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4 ESTABLISHING STORM THRESHOLDS FOR THE SPANISH GULF OF CÁDIZ
5 COAST

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19

20 **Abstract**

21

22 In this study critical thresholds are defined for storm impacts along the Spanish coast of the
23 Gulf of Cádiz. The thresholds correspond to the minimum wave and tide conditions
24 necessary to produce significant morphological changes on beaches and dunes and/or
25 damage on coastal infrastructure or human occupation.

26 Threshold definition was performed by computing theoretical sea-level variations during
27 storms and comparing them with the topography of the study area and the location of
28 infrastructure at a local level. Specifically, the elevations of the berm, the dune foot and the
29 entrance of existing washovers were selected as threshold parameters. The total sea-level
30 variation generated by a storm event was estimated as the sum of the tidal level, the wind-
31 induced setup, the barometric setup and the wave-associated sea-level variation (wave setup
32 and runup), assuming a minimum interaction between the different processes. These
33 components were calculated on the basis of parameterisations for significant wave height
34 (H_s) obtained for the oceanographic and environmental conditions of the Gulf of Cadiz. For
35 this purpose real data and reanalysis time-series (HIPOCAS project) were used. Validation
36 of the obtained results was performed for a range of coastal settings over the study area. The
37 obtained thresholds for beach morphological changes in spring tide conditions range
38 between a significant wave height of 1.5 m and 3.7 m depending on beach characteristics,
39 while for dune foot erosion are around 3.3 to 3.7 m and for damage to infrastructure around
40 7.2 m. In case of neap tide conditions these values are increased on average by 50% over the
41 areas with large tidal range.

42 Furthermore, records of real damage in coastal infrastructure caused by storms were
43 collected at a regional level from newspapers and other bibliographic sources and compared
44 with the hydrodynamic conditions that caused the damage. These were extracted from the
45 hindcast database of the HIPOCAS project, including parameters such as storm duration,
46 mean and maximum wave height and wave direction. Results show that the duration of the
47 storm is not critical in determining the occurrence of coastal damage in the regional study
48 area. This way, the threshold would be defined as a duration ≥ 30 hours, with moderate
49 average wave height (≥ 3.3 m) and high maximum wave height (≥ 4.1 m) approaching from
50 the 3rd and 4th quadrants, during mean or spring tide situation.

51 The calculated thresholds constitute snapshots of risk conditions within a certain time
52 framework. Beach and nearshore zones are extremely dynamic, and also the characteristics
53 of occupation on the coast change over time, so critical storm thresholds will change
54 accordingly and therefore will need to be updated.

55

56

57 **Keywords**

58

59 Storm surge, HIPOCAS, threshold, wave runup, coastal erosion, Gulf of Cadiz

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64 **1. Introduction**

65

66 Storms constitute one of the most significant natural threats to coastal communities,
67 representing the world's foremost coastal natural hazard in terms of property damage and
68 lives lost (Murty, 1988). Storm events can cause coastal erosion, coastal flooding, damage to
69 infrastructure and other undesirable effects, thus creating the need for scientific tools, such
70 as vulnerability maps, predictive techniques or warning systems, that can help to prevent
71 these negative consequences. The development of such tools requires an adequate
72 understanding of both the hydrodynamic processes acting during a storm, and the coastal
73 response to this hydrodynamic forcing.

74 In general terms the impact of storms on the coast is determined by the cumulative effect of
75 large-, meso- and local-scale processes. Barotropic forcing is the main large-scale process
76 affecting short-term sea-level variations. The spatial distribution of atmospheric pressure
77 during a storm can lead to sea-level temporal changes on the coastline (inverse barometer
78 effect). Meso-scale processes are governed by the action of the onshore winds piling up
79 water on the coast (wind setup). The magnitude of this setup is largely affected by the
80 bathymetric characteristics of the continental shelf, such as average slope, width and depth.
81 Furthermore, the generation and growth of the waves (large-scale) and wave transformation
82 processes over the inner continental shelf (meso-scale) are also affected by the above
83 parameters. Finally, closer to the shore (local-scale) the action of wave breaking and the
84 swash processes produce an upwards and subsequently landwards displacement of the sea
85 level (Masselink and Hughes, 2003).

86 The joint action of all the aforementioned processes produce an increase in water levels on
87 the shore, which shift wave attack higher on the beach profile, thus facilitating wave runup
88 to reach areas further inland than fair weather waves (Stockdon et al., 2007). This can result

89 in overtopping of dune ridges and coastal defences, dune breaching, overwashing and other
90 types of coastal damage. The storm surge adds to the astronomical tide to generate the storm
91 tide, so under certain circumstances the combination of storm surge and spring tides (Pye
92 and Blott, 2008) can have devastating consequences on coastal lowlands.

93 The potential severity of the consequences of storms has led to a considerable effort by
94 coastal scientists in understanding and predicting storm impacts at different temporal and
95 spatial scales. One of the approaches used by several authors is the modelling and
96 calculation of storm surge components and the comparison with coastal topography, in order
97 to determine the effects on the coast of different types of storm events. For instance,
98 Sallenger (2000) established a model defining four storm-impact regimes (swash, collision,
99 overwash and inundation) on barrier islands based on the relative relationships between the
100 elevation of coastal features and that of storm-induced water levels. Benavente et al. (2006)
101 used the computation of storm surge components added upon tidal height for determining
102 flooding regime in a low-lying coastal zone in cases of modal and extreme storms. Storm-
103 induced inundation was also studied by Jiménez et al. (2009) in microtidal coasts, where
104 they defined it by calculating wave runup at the peak of the storm. These procedures allow
105 the construction of vulnerability maps that help determining the coastal zones at risk of
106 experiencing storm-induced damage.

107 However, none of these authors focused on the possibility of defining the minimum
108 hydrodynamic conditions necessary to produce a certain type of effect on the coast, as well
109 as estimating the possible effects by using only the offshore wave height and tide level.

110 These conditions constitute the critical storm thresholds, which can be defined for storm
111 impacts such as beach erosion, dune recession or damage to infrastructure located on the
112 backbeach. Threshold definition is an important issue regarding prevention of the negative
113 consequences of storms, as it represents the first step in the development of accurate

114 predictions of storm impacts. This facilitates the implementation of both strategic and
115 operational measures for an adequate coastal planning and management aimed at risk
116 prevention, such as risk mapping, development of warning systems and so on.
117 In this paper an approach is performed on establishing a methodology for the definition of
118 critical thresholds for storm impacts on the Spanish coast of the Gulf of Cádiz. The historical
119 distribution of storms in this area has been studied by Rodríguez-Ramírez et al. (2003), and
120 several authors have worked on storm effects on this coast (e.g. Ballesta et al., 1998; Reyes
121 et al., 1999; Benavente et al., 2002, 2006), but no previous work has been done regarding
122 storm thresholds. In this work two types of storm effects were investigated: the generation of
123 significant morphological changes on beaches and dunes, such as berm erosion, dune foot
124 erosion or washover occurrence, and the generation of damage on coastal infrastructure or
125 human occupation. In both cases the thresholds correspond to the minimum wave and tide
126 conditions necessary to produce the aforementioned effects. For this purpose two
127 complementary approaches were used: the computation of theoretical water levels for
128 different storm conditions, and the collection of newspaper data on the consequences of past
129 storms. The method is developed for the regional coastline of the Gulf of Cádiz (SW Spain)
130 and tested for a variety of local settings along the study area.

131

132 **2. Study area**

133

134 2.1. The Gulf of Cádiz

135

136 The Gulf of Cádiz is located on the Southwestern coast of the Iberian Peninsula, facing the
137 Atlantic Ocean and surrounded by the Spanish, Portuguese and Moroccan shores. The
138 Spanish part of the Gulf extends along 280 km between the Spain-Portugal border and the

139 Strait of Gibraltar, and it can be divided into two main sectors: the coast of Huelva province
140 (to the West) and the coast of Cádiz province (to the East) (Fig. 1).

141

142 ***APPROXIMATE LOCATION OF FIGURE 1***

143

144 Huelva coast shows a regular W-E to WNW-ESE orientation. It is located in the
145 Guadalquivir Neogene Depression, which is formed by postorogenic sub-horizontal
146 sedimentary materials. As a consequence, coastal landscapes are mainly low-lying areas
147 including linear sandy beaches, low sandy cliffs and well-developed sandspits, such as El
148 Rompido and Doñana, enclosing marshland areas. These have been generated by a strong
149 longshore drift directed towards the East. The coast is fed by several important water
150 courses, mainly the Guadiana and Guadalquivir rivers, where dam construction in the last
151 decades has greatly decreased sediment supply to the coast (Rodríguez-Ramírez et al., 2003).

152 Cádiz coastline shows a general NNW-SSE orientation, interrupted by short W-E traits
153 related to recent faults (Fig. 1). From the geomorphological point of view two sectors can be
154 differentiated, located North and South of Cape Trafalgar respectively. The Northern sector
155 belongs to the end of the Guadalquivir Depression and as such is composed of the
156 aforementioned soft, sub-horizontal Neogene materials, giving rise to a generally linear, low-
157 lying coast with several wide embayments. Significant rivers such as Guadalquivir and
158 Guadalete flow into this area, the extensive damming of their basins having also caused an
159 important decrease in sediment supply to the coast (Plomaritis et al., 2009a). The Southern
160 sector belongs to the Betic Ranges, showing higher relief areas on Paleogene and Neogene
161 detritic and calcareous materials that were faulted and folded by the Alpine Orogeny. As a
162 consequence, it is characterized by a young, indented coastline, with alternating cliffs and
163 pocket beaches controlled by numerous neotectonic features.

