

Phase evolution and electrical behaviour of samarium-substituted bismuth ferrite ceramics

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Abstract

$\text{Bi}_{1-x}\text{Sm}_x\text{FeO}_3$ ($x = 0.15-0.18$) ceramics with high density were produced using spark plasma sintering. The effects of composition, synthesis conditions and temperature on the phase evolution were studied, using XRD, TEM and dielectric spectroscopy. The coexistence of the ferroelectric *R3c*, antiferroelectric *Pnam* and paraelectric *Pnma* phases was revealed, with relative phase fractions affected by both calcination conditions and Sm concentration. Experiments on powdered samples calcined at different temperatures up to 950 °C suggest higher calcination temperatures promote Sm diffusion, allowing samples to reach compositional homogeneity. The structural transitions from the *Pnam* and *R3c* phases to the *Pnma* phase were comprehensively investigated, with phase transition temperatures clearly identified. The dielectric permittivity, electrical resistivity and breakdown strength were increased upon Sm-substitution, while ferroelectric switching was suppressed. The polarization-electric field loop became increasingly narrow with increasing Sm-content, but double hysteresis loops, which may reflect a reversible antiferroelectric to ferroelectric transformation, were not observed.

1. Introduction

BiFeO_3 (BFO) is a room-temperature multiferroic material with a rhombohedrally distorted $R3c$ perovskite structure [1]. It shows a high ferroelectric (FE) polarization of *ca.* 90-100 $\mu\text{C cm}^{-2}$ along the [111] direction, with a ferroelectric Curie point of 825 °C and an antiferromagnetic Néel temperature of 370 °C [1, 2]. However, the synthesis of pure BFO is difficult due to the narrow temperature window of compound formation, with secondary phases such as $\text{Bi}_2\text{Fe}_4\text{O}_9$ and $\text{Bi}_{25}\text{FeO}_{40}$ often formed [3, 4]. Additionally, the BFO system always exhibits significant electrical conductivity, due to the reduction of Fe^{3+} to Fe^{2+} and evaporation of volatile bismuth oxide [5]. It is reported that A-site substitution by rare-earth cations could compensate for the volatilization of bismuth oxide and suppress the formation of oxygen vacancies to reduce the electrical conductivity [6, 7]. Meanwhile, rare-earth substitution can enhance the dielectric and electromechanical properties [8-10], making the material a potential candidate for advanced piezoelectric, ferroelectric and multiferroic applications [1, 11, 12].

A large number of studies have focused on the structural evolution in the phase diagrams of binary $\text{BiFeO}_3\text{-REFeO}_3$ systems (where RE=La, Sm, Nd *etc.*) [13-18]. The isovalent substitution of bismuth by rare-earth elements leads to a structure transformation from the rhombohedral FE $R3c$ phase to an orthorhombic paraelectric $Pnma$ phase, with the formation of a morphotropic phase boundary (MPB) [7, 16, 19]. An orthorhombic antiferroelectric (AFE) $Pbam$ phase is reported to be formed in rare-earth-substituted BFO across the MPB region, where it coexists with the $R3c$ and $Pnma$ phases [8, 20]. However, there is an ongoing debate on the details of the structure-composition relationships in $\text{BiFeO}_3\text{-REFeO}_3$ systems [9, 13, 21].

In thin films, Kan *et al.* found that the structural behaviour of $\text{BiFeO}_3\text{-REFeO}_3$ systems is dictated by the average ionic radius of the A-site cations [21, 22]. However, this relationship is less clear in bulk ceramics, with different rare-earth systems exhibiting different phase behaviour irrespective of the average size of the A-site cation. This is further complicated by the effect of synthesis conditions and the level of substitution, which have also been shown to influence the phase distribution [15, 23].

The origin of the double polarization-electric (P-E) hysteresis loops observed in thin films is also controversial. It was initially considered as a result of an electric field-induced AFE to FE phase transition [8, 20]. However, Kan *et al.* suggested that the double hysteresis loops were linked to an electric field-induced paraelectric (PE) to FE phase transition [21]. Using first principles calculations, these authors found that the energy of the PE *Pnma* phase was closer to that of the ground state *R3c* phase, compared to that of the AFE *Pbam* phase [21]. Thus, it is easier for the *Pnma* phase rather than the *Pbam* phase to transform into the *R3c* phase under an external electric field. To date, it is still difficult to obtain saturated polarization-electric field (P-E) hysteresis loops in rare-earth doped BiFeO_3 ceramic samples, due to their low breakdown field and high leakage current [24-27]. Double hysteresis loops have never been observed in BiFeO_3 -based ceramic samples.

