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# On the optimal designs for the prediction of Ornstein–Uhlenbeck sheets



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#### 1. Introduction

A common problem in spatial statistics is deciding how to choose a set of sample locations in order to predict a random process in an optimal way. In the present paper we study the problem of optimal design for the prediction of an Ornstein–Uhlenbeck (OU) sheet on a monotonic set with respect to the integrated mean square prediction error (IMSPE) criterion and the entropy criterion.

We consider the stationary process

$$Y(s,t) = \theta + \varepsilon(s,t) \tag{1.1}$$

(1.1)

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with the design points taken from a compact design space  $\mathcal{X} = [a_1, b_1] \times [a_2, b_2]$ , where  $a_1 < b_1$  and  $a_2 < b_2$  and  $\varepsilon(s, t)$ ,  $s, t \in \mathbb{R}$ , is a stationary OU sheet, that is a zero-mean Gaussian process with covariance structure

$$\mathsf{E}\,\varepsilon(s_1,t_1)\varepsilon(s_2,t_2) = \frac{\dot{\sigma}^2}{4\alpha\beta}\exp\left(-\alpha|s_1-s_2|-\beta|t_1-t_2|\right),\tag{1.2}$$

where  $\alpha > 0$ ,  $\beta > 0$ ,  $\tilde{\sigma} > 0$ . We remark that  $\varepsilon(s, t)$  can also be represented as

$$\varepsilon(s,t) = \frac{\overline{\sigma}}{2\sqrt{\alpha\beta}} e^{-\alpha s - \beta t} \mathcal{W}\left(e^{2\alpha s}, e^{2\beta t}\right),$$

where W(s, t),  $s, t \in \mathbb{R}$ , is a standard Brownian sheet (Baran et al., 2003; Baran and Sikolya, 2012).

# ABSTRACT

Computer simulations are often used to replace physical experiments for exploring the complex relationships between input and output variables. We study the optimal design problem for the prediction of a stationary Ornstein–Uhlenbeck sheet on a monotonic set with respect to the integrated mean square prediction error criterion and the entropy criterion. We show that there is a substantial difference between the shapes of optimal designs for Ornstein–Uhlenbeck processes and sheets. In particular, we show that the optimal prediction based on the integrated mean square prediction error does not necessarily lead to space-filling designs.

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In order to apply the usual notation of spatial modelling (Kiselák and Stehlík, 2008) we introduce  $\sigma := \tilde{\sigma}/(2\sqrt{\alpha\beta})$  and instead of (1.2) we investigate

$$\mathsf{E}\,\varepsilon(s_1,t_1)\varepsilon(s_2,t_2) = \sigma^2 \exp\left(-\alpha|s_1-s_2| - \beta|t_1-t_2|\right),\tag{1.3}$$

where  $\sigma$  is considered as a nuisance parameter.

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Further, we require that the shifted OU sheet (1.1) is measured at the points constituting a *monotonic set*. A monotonic set can be defined in an arbitrary Hilbert space *H*, with real or complex scalars. For  $x, y \in H$ , we denote by  $\langle x, y \rangle$  the real part of the inner product. A set  $E \subset H \times H$  is called monotonic (see Minty (1962, 1963)) provided that for all  $(x_1, y_1), (x_2, y_2) \in E$ we have  $\langle x_1 - x_2, y_1 - y_2 \rangle \ge 0$ . A practical example of such a set is provided by the measurements on isotherms of a stationary temperature field, with several applications in thermal slab modelling (see e.g. Babiak et al. (2005) or Koizumi and Jin (2012)). In this paper we consider the following version of a monotonic set:

Condition D. The design points  $\{(s_1, t_1), (s_2, t_2), \dots, (s_n, t_n)\} \subset \mathcal{X}, n \in \mathbb{N}$ , are not overlapping (observations without repetitions); moreover,  $0 < s_1 < s_2 < \dots < s_n$  and  $0 < t_1 < t_2 < \dots < t_n$  hold.

For the shifted OU sheet (1.1) observed at points satisfying *Condition D*, Baran and Stehlík (submitted for publication) derived the exact form of the Fisher information (matrices) corresponding to the trend parameter  $\theta$  and to covariance parameters  $r = (\alpha, \beta)$ , and the authors investigated the problem of *D*-optimal designs for the estimation of these quantities.

We derive the exact form of the IMSPE recently used in several papers (see e.g. Crary (2002) or Sacks et al. (1989)), and show that in contrast to the case for the OU process on a compact interval investigated by Baldi Antognini and Zagoraiou (2010), the equidistant design is usually not optimal. This is an important observation, and also consistent with the results of Pronzato and Müller (2012), since statistical folklore is that space-filling designs have superior properties when it comes to the prediction of emulator functions. We also investigate the properties of the optimal design with respect to the entropy criterion (Baldi Antognini and Zagoraiou, 2010; Shewry and Wynn, 1987).

