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### Short communication

### Integration of ground aerogel particles as chromatographic stationary phase into microchip

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### <sup>19</sup> **1. Introduction**

 Porous bed is the heart of chromatography since the most essen- tial feature of the chromatographic process is the percolation of the liquid or gas (mobile phase) through the stationary phase [\[1\].](#page-5-1) To achieve high peak resolution, the contact surface area between the stationary and mobile phases, as well as the permeable intra- particle pore space should be as large as possible. That can be reached either by using small chromatographic particles or porous 27 monolithic columns, However, the hydraulic resistance of the bed to the stream of mobile phase should be moderate. The best chro-29 matographic stationary phases have a high volume of through pores 30 and low hydraulic resistance. One of the main trends in chro- matography is to develop new monolithic stationary phases [\[1–3\],](#page-5-1) because those seem to meet quite well the mentioned demands. However, there are some disadvantages of the monolith columns, too: possible wall effects [\[1,4\],](#page-5-1) problems in reproducibility and characterization of the manufactured columns.

<sup>36</sup> Monolithic silica aerogels differ from traditional silica gels and 37 from the chromatographic monoliths significantly both in struc-<sup>38</sup> ture and porosity and can be created by a special supercritical <sup>39</sup> drying technology [\[5\].](#page-5-1) Silica aerogels hold records for the lowest 40 bulk density of any solid materials (as low as  $0.003-0.5$   $\rm g/cm^3$ ), <sup>41</sup> the highest specific surface area of any monolithic materials (up to 1600 m<sup>2</sup>/g) and they show unique characteristics in mechanical, <sup>43</sup> acoustical, thermal, optical and many other fields [\[6\]. C](#page-5-1)ontrary to 44 their extremely high internal porosity (90-95 v/v%), monolithic sil-

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### **ABSTRACT**

C16 modified and ground monolithic silica aerogel particles in submicrometer size, as a new type of stationary phase was prepared and integrated in polydimetilsiloxane (PDMS) microchip. The aerogel particles were packed into the microfluidic channel using a simple procedure, which does not require any special frit or fabrication step to retain the particles. The subnanoliter volume of samples can be transported through the porous, short length of packing with low pressure (<3 bar). Food dyes as test components could be separated using low pressure within 6 s. A 50-fold preconcentration could be achieved by retaining 100 nL volume of sample on the packing and elution with methanol.

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ica aerogels have not yet been used in any kind of chromatographic 45 separations as stationary phases.  $46$ 

Nowadays there is a high demand for miniaturized chromatographic techniques that would provide the same very versatile 48 applications that have been found in liquid chromatography (LC). 49 However, only a few chip-based chromatographic systems have  $\frac{50}{50}$ been reported so far as compared to chip-based capillary elec-<br>51 trophoretic (CE) devices, which is mainly due to technical problems  $52$ inherent in the former [\[7,8\]. M](#page-5-1)ost microfluidic devices are based on  $53$ open tubular flow designs and only a few involve packed-bed chips  $_{54}$ due to the difficulty in preparing frits [\[9,10\]. R](#page-5-1)ecently, this prob- <sup>55</sup> lem has been excellently addressed [\[11\], h](#page-5-1)owever, the high-tech  $_{56}$ manufacturing of the three-laminated polyimide layers chip (use 57 of laser, micromachined frit) is not possible for the large majority  $\frac{58}{58}$ of the researchers.  $\frac{59}{200}$ 

In our recent work we described the fabrication of a PDMS-based  $60$ microfluidic chip containing reversed-phase silica beads without 61 the use of frits or other barriers and different retaining and stabi- 62 lizing effects appearing in the packed channel have been observed  $\qquad \quad$  63 [\[12\]. I](#page-5-1)n this work we demonstrate a new procedure to pack submi-<br><sup>64</sup> crometer particles into a part of the microfluidic channel, and for 65 the first time to prepare and test ground silica arogel particles as  $66$ stationary phase for low-pressure chromatography.  $67$ 