164 Regarding the hydrodynamic regime, tides in most part of the Gulf of Cádiz are of mesotidal
165 semi-diurnal type, with tidal range strongly decreasing from Cape Trafalgar eastwards. Mean
166 spring tidal range (MSTR) is 3.06 m in Huelva, 2.96 m in Cádiz, 2.30 m in Barbate and 1.22
167 m in Tarifa (Fig. 1) (Instituto Hidrográfico de la Marina, 2009), so the area around the Strait
168 of Gibraltar can be considered a microtidal environment according to Davies' (1964)
169 classification. Theoretical maximum tidal range in the Gulf of Cádiz during equinoctial
170 spring tides would reach 3.74 m with a coefficient of 120, but wind and atmospheric
171 pressure during storms may add up to 50 cm to the astronomic high tide in the case of severe
172 storms (Marcos et al., 2009).

173 Both sea and swell waves generally approach the coast from the W and SW, giving rise to a
174 prevailing longshore current towards the E and SE (Fig. 2). Changes in shoreline orientation
175 along the Gulf of Cádiz make the angle of wave approach progressively diminish towards
176 the Strait of Gibraltar, rendering longshore drift much weaker in this area. Average wave
177 height is less than 1 m, with waves over 1.5 m being considered storm waves by the Ministry
178 of Public Works both in Cádiz and Huelva coasts (Benavente et al., 2000). Therefore, the
179 study area can be classified as a low-energy coast according to Tanner (1960) and Hegge et
180 al. (1996), with Huelva coast generally showing slightly lower wave energy than Cádiz coast
181 (MOPT, 1992). The winter storm period spans between November and March, when storm
182 wave heights commonly exceed 4 m, with the 20-year significant wave height being 7.3 m
183 (Puertos del Estado, 2006).

184

185 ***APPROXIMATE LOCATION OF FIGURE 2***

186

187 2.2. The test sites

188

189 Two test sites (Bota and Cortadura-Camposoto) were chosen, located on the western and
190 central Gulf of Cádiz respectively (Fig. 1). The first test site, Bota beach, is located close to
191 Punta Umbría village in the western part of the Huelva Ria. It is a linear, sandy beach
192 extending along 4 km between the villages of El Portil and Punta Umbría. It is a natural
193 beach backed by a foredune and non-vegetated dunes (Fig. 3A). A shore-parallel road runs
194 along the back of the foredune, producing very high human pressure during the summer
195 season. The road affects only the northern sector of the beach, as in the southern sector it is
196 located further inland. This allows a better development of the foredune in the southern area.
197 The beach is composed of fine to medium quartz-rich sands, and it shows a clearly seasonal
198 behaviour, with a dissipative profile during the winter months and an intermediate
199 morphology during fair weather conditions. Between both states, flat bars occasionally
200 appear on the foreshore.

201 The second test site, Cortadura-Camposoto, is located around Cádiz city, in the southern part
202 of the Bay of Cádiz (Fig. 1). It includes two different sandy beaches (Cortadura to the North
203 and Camposoto to the South) extending along 10 km, providing the opportunity for studying
204 the effects of storms on two different, nearby types of environments. Bathymetric contours
205 in both sites are broadly parallel to the coastline and the nearshore zone shows a generally
206 gentle slope, interrupted by several shoreline-parallel rocky outcrops. In detail, Cortadura is
207 an urban beach located in Cádiz city, backed by a seafront on its major part and, on its
208 southernmost sector, by foredunes and a low, mostly non-vegetated dune ridge artificially
209 stabilised by fences (Fig. 3B). It shows an intermediate-dissipative profile composed by
210 medium to fine quartz-rich sands, where wide, flat bars are often observed on the foreshore
211 (Plomaritis et al., 2009b). On the other hand, Camposoto is a natural beach backed by low
212 dune ridges and salt marshes, and belonging to the Bay of Cádiz Natural Park. The dunes are
213 vegetated and show several washover fans of different types and forms. A road and several

214 car parks are located between the dunes and the salt marshes, connected to the beach by
215 wooden pathways (Fig. 3C). The beach is composed of medium sand, showing an
216 intermediate-dissipative, highly seasonal profile (Plomaritis et al., 2009b).

217

218 ***APPROXIMATE LOCATION OF FIGURE 3***

219

220 **3. Methods**

221

222 Human occupation along the Gulf of Cádiz coast can be affected by storm events in two
223 ways. First, by causing direct storm-related damage to human infrastructure, such as
224 seawalls, drainage systems, beach access structures and so on, with the associated economic
225 losses. And second, by producing morphological changes such as long-term reduction in
226 beach width or damage to dune ridges, leading to investments in measures like beach
227 replenishment or dune protection. Therefore, both types of thresholds were considered in this
228 work.

229 Two complementary approaches were adopted for the definition of the aforementioned
230 thresholds. On one hand, theoretical storm-induced sea-level variations were calculated and
231 compared with the topography of the test sites at a local level (Sallenger, 2000). On the other
232 hand, newspaper records of real damage in coastal infrastructure caused by storms were
233 collected at a regional level and compared with the hydrodynamic conditions that caused the
234 damage.

235

236 3.1. Computation of theoretical sea-level variation

237

238 The most common effect of storms in the Gulf of Cádiz beaches is the generation of
239 morphological changes such as beach flattening, erosive escarpments on the beachface,
240 formation or reactivation of washover deposits and dune erosion (Benavente et al., 2002). A
241 major issue in the generation of these effects is sea level during the storm reaching coastal
242 features such as the berm or the dune foot. For this reason, the comparison between coastal
243 topography and storm-induced water level was used in order to calculate minimum wave and
244 tide conditions needed to produce morphological changes. The same rationale was applied
245 for calculating the threshold for damage to coastal infrastructure, by using the elevation of
246 the infrastructure on each case.

247 This way, four different types of threshold were investigated on the test sites according to the
248 characteristics of each location: (a) morphological change in all beaches, mainly berm
249 erosion, (b) dune erosion in all beaches, (c) overwash in Camposoto beach, and (d) damage
250 to infrastructure in Cortadura beach. For each case the elevation of (a) the berm, (b) the dune
251 foot, (c) the entrance of existing washovers and (d) the base of the seawall were respectively
252 selected as threshold parameters. The elevations were average summer values derived from
253 topographic surveys carried out in the test sites by DGPS and total station, that were
254 averaged along 300 m long stretches of coast on each site.

255 The total sea level variation (TSLV) generated by a storm event was estimated following the
256 procedure by Benavente et al. (2006) as the sum of the forcing agents involved in the storm:

257

$$258 \quad \text{TSLV} = \text{TL} + \text{WiS} + \text{BaS} + \text{WaR} \quad (1)$$

259

260 where TL is the tidal level, WiS is the wind-induced setup, BaS is the barometric setup and
261 WaR is the wave-associated sea level variation, which is composed by the wave set up and
262 the vertical swash excursion.

263 For obtaining the tidal level (TL) values, the mean high water springs (MHWS) and the
264 mean high water neaps (MHWN) levels in Huelva and Cádiz coasts were extracted from tide
265 gauge data-series (Instituto Hidrográfico de la Marina, 2009), being around 3.3 m and 2.5 m
266 above the hydrographic zero, respectively.

267 The coastal sea-level variation generated by the combination of wind-induced surge (WiS)
268 and barometric setup (BaS) was estimated based on a correlation between this surge and
269 offshore wave properties in the study area. The meteorological setting in the Gulf of Cádiz
270 favours such a correlation, since the predominant atmospheric and oceanographic conditions
271 that result in surge generation and storm wave heights are the same. The aim was to compute
272 an easy-to-use threshold based only on tide conditions and wave height, instead of a complex
273 expression where four variables (tide, wind, waves and atmospheric pressure) had to be
274 combined in a joint-probability approach. For this purpose the sea-level residual extracted
275 from the tide gauge time series in Mazagón harbour (Huelva) was used as a surge indicator,
276 while Gulf of Cádiz offshore wave buoy (Fig. 1) provided the wave parameters time series.
277 Both datasets overlap over a period of 12 years between 1996 and 2008, being the longest
278 time series available in the Gulf of Cádiz.

279 A peak over threshold (POT) analysis was undertaken over the 12 years in order to extract
280 statistically independent data of wave height and surge level on the coast during storms
281 (Kamphuis, 2000). For the above analysis only the storm season events (October to March)
282 with $H_s \geq 2.5$ m were used (with H_s calculated for offshore conditions). In order to avoid
283 data of momentary storm events that cannot produce a significant surge, a storm duration
284 restriction of at least 12 hours was used. Furthermore, consecutive storm events with calm
285 conditions of less than 24 hours between them were considered as a single storm group
286 event. For the above conditions a total of 204 events were extracted and used to build the

287 correlation. The logarithmic trend was fitted giving the following equation with a value of r^2
288 = 0.61 (Fig. 4).

