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Residual Energy Harvesting from Light Transients using Hematite as an Intrinsic Photocapacitor in a Symmetrical Cell

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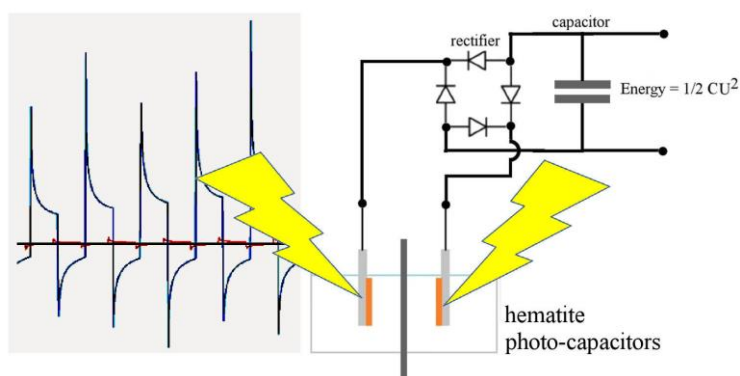
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ABSTRACT

Hematite as a sustainable photoabsorber material offers a band gap close to 2 eV and photoanode characteristics, but usually requires additional catalysts to enhance surface redox chemistry during *steady state* light energy harvesting for water splitting. Here, for a highly doped hematite film, sufficient intrinsic photo-capacitor behaviour is reported for the conversion of *light transients* into energy. Residual energy is harvested in a symmetric architecture with two opposing mesoporous hematite films on conductive glass. Transient light energy harvesting is shown to occur without the need for water splitting.

Ambient energy harvesting technologies have emerged for mechanical vibrations (based on piezo-electrics) and variations of temperature with time (based on pyro-electrics), as well as for static light energy.^{1,2} Often the harvesting mechanism is based on a cycle of high/low mechanical pressure or high/low temperature applied in an alternating fashion to create AC power output that is often rectified and stored in a capacitor. Similarly, for light energy harvesting a light-on/light-off cycle could be imagined. In nature, a similar principle of intermittent energy storage is realised in photosynthesis, which is based on a diurnal light-dark cycle with continuous energy production even during the night-time phase. The “dark process” relies on stored energy and operates out-of-phase to the “light process”. Recently, new artificial systems mimicking this behaviour have been proposed based on stored charge carriers or “photo-capacitance”; for example in photocatalytic hydrogen production.³

Photocapacitor behaviour was initially proposed and developed by Miyasaka^{4,5} which coupled a mesoporous titania photo-active film with a porous carbon capacitive layer. Materials for typical photocapacitors are mainly based on carbon,⁶ PANI,⁷ silicon,⁸ or pedot⁹ which are usually configured as a separate photo-active absorber layer and capacitor layer. A review in this area has appeared recently.¹⁰ However, it is rare for a capacitance to be directly integrated into the light absorber layer, although related bio-photocapacitor systems have been described recently.¹¹ In semiconductor electrodes, intrinsic photocapacitance is usually an unwanted component in solar cells as it can lead to “reversible charging” of traps as opposed to the “irreversible charging” required for flow of electricity and energy production. The irreversible surface chemical step of water oxidation links electrical ionic current flow and leads to internal rectification and energy harvesting. It is shown here that a reversible charging/ discharging effect induced by intrinsic photocapacitance in highly doped hematite in the presence of a transient/pulsed light source can also be used in energy harvesting when rectified externally (see Figure 1). Rules for this AC energy harvesting still need to emerge. However, similar approaches have been used in pyroelectric devices for harvesting residual heat since thermal cycling leads to reversible charging/discharging as a result of an increase and decrease of the polarisation of a material.¹²