### **2. Experimental** 68

2.1. Preparation of C16-functionalized monolithic silica aerogel and obtaining submicrometer size particles from it  $\frac{1}{20}$  70

A solution of tetramethoxysilane (TMOS, 2.25 ml) and hexadecyl trimethoxysilane (HDTMOS 0.250 ml) in methanol (9.90 ml) was  $\frac{72}{12}$ 

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Fig. 1. (a) SEM image of the porous structure of a monolitic silica aerogel. (b) Photo of a block of C16 silica aerogel (0.091 g/cm<sup>3</sup>). Aerogel particles powdered in a ball mill and suspended in methanol (c) and the clear liquid above the suspension after 20 min sedimentation (d).

 stirred well with a dimethyl formamide (19.8 ml) solution of aque- ous ammonia solution (3.30 ml, 25 m/m%-os) and deionized water (2.50 ml) then poured into a tubular plastic mold, sealed and let to stand at room temperature for two days. The alcogel monolith was transfered to a 500 ml volume glass container and soaked first in methanol, then in methanol–acetone mixtures and in acetone, for at least one day in each solvent. The alcogel was then transfered  $\frac{1}{20}$  into a 1.4 dm<sup>3</sup> volume supercritical CO<sub>2</sub> dryer under acetone. After sealing the extractor body, acetone was drained. The remaining ace- tone content of the alcogel was then replaced with liquid carbon 83 dioxide in a slow stream of liquid carbon dioxide at room temperature in 18 h. After 2 h of conditioning at 80 $\degree$ C the pressure was slowly released in a 4 h period of time. The density of the monolith <sup>86</sup> proved to be 0.091 g/cm<sup>3</sup>. The porous structure and a block of the 87 prepared C16 monolithic silica aerogel are shown in Fig. 1a and b, 88 respectively.

 $_{89}$  About 1 cm<sup>3</sup> volume of the obtained aerogel was powdered in a <sup>90</sup> ball mill for 10 min, then stirred with 1 mL methanol in a Eppendorf 91 tube with a vortex mixer (Fig. 1c). After 10 min of sedimentation <sup>92</sup> the uppermost quarter of liquid layer was sucked to use for the 93 preparation of the chromatographic packing (Fig. 1d).

### <sup>94</sup> 2.2. Microchip fabrication

<sup>95</sup> The PDMS chips were prepared by using a mold created by soft 96 photolithography [\[13\]. T](#page-5-1)he pattern consisting of standard cross-97 T type channel of 100 μm wide was printed as a high resolution 98  $(10,000 \,\mathrm{dpi})$  photomask. Close to the crossing of channels, 10  $\mu$ m 99 wide line was drawn ([Fig. 2a\)](#page-3-0) to create a bottleneck in the chan-<sup>100</sup> nel (starting point to retain particles in the channel). Negative type

photoresist (SU-8 2025, Microchem, Newton, MA) was spin-coated 101 onto a  $\frac{3}{2}$ " silicon wafer at 3000 rpm for 30 s to a thickness of 30  $\mu$ m.  $\qquad$  102 The PDMS chip was fabricated by cast molding of a 10:1 mixture  $\frac{103}{103}$ of PDMS oligomer and cross-linking agent (Sylgard 184, Dow Corn- <sup>104</sup> ing, Midland, MI). The PDMS chip was sealed onto a glass slide of 105 1.2 mm thickness after oxygen plasma treatment (PDC-32G Har- <sup>106</sup> rick) [\(Fig. 2b\)](#page-3-0).  $107$ 

#### $2.3.$  Microscopy and image analysis  $108$

To observe the movement of liquids in the microchip channels 109 and to test the chromatographic characteristics of the packing, food 110 dyes (FD&C blue#1 and FD&C yellow#5, all from McCormick&Co., 111  $Inc_{x}$ , MD) were injected and transported in the chip using a low-<br>112 rate peristaltic pump (IPC, Ismatec). The movement of the plugs  $113$ was monitored by using an inverted microscope (Axio Observer 114 A1, Zeiss) equipped with a high speed CCD camera. SEM images 115 were taken on a Hitachi S-4300 CFE instrument.