The focus of the current work is on Sm-substituted BiFeO_3 , where double P-E loops have been observed in thin films. It is agreed that $\text{Bi}_{1-x}\text{Sm}_x\text{FeO}_3$ exhibits an *R3c* structure at $x < 0.1$ [16, 28, 29]. However, the structure of compositions at and above $x = 0.1$ differs between thin films and ceramics. The MPB region is suggested to be located at $x = 0.14$ in $\text{Bi}_{1-x}\text{Sm}_x\text{FeO}_3$ thin films [8]. Substitution by samarium in $\text{Bi}_{1-x}\text{Sm}_x\text{FeO}_3$ (at $x \geq 0.1$) thin films destabilizes the long-range

FE state to form localized AFE clusters within the FE matrix in the compositional range $0.10 \leq x \leq 0.14$, with a *Pnma* phase observed in compositions with $x > 0.14$ [30]. In bulk samples, Khomchenko *et al.* reported that $\text{Bi}_{0.85}\text{Sm}_{0.15}\text{FeO}_3$ was a mixture of *Pbam* and *Pnma* phases, while a pure *Pnma* structure was found at $x = 0.2$ [28]. Troyanchuk *et al.* reported that $\text{Bi}_{1-x}\text{Sm}_x\text{FeO}_3$ ceramics consisted of a mixture of polar and antipolar phases, in the range $x = 0.11-0.13$, while the antipolar phase was dominant at $x = 0.13$ [29]. In particular, the antipolar phase was reported to have *Pnam* symmetry ($\sqrt{2}a_c \times 2\sqrt{2}a_c \times 4a_c$, where a_c is the pseudo-cubic perovskite cell dimension), with double the unit cell volume of the antipolar phase reported in other studies ($\sqrt{2}a_c \times 2\sqrt{2}a_c \times 2a_c$ in space group *Pbam*) [13]. The pure antipolar state was only obtained at $x = 0.14$, while traces of the *Pnma* phase were detected at $x = 0.15$ and the pure *Pnma* phase was obtained at $x = 0.18$ [29].

The calcination temperature has also been found to influence the phase distribution in the $\text{Bi}_{1-x}\text{Sm}_x\text{FeO}_3$ system [23, 31]. Khomchenko *et al.* found that a low calcination temperature of 850°C led to the coexistence of the *Pbam*, *R3c* and *Pnma* phases in the $x = 0.15$ ceramic [23]. The phase separation was attributed to an inhomogeneous distribution of Bi^{3+} and Sm^{3+} cations caused by the low calcination temperature. The *R3c* phase was absent after calcining at a higher temperature of 950°C . Even though preliminary phase diagrams of rare-earth doped BiFeO_3 have been proposed, details of the transitions from the *Pbam* and *R3c* phases to the high temperature *Pnma* phase remain vague. The identification of the characteristic temperatures associated with these transitions is complicated by the coexistence of several phases in the MPB region [13, 21].

In this work, the phase evolution in $\text{Bi}_{1-x}\text{Sm}_x\text{FeO}_3$ ceramics has been studied, including the effect of composition and temperature. X-ray diffraction and transmission electron microscopy were carried out to investigate the presence of an antiferroelectric structure. The temperature dependence of the X-ray diffraction patterns and dielectric properties were used to identify the temperatures associated with the different phase transitions. Polarization-electric field measurements were performed, searching for the possible presence of double hysteresis which could be related to an antiferroelectric to ferroelectric field-induced transition.

2. Experimental Methods

2.1 Preparations

The $\text{Bi}_{1-x}\text{Sm}_x\text{FeO}_3$ compositions ($0.15 \leq x \leq 0.18$) were selected as they are expected to show an MPB region, characterized by the possible presence of an AFE structure [8]. The starting materials Bi_2O_3 (Alfa Aesar, UK, 99.975%), Sm_2O_3 (Alfa Aesar, UK, 99.9%) and Fe_2O_3 (Alfa Aesar, UK, 99.9%) were mixed and milled in ethanol using a planetary ball mill (Nanjing machine factory, China) for 4 h. The dried powders were calcined at selected temperatures (810 °C, 830 °C, 850 °C, 910 °C or 950 °C) for 4 h to identify the optimum calcination conditions. In each case, the synthesized powder was further milled in ethanol for 4 h to obtain fine homogenous particles. The $\text{Bi}_{1-x}\text{Sm}_x\text{FeO}_3$ ceramics ($x = 0.150, 0.160, 0.165$, denoted as BSF15, BSF16 and BSF16.5, respectively) were sintered at 800 °C from powder calcined at 910 °C, using spark plasma sintering (SPS) (HPD-25/1 FCT systeme GmbH) at a pressure of 80 MPa, with a heating rate of 100 °C min^{-1} and a dwell time of 5 min. The $\text{Bi}_{0.82}\text{Sm}_{0.18}\text{FeO}_3$ (denoted as BSF18)

ceramic was sintered at 800 °C from powder calcined at 950 °C using the same sintering procedures. The SPS sintered samples were subsequently annealed in a muffle furnace (Carbolite HTF 1800, UK) at 700 °C in air for 15 h to remove the diffused carbon from the graphite during the SPS processing [32, 33].

