )

2 **V**<sub>P<sub>r</sub>∩P<sub>i</sub></sub>: vector of the intersection of plane P<sub>r</sub> and plane P<sub>i</sub>

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4 **V**<sub>RF∩P<sub>i</sub></sub>: vector of the intersection of the rake face and plane P<sub>i</sub>

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6 **NV**<sub>P<sub>r</sub>.P<sub>i</sub></sub>: normal vector with respect to plane P<sub>r</sub> projected onto plane P<sub>i</sub>

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8 **NV**<sub>RF.P<sub>i</sub></sub>: normal vector with respect to the rake face projected onto plane P<sub>i</sub>

9  
10 **RV**: radius vector

11 Cutting parameters:

12 r<sub>doc</sub>: radial depth of cut (mm)

13 r<sub>p</sub>: radial penetration (mm)

14 Geometrical objects:

15 **P**<sub>m i</sub>: i<sup>th</sup> characteristic point of the mill profile

16 **MP**(z<sub>ce</sub>): mill profile

17 **RF**(r, z<sub>ce</sub>): mill rake face (flute surface)

18 **CE**(z<sub>ce</sub>): mill cutting edge

19 Operators:

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$$\mathbf{R}(\theta): \text{rotating operator } \mathbf{R}(\theta) = \begin{bmatrix} \cos(\theta) & \sin(\theta) & 0 \\ -\sin(\theta) & \cos(\theta) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

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$$\mathbf{N}(\mathbf{V}): \text{normative operator } \mathbf{N}(\mathbf{V}) = \frac{1}{|\mathbf{V}|} \mathbf{V}$$

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# 1 Introduction

## 1.1 Generalities on thread milling

Threads can be produced by many methods among them, there is the thread milling technique. The description on thread milling cycle is given in [1,2]. This technique allows to machine both internal and external thread, and one mill may produce threads with different diameters and having same pitch. Torque is lower and cutting speed may be greater in thread milling than in tapping, and if tool breakage occurs, as the thread mill is having a lower diameter than internal thread, it can be removed easily. As a consequence, thread milling is well adapted to obtain internal thread, large thread dimensions, especially in high cost parts machining which may be done in difficult to cut materials. Further, application of thread milling is increasing in industry [3,4].

## 1.2 Tool and cutting geometry aspects

A thread mill is a rotating cutting tool with grooves, its profile is composed of the threaded one, and its envelope is a revolution surface. During the thread milling cycle, the tool center strategy describes a circular helix. This results in complex geometrical problems.

The first is how to design such cutting tool and which cutting geometry is adapted for machining. Concerning the groove is usually defined as being a helical.

The second is how to grind the thread mill from the CAD design. The definition of the grinding wheel profile used for the groove machining is a specific problematic due to inference problem [5-9]. This aspect of groove obtaining is also common to cylindrical mill manufacturing. Furthermore, the thread mill profile is fixed by the threaded and the grinding of clearance surfaces is a difficult operation which is linked both from the groove positions and from the mill profile. This point is not dealt in earlier study.

Then, from this process it appears a third problem, which is the cutting ability of the mill in relationship with tool angles which are not constant along cutting edges.

For different kinds of tools, like fluted drills, taps, round insert cutters and also thread mills, there are evolutions of tool angles, in hand and/or in used, along the cutting edges. The tool angles can not be directly determined from tool design and the cutting edge definitions. There exist different approaches [10,11] for establishing these tools angles. From this analysis, it is possible to improve the tool design and adapt cutting edge definition in order to minimize rake angle evolution or avoid large negative rake angle. This approach is needed as the rake angle affects cutting forces, tool chip friction, dead metal zone [12-14] and then cutting stability and tool wear [15].

## 1.3 Approach for the study

The complex problem of force modeling in thread milling has been started to be explored [1] and cutting angles are an interesting field for this

development. Better model needs to take into account the real cutting geometry at every point on cutting edge, because it significantly influences cutting forces and specific cutting energy [12-14].

The tool angle evolution on thread mill has not been dealt and a vectorial approach is proposed to investigate this case. The present study deals with the analysis of the cutting geometry of a thread mill having a straight or helical flute. The approach is explained in Fig. 1. The goal of this paper is to parameterize analytically a rake face (**RF**) and its associated cutting edge (**CE**) to calculate the tool angles.

This article is related to [2] and the general context is identical. A metric thread mill is considered, and the notation and  $R_o$  mill referential used are the same as in [2]. All calculations are computed using Mathematica software. The parameterization of the thread mill operation is proposed in Fig. 2. For the different cases studied, the common mill dimension values are:  $D_m = 12$  mm,  $P = 2$  mm,  $k_m = 1/8$ .

## 2 Mill parameterization

This section describes the parameterization of the mill profile (**MP**), the rake face (**RF**) surface and the cutting edge (**CE**).

