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Textversion	author

## 1 Distribution of stress state in the Nankai subduction zone, southwest

## 2 Japan and a comparison with Japan Trench

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41 Key Words: Stress state, Nankai subduction zone, Japan Trench, Ocean drilling

43	Abstract: To better understand the distribution of three dimensional stress states in the
44	Nankai subduction zone, southwest Japan, we review various stress-related
45	investigations carried out in the first and second stage expeditions of the Nankai Trough
46	Seismogenic Zone Experiment (NanTroSEIZE) by the Integrated Ocean Drilling Program
47	(IODP) and compile the stress data. Overall, the maximum principal stress $\sigma_1$ in the
48	shallower levels (< $\sim$ 1km) is vertical from near the center of forearc basin to near the
49	trench and; the maximum horizontal stress $S_{\mbox{\scriptsize Hmax}}$ (interpreted to be the intermediate
50	principal stress $\sigma_2$ ) is generally parallel to the plate convergence vector. The exception to
51	this generalization occurs along the shelf edge of the Nankai margin where $S_{\mathrm{Hmax}}$ is along
52	strike rather than parallel to the plate convergence vector. Reorientation of the principal
53	stresses at deeper levels (e.g., > $\sim$ 1km below seafloor or in underlying accretionary
54	prism) with $\sigma_1$ becoming horizontal is also suggested at all deeper drilling sites. We also

55 make a comparison of the stress state in the hanging wall of the frontal plate-interface 56 between Site C0006 in the Nankai and Site C0019 in the Japan Trench subduction zone 57 drilled after the 2011 Mw9.0 Tohoku-Oki earthquake. In the Japan Trench, the comparison between stress state before and after the 2011 mega-earthquake shows that 58 59 the stress changed from compression before the earthquake to extension after the 60 earthquake. As a result of the comparison between the Nankai Trough and Japan Trench, a similar current stress state with trench parallel extension was recognized at both 61 62 C0006 and C0019 sites. Hypothetically, this may indicate that in Nankai Trough it is still 63 in an early stage of the interseismic cycle of a great earthquake which occurs on the 64 décollement and propagates to the toe (around site C0006).

65

#### 66 1. Introduction

Stress and earthquakes are known to be interrelated: stress triggers earthquakes and
earthquakes alter the shear and normal stresses on surrounding faults (Stein, 1999;
Seeber and Armbruster, 2000; Hardebeck, 2004; Ma et al., 2005; Lin et al., 2007). On the
other hand, the stresses both on the fault and in the formation gradually build up in the
interseismic period (Kanamori and Brodsky, 2001). The Nankai Trough Seismogenic
Zone Experiment (NanTroSEIZE), a comprehensive scientific drilling project conducted

73	by the Integrated Ocean Drilling Program (IODP) in the Nankai subduction zone,
74	southwest Japan, is designed to investigate the mechanics of the subduction megathrust
75	through drilling and a wide range of allied studies (Tobin and Kinoshita, 2006; Tobin et
76	al., 2009a). In this area, Mw 8.0 class great earthquakes repeat at intervals of 100–200
77	years as a result of the convergence of the Philippine Sea and Eurasian plates (Ando,
78	1975; Fig. 1). The last two great earthquakes in the Nankai subduction zone occurred in
79	1944 (Tonankai, M 8.0-8.3) and 1946 (Nankai, M 8.1-8.4), generating tsunamis and
80	causing significant damage in southwest Japan (Kanamori 1972). The NanTroSEIZE
81	project sampled and continues to monitor the characteristics of the seismogenic zone
82	during the interseismic interval. In contrast, IODP expedition 343 to the Japan Trench
83	(also referred to as the Japan Trench Fast Drilling Project or JFAST), was conducted just
84	after a great earthquake, about 13 months after the 2011 Mw 9.0 Tohoku-Oki, Japan
85	earthquake (Mori et al., 2012; Chester et al., 2012; Fig. 1).
86	Establishing the in situ stress state along active subduction zones is critical for

understanding the accumulation and release of most of Earth's seismic energy (Lallemand and Funiciello, 2009). Determination of in situ stress is one of the most important scientific objectives of both NanTroSEIZE and JFAST, and also one of the major goals of the IODP as the seismogenic parts of plate margins are often only

91	accessible through drilling. First, we review various stress-related investigations carried
92	out in association with NanTroSEIZE stages 1 and 2. We then compare the present-day
93	stress states in the frontal part of the plate-interface at the Nankai and Japan Trench
94	subduction zones and propose hypotheses on the temporal and spatial evolution of
95	stresses in the frontal plate-interface in Nankai, SW Japan.
96	
97	2. Stress estimates and direct measurements from stage 1 and 2 of the
98	NanTroSEIZE drilling project
99	The multi-stage scientific drilling project NanTroSEIZE, conducted by the drilling vessel
100	D/V Chikyu, began in 2007 with IODP expedition 314 and is continuing with planned
101	deep riser drilling in the coming years (Kinoshita et al., 2008; Hirose et al., 2013). To
102	date more than 10 drilling sites have been drilled along the NanTroSEIZE transect with
103	at least one vertical borehole(s) at each site. This transect is approximately orthogonal
104	to the Nankai Trough axis (plate boundary) (Fig. 2, 3 and 4a and Table 1).
105	In the first stage of NanTroSEIZE (2007–2008), borehole wall images obtained by
106	logging while drilling (LWD) technology yielded regional patterns of stress orientations
107	and magnitudes through observations of drilling-induced compressive failures

108 (borehole breakouts) and tensile fractures (DITFs) (e.g., Tobin et al., 2009b; Chang et al,

109 2010; Lin et al., 2010a; Moore et al., 2011; Lee et al., 2013). This stage involved five 110 drilling sites in three structural settings in which LWD was performed: the frontal thrust 111 at the toe of the accretionary prism, Site C0006; the megasplay hanging wall and 112 footwall, Sites C0010, C0004 and C0001, and the seaward edge of the Kumano forearc 113 basin, Site C0002 (Fig. 2, 3 and 4a). These regional studies were followed by more 114 detailed core-based analyses and geophysical studies, including interpretation of 115 high-resolution seismic reflection data and S-wave splitting that provided a 116 three-dimensional understanding of the stress field and the evolution of stresses 117 through time (Byrne et al., 2009; Kimura et al., 2011; Tsuji et al., 2011a; Lewis et al., 118 2013; Moore et al., 2013; Sacks et al., 2013; Conin et al., 2014). Taken together, these 119 results show that at all sites except C0004 and C0010, the maximum principal stress  $\sigma_1$ 120 is vertical at shallow levels and that the orientation of the intermediate principal 121 stress  $\sigma_2$  changes from trench perpendicular at C0006 and C0001 to trench parallel at 122 C0002. At sites C0004 and C0010  $\sigma_1$  is interpreted possibly to be horizontal and 123 approximately parallel to the plate convergent direction. 124 In the second stage of NanTroSEIZE (2009-2010), D/V Chikyu carried out the first

riser drilling in IODP history at Site C0009 of Expedition 319. This expedition targeted

126 the hanging wall above the high slip region of the 1944 Tonankai earthquake (Saffer *et* 