Observe that by condition *Condition D*, the results presented here are not applicable for space-filling designs. In the general case the main problem is the difficulty of finding the inverse of the covariance matrix of the observations. The authors have some preliminary results for regular grid designs, where the covariance matrix is the Kronecker product of two simple covariance matrices corresponding to the two spatial dimensions, and this special form allows finding a reasonable form of the inverse and calculating the objective function for the IMSPE criterion. However, the presentation of these results is beyond the space limitations of this work.

#### 28 **2.** Optimal design with respect to the IMSPE criterion

Suppose we observe our process Y(s, t) at the design points  $\{(s_1, t_1), (s_2, t_2), \dots, (s_n, t_n)\}$  satisfying Condition D. The 29 main aim of the kriging technique consists in predicting the output of the simulator on the experimental region, and for 30 any untried location  $x = (x_1, x_2) \in \mathcal{X}$  the estimation procedure is focused on the best linear unbiased estimator of Y(x)31 given by  $\widehat{Y}(x) = \widehat{\theta} + \mathcal{Q}^{\top}(x)C^{-1}(n, r)(\mathbf{Y} - \mathbf{1}_n\widehat{\theta})$ , where  $\mathbf{Y} = (Y(s_1, t_1), \dots, Y(s_n, t_n))^{\top}$  is the vector of observations,  $\mathbf{1}_n$  is the 32 column vector with entries 1 of length n, C(n, r) is the covariance matrix of **Y**, Q(x) is the vector of correlations between 33 Y(x) and **Y** defined by  $Q(x) = (Q(x, s_1, t_1), \dots, Q(x, s_n, t_n))^{\top}$  with  $Q(x, s_i, t_i) := \exp(-\alpha |x_1 - s_i| - \beta |x_2 - t_i|)$  and  $\widehat{\theta}$  is the generalized least squares estimator of  $\theta$ , that is  $\widehat{\theta} = (\mathbf{1}_n^{\top} C^{-1}(n, r) \mathbf{1}_n)^{-1} \mathbf{1}_n^{\top} C^{-1}(n, r) \mathbf{Y}$ . Usually, correlation parameters 34 35  $\alpha$ ,  $\beta$  are unknown and will be estimated by the maximum likelihood method. Thus, the kriging predictor is obtained by 36 substituting the maximum likelihood estimators (MLE) ( $\hat{\alpha}, \hat{\beta}$ ) for ( $\alpha, \beta$ ) and in such a case  $\hat{Y}(x)$  is called the MLE-empirical 37 best linear unbiased predictor (Santner et al., 2003). 38

<sup>39</sup> Thus natural criteria will minimize suitable functionals of the mean squared prediction error (MSPE) given by

$$MSPE(\widehat{Y}(x)) := \sigma^{2} \left[ 1 - (1, \mathcal{Q}^{\top}(x)) \left[ \underbrace{\begin{array}{c} 0 & \mathbf{1}_{n}^{\top} \\ \mathbf{1}_{n} & C(n, r) \end{array} \right]^{-1} (1, \mathcal{Q}^{\top}(x))^{\top} \right].$$
(2.1)

Since the prediction accuracy is often related to the entire prediction region  $\mathfrak{X}$ , the design criterion IMSPE is given by

IMSPE 
$$(\widehat{Y}) := \sigma^{-2} \int_{\mathcal{X}} \text{MSPE} (\widehat{Y}(x)) dx.$$

Without loss of generality, we can assume that the design space  $\mathcal{X} = [0, 1]^2$ . Therefore, as extrapolative prediction is not advisable in kriging, we can set  $t_1 = s_1 = 0$  and  $t_n = s_n = 1$ .

45 **Theorem 2.1.** In our set-up,

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$$MSPE\left(\widehat{Y}(x)\right) = \sigma^{2} \left[1 - \varrho(x, s_{n}, t_{n})^{2} - \sum_{i=1}^{n-1} \frac{(\varrho(x, s_{i}, t_{i}) - \varrho(x, s_{i+1}, t_{i+1})q_{i})^{2}}{1 - q_{i}^{2}} + \left(1 + \sum_{i=1}^{n-1} \frac{1 - q_{i}}{1 + q_{i}}\right)^{-1} \left(1 - \varrho(x, s_{n}, t_{n}) - \sum_{i=1}^{n-1} \frac{\varrho(x, s_{i}, t_{i}) - \varrho(x, s_{i+1}, t_{i+1})q_{i}}{1 + q_{i}}\right)^{2}\right],$$



**Fig. 1.** IMSPE corresponding to the optimal design for the prediction and Fisher information on  $\theta$  as functions of correlation parameters ( $\alpha$ ,  $\beta$ ) for n = 3.

