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## Modification of simulated far-field engine noise by changing near field measurement singular values

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Ray W. Herrick Laboratory, Purdue University August 27, 2013



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## Motivations





- Acoustical testing of diesel engines often requires a combination of fired and motored tests.
- Motored testing is a time-consuming and often expensive task.
- Reducing the needed amount of motored testing might:
  - Reduce financial costs.
  - Increase availability of testing resources (e.g., the semi-anechoic chamber and technical support).



# Introduction

- Method demonstrates how a physical modification to an engine can be simulated by changing 'virtual sources' to simulate far-field noise.
- With an understanding of dominant noise-generating mechanisms, method would allow for a simulation of an attenuation of the dominant source.
- The method shown was validated using two separate tests in which only one engine component (Component A) was removed between the tests.







- Relationship between physical sources and near-field measurements can be determined using singular value decomposition and singular value contribution plots (Leclère *et al.*, 2005; Hayward *et al.*, 2012).
- Relationship between the near-field measurements and the farfield measurements can be estimated by solving a cross-spectral matrix problem (Kompella, 1992; Hayward *et al.*, 2013).



# Outline





### Multiple Input/Multiple Output System





#### Multiple Input/Multiple Output System





• Far field measurement, y(t), can be expressed as

$$y(t) = \sum_{j=1}^{N} \int_{-\infty}^{\infty} x_j(\tau) h_{x_j y}(t-\tau) d\tau.$$
  
Impulse response  
of  $H_{x_j y}$ 

• Cross-spectral density between the input,  $x_i(t)$ , and the output is

$$S_{x_iy}(f) = \sum_{j=1}^N H_{x_jy}(f) S_{x_ix_j}(f),$$

• which can be expressed in matrix form as

$$\left[\mathbf{S}_{xy}\right] = \left[\mathbf{S}_{xx}\right] \left[\mathbf{H}\right] \longleftarrow$$

H can be solved by using any robust matrix solution method



## Multiple Input/Multiple Output System





• A method to determine independent spectral characteristics from a set of partially-correlated data



- $S_{xx}$  is Hermitian symmetric, so U = V.
- Each singular value  $\lambda_i$  is independent/orthogonal.
- The singular values (also called virtual sources) represent independent spectral information present in input measurements, but are not necessarily representative of a particular physical source.



Contributions of singular values to input power spectra help to determine a • relationship between virtual and physical sources.

$$\begin{bmatrix}\mathbf{S}_{\mathbf{x}\mathbf{x}}\end{bmatrix} = \mathbf{U}\mathbf{\Sigma}\mathbf{V}^{\mathbf{H}} = \begin{bmatrix}\mathbf{u}_{1}, \mathbf{u}_{2}, \dots \mathbf{u}_{N}\end{bmatrix} diag[\lambda_{1}, \lambda_{2}, \dots \lambda_{N}] \begin{bmatrix}\mathbf{v}_{1}, \mathbf{v}_{2}, \dots \mathbf{v}_{N}\end{bmatrix}^{H}$$

**Color coding example** 

%

>75

5-25

0-5



- Using a color coding scheme depending on the percentage contribution, these can be visualized graphically.
- A similar method is presented in Leclère et al. (2005) •





#### Singular Value Contribution Plot Properties





# Outline





 Examine relationship between dominant noise source to be modified and near-field singular values using singular value contribution plots.



2. Design shaping function(s) of input singular value(s) to simulate physical modification.









1. Examine relationship between dominant noise source to be modified and near-field singular values using singular value contribution plots.



 Design shaping function(s) of input singular value(s) to simulate physical modification.





## Singular Value Shaping Functions





#### Far-field Simulation





#### Far-field Simulation





3. Express relationship between the measured spectra can be as:

$$\begin{bmatrix} \mathbf{S}_{xy} \end{bmatrix} = \begin{bmatrix} \mathbf{S}_{xx} \end{bmatrix} \mathbf{H} = \mathbf{U} \Sigma \mathbf{V}^{\mathbf{H}} \mathbf{H}$$
4. 
$$\begin{bmatrix} \mathbf{S}_{xy,\text{shaped}} \end{bmatrix} = \mathbf{U} \Sigma_{\text{shaped}} \mathbf{V}^{\mathbf{H}} \mathbf{H}$$
5. 
$$\begin{bmatrix} \mathbf{S}_{xy,\text{shaped}} \end{bmatrix} = \mathbf{U} \Sigma \mathbf{V}^{\mathbf{H}} \mathbf{H}_{\text{shaped}}.$$

$$\begin{bmatrix} \mathbf{U} \Sigma \mathbf{V}^{\mathbf{H}} \mathbf{H}_{\text{shaped}} \end{bmatrix}$$



7. Solve for unknown set of transfer paths,  $\mathbf{H}_{\text{shaped}}$ , between measured input and simulated output  $y_{\text{simulated}}$ .

$$\mathbf{H}_{\text{shaped}} = \left[\mathbf{V}^{\text{H}}\right]^{-1} \boldsymbol{\Sigma}^{-1} \boldsymbol{\Sigma}_{\text{shaped}} \mathbf{V}^{\text{H}} \mathbf{H}$$

8. Calculate simulated far-field time history by convolving measured input signals,  $x_i(t)$ , with newly-calculated impulse response of the transfer paths,  $h_{\text{shaped},i}$ .

$$y_{\text{simulated}}(t) = \sum_{i=1}^{N} \int_{-\infty}^{\infty} x_i(\tau) h_{\text{shaped},i}(t-\tau) d\tau$$



## Validation





- Two separate motored tests were conducted at Roush Industries
- Engine configuration was constant between the two tests except for the presence of Component A
  - Test 1 included Component A in the engine configuration
  - Test 2 was operated without Component A























- Physical modification to an engine can be simulated through alteration of singular values, and recalculation of transfer paths between the near- and far-field.
- This method was validated through application to a motored test in which the contribution of Component A was successfully removed across most of the frequency range of interest.
- Method can only be applied to singular values that exhibit a strong relationship with physical sources (i.e. dominant noise sources, or sources measured with no mixing).



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