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# Influence of the Cladding Structure in PMMA mPOFs Mechanical Properties for Strain Sensors Applications

Arnaldo G. Leal-Junior, Anselmo Frizera, *Member, IEEE*, Rui Min, Maria José Pontes, Andrea Fasano, Getinet Woyessa, Ole Bang, and Carlos Marques

**Abstract**—This paper presents a dynamic mechanical analysis (DMA) of a microstructured polymer optical fiber (mPOF). The fiber material is polymethyl methacrylate (PMMA), which is widely available commercially. The DMA is made by means of sequential strain cycles produced with an oscillatory load with controlled frequency to obtain the variation of the Young's Modulus with respect to temperature, frequency and humidity for mPOFs with 2, 3 and 5-ring hexagonal microstructured cladding. Results show that the 3 different cladding structures have similar Young's modulus on the stress-strain tests performed. Furthermore, the 3-ring structure presents the lowest Young's Modulus variation with temperature among the samples tested, whereas the 5-ring structure presents a Young's Modulus variation with frequency 25% lower than the 2 and 3-rings cladding structures. Regarding the humidity sensitivity, the 2-ring structure presented a 30% lower Young's Modulus variation for a 25% humidity increase. The results obtained provide guidelines for the cladding structure choice for strain or stress sensors applications when low cross-sensitivity with temperature, humidity and frequency is desired.

**Index Terms**—microstructured polymer optical fiber, dynamic mechanical analysis, polymethyl methacrylate.

## I. INTRODUCTION

POLYMER optical fibers (POFs) present intrinsic advantages over the conventional silica optical fibers regarding its material features, including higher strain limits, lower

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Young's modulus, fracture toughness and biocompatibility [1]. For these reasons, POF sensors have been applied in the sensing of different parameters like strain [2], temperature [3], refractive index [4], angle [5], liquid level [6], relative humidity [7] and acceleration [8], antibodies [9]–[11], and glucose [12], [13].

Although there is considerable research towards obtaining POFs with different materials, such as Zeonex [14], TOPAS [15] and polycarbonate (PC) [16], to date, polymethyl methacrylate (PMMA) is the most employed material for POF manufacturing [17]. There are some reports of polymer optical fiber Bragg gratings (POFBGs) in multimode POFs [18]–[20]. However, POFBGs are usually inscribed in single-mode POFs, such as microstructured POFs (mPOFs) that present a pattern of holes through the fiber separated by a certain pitch [21]. If the ratio between holes and pitch is lower than 0.43, the fiber is endlessly single-moded [22].

The polymer is a viscoelastic material that does not present a constant response with stress or strain [23] and a creep or relaxation may be observed both in stress-strain cycles [24] and long term tests with strain cycles applied [25]. In addition, the Young's modulus variation of the PMMA mPOF was characterized in a frequency range of 1 to 2 kHz in [26]. However, the effect of temperature and humidity on the Young's modulus variation of a PMMA mPOF also need to be characterized, since PMMA POFs present sensitivity to such parameters [27]. Furthermore, the Young's modulus variation with the temperature for bulk PMMA POFs and their relation with frequency variations are presented in [28]. However, the different POF microstructures can lead to different response to temperature, strain, humidity and frequency of the FBG, since it changes the stiffness of the POF, and since the air holes can act as thermal insulators. Moreover, the air-hole microstructure may also change the humidity response of the mPOF by means of increasing the contact area between the PMMA and the moisture if water penetrates into the holes. These effects can lead to a cross-sensitivity of temperature, humidity and movement frequency for strain or stress sensors.

In order to verify these assumptions, this paper presents a dynamic mechanical analysis (DMA) of mPOFs with different structures, where the DMA is comprised of sequential strain cycles by means of the application of an oscillatory load with controlled frequency. The DMA is applied to evaluate the

Young’s modulus variation with respect to temperature, humidity and frequency of PMMA mPOFs with hexagonal air-hole structures with 2, 3 and 5 rings. The analysis is made with respect to the general materials properties. Therefore, it helps in the development of the general POF sensor technology, instead of only a certain type of sensor, if the analysis was made with respect to a single sensor response.

