Piezoelectric Semiconducting Nanowires

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1. Introduction

Semiconductor nanowires have been at the forefront of nanotechnology, bringing forth advances in electronics, optoelectronics and basic physics, to name a few. More recently, there has been increasing interest in the existence of *piezoelectricity* in some of these materials, whereby they are capable of inter-converting mechanical and electrical energy. Piezoelectricity has been found to manifest more strongly in nanowires of some semiconductor materials as compared to the bulk, which makes nanowires particularly attractive for applications in strain sensing and mechanical energy harvesting. At the same time, the geometry and unclamped nature of nanowires render them sensitive to small forces/deflections, and hence there has been an ongoing effort to incorporate them into so-called piezoelectric *nanogenerators* that are capable of harvesting energy from ambient vibrations to power autonomous devices, such as ubiquitous wireless sensor nodes. Furthermore, semiconducting piezoelectric materials have been driving the emerging fields of piezotronics and piezo-phototronics, where the development of a piezopotential in response to stress or strain can be used to tune the electronic and/or optical properties of the material by altering the band structure of the semiconductor. There are many potential sensing and energy-based applications that can arise from the development of this area of research, but only a few candidate semiconducting materials systems have been explored thus far for their piezotronic and photo-piezotronic properties. Further development of the field requires investigation and development of a wide range of piezoelectric semiconducting nanowires. However, the direct measurement of piezoelectric properties of these nanowires is challenging, and thus rarely reported. This is due to generic difficulties associated with measurements of piezoelectric properties of nanoscale objects using conventional scanning

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probe microscopy techniques, which present key characterization challenges in this field. Recent advances in nanoscale characterization of piezoelectric semiconducting nanowires, such as the development of non-destructive piezoresponse force microscopy (ND-PFM), are opening up new avenues into the detailed investigation of nanoscale piezoelectricity in these materials. This chapter provides an overview of piezoelectric semiconducting nanowires, with a focus on the nature of the effect itself, how it manifests in different materials, how it is measured at the nanoscale, and finally different types of piezoelectric energy-related devices that can be achieved using these nanowires. A greater understanding of the underlying physics that governs piezoelectricity in semiconducting nanowires will serve to underpin further developments of their applications in energy devices.

2. Background

2.1. Piezoelectricity

The piezoelectric effect results from relative displacement of ions or polar components within a piezoelectric material due to an applied stress, resulting in a change in net polarization. Piezoelectricity, first described by the Curie brothers [1], refers to the linear interrelation between the electrical and mechanical states of certain materials. Piezoelectricity is manifested in 20 out of the 21 non-centrosymmetric crystal classes, with the exception being the 432 cubic system. Centrosymmetric crystal classes do not exhibit piezoelectricity. Piezoelectricity is manifested as both a "direct" effect, where polarization is created in response to an applied stress, and a "converse" effect, where an applied electric field creates a strain within the material. Piezoelectricity is described mathematically with a set of complementary equations given below:

$$D = \epsilon_T E + dT \tag{1}$$

$$S = d^t E + s_E T \tag{2}$$

where T and S represent stress and strain respectively, which are second rank tensors related to an applied force and the normal to the area over which it acts, D and E represent the electric displacement and electric field vectors, ϵ is the dielectric permittivity of the material, where subscript Trepresents constant stress, d is the piezoelectric tensor (third rank), and d_T is the transpose of d. s_E is the elastic compliance at constant electric field. These terms are second, third and fourth rank tensors respectively, and due to symmetry considerations Voigt notation is often used for convenience to describe the tensors. For the piezoelectric tensor this takes the form of a 3×6 matrix. There are four types of piezoelectric coefficients

$$d_{ij} = \left(\frac{\partial D_i}{\partial T_j}\right)^E \tag{3}$$

$$e_{ij} = \left(\frac{\partial D_i}{\partial S_j}\right)^E \tag{4}$$

$$g_{ij} = -\left(\frac{\partial E_i}{\partial T_j}\right)^D \tag{5}$$

$$h_{ij} = -\left(\frac{\partial E_i}{\partial S_j}\right)^D \tag{6}$$

where the superscript indicates differentiation under constant or zero field. d_{ij} and e_{ij} are the most commonly used coefficients, often coined the piezoelectric strain (d) and charge coefficients (e). *i* ranges from 1 to 3 and *j* from 1 to 6 (Voigt), where 1,2,3 are direction axes and the 3-axis typically denotes the polarization direction, while 4,5,6 denote shear deformation about 1,2,3 axes, correspondingly. d_{ij} therefore describes polarization arising in the *i* direction in response to stress along the *j* direction, or alternatively strain in the *j* direction in response to an electric field along the *i* direction.

