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ORIGINAL PAPER

# Tribochemistry of Bulk Zinc Metaphosphate Glasses

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**Abstract** Zinc polyphosphate glasses are the principal component of the antiwear tribofilms formed on steel surfaces in the presence of additives, such as zinc dialkyldithiophosphates. In this work, amorphous, zinc metaphosphate glasses have been synthesized and characterized by means of X-ray diffraction (XRD), Fourier-transform infrared spectroscopy (FT-IR), elemental analysis, and X-ray photoelectron spectroscopy (XPS). Tribological tests were performed by rubbing steel balls against the zinc metaphosphate discs in a poly- $\alpha$ -olefin (PAO) bath at room temperature. XPS was used in order to characterize the tribostressed areas on both metaphosphate discs and steel balls. A transfer film, constituted of iron and zinc polyphosphates, was formed on the contact area of the balls. This transfer film was found to reduce friction and prevent ball wear. A reduction in the relative intensities of XPS signals related to bridging-oxygen species and a binding energy shift of 0.4 eV of the P 2p toward lower values demonstrated the presence of shorter-chain-length phosphates inside the tribo-tracks on the discs. Furthermore, iron was transferred to the glass during the tribological tests. A tribochemical reaction between zinc metaphosphate and iron oxide

has been proposed as an explanation for the depolymerization of the glass and the formation of iron phosphate.

**Keywords** Antiwear additives · Boundary lubrication · Polyphosphate glasses · Tribochemistry · X-ray photoelectron spectroscopy (XPS)

## 1 Introduction

Polyphosphate glasses have been found to be responsible for the good antiwear properties of the tribofilms formed in the presence of phosphorus-based additives. Among them, zinc dialkyldithiophosphate (ZnDTP) is the most successful and widely used engine-oil additive. Its actual antiwear mechanism is only partially understood despite extensive research in recent decades. Interest in polyphosphate glasses has been recently stimulated by the need for more environmentally friendly replacements for ZnDTP, whose degradation products poison automobile exhaust catalysts and are thus harmful for the environment [1, 2].

The composition of tribofilms formed under sliding conditions on steel substrates in the presence of ZnDTP has been extensively investigated. Underneath a viscous layer, which is easily removed by solvent washing, a film consisting of amorphous zinc and/or iron polyphosphates is formed [3–7]. This tribofilm has a layered structure: at the bottom a short-chain-length polyphosphate layer is present, intergrown with the iron oxide film. The top layer is thinner and formed by long-chain-length polyphosphates [3, 4]. Since it is unlikely that there is a clear interface between the different layers, but a gradual transition [5], ZnDTP tribofilms are often described as containing a gradient in composition. ZnDTP tribofilms

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have been shown to respond to different tribological conditions by changing their physical properties. This ability, which has contributed to their success in applications, can also explain the apparent disagreement in the literature on the exact thickness, structure, and chemistry of the films. The mechanism of formation of the tribofilms is still unclear [1]: at room temperature ZnDTP molecules weakly interact with the steel surface, but, under sliding conditions, the additive reacts and forms a thin tribofilm [6]. The effect of temperature and applied pressure on the thickness and chemistry of the films formed under tribological conditions in the boundary-lubrication regime has been recently investigated in our group: increasing the temperature induces the formation of longer polyphosphates and thicker films, while the application of higher pressures leads to shorter polyphosphate chain lengths and to an increase in the film thickness [7, 8]. Some authors have observed a shortening of the polyphosphate chains within the tribological scars as a consequence of rubbing [7, 9]. The origin of the gradient of composition in the tribofilms and the role potentially played in its antiwear mechanism is still under debate. In 1999, Martin proposed a model based on the principle of hard and soft acids and bases (HSAB). According to this principle, first proposed by Pearson [10], the reaction between long-chain zinc polyphosphates and iron oxides to give shorter-chain length iron/zinc polyphosphate is energetically favorable [11]. Based on this model, Minfray proposed that the reaction occurring during friction between polyphosphates and iron oxide plays a double role: not only would it allow the digestion of abrasive iron oxide particles, but it would also provide a strong adhesion of the tribofilms to the substrate through chemical bonding [12].

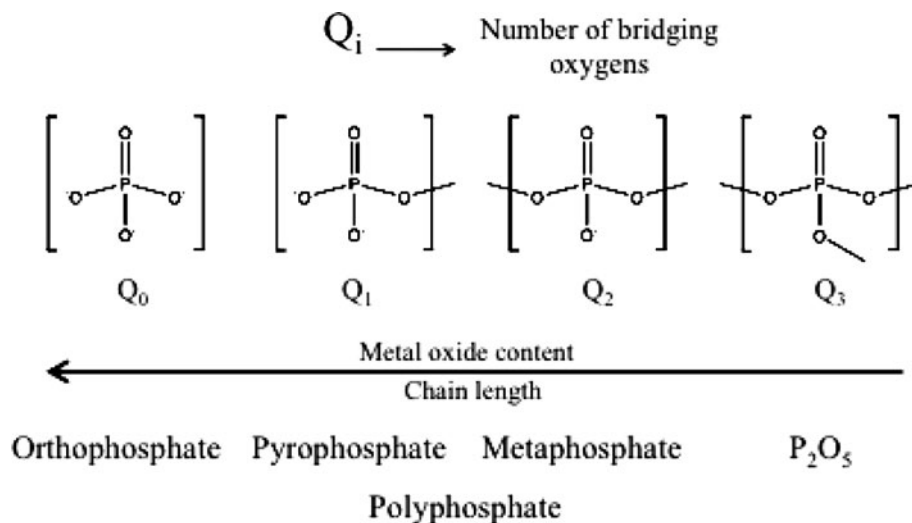
With this cross-linking theory supported by molecular dynamics simulation, Müser proposed a possible alternative mechanism. According to this theory, pressure would be able to induce cross-linking in a phosphate network leading to a highly connected network with improved mechanical properties [13]. The model has not yet been supported by experimental evidence.

Despite enormous efforts made by researchers, who have applied almost every available surface-analytical technique, several open questions about the antiwear mechanisms of ZnDTP remain to be addressed. The study of model systems of ZDTP tribofilms, such as polyphosphates, has been considered in order to reduce the complexity of real systems. Gauvin tested the behavior of pure zinc orthophosphate powder as an antiwear additive. Under boundary-lubrication conditions, the orthophosphate formed an adherent film on the steel substrate. This film was found to reduce wear [14].

The technical applications of polyphosphates glasses are various. They are implemented in the formulation of ceramic restorative cements [15] and more generally of bioactive functional materials [16]. They possess many useful optical properties and have been widely employed as active elements in laser engineering [17, 18]. The hope to understand the antiwear mechanism of phosphorus-based additives renewed the interest of researchers in investigating the mechanical and tribological properties of zinc and iron polyphosphates themselves.

Condensed phosphates are formed by repeated condensation of tetrahedral  $\text{PO}_4$  groups, which, by linking through covalent bridging oxygen (BO) atoms, can share their corners with neighboring tetrahedra. The tetrahedra can be classified by the number of BOs (P–O–P) per tetrahedron ( $Q_i$  terminology, see Scheme 1). The vitreous  $\text{P}_2\text{O}_5$  is

**Scheme 1** Terminology for different composition and structures in polyphosphate glasses



formed by a cross-linked network of  $Q_3$  tetrahedra. When a modifying oxide is added to  $P_2O_5$  the network is depolymerized and the concentration of  $Q_i$  tetrahedra depends on the glass composition (Scheme 1) [19, 20]. In other words, depending on the oxygen-to-phosphorus ratio ( $[O]/[P]$ ) the number of tetrahedral linkages through BO atoms changes and thus a wide range of compositions and structures is possible [21].