### 2.1 Mill profile

The mill profile (**MP**) is resulting from the thread profile [16]. The used mill profile (**MP**) is shown in Fig. 3, and it is defined by equation (1) [2] as a function of  $z_{ce}$  axial coordinate. The maximum diameter of the mill is defined by  $D_m$  and its pitch by  $P$ . The crest of the mill is defined by a reduction coefficient for the mill profile height called  $k_m$ . As explained in [2], the mill profile is not completely engaged with the thread. The lower cutting edge (lce) works between the  $P_{m\ inf.\ lim.}$  and  $P_{m3}$  mill profile points. Symmetrically, the upper cutting edge (uce) works between the  $P_{m4}$  and  $P_{m\ sup.\ lim.}$  mill profile points.

$$\mathbf{MP}(z_{ce}) = [\mathbf{MP}_r(z_{ce}), z_{ce}]^T \quad (1)$$

### 2.2 Rake face parameterization

It is decided to model the mill flute as being a helicoid. The pitch per radian ( $p_{fm}$ ) of this helicoid is defined by the flute angle ( $\lambda_{sm}$ ) on the maximum diameter ( $D_m$ ). The expression of this pitch is given by (2).

$$p_{fm} = \frac{1}{2} D_m \cdot \tan(\pi/2 - \lambda_{sm}) \quad (2)$$

In addition to the flute angle ( $\lambda_{sm}$ ) on the circular helix enveloping the thread mill, the orthogonal rake angle ( $\gamma_{om}$ ) on the maximum diameter ( $D_m$ ) is defined. From these tool angles, we obtain the  $V_{RF1}$  vector (3), included in the rake face (**RF**), and the  $V_{RF2}$  vector (4), which is tangent to this circular helix.

$$\mathbf{V}_{RF1} = [\cos(\pi - \gamma_{om}), \sin(\pi - \gamma_{om}), 0]^T \quad (3)$$

$$\mathbf{V}_{RF2} = [0, \sin(\lambda_{sm}), \cos(\lambda_{sm})]^T \quad (4)$$

From the centre point of the mill profile ( $P_{m0}$ ), the expression for the generative line of the rake face ( $\mathbf{GL}_{\mathbf{RF}}$ ) is (5). The  $u$  parameter is the distance from point  $P_{m0}$ , and  $\theta$  is an angular parameter. The rake face ( $\mathbf{RF}$ ), which is considered as being a helicoid, can be parameterized by equation (6) according to [8,9].

$$\mathbf{GL}_{\mathbf{RF}}(u) = [D_m / 2, 0, P / 2]^T + u \cdot \mathbf{V}_{\mathbf{RF}1} \quad (5)$$

$$\mathbf{RF}(u, \theta) = [0, 0, p_{\text{fm}} \cdot \theta]^T + \mathbf{R}(\theta) \cdot \mathbf{GL}_{\mathbf{RF}}(u) \quad (6)$$

In order to use cylindrical parameters, relation (7) is calculated, connecting the radial coordinate and the  $u$  parameter. The axial coordinate  $z_{\text{ce}}$  is linked with the angular parameter  $\theta$  (8). By using these parameter changes, a new analytical parameterization (9) of the rake face ( $\mathbf{RF}$ ) is established.

$$r^2 = (\mathbf{RF}(u, \theta) \cdot \mathbf{e}_1)^2 + (\mathbf{RF}(u, \theta) \cdot \mathbf{e}_2)^2$$

$$\Leftrightarrow u(r) = \frac{1}{2} D_m \cdot \cos(\gamma_{\text{om}}) - \sqrt{r^2 - D_m^2 / 8 + D_m^2 \cos(2 \cdot \gamma_{\text{om}}) / 8} \quad (7)$$

$$p_{\text{fm}} \cdot \theta = z_{\text{ce}} - P / 2 \quad (8)$$

$$\mathbf{RF}(z_{\text{ce}}, r) = [0, 0, z_{\text{ce}} - P / 2]^T + \mathbf{R}((z_{\text{ce}} - P / 2) / p_{\text{fm}}) \cdot \mathbf{GL}_{\mathbf{RF}}(u(r)) \quad (9)$$

Fig. 4 shows the mill profile ( $\mathbf{MP}$ ), the rake face ( $\mathbf{RF}$ ) and the geometrical construction of the cutting edge ( $\mathbf{CE}$ ).

### 2.3 Cutting edge parameterization

The cutting edge ( $\mathbf{CE}$ ) is the curve on the rake face ( $\mathbf{RF}$ ) surface which generates the same envelope as the mill profile ( $\mathbf{MP}$ ) when it rotates around the  $(0, \mathbf{e}_3)$  axis. Thus, the cutting edge ( $\mathbf{CE}$ ) can be expressed analytically by equation (10). The radial component of the mill profile ( $\mathbf{MP}_r$ ) is obtained by using the rake face ( $\mathbf{RF}$ ) equation (9) in cylindrical coordinates. The cutting edge ( $\mathbf{CE}$ ), with characteristic points, is drawn in Fig. 5.

$$\mathbf{CE}(z_{\text{ce}}) = \mathbf{RF}(z_{\text{ce}}, \mathbf{MP}_r(z_{\text{ce}})) \quad (10)$$

## 3 Cutting angle calculation

Definitions of tool planes and tool angles given by [17,18] are used. From the cutting edge parameterization, tool planes and tool angles may be calculated at every point of the cutting edge ( $\mathbf{CE}$ ). All geometrical characteristics concern the tool-in-hand system. The various planes are defined only by unit vectors.