127	al., 2009). The borehole penetrated the Kumano forearc basin sediments and the
128	underlying accretionary prism; and was the deepest drilling ( $\sim$ 1.6 km) during the first
129	and second stages of NanTroSEIZE. In a depth range from approximately 700 mbsf
130	(meters below seafloor) to the target depth of 1600 mbsf, wireline logging included a
131	borehole caliper and a fullbore formation microimager (FMI) that provided resistivity
132	images. From the borehole images and caliper data, borehole breakouts and DITFs were
133	identified and the horizontal stress orientations were obtained (Saffer et al., 2009; Lin et
134	al., 2010a; Wu et al., 2012). Due to limited azimuthal coverage ( $\sim$ 50%) of the wellbore
135	walls by FMI, the width of breakouts was not well constrained, and therefore no reliable
136	information about stress magnitudes could be extracted from the wellbore failures.
137	The first hydraulic fracturing experiments in the scientific ocean drilling history
138	also were carried out using two techniques at Site C0009. The first, an "extended leak-off
139	test", was conducted as part of drilling operations and provided a measurement of
140	minimum principal stress magnitude at $\sim$ 708 mbsf (Saffer et al., 2013; Lin et al., 2008).
141	The second technique, a "two dual-packer hydraulic fracture test" was conducted using
142	Modular Dynamic Tester (MDT) tool (Ito et al., 2013; Saffer et al., 2013; Haimson and
143	
110	Cornet, 2003), and yielded two additional measurements of in situ minimum principal

145 Drill core samples were also recovered in a ~80m depth interval in mudstones 146 interpreted as either the uppermost accretionary prism or a paleo-slope basin. Anelastic 147 strain recovery (ASR) measurements on core samples were used to determine the 148 three-dimensional stress orientations by the same method as Byrne et al. (2009) (Lin et al., 2010b). In addition, results of a "walkaround" vertical seismic profiling (VSP) 149 150 experiment recorded at Site C0009 and conducted by D/V Chikyu and R/V Kairei showed 151 a clear anisotropy in P wave velocity and amplitude, and documented S wave splitting. 152 These data have also been interpreted as indicators of horizontal stress orientations 153 (Tsuji et al., 2011b).

154 During IODP expeditions 322 in stage 2, two reference sites were drilled on the 155 incoming Philippine Sea Plate: Site C0012, located ~31 km seaward of the trench on 156 basement high to sample a condensed sedimentary section, and Site C0011, ~22 km 157 seaward of the trench designed to sample the section at a basement low. LWD resistivity images documented borehole breakouts and provide an indication of horizontal 158 159 principal stress orientations at Site C0011 (Expedition 322 Scientists, 2010; Wu et al., 160 2013). Site C0012 was not drilled with LWD; however, ASR measurements on core 161 samples yielded constraints on stress states in both the oceanic crust (basalt) and the 162 sedimentary cover (Yamamoto et al., 2013).

# 164 3. Results of Stage 1 drilling, Nankai subduction zone, SW Japan

*3.1. C0001* 

166	Borehole breakouts, tensile fractures and core-scale faults are present in the upper half
167	of the boreholes at Site C0001 and provide constraints on the orientation, ratios and
168	magnitudes of the principal stresses (Expedition 314 Scientists, 2009a). The maximum
169	horizontal stress $S_{\text{Hmax}}$ orientation determined from borehole breakouts and tensile
170	fractures consistently trend $\sim$ 335° throughout the hole, although Chang et al. (2010)
171	proposed that the stress regime changes with depth, likely due to increasing $S_{\mbox{\scriptsize Hmax}}$ (Fig.
172	2). At shallow levels (<~500 mbsf) $S_{\text{Hmax}}$ is interpreted to be $\sigma_2$ and smaller in
173	magnitude than the vertical stress, reflecting a normal faulting regime. Consolidation
174	and triaxial compression tests of slope sediments in the uppermost $\sim 200$ mbsf also
175	suggest horizontal effective stresses are $\sim$ 41% of the vertical effective stress consistent
176	with a normal faulting regime (Song et al., 2011). Stress inversion of core-scale faults
177	from C0001 provide a measure of the three-dimensional stress state at relatively
178	shallow levels and also show normal faulting with extension parallel to the margin
179	(Lewis et al., 2013). These results are consistent with faulting patterns observed in
180	seismic reflection data as well as with the borehole breakout data that show $\sigma_2$

181	subparallel to the plate convergence vector. Lewis et al. (2013) also recognized an older
182	suite of faults that, when inverted for stress orientations, show $\sigma_1$ trending northwest,
183	parallel to the plate convergence vector. Chang et al. (2010) interpret $S_{\text{Hmax}}$ at deeper
184	levels (>~500 mbsf) to be $\sigma_1$ , reflecting a change with depth from normal faulting to
185	strike-slip, or possibly thrusting. Unfortunately, sediment cores were not retrieved from
186	deeper levels where the principal stresses appear to permutate.
187	<i>3.2. C0002</i>
188	Site C0002, which penetrated the Kumano forearc basin and the upper part of the
189	underlying accretionary prism, also shows a consistent orientation of borehole
190	breakouts with depth and a possible permutation of stresses with depth. $S_{\mbox{\scriptsize Hmax}}$
191	determined from breakouts, however, trend northeast, approximately perpendicular to
192	$S_{Hmax}$ at C0001, which is only 10 km to the southeast (Fig. 2 and 3). Analysis of the
193	breakouts, results from ASR experiments and inversion of core-scale faults show a
194	normal faulting regime in the forearc sequence with the minimum principal stress $\sigma_{3}$
195	nearly parallel to the plate convergence vector and perpendicular to the shelf break.
196	These results are consistent with numerous margin parallel normal faults observed in
197	seismic reflection data (Gulick et al., 2010; Moore et al., 2013; Sacks et al., 2013). Many
198	of the faults also cut the seafloor, suggesting that they are active or recently active, and

199 the lack of growth data suggests that the transition to an extension dominated basin 200 occurred less than ~1 Ma ago (Gulick et al, 2010). Sacks et al. (2013) and Moore et al. 201 (2013) also show that there is a systematic change from any an early phase of generally 202 trench-parallel extension that started before 0.44 Ma to trench-normal extension 203 associated with faults that often cut the seafloor. These results are consistent with 204 observations of core-scale fault populations that show a change from NE-SW extension 205 to NW-SE extension (Expedition 315 Scientists, 2009). Chang et al. (2010) propose that 206 the stress regime changes below the forearc sediments with  $S_{Hmax}$  becoming  $\sigma_1$ , 207 suggesting a change from normal faulting to strike-slip or thrusting similar to the change 208 proposed for Site C0001. The stress states at the two sites, however, are still 209 fundamentally different as the borehole breakouts, and therefore S<sub>Hmax</sub>, are 210 perpendicular even at the deepest structural levels. In fact, the trend of S<sub>Hmax</sub>, which is 211 interpreted to be  $\sigma_1$  in the deeper levels of C0002, suggests margin-parallel shortening 212 rather than margin perpendicular shortening as interpreted for the deeper levels of 213 C0001 (Fig. 2).