289

$$290 \quad S = 41.45 \ln (H_0) - 36.16 \quad (2)$$

291

292 where S is the surge height, considered to be the combination of WiS and BaS, and H_0 is the
293 offshore significant wave height. To demonstrate the applicability of the above correlation
294 over the Gulf of Cádiz the data of sea-level residual from the tide gauge in Cádiz harbour
295 (years 2008-2010) are also presented on Figure 4. It has to be noted that the majority of the
296 events used for fitting Equation 2 correspond to storm events coming from westerly
297 directions. The secondary wave direction (SE) that is shown in Figure 2 does not involve
298 surge generation in the study area, as easterly winds and waves occur during conditions of
299 high atmospheric pressure (so barometric setup is not generated), easterly winds are roughly
300 parallel to the coastline (so they do not induce any significant wind setup) and the
301 corresponding wave fetch is very short.

302

303 ***APPROXIMATE LOCATION OF FIGURE 4***

304

305 Finally, the most critical factor in determining storm thresholds in coastal areas is wave-
306 associated sea-level variation (WaR) (Sallenger, 2000). Several formulations were tested for
307 runup calculation in the study area, including those by Holman (1986), Ruessink et al.
308 (1998) and Stockdon et al. (2006). Due to the characteristics of beach slope and wave
309 steepness in the test sites and following the proposal by Benavente et al. (2006), the
310 expression by Komar (1998), modified from an initial equation by Holman (1986), was
311 selected for runup calculation:

312

$$313 \quad WaR = 0.36 g^{0.5} H_0^{0.5} T \tan\beta \quad (3)$$

314

315 where H_0 represents significant deep-water wave height, T is deep-water wave period, $\tan\beta$

316 is average beach slope and g is gravity. Wave data were computed on the basis of the

317 extreme regime relationship of H_0 and T_p (spectral peak period) established for the Cádiz

318 wave buoy by the National Ports Authority (Puertos del Estado, 2006):

319

$$320 \quad T_p = 4.95 H_0^{0.49} \quad (4)$$

321

322 Deep-water significant wave height (H_0) was then estimated using reverse shoaling and

323 assuming linear wave theory. Beach slopes were averaged from topographic profiles

324 performed at the test sites by DGPS and total station. Average winter slopes in Bota,

325 Cortadura and Camposoto were 0.029, 0.017 and 0.024 respectively, while average summer

326 slopes were 0.065, 0.025 and 0.044 respectively.

327 Finally, an important issue regarding the threshold for morphological change is the existence

328 of erosive wave conditions for berm erosion to occur. The height of the berm crest is

329 governed, according to Takeda and Sunamura (1982), by offshore wave periods and wave

330 breaking height (H_b). Hence, beach slope over intermediate and shallow water as well as the

331 distance of the breaker zone and the slope of the surf zone can play a role in the final height

332 of the berm crest. In general terms both berm formation and berm erosion require

333 overtopping of the berm crest by waves (Masselink and Hughes, 2003; Weir et al., 2006).

334 Hence, for the case of the morphological threshold two conditions have to be met, namely

335 the total sea-level variation (TSLV) to reach the height of the berm crest and erosive wave

336 conditions to exist in order to shift from a berm-type to a bar-type profile. The most common

337 erosion predictor is the Dean number (1973) (Ω), also known as the dimensionless fall
338 velocity number:

339

$$340 \quad \Omega = H_0/(w_s T) \quad (5)$$

341

342 where H_0 is the offshore wave height, w_s is the sediment fall velocity calculated using the
343 Soulsby formula for natural grains (Soulsby, 1997) and T is the wave period. The critical
344 value between accretion and erosion condition proposed by Dean (1973) was 1 and it was
345 based on small scale experiments, while larger scale experiments suggested a value between
346 2 and 2.5 (Masselink and Hughes, 2003). However, in recent large scale experiments by
347 Roberts et al. (2010), they used an erosive Dean criterion of 5 for their experimental
348 conditions. In the present work the methodology of Kraus et al. (1991) was used to
349 determine the Dean number criterion for erosive conditions. In this approach the Dean
350 number is plotted against the wave steepness H_0/L_0 , where L_0 is deep-water wavelength
351 computed by the linear wave theory (Dean and Dalrymple, 1991). The conditions for very
352 likely erosion are estimated as $H_0/L_0=0.00014\Omega^3$.

353

354 3.2. Newspaper data collection

355

356 Another approach at a wider spatial scale was adopted for the definition of a critical storm
357 threshold for damage to infrastructures or human occupation not only in the test sites, but
358 along the whole Spanish coast of the Gulf of Cádiz. The method consisted in comparing
359 recorded evidence of real damage with the hydrodynamic conditions that caused it.
360 Storminess and damage reconstruction from historical records in the Atlantic region has been
361 attempted before with good results (Andrade et al., 2008).

362 The damage generated by historical storms having occurred in the study area was derived
363 from an extensive bibliographic search, in which the main source of information were local
364 newspapers from Cádiz and Huelva provinces spanning the period between 1945 and 2005.
365 The events recorded in Huelva province were cross-checked with the information about
366 storm periods in Rodríguez-Ramírez et al. (2003). The hydrodynamic forcing causing the
367 damage was extracted from the SIMAR-44 dataset of the HIPOCAS project (HIIndcast of
368 dynamic Processes of the Ocean and Coastal Areas of Europe). These data stem from high-
369 resolution numerical modelling and provide 3-hour wind, sea-level (meteorological residual)
370 and wave data spanning the period between 1958 and 2001 (Guedes-Soares et al., 2002). For
371 this work the database was analysed for the grid points (nodes) located closest to Cádiz and
372 Huelva cities, and the data were filtered in order to consider only storm data, i.e. those
373 corresponding to winter months, with wave approach directions from the 3rd and 4th
374 quadrants, and Hs over 2 m. For each storm event having caused reported damage, storm
375 duration, mean and maximum wave height, wave direction and wind speed were extracted
376 from the HIPOCAS database, and tidal height information was derived from t-tide
377 (Pawlowicz et al., 2002) by using the full tidal constituents of Cádiz port. The differences in
378 tidal characteristics between Cádiz and Mazagón are on average less than 10 cm in range and
379 less than 5 minutes in time. The combined analysis of both elements (damage and
380 hydrodynamic parameters) allowed the identification of a minimum threshold of wave and
381 tide conditions having caused real damage to structures in the past.

382 It is important to note that the wave heights used in the analysis were obtained from the
383 HIPOCAS nodes, and then they were corrected according to the relationship between a two-
384 year period of real data recorded by wave buoys in the area and HIPOCAS modelled data for
385 the same period (Del Río et al., 2009). The expression used was:

386

387 $H_{co} = -0.12 + (1.554 H_{hi}^{0.822})$ (6)

388

389 where H_{co} is the corrected wave height and H_{hi} is the wave height extracted from the
390 HIPOCAS database.

391 Several considerations must be made regarding this method. On one hand, only coastal
392 damage related to Atlantic storms (i.e. wind and waves approaching from the 3rd and 4th
393 quadrants) was taken into consideration, as longer fetch in these directions is responsible for
394 generating high waves and surge (Rodríguez-Ramírez et al., 2003). Therefore, reported
395 damage caused by strong Easterly winds that blow under conditions of high atmospheric
396 pressure was not included, as these events do not generate high waves or storm surge due to
397 the short fetch in this direction and the high-pressure conditions. It must also be pointed out
398 that the methodology implies considering only those events for which there is a written
399 record of their destructive effects on coastal infrastructure due to high waves or storm surge.
400 Therefore, reports of damage by wind or flooding by rainfall caused by winter storms on
401 inland areas of coastal cities were not taken into account, nor have shipwrecks or other
402 incidents not directly involving damage to coastal infrastructure.

403

404 **4. Results**

405

406 4.1. Thresholds in the local-scale approach

407

408 The elevations above the hydrographic zero of the features related to the aforementioned
409 storm effects (morphological change, overwash, dune erosion and damage to infrastructure)
410 are presented in Table 1 for the corresponding test sites.

411

412 ***APPROXIMATE LOCATION OF TABLE 1***

413

414 Based on equations (1) to (4) the total storm-induced sea-level variation (TSLV) was
415 calculated for each test site, considering spring high tides in a worst-case approach, and it
416 was compared with the elevations in Table 1. The values of significant wave height needed
417 to reach the corresponding TSLV and therefore the critical threshold for each type of process
418 are shown in Table 2. The exact minimum wave height conditions for each threshold were
419 calculated by linear interpolation based on the results of equations (1) to (5) and the
420 elevations in Table 1.

421

422 ***APPROXIMATE LOCATION OF TABLE 2***

423

424 The thresholds for beach morphological changes, considered as berm erosion, were found to
425 be 3.75 m, 2 m and 1 m of significant wave height for Cortadura, Bota and Camposoto
426 beaches respectively. The reason for the difference between two points as close to each other
427 as Cortadura and Camposoto is mainly related to the heights of the berm crest, which is 0.5
428 m higher in Cortadura. This variation can be attributed to different transformation of the
429 waves along the nearshore area, related to the submerged rocky outcrops, which could give
430 rise to slightly different infragravity waves under mild accretionary conditions, resulting in a
431 different berm height. Besides, beach slope is significantly gentler in Cortadura, thus
432 creating very low wave runup values. The test of Dean's erosive conditions according to the
433 method by Kraus et al. (1991) resulted in a slight change in the threshold for Camposoto,
434 which would be 1.5 m of significant wave height.