## II. EXPERIMENTAL SETUP

The PMMA mPOFs employed in this work have a length of 10 mm with a hexagonal air-hole pattern with 2, 3 and 5 rings of holes, where their hole diameter, pitch, fiber diameter, and solid material area are presented in Table I. In addition, Fig. 1 presents the cross-sectional view of each mPOF employed. The mPOFs were fabricated at Technical University of Denmark (DTU) in two steps: first a PMMA rod is drilled with a predefined hole diameter and pitch, which is extruded to form a rod with lower diameter. Then, in the second step, the rod is sleeved with PMMA tubes, resulting in a new preform that is extruded again. Therefore, the inner part of the fiber is extruded two times, whereas the outer part is extruded only one time. In addition, the inner and outer part of the mPOFs were drawn in different times. Thus, it is possible that differences in the fabrication process, such as applied stress in the drawing or preform annealing resulted in this slight color difference between the inner and outer part of the fiber. Since the fiber is made with the same material (PMMA), we do not expect that such slight differences will lead to large differences in the material properties.

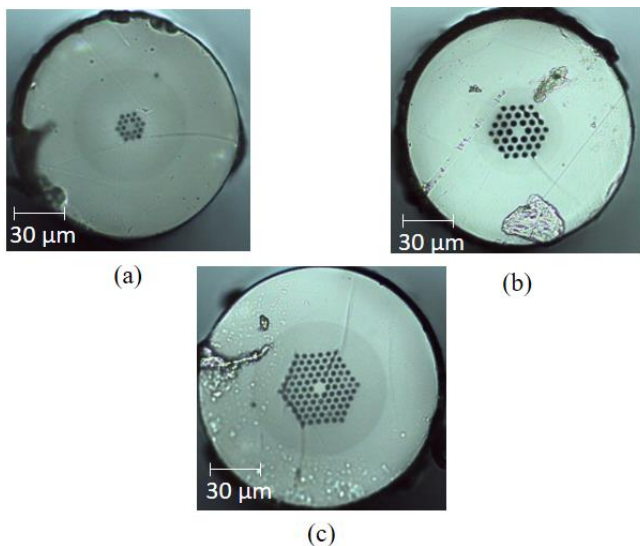


Fig. 1. Cross-sectional view of the mPOFs employed on the DMA. (a) 2-rings mPOF, (b) 3-rings mPOF and (c) 5-rings mPOF.

TABLE I  
GEOMETRICAL PARAMETERS OF THE PMMA MPOFS

Cladding Structure	Hole diameter/pitch (µm)	POF diameter (µm)	Solid Material Area (mm <sup>2</sup> )
2 ring hexagonal	1.70/3.95	138±13	1.49×10 <sup>-2</sup>
3 ring hexagonal	1.90/4.60	139±11	1.51×10 <sup>-2</sup>
5 ring hexagonal	1.70/3.95	140±15	1.52×10 <sup>-2</sup>

The cleaving of mPOFs is an important process prior to its connectorization, the cleaving parameters, such as temperature, speed, and angle, can influence the quality of the mPOF end facet [29]. For this reason, the employed mPOFs are cleaved with a razor blade perpendicular to the fiber at about 50°C. In some applications of POFBG sensors the POF need to be annealed, since the annealing can reduce the sensor hysteresis and provide higher sensitivity for certain type of sensors [14], [30], [31], all the samples were pre-annealed for 24 hours at 80°C.

After the preparation of the samples, the mPOFs are positioned on the dynamic mechanical analyzer DMA 8000 (Perkin Helmer, USA) presented in Fig. 2. The length of the fiber samples is about 10 mm, whereas each clamp has 3 mm length (see Fig. 2). Therefore, only 4 mm of the fiber will be under test. Thus, the longitudinal uniformity of the fiber will present lower influence in the tests results, since such small portion of the fiber is under stress, temperature, frequency or humidity variations. For this reason, we are not considering the longitudinal uniformity of the fiber in the performed tests.

