

Dynamics of two-component Bose-Einstein condensates in rotating trapsI. Corro,¹ R. G. Scott,² and A. M. Martin¹¹*School of Physics, University of Melbourne, Parkville, Victoria 3010, Australia*²*Midlands Ultracold Atom Research Centre, School of Physics and Astronomy, University of Nottingham, Nottingham NG7 2RD, United Kingdom*

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The dynamics of two-component Bose-Einstein condensates in rotating traps is investigated. In the Thomas-Fermi limit, equations of motion are derived showing multiple static solutions for a vortex-free condensate. Dynamic stability analysis of these solutions and comparison to truncated Wigner simulations enable us to identify the regimes for which vortex states will occur. In addition, our analysis predicts center-of-mass oscillations that are induced by interspecies interactions and affect each component separately. For attractive interspecies interactions, these oscillations lead to a stable symmetry-broken state.

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I. INTRODUCTION

A two-component Bose-Einstein condensate (TCBEC) exhibits a wide range of interesting behavior that has been the subject of much theoretical and experimental research. The two components may form either miscible or immiscible phases exhibiting complex density profiles [1–5]. For repulsive interspecies interactions, the two components may also form symmetry-broken states [4–10]. For rotating TCBECs, interlocking vortex lattices [11] and vortex sheets [12] have been predicted theoretically, with vortex lattices being confirmed experimentally [13]. This has led to much interest in the dynamics and collective excitations of these systems [14–16] and recently a number of papers have also predicted, through thermodynamic arguments, the possibility of forming giant vortices [17,18].

This large number of phenomena is due to the numerous experimental parameters that can be varied. For example, the atom number, masses, interaction strengths, trapping frequency, and trap ellipticity can all be varied for each component separately. The parameter space is far too large to be fully investigated through numerical simulations. For this reason, we investigate the dynamics of a TCBEC through analytic methods then investigate points of interest through numerical simulations. For single-component Bose-Einstein condensates (BECs), considerable theoretical [19–25] and experimental [26–30] (for a summary, see Ref. [22]) effort has been applied to understanding their dynamical properties under rotation. A major result of this work was that only considering the thermodynamic stability of the BEC [31] does not correctly predict the onset of vortex nucleation. It is instead necessary for the BEC to be dynamically unstable (dynamical instability implies thermodynamic instability, but not visa versa: see, for example, Ref. [32]).

We study the dynamical instabilities of TCBECs in rotating traps by deriving static solutions in the rotating frame in the Thomas-Fermi limit. We find that these solutions describe quadrupolar dynamics. Through numerical simulations, we show that instabilities in these solutions lead to phases that have already been predicted thermodynamically, such as interlocking vortex lattices. In addition, these solutions predict interspecies-interaction-mediated center-of-

mass (c.m.) instabilities. We observe these oscillations numerically and find that they can settle down into a stable symmetry-broken state. This state is different to previously studied symmetry-broken states [4–10] in that it only occurs for attractive interspecies interactions.

The paper is laid out as follows. In Sec. II, we derive equations that govern the stable irrotational (vortex-free) motion of a TCBEC in a rotating trap. We employ the Thomas-Fermi approximation to derive analytic results and find that when stable, both components undergo quadrupolar oscillations of different magnitudes. In Sec. III, we derive stability equations for these static solutions (critical points) in the rotating frame. These instabilities indicate that the TCBEC will begin to evolve dynamically. We identify four different instabilities: (i) catastrophic instability, (ii) ripple instability, (iii) c.m. instability, and (iv) intraspecies c.m. instability. Types (i) and (ii) lead to turbulence and vortex nucleation. Types (iii) and (iv) lead to c.m. motion. In Sec. IV, we detail the results of numerical simulations used to investigate the analytic predictions. These simulations reveal the dynamics induced by the instabilities studied in Sec. III. They show how turbulence in the TCBEC allows for the formation of states with topologically distinct phase profiles which eventually settle down into either giant vortices, interlocking vortex lattices, or vortex sheets. The simulations also show that the c.m. instabilities do not lead to vortex nucleation, but eventually settle down into a stable state (in the rotating frame), which, for the case of attractive interspecies interactions, breaks the 180° rotational symmetry of the rotating-frame Hamiltonian.

II. THOMAS-FERMI APPROXIMATION**A. Hydrodynamical equations**

In practice, a TCBEC can be stirred by introducing a rotating anisotropy into the confining potential. If done adiabatically, the TCBEC will settle down into a state that oscillates in unison with the rotating trap. The equations of motion can then be found by considering static solutions in the rotating frame. A TCBEC can be described by two mean-field wave functions (Ψ_1 and Ψ_2) whose time evolution is

dictated by the coupled two-component Gross-Pitaevskii equation (GPE) [33]. In a reference frame rotating with angular velocity $\mathbf{\Omega}$, these coupled equations become

$$i\hbar \frac{\partial \Psi_j}{\partial t} = \left[\frac{\hbar^2 \nabla^2}{2m_j} + \mathbf{V}_j + g_j |\Psi_j|^2 + g_{12} |\Psi_{j'}|^2 - \mathbf{\Omega} \cdot \hat{\mathbf{L}} \right] \Psi_j, \quad (1)$$

where the j subscripts ($j=1$ or 2) refer to the component under consideration and $j' \neq j$. m_j and \mathbf{V}_j are the mass and the potential affecting component j . g_j and g_{12} are the intra- and interspecies-interaction coefficients given by $g_j = 4n_0 \pi \hbar^2 a_j / m_j$ and $g_{12} = 2n_0 \pi \hbar^2 a_{12} [m_1 + m_2] / [m_1 m_2]$. Here, a_j and a_{12} are the intra- and interspecies scattering lengths, respectively. The n_0 term allows for a rescaling such that $\|\Psi_j\| = N_j / n_0$, where N_j is the number of atoms in component j .