### 3.1 Cutting plane calculation

The reference plane ( $P_r$ ) is defined as being normal to the cutting speed. Thus, the normal vector to the reference plane ( $\mathbf{NV}_{P_r}$ ) may be expressed by equation (11).

$$\mathbf{NV}_{Pr}(z_{ce}) = \mathbf{N}(\mathbf{CE}(z_{ce}) \times [0, 0, 1]^T) \quad (11)$$

The tangential vector of the cutting edge ( $\mathbf{TV}_{CE}$ ) is calculated using equation (12). Equation (13) gives the projection of this vector ( $\mathbf{TV}_{CE.Pr}$ ) on the reference plane ( $P_r$ ).

$$\mathbf{TV}_{CE}(z_{ce}) = \mathbf{N}\left(\frac{\partial \mathbf{CE}(z_{ce})}{\partial z_{ce}}\right) \quad (12)$$

$$\mathbf{TV}_{CE.Pr}(z_{ce}) = \mathbf{N}\left(\mathbf{TV}_{CE}(z_{ce}) - (\mathbf{TV}_{CE}(z_{ce}) \cdot \mathbf{NV}_{Pr}(z_{ce})) \cdot \mathbf{NV}_{Pr}(z_{ce})\right) \quad (13)$$

The normal vector to the cutting edge normal plane ( $\mathbf{NV}_{Pn}$ ) is tangential to the cutting edge ( $\mathbf{CE}$ ), and thus it is given by equation (14). The normal vector to the orthogonal plane ( $\mathbf{NV}_{Po}$ ) is equal to the cutting edge tangential vector projected onto the reference plane ( $\mathbf{TV}_{CE.Pr}$ ). It is defined by equation (15).

$$\mathbf{NV}_{Pn}(z_{ce}) = \mathbf{TV}_{CE}(z_{ce}) \quad (14)$$

$$\mathbf{NV}_{Po}(z_{ce}) = \mathbf{TV}_{CE.Pr}(z_{ce}) \quad (15)$$

In Fig. 5 it can be seen that, at the cutting edge point altitude  $3P/4$ , the rake face is in front of the reference plane ( $P_r$ ) along the normal plane ( $P_n$ ), whereas this is not the case at the cutting edge point altitude  $P/4$ . That would mean the rake angle measured in this direction is negative on the upper cutting edge (uce).

The z axial component of the feed motion direction is not taken into account because it is the tool-in-hand angles, and not the working angles, which are considered. Consequently, the normal vector to the working plane ( $\mathbf{NV}_{Pf}$ ) may be calculated using equation (16)

$$\mathbf{NV}_{Pf}(z_{ce}) = [0, 0, 1]^T \quad (16)$$

Concerning the cutting edge plane ( $P_s$ ), it is normal to the reference plane ( $P_r$ ) and to the orthogonal plane ( $P_o$ ). Thus, its normal vector ( $\mathbf{NV}_{Ps}$ ) can be calculated by equation (17)

$$\mathbf{NV}_{Ps}(z_{ce}) = \mathbf{NV}_{Pr}(z_{ce}) \times \mathbf{NV}_{Po}(z_{ce}) \quad (17)$$

A graphic representation of the cutting planes, on a point of the cutting edge, is given in Fig. 6.

Equation (18) gives the normal vector to the rake face ( $\mathbf{NV}_{RF}$ ) at a cutting edge ( $\mathbf{CE}$ ) point defined by  $z_{ce}$  altitude.

$$\mathbf{NV}_{RF}(z_{ce}) = \mathbf{N}\left(\frac{\partial \mathbf{RF}}{\partial z_{ce}}(z_{ce}, \mathbf{MP}_r(z_{ce})) \times \frac{\partial \mathbf{RF}}{\partial r}(z_{ce}, \mathbf{MP}_r(z_{ce}))\right) \quad (18)$$

In order to calculate the cutting angle in the ( $P_i$ ) plane ( $i \in \{n, f, o, s\}$ ), it is necessary to know the traces of different geometrical elements in this plane, as shown in Fig. 7.

Vector ( $\mathbf{V}_{Pr \cap Pi}$ ) of the line of intersection between reference plane ( $P_r$ ) and plane  $P_i$  can be calculated from equation (19). The normal vector ( $\mathbf{NV}_{Pr.Pi}$ ) to reference plane ( $P_r$ ) projected on plane  $P_i$  is given by equation (20).



$$\mathbf{V}_{Pr \cap Pi}(z_{ce}) = \mathbf{N}(\mathbf{NV}_{Pr}(z_{ce}) \times \mathbf{NV}_{Pi}(z_{ce})) \quad i \in \{n, f, o, s\} \quad (19)$$

$$\mathbf{NV}_{Pr.Pi}(z_{ce}) = \mathbf{N}(\mathbf{NV}_{Pr}(z_{ce}) - (\mathbf{NV}_{Pr}(z_{ce}) \cdot \mathbf{NV}_{Pi}(z_{ce})) \cdot \mathbf{NV}_{Pi}(z_{ce})) \quad i \in \{n, f, o\} \quad (20)$$