2.2. Piezoelectric Semiconductors

The most common semiconductors, with the exception of silicon and germanium, are piezoelectric; these include III-Vs and II-VIs. The wurtzite GaN family of materials, and ZnO are best known for their piezoelectric properties. Piezoelectricity in semiconductor materials can bring about both advantages and disadvantages. Unlike cubic structured GaAs/AlGaAs high electron mobility transistor (HEMT) technology which relies on the separation of dopants from the charge carriers [2], GaN/AlGaN HEMT technology is based on the piezoelectricity and spontaneous polarization discontinuities in III-N heterostrucutres, and does not rely on doping to achieve conductance (Figure 1) [3]. Interestingly, in the more established GaN LED lighting technology, the existence of piezoelectricity and spontaneous polarization is undesired, reducing emission efficiency [4]. This particular issue is directing research efforts towards "non-polar" III-N technology, and polarization-matched layers. For an exhaustive discussion on polarization in semiconductors, consult Ref. [5]



Figure 1: Schematic of the interplay between spontanous polarization, piezoelectricity and crystal orientation in the GaN/AlGaN heterostructure system, leading to the creation of a two-dimensional electron gas at the interface. Reproduced with permission from AIP [3].

Semiconductors include bound and free charges, and the relation between the charges and external and internal potentials is dominated by Poisson's equation and Fermi-Dirac distribution [6], taking the following form:

$$-\nabla^2 \phi = \boldsymbol{\nabla} \cdot \boldsymbol{D} = \rho \tag{7}$$

$$\rho = q \cdot \left(N_D^+ - N_A^- + p - n \right) \tag{8}$$

$$n = \frac{2}{\sqrt{\pi}} N_c F_{1/2} \left(q\phi/k\tilde{T} \right) \tag{9}$$

where q is the electron charge, ϕ is the electric potential (related to the conduction band and Fermi level through $-q\phi = E_C - E_F$), and ρ is the free charge distribution, determined by the ionized donor and acceptor concentrations (N_D^+, N_A^-) , and electron and hole concentrations (n, p). The free carrier concentrations are then related to the potential through the effective density of states (N_c) and Fermi integral $(F_{1/2})$. k is the Boltzmann constant, and here \tilde{T} is temperature.

For a piezoelectric semiconductor, Eqs. 1,2,7-9 are coupled to describe the electro-mechanics of the material. It is important to note that observation of piezoelectric effects in semiconductors relies on the existence of a depletion region, where the semiconductor is not neutral, and therefore is related to junctions and surfaces. Initial observations of coupled behaviour were studied in early and late 1970s reporting photo-mechanical coupling in piezoelectric semiconductors [7, 8] and mechanical modulation of metalsemiconductor Schottky contact barrier height [9, 10], later coined as the piezotronic effect [11, 12]. Lagowski and Gatos described the deformation of CdS and GaAs cantilevers in response to light absorption [7, 8] (Figure 2). They ascribe the observation to generation of surface voltage and converse piezoelectric deformation. This effect was exhibited only when the polar surfaces, [0001] in CdS and [111] in GaAs, were examined (the wide faces of the cantilever). No measurable effect was found for samples with non-polar surfaces, indicating that this effect is related to piezoelectricity. Furthermore, no effect was measured when GaP samples were examined.

Kusaka *et al.* examined the direct piezoelectric effect, where the Schottky barrier height was measured during bending of metal-semiconductor junctions of CdS and GaP [9, 10]. The Schottky barrier change was monitored through current measurements, and it was found that the polarity of the change corresponded to the crystal face of the Schottky contact, and the material (II-VI and III-V semiconductors' piezoelectric coefficients have opposite signs) - indicating that the effect originated in piezoelectricity. It is interesting to note that GaP was examined in both experiments, however it



Figure 2: Schematic of the optical setup to measure the photomechanical coupling in piezoelectric semiconducting cantilevers. Reproduced with permission from Elsevier [8].

only exhibited a piezoelectric related effect in the latter - where a device was fabricated. As mentioned by Lagowski and Gatos, this is most likely due to the presence of a surface accumulation layer in free GaP surfaces, shortening the generated surface photovoltage [8]. This layer is depleted when forming a Schottky contact, allowing for the piezoelectric effect to modify the barrier height.

By solving the piezoelectric equations coupled to Poisson's equation (Eqs. 1,2,7-9) an expression for the piezotronic effect, the change in barrier height with strain, was presented

$$\Delta \phi_B = \pm \frac{d_{31}}{S_{11}} \cdot \frac{V_{bi}}{qN_D} \cdot \frac{1}{R} \tag{10}$$

where V_{bi} is the built in voltage, and 1/R the curvature of the substrate the piezotronic Schottky diode was mounted on. Figure 3 shows a schematic representation of the piezotronic effect in NWs, as was extensively studied in work from Z.L. Wang's group. Importantly, direct stretching and compressing along the polar axis is more accessible in NWs compared to the bulk.

3. Why are piezoelectric semiconducting nanowires special?

This section explores early studies that capture the essence of piezoelectricsemiconductor coupling: interesting phenomena arise in junction regions, where the unique behaviour of semiconductors comes into play. When it comes to semiconductor NWs, their inherent electromechanical characteristics may contribute to an enhanced piezoelectric response, as explained below.