As in the one-component case [19], it is possible to derive exact solutions in the Thomas-Fermi approximation (TFA) (for a detailed description of the analytic methods, see [25]). The GPE in the frame rotating with the potential is transformed using $\Psi_j = \sqrt{\rho_j(\mathbf{r}, t)} e^{i\phi_j(\mathbf{r}, t)}$ (ρ_j is the density of component j and ϕ_j is the phase), and the TFA [34] is applied, giving the hydrodynamical equations of motion

$$\frac{\partial \rho_j}{\partial t} = \nabla \cdot \left[\rho_j \left(\frac{\hbar}{m_j} \nabla \phi_j - \mathbf{\Omega} \times \mathbf{r} \right) \right], \quad (2)$$

$$-\hbar \frac{\partial \phi_j}{\partial t} = \Theta_j + g_j \rho_j + g_{12} \rho_{j'}, \quad (3)$$

$$\Theta_j = \frac{\hbar^2}{2m_j} |\nabla \phi_j|^2 + V_j - \hbar \nabla \phi_j \cdot \mathbf{\Omega} \times \mathbf{r}. \quad (4)$$

We take $\mathbf{\Omega} = \Omega(0, 0, 1)$ and $V_j = \frac{m_j}{2} [(1 - \epsilon_j) \omega_j^2 x^2 + (1 + \epsilon_j) \omega_j^2 y^2 + \omega_{zj}^2 z^2]$. Here, ϵ_j , ω_{zj} , and ω_j are, respectively, the ellipticity in the x - y plane, the frequency in the z direction, and the frequency in the x - y plane when $\epsilon_j = 0$. This gives a reference frame that is rotating around the z axis in which the potential is static, which corresponds to modeling a potential that is rotating around the z axis with angular velocity $-\mathbf{\Omega}$. In what follows, we enumerate the species so that $m_1^2 \omega_1^4 / g_1 < m_2^2 \omega_2^4 / g_2$. We will see later that the behavior of each component depends heavily on these criteria.

Steady state solutions in the rotating frame are obtained by setting $\frac{\partial \rho_j}{\partial t} = 0$ and $-\hbar \frac{\partial \phi_j}{\partial t} = \mu_j \equiv$ the chemical potential of species j . Solving Eq. (3) gives two possible solutions for the density: if the density of both components is nonzero, then

$$\rho_j^o = \frac{g_{j'}(\mu_j - \Theta_j) - g_{12}(\mu_{j'} - \Theta_{j'})}{g_j g_{j'} - g_{12}}. \quad (5)$$

If one of the components has zero density, then the solution for the other component is

$$\rho_j^s = \frac{1}{g_j} (\mu_j - \Theta_j). \quad (6)$$

Regions in the BEC where Eqs. (5) and (6) are applicable will be referred to as the *overlapping region* and *singular*

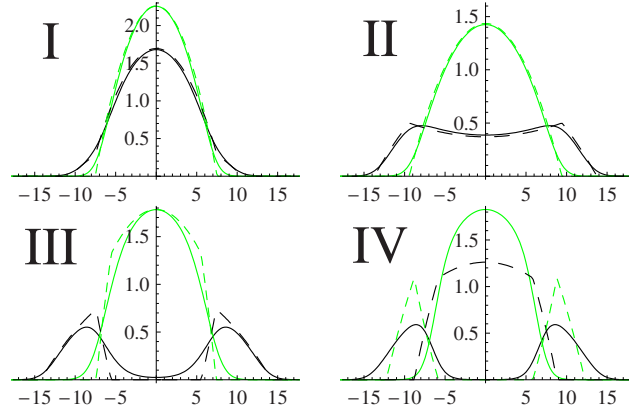


FIG. 1. (Color online) Examples of one-dimensional (1D) slices of the TF density profiles (dashed curves) and exact numerical solutions of the two-component GPE (solid curves) for component 1 (black), component 2 [green (gray)], $\epsilon_1 = \epsilon_2 = 0$, $\omega_1 = \omega_2 = 0.1$, $\hbar = 1$, $m_1 = 1$, $m_2 = 1.5$, $g_1 = 1$, $g_2 = 0.5$. (I) $g_{12} = -0.5$, (II) $g_{12} = 0.4$, (III) $g_{12} = 0.65$, and (IV) $g_{12} = 0.8$. The horizontal (vertical) axes are given in units of $l(l^{-3})$, where $l = g_1 m_1 / \hbar^2$.

region, respectively (indicated by superscripts o and s). As in the one-component case, the TFA has the effect that ρ_j can become negative [34]. When this is the case, we assume that $\rho_j = 0$. Given the above, the total density for each component can be expressed as

$$\rho_j = \rho_j^o H(\rho_j^o) H(\rho_{j'}^o) + \rho_j^s H(-\rho_j^o) H(\rho_{j'}^s), \quad (7)$$

where $H(\rho) = 0$ for $\rho < 0$ and $H(\rho) = 1$ for $\rho > 0$. Without rotation ($\mathbf{\Omega} = \nabla \phi_1 = \nabla \phi_2 = 0$), Eq. (7) corresponds to that derived in Refs. [1,2].