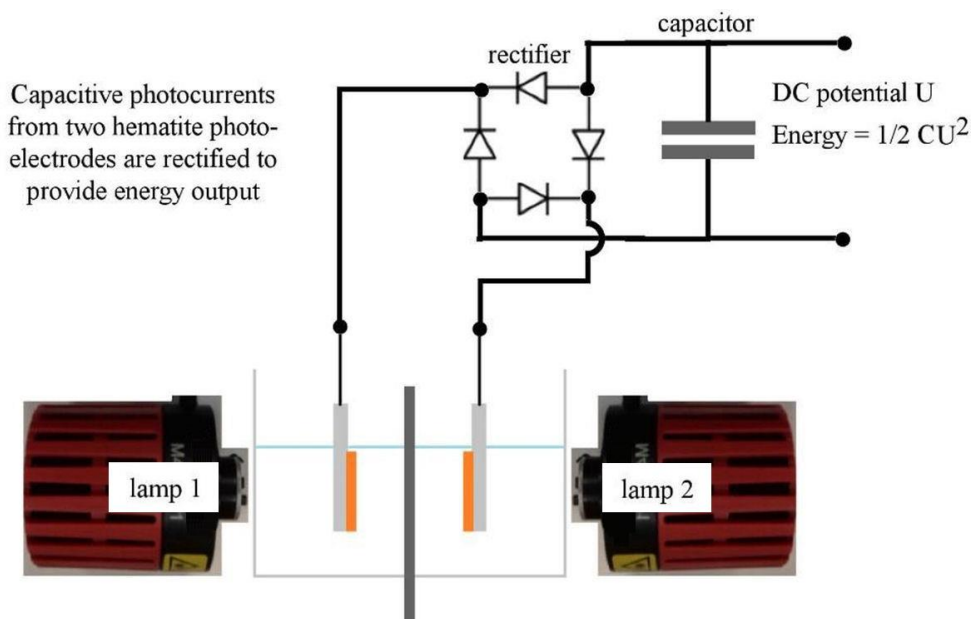


Figure 1. Schematic of a symmetric electrochemical cell with two hematite-coated FTO electrodes immersed in aqueous 0.1 M NaOH. Lamp 1 and lamp 2 apply synchronised on-off cycles so that one electrode is always illuminated and the other dark. An external rectifier converts the AC output to DC energy.

The net energy harvesting efficiency under “steady state” conditions could in principle be comparable to that under “transient” or cyclic conditions (given similar light absorption coefficients and recombinational losses), although very different parameters need to be optimised in the two approaches. The ability to store charges or “intrinsic photocapacitance” as well as the charging/ discharging time constant are crucial in the latter case. The switching frequency of the light source will therefore be of importance.

For hematite, the intrinsic capacitance (or redox pseudo-capacitance) response has been shown to be associated with surface states and exploited in light or potential modulated adsorption spectroscopy (LMAS or PMAS).¹³ Hematite has often been highlighted as an abundant and sustainable raw material with potential for

applications as a photoabsorber.^{14,15,16} Hematite offers a band gap of typically 2 eV with good characteristics as a photoanode for water splitting.^{17,18,19} Problems in performance are linked mainly to recombination of photo-generated charge carriers in the bulk and at surface states,²⁰ slow surface kinetics associated with the formation of oxygen,¹³ and poor electrical conductivity.^{21,22,23} In this study fluorine-doped tin oxide (FTO) electrodes were used as a substrate and hematite films prepared following the spin-coating methodology introduced by Souza et al.^{24‡} A notable modification to the preparation method here is a shorter calcination/annealing time to provide a more highly doped (and more capacitive) hematite product of semi-transparent reddish-brown coloration (see inset in Figure S1A). The cross-sectional image of a hematite spin-coated electrode after annealing is shown in Figure S1A. Top view images reveal only a very smooth layer (not shown). The cross-section of the sample shows a thin hematite layer of approximately 600 nm thickness on an equally thick FTO support. The hematite layer is composed of smaller nanoparticles of about 40 nm diameter. XRD data (Figure S1B) confirm the formation of hematite without any other iron oxide phases being identified. However, the crystallinity of samples was variable, with minor unidentified signals at 28.47° and 42.57°.