Figure 3: The fields developing within a ZnO NW and near the Schottky contacts for a) unstrained; b) compressed; c) stretched NWs. Reproduced with permission from ACS [11].

3.1. Mechanical properties of piezoelectric semiconducting nanowires

Nanowires have unique mechanical properties due to their size and slender shape. Nanowires exhibit increased failure stress, compared to known bulk properties. The main reason is the smaller likelihood of structural defects in smaller sizes [13, 14, 15]. For example Wang *et al.* found that GaAs of 50-150 nm in diameter could sustain 10-11% strain before failure, a value significantly larger than measured in bulk material [15]. If so, NWs can withstand higher stresses, which in turn can result in increased piezoelectric response. Furthermore, there are reports of increased stiffness (Young's modulus) in NWs [16]. Revisiting Equation 10 for the piezotronic effect, an increased stiffness (reduced compliance) may result in an increased effect for a given strain.

Due to their aspect ratio, NWs are flexible, unconstrained by their envi-



Figure 4: a-d) Different stages of GaAs NW deformation, from contact to failure. Reproduced with permission from Wiley [15].

ronment, and inherently allow larger deformations. Furthermore, they allow the application of tensile and compressive stresses in the same orientation where the electrical properties are examined (d_{33} type effect) [17]. This is unlike the bulk case, where generally the main deformation axis is orthogonal to the examined electrical properties $(d_{31}$ type effect) - see Figure 5. Generally $d_{33} > d_{31}$, and thus a larger response is to be expected from the former. The increased degree of mechanical freedom comes into play through elimination of substrate boundary condition for the inverse piezoelectric coefficient [18, 19]

$$d_{33,bulk}^{eff} = d_{33} - \frac{2S_{13}}{S_{11} + S_{12}} d_{31} \tag{11}$$

where $d_{33,bulk}^{eff}$ is the observed, clamped, coefficient, and S_{ij} are elastic compliance coefficients. For unclamped nanostructures the second term vanishes

$$d_{33,NW}^{eff} = d_{33} \tag{12}$$

Zhao *et al.* have estimated the (negative) contribution of the substrate to ZnO piezoelectricity results in about 50% reduction in the effective piezoelectric coefficient [19].



Figure 5: a) Schematic of an axial ZnO NW piezoelectric nanogenerator, experiencing axial deformation. Reproduced with permission from Nature Publishing Group [17]; b) Schematic of a GaN/AlGaN HEMT experiencing bending, where the device contacts are transverse to the main strain orientation. Reproduced with permission from Eslsevier [20].

3.2. Electronic properties of piezoelectric semiconducting nanowires

Semiconductor NWs have an increased tendency for depletion as their diameter decreases, due to geometry and size related electrostatic effects. Briefly, the cylindrical geometry induces a shallow profile of the potential, compared to bulk [21, 22]. When solving Poisson's equation in cylindrical coordinates, considering a depletion region extending from the NW surface towards its center, Eq. 7 takes the form [22]

$$\frac{d^2\phi}{dr^2} + \frac{1}{r}\frac{d\phi}{dr} = -\frac{qN_D}{\epsilon_s} \qquad ; \qquad R_{dep} < r < R \tag{13}$$

where R is the NW radius and R_{dep} is the onset of the depletion region. Unlike the equation in Cartesian coordinates (used for bulk material), the additional 1/r term (second) requires the first derivative of the potential (*i.e.*, the electric field) to decay slowly in order to avoid singularity - leading to increased depletion.

NW electrostatics also have implications on Schottky barrier height, where non-ideal barrier-lowering effects are weakened in NWs (Figure 6) [23, 24]. A possible implication of increased barrier height and depletion length is reduced screening of the piezoelectric potential formed within NWs in response to strain, leading to a more pronounced piezoelectric response.



Figure 6: Calculated Schottky barrier height for an N-type semiconducting NW as a function of diameter. Non-ideal effects lowering the barrier become less significant as size is reduced, resulting in a higher barrier for smaller NWs, and increased depletion. The barrier height approaches bulk value (dashed) with size. Reproduced with permission from AIP [24].



Figure 7: Schematic of the group-V modulation during NW growth (left) resulting in controlled crystal phase switching in several III-V NWs (right). Reproduced with permission from ACS [25].

3.3. Effect of growth on the piezoelectric properties of semiconducting nanowires

Semiconductor NWs of the III-V family may crystallize in wurtzite as well as zinc-blende phase, unlike their bulk counterparts which crystallize exclusively as zinc-blende (non-nitride III-Vs)[25]. Figure 7 shows the control achieved in switching growth from zinc-blende to wurtzite structure in InAs, GaAs, InP and GaP NWs. Furthermore, it is possible to control growth orientation to grow NWs where the axial orientation is polar/non-polar. The piezoelectric coefficient matrix (Voigt notation) for wurtzite semiconductors contains three non-degenerate coefficients and is given by

$$d_{WZ} = \begin{pmatrix} 0 & 0 & 0 & 0 & d_{15} & 0 \\ 0 & 0 & 0 & d_{15} & 0 & 0 \\ d_{31} & d_{31} & d_{33} & 0 & 0 & 0 \end{pmatrix}$$
(14)

This matrix is well known and used, considering the majority of work on piezoelectricity in semiconductors is related to ZnO and GaN - both wurtzite materials. It is easily and directly applied to NWs, since the growth orientation of the NW is usually [0001], corresponding to the polar axis (3-axis) of the matrix.