B. Validity of the Thomas-Fermi approximation

In this section, we investigate the Thomas-Fermi approximation and its validity for a nonrotating TCBC. A two-component BEC has two phases. When $-\sqrt{g_1 g_2} < g_{12} < \sqrt{g_1 g_2}$, the system is in the *miscible phase* where both components interpenetrate. $g_{12} > \sqrt{g_1 g_2}$ is the *immiscible phase* [35,36] where the two components repel each other. In the case of a harmonic trap, the interspecies repulsion causes either one component to form a shell around the other or both components to separate asymmetrically [4] about the trap center. The asymmetric state occurs for $g_1 \approx g_2$, $m_1 \approx m_2$, and $g_{12} > \sqrt{g_1 g_2}$ [37].

For BECs in a harmonic trap, the following general behavior can be seen from Eq. (5). When $g_{12} < g_2 m_1 \omega_1^2 / (m_2 \omega_2^2)$, both components form overlapping density profiles with concave down parabolic shapes [Fig. 1(I)]. When $g_{12} = g_2 m_1 \omega_1^2 / (m_2 \omega_2^2)$, ρ_1^o is a constant, and for values of g_{12} larger than this, ρ_1^o begins to dip in the overlapping region at the center of the condensate [Fig. 1(II)]. As g_{12} is increased, ρ_1^o dips further until $g_{12} > g_2 m_2 / \mu_1$ where the TFA predicts $\rho_1^o = 0$ at the very center of the trap [Fig. 1(III).]

The Thomas-Fermi approximation assumes that the kinetic energy of the wave function is negligible compared to the interaction and potential-energy terms. For single-component BECs, it is valid for large g and atom number,

which is satisfied for typical experimental parameters. These criteria must also be satisfied for each component individually if the TFA is applied to a TCBE. Moreover, it has been shown [3] that the accuracy of the TFA in the two-component case can have a more complicated dependence on the parameters used. In this section, we explore the parameter space of a TCBE to identify these additional constraints.

We have conducted extensive comparisons between the TFA and full GPE solutions, identifying the following conditions for TFA validity. For $-\sqrt{g_1 g_2} < g_{12} < g_2 \mu_2 / \mu_1$, we find excellent agreement [Fig. 1(I) and Fig. 1(II)] [$g_{12} = g_2 \mu_2 / \mu_1$ is the point where the TFA predicts $\rho_1(\mathbf{r})$ reaches 0 at $\mathbf{r}=0$]. As $g_{12} = g_2 \mu_2 / \mu_1$ is approached, the TFA results deviate from the full GPE results, but remain qualitatively correct for $g_2 \mu_2 / \mu_1 < g_{12} < \sqrt{g_1 g_2}$ [Fig. 1(III)]. For $g_{12} > \sqrt{g_1 g_2}$, the TFA solutions are completely different from the full GPE solutions [Fig. 1(IV)]. This is due to the intense repulsion between the two components resulting in sharp curvature in the wave functions and hence kinetic energy cannot be neglected. For $g_{12} < -\sqrt{g_1 g_2}$, the TFA solutions are unphysical, reflecting the fact that without kinetic energy, the condensate is unstable. In what follows, we therefore consider the TFA solutions only in the region of their validity: $-\sqrt{g_1 g_2} < g_{12} < \sqrt{g_1 g_2}$. In other words, the TFA is valid for any two-component BEC that is within the miscible phase. Equation (5) shows that in this region of validity, the component with the smallest value of $m^2 \omega^4 / g$ (component 1 by definition) will always sit to the outside of component 2 and, as expected, this behavior continues into the immiscible phase where component 1 forms an almost hollow shell around component 2.

One should note that the condensates begin to separate before the immiscible phase is reached and the transition as g_{12} passes $\sqrt{g_1 g_2}$ is continuous, i.e., there is no qualitative difference upon reaching the immiscible phase. However, as shown by Timmermans [35], the nature of the component separation is different in the two phases. For $g_{12} < \sqrt{g_1 g_2}$, any separation is caused purely by the potential; if no trap gradient existed then both species would overlap with constant densities. For $g_{12} > \sqrt{g_1 g_2}$, the two species separate irrespective of the trap. Timmermans pointed out that this situation is much like the case for ordinary fluids. Two fluids may mix freely but can still be separated by an external potential such as gravity. They will, however, mix freely again once stirred. Conversely, immiscible fluids such as oil and water always separate and remain so even after mixing. Indeed, we find that although initially, while the condensate is irrotational, there is no observable crossover between the two phases, once the BEC is stirred via rotation, the condensate displays very different behavior depending on which phase it is in.

C. Rotation

In this section, we derive the response of the condensate phase and density to rotation. Without rotation, the wave-function phase is constant for both components. After introducing rotation, solutions to the equations of motion can be found by inserting a quadrupolar oscillation ansatz for the phase