Characteristic Raman peaks for hematite (Figure S1C) are anticipated²⁵ at 225, 247, 293, 299, 412, 498, and 613 cm⁻¹. As shown in Figure S1C, only five main signals are present at 215, 243, 279, 401, 493, and 599 cm⁻¹. These signals demonstrate the presence of hematite, and the small shift in signals can be attributed to the use of a higher laser power.²¹ In addition, a strong peak at 1314 cm⁻¹ commonly encountered in hematite, is visible and may be associated with an artefact caused by antiferromagnetic behaviour of α -Fe₂O₃.²¹ Partially covered by this signal, a smaller

peak around 1100 cm^{-1} is visible. A broad signal at $2400\text{-}2600\text{ cm}^{-1}$ and a smaller bump at 814 cm^{-1} are also visible and possibly linked to the presence of FTO underneath the hematite layer. Some of these signals could be associated with the presence of residual carbon inclusions due to incomplete calcination of the carbon-rich precursor material. Carbon containing materials usually display a strong signal in the $1300\text{-}1350\text{ cm}^{-1}$ range for sp^3 hybridised carbon.²⁶ The colour of films and cut off wave length at 592 nm are consistent with hematite and a band gap of 2 eV .²¹

Voltammetry experiments were performed in aqueous 0.1 M NaOH initially in the absence of light which revealed the onset of a reduction at -0.2 V vs. SCE (see Figure 2A). Therefore, further experiments were initiated at -0.2 V vs. SCE . Next, linear sweep voltammograms were recorded in the presence of pulsed light, as shown in Figure 2B. Photocurrent density measurements were performed with back and with front illumination. Back illumination can be seen to produce considerably higher photocurrents. With back illumination, charge carriers are generated closer to the FTO-hematite interface, which facilitates their extraction into the FTO layer and thereby reduces the extent of transport/recombinational losses. In hematite films, light has a penetration depth of approximately 500 nm thickness.¹⁷ With an estimated thickness of 600 nm for these films, front illumination light may not penetrate deep enough for charge separation to be effectively collected at the interface. The transport layer for electrons, $\delta_{\text{transport}}$ (see inset Figure 2A), is likely to be only a fraction of the total thickness. The reaction layer, $\delta_{\text{reaction}} = (D_e/k_{\text{surface}})^{0.5}$, can be defined based on the electron diffusivity and the first order surface reaction for the water splitting process involving holes at the hematite surface. This is likely to be more extended in

the case of low surface reactivity, *i.e.* the process becomes transport limited and current spikes are observed.

Transient photocurrents for both back and front illumination show a characteristic light-on spike of anodic current, which is followed by a decay to give a steady state current density. When the light is switched off, a cathodic current spike is observed. The anodic spike arises from charge separation and rapid electron diffusion towards/into the FTO-hematite interface.^{27,28} The fast decay following the anodic spike is usually associated with slow oxygen evolution kinetics and the presence of surface traps (pseudo-capacitance). Trap concentrations can be enhanced due to defects on the surface or in the crystal structure often associated with a low degree of crystallinity and purity of the hematite film.^{23,29} When the light is turned off, the generation of mobile charges is interrupted and electrons flow back and undergo recombination with holes, which can occur by reduction of the previously oxidised surface traps. This process induces a cathodic light-off current spike.

Spin-coated electrodes were found to exhibit current spikes of typically 1.0 mA cm^{-2} and steady state currents of typically 0.5 mA cm^{-2} at 0.4 V vs SCE . Some variation in photocurrent between samples was observed, but the behaviour explained above was common to all samples. Even though the same procedure was applied for each spin-coated sample, these variations suggest that photo-activity is highly sensitive to layer composition and calcination conditions. More extended calcination resulted in less cathodic light-off current responses. Harvesting energy from the steady state water splitting response of the films in Figure 2B is inefficient because of extensive charging and slow oxygen evolution. Traditionally, a catalyst such as Co(II) has been

proposed as a way to improve performance. Figure 2C shows data for hematite films with Co(II) coated hematite following the procedure suggests by Zhong et al.³⁰ Much improved water splitting responses (higher steady state photo-anodic currents and less evidence for light-on/off transients) are observed in particular for back illumination.