### 2.4. Chromatographic separation in chip  $117$

The samples (0.5–100  $\mu$ L) were sucked into the peristaltic pump  $_{118}$ tubing (ID: 0.25 mm), which was initially filled with liquid (water  $119$ or eluent). This sample was split in the junction and a small volume  $120$ of the original sample was manipulated into the separation chan-<br>121 nel (approximately 0.5-100 nL). The sample injected at the sample 122 inlet port (port I in [Fig. 2b](#page-3-0)) flows into the other three channels  $123$ with different flow rates depending on the hydraulic resistance  $124$ of each channel. Because the hydraulic resistance in the separa-<br>125 tion channel of the used chip is estimated to be approximately one  $126$ 

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**Fig. 2.** (a) Part of the lithographic mask pattern about the crossing of channels and the 4  $\mu$ m wide line positioned close to the crossing to create a bottleneck in the chip (starting point to retain particles in the channel). (b) Photo of the microchip (I: sample inlet, O: separation outlet, O1 and O2 are outlet reservoirs. The suspension of particles is pumped from O during the packing, the sample solutions to be separated or preconcentrated are injected from I). Optical micrographs of the fluid channel with the frit-like bottleneck (c) and the created packing of ground silica aerogel particles (particles were pumped from O port (d)).

127 thousand times higher (that is the flow rate is one thousand times 128 smaller) than in the other channels, when one microliter of sam-<sup>129</sup> ple is injected into the chip with the peristaltic pump, only about <sup>130</sup> one nanoliter is injected in the separation channel; the majority of <sup>131</sup> the sample solution flows to the waste outlet reservoirs O1 and O2 <sup>132</sup> ([ESM Video 1\).](#page-5-1) This simple hydrodynamic injection of subnanoliter 133 volume of samples was characterized in our earlier work [\[12,14\].](#page-5-1)

<sup>134</sup> The packing was prepared daily, and it was preconditioned with 135 10 min washing with methanol and 5 min with the mobile phase <sup>136</sup> before chromatographic separation/preconcentration.

### <sup>137</sup> **3. Results and discussion**

### <sup>138</sup> 3.1. Packing

 In order to create a compact, homogeneous packing, a very dilute suspension of little particles was needed. Therefore, ground aerogel 141 particles were dispersed in methanol, homogenized and allowed to 142 be sedimented for 20 min. After that time the clear supernatant 143 layer, which contained the particles of 0.2–1  $\mu$ m diameter, was sucked out from above the dense sediment and used for packing ([Fig. 1d](#page-2-0)). A few microliters of solution sucked from the clear liq- uid layer was injected into the chip through the port O (outlet of 147 the separation channel of the chip) and transported toward the 148 bottleneck. At the bottleneck not only the width of the channel is 149 shortened to about 20  $\mu$ m, but also the height of the channel is 150 reduced from 30  $\mu$ m to about 5  $\mu$ m ("3D bottleneck"). The liquid could flow through the bottleneck without remarkable hydraulic resistance [\(ESM Video 2\),](#page-5-1) but the particles were retained. The first aerogel particles retained around the bottleneck, and then the newly arrived particles adhere smoothly to the packing; increas- ing its length continuously. The first particles acted as keystones, blocking the other particles. Earlier experiments demonstrated that it was only necessary to taper a rigid capillary [\[9\]](#page-5-1) or flexible  $\,$  microfluidic channel [12] to approximately 10  $\mu$ m (inner diameter)  $_{159}$  to achieve the *keystone effect* [\[9\]](#page-5-1) and to retain 3  $\mu$ m sized particles. It was observed that at the bottleneck, the particles were compressed

higher and higher resulting in a homogeneous, compact and dense 161 packing as shown in Fig. 2c and d, and [ESM Video 3. F](#page-5-1)inally, the 162 methanol was washed out by water. The methanol was washed out by water.