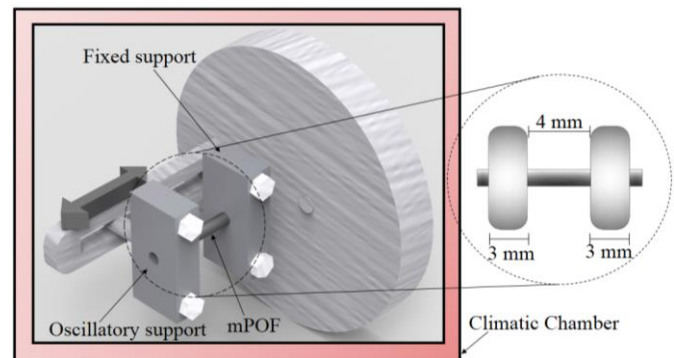


Fig. 2. mPOF samples fixation and geometrical parameters for the DMA tests.

The DMA is performed by applying an oscillatory load with controlled frequency and amplitude in the mPOF sample positioned as shown in Fig. 2. One end of the fiber is fixed in the oscillatory support, which applies the load on the sample, whereas the other end is fixed without movement. In addition, a load cell is positioned in within the fixed support to measure the stress in the sample and a linear variable differential transformer (LVDT) sensor is positioned in the oscillatory support to measure the fiber strain. In these tests, the strain is below 1% in order to keep the sample stress within the elastic region, where the well-known Hooke’s law can be applied to obtain the fiber Young’s modulus. Thus, the Young’s modulus is estimated by the ration between stress and strain in the fiber material. Additionally, the analyzer contains a climatic chamber for humidity and temperature control, and the control of the strain and frequency is made by means of the displacement and velocity control of the movable support illustrated in Fig. 2. First, a stress-strain test was made on the mPOFs with constant temperature of 25°C and humidity of 78% to evaluate the Young’s modulus of each fiber. Then, a temperature scan was made from 25°C (room temperature) to about 100°C, which is a temperature below the PMMA glass transition temperature (T<sub>g</sub>) [15]. Furthermore, tests with humidity variation from about 75% to 95% are made with the mPOFs to evaluate their humidity sensitivity. The frequency

of the strain cycles is also varied to evaluate the Young's modulus dependency on the frequency for frequencies lower than 10 Hz. Then, tests with the variation of both humidity and temperature are made to evaluate if the mPOFs presents a cross-sensitivity between these parameters.

### III. RESULTS AND DISCUSSION

The goal of the stress-strain cycles is to obtain the Young's modulus of each sample. For this reason, the cycles are made for strains below 0.25%, which is the region recommended for the evaluation of the Young's modulus in polymers by the standard ISO 527-1:2012, where the Young's modulus is obtained by the slope of the linear regression at each stress-strain curve. Figure 3 (a) presents the Young's modulus obtained for each cladding structure, where the mean and standard deviation were obtained from 3 tests with 3 different 10 mm lengths of the mPOF with that cladding structure. It is worth to mention that all cycles were made with a controlled temperature of 25°C and constant relative humidity of 78%. In order to show the effect of the temperature on the stress cycle, Fig. 3(b) shows the stress-strain curve for the 5-ring mPOF with 3 different temperatures, namely 25°, 70°C and 95°C in a constant humidity environment of 78%. In addition, the effect of the relative humidity on the stress cycle is presented in Fig. 3(c), where the 5-ring mPOF is submitted to 3 different relative humidity conditions (25%, 78% and 95%) in a constant temperature of 25°C.