In the last 50 years, several techniques have been used to investigate the short- and long-range order of these glasses. The coordination of metal cations has been studied by means of  $^{31}P$  MAS-NMR, as well as neutron and X-ray diffraction (XRD) [22–26]. High-performance-liquid-chromatography (HPLC) has been used in order to determine the distribution of phosphate-anion chains and rings and to provide detailed information about the structure. The results obtained for zinc polyphosphate glasses showed that the average chain length can be computed directly from the glass composition when the presence of ring anions can be neglected [27]. In the region of the metaphosphate composition, long-chain structures are mainly found, while cross-linked chains and rings, typical of the ultraphosphate region, disappear [28]. At higher concentrations of ZnO a depolymerization of the phosphate network is observed and the long chains are transformed into trimers, dimers, and monomers, as the composition approaches orthophosphate.

X-ray photoelectron spectroscopy (XPS) has been used to analyze the short-range structure of polyphosphate glasses. Gresch [29] studied sodium phosphate glasses and found that two different signals can be resolved in the XPS spectra: at higher binding energy the signal of the BO, which links two phosphate groups together (P–O–P), and at lower binding energy the signal of the non-bridging oxygen (NBO), which terminates the phosphate ( $-PO_x$ ). Moreover, their intensity ratio is directly proportional to the composition of the glass. Iron-, zinc- and boron-containing phosphate glasses have been investigated by Brow [30, 31].

More recently X-ray absorption near-edge structure (XANES) spectroscopy was also used to distinguish between polyphosphates with different chain lengths: the P L-edge XANES spectra are sensitive to the structural changes caused by the bridging P–O bonds [32].

In this work, a sample-preparation protocol that allows the reproducible synthesis of zinc metaphosphate glasses for tribological testing has been established. The samples were characterized by means of XRD, FT-IR, elemental analysis, and XPS. The tribological tests were then performed by sliding steel balls on the metaphosphate discs. Light microscopy and profilometry were used in order to assess the wear behavior of the glasses, while the surface chemistry of the tribostressed balls and discs was investigated by means of XPS.

## 2 Experimental

### 2.1 Synthesis of the Glasses

Different chain length zinc polyphosphates were synthesized starting from stoichiometric mixtures of ammonium dihydrogen phosphate (Acros Organics, 99.9% extra pure) and zinc oxide (Alfa Aesar, 99.9%). The reaction for zinc metaphosphate is described in the following as an example:

$$2NH_4H_2PO_4 + ZnO \rightarrow 3H_2O + 2NH_3 + Zn(PO_3)_2$$

The reagents in powder form were melted in alumina crucibles (high-density alumina produced by Metoxit AG, Thayngen, Switzerland) at 1,473 K in a RHF 16/3 furnace (Carbolite<sup>®</sup>, Hope Valley, UK) and then quenched in a copper tray that had been previously cooled to 253 K. The samples obtained were clear and transparent, in the shape of round discs of 2–3 cm in diameter and 3–4 mm in thickness. After quenching, the samples were annealed at 623 K for 5 h in order to reduce internal stresses.

### 2.2 Characterization of the Glasses

XRD was used in order to ascertain that the samples were amorphous. The analyses were performed using a powder diffractometer STOE STADI P (STOE & Cie GmbH, Darmstadt, Germany) equipped with an image-plate detector and a Cu K- $\alpha$  X-ray source.

The microelemental analysis for oxygen was carried out by means of a RO-478 (Leco Corporation, St. Joseph, MI, USA). The phosphorus content was determined by the molybdovanadate method after microwave digestion and subsequent leaching ( $2 \times 50$  min) in concentrated sulfuric acid and perchloric acid at 483 and 508 K.

Transmission FT-IR spectra were acquired with a Nicolet<sup>™</sup> 5700 Fourier-transform infrared spectrometer (Thermo Electron Corporation, Madison, WI, USA). The experimental conditions are shown in Table 1. The glasses were ground with dried KBr and pressed into a pellet. The spectra were processed with OMNIC<sup>™</sup> software (V7.2, Thermo Electron Corporation, Madison, WI, USA). A single-beam spectrum of a bare KBr pellet was acquired before each measurement as a background spectrum.

**Table 1** Transmission FT-IR experimental conditions

Detector	DGTS/KBr
Resolution	$2 \text{ cm}^{-1}$
Number of scans	64
Scan velocity	0.6329 cm/s
Acquisition time	136 s
Gain control	1

### 2.3 Mechanical Polishing

Prior to the tribological tests, the samples were mechanically polished. Grinding was performed using P320, P600, P1200, and P2400 silicon carbide paper (Presi, Grenoble, France). The polishing was then performed using 3 and 1  $\mu\text{m}$  diamond paste on polishing cloths (Struers GmbH, Birmensdorf, Switzerland). The average surface roughness (Ra) was measured by AFM and found to be  $4.0 \pm 0.2$  nm. Ethanol was always used as a polishing lubricant, in order to remove the heat produced by friction and to avoid chemical changes at the surface. The samples were then kept in an ultrasonic bath in ethanol for 10 min prior to the tests.

The mechanically polished samples were characterized by XPS.

### 2.4 Tribological Tests

The tribological tests were carried out by means of a CETR UMT-2 tribometer with a ball-on-disk set-up. The load cell had a maximum load of 20 N and a resolution of 1 mN in two axes: normal load and friction force. 100Cr6 steel balls (6-mm diameter) were rubbed against the zinc metaphosphate polished discs. The roughness of the balls was characterized by means of a white-light profilometer (Sensofar PLu Neox, Sensofar-Tech SL., Terrassa, Spain) and was found to be  $0.277 \pm 0.003$   $\mu\text{m}$ . The tests were performed at room temperature in pure polyalphaolefin (PAO, Durasyn<sup>®</sup> 166, Tunap Industrie GmbH & Co., Mississauga, Canada) at two different loads, 5 and 7 N, with a constant sliding speed of 30 mm/min. Lubricated, rather than dry conditions were chosen, so as to resemble the rheological and heat transfer properties of a metal-metal lubricated contact. Four concentric wear tracks, separated from each other by 0.75 mm, were obtained on each disc. In order to achieve a conformal and reproducible flat on the ball, the running-in was performed on a 100Cr6 steel disc at 10 N and 300 mm/min for 2 h in the presence of pure PAO. Before the analysis balls and discs were cleaned in an ultrasonic bath for 10 min in *n*-hexane and gently wiped with a tissue paper. The tribostressed balls and discs were then examined with the aid of a light microscope.

### 2.5 XPS and Imaging-XPS

The XPS analyses were performed by means of a PHI Quantera SXM spectrometer (ULVAC-PHI, Chanhassen, MN, USA) equipped with an Al K $\alpha$  monochromatic source whose beam size ranges from 5 to 200  $\mu\text{m}$ . The Gauze input lenses collect the photoelectrons at an emission angle of 45° and direct them through the high-resolution

spherical capacitor analyzer to the 32-channel detector system. The spectrometer is also equipped with a low-voltage argon ion gun and a sample neutralizer for charge compensation. The calibration was performed using sputter-cleaned gold, silver, and copper as reference materials according to ISO15472:2001. The accuracy was found to be  $\pm 0.1$  eV. All the experiments were run at residual pressures below  $5 \times 10^{-7}$  Pa. Binding-energy values are reported in this work as means over three or more independent measurements with their corresponding standard deviations.