**214** *3.3. C0004* 

Site C0004 penetrated the megasplay fault, which appears to have slipped coseismicallyduring the 1944 earthquake (Sakaguchi et al., 20011b) and borehole breakouts show

11

217 consistent trends throughout the hole with SHmax trending northwest-southeast, 218 approximately parallel to S<sub>Hmax</sub> at C0001 (Expedition 314 Scientists, 2009b; Fig. 2). Site 219 C0004 is only a few kms from C0001 and Byrne et al. (2009) assumed a relatively 220 homogeneous stress field and proposed that  $S_{Hmax}$  at this site represented  $\sigma_2$  rather than 221  $\sigma_1$ . More recent analyses of borehole breakouts, however, by Olcott and Saffer (2012) 222 and Yamada and Shibanuma (2015) suggest that  $S_{Hmax}$  at this site possibly represents  $\sigma_1$ 223 consistent with a reverse or strike-slip faulting regime. They described that the 224 magnitude of the vertical stress Sv may be smaller than that of SHmax but within the 225 possible range of Shmin (see Fig. 4 in Yamada and Shibanuma, 2015).

**226** *3.4. C0006* 

227 Site C0006 penetrated and sampled the hanging wall of the frontal thrust and borehole 228 breakouts, anelastic strain and core-scale faults provide a more complete picture of the 229 stress state than at C0004. Borehole breakouts occur throughout most of the hole 230 although they appear much more weakly developed than at the other three sites. The 231 breakouts trend 060° consistent with results from Sites C0001 and C004, indicating that S<sub>Hmax</sub> trends about 330°, approximately parallel to the plate convergence vector 232 233 (Expedition 314 Scientists, 2009c). ASR on a core sample from the hanging wall and 234 inversion of the youngest suite of core-scale faults show a steeply plunging  $\sigma_1$  with  $\sigma_3$ 

235	trending northeast, indicating normal faulting and margin-parallel extension, similar to
236	Site C0001 at shallow depths (Fig. 6b). Interpretations of the stress field around Site
237	C0006 using a slip deficit model also indicate a normal faulting regime (Fig. 6a; Wu et al.,
238	2013), and conjointly a significant erosion at the top of the slope sediments can be
239	observed (Strasser et al, 2011; Conin et al, 2011). Anisotropy of magnetic susceptibility
240	data (Byrne et al., 2009; Kitamura et al., 2010) and suites of core-scale structures that
241	pre-date the normal faults show an earlier phase of margin-perpendicular shortening,
242	which is also similar to the observations from Site C0001 (Lewis et al. 2013).
243	<i>3.5. C0007</i>
244	Site C0007, located less than a kilometer seaward of Site C0006 and a few hundred
244 245	Site C0007, located less than a kilometer seaward of Site C0006 and a few hundred meters from the deformation front, was drilled after coring at Site C0006 failed to reach
245	meters from the deformation front, was drilled after coring at Site C0006 failed to reach
245 246	meters from the deformation front, was drilled after coring at Site C0006 failed to reach the frontal thrust (Fig. 3). Although the holes drilled at Site C0007 were not logged, so
245 246 247	meters from the deformation front, was drilled after coring at Site C0006 failed to reach the frontal thrust (Fig. 3). Although the holes drilled at Site C0007 were not logged, so borehole images are not available, observations of cores indicate a deformation history
245 246 247 248	meters from the deformation front, was drilled after coring at Site C0006 failed to reach the frontal thrust (Fig. 3). Although the holes drilled at Site C0007 were not logged, so borehole images are not available, observations of cores indicate a deformation history similar to the history documented at Site C0006; that is, early northwest-southeast
245 246 247 248 249	meters from the deformation front, was drilled after coring at Site C0006 failed to reach the frontal thrust (Fig. 3). Although the holes drilled at Site C0007 were not logged, so borehole images are not available, observations of cores indicate a deformation history similar to the history documented at Site C0006; that is, early northwest-southeast shortening followed by normal faulting. In addition, vitrinite reflectance measurements

also sampled the front thrust after it slipped co-seismically.

254

### 255 4. Results from Stage 2, Nankai subduction zone, SW Japan

**256** *4.1. C0009* 

257 At Site C0009, direct measurements of  $\sigma_3$  via hydraulic fracturing tests and leak-off test 258 (LOT) indicate that the stress regime changes from a normal faulting stress regime in the 259 Kumano basin sediments to a possible strike-slip or thrusting stress regime in the 260 underlying slope basin or accretionary wedge, to a depth of at least ~1600 mbsf similar 261 to the change at Site C0001 (Fig. 2; Lin et al., 2010b; Ito et al., 2013; Saffer et al., 2013; 262 Wu et al., 2013). Estimates of stress magnitude from the width of borehole breakouts at 263 Site C0002 suggested a similar pattern, i.e. changing from a normal faulting stress 264 regime in the basin sediments to a strike slip or thrust faulting regime in the underlying 265 accretionary prism to the depth of ~1380 mbsf (the lower limit of breakout occurrence in borehole C0002A) (Tobin et al., 2009a; Byrne et al., 2009; Chang et al., 2010; Lee et al., 266 267 2013).

**268** *4.2. C0010* 

Site C0010 is located a few km along strike from Site C0004 and, similar to C0004,penetrated the hanging wall and footwall of the megasplay, one of primary drilling

271 targets of the NanTroSEIZE. Shipboard analysis of the borehole breakouts showed a 272 consistent pattern above the megasplay with the maximum horizontal stress trending 273 NW-SE. McNeill et al. (2010) noted that the megasplay corresponds to a seismic reflector 274 with negative polar, suggesting a reduction in velocity and/or density in the footwall. 275 They also recognized an abrupt change in orientation of the breakouts across the 276 megasplay and proposed that the fault zone represented a sharp mechanical 277 discontinuity. Although Olcott and Saffer (2012) proposed that  $\sigma_1$  remained horizontal 278 beneath in the footwall similar to the results from C0004, they also documented a shift 279 to lower stress magnitudes in the footwall, based on the widths of borehole breakouts. 280 *4.3. C0011 and C0012* 281 At Site C0011, the orientation of S<sub>Hmax</sub> was determined by borehole breakouts observed 282 in a narrow depth interval (~600 – 650 mbsf, Expedition 322 Scientists, 2010) and is 283 oblique to the plate convergence vector. Although estimates of stress magnitude are 284 strongly dependent on assumed rock strength parameters, a normal faulting stress 285 regime was suggested on the basis of wellbore breakout widths at ~610 mbsf (Wu et al., 2013). 286

At Site C0012, which is the most seaward input site and occurs on the crest of a
prominent basement high (Kashinosaki Knoll), ASR results suggest a normal faulting

289	regime in the sedimentary sequence, with $S_{Hmax}$ oriented WNW-ESE (Yamamoto et al.,
290	2013). In contrast, ASR analysis of a core sample of oceanic basement basalt shows a
291	strike slip or a reverse faulting stress regime, with the maximum horizontal stress
292	orientated northeast - southwest approximately parallel to the trough axis. The
293	basement stress orientation could be the result of hinge extension during bending of the
294	Philippine Sea plate, either in association with subduction or with the formation of an
295	anticline during intraoceanic thrusting (Yamamoto et al., 2013).