435 It has to be noted that the majority of experiments undertaken for the evaluation of beach
436 erosion criteria have used equilibrium beach profiles as initial conditions. Hence, for

437 ultradissipative profiles composed of fine sands the Dean number generally produces high
438 values and consequently overestimates the erosive conditions. The introduction of beach
439 slope in the evaluation of erosion/accretion conditions as in the case of Hattori and
440 Kawamata (1980) significantly improves the estimation for the latter beach case. This way,
441 according to this procedure all wave heights above 2 m correspond to erosive conditions in
442 the test sites.

443 As for dune erosion, the threshold was found to be at a significant wave height of 3.33 m in
444 Bota beach and 3.75 m in Camposoto beach. This can be related to steeper slopes in the
445 former giving rise to higher runup values, so that wave thresholds are lower even if the
446 elevation of the dune foot is higher than in Camposoto beach. On the other hand, it must be
447 noted that the lowest limit for the occurrence of overwash in Camposoto beach is at a
448 significant wave height of 2.57 m, which was found in the Northern sector of the study site
449 and corresponds to the reactivation of an existing washover. This limit is lower than the
450 threshold for dune foot erosion, due to the local morphology of the beach in the mouth of the
451 existing washover area, which is characterised by a topographic depression. The Dean
452 erosive conditions were also tested here, but due to the increased wave height and surge
453 needed for the TSLV to reach the dune foot this always occurs under erosive conditions.
454 Finally, the threshold for potential structural damage in Cortadura beach was found to be at a
455 significant wave height of 7.19 m. It is clear that the fact of water level reaching the base of
456 the seawall during a storm does not imply that the structure will collapse, but it certainly
457 involves other types of damage such as the flooding of beach facilities located at the base of
458 the seafront. In any case, it must be noted that these thresholds represent minimum values
459 from which there can be negative consequences.

460 It must be stressed that all these values correspond to spring tide conditions; in the case of
461 storms arriving on a neap tide the threshold values would be increased on average by a factor
462 of 50%.

463

464 4.2. Thresholds in the regional-scale approach

465

466 The analysis of the newspapers allowed the identification of a significant number of storm
467 events having caused coastal damage in the regional study area. Table 3 shows the main
468 hydrodynamic characteristics of these storms and the type and extent of the damage they
469 caused. As can be observed, long duration of the storm is important but does not seem
470 critical in determining the occurrence of coastal damage. This way, even if the long-lasting
471 events obviously generated important damages, also several events with relatively short
472 durations have caused reported destruction on coastal infrastructure, as occurred in January
473 1982 in both Huelva and Cádiz coasts. On the other hand, the simultaneous occurrence of a
474 storm event and mean or spring tides can be regarded as an important factor in the generation
475 of damage.

476

477 ***APPROXIMATE LOCATION OF TABLE 3***

478

479 The details of which specific locations were affected along Huelva or Cádiz coast are not
480 included in Table 3, but it is important to note that most of the destructive effects were
481 reported along Cádiz coast or in both provinces, while very few were reported only in
482 Huelva coast. The locations having recorded damage in the analysed period are shown in
483 Figure 5, where clear hotspots of damage occurrences are observed around Northern Cádiz

484 coast and Western Huelva coast, which are the most densely populated areas along the
485 Spanish Gulf of Cádiz shore.

486

487 ***APPROXIMATE LOCATION OF FIGURE 5***

488

489 Regarding the time distribution of the storm events with associated recorded damage, Figure
490 6 shows that the highest frequency was recorded in the 1980s, apart from the unusually
491 intense storm season that occurred in 1996. These periods correspond to strongly negative
492 NAO (North Atlantic Oscillation) conditions, which generate more frequent storms in the
493 study area (Plomaritis et al., 2009a). A slightly increasing trend can be observed in the data
494 that could be related to the combination of two factors: the strong growth in human
495 occupation experienced along the Gulf of Cádiz coasts in the last couple of decades, and the
496 long-term erosion trend recorded at many locations along the study area (Ballesta et al.,
497 1998; Domínguez et al., 2005; Gracia et al., 2006; Del Río, 2007).

498

499 ***APPROXIMATE LOCATION OF FIGURE 6***

500

501 In order to extract the critical threshold of wave conditions that caused damage reported in
502 the newspapers, average and maximum wave heights of the storm events in Table 3 are
503 presented in Figure 7.

504 These results allow the acquisition of a critical threshold for the minimum storm conditions
505 capable of generating damage to infrastructure or human occupation in the regional study
506 area. The threshold would be defined as follows:

507

508 – Event with duration of 30 hours or higher.

509 – Moderate average wave height (≥ 3.3 m) and high maximum wave height (≥ 4 m).

510 – Mean or spring tide situation.

511 – Average wind speed above 9 m/s, approaching from the 3rd and 4th quadrants.

512

513 ***APPROXIMATE LOCATION OF FIGURE 7***

514

515 **5. Discussion**

516

517 The application of two complementary methodologies aimed at defining critical storm
518 thresholds at different scales led to a variety of results, which at some points delivered
519 markedly different thresholds for the same type of effect. This way, minimum significant
520 wave height needed for the generation of damage to infrastructure was found to be $H_s > 7.2$
521 m in the local test site and $H_s > 3.3-4$ m in the regional coastline. It is evident from these
522 results that Cortadura beach is not particularly vulnerable in this sense due to its high
523 elevation above zero level, while other beaches along the Spanish Gulf of Cádiz would
524 suffer this kind of damage much more frequently. That is the case for Huelva coast, where
525 average wave height is generally lower than in most part of Cádiz coast (MOPT, 1992).

526 Several authors highlight that the potential damage caused by a storm is greatly determined
527 by its relative intensity, i.e. the relationship between storm and modal wave height in the
528 area (Reyes et al., 1999; Cooper et al., 2004). This way, storms usually have a greater
529 influence in coastal morphology in areas characterized by low modal wave energy (Roy et
530 al., 1994). If more detailed data on storm impacts were available in order to derive separate
531 structural thresholds for Cádiz and Huelva provinces, the latter would probably be lower. It
532 is also clear that if a regional single value of wave height threshold should be chosen in a
533 worst-case approach, this would be the lowest one, namely $H_s > 3.3$ m. However, the above

534 methodology shows that local morphological characteristics (natural or anthropogenic) play
535 an important role on the derived thresholds.

536 Regarding the thresholds for morphological change, it must be noted that in all the test sites
537 the significant wave height needed to cause berm erosion shows a return period of less than
538 one year, as would be expected (Fig. 8). Camposoto beach, with a threshold of 1.5 to 2 m of
539 significant wave height, presents a very dynamic behaviour and is in fact eroded and
540 flattened several times every winter season; on the other hand, Cortadura beach, with a
541 threshold of 3.75 m of significant wave height, is more stable and related to its typically
542 seasonal behaviour it requires higher wave energy to change shape from the steeper summer
543 profile to the more gentle winter profile (Plomaritis et al., 2009b).

544

545 ***APPROXIMATE LOCATION OF FIGURE 8***

546

547 The differences in TSLV over the study area are generally produced by local-scale wave
548 processes, as large-scale (barometric setup) and meso-scale (storm surges) processes do not
549 show a spatial variability over the study area. The former, because the dimensions of the
550 Gulf of Cádiz are comparable with the typical extent of a low-pressure system in the area
551 (Holton, 2004). The latter, because the general morphology of the continental shelf exhibits
552 similar width and bathymetric characteristics in Huelva and the Western part of Cádiz. The
553 above similarities are exemplified in equation (2), where the combination of barometric
554 setup and storm surge in Cádiz are within the 95% confidence interval of the same
555 parameters in Mazagón (Fig. 4). The above relation is not valid eastwards of Cape Trafalgar,
556 where the continental shelf is much narrower and steeper (Fig. 1).

557 For the local-scale processes the total vertical runup equation of Holman (1986) modified by
558 Komar (1998) was used, which estimates the combined wave setup and the 2% of the highest

559 vertical runups. In the computation of wave runup a worst-case approach was adopted by
560 selecting the beach profiles with the maximum winter intertidal slope, as steeper slopes
561 involve higher wave runup values (Holman, 1986). In fact, authors such as Cooper et al.
562 (2004) point out the higher susceptibility of intermediate-reflective beaches to changes in
563 wave regime. This can be observed in Figure 9a, where the most dissipative test site
564 (Cortadura) presents a significantly low rate of increase in total sea-level variation (TSLV)
565 with increased wave heights, while the steepest test site (Bota) is much more susceptible to
566 higher waves. Despite of the slope differences all the test sites can be characterised as
567 dissipative type beaches with low Irribaren numbers; under such conditions the swash height
568 is saturated and infragravity waves are dominant (Holman and Sallenger, 1985; Ruessink et
569 al., 1998). Overall, in a mesotidal area such as the Gulf of Cádiz, tidal conditions during a
570 storm are a critical factor on which the thresholds depend, with threshold values increasing
571 by 50% between typical spring and typical neap tide conditions. The percentage of TSLV
572 explained by each parameter is presented in Figure 9b for the three test sites. In the most
573 dissipative case (Cortadura) the importance of tidal level is significant with percentages
574 dropping slowly from 100% under minimum wave heights to 60% in case of an extreme
575 storm event. The contribution of waves to TSLV is higher by a factor of 2 in comparison
576 with the wind and barometric contributions for the most dissipative site (Cortadura). In the
577 case of the steepest beach shoreface (Bota), the relative importance of tidal level is decreased
578 and the variation due to local wave processes is increased up to 50% in extreme cases. As
579 expected no significant variation occurs for the surge and barometric setup, since the
580 foreshore slope is not affecting these processes.