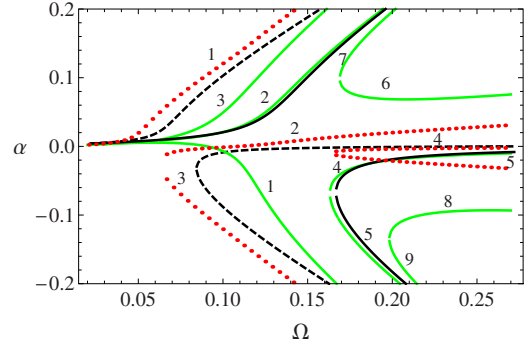


FIG. 2. (Color online) The solutions for the α 's with $\hbar = \mu_1 = \mu_2 = 1$, $\omega_1 = 0.2$, $\omega_2 = 0.1$, $\epsilon_1 = \epsilon_2 = 0.1$, $m_1 = 1$, $m_2 = 1.5$, $g_1 = 1$, $g_2 = 0.5$, $g_{12} = 0.1$. Shown are solutions to α_1^o [thick green (thick gray)], α_2^o [red dots (gray dots)], α_1^s (black dashed), and α_2^s (black line). The branch numbering sits above the corresponding branch; it allows matching of each α_1^o solution to the corresponding α_2^o solution. Ω and α are in units of μ_1 / \hbar .

$$\phi_j = \frac{m}{\hbar} [\alpha_j^o H(\rho_j^o) H(\rho_{j'}^o) + \alpha_j^s H(-\rho_{j'}^o) H(\rho_j^s)] x y \quad (8)$$

and Eq. (7) into Eq. (2) and solving for the α 's. For α_j^s , this gives

$$\alpha_j^{s3} - 2\alpha_j^s \Omega^2 + \omega_j^2 (\alpha_j^s - \epsilon_j \Omega) = 0, \quad (9)$$

which has up to three real solutions and is identical to the one-component case [20]. For the α^o 's, we get two simultaneous equations

$$\begin{aligned} -2g_{12} m_j [\omega_j^2 (\alpha_j^o - \epsilon_j \Omega) + \alpha_j^o (\alpha_j^o \alpha_{j'}^o - 2\Omega^2)] \\ + 2g_j m_{j'} [\alpha_{j'}^{o3} - 2\alpha_{j'}^o \Omega^2 + \omega_{j'}^2 (\alpha_{j'}^o - \epsilon_{j'} \Omega)] = 0. \end{aligned} \quad (10)$$

This yields up to nine real solutions for $\{\alpha_1^o, \alpha_2^o\}$.

The α 's are real constants representing the magnitude and orientation (positive or negative) of quadrupolar oscillation in the two components. Specifically, the singular and overlapping regions of component 1 (component 2) undergo quadrupolar oscillations of different magnitudes, labeled α_1^s and α_1^o (α_2^s and α_2^o), respectively. The density profile of each component is heavily influenced by this oscillation, in particular its ellipticity. This dependence has the interesting property that when α is negative, the BEC is deformed oppositely to the elliptical deformation caused by the trap. In other words, the BEC forms an elliptical profile that is rotated 90° to that of the confining elliptical potential.

D. Discussion

An example with seven solutions to Eq. (10) for $\{\alpha_1^o, \alpha_2^o\}$ is shown in Fig. 2. Each branch represents a different static solution for a TCBE in a rotating trap, each with quadrupolar oscillations of different magnitudes and orientations. Although these static solutions display a very complicated dependence on the many free parameters in the system, the situation is greatly simplified by the fact that the BEC will prefer the branch with the lowest energy.

The energy of a given solution increases as the magnitude of α increases. Also, for the solutions given by Eq. (5), the

density of component i in the overlapping and singular regions does not join continuously at the boundary unless $\alpha_i^o = \alpha_i^s$. This adds a large amount of kinetic energy at the interface of the two regions as the density profile must vary rapidly to join the two regions. The solution with the smallest energy can therefore be determined by removing α_i^o branches that do not correspond closely to one of the α_i^s branches. One then selects the remaining branch which has the smallest magnitude. From the figure, it is evident that for $\Omega < 0.06$, branch 1 has the lowest energy, for $0.06 < \Omega < 0.16$ branch 2 has the lowest energy, and for $\Omega > 0.16$ branch 4 has the lowest energy.

The behavior of the BEC can then be described as follows. Initially, after condensation and before introducing rotation, the BEC will be in a state that corresponds to the stable static solution which has the lowest energy for the given set of experimental parameters. The BEC can then be transferred to a new state by adiabatically ramping these parameters. As this is done, the BEC will move along one of the static solutions. In the case of Fig. 2, each of branches 1, 2, and 4 can be accessed by ramping the parameters in different ways. Branch 1 can be accessed by keeping ϵ constant while ramping Ω from 0 to some final value or by keeping $\Omega < 0.06$ fixed and ramping ϵ . Branch 2 (4) can be accessed by fixing $0.06 < \Omega < 0.16$ ($\Omega > 0.16$) and ramping ϵ from 0 to some final value. Branch 2 is also of particular interest because it leads to each BEC component undergoing quadrupolar oscillations in opposite directions (i.e., $\alpha_1^o > 0$ and $\alpha_2^o < 0$).

The BEC cannot follow these static solutions for all parameter values; eventually, one of two possibilities occurs. In the first case, the static solution which the BEC is following can cease to exist (*catastrophic instability*) [24]. This leads to a massive disruption in the BEC's density profile, followed by the onset of turbulence and vortex nucleation. The second case occurs when the BEC is still in a state described by a static solution, but the solution itself is not stable. In this case, either the BEC can become turbulent (*ripple instability*), which leads to the formation of vortices, or the c.m. of the BEC can become unstable (*center of mass instability*).