296

297 5. Discussion: Nankai Margin

298 Although the drilling depths in stages 1 and 2 are relatively shallow (<~1.6 km at Site 299 C0009), the results suggest important trends in both depth and map view. For example, 300 observations at many of the sites suggest a change from a normal faulting regime at 301 shallow structural levels to strike-slip or thrusting at deeper levels. These results 302 suggest that gradients in topography may play an important role in defining the state of 303 stress. Deeper drilling, like the programs completed as part of Expedition 348 which 304 penetrated to ~3 kmbsf at Site C0002 and the future NanTroSEIZE expeditions planned 305 to drill to > 5 kmbsf in the same borehole will better define change in stress states with 306 depth and provide a clearer understanding of how stress changes temporally and307 spatially in the prism.

308 The above review suggests two general patterns for the states of stress at 309 relatively shallow levels: First,  $\sigma_1$  appears to be vertical at all sites except in the hanging 310 wall of the megasplay at Sites C0004 and C0010 where  $\sigma_1$  is interpreted to be 311 sub-horizontal and parallel to the plate convergence vector. Second, the maximum 312 horizontal stresses S<sub>Hmax</sub> appear to be parallel to the plate convergence vector except 313 near the seaward edge of the Kumano Basin at Site C0002 where  $\sigma_3$  is parallel to the 314 plate convergence vector.

315 A possible explanation for the reorientation of  $\sigma_1$  at C0004 and C0010 may be 316 that the sediments being carried in the hanging wall are relatively strong and capable of 317 supporting plate tectonic stresses. The occurrence of an extensional regime at higher 318 structural levels where slope sediments are dominant (e.g., Site C0001) and the 319 identification of a relatively weak footwall (Olcott and Saffer, 2012; McNeill et al, 2010) 320 are consistent with this interpretation. We therefore propose that the hanging wall of the 321 megasplay is relatively strong and supports a compressional stress state that is 322 consistent with plate convergence. In contrast, the transmission of the stresses 323 associated with plate convergence appears to be less effective in the slope sequence

324	where $\sigma_2$ is observed to be parallel to the plate convergence vector and in the footwall
325	where stress magnitudes decrease and possibly reorient. Drilling and sampling of
326	core-scale faults across the décollement at Site 808 during the Ocean Drilling Program
327	(ODP) Leg 131 along the Muroto transect also documented a reorientation of stresses
328	(Lallemant et al., 1993). At this site $\sigma_1$ is sub-horizontal and NW-trending above the
329	décollement, similar to the results from C0004 and C0010, and but sub-vertical below
330	the décollement (Lallemant et al., 1993). One possibility is that the stresses below the
331	megasplay have also been reoriented and $\sigma_1$ is vertical (Fig. 3) or they record a transition
332	in stress states.

At C0002 the reorientation of  $\sigma_3$  relative to the regional pattern may reflect 333 334 gravitation collapse of the prism as the décollement weakens either continuously or 335 during large earthquakes as suggested for the Tohoku region (McKenzie and Jackson, 336 2012; Kimura et al., 2012; Tsuji et al., 2013). A seismic reflection profile running NW-SE 337 and including Site C0002 displays a clear sequence of trough-parallel normal faults in 338 the basin sediments consistent with the maximum horizontal stress orientation data (e.g. 339 Tobin et al., 2009a). Sacks et al. (2013) (and see also Moore et al., 2013) analyzed this 340 regional-scale fault system in more detail and recognized two patterns of extension – an 341 early phase of generally northeast-southwest, or margin-parallel, extension and a later

342 phase of trench-perpendicular extension that is concentrated on the seaward edge of the 343 basin. The fact that trench-perpendicular extension appears to be limited to the area of 344 the shelf edge, which is both relatively far from the plate interface and at the topographic 345 crest, is consistent with the hypothesis that gradients in topography (including effects of 346 the "notch" proposed by Martin et al., 2010) are important in defining the state of stress 347 along the margin. Theoretical studies as well as analog and numerical models also 348 suggest that variations in the strength of the décollement below the wedge can lead to 349 extension in the overlying accretionary wedge. For example, Haq and Davis (2008) show 350 that for wedges with a ductile base, accretion can lead to over steepened topography and 351 flow at lower structural levels, which drive trench-perpendicular extension (i.e., normal 352 faulting) at higher structural levels. In fact, several authors have proposed that a regional low-velocity zone beneath the Nankai margin represents weak, and probably 353 354 overpressured sediments (Park et al., 2010; Byrne et al. 2009; Bangs et al., 2009; Kamei 355 et al., 2012; Kitajima & Saffer, 2012) that may act like the ductile lower crust in the analog models. 356

The above hypothesis for the pattern of regional-scale stresses, however, fails to consider the possible change in stresses associated with the earthquake cycle. For example, this region of the Nankai margin experienced a major earthquake and tsunami 360 in 1944; and Sakaguchi et al. (2011a), based on maturation studies of vitrinite collected 361 from fault zones sampled at Sites C0004 and C0007, proposed that megasplay and 362 décollement slipped during the earthquake(s). Presumably, for some period before, and 363 up to the beginning of the earthquake the state of stress in the hanging wall would have 364 been compressional with  $\sigma_1$  orientated sub-parallel to the plate convergence vector. The 365 evidence from all of the sites along the Kumano transect where the principal stress 366 orientations can be determined, however, shows a normal faulting regime, at least at 367 shallow structural levels and excluding Sites C0004 and C0010 which sampled the 368 hanging wall of the megasplay. These data also show that the rocks failed exclusively by 369 normal faulting; that is, there is no evidence in the cores or seismic reflection data for 370 alternating periods of extension and compression that could be interpreted as stress 371 permutations associated with an earthquake cycle. For example, observation from Site 372 C0002 and detailed studies of the deformation history in the Kumano Basin (Lewis et al., 373 2013 and Sacks et al., 2013, respectively) show an early phase of trench-parallel 374 extension followed by a phase of trench-perpendicular extension. Neither data set shows 375 stress permutations where the principal stresses switch multiple times, for example over 376 several earthquake cycles. At least two explanations are possible, either: 1) all of the late 377 stage normal faults formed after the last earthquake (e.g., after 1944) due to stress 378 relaxation and stress permutations or 2) the stress states vary during the seismic cycle 379 (e.g.,  $\sigma_1$  alternates between horizontal and vertical from one cycle to the next) (Wang and 380 Hu, 2006; Conin et al., 2012; Kinoshita and Tobin, 2013; Sacks et al., 2013; Hashimoto et 381 al., 2014), but during an earthquake, failure is accommodated only or primarily by slip 382 on major thrust faults and not on core-scale faults. After a major earthquake, the 383 associated stress drop and relaxation leads to decrease in S<sub>Hmax</sub>, such that the vertical 384 stress  $S_v$  becomes  $\sigma_1$ , depending on the local stress field. Hsu et al. (2009) recently 385 proposed an interpretation similar to the second alternative (#2 above) for stress 386 permutations before and after the 1999 Chichi earthquake in Taiwan.