Vector ( $\mathbf{V}_{RF \cap Pi}$ ) of the line of intersection between the rake face (**RF**) and plane  $P_i$  can be calculated from equation (21). The normal vector ( $\mathbf{NV}_{RF.Pi}$ ) to the rake face (**RF**) projected onto plane  $P_i$  is given by equation (22).

$$\mathbf{V}_{RF \cap Pi}(z_{ce}) = \mathbf{N}(\mathbf{NV}_{RF}(z_{ce}) \times \mathbf{NV}_{Pi}(z_{ce})) \quad i \in \{n, f, o\} \quad (21)$$

$$\mathbf{NV}_{RF.Pi}(z_{ce}) = \mathbf{N}(\mathbf{NV}_{RF}(z_{ce}) - (\mathbf{NV}_{RF}(z_{ce}) \cdot \mathbf{NV}_{Pi}(z_{ce})) \cdot \mathbf{NV}_{Pi}(z_{ce})) \quad i \in \{n, f, o\} \quad (22)$$

The radius vector (**RV**), defined by equation (23), is included in the reference plane ( $P_r$ ).

$$\mathbf{RV}(z_{ce}) = \mathbf{N}([\mathbf{CE}(z_{ce}) \cdot \mathbf{e}_1, \mathbf{CE}(z_{ce}) \cdot \mathbf{e}_2, 0]^T) \quad (23)$$

### 3.2 Cutting angle calculation

From the geometrical elements which are previously defined, as shown in Fig. 7, the rake angle, measured in plane ( $P_i$ ), can be expressed by both equations (24) and (25). It may be computed from the cross product and the dot product of the vectors. At point  $P_{m0}$  of the cutting edge, the rake angle ( $\gamma_n(P/2)$ ) in the normal plane is analytically given by equation (26).

$$\gamma_i(z_{ce}) = \angle(\mathbf{V}_{RF \cap Pi}(z_{ce}), \mathbf{V}_{Pr \cap Pi}(z_{ce})) \quad (24)$$

$$\gamma_i(z_{ce}) = \angle(\mathbf{NV}_{RF.Pi}(z_{ce}), \mathbf{NV}_{Pr.Pi}(z_{ce})) \quad (25)$$

$$\gamma_n(P/2) = \pi/2 - \arccos\left(\frac{1}{\sqrt{1 + \cot(\gamma_{om})^2 \cdot \sec(\lambda_{sm})^2}}\right) \quad (26)$$

Angle  $\lambda_s$  is the inclination of the cutting edge from the reference plane ( $P_r$ ), as shown in Fig. 7, and may be calculated using equations (27) or (28).

$$\lambda_s(z_{ce}) = \angle(\mathbf{TV}_{CE}(z_{ce}), \mathbf{TV}_{CE.Pr}(z_{ce})) \quad (27)$$

$$\lambda_s(z_{ce}) = \angle(\mathbf{NV}_{Pr}(z_{ce}), \mathbf{NV}_{Pr.Pn}(z_{ce})) \quad (28)$$

The cutting edge angle ( $\kappa_r$ ) is the angle between the cutting edge (**CE**) and the radius vector (**RV**) measured in the reference plane ( $P_r$ ), as shown in Fig. 7. It is expressed by equation (29).

$$\kappa_r(z_{ce}) = \angle(\mathbf{TV}_{CE.Pr}(z_{ce}), \mathbf{RV}(z_{ce})) \quad (29)$$

## 4 CUTTING ANGLE ANALYSIS

This section details an example of cutting geometry analysis by using the developed approach on a given mill. Then, the approach is applied to

1 different mill geometries to observe the effects of flute angle ( $\lambda_{sm}$ ) and of  
2 orthogonal rake angle ( $\gamma_{om}$ ) on normal rake angle ( $\gamma_n$ ).  
3

#### 4 4.1 Analysis of a thread mill angle

5 A thread mill is analysed (case A) with:  $D_m = 12$  mm,  $P = 2$  mm,  $k_m = 1/8$ ,  
6  $\gamma_{om} = 10^\circ$ ,  $\lambda_{sm} = 30^\circ$ . Fig. 8 shows the evolution of the cutting angles  
7 along the cutting edge (**CE**). All cutting angles are constant on the front  
8 cutting edge, because it is a circular helix. The cutting edge angle ( $\kappa_r$ ) is  
9 constant on the three parts of the cutting edge: the lower cutting edge  
10  $\kappa_r = 30^\circ$ , the front cutting edge  $\kappa_r = 90^\circ$ , and the upper cutting edge  
11  $\kappa_r = 150^\circ$ . This is the consequence of the mill profile (**MP**) defined for  
12 machining metric thread, which is dealt with in this study.  
13