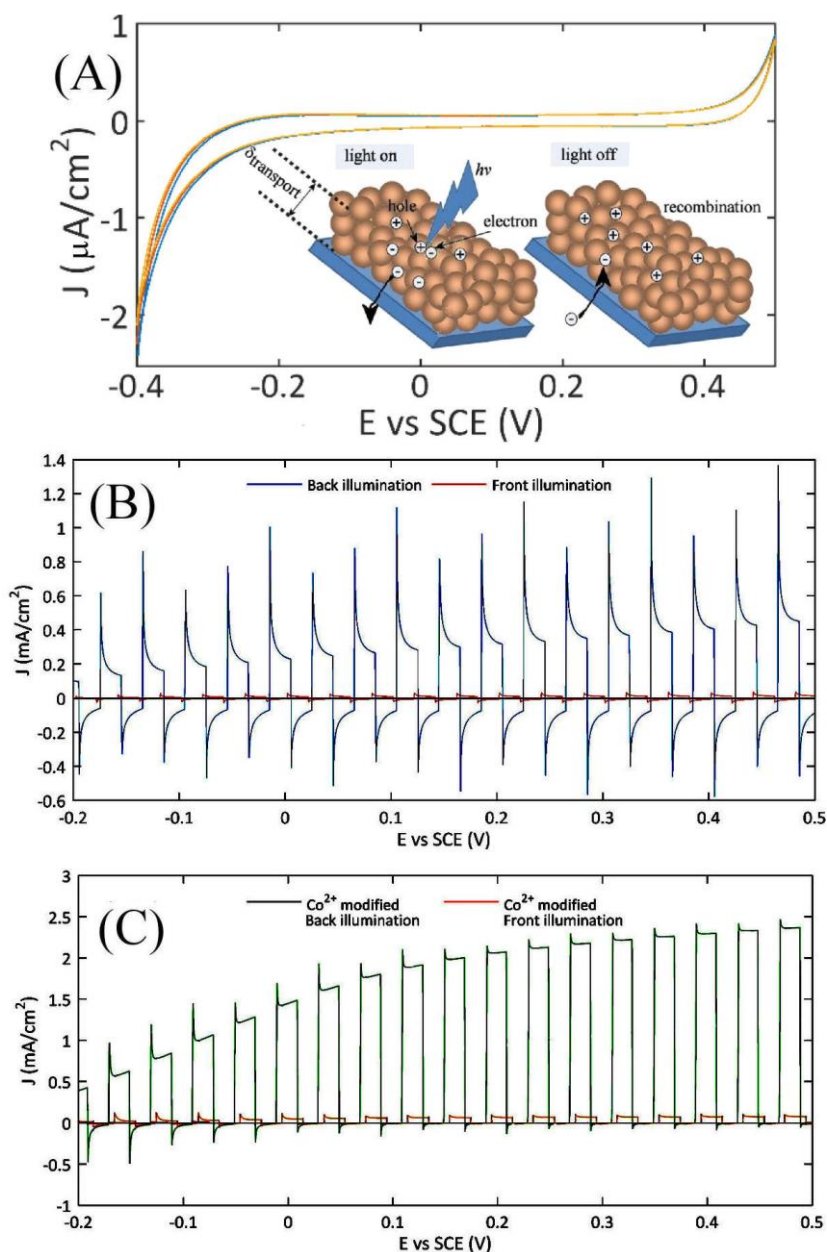


Figure 2. (A) Schematic of light-on and light-off processes in mesoporous hematite. Cyclic voltammograms (3 consecutive cycles, scan rate 20 mVs^{-1}) for hematite film immersed in 0.1 M NaOH . (B) Linear scan voltammogram (scan rate 20 mVs^{-1} ; pulsed LED light; 1 s on 1 s off pulses; irradiance ca. 100 mWcm^{-2}) for a hematite film immersed in aqueous 0.1 M NaOH . (C) As before, but with Co(II)-catalyst coated hematite.

The production of oxygen at the hematite surface by photocatalytic water splitting introduces irreversibility (rectification *via* semi-conductor interfaces and chemistry) to allow conversion of light energy into chemical energy. The transient or intrinsic photocapacitive behaviour of the hematite electrodes in Figure 2B is usually considered a drawback of photoanode materials due to the considerable drop in photocurrent as a result of charging of the semiconductor interface and extensive charge recombination in trap states. However, energy stored in this intrinsic capacitive charging process can be extracted by switching the light source on and off. The resulting AC current output can be rectified and accumulated/rectified in an external capacitor as shown in Figure 1. Instead of employing a single hematite photoanode with a second non-photoactive electrode, here two hematite electrodes are used in tandem with one light source being switched on simultaneous to the second being switched off. As a result the voltage between the two electrodes will change with time, as well as the charge state, to generate current.