387

388 6. Stress states at the Japan Trench

**389** *6.1. IODP drilling Site C0019 and ODP Sites 1150 and 1151* 

The Japan Trench lies along the eastern edge of Japan and marks the boundary where the Pacific plate subducts beneath the Okhotsk plate (or North American plate) at ~8 cm/year (Loveless and Meade, 2010) (Fig. 1). The Tohoku-Oki earthquake (Mw 9.0) occurred on March 11, 2011 and was followed by a huge tsunami (Simons et al., 2011; Ide et al., 2011) that flooded many coastal regions of northeast Japan, taking over 18,000 lives. Planning for IODP Expedition 343 (informally called the "Japan Trench Fast Drilling

396	Project" or JFAST) began soon after the earthquake with the primary goal of better
397	understanding the stress and slip history along the fault. To this end, the goals of the
398	expedition were to: 1) test the possibility that coseismic slip on a major fault generated
399	frictional heat; 2) to investigate stress state on the fault and 3) retrieve samples from the
400	proposed fault zone. To achieve these goals IODP expedition 343 conducted a rapid
401	response drilling program about 13 months after the earthquake. The expedition
402	successfully penetrated and sampled the frontal fault at a depth of $\sim$ 820 mbsf at IODP
403	Site C0019 where coseismic displacements were relatively large ( $\sim$ 50 m) (Mori et al.,
404	2012; Chester et al., 2012). Site C0019 is located $\sim$ 93 km seaward from the epicenter of
405	the mainshock of the Tohoku-Oki earthquake and $\sim$ 6 km landward of the trench axis (Fig.
406	4b and 5).
407	In addition to the JFAST site, Sites 1150 and 1151, also located near the source
408	area of the Tohoku-Oki earthquake, were drilled during ODP Leg 186 in 1999 prior to the
409	earthquake (Lin et al., 2011) (Fig. 4b). Lin et al. (2011) integrated FMS images with
410	caliper data to interpret the orientation of $S_{\mbox{\scriptsize Hmax}}$ at the two sites.

*6.2. Results from C0019* 

412 Lin et al. (2013) analyzed LWD data collected by JFAST at Site C0019 (Fig. 4b)413 and integrated these data with compressive strength and core-based observations to

414 determine the stress state and to infer stress history at this site. Although borehole 415 breakouts are present throughout the hanging wall of the plate boundary, they are show 416 a wide range in orientations at shallow structural levels (<500 mbsf), suggesting that 417 SHmax and Shmin are close in magnitude, and/or that SHmax orientation is highly variable 418 with depth. At deeper levels (>500 mbsf) S<sub>Hmax</sub> shows a clear trend to the northwest 419  $(319 \pm 23^\circ)$ , which is sub parallel to the plate convergence vector of 292° at this location 420 (Fig.4b; Argus et al., 2011). Lin et al. (2013) also used the width of the borehole 421 breakouts and the results of initial shipboard experiments on the unconfined 422 compressive strength (UCS) of sediments from two depth intervals to determine the 423 stress magnitudes. Their results show that the frontal part of the prism above the plate 424 boundary fault is in, or close to, a normal faulting regime (Fig. 6c). These results contrast 425 with core-scale observations, however, that show dominantly thrusting and horizontal 426 shortening with only limited evidence of extension at relatively shallow structural levels. 427 Based on these results, the authors suggested a distinct coseismic stress change from a 428 reverse faulting stress regime before the earthquake to a normal faulting stress regime after the earthquake (Fig. 7). This interpretation is well-consistent with Hasegawa et al. 429 430 (2012).

**431** *6.3. Results from ODP Sites 1150 and 1151* 

432 FMS and caliper data from Sites 1150 and 1151 were used to define the orientation of 433 S<sub>Hmax</sub> at these two sites, which were drilled prior to the Tohoku-Oki earthquake. The FMS 434 images showed the development of drilling induced tensile fractures (DITF) and 435 borehole breakouts at deeper structural levels (e.g., > 700mbsf) and the caliper data 436 provide a general constraint on the orientation of borehole breakouts. Although there is 437 variability between the two sites, the combined data set shows S<sub>Hmax</sub> trending northwest, 438 generally parallel to the plate convergence vector (Lin et al., 2011) (Fig. 4b). Based on 439 the presence of DITFs at both sites and significant seismic activity associated with 440 northwest-southeast directed shortening, Lin et al. (2011) concluded that the hanging of 441 the plate boundary in this area possibly was in a thrusting regime before the 2011 442 earthquake.

443

## 444 7. Comparison between Nankai and Japan Trench

The general comparison of the Nankai and Tohoku margins presented above shows that
the margins share important similarities as well as at least one critical difference (Fig. 5).
First, available data suggest that both margins are dominated by an extensional stress
regime with a vertically oriented maximum principal stress. Extension along the Tohoku
area is show by the dominance of normal faulting aftershocks in the hanging wall above

450 the décollement (Tsuji et al., 2013) as well as the in situ stress data from Site C0019. 451 Extension along Nankai is documented by seismic reflection data along the shelf edge 452 and observations from 3 drill sites that span the accretionary prism. Horizontal 453 compression may occur at deeper levels and in the hanging wall of the megasplay, but 454 normal faulting appears to be the dominant pattern. The second similarity is that both 455 margins can be divided into inner and outer wedges separated by a regionally significant 456 normal fault or a complex system of normal and oblique slip faults. At Tohoku, a 457 landward dipping normal fault with significant offset separates a deep-sea terrace from 458 the upper, middle and low slope that define the accretionary wedge. At Nankai, the 459 seaward edge of the forearc basin is marked by relatively intricate set of normal faults 460 associated with a graben-like structure that marks shelf edge. Some of the normal faults may also have oblique slip that accommodate strike-parallel motion related to 461 462 moderately oblique plate convergence (Martin et al., 2010). Finally, one critical 463 difference appears to be the presence of a megasplay in the accretionary prism of the 464 Nankai margin and the apparent absence of similar structures along the Tohoku margin. 465 Interestingly, the similarities of the two margins are also the primary 466 characteristics of margins that typically produce tsunami earthquakes (Tsuji et al., 2013; 467 McKenzie and Jackson, 2012). For example, recent theoretical studies (McKenzie and

468	Jackson, 2012) as well as recent observations from Tohoku (Tsuji et al., 2013) suggest
469	tsunami genic earthquakes result from the simultaneous slip along the décollement and
470	a landward-dipping normal fault or a suite of normal faults that separate the inner and
471	outer wedges. McKenzie and Jackson (2012) also propose that displacements on these
472	regional-scale faults and the seaward motion of the outer wedge is driven by the release
473	of gravitational potential energy as well as elastic strain. Although McKenzie and Jackson
474	(2012) do not address what processes cause the décollement and the normal fault to fail
475	simultaneously, Kimura et al. (2012) suggest that progressive dewatering of underthrust
476	sediments along the Tohoku margin lead to failure and "runaway" slip along the
477	décollement probably weakened by over pore pressure (e.g. Tobin and Saffer, 2009;
478	Kitajima et al., 2012; Hashimoto et al., 2013; Tsuji et al., 2014). Tsuji et al. (2013), based
479	on sea floor observations of extension cracks and heat flow anomalies, also propose that
480	normal faulting in the hanging wall occurred simultaneously with slip on the
481	décollement. Along the Nankai margin, the décollement is also interpreted to be
482	anomalously weak and the seaward edge of the Kumano Basin is deformed exclusively
483	by normal faults, suggesting a tectonic setting similar to Tohoku. One possibility,
484	therefore, is that during a historic great earthquake, which also produced a tsunami

485 along southwest Japan, slip occurred simultaneously on normal faults in the hanging486 wall and along the décollement.