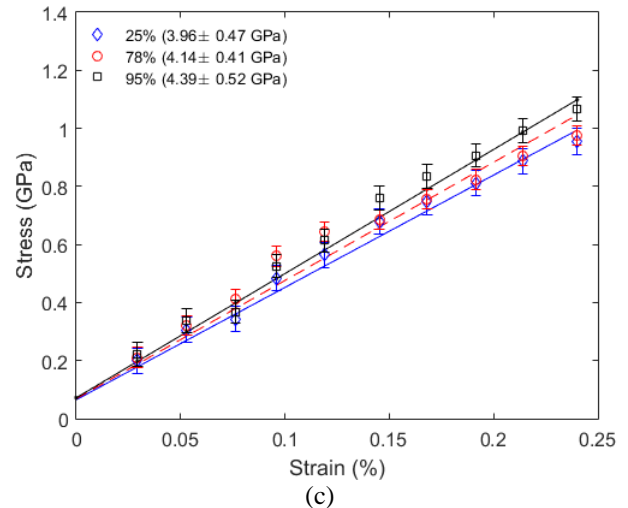
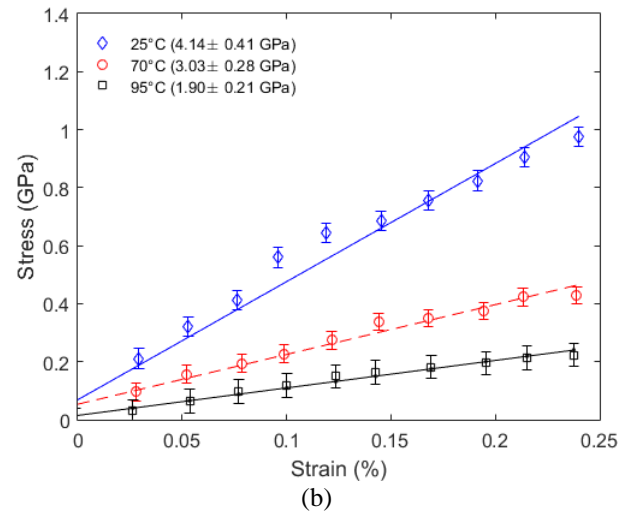
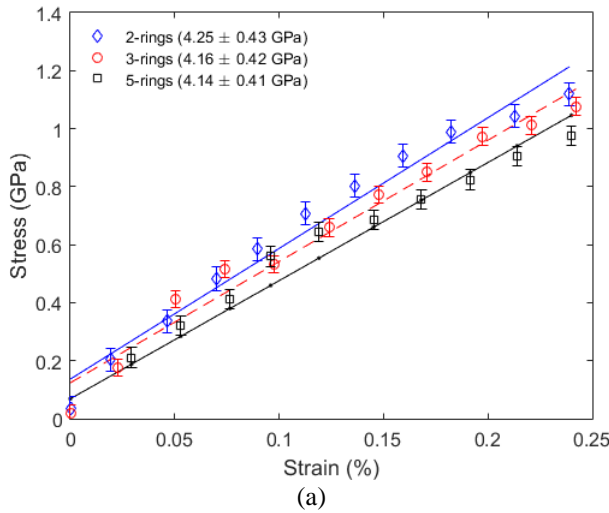


Fig. 3. (a) Stress-strain cycles and Young's Modulus for the 2-ring (blue), 3-ring (red), and 5 ring (black) mPOF. (b) Stress-strain curves for the 5-ring mPOF at 25°C (blue), 70°C (red) and 95°C (black). (c) Stress-strain curves for the 5-ring mPOF at humidity of 25% (blue), 78% (red) and 95% (black).

The results show that there could be a slight dependency of the Young's Modulus on the cladding structure, which can be due to the reduction of the cross-sectional area of solid material presented in Table I. However, the difference between the Young's Modulus of the 3 mPOF types is small, indicating that such difference is not significant. In addition, the standard deviation of each mPOF measurement is about 0.4 GPa, which is lower than the difference between the maximum Young's modulus, obtained for the 2-rings mPOF, and the minimum (for the 5-rings mPOF), where such difference is about 0.11 GPa. Regarding the temperature effect, there is a variation of the stress-strain slope due to the temperature that leads to a reduction of the fiber Young's Modulus. Similar behavior is found with the relative humidity variation. However, the temperature leads to higher variation of the modulus than the relative humidity.

In order to show the temperature effect in all cladding structures presented, temperature tests were made following the ASTM D5418 standard with each mPOF and the Young's modulus variation is presented in Fig. 4, where it can be seen that the 5-ring mPOF presented the higher variation of its Young's modulus.

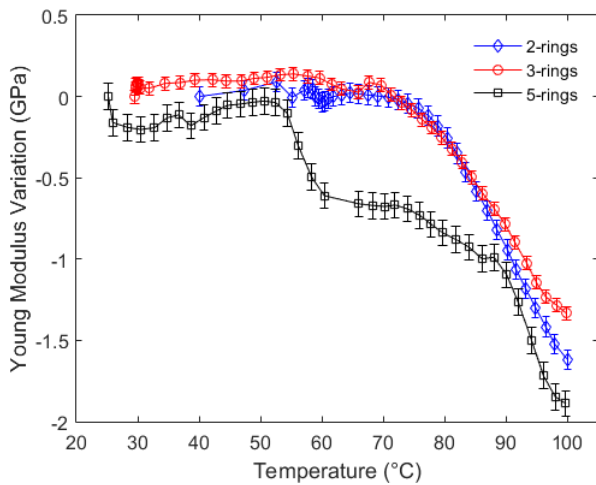


Fig. 4. Young's Modulus versus temperature for the 2-ring (blue), 3-ring (red), and 5-ring (black) mPOF.