For zinc-blende materials (non-nitride III-Vs) a more complicated picture arises: the piezoelectric matrix is usually presented such that the 3-axis coincides with one of the main cubic axis

$$d_{ZB,[001]} = \begin{pmatrix} 0 & 0 & 0 & d_{14} & 0 & 0 \\ 0 & 0 & 0 & 0 & d_{14} & 0 \\ 0 & 0 & 0 & 0 & 0 & d_{14} \end{pmatrix}$$
(15)

This matrix has only one non-degenerate coefficient, the shear coefficient d_{14} . However, III-V NWs, either crystallizing in wurtzite or zinc-blende, have a tendency to grow in the [111]/[0001] orientation (for zinc-blende/wurtzite correspondingly). Considering the NW symmetry, it makes sense to rotate the piezoelectric matrix in Equation 15 such that the 3-axis is [111]. When done in complete analogy to wurtzite, *i.e.* the 1-axis corresponding to $[11\overline{2}]/[10\overline{10}]$ and the 2-axis corresponds to $[\overline{110}]/[\overline{1210}]$, the matrix takes the following form [26]

$$d_{ZB,[111]} = \begin{pmatrix} d_{11} & -d_{11} & 0 & 0 & d_{15} & 0\\ 0 & 0 & 0 & d_{15} & 0 & d_{26}\\ d_{31} & d_{31} & d_{33} & 0 & 0 & 0 \end{pmatrix}$$
(16)

The distinctions between the piezoelectric matrices of zinc-blende and wurtzite, given by Equations 14 and 16 open up opportunities to engineer the piezoelectric properties of a single NW through formation of crystal-phase heterostructures. For example, there is no radial symmetry in ZB since the response to a field applied along the 1-axis will result in a response different than a field applied along the 2-axis.

Demonstrating some of the principles mentioned above (Sections 3.1-3.2), even in bulk material, is the work published by Gerngross *et al.*, who measured the piezoelectric response of chemically etched porous InP (zinc blende) [27]. The measured coefficients were found to be up to 30 times those of bulk InP, due to enhanced depletion in the material (increased surface area), and porosity induced softening [28]. On the other extreme, quantum mechanical simulations have predicted two orders of magnitude increase in the piezoelectric coefficients of ultra-thin (1-2 nm) ZnO and GaN NWs [29].

The piezoelectric properties of ZnO, coupled with the relative ease of fabrication of nanostructures of this material, render it particularly useful and popular for applications in piezoelectric energy harvesting. ZnO is a direct wide band gap ($\sim 3.3 \text{ eV}$) semiconductor with a wurtzite structure, inducing polarity along the c-axis of the structure [30, 31, 32]. Figure 8a shows the wurtzite lattice structure of ZnO with a = 3.25 and c = 5.20, and the origin of the dipole moment that gives rise to piezoelectric in this material [33]. Figure 8b illustrates a typical growth morphology of ZnO nanowire or nanorod with a hexagonal crystal structure and the corresponding facets, where (001) is the polar surface and relatively more reactive while the side facets are non-polar and more stable [30, 31, 32]. Therefore, the ZnO crystal tends to grow faster along c-axis, which is favourable particularly during nanowire growth as it results in a net dipole moment along the axis of the nanowire. ZnO has been shown to be easily grown into a variety of nanostructures with different morphologies and shapes, such as nanorods [31, 34, 35], nanotubes [36, 37], nanowires [38, 31, 39, 40], nanobelts [41] and nanorings, onto a variety of different substrates at relatively low temperatures (<100°C) compared to high-temperature-sintered piezoceramics.

Commonly used synthesis techniques include chemical vapour deposition [42], physical vapour deposition [30, 43], sol-gel synthesis [44, 45] electrodeposition [45, 46, 47, 48] and hydrothermal synthesis [31, 32, 49, 50, 51, 52, 53]. ZnO bulk and thin films are likely to suffer from poor piezoelectric performance due to defects both in the bulk and on the surface that may arise due to environmental degradation [38, 54, 55], while the relatively high stiffness constant of ZnO renders it prone to mechanical failure [56]. However, these limitations of ZnO could be overcome by incorporating nanostructures into nanocomposite systems, as nanostructured ZnO with higher aspect ratio and surface-to-volume ratio, possesses enhanced sensitivity to low-amplitude ambient vibrations as well as reduced fragility compared with their bulk or thin film counterparts [57, 58], making them particularly attractive for energy harvesting applications. In general, single crystal NWs are preferred over polycrystalline ones because there is a single domain of electric dipoles with one polarization direction, but even polycrystalline ZnO nanowires with preferred orientation along the nanowire axis have been shown to exhibit robust piezoelectric energy harvesting performance [57, 59].