where  $q_i := \exp(-\alpha d_i - \beta \delta_i)$  with  $d_i := s_{i+1} - s_i$  and  $\delta_i := t_{i+1} - t_i$ , i = 1, 2, ..., n-1. Further,

IMSPE 
$$(\widehat{Y}) = 1 - A_n + \left(1 + \sum_{i=1}^{n-1} \frac{1 - q_i}{1 + q_i}\right)^{-1} B_n,$$
 (2.2)

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where

$$A_n = R_{1,1} + \sum_{i=1}^{n-1} \frac{R_{i,i}q_i^2 - 2R_{i+1,i}q_i + R_{i+1,i+1}}{1 - q_i^2},$$
(2.3)

$$B_{n} = 1 - 2\omega_{n} + R_{n,n} + \sum_{i=1}^{n-1} \left( \frac{R_{i,i} - 2R_{i+1,i}q_{i} + R_{i+1,i+1}q_{i}^{2}}{(1+q_{i})^{2}} + 2\frac{(R_{n,i} - \omega_{i}) - (R_{n,i+1} - \omega_{i+1})q_{i}}{1+q_{i}} \right) \\ + 2\sum_{i=2}^{n-1} \sum_{j=1}^{i-1} \frac{R_{i,j} - R_{i+1,j}q_{i} - R_{i,j+1}q_{j} + R_{i+1,j+1}q_{i}q_{j}}{(1+q_{i})(1+q_{j})},$$

$$(2.4)$$

with

$$\omega_{i} = \frac{1}{\alpha\beta} \left[ 2 - e^{-\alpha(d_{1} + \dots + d_{i-1})} - e^{-\alpha(d_{i} + \dots + d_{n-1})} \right] \left[ 2 - e^{-\beta(\delta_{1} + \dots + \delta_{i-1})} - e^{-\beta(\delta_{i} + \dots + \delta_{n-1})} \right], \quad (2.5)$$

$$R_{i,j} = \left[ \frac{1}{2\alpha} \left( 2e^{-\alpha(d_{j} + \dots + d_{i-1})} - e^{-\alpha(2d_{1} + \dots + 2d_{j-1} + d_{j} + \dots + d_{i-1})} - e^{-\alpha(d_{j} + \dots + d_{i-1} + 2d_{i} + \dots + 2d_{n-1})} \right) + (d_{j} + \dots + d_{i-1})e^{-\alpha(d_{j} + \dots + d_{i-1})} \right]$$

$$\times \left[ \frac{1}{2\beta} \left( 2e^{-\beta(\delta_{j} + \dots + \delta_{i-1})} - e^{-\beta(2\delta_{1} + \dots + 2\delta_{j-1} + \delta_{j} + \dots + \delta_{i-1})} - e^{-\beta(\delta_{j} + \dots + \delta_{i-1} + 2\delta_{i} + \dots + 2\delta_{n-1})} \right) + (\delta_{j} + \dots + \delta_{i-1})e^{-\beta(\delta_{j} + \dots + \delta_{i-1})} \right], \quad i, j \in \mathbb{N}, 1 \le j \le i \le n. \quad (2.6)$$

**Example 2.2.** Consider a three-point design, that is n = 3,  $s_1 = t_1 = 0$ ,  $s_2 := d$ ,  $t_2 := \delta$ ,  $s_3 = t_3 = 1$ . For this particular design we obviously have  $d_1 = d$ ,  $d_2 = 1 - d$ ,  $\delta_1 = \delta$ ,  $\delta_2 = 1 - \delta$ . By analysing the partial derivatives of IMSPE  $(\widehat{Y})$  one can easily show that the minimum of IMSPE is reached at d = 1/2,  $\delta = 1/2$ , so for n = 3 the equidistant design is optimal. 10 11 In Fig. 1, IMSPE  $(\widehat{Y})$  corresponding to the optimal design and the Fisher information on the shift parameter  $\theta$  are plotted 12 as functions of correlation parameters ( $\alpha$ ,  $\beta$ ). Having a look at the figures for IMSPE and  $M_{\theta}$  one can observe that there is



**Fig. 2.** The values of  $d_1^*$ ,  $d_2^*$  and  $\delta_1^*$ ,  $\delta_2^*$  giving the optimum of IMSPE as functions of correlation parameters ( $\alpha$ ,  $\beta$ ) for n = 5.

a substantial difference between the variations of the estimation and the prediction criterion with respect to correlation parameters ( $\alpha$ ,  $\beta$ ). The equilateral lines for  $M_{\theta}$  differ considerably from equilateral curves for IMSPE, which shows the different level of sensitivity of these criteria to the misspecification of correlation parameters. For more information on the sensitivity of optimal design criteria with respect to parameter misspecification, see e.g. Stehlík (2004).