14 It appears on the front edge that the inclination angle and the orthogonal  
15 cutting angle values are those which were defined ( $\lambda_s = \lambda_{sm} = 30^\circ$ ,  
16  $\gamma_o = \gamma_{om} = 10^\circ$ ). In addition, the normal rake angle ( $\gamma_n$ ) on the front cutting  
17 edge is  $8.68^\circ$ . The inclination angle ( $\lambda_s$ ) is not constant on the flank cutting  
18 edges but remains nevertheless positive.  
19

20 Along the front edge, which is a circular helix, the orthogonal plane ( $P_o$ )  
21 and the working plane ( $P_f$ ) are the same. As a consequence, the rake  
22 angles measured in these planes are also identical ( $\gamma_o = \gamma_f$ ). On the flank  
23 cutting edges, the working rake angle ( $\gamma_f$ ) varies very little. However, this  
24 angle is not really significant for the cutting geometry. The normal rake  
25 angle ( $\gamma_n$ ) and the orthogonal rake angle ( $\gamma_o$ ) become negative on the  
26 upper cutting edge (uce). This is due to the flute angle ( $\lambda_{sm}$ ) combined with  
27 the cutting edge angle ( $\kappa_r$ ). Thus, it necessarily has an effect on cutting  
28 force intensity on this cutting edge.  
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#### 30 4.2 Analysis of different thread mills

31 The combination of the flute angle ( $\lambda_{sm}$ ) and the mill orthogonal rake angle  
32 ( $\gamma_{om}$ ), influences the normal rake angle ( $\gamma_n$ ) along the cutting edge (**CE**).  
33 The first analysis is focused on the evolution of this angle ( $\gamma_n$ ) for mills  
34 having the same flute angle ( $\lambda_{sm} = 15^\circ$ ) and a different orthogonal rake  
35 angle ( $\gamma_{om}$ ), as shown in Fig. 9. For the mill having a null rake angle  
36 ( $\gamma_{om} = 0$ ) due to the flute angle ( $\lambda_{sm}$ ), the normal rake angle ( $\gamma_n$ ) is positive  
37 on the lower cutting edge (lce), null on the front cutting edge (fce), and  
38 negative on the upper cutting edge (uce). If the thread mill is designed with  
39 a higher orthogonal rake angle ( $\gamma_{om}$ ), the normal rake angle ( $\gamma_n$ ) is shifted  
40 to a positive value.  
41

42 The second analysis, whose results are presented in Fig. 10, deals with  
43 the variation in the normal rake angle ( $\gamma_n$ ) for mills having the same  
44 orthogonal rake angle ( $\gamma_{om} = 10^\circ$ ) and a different flute angle ( $\lambda_{sm}$ ). For the  
45 straight flute mill ( $\lambda_{sm} = 0^\circ$ ), the normal rake angle ( $\gamma_n$ ) is positive and  
46 identical on the lower cutting edge (lce) and on the upper one (uce). The  
47 cutting edge (**CE**) has a symmetrical plane. If the thread mill is designed  
48 with a higher flute angle ( $\lambda_{sm}$ ), the normal rake angle ( $\gamma_n$ ) increases on the  
49 lower cutting edge (lce) and decreases, and may become negative, on the  
50 upper one (uce).  
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### 4.3 Discussion

The use of a cylindrical mill with a positive flute angle is interesting, because it enables its normal rake angle ( $\gamma_n$ ) to be increased and the cutting forces to be shared during one mill revolution. It induces lower cutting forces, lower cutting force variations and thus fewer vibrations. Additionally, increasing the radial depth of cut allows a higher number of teeth to be engaged and reduces cutting force variations.

In thread milling, such freedom of settings is not possible. The radial depth of cut ( $r_{doc}$ ) can not be changed because the radial penetration ( $r_p$ ) is determined by the thread pitch, as shown in Fig. 2. As a consequence, a method for reducing cutting force variations would be to use a thread mill with a high flute angle. Nevertheless, the present study shows that a thread mill designed with a flute angle introduces a negative rake angle on the upper cutting edge (uce), which leads to higher cutting forces. Therefore a compromise is necessary in the determination of the flute angle.

### 5 CONCLUSION

This article proposed a full analytical parameterization of the thread mill cutting edge based on the mill profile defined in [2] and also on a flute geometry hypothesis. Based on this, the cutting planes are parameterized to enable the calculation of the cutting angles.

As soon as there is a flute angle on a thread mill, there appears a negative normal rake angle along it, because of the cutting edge angle on the upper cutting edge. This leads to conclusion that a compromise in the flute angle value is required to reduce cutting force variations without having excessive negative cutting. This aspect leads to the optimisation of the thread mill geometry.

Because of different rake angles on the upper and lower cutting edges, force modelling should consider specific cutting energy, taking into account the effect of the rake angle. Even if the mill design defines that the clearance angle is also the same along the cutting edge, the working clearance angle will be different on the upper and lower cutting edges, because of the axial speed of the mill during the helical interpolation. The working clearance angle is lower on the flank edge opposite the axial speed direction. A precise force model should also integrate these aspects.

Finally, the proposed formulation for tool angle calculation is also available for any cutting edge. Then it would be used for other mill profiles or any cutting tool.