III. STABILITY

A. Equations

Stability can be analyzed by linearizing Eqs. (2) and (3) about the critical points. We consider infinitesimal perturbations $\rho_j \rightarrow \rho_{0j} + \delta\rho_j$ and $\phi_j \rightarrow \phi_{0j} + \delta\phi_j$, with $\{\rho_{0i}, \phi_{0i}\}$ being a set of static solutions to Eqs. (2) and (3). In the overlapping region where both condensates coexist, one obtains

$$\frac{\partial}{\partial t} \begin{bmatrix} \delta\phi_1 \\ \delta\rho_1 \\ \delta\phi_2 \\ \delta\rho_2 \end{bmatrix} = \begin{bmatrix} A_1 & 0 & \frac{g_{12}}{\hbar} \\ 0 & 0 & 0 \\ 0 & \frac{g_{12}}{\hbar} & A_2 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \delta\phi_1 \\ \delta\rho_1 \\ \delta\phi_2 \\ \delta\rho_2 \end{bmatrix}, \quad (11)$$

$$A_j = \begin{bmatrix} \mathbf{v}_j \cdot \nabla & \frac{g_j}{\hbar} \\ \nabla \cdot \left(\rho_{0j} \frac{\hbar}{m_j} \nabla \right) & \mathbf{v}_j \cdot \nabla \end{bmatrix}, \quad (12)$$

and in the singular region one obtains

$$\frac{\partial}{\partial t} \begin{bmatrix} \delta\phi_j \\ \delta\rho_j \end{bmatrix} = A_j \begin{bmatrix} \delta\phi_j \\ \delta\rho_j \end{bmatrix}. \quad (13)$$

Here $\mathbf{v}_j = \frac{\hbar}{m_j} \nabla \phi_{0j} - \Omega \times \mathbf{r}$ is the wave-function velocity in the rotating frame at position \mathbf{r} . ρ_{0j} is given by Eq. (5) in the overlapping region and Eq. (6) in the singular region.

As in the one-component case [20], we find that the eigenfunctions of the collective-mode equations [Eqs. (11)–(13)] are polynomials of the form $\delta\rho_j = \sum_{pqr} \beta_{jpqr} x^p y^q z^r$, $\delta\phi_j = \sum_{pqr} \gamma_{jpqr} x^p y^q z^r$, where β_{jpqr} and γ_{jpqr} are constants. The BEC is unstable when one of the eigenvalues has a positive real part, meaning that small perturbations about the static solutions grow exponentially.

As well as the above method, extra information can be obtained by investigating the stability of the overlapping region of each component separately. This is done by substituting Eq. (5) [instead of Eq. (6)] into Eq. (13). By doing so, one can see in which component and in which region an instability originates. This, however, neglects interspecies cross terms; it is equivalent to treating the interaction between components as a static potential. Interestingly, we find that this second method gives more accurate results than if cross terms are considered. We take this to be an indication that the collective-mode cross interactions are not well described within the TFA framework.

B. Different types of instabilities

Calculating the eigenvalues to Eq. (11) gives the regions of instability in the parameter space. Valuable information regarding the nature of the instability can also be gained by observing the corresponding eigenvectors. This allows the instabilities of a two-component BEC in a rotating trap to be divided into four different types based on the very different effects they have on the overall structure of the BEC. Simulations showing the effects of these instabilities in detail are given in the next section.

1. Classical c.m. instability

In its original static configuration, the density of BEC component j is a quadratic of the form (for simplicity of the argument, we ignore trap anisotropy and the distinction between the overlapping and singular regions) $\rho_j = \mu_j - x_j^2 - y_j^2 - z_j^2$. Consider the case where an eigenvalue λ corresponds to an eigenvector first order in a position coordinate, e.g., one of the form $\delta\rho_j = \Delta_x x_j$. This perturbation will have the effect of displacing the center of mass of the BEC along the x axis, i.e., $\rho + \delta\rho = (x_j + 0.5\Delta_x)^2 + y_j^2 + z_j^2 + \mu'_j$. If λ has a positive real part then this perturbation will grow in magnitude, displacing the center of mass of the BEC even further and hence causing a *c.m. instability*. We find that component 1 always has such an instability in the range

$\omega_1\sqrt{1-\epsilon_1} < \Omega < \omega_1\sqrt{1+\epsilon_1}$ regardless of the other parameters. This is in fact the same instability as experienced by a classical point particle in a rotating harmonic trap. It is caused by the rotation frequency coupling to the oscillation frequency and is also experienced by a one-component BEC [19]. In this case, it either causes the BEC to oscillate as a whole about the trap center or it can drive the BEC out of the trap [25]. In a two-component BEC, it can still occur provided there is little interaction between the components. This is discussed in more detail in Sec. III C.

2. Intraspecies c.m. instability

The above classical c.m. instability affects each component separately and independently of the interspecies interactions. We find another class of c.m. instability that occurs due to the interaction of the two components and can have a profoundly different effect on the BEC. They are again predicted by the instability of a perturbation first order in a position coordinate, but are differentiated from the first type in that they appear in the overlapping region of the condensate where both components are interacting. These *intraspecies c.m. instabilities* are due purely to interactions of the superfluid components and lead to instability in the c.m. of each component separately, but the total c.m. of the condensate remains stable. They result in interesting dynamics which are described in Sec. IV.

3. Ripple Instability

Perturbations of quadratic or higher in the position coordinates represent ripples through the phase and density profile of the BEC. If these perturbations are unstable, they directly disrupt the smooth quadratic profile. These *ripple instabilities* lead to turbulence and vortex nucleation.

4. Catastrophic Instability

In this case, the static solution that the BEC was following during adiabatic ramping ceases to exist. Perturbations of all orders are unstable and the BEC is torn apart in a spectacular fashion [24]. After the initial onset, the BEC becomes turbulent and, as in the ripple instability, vortices nucleate.