Survey spectra were acquired in fixed analyzer transmission (FAT) mode using a pass energy (PE) of 280 eV, while the high-resolution spectra were collected with a PE of 26 eV; the full width at half maximum of the peak height, FWHM, of the silver Ag 3d<sub>5/2</sub> signal for high-resolution spectra was 0.62 eV. The beam diameters used were 100 and 20  $\mu\text{m}$ , depending on the size of the feature analyzed. X-ray excited secondary electron images (SXI) were used in order to determine the topography and, thus, to be able to collect small area XPS spectra from the features present on the sample. When analyzing the glass discs the electron neutralizer was used in order to compensate for sample charging and the spectra were further corrected with reference to adventitious aliphatic carbon at 285.0 eV.

Imaging-XPS (i-XPS) was performed with a beam size of 20  $\mu\text{m}$  and a PE of 140 eV in snapshot mode; in these conditions the spectra were acquired over a BE range of 15.5 eV. The area of the maps was  $600 \times 600$   $\mu\text{m}^2$  and required 1–2 h of acquisition per map. Maps of the carbon signal, C 1s, were acquired in order to exclude the possibility of localized sample charging.

The spectra were processed using CasaXPS software (version 2.3.15, Casa Software Ltd, Wilmslow, Cheshire, UK). The background subtraction was performed using the Shirley–Sherwood iterative method. The product of Gaussian and Lorentzian functions was used for curve fitting. The maps were processed using Multi-Pak<sup>TM</sup> software (version 8.1c, ULVAC-PHI, Chanhassen, MN, USA).

The quantitative analysis was performed using the first-principles method valid for homogeneous samples [33]. The area of the peaks assigned to each component A is proportional to the atomic concentration after correcting for the sensitivity factor, calculated as follows:

$$s_A = \sigma_A(h\nu) \cdot \Lambda_{MA} \cdot L_A(\gamma) \cdot T(E_A),$$

where  $\sigma$  is the Scofield photoelectric cross-section [34],  $L_A$  is the asymmetry parameter, calculated according to [35], and  $T$  is the analyzer transmission function. The inelastic mean free path,  $\Lambda$ , was calculated using the TPP-2M formula [36] as a function of the material characteristics.

### 3 Results

#### 3.1 Characterization of Zinc Metaphosphate

The samples were characterized by XRD. All the samples investigated presented a broad peak, characteristic of amorphous compounds as shown in Fig. 1a.

The phosphorus content was determined by microelemental analysis and found to be  $27.6 \pm 0.1$  wt% (the expected value for the phosphorus content was 27.7 wt%).

The transmission FT-IR spectrum of the prepared glassy zinc metaphosphate is shown in Fig. 1b. Similarly to the FT-IR spectra of vitreous phosphate glasses with different compositions reported in the literature [37–40], the vibrational spectrum of amorphous zinc metaphosphate is characterized by complex peak shapes. The asymmetric peak between 1350 and  $1200\text{ cm}^{-1}$  with a maximum at  $1270\text{ cm}^{-1}$  can be assigned to the  $\nu_{\text{as}}(\text{PO}_2^-)$  of the  $Q_2$  units and to the  $\nu(\text{P}=\text{O})$  of the  $Q_3$  units [38, 40, 41]. In the region between 1050 and  $1150\text{ cm}^{-1}$  the characteristic stretching mode of the  $Q_1$  units ( $\nu_{\text{as}}(\text{PO}_3^{2-})$ ), which is usually very intense in IR spectra, was not detected, indicating that the phosphate tetrahedral structure did not undergo any disproportionation reaction as reported in [40].

In Fig. 2, the XPS spectra acquired on the as-received samples are shown. The samples were introduced into the spectrometer immediately after the synthesis, in order to minimize contamination from the lab environment. The survey spectra show a very low intensity carbon peak, which confirms that the level of contamination is very low, and aluminum is also present in trace amounts. In the O 1s high-resolution spectrum two components are resolved with two peaks at  $532.3 \pm 0.1$  eV and  $533.9 \pm 0.1$  eV. The peak at lower binding energy can be assigned to the NBO, while the second peak has to be assigned to the BO (see Scheme 2). Previous studies have shown that the

intensity ratio BO/NBO is directly correlated with the average chain length [31]. For the metaphosphate composition the theory predicts an infinite chain length with a corresponding BO/NBO of 0.5. In this work, the experimental BO/NBO was found to be  $0.45 \pm 0.05$ , in good agreement with the expected value. The phosphorus P 2p<sub>3/2</sub> was found at  $134.7 \pm 0.1$  eV, the Zn 3s at  $140.9 \pm 0.1$  eV and the Zn 2p at  $1022.7 \pm 0.1$  eV. Since the average is proportional to the ZnO to P<sub>2</sub>O<sub>5</sub> ratio, the corrected intensity P/Zn ratio can also be used as quantitative information on the glass composition. In our case, the P/Zn ratio on the as-received samples was found to be  $2.3 \pm 0.5$ , while the stoichiometric ratio would be 2. The composition of the glass calculated by means of the first-principles method is shown in Table 2.

#### 3.2 Characterization of Zinc Pyrophosphate and Zinc Orthophosphate

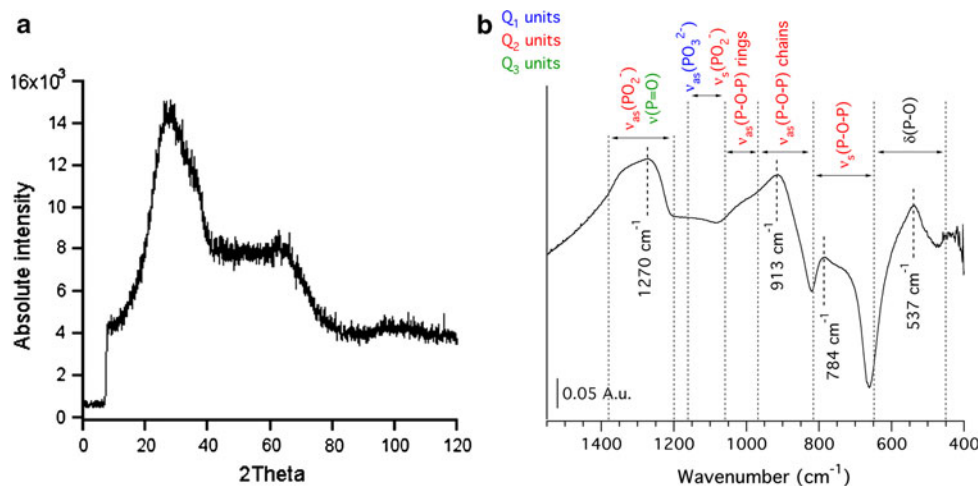
Zinc pyrophosphate and zinc orthophosphate were also synthesized and characterized, as for the metaphosphate case. The XRD results showed that the orthophosphate could only be obtained in the crystalline form, while the pyrophosphate was amorphous.

Information on the composition of the samples was obtained by elemental analysis and XPS; the results are summarized in Table 2.