581 On another note, the methodology adopted in this work assumes that if initial conditions
582 remain the same, coastal response to different events of the same magnitude will be similar.
583 Nevertheless, the fact that threshold computation involves choosing a fixed value for

584 intertidal slope and a fixed height of morphological features considered for each site implies
585 ignoring beach state prior to storm arrival. Hydrodynamic processes during a storm
586 continuously reshape beach morphology, modifying parameters like intertidal slope or berm
587 height; in this way, the initial conditions for successive storms are different, so the threshold
588 for morphological change can also be different.

589 Beaches that have been eroded and flattened by a storm tend to dissipate incident wave
590 energy, which together with the lower wave runup in gentler slopes could point to a lower
591 vulnerability to the impact of subsequent storms, and so to a higher threshold for subsequent
592 morphological change. On the other hand, flattened beaches allow a given water level to
593 reach areas further inland than it would in steeper profiles, hence increasing the probability
594 of damage by subsequent storms to structures located on the backbeach (e.g. by flooding);
595 this would imply a lower threshold for damage to infrastructure for the following storm.

596

597 ***APPROXIMATE LOCATION OF FIGURE 9***

598

599 In this sense, possible changes in the initial conditions of the coast for storms to act upon are
600 especially important in case of storm groups (Ferreira, 2005), as beach erosion is increased
601 when storm frequency exceeds the beach recovery period for individual storms (Morton et
602 al., 1995). However, storm groups commonly produce limited effects in the study area, since
603 except for the highly dynamic Camposoto beach, most beaches generally show long
604 recovery periods (Benavente et al., 2000). The recovery usually takes place by onshore
605 migration of nearshore bars that get attached to the berm in the beginning of the summer
606 months (Benavente et al., 2000). As a consequence of this, beach profile morphology is
607 generally not recovered during the calm periods within storm groups. On the contrary, beach
608 profiles are eroded by the first storms, increasing their dissipativeness; this facilitates profile

609 self-protection against successive storms, as the energy of shoaling waves tends to be
610 dissipated across the profile, thus reducing wave erosive capacity. Since beach profile is not
611 recovered between two events within a storm group, the effects of several medium-energy
612 storms are generally not higher than those of a single higher-energy event, opposite to the
613 statements by authors like Lee et al. (1998) or Ferreira (2005).

614 An interesting example of exceptionally severe effects of storm groups in the study area is
615 presented in Figure 10, which shows the consequences of the successive storms that occurred
616 in Cortadura-Camposoto test site between 21st December and 15th January 2010. Average
617 significant wave height recorded during the storm peaks was around 4.3 m, thus above
618 theoretical thresholds for berm erosion in Cortadura, and berm erosion, washover and dune
619 foot erosion in Camposoto, but below the threshold for damage to infrastructure in
620 Cortadura. However, the long-lasting character of the storm group, with significantly low
621 atmospheric pressures and sustained strong winds blowing onshore for almost three weeks,
622 generated a nearly continuous storm surge over the whole period, which together with the
623 coincidence of some storm peaks with spring tide conditions led to widespread, significant
624 damage along the whole Gulf of Cádiz coast (Del Río et al., 2010). In this case, a sequence
625 of moderate storms resulted in as much morphological change and damage as one that would
626 have resulted from a single higher-magnitude event (Lee et al., 1998), which is not a
627 common behaviour in the study area.

628

629 ***APPROXIMATE LOCATION OF FIGURE 10***

630

631 In this sense, thresholds in the test sites were specifically derived for spring tide conditions,
632 as many authors have pointed out the relevance of the coincidence between storm events and
633 spring tides in meso- and macrotidal environments (e.g. Cooper et al. 2004, Pye and Blott

634 2008). In fact, the newspaper record analysed in this work shows the prime importance of
635 tide type in causing damage to coastal infrastructure, as 70% of the events with recorded
636 damage occurred during spring tides (Table 3). It is clear that in some cases the long
637 duration of the storm events or storm groups involved transitions between different tide
638 types, but this very rarely included neap tides.

639 It is important to note that the processes described above are of utmost importance in an area
640 like the study zone, where tourism is a major source of income. Apart from the obvious
641 economic losses caused by damage to infrastructure, storm-induced morphological changes
642 on beaches can also have important socioeconomic impacts in the area. User's demand for
643 wide and healthy beaches often triggers the need for strong investments in artificial beach
644 replenishments, which have indeed been carried out along many beaches in the Spanish Gulf
645 of Cádiz by the Ministry of Environment (Muñoz et al., 2001). Regarding the test sites, La
646 Bota was nourished in 1995 with 930,000 m³ of sand; Cortadura and the adjacent La Victoria
647 beach were nourished in 1991 and 2004 with a total amount of sediment over 2 million m³;
648 finally, Camposoto beach was replenished in 1998 with 740,000 m³ of sand (Muñoz et al.,
649 2001), and here significant efforts are also being made on recovery and protection of the
650 dune ridges. For these reasons, critical storm thresholds may be very useful tools that help to
651 minimize the need for these kinds of investments, by facilitating the development of
652 vulnerability maps, spatial planning strategies, early warning systems and other instruments
653 of risk prevention.

654

655 **6. Conclusions**

656

657 Diverse methodologies were applied in the Gulf of Cádiz coast with the aim of establishing
658 critical storm thresholds, regarding these as the minimum wave conditions necessary to

659 cause a certain type of effect on the coast. On a regional scale, newspapers and historical
660 wave databases were used to define critical storm thresholds for the generation of damage to
661 infrastructure or human occupation along the coastlines of Huelva and Cádiz provinces. The
662 resulting minimum threshold is defined by Atlantic storms with an average wave height \geq
663 3.3 m, a maximum wave height \geq 4 m and a duration of 30 hours or higher in mean or spring
664 tide situation. On a more local scale, theoretical computations of water elevation due to
665 storms were performed and compared to beach topography in three test sites in order to
666 assess the risks of beach morphological change, dune foot erosion and overwash. In this case
667 the minimum thresholds in spring tide conditions range between 1.5 and 3.75 m of
668 significant wave height depending on the test site and the risk assessed. The difficulties
669 found in defining a single regional storm threshold are mainly related to the particular
670 characteristics of the study area, where beach morphology, degree of human occupation and
671 other important aspects show significant spatial variability.

672 Thresholds proposed in this work provide a guideline of coastal response to storms in the
673 area that can help to prevent the negative impacts of storm events. In this sense, they could
674 also be useful for adequately planning future development in the coastal zones which are still
675 undeveloped along this high-pressure area. In the case of damage to infrastructure it must be
676 noted that a forecast of waves exceeding the critical threshold does not necessarily mean that
677 serious coastal damage will always occur, but there is a strong likelihood of some kind of
678 effect on the structures located in the backbeach. Regarding the threshold for storm-induced
679 morphological change, it is clear that beach erosion, dune retreat or washover occurrence do
680 not depend solely on wave height and tidal level, but also on other factors such as previous
681 beach state, storm duration and time interval between successive storms. Nonetheless, the
682 thresholds proposed are aimed to be at the same time scientifically sound and easy to use,
683 which is the reason why in this first approach only wave and tide conditions have been

684 considered, together with an empirically derived relationship between waves and surge.
685 Further work will include the effects of antecedent beach morphology and other more
686 complex parameters, such as dynamic response of the beach .
687 Finally, another key issue regarding storm thresholds is the time framework considered. All
688 the thresholds proposed in this work were obtained from data spanning a given period of
689 time, thus constituting snapshots of risk conditions at that time. However, beach and
690 nearshore zones are extremely dynamic due to both natural and human-related factors (such
691 as beach nourishments or coastal defence structures), and also the characteristics of
692 occupation on the coast change over time. As a consequence, critical storm thresholds will
693 change accordingly and therefore will need to be updated. In this sense it is important to
694 state that the proposed methodology can be easily applied over any area by using simple
695 morphological measurements (beach slope, berm height, dune foot, etc.) that can be updated
696 frequently. Future work will be directed towards the use of these thresholds as initial values
697 for the generation of dynamic thresholds by means of numerical modelling. The final aim in
698 the framework of MICORE project will be the integration of these thresholds into an early
699 warning system that could provide an adequate prediction of the effect of future storms, to be
700 used by Civil Protection agencies and coastal authorities.

701

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709

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829

830 **Figure captions**

831

832 Figure 1. Location map of the study area and the test sites.

833 Figure 2. Wave rose of the offshore buoy located at the centre of the Spanish Gulf of Cádiz
834 (1996-2002) (wave height in metres).

835 Figure 3. Aerial photographs of the test sites. A: Bota beach in Huelva coast (Photo: Google
836 Earth). B: Cortadura beach in Cádiz coast. C: Camposoto beach in Cádiz coast.

837 Figure 4. Correlation for storm data of sea level residual (storm surge) recorded at Mazagón
838 tide gauge and wave height recorded at Gulf of Cádiz offshore wave buoy between 1996 and
839 2008 (crosses). Circles show the same correlation for Cádiz tide gauge and Gulf of Cádiz
840 offshore wave buoy between 2008 and 2010.

841 Figure 5. Spatial distribution of storm events in the Spanish Gulf of Cádiz having caused
842 damage to coastal infrastructure between 1958 and 2001, according to the newspaper
843 records.