Theorem 2.3. IMSPE given by (2.2) is symmetric in the sense that the interchange of pairs of distances  $(d_i, \delta_i)$  and  $(d_{n-i}, \delta_{n-i})$ , i = 1, 2, ..., n - 1, does not change the value of IMSPE  $(\widehat{Y})$ .

7 Theorem 2.3 gives us some idea of the behaviour of the optimal design with respect to the IMSPE criterion.

**Corollary 2.4.** The optimal design with respect to the IMSPE criterion is symmetric, that is if the optimum of IMSPE  $(\widehat{Y})$  is reached at  $(d_1^*, d_2^*, \dots, d_{n-1}^*, \delta_1^*, \delta_2^*, \dots, \delta_{n-1}^*)$  then  $d_i^* = d_{n-i}^*$  and  $\delta_i^* = \delta_{n-i}^*$ ,  $i = 1, 2, \dots, n$ .

**Example 2.5.** Consider a five-point design, that is n = 5 and  $s_1 = t_1 = 0$ ,  $s_5 = t_5 = 1$ . By Corollary 2.4, for the optimal design we have  $d_1^* = d_4^*$ ,  $d_2^* = d_3^*$  and  $\delta_1^* = \delta_4^*$ ,  $\delta_2^* = \delta_3^*$ . In Fig. 2 the values of  $d_1^*$ ,  $d_2^*$  and  $\delta_1^*$ ,  $\delta_2^*$  are plotted as functions of correlation parameters  $\alpha$  and  $\beta$  both varying between 0 and 3. We remark that by symmetry,  $d_1^* + d_2^* = \delta_1^* + \delta_2^* = 1/2$ .

#### **3.** The optimal information gain for a shifted OU sheet

Another approach to optimal design is to find locations which maximize the amount of information obtained. Following the ideas of Shewry and Wynn (1987), one has to maximize the entropy  $Ent(\mathbf{Y})$  of the observations corresponding to the chosen design, which in the Gaussian case form an *n*-dimensional normal vector with covariance matrix  $\sigma^2 C(n, r)$ , that is

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$$\operatorname{Ent}(\mathbf{Y}) = \frac{n}{2} \left( 1 + \ln(2\pi\sigma^2) \right) + \frac{1}{2} \ln \det C(n,$$

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**Theorem 3.1.** Under the conditions of Theorem 2.1, entropy Ent(**Y**) has the form

$$\operatorname{Ent}(\mathbf{Y}) = \frac{n}{2} \left( 1 + \ln(2\pi\sigma^2) \right) + \frac{1}{2} \sum_{i=1}^{n-1} \ln\left(1 - q_i^2\right).$$
(3.1)

For any sample size, the equidistant design when values  $\alpha d_i + \beta \delta_i$ , i = 1, 2, ..., n-1 (and in this way  $q_i$ ), are constant is optimal with respect to the entropy criterion.

**Remark 3.2.** Observe that the equispaced monotonic design  $d_1 = d_2 = \cdots = \delta_n$  clearly optimizes the entropy criterion.

Remark 3.3. If the design space  $\mathcal{X}$  is the unit square then the optimal value of the entropy equals

<sup>25</sup> 
$$\frac{n}{2}\left(1+\ln(2\pi\sigma^2)\right)+\frac{n-1}{2}\ln\left(1-\exp\left(-(\alpha+\beta)/(n-1)\right)\right)\to-\infty \quad \text{as } n\to\infty.$$

#### Table 1

IMSPE values corresponding to the optimal and to the equispaced monotonic design and relative efficiency of the equispaced monotonic design.

n		$\alpha = 0.5, \beta = 0.8$	$\alpha = 1, \beta = 1$	$\alpha = 1, \beta = 10$	$\alpha = 2.5, \beta = 1.5$	$\alpha = 3, \beta = 3$
4	Optimal	0.2602	0.4008	0.9266	0.6549	0.8487
	Equispaced	0.2693	0.4010	0.9326	0.6598	0.8493
	Rel. eff. (%)	96.62	99.95	99.36	99.26	99.93
5	Optimal	0.2309	0.3699	0.8290	0.5981	0.7866
	Equispaced	0.2473	0.3700	0.8409	0.6065	0.7873
	Rel. eff. (%)	93.37	99.97	98.58	98.62	99.91
6	Optimal	0.2130	0.3529	0.7593	0.5640	0.7502
	Equispaced	0.2351	0.3530	0.7766	0.5763	0.7509
	Rel. eff. (%)	90.60	99.97	97.77	97.87	99.91
7	Optimal	0.2007	0.3423	0.7066	0.5241	0.7269
	Equispaced	0.2274	0.3424	0.7288	0.5571	0.7275
	Rel. eff. (%)	88.26	99.97	96.95	94.08	99.92
8	Optimal	0.1692	0.3351	0.6655	0.5007	0.7111
	Equispaced	0.2222	0.3352	0.6918	0.5441	0.7115
	Rel. eff. (%)	76.15	99.97	96.20	92.02	99.94
9	Optimal	0.1620	0.3300	0.6325	0.4858	0.6997
	Equispaced	0.2184	0.3301	0.6626	0.5348	0.7001
	Rel. eff. (%)	74.18	99.97	95.46	90.84	99.94
10	Optimal	0.1570	0.3262	0.6057	0.4756	0.6912
	Equispaced	0.2155	0.3262	0.6390	0.5278	0.6915
	Rel. eff. (%)	72.87	99.98	94.79	90.11	99.95