Typical chronopotentiometry (zero current) for light-on and light-off transients for a single hematite electrode are shown in Figure 3A. Back illumination can be seen to result in more pronounced changes in potential with approximately 0.2 V voltage span between light-on and light-off conditions. When considering two coupled hematite electrodes, as shown in Figure 1, the complexity of resolving processes at individual hematite electrodes under these conditions is beyond the scope of this report. However, preliminary proof-of-principle data sets in Figure 3B demonstrate that the potential U (measured across an external capacitor) is increased when switching the

light sources at a 1 Hz frequency. A small external capacitor of 1 μF (see circuit in Figure 1) rapidly charges to approximately $U = 0.18 \text{ V}$ (corresponding to an energy of $\frac{1}{2}CU^2$) but then rapidly loses energy during the second part of the cycle. This is due to one of the two hematite electrodes being less effective, thereby leading to a modulation. The “potential ceiling” at 0.18 V (compare 0.2 V transients in Figure 3A) suggests that at this relative voltage the loss of charge at the semiconductor | electrolyte interface is increased so much (possibly due to oxygen evolution or reduction) that further charging is impossible. Water splitting chemistry at more positive potentials now may be considered an unwanted side reaction causing energy losses. In order to suppress the “voltage ceiling” effect, increasing the external capacitor value (C) to 100 μF or 470 μF is effective (see Figure 3B iv and v) since this leads to a lower voltage for a given charge (Q) level, since $Q=C \times U$. When compared to the experiment with the 1 μF capacitor, the 470 μF capacitor provides an approximately 200 fold increase in energy harvesting after 120 s.

Cuadras et al.³¹ provide an approximate analysis of the ceiling voltage U_{ceiling} based on the assumption of ideal diodes, Q the charge generated each cycle, Q_{leak} the charge leaked over a cycle (here mainly due to oxygen evolution), U_{diode} the voltage dropped across the diodes (here a very significant factor), and C_{photo} here the intrinsic photocapacitance (see equation 1).

$$U_{\text{ceiling}} = \frac{Q - Q_{\text{leak}} - 4U_{\text{diode}}C_{\text{photo}}}{2C_{\text{photo}}} \quad (1)$$

Clearly, the voltage U_{ceiling} is not dependent on the external capacitor (see Figure 3B), but the energy harvested is directly proportional to the external capacitor. The parameter Q_{leak} here is mainly associated with the charge transfer resistance for oxygen evolution and is crucial in limiting the voltage and limiting energy harvesting. The voltage U_{diode} as well as Q_{leak} should ideally be small so that ultimately $U_{\text{ceiling}} = Q/2C_{\text{photo}}$. Both are considerable in the work reported here and therefore further improvements are likely. The charge generated in the energy harvesting cycle should be high (compared to Q_{leak}). Other components to consider are the effects of frequency and wave shape. Any deviation from an ideal square waves will cause losses.

The frequency of light source switching offers a further parameter to optimise the energy harvesting process. High frequencies lead to energy losses due to an insufficient photovoltage being built up and low frequencies lead to losses due to more recombination and water splitting. The plots in Figure 3B can be interpreted as square root of energy *versus* time (with a fixed capacitance) and clearly lower frequencies are beneficial. Even lower frequencies (not shown) caused loss in performance and the optimum light switching frequency here was 0.1 Hz. The energy stored in 60 s reaches 3.3 μJ corresponding to 0.05 $\mu\text{W cm}^{-2}$ (or 0.5 μA at 0.1 V). This energy output seems low when compared to the light energy absorbed (assuming ca. 100 mWcm^{-2} LED intensity), but is comparable to output of other devices for residual energy harvesting³² and improvements will be possible. In particular surface blocking layers could be applied to the hematite surface to further suppress water splitting and to allow higher voltages to build up on the capacitor. Although water and particularly protons may be important in the photocapacitance effect, it may also be possible to operate similar devices under non-aqueous conditions. Furthermore,

better matching of applied frequency and internal photo-capacitance leakage resistance will be important. Also the stability of photocapacitance responses under light transient conditions for these hematite electrodes in aqueous 0.1 M NaOH appears limited and will need further attention.