4. Characterization of Piezoelectricity in Semiconducting Nanowires

Traditional macro-scale characterization of piezoelectricity is usually done by optical methods (see Figures 9a and 2) for displacement measurement. However these methods are hardly applicable when considering nanostructures such as NWs, which are smaller than the characteristic wavelength. The prevalent tool for nanoscale piezoelectric characterization is piezoresponse force microscopy (PFM), which has been widely used for characterization of ferroelectric and piezoelectric materials [60]. However, when it comes to NWs, either vertical or horizontal, the application of PFM is challenging, due



Figure 8: a) Wurtzite structure model of ZnO; b) Typical growth morphology of ZnO with hexagonal crystal structure. The arrow indicates the polarization direction and the c-axis direction.

to possible mechanical damage and/or dislodgment during contact-mode operation, and reports of PFM-based NW characterization are not common. Other methods such as atomic force microscopy (AFM) based current generation or characterization of the direct piezoelectric effect, are usually applied to NWs. These are discussed in the following sections:



Figure 9: a) Schematic of a dual beam interferometer used to measure bulk material piezoelectric effects. Reproduced with permission from AIP [61]; b) Schematic of a PFM setup: a conductive tip applies AC voltage to a piezoelectric sample, and simultaneously follows the resulting deformation. Reproduced with permission from The Royal Society of Chemistry [62].

4.1. Piezoresponse Force Microscopy

PFM works on the basis of the converse piezoelectric effect: a conductive AFM tip is scanned across a piezoelectric sample in contact mode, while an

AC voltage is applied between the tip and the bottom electrode, through the sample. In response to the bias the sample deforms, and the deformation is monitored through a laser spot reflection from the tip, maintaining a constant contact with the sample through the feedback (Figure 9b). Due to contact mode operation, application of PFM to nanostructures is challenging, and advanced PFM methods are be required for characterization[26], as discussed below in detail.

The first report of PFM application to semiconductor nanostructures was published by Zhao *et al.*, describing the measurement of piezoelectricity in ZnO nanobelts [19]. It was found that the piezoresponse of the nanobelt is 2-3 times stronger than that of bulk material. This finding was explained by the unconstrained boundaries of the nanobelt (Eqs. 11-12).

Most PFM work revolved around characterization of relatively thick, vertical, NWs - predominantly ZnO and GaN [63, 35, 64, 65]. Scrymgeour and Hsu have correlated PFM and conductive AFM (c-AFM) measurements of ZnO nanorods (Figure 10). Interestingly, they have found that thinner nanorods (\sim 150 nm) yield higher piezoelectric responses, and these are coupled to lower conductivity, while the opposite is true for thicker nanorods (\sim 500 nm). The size dependence could be explained by the increased depletion tendency of thin NWs, as discussed in section 3.2. In is noteworthy that the NWs in this study underwent an annealing treatment to form ohmic contacts, and therefore the more common piezotronic effect is not observed in this case. Furthermore, the NWs were mechanically protected by embedment in a polymer layer, probably to overcome contact-PFM induced mechanical damage for non embedded NWs.

Reports of PFM measurements on horizontal NWs are scarce, mainly due to the challenge of using contact mode PFM on unconstrained objects. In a study by Minary-Jolandan *et al.* horizontal GaN NWs were studied by PFM. To avoid mechanical damage, the NWs were clamped to the surface at the edges [66]. In this work two configurations were used to realize characterization of the three non-degenerate piezoelectric coefficients of the wurtzite structure - d_{33} , d_{31} and d_{15} . For a horizontal NW in a standard PFM configuration, where the voltage is applied across the NW axis, the only measurable deformation is related to d_{15} , through a lateral signal (Figure 11b). Characterizing d_{33} and d_{31} requires applying voltage along the NW axis (assuming it is in [0001] orientation), and therefore should be done by applying the signal through lateral electrodes to the NW (Figure 11a). The results ob-



Figure 10: a) PFM and b) c-AFM signals from the same area; c) PFM expansion and d) measured current from the NW shown in (a,b). Reproduced with permission from ACS [35].

tained by Minary-Jolandan *et al.* for the piezoelectric coefficients, $d_{33} = 12.8$, $d_{31} = -8.2$ and $d_{15} = 10.2$ pm/V, are 3-4 times higher than accepted bulk values [66].