Some phenomena regarding the stability of the packing pre-<br>164 pared from conventional chromatographic beads were observed. 165 The hard particles adjacent to the wall deform the soft PDMS and  $166$ partially penetrate into the channel wall which acts as anchors  $167$ for the packing (anchor effect) [\[12\]. W](#page-5-1)hen the pumping pressure  $168$ (about  $1-2$  bar) was applied to compress the packing, the wall of the  $169$ channel was deformed (extended). During this period the particles 170 fill the enlarged volume of the channel and then the channel shrinks  $171$ when the pressure is released thereby forming a continuous strain 172 around the packing. The particles of the packing are compressed  $173$ by the forces of the elastic strains acting perpendicularly from the <sup>174</sup> wall toward the middle of the channel (clamping effect) [\[12\].](#page-5-1) 175

### 3.2. Chromatographic test 176

The C16 modified silica aerogel particles are expected to have 177 similar chromatographic features as the C18 conventional chro-<br>178 matographic beads. The blue food dye can be completely retained 179 on the aerogel packing in aqueous solution. The retained compo- <sup>180</sup> nent was not immobilized by washing with water, but it could 181 be immediately eluted with methanol. Therefore this component 182 could be effectively concentrated on the packing. When 100 nL vol-<br>183 ume of diluted dye sample was pumped toward the packing (about 184 300 s), the components were completely retained and concentrated 185 in the first 250  $\mu$ m length of the packing. The subsequent methano- $_{186}$ lic washing eluted the components merely in a  $2 \text{ nL}$  volume, that  $187$ is, about  $50\times$  concentration could be achieved. This concentration efficiency can be further increased if larger sample volume 189 is used (nevertheless, a few microliter volume of sample gener-<br>190 ally is available for an analysis). The overall extraction capacity 191 of the packing related to the blue component was calculated to 192 be 7.5  $\times$  10<sup>-11</sup> mol/ $\mu$ m packing (cross-section area of the packing: 193  $0.0035$  mm<sup>2</sup>). While in aqueous solution the blue food dye was  $194$ completely retained, the yellow dye was passed through the pack- <sup>195</sup>

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**Fig. 3.** Separation of food dyes (1: yellow, 2: blue) in chip packed with ground C16 modified silica aerogel particles. The water mobile phase was changed to methanol when sample plug was reached the packing. The flow rate in the separation channel was 0.2 nL/s.

<sup>196</sup> ing. Changing the mobile phase to methanol, the blue component <sup>197</sup> was washed out (Fig. 3).

 The two dye components could be separated under isocratic 199 condition, too. Using 35% methanol: water as mobile phase the dyes were eluted one after the other. A chromatographic packing of 1 mm length was suitable for the separation of 1 nL volume of the dye mixture (Fig. 4). Using the maximal pumping pressure with the peristaltic pump (about 3 bars), extremely fast separation has been achieved.

 High efficiency of separation can be obtained within a short sep- aration length only if the length of the injected sample plug ( $l_{\text{inj}}$ ) or the detector observation length ( $l_{\text{det}}$ ) can be shortened to a mini- mum.  $l_{\text{det}}$  could be kept minimal due to the microscopic detection in a single point (pixel) based on measuring the intensity of colors (RGB) at any part of the channel.

<sup>211</sup> In a hunt for the fastest chromatographic separation 0.5 mm <sub>212</sub> length of packing (L), 1 nL volume of sample (l<sub>inj</sub>: 250 µm) and the <sup>213</sup> maximal pressure of the peristaltic pump (3 bar) was applied ([ESM](#page-5-1) <sup>214</sup> [Video 4\).](#page-5-1) When right after the packing was detected almost base-<sup>215</sup> line separation was achieved within 8 s [\(Fig. 5c\)](#page-5-1). Since the thickness  $_{\rm 216}$  of the packing in the transparent PDMS chip is only 35  $\rm \mu m$ , the 217 dyes could be monitored and detected even through the packing  $_{\rm 218}$   $\,$  (Figs. 4a and b and 5a and b). While an only 200  $\rm \mu m$  travelling 219 through the packing could not result in complete separation yet,  $_{\rm 220}$   $\rm = 300\, \mu m$  length provided baseline separation of the dyes within 6 s. <sup>221</sup> The detection beyond the packing gives worse separation due to 222 the dispersion of the components ([Fig. 5d\)](#page-5-1).