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FIGURES

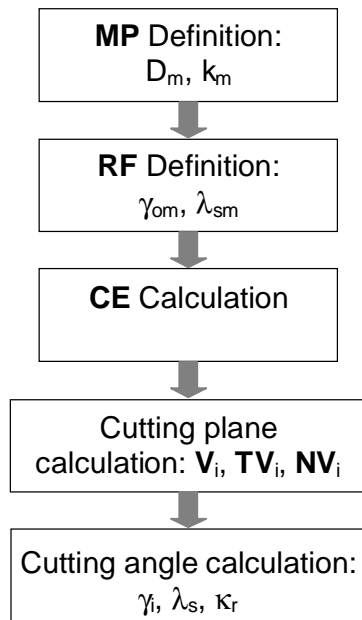


Fig. 1 Approach for the cutting angle calculation

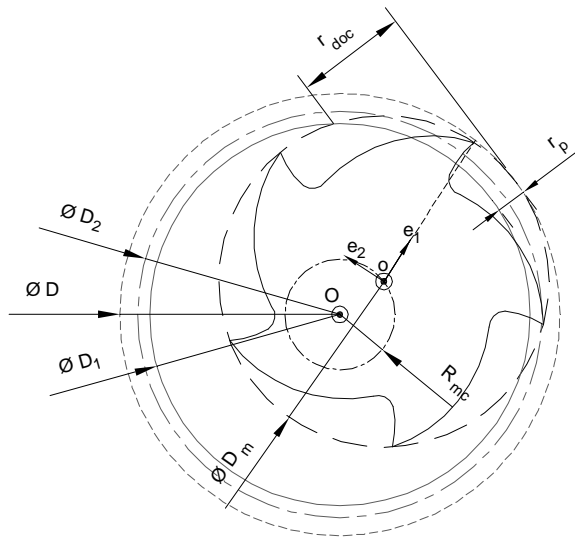


Fig. 2 Parameterization of the thread milling operation

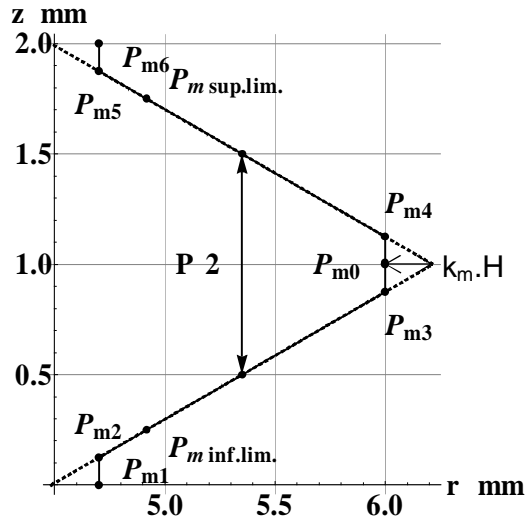


Fig. 3 Mill profile (MP) - case A:  $P = 2$  mm,  $D_m = 12$  mm,  $k_m = 1/8$

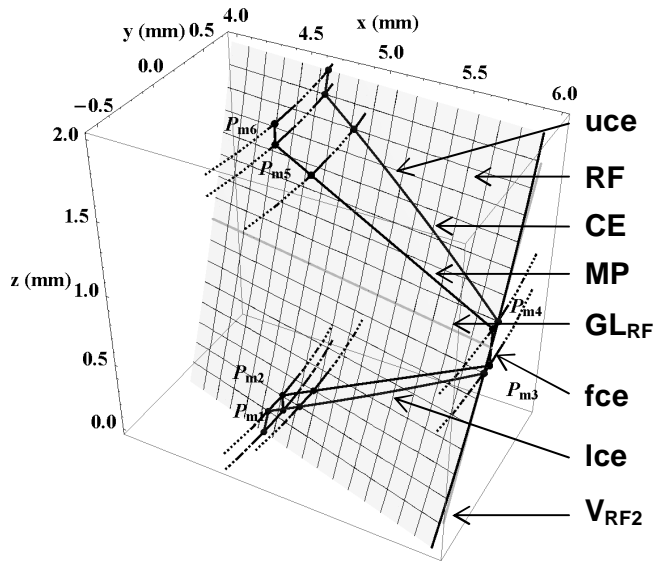


Fig. 4 Geometrical construction of the cutting edge (CE) - case A:  $\alpha_{om} = 10^\circ$ ;  $\lambda_{sm} = 30^\circ$

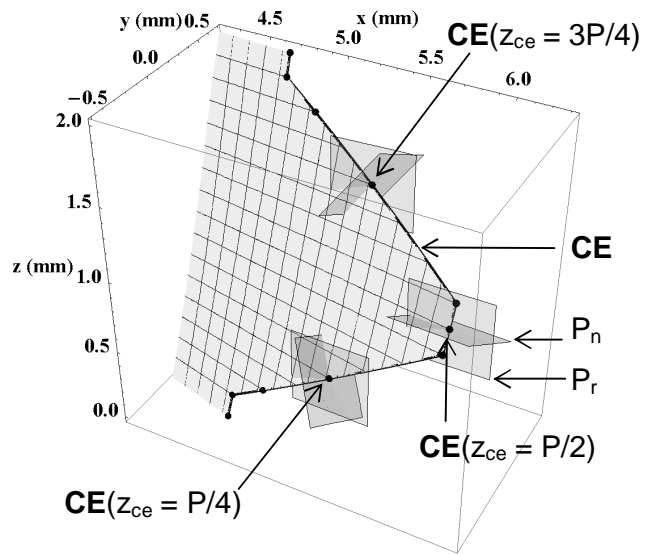


Fig. 5 Cutting edge (CE) with reference planes ( $P_r$ ) and normal planes ( $P_n$ ) - case A:  $\alpha_{om} = 10^\circ$ ;  $\lambda_{sm} = 30^\circ$