#### Table 2

Optimal four-point designs with respect to the IMSPE criterion.

	$\alpha = \beta = 0.5$	$\alpha = \beta = 1$	$\alpha = \beta = 1.5$
$d_1 = \delta_1$	0.3372	0.3401	0.3421
$d_2 = \delta_2$	0.3256	0.3199	0.3158
$d_3 = \delta_3$	0.3372	0.3401	0.3421

#### 4. Numerical experiments

#### 4.1. Comparison of the IMSPE criterion and the entropy criterion

In order to compare the performances of the two criteria we compare the optimal values of  $IMSPE(\widehat{Y})$  calculated using the fmincon function of Matlab to its values corresponding to the equispaced monotonic design which is optimal for the entropy criterion. In Table 1 the values of IMSPE are given for both designs together with the relative efficiency of the equispaced monotonic design with respect to the optimal one for various sample sizes and combinations of parameters  $(\alpha, \beta)$ . Unfortunately, larger sample sizes cause technical problems in optimization, since for *n* design points one has to find numerically the constrained minimum of functions with 2n - 2 parameters.

Observe that for symmetric models when  $\alpha = \beta$ , the efficiency of the equispaced monotonic design is nearly 100%, while for different covariance parameters it reduces significantly. However, even in this special case the optimal designs with respect to the IMSPE and entropy criteria do not coincide. As an example, consider Table 2 where distances  $d_i$  and  $\delta_i$  corresponding to the optimal four-point design are given for three different values of  $\alpha = \beta$ . Obviously, in all three cases we have  $d_1 + \delta_1 \neq d_2 + \delta_2$ , so according to Theorem 3.1 these designs cannot be optimal with respect to the entropy criterion.

#### 4.2. IMSPE on a monotonic set and on a regular grid

In Theorem 2.1, the exact form of IMSPE is derived only for designs satisfying *Condition D*. However, one might ask what is the relative efficiency of the optimal value of IMSPE on monotonic sets containing  $n = m^2$  design points compared to the IMSPE of a regular grid with the same number of points. Table 3 gives the optimal values of IMSPE on monotonic sets, IMSPE values for regular designs and the relative efficiencies of the optimal IMSPE values on monotonic sets for different sample sizes and combinations of parameters ( $\alpha$ ,  $\beta$ ). Observe, that for four points the optimal monotonic design gives much better IMSPE values than the regular grid and for  $\alpha = \beta = 3$  the relative efficiency is slightly above 100% even in the case n = 9.

#### 5. Conclusion

We derive the exact form of the IMSPE for an OU sheet on a monotonic set. We show that the optimal design for the prediction based on IMSPE may differ substantially from the equidistant one. This is in contrast both to the optimal design

Table 3

IMSPE values corresponding to the optimal monotonic and to the regular grid design and relative efficiency of the optimal monotonic design.

n		$\alpha = 0.5, \beta = 0.8$	$\alpha = 1, \beta = 1$	$\alpha = 1, \beta = 10$	$\alpha = 2.5, \beta = 1.5$	$\alpha = 3, \beta = 3$
4	Monotonic	0.2602	0.4008	0.9266	0.6549	0.8487
	Regular	0.3580	0.5389	1.1449	0.8370	1.0094
	Rel. eff. (%)	137.59	134.46	123.56	127.81	118.93
9	Monotonic	0.1620	0.3300	0.6325	0.4858	0.6997
	Regular	0.1527	0.3018	0.5762	0.4850	0.7011
	Rel. eff. (%)	94.26	91.45	91.10	99.84	100.20

for estimation on a monotonic set (Baran and Stehlík, submitted for publication) and to the optimal design for the prediction of the OU process on a compact interval investigated by Baldi Antognini and Zagoraiou (2010). We also investigate the properties of the optimal design with respect to the entropy criterion, where constraining sample points from a rectangle to a monotonic set, as expected, decreases the entropy of the Gaussian field. Simulations illustrate selected cases of optimal designs for small number of sampling locations. Since the above discussed designs depend on the values of the correlation parameters, the optimal designs obtained are only locally optimal. We briefly study the dependence of the designs obtained on these parameters, too. Such knowledge may be crucial for an experimenter for increasing the efficiency of a design in a practical set-up.