The test is made with a temperature increase in steps of 2°C with a soak time of 1 minute as recommended by ASTM D5418 standard for temperature sweep in DMA. The strain cycle is made within about 1 second (frequency of 1 Hz) and the interval between the strain cycles is about 1 minute (soak time of 1 minute) when the temperature is increased by 2°C and another strain cycle is made. As the temperature is higher than 80°C and approaches the  $T_g$ , the 5-rings fiber presented a sharp decrease of its Young's Modulus, which can be related to the higher difference in temperature along the fiber cross-section that such microstructure presents. In contrast, the 2-rings fiber presents a lower temperature gradient along the mPOF cross-section, which leads to a linear decrease of the Young's Modulus as the temperature approaches the PMMA  $T_g$ . In addition, the Young's Modulus of the 2 and 3-rings mPOFs presented a lower variation in temperatures lower than 80°C than the ones of the 5-ring PMMA fiber. However, it should be noted that the 3-ring structure shows the lowest variation, which may also be related to the lower hole-to-pitch ratio than 2-ring and 5-ring fibers, since the fiber with lower hole-to-pitch ratio presented the lower temperature variation due to the highest homogeneity of the fiber cross-section. A lower Young's Modulus variation with the temperature may be preferred if a temperature sensor with lower strain cross-sensitivity is desired.

The Young's Modulus variation for the oscillatory load frequency variation from 0.01 Hz to 10.00 Hz is presented in Fig. 5. Such frequency variation is within the range of some applications of joint angle measurements [5].

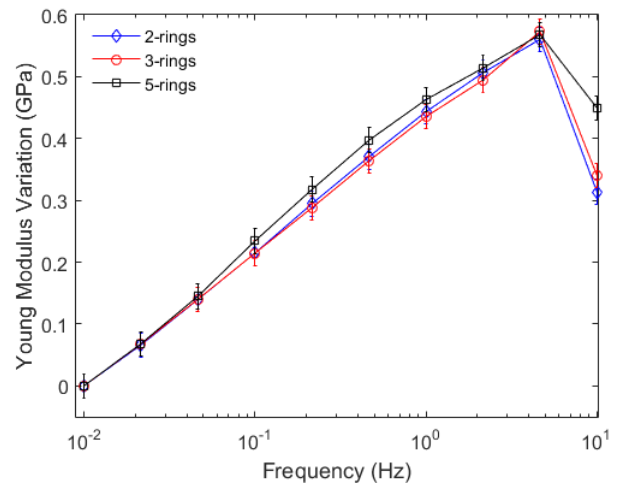


Fig. 5. Young's Modulus versus frequency for the 2-ring (blue), 3-ring (red), and 5-ring (black) mPOF.

Regarding Fig. 5, the variation of the Young's Modulus presented an upward trend for all the samples until the frequency of 5 Hz is reached. After that, the variation of the Young's Modulus starts to decrease and the lowest decrease among the samples tested is the one of the 5-ring structure, which was 25% lower than for the 2-rings structure. Such lower decrease indicates a lower cross-sensitivity with the movement velocity for the 5-ring cladding structure that can be an advantage for angle sensors for flexion/extension cycles [18] and accelerometers [9]. The lower decrease may be related to a natural damping that the air hole structure promotes on the fiber that will be higher on the 5-ring structure than on the structures with lower number of rings.

Finally, tests with relative humidity variation are made to evaluate the effect of the microstructure on the fiber humidity sensitivity. Figure 6 shows the variation of the Young's Modulus for a humidity variation from 75% to 95%, where the lower bound of the test is due to the room environmental conditions. Both upper and lower bounds are left to stabilize for about 30 minutes each.