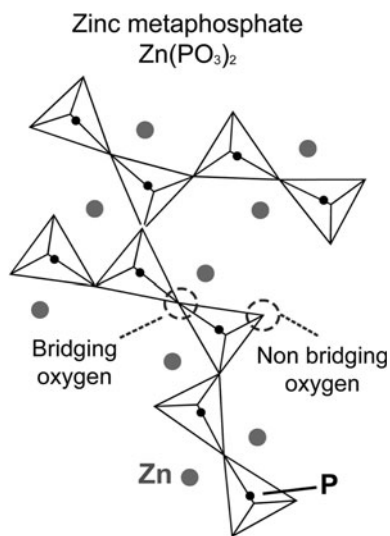
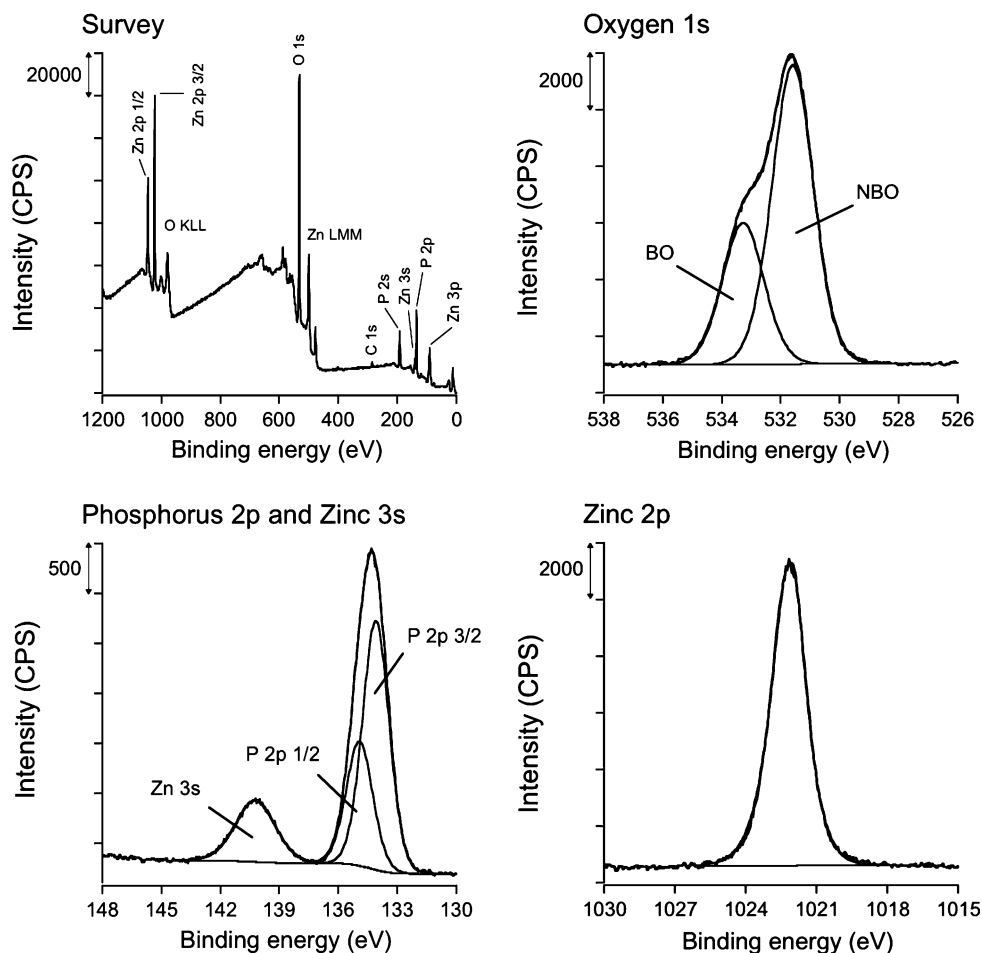
The BO/NBO ratio and the P 2p 3/2 binding energies for all the polyphosphate compositions are shown in Table 3. With increasing Zn content the chain length of the glass decreases. A lower BO/NBO ratio corresponds to shorter chain lengths, moreover a chemical shift toward lower binding energies is observed in the P 2p signal moving from longer to shorter chains.

All the FT-IR spectra were found to be in good agreement with the literature.

**Fig. 1** Characterization of the amorphous zinc metaphosphate samples: (a) X-ray diffraction spectrum; (b) transmission FT-IR spectrum



**Fig. 2** XPS high-resolution spectra of O 1s, P 2p, Zn 3s, Zn 2p signals and survey spectrum acquired on as received zinc metaphosphate



**Scheme 2** Schematic representation of the zinc metaphosphate structure

### 3.3 Friction and Wear

In Fig. 3, the values of the coefficient of friction at two different loads for steel-versus-steel and steel-versus-zinc-

metaphosphate tribopairs are shown. No significant changes of the friction were observed during a 2-h test. Since the coefficient of friction did not exhibit any change with sliding time, the average coefficient of friction values were calculated and are shown in Fig. 3. The coefficient of friction was always lower in the case of the steel-versus-zinc-metaphosphate tribopair. The wear coefficient of the balls was calculated from the flattened area on top of the balls, which was measured by means of optical microscopy. The dimensional wear coefficient was then calculated as worn volume divided by load and sliding distance (Fig. 4). The contact pressures were calculated and found to be around 200 MPa for the steel-versus-steel and 300 MPa for the steel-versus-metaphosphate tribopair. Compared to the steel-versus-steel tribopair, which does not exhibit any dependence of the wear coefficient with the applied load, lower values were obtained for the steel-versus-metaphosphate tribopair with the lowest value for the experiment performed at 5 N. The tribotacks on the discs were investigated with the light microscope: both the metallic samples appeared drastically damaged while, on the other hand, on the zinc metaphosphate samples the damage was very limited for both the investigated loads.

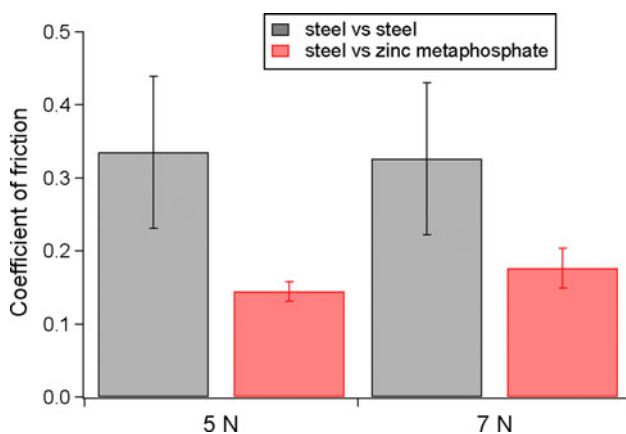
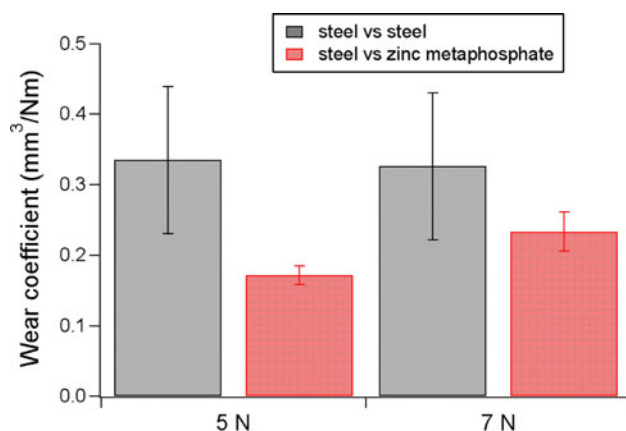
**Table 2** Characterization of zinc polyphosphates of different chain lengths