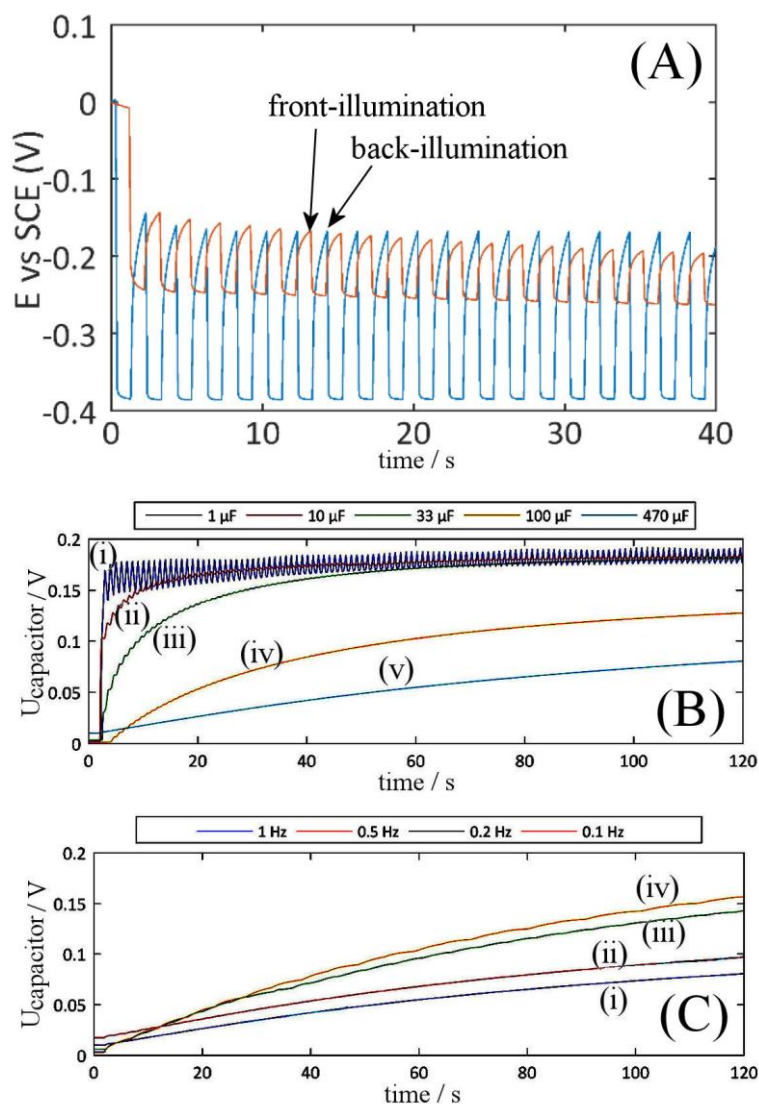


Figure 3. (A) Chronopotentiometry (zero current) for a hematite electrode in 0.1 M NaOH under front (orange) and back (blue) illumination conditions (irradiance ca. 100 mWcm^{-2}). (B) Capacitor charging potential (light switching frequency 1 Hz) as a function of time for external capacitance (i) 1, (ii) 10, (iii) 33, (iv) 100, and (v) 470 μF . (C) As before, but for 470 μF capacitance and (i) 1, (ii) 0.5, (iii) 0.2, (iv) 0.1 Hz light switching frequency.

In conclusion, highly doped pseudo-capacitive hematite thin film electrodes were successfully synthesised using a spin-coating deposition method adapted from Souza et al.²⁴ using the citric acid polymerisation approach. The resulting electrodes were semi-transparent and of a dark-red-orange colour and based on approximately 600 nm thick hematite. Doping-enhanced intrinsic photocapacitance was observed compared to that observed for more thoroughly calcined hematite. Transient photocurrent behaviour has been exploited with an external rectifier circuit to provide an example of an “AC solar cell” for residual energy harvesting. Energy loss mechanisms have been identified primarily based on the voltage drop in the diode rectifier circuit (to be dealt with in future by working at higher voltages) and due to residual water splitting activity (to be dealt with in future by improving hematite surface chemistry and by changing the electrolyte). The frequency for energy harvesting to maximise was shown in this case to be 0.1 Hz. This optimum frequency (or time constant) will need to be adjusted depending on application to diurnal (for solar light harvesting) or much faster to 50 Hz (for harvesting from artificial light sources). More work will also be required to explore/improve the principal limits of AC mode light harvesting devices compared to DC mode light harvesting cells.

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‡ For experimental information please see Electronic Supporting Information.

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