C. Results

Using Eq. (11), we present two examples (Figs. 3 and 4) of the instabilities predicted by the TFA and how they appear in different regions of the parameter space. We have used the second method described in Sec. III. On the same figures are plotted the point where the BEC becomes unstable in GPE simulations conducted for the same set of parameters. In general, the solutions and their stability can be evaluated for any ramping procedure, the only difference being that different ramping paths can access different α branches. In our GPE simulations, we fix Ω and then ramp $\epsilon_1 = \epsilon_2$ from 0. This allows us to investigate regions of the phase diagram that, for example, would not be accessible by ramping Ω for fixed ϵ . The point of instability is then determined from the simulations using the method presented in [25].

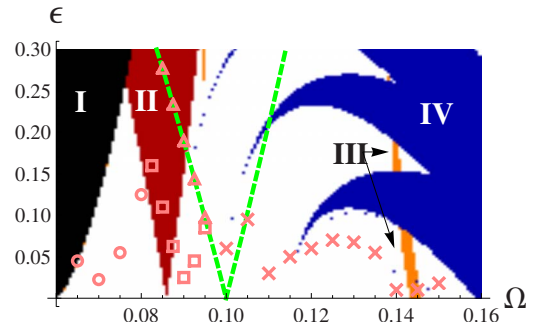


FIG. 3. (Color online) The instability regions within the parameter space for a system with $\hbar = \mu_1 = \mu_2 = 1$, $\omega_1 = 0.2$, $m_1 = 1$, $g_1 = 1$, $\omega_2 = 0.1$, $m_2 = 1.5$, $g_2 = 0.5$, $g_{12} = 0.1$, catastrophic instability (region I, black), intraspecies c.m. instability [region II, red (dark gray)], ripple instability in component 2 [region III, orange (light gray)], ripple instability in component 1 [region IV, blue (dark gray)], and classical c.m. instability in component 2 [green (light gray) dashed line]. Marks show the results for instabilities found using GPE simulations for catastrophic instabilities (circles), intraspecies c.m. instabilities (squares), classical c.m. instabilities (triangles), and ripple instabilities (crosses). Ω is in units of μ_1/\hbar .

The results of the simulations show how the TFA results can be used to predict BEC behavior. The methods derived above successfully pick up the different regions in the parameter space where different instabilities occur. Sometimes the results of the GPE simulations are exactly predicted in the TFA; at other times, the phenomenology is as predicted but its location numerically shifted in Ω by as much as 15%. As discussed above, the TFA is valid within the bulk of the condensate. The shifting is an indication that for the chosen parameters, the boundary of the BEC is affecting the particular instability that has been shifted.

For the case of repulsive interspecies interaction ($g_{12} > 0$), we find that the stability of the overlapping region of component 1 is highly dependent on its connection to the singular region [see, for example, the nonrotating case Fig. 1(III)]. The results using the TFA on the overlapping region of component 1 are only accurate when $g_{12} < 0$ and should not be used for $g_{12} > 0$.

Figure 3 shows the instabilities found on branch 2 of Fig. 2. A BEC on this branch can, depending on the parameters, experience either an intraspecies c.m., ripple, catastrophic, or classical c.m. instability. The actual position of the cata-

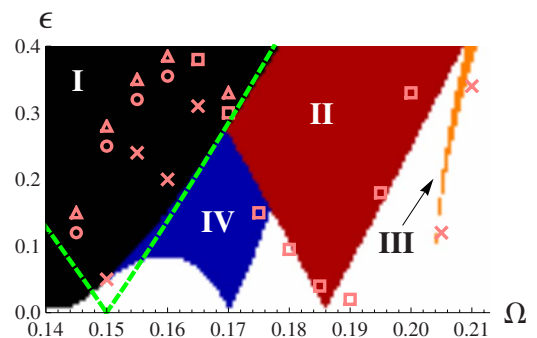


FIG. 4. (Color online) Same as Fig. 3 but with $\hbar = \mu_1 = \mu_2 = 1$, $\omega_1 = 0.1$, $m_1 = 1$, $g_1 = 0.5$, $\omega_2 = 0.15$, $m_2 = 1$, $g_2 = 1$, $g_{12} = -0.3$.

strophic instability is shifted to higher Ω from the TFA prediction by $\sim 10\%$ and the intraspecies c.m. instability is shifted to higher Ω by 5% . The green dashed line indicates the region where the classical c.m. instability would be for component 2 if the other component was not present.

Figure 4 focuses on the c.m. instability for a different system. This system has attractive interspecies interactions and equal masses but different trapping frequencies, which could correspond, for example, to two condensates of the same atomic species but different hyperfine states. The intraspecies c.m. instability and ripple instability in component 2 are exactly as predicted. The catastrophic instability is shifted to lower Ω from the predictions by 10% . The ripple instability in the singular region of component 1 is similar to, but much less influential than, the prediction. However this is not surprising because for attractive interspecies interactions, the two components are pulled tightly together and the singular region is almost nonexistent [see Fig. 1(I)].

The TFA predictions for both examples show that the interspecies interactions should halt the onset of the classical c.m. instabilities when both species are performing stable quadrupolar oscillation. Interestingly, the intraspecies c.m. instability pulls the two components apart leaving them once again susceptible to the classical c.m. instability. If this has occurred before reaching or whilst within the classical c.m. instability, the component in question will exit the trap as though the other components were not present. Likewise, the catastrophic instability causes both components to be wrenched apart. If one of the components is within a classical c.m. instability during the breakdown, it is free of the other component for long enough that it will exit the trap. This effect is clearly seen on Figs 3 and 4.