	Zinc metaphosphate	Zinc pyrophosphate	Zinc orthophosphate
XRD	Amorphous	Amorphous	Crystalline
Elemental analysis	[P] = $27.6 \pm 0.1$ wt%	[P] = $20.3 \pm 0.1$ wt%	[P] = $16.1 \pm 0.1$ wt%
XPS <sup>a</sup>	[P] = 32 wt%; [O] = 42 wt%; [Zn] = 27 wt%	[P] = 23 wt%; [O] = 36 wt%; [Zn] = 41 wt%	[P] = 19 wt%; [O] = 33 wt%; [Zn] = 48 wt%

<sup>a</sup> The maximum relative error in the quantitative analysis is 10%

**Table 3** BO/NBO ratios and P 2p 3/2 binding energies for the reference and the tribological samples

	Zinc ortho-phosphate	Zinc pyro-phosphate	Zinc metaphosphate	Mechanically polished metaphosphate	Metaphosphate after tribological test Non contact	Metaphosphate after tribological test In contact
BO/NBO	0.15	0.20	0.45	0.39	0.40	0.33
P 2p 3/2 BE	134.1 eV	134.3 eV	134.7 eV	134.7 eV	134.7 eV	134.3 eV

**Fig. 3** Tribological results; comparison between steel-versus-steel and steel-versus-zinc-metaphosphate tribopairs**Fig. 4** Wear coefficient of the ball; comparison between steel-versus-steel and steel-versus-zinc-metaphosphate tribopairs

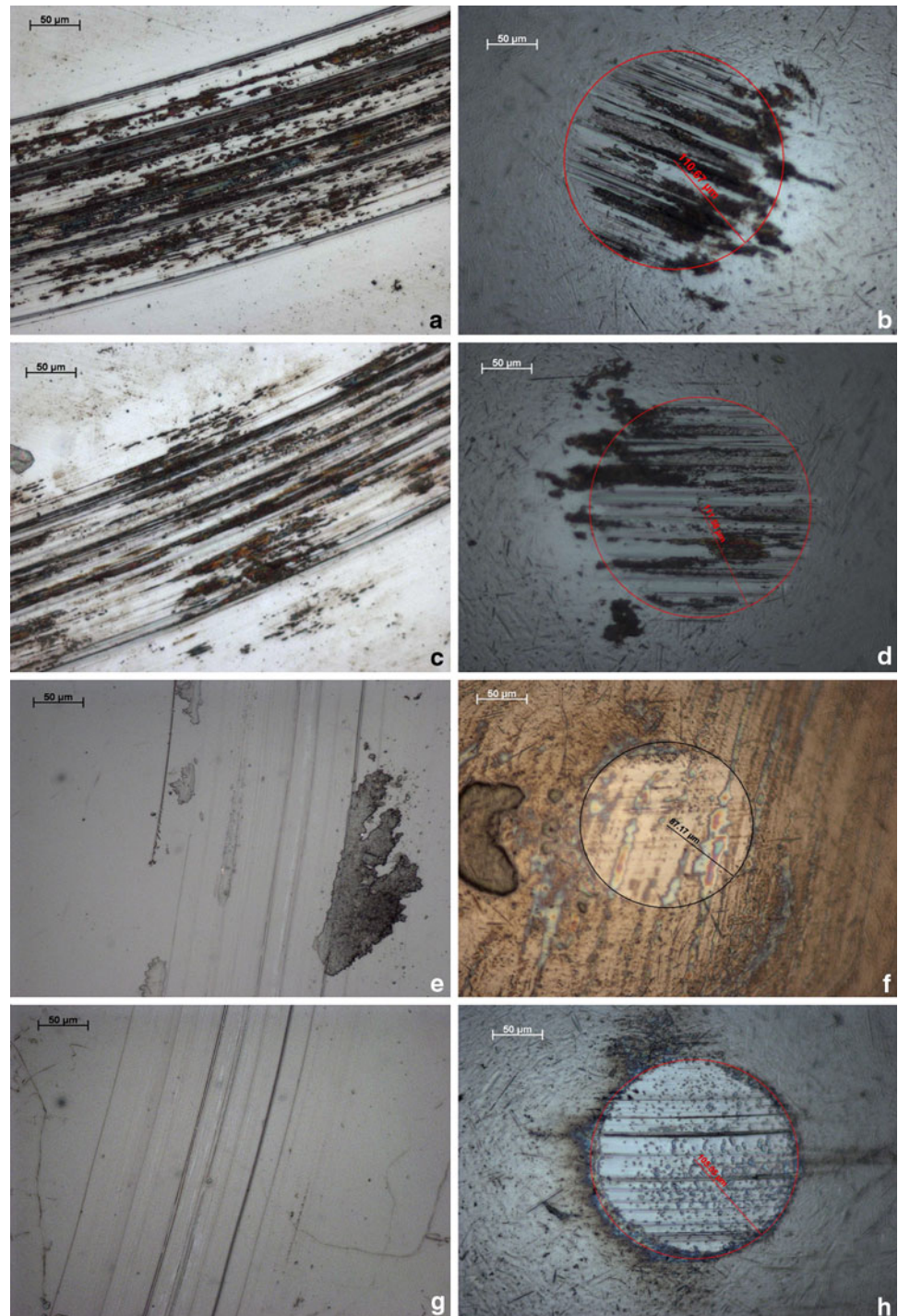
The dark large spots visible in Fig. 5b, c can be attributed to the debris originated from the ball and transferred to the disc. The tests shown in Figs. 3 and 4 were run using a new ball for each new test on a different track. Some other tests were performed using one single ball (previously flattened during a running-in experiment) and moving it from one radius to the other on the same sample: a decrease in the friction with the order of the test, and independently on the applied load, was observed. These findings suggest that during sliding the chemistry on the surface ball is changing. This change is able to affect both friction and wear. This is the reason why, in order to obtain reproducible data, a new ball was used for every test.

### 3.4 XPS Results

#### 3.4.1 Analysis of the Balls

Small-area XPS and i-XPS were used in order to characterize the balls after the tribological tests. The maps in Fig. 6 show the spatial distribution of the intensity of each element. For each pixel a complete spectrum was acquired, the calculated intensity of each spectrum corresponding to the color in the map. The oxygen O 1s signal was fitted using three different functions, one corresponding to the oxygen of the iron oxide at 530 eV, one to the NBO at 532.3 eV (this component may also include iron oxides and hydroxides), and one to the BO at a BE of 1.6 eV higher than the NBO peak. Three maps corresponding to the three chemical states were reconstructed using a linear-least-squares routine. The images show the presence of a uniform layer on the contact area, where zinc, phosphorus, bridging and non-bridging oxygen are present, while the signal of iron oxide is not detected. On the other hand, in

**Fig. 5** Light microscopy image of the wear track on the disc and the contact area on the ball for the steel-versus-steel tribopair at 5 N (**a, b**) and 7 N (**c, d**). Wear track on the disc and the contact area on the ball for the steel-versus-zinc-metaphosphate tribopair at 5 N (**e, f**) and 7 N (**g, h**)