487 A complication to this interpretation is that models of the 1944 tsunami suggest 488 that a significant amount of the coseismic slip occurred on the megasplay rather than the 489 décollement (Tanioka and Satake, 2001; Cummins et al., 2002). However, Sakaguchi et al. 490 (2011a), based on observations from Site C0007 which is near the toe of the prism, show 491 that the décollement also moved co-seismically, although the timing of co-seismic slip is 492 unknown. If the model proposed for Tohoku (McKenzie and Jackson, 2012) also applies 493 to the 1944 event along the Kumano transect, then movement along both the megasplay 494 and the décollement must have driven forward motion of the accretionary wedge. 495 We therefore propose that the two margins represent similar states between 496 tsunami earthquakes, although there are differences. Following this interpretation, the 497 stress state of the accretionary wedge, including the frontal plate interface builds up 498 from a normal faulting stress regime just after a large earthquake to a reverse faulting

regime before the next earthquake. In other words, the tectonic horizontal stress caused
by plate convergence gradually builds up during the interseismic period and dynamically
drops during an earthquake consistent with the conventional stress accumulation
fundamental model (e.g. see Kanamori and Brodsky, 2001). Following this interpretation,

503	both Sites C0006 (Nankai) and Site C0019 (Tohoku) appear to be in the early stages of
504	the interseismic cycle with $\sigma_1$ is vertical and that $S_{Hmax}$ (interpreted to be $\sigma_2$ ) is generally
505	parallel to the plate convergence vector (Fig. 6). In Nankai margin, more than 60 years
506	have passed from the previous M8-class earthquake propagated through the megasplay
507	fault to the time of drilling at C0006 (2007), but the time length from the previous great
508	earthquake occurred on the décollement and propagated to C0006 is unknown.
509	Hypothetically, the stress state may indicate that in Nankai margin, it is still in an early
510	stage of the interseismic cycle of a great earthquake which occurs on the décollement
511	and propagates to the toe, even cuts the seafloor.

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## 852 <u>Table and Figures' captions</u>

- Table 1 Specifications of the stress measurement related boreholes in NanTroSEIZE and
  JFAST drilling sites. For example, C0002 denotes the drilling site; whereas C0002A is
  the name of the borehole "A" located at Site C0002. Usually, multi boreholes were
  drilled for different operations within a narrow area (e.g. a few tens meters) in a site in
  IODP.
- 859

Fig. 1 (1.5-column fitting) Nankai and Japan Trench subduction zones and plates around
Japan islands. Red stars and numbers show the epicenters of the earthquakes and
its occurrence year; the red frames are the area of rupture zones during the
earthquakes. White arrows and numbers show directions and rates of plate motion,
respectively (Sella et al., 2002; Apel et al., 2006; Loveless and Meade, 2010; Ozawa
et al., 2011).

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Fig. 2 (2-column fitting) Distributions of semi three-dimensional stress state in
NanTroSEIZE transect. Codes (e.g. C0009) are the number of drilling sites. Red,
black and light blue arrows are the orientations of the maximum, intermediate and
minimum principal stresses, respectively. Two pair arrows in the same light blue
color in the deeper part of C0009, C0002 and C0012 mean that the intermediate
and minimum principal stresses are nearly equal each other, or the intermediate
and minimum principal stresses are highly variable.

874

875 Fig. 3 (2-column fitting) Seismic reflection section of NanTroSEIZE transect (modified 876 from Saito et al., 2009). Depths denote the depth below sea level. The gray overlay 877 shows the predicted area of horizontal  $\sigma_1$  (the maximum principal stress). Around 878 megasplay site C0004 and the frontal thrust site C0006, two patterns of  $\sigma_1$ 879 distribution are considered to be possible. The first one is a gradual change: but the 880 other shows a drastic change around the decollement and the megasplay suggested 881 from the observations at ODP Site 808 and Alaska (Lallemant et al., 1993 and Byrne 882 & Fisher, 1990).

883

Fig. 4 (2-column fitting) The maximum horizontal stress (S<sub>Hmax</sub>) orientations in SW and
NE Japan subduction zones. Red bars at the drilling sites show the representative
S<sub>Hmax</sub> orientations in the sites. Two rad rectangles in inset shows locations of figures
(a) and (b), respectively. (a) Stress orientations at Site C0009 compiled from Lin et

888 al. (2010a) and Wu et al., (2012); C0002, C0001, C0004 and C0006 from Chang et al. 889 (2010), C0011 from Expedition 322 Scientists (2010), C0012 from Yamamoto et al. 890 (2013), and at ODP Site 808 from McNeill et al. (2004) and Ienaga et al. (2006). 891 Yellow arrows show the far-field convergence vectors between the Philippine Sea 892 plate and Japan (Heki and Miyazaki, 2001; Miyazaki and Heki, 2001). (b) Location of 893 JFAST Site C0019 and S<sub>Hmax</sub> orientation in the deep part of the borehole (Lin et al., 894 2013). Red solid and dashed lines show the mean S<sub>Hmax</sub> orientation and one 895 standard deviation (SD), respectively, determined in 2012 after the 2011 Tohoku 896 earthquake. Green circles and lines show ODP sites drilled in 1999 and their SHmax 897 orientations prior to the 2011 earthquake (Lin et al., 2011). The gray arrow shows 898 relative plate motion around Site C0019 (Argus et al., 2011). The white numbers 899 and the contour lines show water depths.

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901 Fig. 5 (2-column fitting) A comparison of seismic reflection profiles of NanTroSEIZE 902 transect and around JFAST drilling site in the same scale (modified from Moore et al., 903 2009 and Kodaira et al., 2012 respectively) shows the overall similar structures. The 904 five structure horizontal areas, the deep sea terrace, the upper, middle and lower 905 slopes and the trench axis were defined by Kodaira et al. (2012). Site C0006 in the 906 Nankai subduction zone is at the similar location as Site C0019 in the Japan Trench. 907 At exact location of C0019 no wider seismic profile available, thus we used this 908 profile locating just 15 km north of C0019.

909

910 Fig. 6 (2-column fitting) A comparison of stress states in the hanging wall of the frontal 911 plate-interfaces in toe of Nankai and Japan Trench subduction zones revealed from 912 Sites C0006 and C0019. (a) Possible stress state at 476 mbsf in borehole C0006B 913 constrained from breakout width and assumed wall rock unconfined compressive 914 strength (UCS) locates in the area of normal faulting stress regime (Wu et al., 2013). 915 (b) Stress state at 468 mbsf in borehole C0006F determined from ASR 916 measurements is of normal faulting stress regime being consistent with that from 917 breakouts in C0006B (Byrne et al., 2009). (c) Possible stress state at 720 mbsf in 918 borehole C0019B constrained from breakout width and measured UCS 3.8 MPa 919 locates in the area of normal faulting stress regime (Lin et al., 2013). (d) Schematic 920 of the current common stress state in the hanging wall of the frontal plate-interfaces 921 in both Sites C0006 and C0019.