Recently, the problems related to contact mode PFM characterization of nanomaterials have been recognized, and non-destructive PFM methods combining mechanical indentation modes with piezoresponse analysis have been developed (Figure 12) [62, 67]. At the heart of these methods lie two principles: i) minimizing the contact-mode mechanical damage to the sample using an intermittent contact mode; ii) extraction of the PFM data from the period of time were significant tip/sample contact is achieved. using ND-PFM the piezoelectric properties of non-clamped horizontal GaAs NWs were examined, as well as vertical InP NWs. This was the first direct PFM measurement of the d_{33} value of wurtzite InP. The value obtained, ~1 pm/V, was in the center of the theoretical predicted range of values [26].

ND-PFM was further employed to characterize VLS grown horizontal



Figure 11: Two configurations for complete characterization of piezoelectricity in horizontal GaN NWs: a) voltage is applied along the NW [0001] axis for d_{33} and d_{31} measurement; b) voltage is applied across the NW axis to measure d_{15} . Reproduced with permission from ACS [66].



Figure 12: Schematic of the ND-PFM setup: the tip periodically indents the sample, minimizing shear stress damage. An AC voltage is applied to induce the converse piezoelectric effect, and the piezoresponse is then extracted from the time periods the tip is in contact with the sample. Reproduced with permission from The Royal Society of Chemistry [62].

GaAs NWs with a predominant zinc-blende phase [26], and electrodeposited ZnO NWs [57]. Both materials allowed examination of the material in uncommon configurations: for GaAs - due to the horizontal configuration, and for ZnO - due to predominant polycrystalline nature, and a non-polar oriented NW axis. ND-PFM provided insight into intricacies of nanoscale piezore-sponse, unavailable by contact PFM, which caused sample damage. In the case of GaAs NWs, the results were found to coincide with finite element simulations for the vertical and lateral deflections of the AFM due to the piezoelectric response of the NW, demonstrating the distinct contributions of different piezoelectric coefficients and side facets (Figure 13c,d). For ZnO, a piezoresponse matching the polycrystalline nature of the sample was found

(Figure 13f).

4.2. Conductive AFM based measurements

A significant portion of piezoelectric NW characterization was performed using conductive-AFM techniques [35, 68, 69, 70, 71, 72, 73]. Generally, the tip is scanned or indented over vertically aligned NWs, grown on a conductive substrate (Figure 14). Since current conduction takes place in this setup, electrical contacts to the NWs play a significant role in understanding the measurement results, and often there is a Schottky contact between the NW and the conductive AFM tip. As shown in Figure 14 as the tip is scanned across the tip of the vertical NW, one side of the NW is strained while the other is compressed. The direction of the generated piezoelectric voltage is opposite in the two cases. Due to the piezotronic effect, in one instance the Schottky barrier between the NW and tip is lowered, while in the other it is increased; correspondingly, in the first case current flow (piezo-generated) is more efficient,



Figure 13: ND-PFM measurements of a GaAs (a-d) and ZnO (e-f) NWs, taken across the NWs: a) GaAs NW topography, with scan direction and cantilever orientation (dashed and solid arrows correspondingly); b) PFM results, showing the vertical and lateral signals, alongside the scan topography. The dashed circle indicates the area of interest; c) close-up to the vertical PFM signal, the dashed lines indicate the simulated signals which may explain the experimental results; d) close-up to the lateral PFM signal, showing the signature of the side facets. Reproduced with permission from IOP [26]; e) ZnO polycrystalline NW topography; f) calibrated vertical PFM response from the NW, showing regions of \pm 10 pm/V, in agreement with the poly-crystallinity and non-polar growth orientation.

while in the latter, significantly less current is measured. Lu *et al.* have measured current generation from both n- and p-type ZnO NWs. It was found that the measured voltage in the two cases is of opposite polarity, and that it originates from different sides of the NW (strained/compressed) - in accordance with the explanation that the piezotronic effect dominates the measurement.



Figure 14: Current asymmetry in the cAFM measurements of a GaN NW a) NW topography; b) current map, showing the current arising in one side; c) line scan of the current map and topography showing the current arising on the stretched side of the NW, and subsiding on the compressed side. Reproduced with permission from AIP [72].

Wang et al. have examined the influence of doping concentration in the range of $10^{17} - 10^{19}$ cm⁻³ on the performance of NW based nanogenerators and piezotronic junctions [74]. They have found that for nanogenerator operation, where there is a need to generate voltage and induce current flow, output current voltage was not a monotonic function of the doping, but that there is an optimal value of doping mitigating the decrease in resistivity on the one hand side, and screening of the piezoelectric potential on the other. For piezotronic applications, where the main effect is changing the Schottky barrier height, they have found that the lowest concentration yields the highest electromechanical gauge factor. This result stems from the increased

depletion region associated with lower doping levels. A notable distinction between this method and PFM is the need to generate significant stresses (by bending), while due to the AFM deflection sensitivity (pm range) horizontal NWs can be examined as well as vertical.