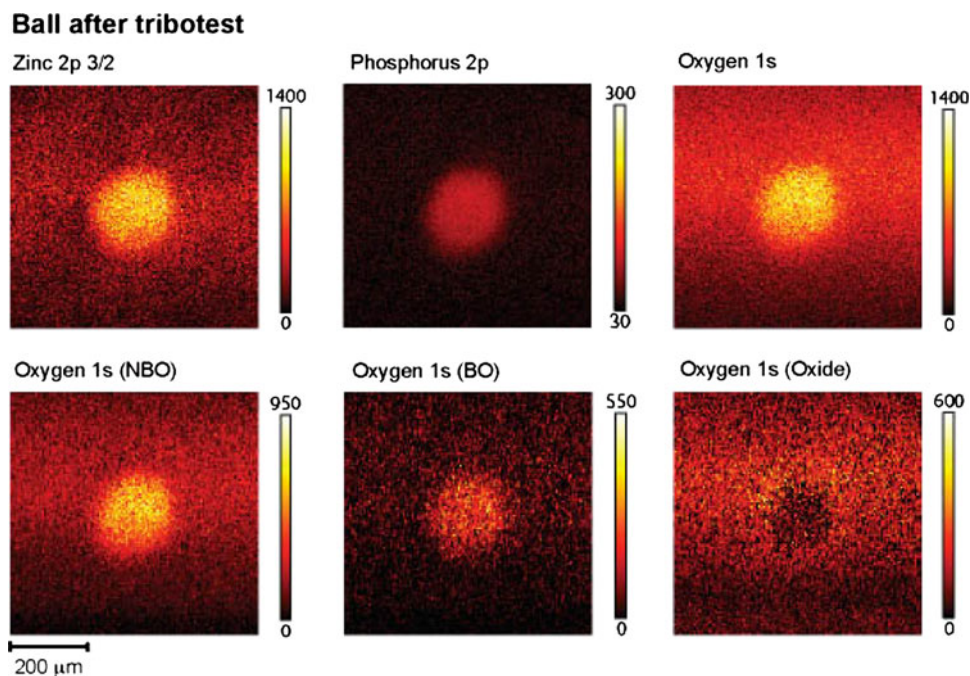
the non-contact region only the oxide and NBO signal are present. The diameter of the contact area in the chemical maps, around 150  $\mu\text{m}$  for the 5 N test as shown in Fig. 5, was comparable to that observed with the light microscope.

Small-area XPS was performed in three different locations: inside, outside, and at the border of the contact area (Fig. 7). Also in this case the O 1s spectra were curve fitted

with three components, i.e. oxide, NBO, and BO. In the O 1s spectra of the contact area only the BO and NBO components are present, while the oxide component is not detected. Inside the contact area the Fe 2p signal (Fig. 7c) is completely attenuated: considering that  $\lambda\cos(\theta)$  for the Fe 2p peak is 2 nm, it means that the glassy layer is at least thicker than 6 nm. Since in this case hydroxides do not contribute to the NBO signal, the spectra can be used for



**Fig. 6** i-XPS on the ball following the tribotests. Each pixel on the map corresponds to a complete spectrum: the color is proportional to the intensity of the spectrum calculated as the area under the peak



calculating the composition of the transfer film. Since the value of the BO/NBO intensity ratio was 0.3, it was possible to determine that the polyphosphate chain length was intermediate between a pyrophosphate and a metaphosphate.

The O 1s spectrum acquired at the border of the contact area shows the presence of the iron oxide signal at lower BEs, together with the BO and NBO signals. In this position the phosphorus peak is present with lower intensity, while neither the Zn 2p nor the Zn 3p signals could be detected.

In the non-contact region, the BO signal could no longer be detected.

The P 2p signal is intense in the contact area (P 2p<sub>3/2</sub> was found at  $134.6 \pm 0.2$  eV). In the border and out-of-contact regions, however, this signal was very weak. The position of the P 2p<sub>3/2</sub> is shifted toward lower BEs:  $134.2 \pm 0.2$  eV at the border and  $134.0 \pm 0.2$  eV in the out-of-contact region.

### 3.4.2 Analysis of the Discs

The wear tracks on the discs were characterized by i-XPS, and small-area XPS spectra were acquired both inside and outside the tribotracks. The O 1s intensity map is shown in Fig. 8. As described in the previous paragraph, the O 1s signal was curve fitted with the two characteristic signals of the polyphosphate glass: NBO at 532.3 eV and BO at 533.9 eV. The intensity of the total oxygen is lower inside the tribotrack, with the BO/NBO ratio being lower in the entire contact area (Fig. 9).

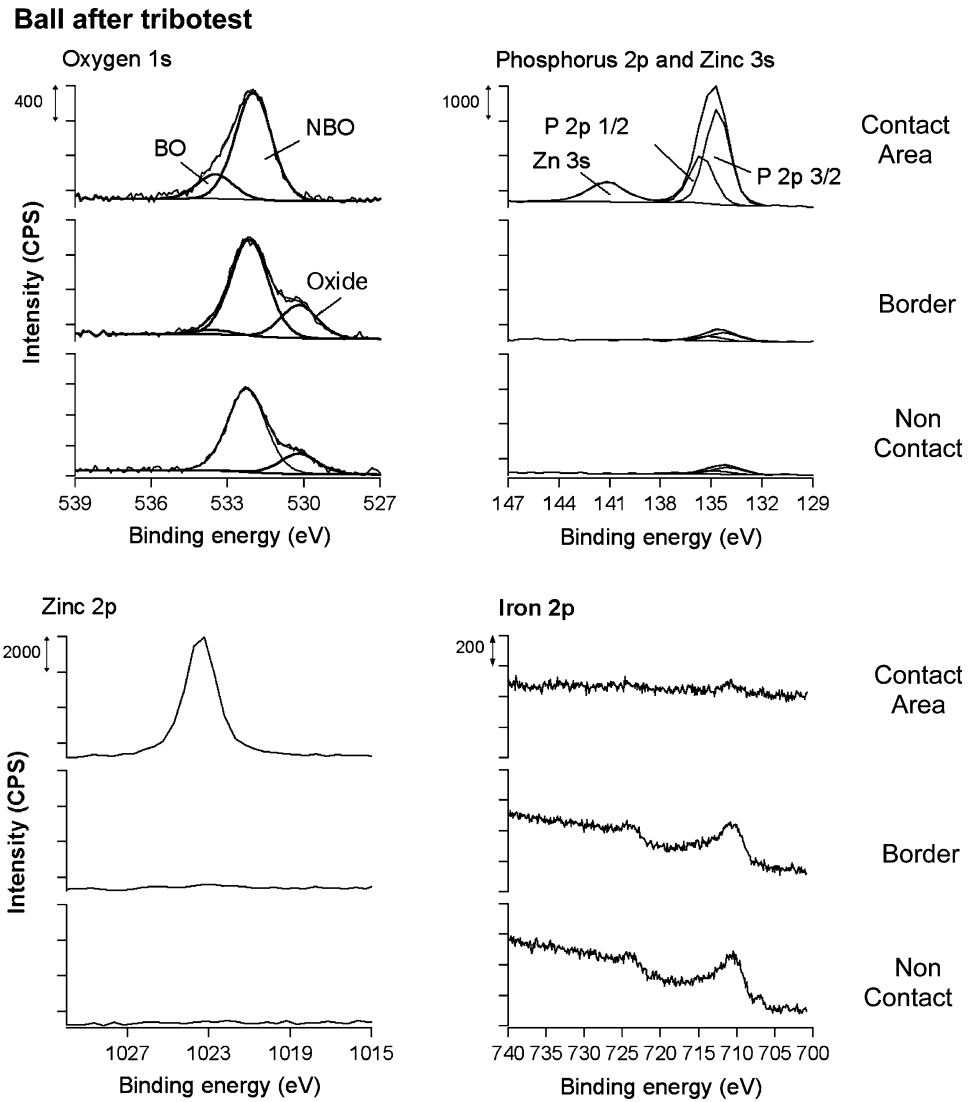
From the quantitative analysis of the small area XPS results (Fig. 8) a BO/NBO ratio of  $0.3 \pm 0.05$  was obtained in the contact area compared to the  $0.4 \pm 0.05$  obtained in the non-contact area (same value obtained for the mechanically polished samples). The NBO signal is shifted from  $532.4 \pm 0.1$  to  $532.1 \pm 0.1$  eV. Also the P 2p signal is shifted toward lower BEs: the signal was found at  $134.7 \pm 0.1$  eV for the non-contact region and  $134.3 \pm 0.2$  eV inside the tribotrack. These results suggest that the glass is depolymerized within the contact area as a consequence of the tribological test (see also Table 3).