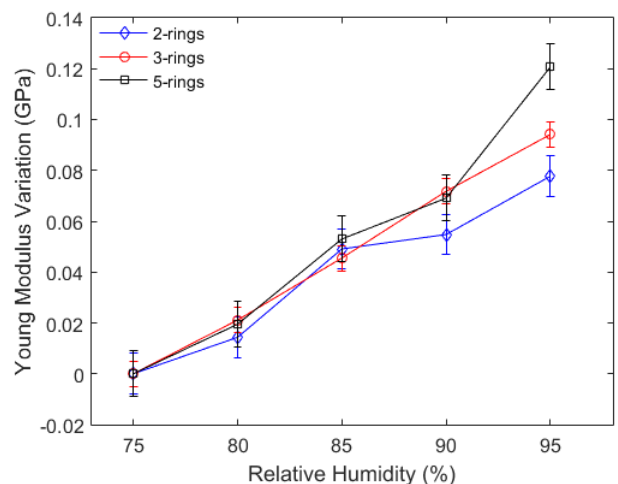


Fig. 6. Young's Modulus versus relative humidity for the 2-ring (blue), 3-ring (red), and 5-ring (black) mPOF.

Results show that the 5-rings cladding structure presents higher sensitivity than the others tested, whereas the lower

sensitivity was obtained in the 2-rings structure. Since the 5-rings structure presents more air holes, there will be more contact area between the PMMA and the humid air, which leads to a higher and faster water absorption of the 5-rings mPOF. For this reason, if it is desired a lower humidity cross-sensitivity, the 2-rings structure will present better performance than 3 and 5-rings cladding structures with a Young's Modulus variation of about 30% lower than the one of the 5-rings mPOF.

In order to present a broader comparison between the cladding structures, tests with simultaneous variation of the temperature and relative humidity are presented. In these tests, the strain cycles are made at 25°C, 70°C and 95°C with a relative humidity of 25%. Then, cycles are repeated with the same temperatures, but with the relative humidity at about 75% and, finally, at a relative humidity of 95% for each cladding structure analyzed. The results obtained for the 2-rings, 3-rings and 5-rings mPOFs are presented in Fig. 7(a), (b) and (c), respectively.

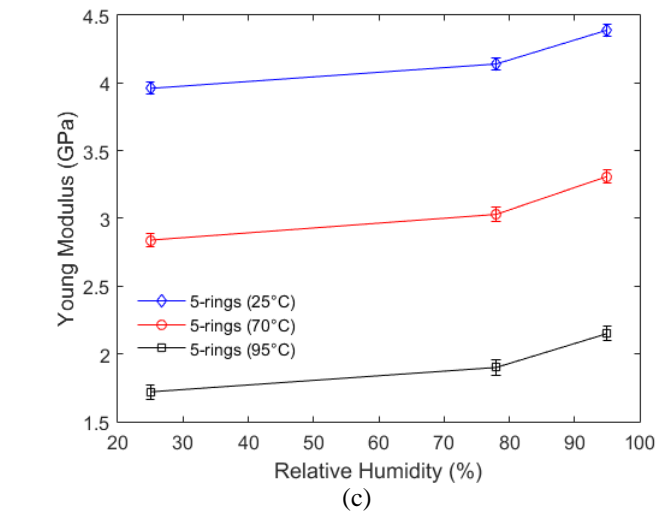
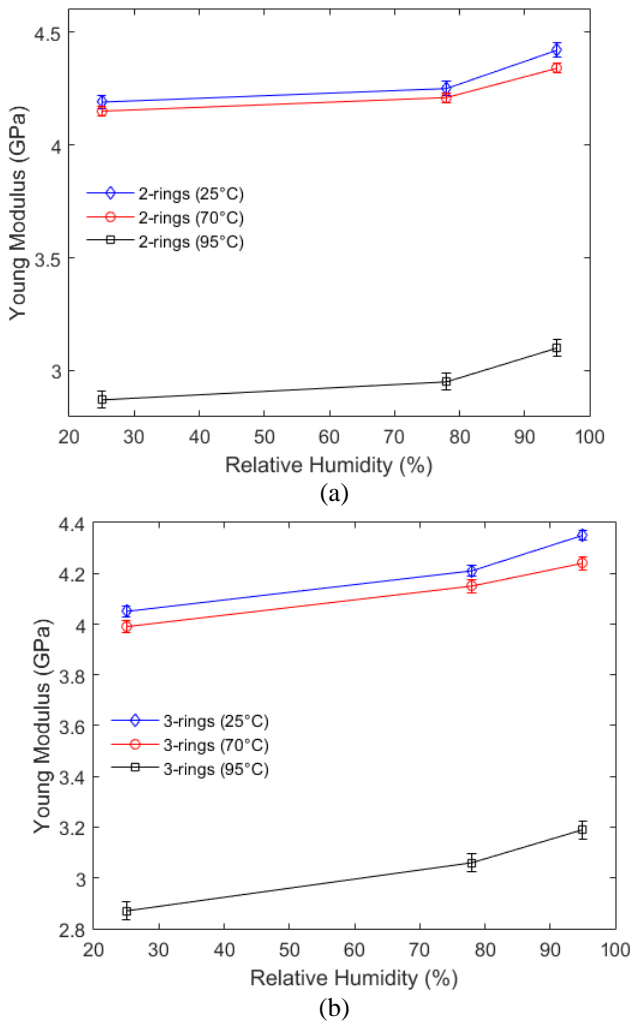