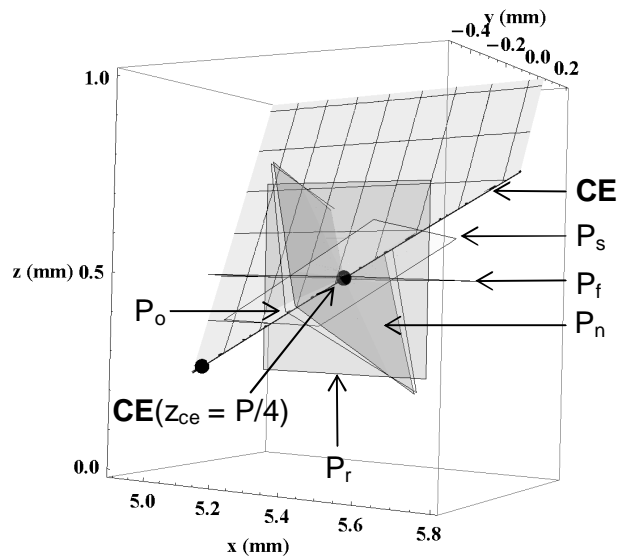


Fig. 6 Cutting edge (CE) with cutting planes ( $P_r$ ) at point  $z_{ce} = P/4$  - case A:  $\alpha_{om} = 10^\circ$ ;  $\lambda_{sm} = 30^\circ$