IV. SIMULATIONS

To compliment these Thomas-Fermi results, we have adapted two-dimensional (2D) truncated Wigner simulations [38] to the two-component case and investigated the instabilities predicted. Interesting results are attained for each different type of instability and these can be understood in terms of the TFA results. Also, the numerical methods allow us to extend the investigation to the immiscible phase where the TFA is no longer valid.

As well as the results shown in Figs. 3 and 4, we conduct simulations for parameters that correspond to an ^{87}Rb - ^{133}Cs system [39] and an ^{87}Rb - ^{85}Rb system [40]. These systems are of particular interest because the scattering lengths of ^{133}Cs and ^{85}Rb can be tuned via a Feshbach resonance [40,41]. This means that both the immiscible and miscible phases can be accessed experimentally. The ^{87}Rb - ^{85}Rb is also important because it satisfies the requirements for the creation of vortex sheets. The ^{87}Rb - ^{133}Cs system is used to simulate the creation of the other rotating states. For the ^{87}Rb - ^{133}Cs system, a_{12} is unknown. We, therefore, give examples of simulations conducted for a number of different choices of a_{12} .

The truncated Wigner method simulates quantum vacuum fluctuations by adding appropriate classical random fluctuations to the coherent field of the BECs initial state. In this

system, the fluctuations serve two purposes. Firstly, the fluctuations provide a seed of noise to break the BEC symmetry when the quadrupolar oscillation becomes unstable. Secondly, they enable incoherent-scattering processes to occur, by which condensate atoms are scattered into a thermal cloud. This method has been used to describe, for example, the formation of scattering halos in condensate collisions [42,43] and the suppression of Cherenkov radiation [44]. Hence the turbulent BEC can relax into a rotating eigenstate, such a vortex lattice, in contrast to the bare GPE which conserves energy and atom number.

In practice, the fluctuations are included as follows. The initial wave function for each species is obtained by solving the time-independent two-component GPE. These two wave functions are then expanded over a plane-wave basis, with a maximum cutoff wave vector to prevent Fourier aliasing. Quantum fluctuations are introduced into each wave function separately by adding random complex noise to each plane-wave mode. The amplitude of the quantum fluctuations has a Gaussian distribution, with an average value of half a particle [42]. For a thorough description of the method, see Refs. [38,43].

Results

Intraspecies c.m. instability

The TFA results show that as g_{12} is increased or decreased from 0, the classical c.m. instability of component 2 begins to shift and becomes an intraspecies c.m. instability. For $g_{12} < 0$, the simulations show that when this instability is reached, the c.m. of the entire BEC is stable; however, the c.m. of the individual components becomes unstable and the two components separate. The instability is caused purely by interspecies interactions, so as the components separate and interactions decrease, the trap pushes the two components back together again. The effect is that both components begin oscillating; eventually, the BEC settles down into a stable state with both components orbiting around one another [Fig. 5(a)]. This state is static in the rotating frame and implies a breaking of the 180° symmetry of the rotating-frame Hamiltonian.

For $g_{12} > 0$, component 2 sits within component 1. When the intraspecies c.m. instability in component 2 is reached, it is still trapped within component 1; it begins bouncing off the surrounding shell [Figs. 5(b) and 5(c)]. Eventually, the two components disrupt each other and settle down into a state that has component 2 still sitting within component 1, but with both components significantly diffused into one another. During these instabilities, no vortices are formed.

Classical c.m. instability

The classical c.m. instability can affect a TCBE if both components experience it at the same time (i.e., if $\omega_1 \approx \omega_2$). However, if only one component is in a regime of classical c.m. instability, then the TFA results predict, and simulations confirm, that this instability is suppressed during stable rotational motion. Nonetheless, as already discussed in Sec. III C, each component can still experience its classical c.m.

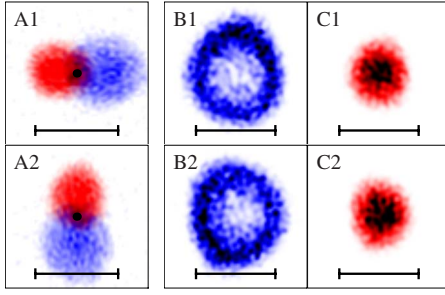


FIG. 5. (Color online) Plots of the density for BECs undergoing intraspecies c.m. instabilities for an ^{87}Rb [component 1, blue (panels B1 B2, right half of A1, and bottom half of A2)] - ^{133}Cs [component 2, red (panels C1 C2, left half of A1 and top half of A2)] system with $a_1=a_2=5.4$ nm and $\omega_1=\omega_2=3.15$ Hz. Attractive case ($g_{12}<0$): $a_{12}=-0.65$ nm, $\Omega=3.66$ Hz. (A2) is the density shortly after (A1) showing the two components rotating around each other. The black dot is the c.m. of the system. Repulsive case ($g_{12}>0$): $a_{12}=3.9$ nm, $\Omega=3.66$ Hz. (B1) and (C1) is the density shortly after (B2) and (C2) showing component 2 [(C1) and (C2)] bouncing off the shell of the enclosing component 1 [(B1) and (B2)]. The horizontal bars denote $40 \mu\text{m}$.

instability independently of the other component provided it is freed from the other component first via a catastrophic or intraspecies c.m. instability.