Fig. 7. Young's Modulus versus relative humidity in different temperature for (a) 2-ring, (b) 3-ring, and (c) 5-ring mPOF.

Regarding to Fig. 7, the offset of the curves is due to the temperature variation. For the case of 2-rings and 3-rings mPOFs there is only a slight variation of the Young's Modulus in temperatures lower than 70°C. For this reason, the blue and red curves of Fig. 7(a) and (b) are close to each other, whereas the 5-ring mPOF presented similar offset in all temperatures tested due its higher Young's Modulus variation with temperature that is demonstrated in both Fig. 4 and Fig. 7(c). In addition, the highest variation of the modulus with respect to the relative humidity was obtained in the 5-ring cladding structure in all temperatures tested (see Table II). In order to verify if there is a cross-sensitivity between relative humidity and temperature on the mPOF Young's Modulus, Table II presents the modulus variation for the cladding structures tested in each temperature.

The Young's Modulus presented almost constant variation in all temperatures tested for each of the three cladding structures analyzed. The highest standard deviation of the Young's Modulus when comparing the same relative humidity level at different temperatures was obtained in 3-rings mPOF. However, the standard deviation remains lower than 0.03 GPa, which can indicate that the temperature does not lead to high variations on the slope curve of the Young's Modulus with respect to the humidity variation.

TABLE II  
YOUNG'S MODULUS VARIATION IN EACH HUMIDITY AND TEMPERATURE TESTS FOR THE PMMA MPOFS

Cladding Structure	Young's Modulus variation at 25°C (GPa)	Young's Modulus variation at 70°C (GPa)	Young's Modulus variation at 95°C (GPa)
2 ring hexagonal	0.23±0.03	0.19±0.02	0.22±0.04
3 ring hexagonal	0.28±0.02	0.25±0.02	0.31±0.03
5 ring hexagonal	0.43±0.05	0.47±0.05	0.45±0.06

#### IV. CONCLUSIONS

This paper presented the comparison between different mPOFs Young's modulus variation with respect to temperature, frequency and humidity. The employed PMMA mPOFs present a hexagonal microstructure with 2, 3 and 5-

rings and are positioned on a DMA for the tests. A stress-strain test was made on each fiber and shows that there is not a significant variation of the Young's Modulus for different cladding structures and temperatures tests show that the 3-rings mPOF presents the lower variation of its Young Modulus with this parameter. In contrast, 5-ring structure presents a frequency dependency 25% lower than the other tested mPOFs, providing advantages on accelerometers and oscillatory movement assessment applications. Finally, the humidity tests show that the 2-ring structure presents a sensitivity 30% lower than the others mPOFs. The humidity tests were repeated in different temperature conditions and there was not a considerable variation of the mPOF sensitivity to relative humidity when the temperature is changed. Such tradeoff points towards the possibility of optimization of the cladding structure of an mPOF for each sensor application, which will be investigated in future works.

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