922

923 Fig. 7 (1.5-column fitting) Schematic of inferred coseismic three-dimensional stress state

924 change from a reverse faulting regime before the Tohoku-oki earthquake (a) to a 925 normal faulting regime after the earthquake (b) in the lower portion of the frontal 926 prism in Japan Trench subduction zone obtained from JFAST (Modified from Lin et 927 al., 2013). NAP denotes North American Plate. Red arrows indicate the maximum 928 principal stress ( $\sigma_1$ ); blue arrows: the intermediate principal stress ( $\sigma_2$ ); black 929 arrows: the minimum principal stress ( $\sigma_3$ ). Because the static vertical stress ( $\sigma_v$ ) is 930 under a mechanical equilibrium state with the overburden pressure (the gravity of 931 the formations above the depth), the magnitude of  $\sigma_v$  may not change before and 932 after the earthquake; however was the  $\sigma_3$  before the earthquake, the  $\sigma_1$  after the 933 earthquake according to the changes of horizontal stress magnitudes during the 934 earthquake.

- Table 1 Specifications of the stress measurement related boreholes in NanTroSEIZE and
  JFAST drilling sites. For example, C0002 denotes the drilling site; whereas C0002A is
  the name of the borehole "A" located at Site C0002. Usually, multi boreholes were
  drilled for different operations within a narrow area (e.g. a few tens meters) in a site in
  IODP.

Holes	Location		Water	Total	
(stress related	Latitude	Longitude	depth	depth	Source of data
operations)			m	mbsf	
C0009A (WL&C*)	33°27.47′N	136°32.15′E	2054	1604	Exp 319 Summary
C0002A (LWD**)	33°18.02′N	136°38.18′E	1936	1402	Exp 314 Summary
C0002B (Coring)	33°17.99′N	136°38.20′E	1938	1057	Exp 315 Summary
C0001D (LWD)	33°14.33′N	136°42.70′E	2198	976	Exp 314 Summary
C0001E (Coring)	33°14.34′N	136°42.69′E	2198	118	Exp 315 Summary
C0001F (Coring)	33°14.34′N	136°42.71′E	2197	249	Exp 315 Summary
C0004B (LWD)	33°13.23′N	136°43.35′E	2637	400	Exp 314 Summary
C0010A (LWD)	33°12.60′N	136°41.12′E	2524	555	Exp 319 Summary
C0006B (LWD)	33°01.64′N	136°47.64′E	3872	886	Exp 314 Summary
C0006E (Coring)	33°01.64′N	136°47.63′E	3876	409	Exp 316 Summary
C0011A (LWD)	32°49.73′N	136°52.89′E	4049	952	Exp 319 Summary
C0012A (Coring)	32°44.89′N	136°55.02′E	3511	576	Exp 322 Summary
C0019B (LWD)	37°56.34′N	143°54.81′E	6890	851	Exp 343 Summary

- 871 \*WL&C: Wireline logging and coring
- 872 \*\*LWD: Logging While Drilling

## 875 Figures and their captions

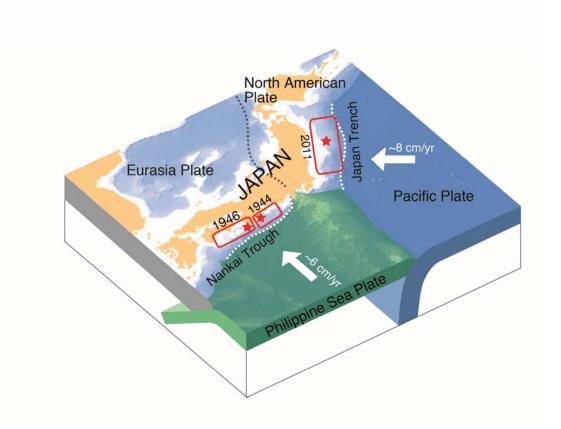
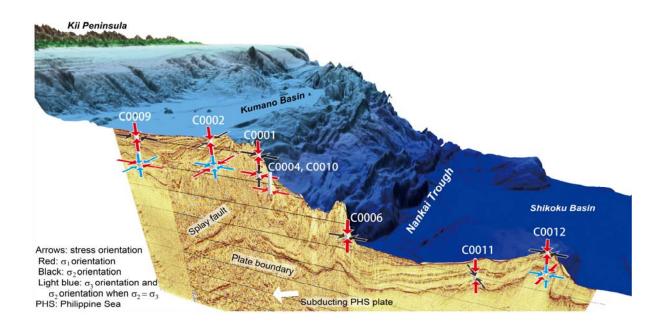


Fig. 1 (1.5-column fitting) Nankai and Japan Trench subduction zones and plates around
Japan islands. Red stars and numbers show the epicenters of the earthquakes and
its occurrence year; the red frames are the area of rupture zones during the
earthquakes. White arrows and numbers show directions and rates of plate motion,
respectively (Sella et al., 2002; Apel et al., 2006; Loveless and Meade, 2010; Ozawa
et al., 2011).



## Figure 2 (2-column fitting)

Fig. 2 (2-column fitting) Distributions of semi three-dimensional stress state in
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black and light blue arrows are the orientations of the maximum, intermediate and
minimum principal stresses, respectively. Two pair arrows in the same light blue
color in the deeper part of C0009, C0002 and C0012 mean that the intermediate
and minimum principal stresses are nearly equal each other, or the intermediate
and minimum principal stresses are highly variable.

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Gray zone shows regime where Based on observations from Site σ1 is sub-horizontal 808 and field studies C0009 C0001 C0002 C0012 C0006 1C0007 C0011 2 Kumano Basir u Basin sedir Depth (km) <sup>8</sup> <sup>9</sup> <sup>5</sup> Turbidite Accretionary prism 5 Old accretionary sediments 2 Décollement Oceanic basement Subducting PHS plate 10 The range of Fig.5(b) 0 2 4 6 8 10 km



896



898 899 Fig. 3 (2-column fitting) Seismic reflection section of NanTroSEIZE transect (modified 900 from Saito et al., 2009). Depths denote the depth below sea level. The gray overlay 901 shows the predicted area of horizontal  $\sigma_1$  (the maximum principal stress). Around 902 megasplay site C0004 and the frontal thrust site C0006, two patterns of  $\sigma_1$ 903 distribution are considered to be possible. The first one is a gradual change: but the 904 other shows a drastic change around the decollement and the megasplay suggested **9**05 from the observations at ODP Site 808 and Alaska (Lallement Lallemant et al., 1993 906 and Byrne & Fisher, 1990).