844 Figure 6. Yearly frequency of storm events having been reported to generate damage to
845 coastal infrastructure in the Spanish Gulf of Cádiz.

846 Figure 7. Average and maximum wave height of the events having caused reported damage
847 to coastal structures in the Spanish Gulf of Cádiz.

848 Figure 8. Return period of significant wave heights in the coast of Cádiz according to the
849 HIPOCAS database. Wave heights have been corrected by means of the calibration in
850 equation (5). The parameters μ and ψ are the location and scale parameters of the Gumbel
851 distribution (Graphical product of CAROL software, University of Cantabria).

852 Figure 9. (a) Relationship between significant wave height and the associated total sea level
853 variation (TSLV) according to the equations (1) to (4) in the test sites. (b) Relative

854 contributions of waves (dotted line), pressure plus winds (dashed line), and tides (dash
855 dotted line) in controlling TSLV on the test sites.

856 Figure 10. Examples of the effects of winter 2010 storms in the study area. A: Beach and
857 dune erosion in Camposoto beach (31st December 2009). B: Overtopping and inundation of
858 the seafront in Cádiz city (1st January 2010). C: Wave runup reaching the seawall at northern
859 Cortadura beach (1st January 2010). D: Flooding of beach facilities by wave runup in
860 southern Cortadura beach (5th January 2010).

861

862 **Table captions**

863

864 Table 1. Topographic elevations of the different types of threshold analyzed in the test sites,
865 corresponding to average summer values.

866 Table 2. Minimum wave height thresholds for morphological change, overwash, dune foot
867 erosion and damage to infrastructure in the test sites in case of MHWS.

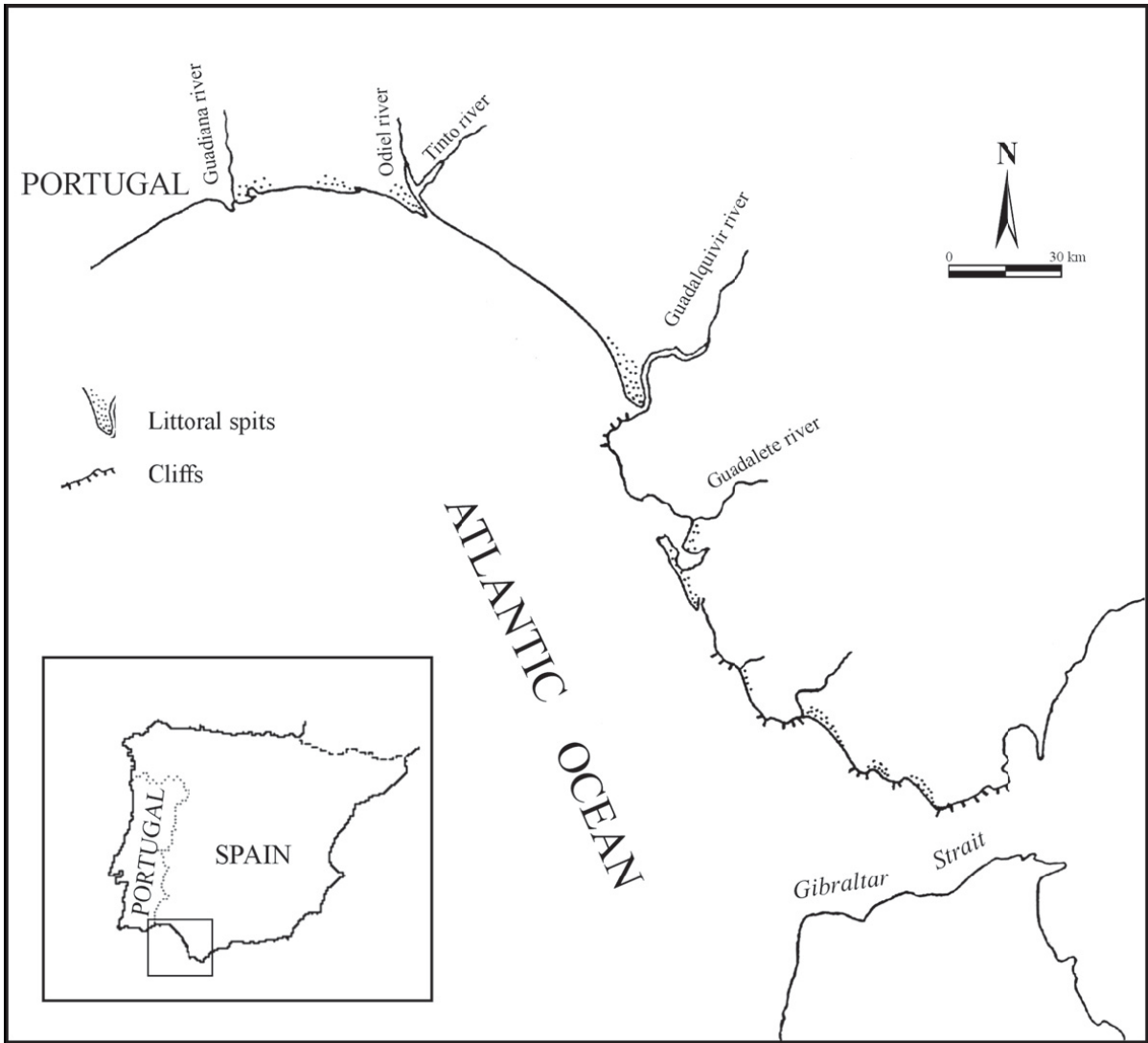
868 Table 3. Hydrodynamic characteristics of storm events having caused reported damage on
869 coastal infrastructure along Cádiz and/or Huelva coasts. Wave heights have been corrected
870 from HIPOCAS data according to equation (6). Tide type: S (spring), M (mean), N (neap).

871 Newspapers: Diario de Cádiz (1), ABC (2), El Correo de Andalucía (3), Odiel (4), Huelva
872 Información (5) and La Voz de Huelva (6).

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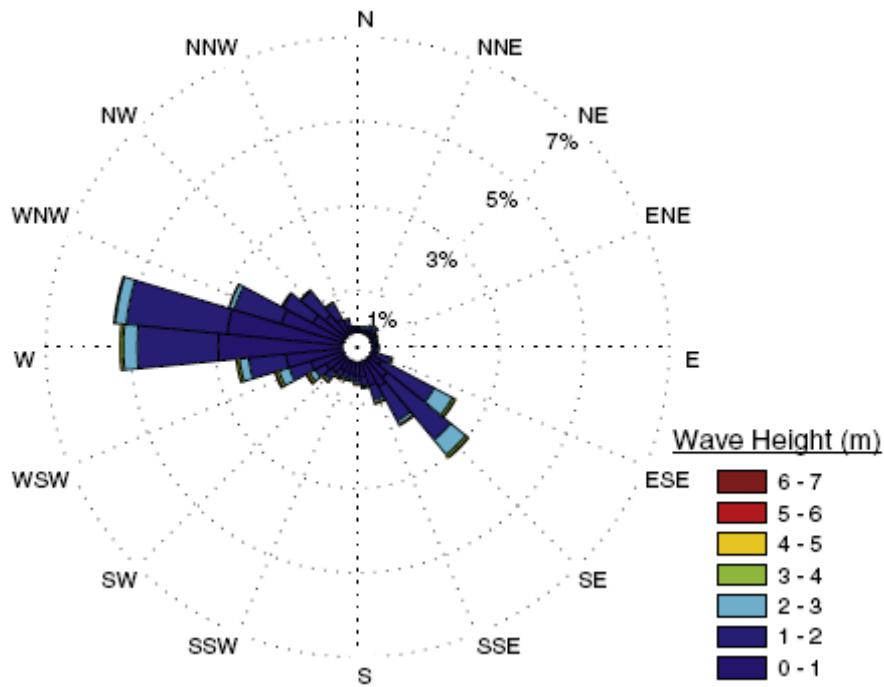
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877 Figure 1