Another case where a classical c.m. instability can occur is near or in the immiscible phase where both components have a large singular region. In this case, component 2 forms a tightly packed ball within the shell of component 1. When component 2 reaches its classical c.m. instability, it builds up enough momentum to break through component 1 while component 1 remains stable. Component 2 then either exits the trap or begins to oscillate within the trapping potential. The result is similar to a wrecking ball as the highly dense component 2 smashes through the dilute component 1.

Catastrophic and ripple instabilities

In the miscible phase, the simulations show that when a ripple or catastrophic instability is reached, the BEC becomes turbulent and vortices enter. They then form an inter-

locking vortex lattice [Figs. 6(f) and 6(g)]. This state is of the same type as has been seen to form in experiments when a one-component BEC with a vortex lattice already present was split into two hyperfine components [13].

We also investigated the behavior of the rotational instabilities near to and within the immiscible phase. When g_{12} is close to but less than $\sqrt{g_1 g_2}$, component 1 forms an almost hollow shell around component 2 even though the immiscible phase has not been reached. As expected from the discussion at the end of Sec. II B, once the condensate is stirred and turbulence reached, the two components mix together and a vortex lattice is formed.

Once within the immiscible phase however, there is a discontinuous change in the behavior of a rotated BEC and, importantly, the two components do not mix. We find that once turbulence is induced, two different possible configurations with nontrivial phase topology form. The first is a vortex sheet which has been shown to be preferable thermodynamically in regions of parameter space where $g_1 \approx g_2$, $m_1 \approx m_2$, and $g_{12} > \sqrt{g_1 g_2}$ [12,15] [Figs. 6(h) and 6(i)]. In this configuration, the two components form separate domains of high density. We find that the parameters required for the dynamical formation of a vortex sheet matches that of the thermodynamic analysis provided an instability has been reached; without an instability, they do not form. These conditions for vortex sheet formation also coincide with the parameters required for a symmetry-broken initial state in the absence of rotation [37].

The second state we find is a giant vortex which has also been predicted thermodynamically [17,18]. We find that this state forms for any set of parameters that fall within the immiscible phase but do not match the requirements for the formation of vortex sheets. As with the vortex sheets, a ripple or catastrophic instability must first be induced in order for this state to form dynamically. The simulations show that once instability is reached, multiple vortices push their way through the outer shell of component one and into the low-density region in the middle of the trap where they congregate forming a giant vortex [Figs. 6(d) and 6(e)]. Normally, two overlapping vortices are predicted to be thermodynamically unstable [45]. However, in this system, the large density of component 2 attracts them to the center while the

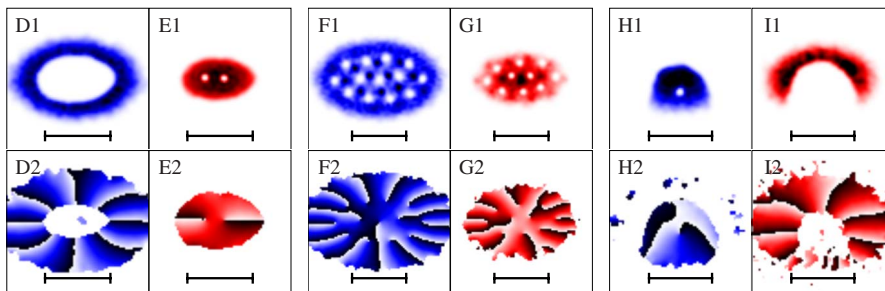


FIG. 6. (Color online) Results of 2D truncated Wigner simulations ending in vortex nucleation. Panels D–G show an ^{87}Rb (component 1) - ^{133}Cs (component 2) system with $a_1=a_2=5.4$ nm and $\omega_1=\omega_2=3.15$ Hz. [(D) and (E)] $a_{12}=7$ nm; [(F) and (G)] $a_{12}=3.3$ nm. Panels H and I show an ^{87}Rb (component 1) - ^{85}Rb (component 2) system with $a_1=5.24$ nm, $a_2=11.27$ nm, $a_{12}=11.3$ nm, and $\omega_1=\omega_2=3.15$ Hz. The horizontal bars denote $40 \mu\text{m}$. The number of atoms in each simulation is such that the peak density of ^{87}Rb is $4 \times 10^{18} \text{ m}^{-3}$ and both components have equal norms. D1, F1, and H1 (E1, G1, and I1) are the densities and D2, F2, and H2 (E2, G2, and I2) the phases of component 1 (2). The simulations are conducted by ramping ϵ while fixing Ω at 1.75 Hz.

outer shell of Rb holds them in. These results show how in practice such a state could be created and that this state is a product of the immiscibility of the two components.

In summary, the above results show that there is a direct connection between the state of the nonrotating TCBE and the state the rotating TCBE will settle down into after instability has been reached. That is, a miscible phase leads to a vortex lattice after rotating, a symmetry-broken state leads to vortex sheets, and an immiscible phase (other than the symmetry-broken state) leads to a giant vortex.

V. CONCLUSION

These results illustrate that BEC mixtures produce a rich variety of dynamical regimes that may be accessed by tuning

experimental parameters. We have examined the applicability of the TFA to a TCBE and extended it to the rotating case allowing us to find symmetry-breaking c.m. oscillations that are induced by interspecies interactions. In addition, the results give conditions under which interlocking vortex lattices, giant vortices, and vortex sheets will spontaneously form. The method allows all these phenomena to be understood and classified through particular instabilities occurring in different parts of the total condensate.

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