4.3. Directly measured piezoelectric properties of semiconducting nanowires

Both AFM based methods open up an avenue for basic studies of NW piezoelectricity, however, the motivation for piezoelectric work on semiconductor NWs is mechanical energy harvesting and piezo-photo-tronic applications, and direct piezoelectric performance was frequently examined. Two configurations are usually considered: vertical (Figure 15a), where the NWs are compressed and released to excite the piezoelectricity[73, 75, 76, 77], and horizontal (Figure 15b), where the NWs are lying on a flexible substrate and are compressed/strained in accordance with the substrate [17, 76, 78]. Notably, in most of these cases, the NW experiences uniform strain/compression, unlike the conductive AFM case, where the NW experiences nearly pure bending. Furthermore, through rational design of growth and contacting, enhancement of the output voltage from mV to V range (serial connection of lateral devices), and current from nA to μ A range (vertical array devices) was achieved.



Figure 15: Connecting NWs for energy applications. a) parallel connections of a NW array, maximizing generated current. Adapted with permission from Wiley [77]; b) serial connection of NWs, maximizing generated voltage. Adapted with permission from ACS [78]

The potential of piezoelectric semiconductor NWs for realizing further advanced applications such as piezoelectric modulated field effect transistors (FETs) [79, 80], or piezotronic logic [81], have also been demonstrated. Kwon *et al.* have shown that through piezotronic modulation of the gateoxide-semiconductor junction, the effective carrier mobility increases 4 times for 1.5% strain of the NW FET. They have ruled out piezoresistive effects by demonstrating an opposite effect on top- and bottom-gated devices, indicating that the crystal orientations determines the performance, and not the strain in-itself. Wu *et al.* used horizontal ZnO NWs located on both sides of a flexible substrate to realize a logic inverter [81]. Bending the substrate results in compression of NWs on one side, and strain of the NW on the other. Due to the piezotronic effect, one Schottky barrier is reduce while the other increased leading to inverter operation (Figure 16).



Figure 16: Schematic of the two sided ZnO NW based logic. The complementary response of the NWs on the opposite sides of the substrate, allows realizing an intverter operation. Reproduced with permission from Wiley [81].

5. Piezoelectricity in Semiconductor Nanowires for Energy Applications

5.1. II-VI Nanowires

Owing to a variety in synthesis methods [82, 83] and outputs [82, 84] (NWs, nanoribbons) ZnO was the first semiconductor nanostructure to be vastly studied for nanoscale piezoelectric applications [85, 86]. Other members of the II-VI family such as CdSe, CdS, and ZnS were examined as

well [87, 88, 89]. These materials generally have large, direct, band-gaps, and higher piezoelectric coefficients compared to III-Vs (also of opposite sign)[90, 91], making them attractive candidates for piezotronic applications.

5.1.1. ZnO NWs

ZnO NWs have been widely reported for their use in various energy applications, including as piezoelectric nanogenerators for mechanical energy harvesting. ZnO possesses good piezoelectric properties at nanoscale [92, 93], which in some cases can be comparable to lead-free piezoceramic oxides. Other attractive properties include ease of nano-synthesis [57], being environment friendly [94] biocompatible [95], lightweight [96], scalable and low-cost [97] with good mechanical [98] and thermal stability [44]. In most cases, ZnO nanowires are grown on a conducting substrate which serves as the bottom electrode, and a top electrode is separately applied post-growth. The device is then subjected to mechanical excitation and the resulting piezo-generated charge is collected to drive an external circuit. The presence of a substrate may introduce issues related to flexibility of the device and/or delamination of NWs during operation. To overcome this issue, ZnO nanowire-based nanogenerators have been developed where a polymer is introduced into the device design to improve mechanical stability as well as flexibility. Such device designs include dispersions of ZnO NWs within a soft polymeric matrix, however, this has the disadvantage of randomised polarization directions of the individual ZnO NWs. As a matter of fact, fatigue performance of ZnObased nanogenerators is often not reported in the literature, as the material is additionally prone to environmental and mechanical degradation over time. However, studies where ZnO nanowires have been grown within nanoporous polycarbonate templates, and then incorporated into nanogenerators while still embedded and aligned, have resulted in long and reliable energy harvesting device lifetimes [57, 59]. Table 1 summarizes key ZnO nanowire-based nanogenerators that have been reported over the years, highlighting inherent advantages and disadvantages of each.

5.1.2. Other II-VIs

An early demonstration of piezoelectric current generation from a 150-100 nm CdS NWs was published by Lin *et al.*in 2008[87]. Using the conductive AFM method, different responses were achieved on the stretched and compressed sides of the NW, confirming piezoelectric dominated behaviour. The output current was found to increase when pure WZ NWs were examined,