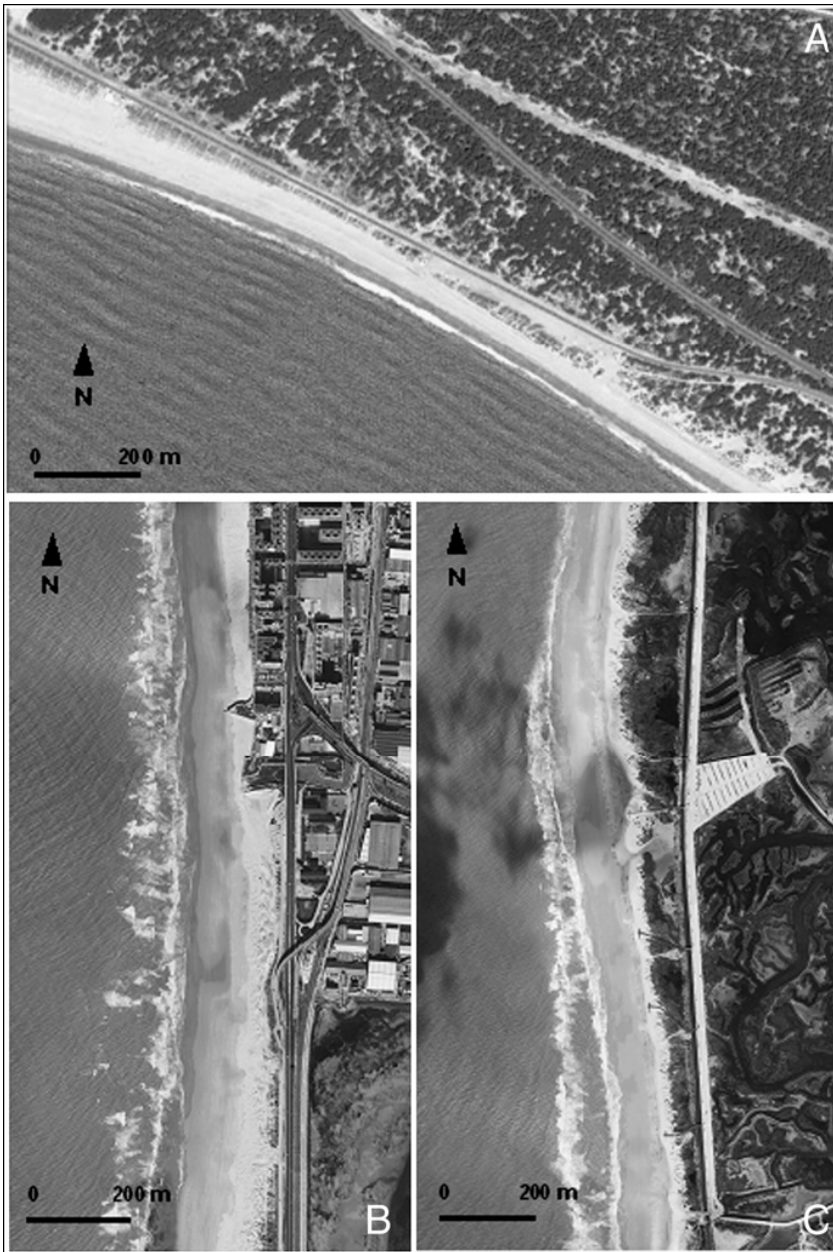
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880 Figure 2

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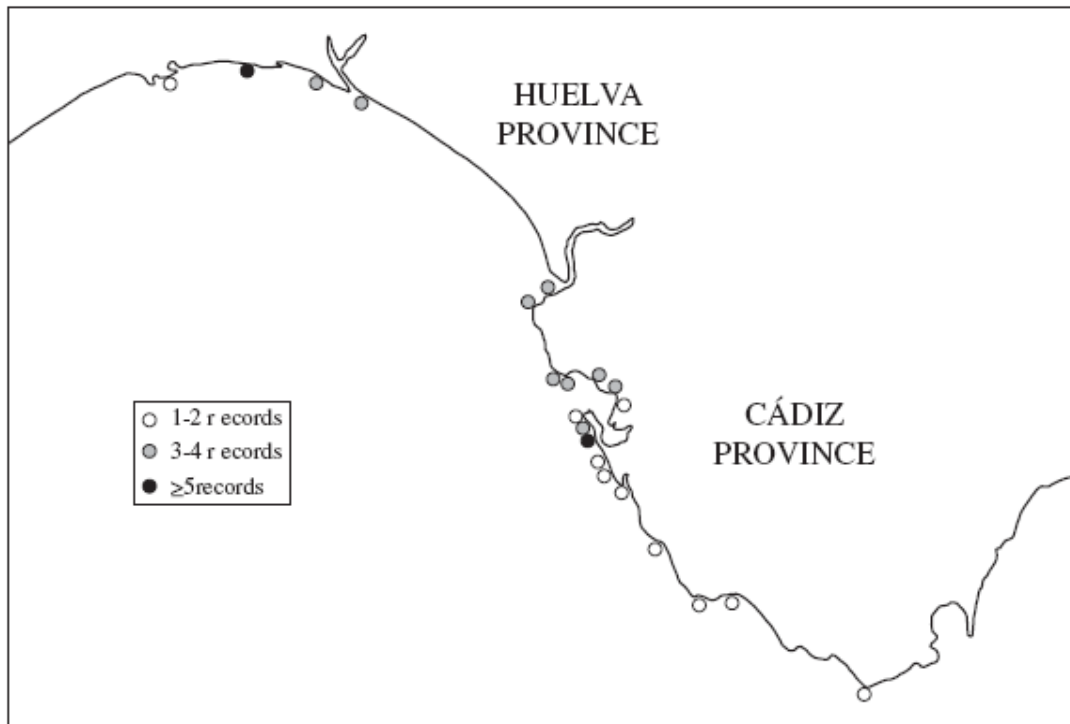


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883 Figure 3

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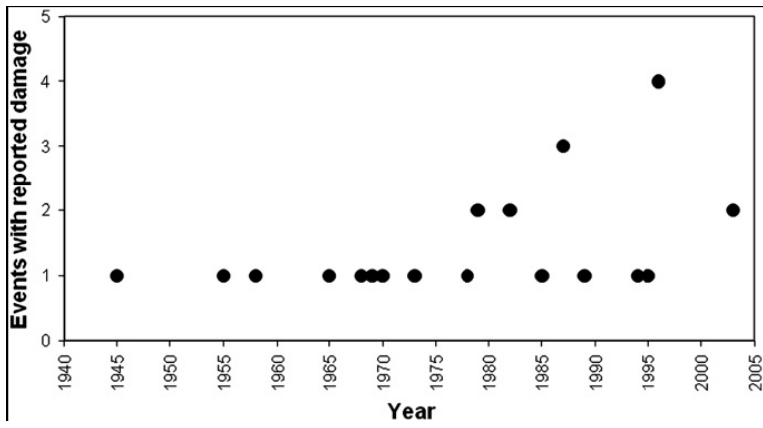


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891 Figure 5

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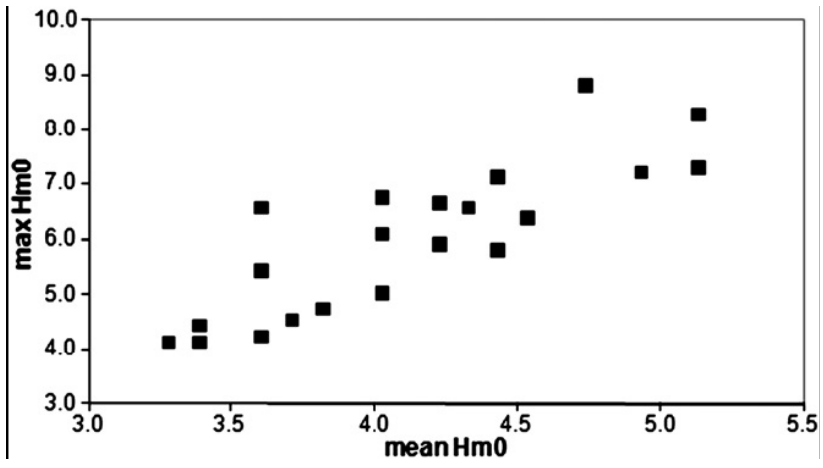


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895 Figure 6

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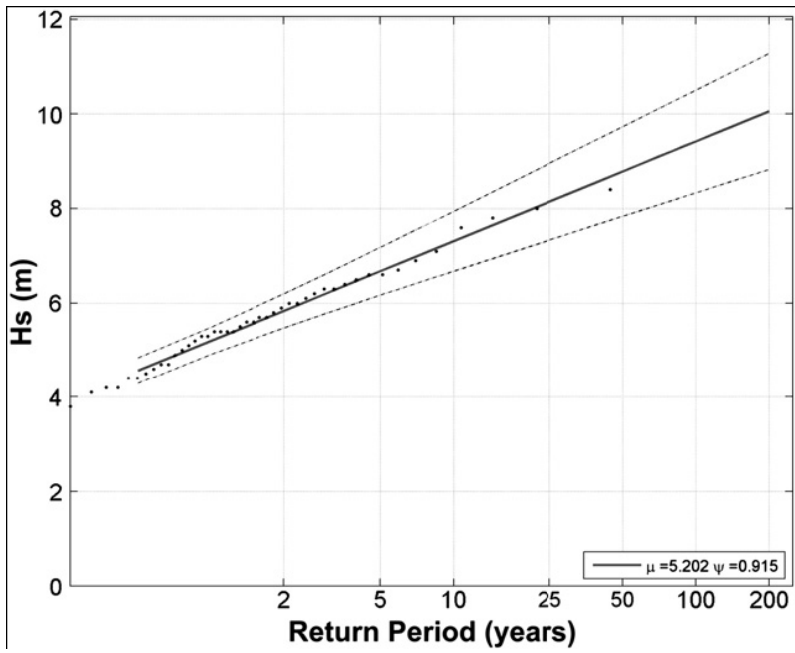