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#### 16 Appendix

#### A.1. Proof of Theorem 2.1

To shorten our formulae, in what follows instead of  $\rho(x, s_i, t_i)$  we are using simply  $\rho_i$ , i = 1, 2, ..., n. Consider first MSPE  $(\widehat{Y}(x))$  given by (2.1). Short matrix algebraic calculations show that

$$\begin{bmatrix} \mathbf{0} & \mathbf{1}_n^\top \\ \mathbf{1}_n & C(n,r) \end{bmatrix}^{-1} = \begin{bmatrix} \mathbf{0} & \mathbf{0}_n^\top \\ \mathbf{0}_n & C^{-1}(n,r) \end{bmatrix} - \left(\mathbf{1}_n^\top C^{-1}(n,r)\mathbf{1}_n\right)^{-1} \begin{bmatrix} \mathbf{1} & -\left(C^{-1}(n,r)\mathbf{1}_n\right)^\top \\ -C^{-1}(n,r)\mathbf{1}_n & C^{-1}(n,r)\mathbf{1}_n\left(C^{-1}(n,r)\mathbf{1}_n\right)^\top \end{bmatrix}$$

and according to the results of Baran and Stehlík (submitted for publication) we have  $\mathbf{1}_n^\top C^{-1}(n, r)\mathbf{1}_n = 1 + \sum_{i=1}^{n-1} \frac{1-q_i}{1+q_i}$ . We remark that  $\mathbf{1}_n^\top C^{-1}(n, r)\mathbf{1}_n$  is the Fisher information on  $\theta$  based on **Y**. In this way, we obtain

<sup>23</sup> MSPE 
$$(\widehat{Y}(x)) = \sigma^2 \left[ 1 - \mathcal{Q}^\top(x)C^{-1}(n,r)\mathcal{Q}(x) + \left(\mathbf{1}_n^\top C^{-1}(n,r)\mathbf{1}_n\right)^{-1} \left(1 - \mathcal{Q}^\top(x)C^{-1}(n,r)\mathbf{1}_n\right)^2 \right]$$

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$$=\sigma^{2}\left[1+\frac{\varrho_{1}^{2}-2\varrho_{1}\varrho_{2}q_{1}}{q_{1}^{2}-1}+\frac{\varrho_{n}^{2}}{q_{n-1}^{2}-1}-\sum_{i=2}^{n-1}\left(\frac{2\varrho_{i}\varrho_{i+1}q_{i}}{q_{i}^{2}-1}+\frac{\varrho_{i}^{2}(1-q_{i}^{2}q_{i-1}^{2})}{(q_{i}^{2}-1)(q_{i-1}^{2}-1)}\right)\right]$$
$$-\left(1+\sum_{i=1}^{n-1}\frac{1-q_{i}}{q_{i}^{2}-1}\right)^{-1}$$

$$-\left(1+\sum_{i=1}^{n}\frac{1}{1+q_i}\right)$$

$$\times \left(1 + \frac{\varrho_1 - (\varrho_1 + \varrho_2)q_1}{q_1^2 - 1} + \frac{\varrho_n}{q_{n-1}^2 - 1} - \sum_{i=2}^{n-1} \left(\frac{(\varrho_i + \varrho_{i+1})q_i}{q_i^2 - 1} + \frac{\varrho_i(1 - q_i^2q_{i-1}^2)}{(q_i^2 - 1)(q_{i-1}^2 - 1)}\right)\right)^2$$

$$= \sigma^{2} \left[ 1 - \varrho_{n}^{2} - \sum_{i=1}^{n-1} \frac{(\varrho_{i} - \varrho_{i+1}q_{i})^{2}}{1 - q_{i}^{2}} + \left( 1 + \sum_{i=1}^{n-1} \frac{1 - q_{i}}{1 + q_{i}} \right)^{-1} \left( 1 - \varrho_{n} - \sum_{i=1}^{n-1} \frac{\varrho_{i} - \varrho_{i+1}q_{i}}{1 + q_{i}} \right)^{2} \right].$$

<sup>28</sup> Further, according to the definition of the IMSPE criterion, we can write