### <sup>223</sup> **4. Conclusion**

<sup>224</sup> This is the first case reported so far when a silica aerogel <sup>225</sup> was used as a chromatographic stationary phase in a microchip. <sup>226</sup> The great advantage of ground monolithic aerogel particles over 227 other phases is the very high inner porosity ( $\varepsilon > 0.90 - 0.95$ ) and <sup>228</sup> the homogenous distribution of wide 10–100 nm mesopores which <sup>229</sup> form a dynamically readily accessible open pore system with a large <sup>230</sup> number of throupores. In comparison, the monolithic columns  $_{231}$  have approx. 2–3  $\mu$ m sized open channels and 10–13 nm meso-232 pores within the porons (with an overall porosity of  $\varepsilon = 0.85$ ), <sup>233</sup> while conventional silica-based stationary phases are character-234 ized with 6–15 nm mesopores and moderate porosity ( $\varepsilon$  = 0.62) 235 [\[16\].](#page-5-1) Although the solid macroscopic skeleton of the aerogel col-<sup>236</sup> lapsed when it got contact with any liquid (water), the average size 237 of the particles obtained after grinding and suspending was about <sub>238</sub> 0.2−1 μm.



**Fig. 4.** Optical micrographs of the silica aerogel packing during separation of food dye components using 35% methanol:water as mobile phase. The flow rate in the separation channel was 2 nL/s (maximal rate attainable by peristaltic pump). (Time between (a) and (d) is 8 s.)

The aerogel particles were packed into the microfluidic chan-<br>239 nel using a simple procedure, which does not require any special <sub>240</sub> frit to retain the particles. The bottleneck in the channel can be  $\frac{241}{2}$ easily created at any part of the microfluidic chip. The simplicity  $\qquad$  242 of replication of the PDMS chips and the minimal consumption of 243 the conventional packing particles (some tens of nanograms for a 244 10 mm length of packing) makes the chips inexpensive and dispos-<br>245 able. Since reversed-phase silica particles are widely used as the  $246$ stationary phase in HPLC and SPE, the described chip-based chromatographic system has great potential in many applications (e.g.  $248$ preconcentration, purification, separation). Further optimization of 249 the chromatographic separations would be beneficial.

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<span id="page-5-1"></span>

**Fig. 5.** Separation of food dyes in chip packed with ground C16 modified silica aerogel particles using 35% methanol:water as mobile phase. The color intensity measurement (detection) was carried out at 0.2 mm (a), 0.3 mm (b), 0.5 mm (c) and 1 mm (d) from the front part edge of the packing. The flow rate in the separation channel was 2 nL/s.

### <sup>251</sup> **[Q1](#page-0-0) Uncited reference**

### <sup>252</sup> [15].

### <sup>253</sup> **Acknowledgements**

<span id="page-5-0"></span><sup>254</sup> The authors gratefully acknowledge financial support obtained from the National Scientific Research Fund, Hungary (K75286, K76834) and TÁMOP 4.2.1./B-09/1/KONV-2010-0007 project. The 255 authors also would like to express their thank to L. Daróczi (UD) 256 for recording SEM images and H. Bereczki and M. Andrási (UD) for  $257$ help in preparation of the C16 silica aerogel and the PDMS chips,  $258$ respectively. 259

### **Appendix A. Supplementary data** 260

Supplementary data associated with this article can be found, in 261 the online version, at [doi:10.1016/j.chroma.2010.12.091.](http://dx.doi.org/10.1016/j.chroma.2010.12.091)

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