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899 Figure 7

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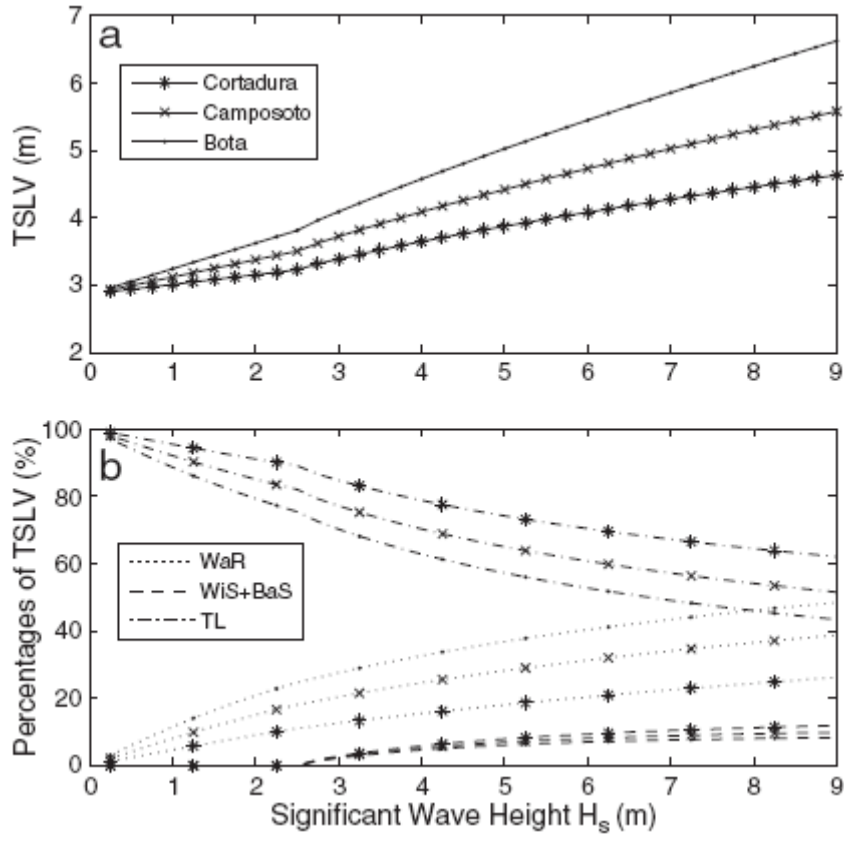


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903 Figure 8

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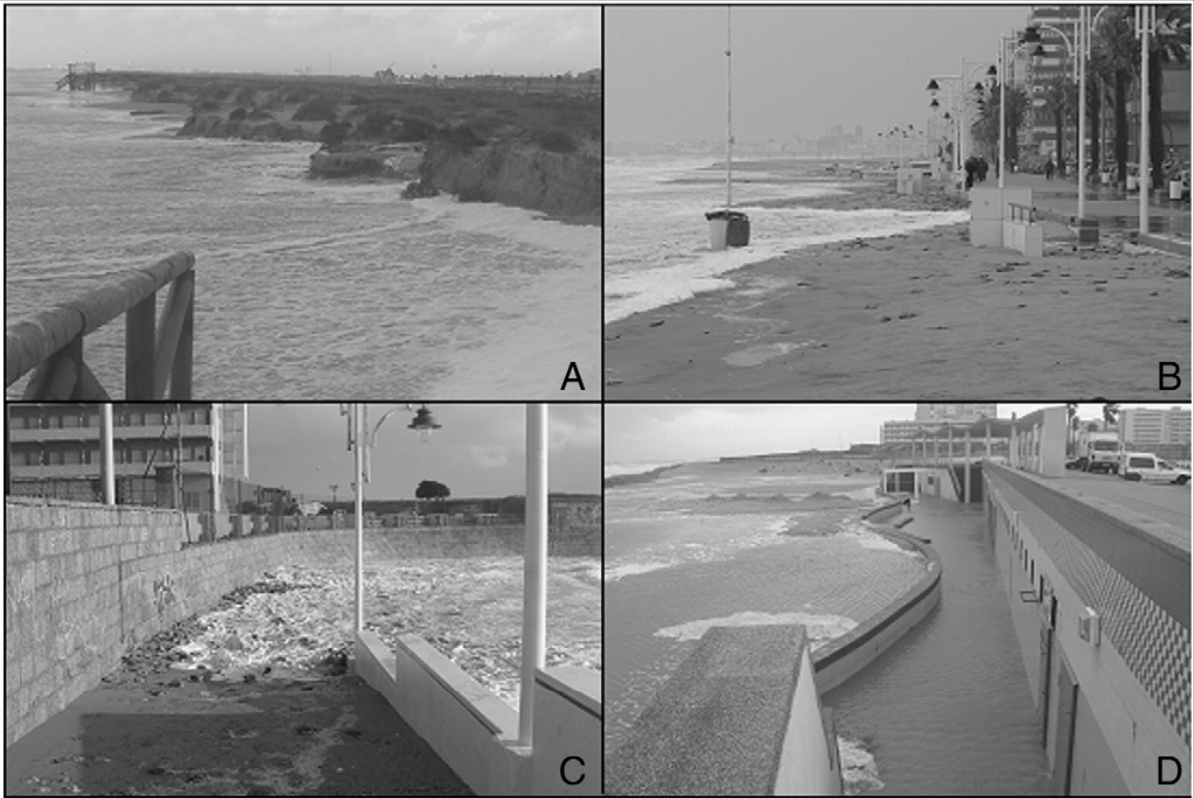


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907 Figure 9

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911 Figure 10

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913

914 Table 1.
915

	Berm	Washover	Dune foot	Base of seawall
Bota beach	3.60 m	---	4.26 m	---
Cortadura beach	3.70 m	---	---	4.40 m
Camposoto beach	3.20 m	3.65 m	4.10 m	---

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920 Table 2.
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	Morphological change	Overwash	Dune foot erosion	Structural damage
Bota beach	Hs = 2.00 m	---	Hs = 3.33 m	---
Cortadura beach	Hs = 3.75 m	---	---	Hs = 7.19 m
Camposoto beach	Hs = 1.00 m	Hs = 2.57 m	Hs = 3.75 m	---

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Event n°	Start date	Duration (hours)	Hours $H_{m0} > 4\text{ m}$	Mean H_{m0}	Max H_{m0}	Tide type	Mean W (m/s)	Sea level residual (cm)	Newspaper	Damage type and extent (H: Huelva; C: Cádiz)
1	13/12/1958	240	126	4.9	7.2	N-S	12.3	15.4	1, 2	C: damage in harbour
2	26/09/1965	30	3	3.3	4.1	S	10.5	10.4	2	C: great damage in seafront, damage in beach bars and beach huts
3	31/10/1968	69	3	3.4	4.0	M	10.4	14.1	1	C: damage in a beach hotel
4	01/05/1969	42	6	3.4	4.4	S	9	12.0	1	C: beach huts destroyed
5	02/01/1970	330	108	4.5	6.4	N-S	10.4	19.5	1, 3, 4	H: serious damage and surge flooding in beach restaurants and beach houses, some beach houses destroyed C: great damage in seafront, beach houses, beach restaurants
6	15/01/1973	87	30	4.7	8.8	M-S	12.2	2.3	1	C: damage in cars parked by the seafront
7	23/02/1978	240	30	4.0	6.1	M-S	10.1	10.0	1, 3	C: damage in seawall
8	24/01/1979	114	36	4.4	5.8	M-S	10.7	17.8	1, 4	H: seafront, beach restaurants and houses damaged, pipelines destroyed C: damage in harbour
9	09/02/1979	171	96	5.1	7.3	M	12.2	13.4	1	C: damage in seawall and seafront, stairs of beach access destroyed
10	10/01/1982	48	9	4.0	5.0	S	9.7	15	1, 3, 4	H: damage in beach houses C: damage in seafront and coastal road, access and huts destroyed
11	06/11/1982	60	36	5.1	8.3	M-S	11.2	20	1	C: jetty of harbour damaged
12	06/02/1985	159	57	4.2	5.9	M-S	9.0	3.3	1	C: damage in seafront
13	12/01/1987	72	27	4.4	7.1	M	11.8	10.2	1	C: small damage in seafront fence
14	26/01/1987	117	12	3.8	4.7	M-S	9.4	11.1	1	C: great damage in seafront, damage in beach accesses, beach facilities flooded by surge
15	07/12/1987	27	0	2.9	3.2	M	10.1	23.6	1, 5	H: damage in beach houses C: coastal road flooded
16	26/11/1989	36	0	3.7	4.5	M	8.4	21.1	3, 5	H: damage in beach houses and restaurant, one house destroyed
17	26/02/1994	69	0	3.6	4.2	S	9.1	11.1	1, 3	C: beach facilities and beach restaurant flooded and damaged by surge, damage in PA system, damage in breakwater
18	25/12/1995	129	15	3.6	5.4	M-S	9.6	7.8	1	C: viewpoint destroyed, serious damage in breakwater and seawall, sections of groin collapsed, damage in stairs of beach access

19	04/01/1996	207	66	4.3	6.6	M	9.9	11.2	1, 3, 6	H: damage in beach hotel, beach bars collapsed C: extensive damage in jetty, groins, breakwaters, drainage system, beach accesses destroyed
20	20/01/1996	213	63	4.0	6.8	M-S	10.5	20.8	1, 3, 6	H: beach Yacht Club, tennis courts and wastewater sewers destroyed, beach houses damaged C: extensive damage in seafronts, breakwaters, seawall, beach bars and beach accesses, PA systems destroyed, coastal roads flooded
21	11/11/1996	90	15	3.6	6.6	M-S	9.9	18.2	1	C: damage in seafront and beach access
22	10/12/1996	354	114	4.2	6.7	M-S	10.4	16.4	1, 6	H: beach houses, beach bars and coastal roads flooded C: damage in seafront, beach facilities and beach accesses, coastal roads flooded

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