<sup>29</sup> IMSPE 
$$(\widehat{Y}) = 1 - A_n + \left(1 + \sum_{i=1}^{n-1} \frac{1 - q_i}{1 + q_i}\right)^{-1} B_n,$$

where

$$A_{n} \coloneqq \int_{\mathcal{X}} \mathcal{Q}^{\top}(x) C^{-1}(n, r) \mathcal{Q}(x) dx = \operatorname{tr} \left[ C^{-1}(n, r) \mathcal{R} \right],$$
  

$$B_{n} \coloneqq 1 - 2 \mathbf{1}_{n}^{\top} C^{-1}(n, r) \mathcal{W} + \mathbf{1}_{n}^{\top} C^{-1}(n, r) \mathcal{R} C^{-1}(n, r) \mathbf{1}_{n},$$
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with

$$\mathcal{W} = (\omega_1, \dots, \omega_n)^\top := \int_{\mathcal{X}} \mathcal{Q}(x) dx \quad \text{and} \quad \mathcal{R} = \left\{ R_{i,j} \right\} := \int_{\mathcal{X}} \mathcal{Q}(x) \mathcal{Q}^\top(x) dx.$$

Obviously,

$$\omega_{i} = \frac{1}{\alpha\beta} \left[ 2 - e^{-\alpha s_{i}} - e^{-\alpha(1-s_{i})} \right] \left[ 2 - e^{-\beta t_{i}} - e^{-\beta(1-t_{i})} \right]$$

$$= \frac{1}{\alpha\beta} \left[ 2 - e^{-\alpha(d_1 + \dots + d_{i-1})} - e^{-\alpha(d_i + \dots + d_{n-1})} \right] \left[ 2 - e^{-\beta(\delta_1 + \dots + \delta_{i-1})} - e^{-\beta(\delta_i + \dots + \delta_{n-1})} \right],$$

$$R_{i,j} = \left[ \frac{1}{2\alpha} \left( 2e^{-\alpha|s_i - s_j|} - e^{-\alpha(s_i + s_j)} - e^{-\alpha(2 - s_i - s_j)} \right) + |s_i - s_j| e^{-\alpha|s_i - s_j|} \right]$$

$$\times \left[ \frac{1}{2\beta} \left( 2e^{-\beta|t_i - t_j|} - e^{-\beta(t_i + t_j)} - e^{-\beta(2 - t_i - t_j)} \right) + |t_i - t_j| e^{-\beta|t_i - t_j|} \right]$$

$$= \left[\frac{1}{2\alpha} \left(2e^{-\alpha(d_{i\wedge j} + \dots + d_{i\vee j-1})} - e^{-\alpha(2d_1 + \dots + 2d_{i\wedge j-1} + d_{i\wedge j} + \dots + d_{i\vee j-1})} - e^{-\alpha(d_{i\wedge j} + \dots + d_{i\vee j-1} + 2d_{i\vee j} + \dots + 2d_{n-1})}\right)\right]$$

+ 
$$(d_{i\wedge j} + \dots + d_{i\vee j-1})e^{-\alpha(d_{i\wedge j} + \dots + d_{i\vee j-1})}$$

$$\times \left[\frac{1}{2\beta} \left(2e^{-\beta(\delta_{i\wedge j}+\dots+\delta_{i\vee j-1})} - e^{-\beta(2\delta_1+\dots+2\delta_{i\wedge j-1}+\delta_{i\wedge j}+\dots+\delta_{i\vee j-1})} - e^{-\beta(\delta_{i\wedge j}+\dots+\delta_{i\vee j-1}+2\delta_{i\vee j}+\dots+2\delta_{n-1})}\right)\right]$$
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+ 
$$(\delta_{i\wedge j} + \dots + \delta_{i\vee j-1})e^{-\beta(\delta_{i\wedge j} + \dots + \delta_{i\vee j-1})}$$
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where  $i \land j := \min\{i, j\}, i \lor j := \max\{i, j\}, i, j \in \mathbb{N}$ , and the empty sum is defined to be zero. In this way, we obtain

$$A_{n} = R_{n,n} + \sum_{i=1}^{n-1} \frac{R_{i,i} - 2R_{i+1,i}q_{i} + R_{i+1,i+1}q_{i}^{2}}{1 - q_{i}^{2}} = R_{1,1} + \sum_{i=1}^{n-1} \frac{R_{i,i}q_{i}^{2} - 2R_{i+1,i}q_{i} + R_{i+1,i+1}}{1 - q_{i}^{2}},$$
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$$\begin{split} B_n &= 1 - 2\omega_n - 2\sum_{i=1}^{n-1} \frac{\omega_i - \omega_{i+1}q_i}{1+q_i} + R_{n,n} \\ &+ 2\sum_{i=1}^{n-1} \frac{R_{n,i} - R_{n,i+1}q_i}{1+q_i} + \sum_{i=1}^{n-1} \sum_{j=1}^{n-1} \frac{R_{i,j} - R_{i+1,j}q_i - R_{i,j+1}q_j + R_{i+1,j+1}q_iq_j}{(1+q_i)(1+q_j)} \\ &= 1 - 2\omega_n + R_{n,n} + \sum_{i=1}^{n-1} \left( \frac{R_{i,i} - 2R_{i+1,i}q_i + R_{i+1,i+1}q_i^2}{(1+q_i)^2} + 2\frac{(R_{n,i} - \omega_i) - (R_{n,i+1} - \omega_{i+1})q_i}{1+q_i} \right) \\ &+ 2\sum_{i=2}^{n-1} \sum_{j=1}^{i-1} \frac{R_{i,j} - R_{i+1,j}q_i - R_{i,j+1}q_j + R_{i+1,j+1}q_iq_j}{(1+q_i)(1+q_j)}. \end{split}$$