The iron 2p peak is detected within the tribotrack, indicating a transfer of iron from the ball to the disc. The chemical state of iron is a mixture of oxides, hydroxides and, possibly, phosphates.

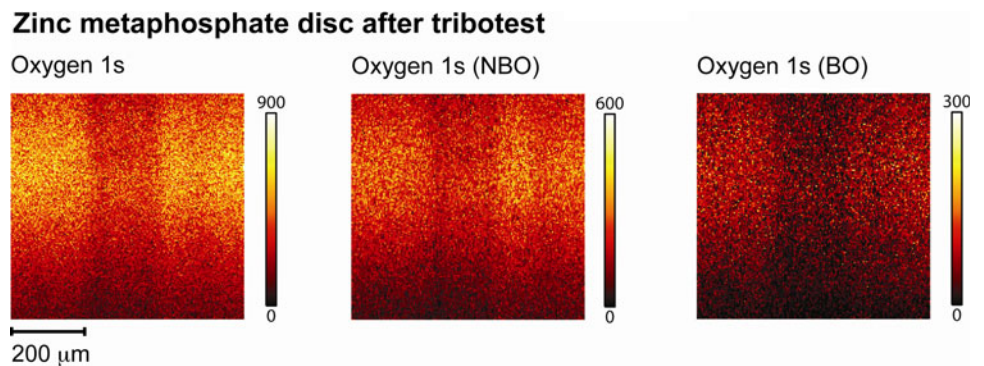
## 4 Discussion

In this article, a protocol for the synthesis and testing of bulk amorphous zinc metaphosphate glasses has been proposed. The characterization results confirm the expected composition and structure of the samples. By means of a surface-sensitive analytical tool, XPS, it was possible to investigate the tribochemical reactions taking place under sliding conditions. Studying the effect of tribochemical reactions on the fully formulated tribofilms is a very complex analytical problem. The experiments described in this work have the unquestionable advantage of using a homogeneous and well-characterized sample as a starting point.

**Fig. 7** Small-area XPS on the contact area of the ball after the tribotest



**Fig. 8** i-XPS of the tribotrack on the zinc metaphosphate disc



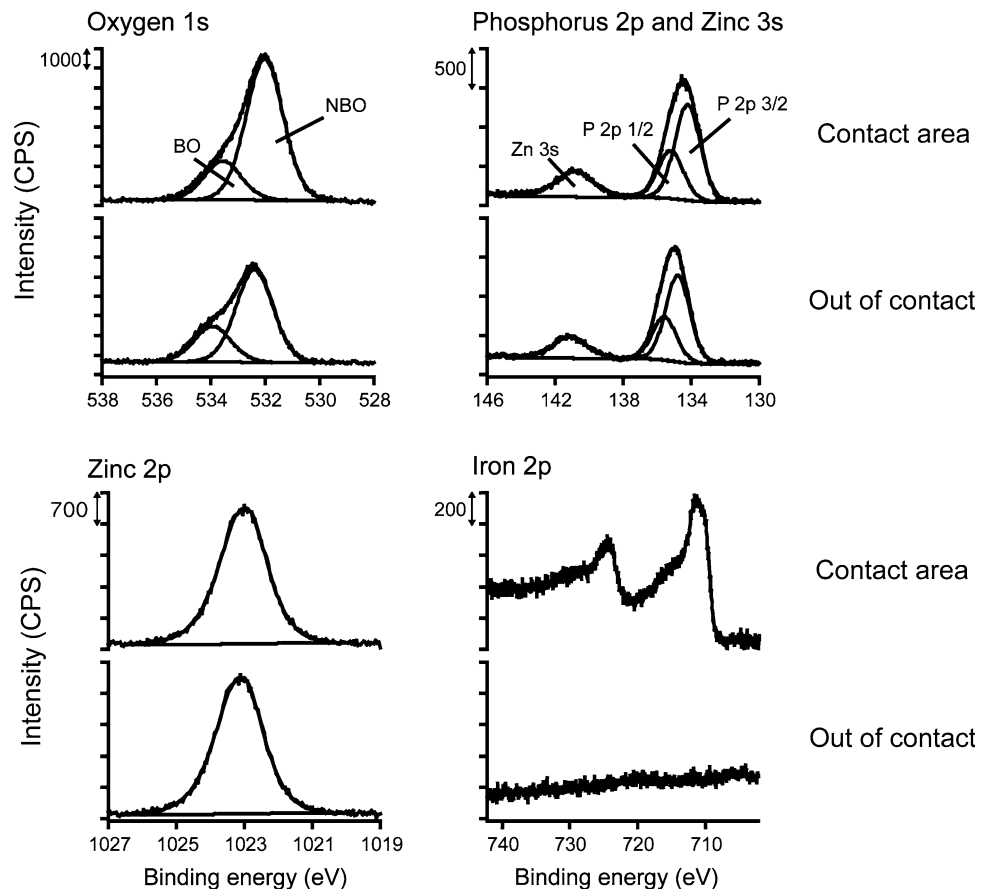
#### 4.1 Proposed Reaction at the Ball/Disc Interface

The composition and chain length of polyphosphate glasses can be quantitatively determined by XPS. Information on the average chain length of the glass is obtained using both

the BO/NBO ratio and the P 2p<sub>3/2</sub> binding energy [6, 8, 19, 42, 43]. Bridging and non-bridging oxygen are separated by approximately 1.6 eV in binding energy. Thanks to the use of the monochromatic X-ray source, which provides an energy resolution of 0.63 eV under these experimental

**Fig. 9** High-resolution spectra of the tribotrack on the zinc metaphosphate disc

### Zinc metaphosphate disc after tribotest



conditions, the two signals can be resolved and used for calculating the average chain length of the glass. The presence of contaminants on the glass surface turned out to strongly influence the quantitative analysis. Careful sample preparation and fast introduction into the UHV, which allowed the sample surface to be contamination-free and, as a consequence, the quantitative analysis to correspond to the expected composition, was found to be essential. The binding energy of the phosphorus 2p signal, being sensitive to the chain length of the glass, provides further experimental support for the results obtained from the BO to NBO ratio. These tools, combined with the surface sensitivity of XPS, were used in this investigation in order to gain an insight into the chemical changes occurring at the surface of tribostressed samples.

#### 4.1.1 Analysis of the Ball: Composition of the Transfer Film

The imaging-XPS of the ball shows a very clear contrast between the contact area and the non-contact area: a transfer film is present in the contact area and is mainly composed of zinc polyphosphates. The diameter of the

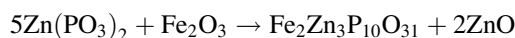
transfer film, around 150  $\mu\text{m}$ , is approximately the same as that of the flattened area on the ball. The detailed spectra acquired in the center of the contact area show the absence of an iron peak. Therefore, at this point the transfer film is thick enough to completely attenuate the iron peak (the layer is therefore thicker than 6 nm). Also at this point the signal of the O 1s spectrum at 530.0 eV, assigned to iron oxide, is absent; the two components used for the curve fitting correspond to the characteristic signals of polyphosphates, i.e., the BO and NBO peaks. The BO/NBO ratio was found to be 0.3 within the contact area. The average chain length is thus shorter than the metaphosphate composition of the disc before the tribological test. In the non-contact area the zinc signal and the BO signal are not detected: iron oxide is mainly present together with a very low-intensity phosphorus peak. At the border of the contact area a small peak assigned to the BO was detected together with the oxide peak, which means that a thinner layer of glass is present. However, neither of the zinc signals, Zn 2p and Zn 3s, could be detected. The only possible cation in this case is iron, i.e., the presence of iron phosphate is indicated. Moreover the phosphorus peak is shifted toward lower BE values suggesting the presence of shorter chain

lengths at the border of the area and, therefore, of a lateral compositional gradient in the transfer film.