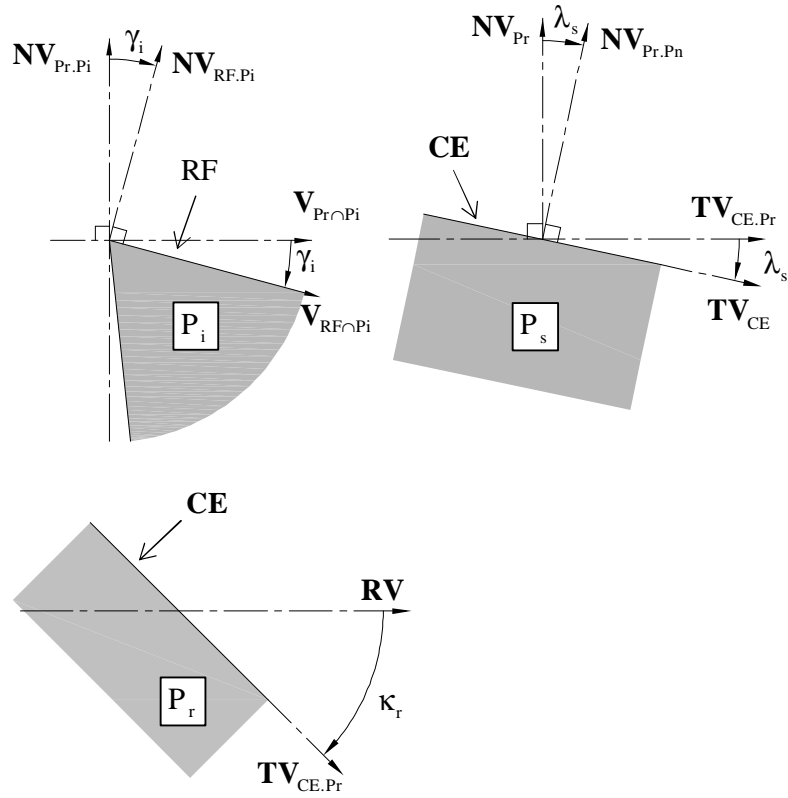


Fig. 7 Cutting edge cross sections for angle parameterization

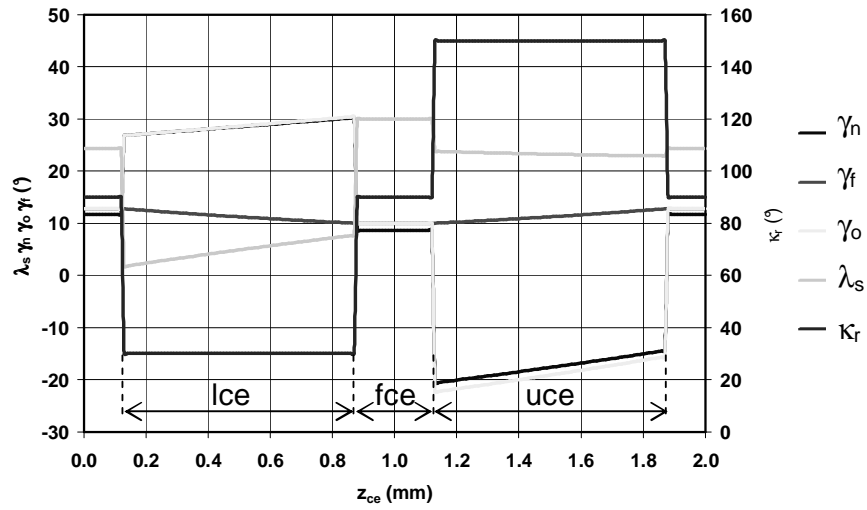


Fig. 8 Cutting angles - case A:  $\gamma_{om} = 10^\circ$ ;  $\lambda_{sm} = 30^\circ$



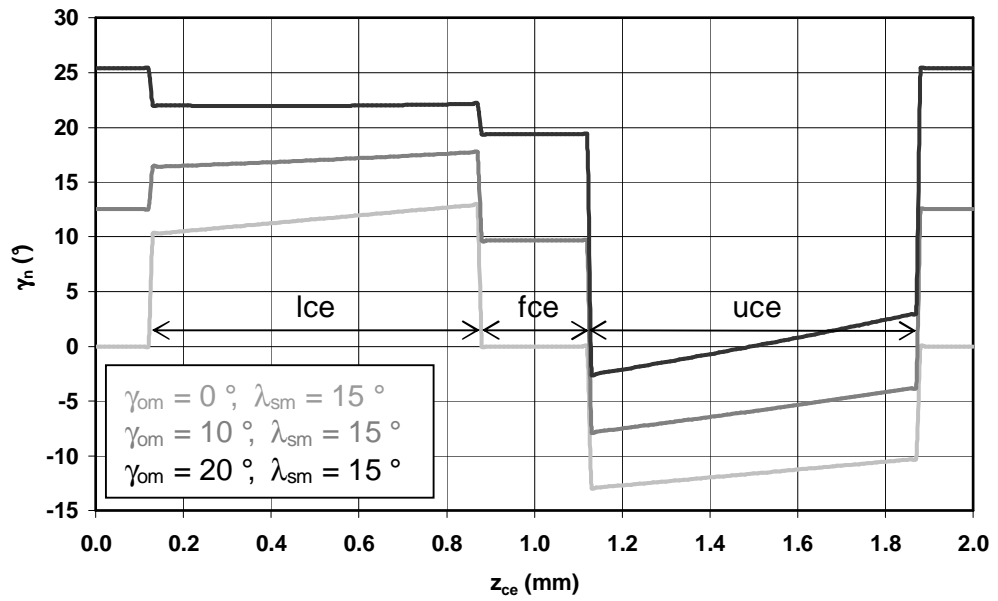


Fig. 9 Normal rake angle ( $\gamma_n$ ) for mills having an identical flute angle -  $\lambda_{sm} = 15^\circ$

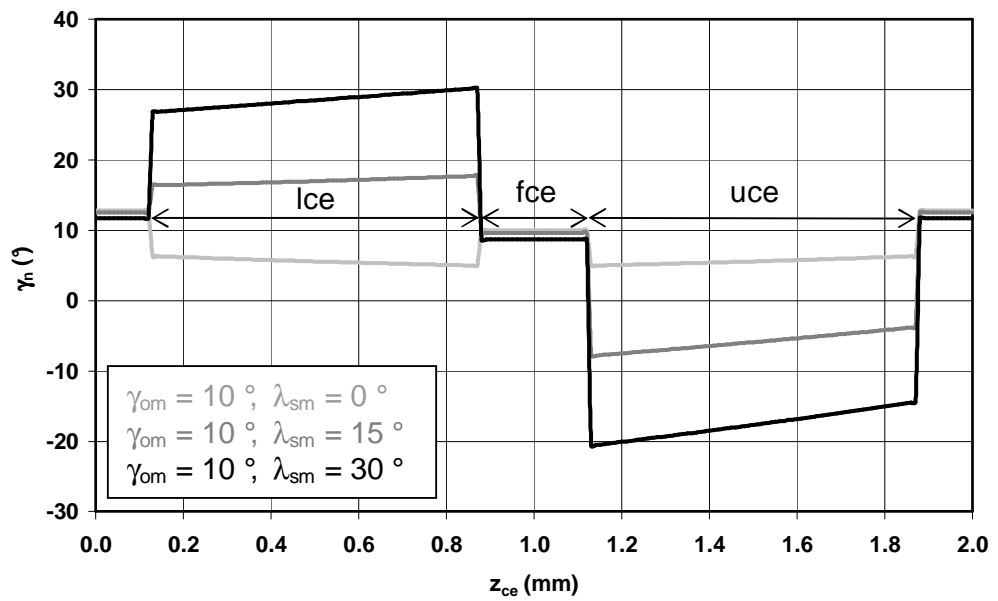


Fig. 10 Normal rake angle ( $\gamma_n$ ) for mills having a constant orthogonal rake angle -  $\gamma_{om} = 10^\circ$