#### A.2. Proof of Theorem 2.3

Let  $\widetilde{d}_i := d_{n-i}, \widetilde{\delta}_i := \delta_{n-i}, \widetilde{q}_i := \exp\left(-\alpha \widetilde{d}_i - \beta \widetilde{\delta}_i\right), i = 1, 2, ..., n-1$ , and denote by  $\widetilde{\omega}_k$  and  $\widetilde{R}_{k,\ell}$  the values calculated from (2.5) and (2.6), respectively, using distances  $(\widetilde{d}_i, \widetilde{\delta}_i), i = 1, 2, ..., n-1$ . Further, let  $q_i, \omega_k$  and  $R_{k,\ell}$  denote the corresponding quantities calculated from the original distances  $(d_i, \delta_i), i = 1, 2, ..., n-1$ . It is easy to see that

$$\widetilde{q}_i = q_{n-i}, \quad i = 1, 2, \dots, n-1, \quad \text{and} \quad \widetilde{\omega}_k = \omega_{n-k+1}, \qquad R_{k,\ell} = R_{n-k+1,n-\ell+1}, \quad k, \ell = 1, 2, \dots, n,$$
(A.1)

and in this way we obtain

$$\sum_{i=1}^{n-1} \frac{1 - \widetilde{q}_i}{1 + \widetilde{q}_i} = \sum_{i=1}^{n-1} \frac{1 - q_i}{1 + q_i}.$$

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- completes the proof.  $\Box$
- A.3. Proof of Theorem 3.1
- According to the results of Baran and Stehlík (submitted for publication), 5

$$C(n,r) = \begin{bmatrix} 1 & q_1 & q_1q_2 & q_1q_2q_3 & \cdots & \cdots & \prod_{i=1}^{n-1} q_i \\ q_1 & 1 & q_2 & q_2q_3 & \cdots & \cdots & \prod_{i=2}^{n-1} q_i \\ q_1q_2 & q_2 & 1 & q_3 & \cdots & \cdots & \prod_{i=3}^{n-1} q_i \\ q_1q_2q_3 & q_2q_3 & q_3 & 1 & \cdots & \cdots & \vdots \\ \vdots & \vdots & \vdots & \vdots & \ddots & \ddots & \vdots \\ \vdots & \vdots & \vdots & \vdots & \ddots & \ddots & q_{n-1} \\ \prod_{i=1}^{n-1} q_i & \prod_{i=2}^{n-1} q_i & \prod_{i=3}^{n-1} q_i & \cdots & \cdots & q_{n-1} & 1 \end{bmatrix}.$$

Hence, one can use the same type of decomposition as Baldi Antognini and Zagoraiou (2010, Lemma 3.1), that is

$$C(n, r) = LDL^{\top}$$

where *L* is a lower triangular matrix with entries 1 in its main diagonal and *D* is a diagonal matrix where in the diagonal we have  $(1, 1 - q_1^2, 1 - q_2^2, ..., 1 - q_{n-1}^2)$ . In this way 10

$$\det C(n, r) = \det D = \prod_{i=1}^{n-1} (1 - q_i^2),$$

which proves (3.1). 12

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In order to find the optimal design one has to find the constrained maximum of 13

$$F(q_1, q_2, \dots, q_{n-1}) := \sum_{i=1}^{n-1} \ln(1 - q_i^2) \quad \text{under condition } \sum_{i=1}^{n-1} \ln q_i = -\alpha - \beta.$$

By analysing the first partial derivatives and the Hessian of the Lagrange function 15

$$\Lambda\left(q_{1}, q_{2}, \ldots, q_{n-1}; \lambda\right) := \sum_{i=1}^{n-1} \ln\left(1-q_{i}^{2}\right) + \lambda\left(\sum_{i=1}^{n-1} \ln q_{i} + \alpha + \beta\right)$$

one can easily see that the maximum is reached when  $q_1 = q_2 = \cdots = q_{n-1}$ , which completes the proof.  $\Box$ 17

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