NG Design	Type	Examples	Advantages	Disadvantages
Substrate based	ZnO NWs + Rigid substrate	ZnO NWs on indiumtinoxidetinoxidecoated glass substrate[35, 99, 100]orAu-coatedSiT6, 31, 49, 101]	Easy to obtain dense and well-aligned NWs.	Not flexible and bendable; NWs are short (< 4 m), leading to low power out- put; reduced strain levels due to the brittleness of ZnO [102].
	ZnO NWs + Flexible substrate	ZnO NWs on ITO-coated polyester substrate [96, 103, 39, 104], polyimide film [38] plastic film [68], or paper substrate [105]	Flexible and bend- able; easy to obtain dense and well-aligned NWs.	NWs are short, leading to low power output; prone to delamination when bent; re- duced strain levels [102]
Substrate less	ZnO NWs + Di- electric polymer	ZnO NWs + poly(dimethylsiloxane) (PDMS) [106, 102], or poly(methyl methacrylate) (PMMA)[107]	Flexible, bendable and robust	Low power output due to randomly oriented ZnO NWs and low proportion of NWs inside the composite; less control on the ratio of ceramic and polymer; not scalable, repeatable and reproducible
	ZnO NWs + Piezo- electric polymer	ZnO NWs + polyvinylidene flu- oride (PVDF)[108]	Flexible, bendable and robust	Randomly oriented ZnO NWs has lower piezoelectric coefficient than PVDF; this composite does not improve the overall power output
Template-assisted	ZnO NWs + Poly- meric template	ZnO NWs $+$ polycarbonate (PC) template [59, 57, 44, 37, 46, 47]	Easy to obtain long and well-aligned NWs; flexible, bendable and robust; superior me- chanical stability	fatigue endurance limit Rel- atively low output power due to the lower proportion of ZnO NWs.

compared to WZ/ZB mixed phase NWs. In a later work, the piezotronic effect was also demonstrated on CdS and CdSe NWs [109, 110], and energy harvesting with CdTe NWs [111].

5.2. III-V Nanowires

5.2.1. III-Nitride Nanowires

Alongside ZnO, III-Ns, and GaN in particular is the most widely studied piezoelectric NW material. The piezoelectric coefficients of GaN and AlN (about 3 and 5 pm/V [112]) are smaller than those of ZnO (10-12 pm/V), thus making them less attractive for energy harvesting applications. However the large range of visible range band-gap tunability provided by III-N alloying, suggests that combining piezotronic and photonic applications - coined as piezo-phototronics is worthwhile. The effect of strain on the performance of III-N based optical devices has been examined [113, 114, 115, 116]. As mentioned above (Section 2.2), polarization induced internal fields result in reduced emission efficiency. Peng *et al.* have demonstrated the control of InGaN/GaN multi-quantum well NW LED by application of stress [113]. Subsequently, strain has been shown to improve the emission of bulk In-GaN/GaN based LEDs [117].

Mechanical energy harvesting has also been successfully demonstrated using various types of III-N NWs, exploring issues such as doping and geometrical design and their influence on energy harvesting efficiency.[118, 119, 71, 73, 74, 120].

5.2.2. Non-nitride III-V Nanowires

The piezoelectric properties of III-As and III-P have not received significant attention, despite being known and utilized for electro-mechanical applications [121, 122]. The main reasons for that are the lower piezoelectric coefficients, and non-polar technology ([001] and [110] cubic orientations in zinc-blende), prevailing non-nitride III-V bulk electronic and optoelectronic technology [123, 5]. Nonetheless, the various nanostructures Vs. bulk distinctions described in Section 3, apply to non-nitride III-Vs as well. Indeed high piezoelectric coefficients have been predicted for III-Vs in the wurtzite phase [124], which is relevant for III-V NWs. Except from PFM work mentioned above[26], piezoelectric generation from III-V were examined [125, 126], pointing out the role of stress distribution from an upper contact to a single NW piezo-element, in increasing the piezoelectric efficiency. Recently, the piezoelectric properties of wurtzite GaAs were examined using



Figure 17: Schematic and operation of a GaN array based nanogenerator. a) schematic of the device and experimental setup; b) schematic of the mode of operation, note that the NWs are compressed through transverse stretching; c) nanogenerator output voltage; d) schematic band diagram for the Schottky contact, which is responsible for the effect through modulation of the charges in the depletion region. Reproduced with permission from IOP [73].

the c-AFM apparatus [127], demonstrating the piezo-phototronic effect in increasing generated current under illumination.

6. Summary

The piezoelectric properties of semiconducting nanowires have many applications in energy harvesting and sensing devices based on the inter-dependence of the mechanical, electrical and optical properties of these materials. In most cases, nanowires have been found to exhibit superior electromechanical properties when compared to the bulk of the material, and these can be further tuned by controlling the growth method. The crystalline phases present in these semiconducting nanowires play a strong role in determining the nature of piezoelectricity in these systems, and hence advances in growth and characterization of these nanowires have paved the way for the development of novel devices based on this effect. Importantly, a greater level of understanding and control of piezoelectric properties of semiconducting nanowires will serve to underpin advances in the emerging fields of piezotronics and photo-piezotronics, as well as in the development of energy harvesters for small-power applications. Materials and device engineering at the nanoscale therefore offer new routes towards exploiting the piezoelectric properties of semiconducting nanowires for a wide range of energy applications, and there remains plenty of scope for innovation in this area.

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