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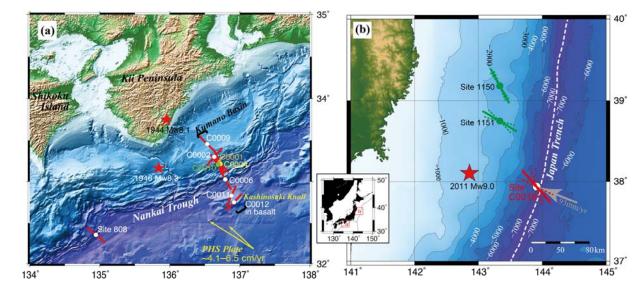
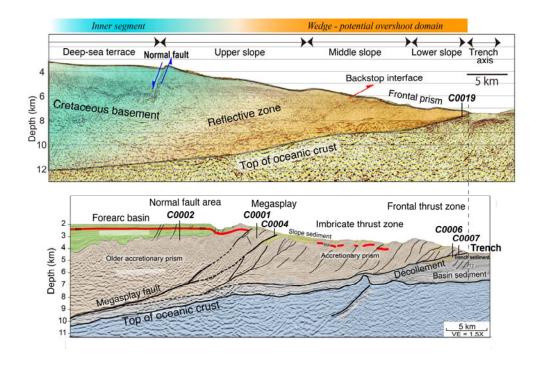
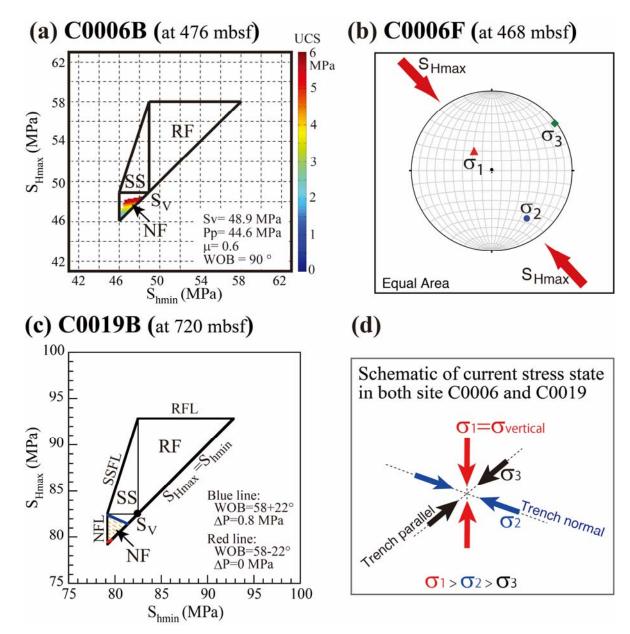


Fig. 4 (2-column fitting) The maximum horizontal stress (S<sub>Hmax</sub>) orientations in SW and 912 913 NE Japan subduction zones. Red bars at the drilling sites show the representative 914 S<sub>Hmax</sub> orientations in the sites. Two rad rectangles in inset shows locations of figures 915 (a) and (b), respectively. (a) Stress orientations at Site C0009 compiled from Lin et 916 al. (2010a) and Wu et al., (2012); C0002, C0001, C0004 and C0006 from Chang et al. 917 (2010), C0011 from Expedition 322 Scientists (2010), C0012 from Yamamoto et al. 918 (2013), and at ODP Site 808 from McNeill et al. (2004) and Ienaga et al. (2006). 919 Yellow arrows show the far-field convergence vectors between the Philippine Sea 920 plate and Japan (Heki and Miyazaki, 2001; Miyazaki and Heki, 2001). (b) Location of 921 JFAST Site C0019 and S<sub>Hmax</sub> orientation in the deep part of the borehole (Lin et al., 922 2013). Red solid and dashed lines show the mean S<sub>Hmax</sub> orientation and one 923 standard deviation (SD), respectively, determined in 2012 after the 2011 Tohoku 924 earthquake. Green circles and lines show ODP sites drilled in 1999 and their SHmax 925 orientations prior to the 2011 earthquake (Lin et al., 2011). The gray arrow shows 926 relative plate motion around Site C0019 (Argus et al., 2011). The white numbers 927 and the contour lines show water depths.

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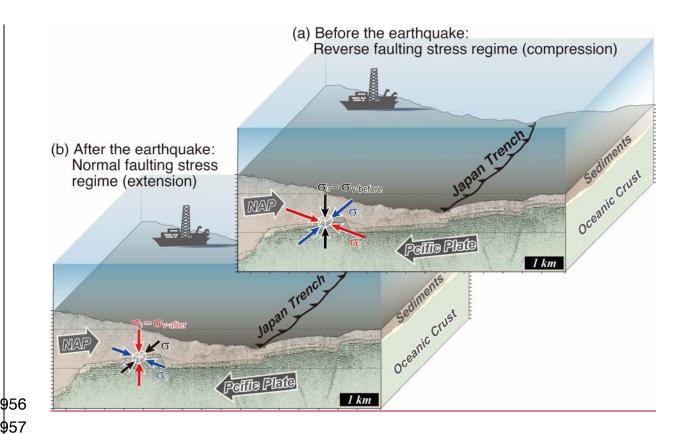


932	Fig. 5 (2-column fitting) A comparison of seismic reflection profiles of NanTroSEIZE
933	transect and around JFAST drilling site in the same scale (modified from Moore et al.,
934	2009 and Kodaira et al., 2012 respectively) shows the overall similar structures. The
935	five structure horizontal areas, the deep sea terrace, the upper, middle and lower
936	slopes and the trench axis were defined by Kodaira et al. (2012). Site C0006 in the
937	Nankai subduction zone is at the similar location as Site C0019 in the Japan Trench.
938	At exact location of C0019 no wider seismic profile available, thus we used this
939	profile locating just 15 km north of C0019.
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943 Fig. 6 (2-column fitting) A comparison of stress states in the hanging wall of the frontal 944 plate-interfaces in toe of Nankai and Japan Trench subduction zones revealed from 945 Sites C0006 and C0019. (a) Possible stress state at 476 mbsf in borehole C0006B 946 constrained from breakout width and assumed wall rock unconfined compressive 947 strength (UCS) locates in the area of normal faulting stress regime (Wu et al., 2013). 948 (b) Stress state at 468 mbsf in borehole C0006F determined from ASR 949 measurements is of normal faulting stress regime being consistent with that from 950 breakouts in C0006B (Byrne et al., 2009). (c) Possible stress state at 720 mbsf in 951 borehole C0019B constrained from breakout width and measured UCS 3.8 MPa 952 locates in the area of normal faulting stress regime (Lin et al., 2013). (d) Schematic 953 of the current common stress state in the hanging wall of the frontal plate-interfaces **9**54 in both Sites C0006 and C0019.



**9**58 Fig. 7 (1.5-column fitting) Schematic of inferred coseismic three-dimensional stress state 959 change from a reverse faulting regime before the Tohoku-oki earthquake (a) to a 960 normal faulting regime after the earthquake (b) in the lower portion of the frontal 961 prism in Japan Trench subduction zone obtained from JFAST (Modified from Lin et 962 al., 2013). NAP denotes North American Plate. Red arrows indicate the maximum 963 principal stress ( $\sigma_1$ ); blue arrows: the intermediate principal stress ( $\sigma_2$ ); black 964 arrows: the minimum principal stress ( $\sigma_3$ ). Because the static vertical stress ( $\sigma_v$ ) is under a mechanical equilibrium state with the overburden pressure (the gravity of 965 966 the formations above the depth), the magnitude of  $\sigma_v$  may not change before and 967 after the earthquake; however was the  $\sigma_3$  before the earthquake, the  $\sigma_1$  after the 968 earthquake according to the changes of horizontal stress magnitudes during the 969 earthquake.