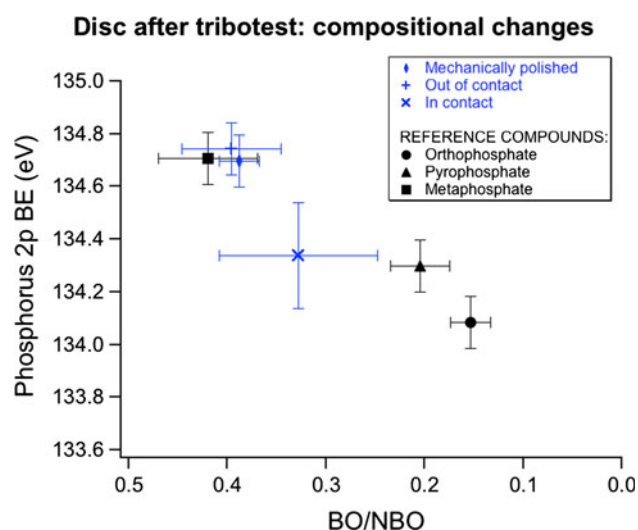
#### 4.1.2 Analysis of the Disc: Composition in the Tribotracks

The tribostressed area is clearly visible in the O 1s map (Fig. 8). Qualitatively it is already possible to observe in the chemical-state maps that the intensity of the BO signal is lower inside the contact area. Comparing the high-resolution spectra inside and outside the contact, the presence of a shorter-chain-length polyphosphate inside the tribotrack is supported by the lower BO/NBO value and the chemical shift of the phosphorus peak. In Table 3 and Fig. 10 these results are compared with the data obtained from reference zinc polyphosphate glasses of different chain lengths. The observed depolymerization was very reproducible despite the inhomogeneous appearance of the tribotrack in the optical microscope, where it was possible to observe islands of material transferred from the ball to the disc. The iron signal due to this transfer film was detected inside the tribotrack and suggests the presence of a mixture of iron oxides and phosphates.

A reaction mechanism for the tribochemical reaction between iron oxide and zinc polyphosphates has been proposed by Martin [11]. According to the HSAB (hard-and-soft acid–base) principle a hard base reacts preferentially with a hard acid and a soft base with a soft acid [10]. The formation of mixed zinc and iron glass is therefore the result of the reaction between the hard-base  $\text{PO}_4^{3-}$  with the hard-acid  $\text{Fe}^{3+}$ . As an example, the reaction between metaphosphate and iron(III)oxide is reported.



This reaction could be activated by high shear stress and



**Fig. 10** BO/NBO versus P 2p<sub>3/2</sub> BEs: comparison between reference and tribological samples

would explain the shortening of the polyphosphate chain and the formation of iron phosphate. This reaction normally takes place only at high temperatures (above 1,300 K). This means that enough energy has to be available for the reaction in the tribological system.

Moreover, since the mechanically polished samples showed a slight depolymerization compared to the samples in their initial state (see Table 3, Fig. 10), control experiments were carried out using quartz balls as inert tribopartners. These tribological tests were performed using exactly the same experimental conditions reported previously for the steel balls. The results showed no significant depolymerization for the 5 N tests, while at 7 N a slight depolymerization was present. Thus, it can be stated that the depolymerization of the glass can be caused not only by a chemical reaction with iron oxide or water, but can also occur as a consequence of high pressure and shear stress.

#### 4.2 Comparison with the Tribochemistry of ZnDTP Films

The composition of the tribological films formed in the presence of ZnDTP is heterogeneous, with longer polyphosphate chain lengths being present in the outermost layer and a layer of shorter-chain-length polyphosphates at the bottom, which also contains zinc, iron, and some sulfur and unreacted/partially reacted additive adsorbed on the surface [8–10, 44]. Many parameters can influence the composition and the thickness of the tribofilms. For example, longer-chain-length films are obtained when alkyl ZnDTPs are used instead of their aryl counterparts [45]. Tribological stress is able to activate the degradation reactions of ZnDTP and the tribofilm is already formed at ambient temperatures [6], where only a weak interaction of the additive with the steel surface is present in the absence of mechanical stress. On the other hand, thermal films, formed on the metallic surface in a heated oil solution, show a different composition compared to the tribofilms and do not resist rubbing [9, 46]. The tribofilms are, therefore, not only the result of a thermal degradation of the additive, but also of tribochemical reactions occurring at the interface between the lubricant and the steel surface, activated only by the sliding process. Temperature, pressure, composition, and degree of degradation of the additive also influence the chain length of the polyphosphate in the tribofilms.

A mechanism for the formation of a layered tribofilms involving the reaction between zinc polyphosphate and iron oxide has been proposed by Yin [3], but it has been very difficult to obtain any experimental evidence for these tribological reactions. Starting from fully formed ZnDTP tribofilms, Canning [9] has observed that long-chain polyphosphates convert to short-chain polyphosphates

upon rubbing in base oil, as has also been found in the present study. It has also been proven that an increased contact pressure leads to the formation of tribofilms characterized by shorter chain lengths [8, 9]. In this work, it has been shown that a long-chain phosphate glass is depolymerized as a consequence of sliding against steel. The reaction between zinc metaphosphate and iron oxide is activated by sliding and is more likely to take place on the ball surface, which undergoes the most severe mechanical stress. Moreover the tribological results have shown that the transfer film formed on the ball is able to reduce friction and prevent wear. The formation of a transfer film is common to many different tribological systems and it has been shown to be a very dynamic process [47]. The presence of an adhesive transfer film has also been found to correlate with the antiwear action in the case of ZnDTP [44] but more work is necessary, in order to establish whether the tribochemical reaction has a beneficial effect on the formation of the transfer film and its antiwear action.

## 5 Conclusion

From the data obtained in this work the following conclusions can be drawn:

- Polyphosphate glasses of different chain length have been synthesized and characterized. A protocol for tribological tests on the metaphosphate samples has been established.
- As a consequence of sliding against the zinc metaphosphate disc, a glassy transfer film is formed on the steel ball. In this area the chain length of the glass (calculated from the intensity ratio of the bridging and non-bridging oxygen signals BO/NBO in the O 1s XPS peak) is lower (BO/NBO: 0.3) than that of the glass before the test (BO/NBO: 0.4 for the mechanically polished disc).
- The transfer film formed on the ball is able to reduce friction and prevent further wear on the ball.
- A depolymerization of the polyphosphate glass was observed in the tribotracks present on the zinc metaphosphate discs. The material transfer from the ball to the disc resulted in the presence of iron in the tribostressed area on the discs.
- A tribochemical reaction between zinc metaphosphate and iron oxide at the ball/disc interface has been proposed. This leads to the formation of iron phosphate and causes the depolymerization of the glass. The depolymerization of the glass can also occur as a consequence of high pressure and shear stress, and thus a synergy between chemical and physical effects cannot be excluded.

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