2.2 Structure analysis

The structures of the calcined powders and sintered ceramics were analysed by X-ray powder diffraction (XRD, X'pert Pro, PANalytical, Almelo, The Netherlands) at room temperature over the 2θ range 5° to 120°, in steps of 0.0167°, with an effective count rate of 200 s per step, using Ni filtered Cu-K α (1.5418 Å) radiation. Elevated temperature measurements were carried out on BSF15 and BSF18 calcined powders using an Anton-Paar HTK-16 high-temperature camera. The data were collected at 25 °C and at 50 °C intervals from 100 °C to 950 °C. The sample was held at each temperature for *ca.* 45 min during data collection. Diffraction patterns were acquired over the 2θ range 5° to 120°, in steps of 0.0167°, with an effective count rate of 50 s per step. The temperature calibration was carried out by measuring the phase transition of KNO₃ and melting points of high purity KNO₃, KI, NaCl and K₂SO₄ standards. All the XRD patterns were modelled by the Rietveld method using the General Structure Analysis System (GSAS) software [34]. The initial structural models were based on those reported by Khomchenko *et al.* for the AFE phase with space group *Pnam* and the PE phase with space group *Pnma* [35] and by Moreau *et al.* for the FE phase with space group *R3c* [36]. The microstructure was studied using scanning electron microscopy (SEM, FEI Inspect F).

Selected area electron diffraction (SAED) patterns were recorded on BSF15 calcined powder using a JEOL 2010 transmission electron microscope. For this measurement, the powder was crushed and dispersed in ethanol and a drop of this suspension was placed on a copper grid covered with a holey carbon film.

2.3 Electrical characterization

For the electrical measurements, the electrodes were deposited on the sintered pellets with fired-on silver paste (Johnson Matthey, E1100). Frequency-dependent dielectric permittivity and loss were measured using an Agilent 4294 precision impedance analyser. The temperature dependence of dielectric permittivity and loss was measured from 25 °C to 450 °C, with a heating rate of 5 °C min⁻¹, at selected frequencies (50 kHz, 100 kHz, 500 kHz and 1 MHz), using an Agilent 4284A LCR meter connected to a furnace (Lenton, LTF). The P-E hysteresis loops were measured by a ferroelectric hysteresis measurement tester (NPL, UK), at a frequency of 10 Hz [37].

3. Results and Discussion

The XRD patterns of the calcined powders (supporting information Figure S1) indicate that a small amount of Bi₂Fe₄O₉ (JCPDS No. 25-0090) is formed as a secondary phase in powders calcined at low temperatures, but is absent at 910 °C and above. Selected area electron diffraction (SAED) patterns of BSF15 powder calcined at 910 °C are shown in Figure 1 (a-f). The analysis of the reflection conditions ($0kl: k + l = 2n$; $h0l: h = 2n$; $h00: h = 2n$; $0k0: k = 2n$; $00l: l = 2n$) on the SAED patterns points towards the *Pnam* (No. 62) space group, which differs from the

previous studies reporting the presence of an AFE structure with space group $Pbam$ (No. 55) [13, 18]. The unit cell based on the $Pnam$ space group has the following relation to the pseudo-cubic perovskite cell: $a = \sqrt{2}a_c$, $b = 2\sqrt{2}a_c$, $c = 4a_c$, where a_c is the unit cell parameter of the pseudo-cubic perovskite, and is illustrated diagrammatically in Figure S2. Thus, the $0k0$ reflection corresponds to $\frac{1}{4}(hh0)$ in the cubic sub-cell (Figure 1a), while the $00l$ reflection in the $Pnam$ space group corresponds to $\frac{1}{4}(00l)$ in the cubic sub-cell (Figure 1c). The appearance of the forbidden reflections $00l$ ($l \neq 2n$) on the $[210]$ and the $[110]$ patterns, as well as $h00$ ($h \neq 2n$) and $0k0$ ($k \neq 2n$) on the $[001]$ and the $[011]$ patterns, are due to double diffraction; this follows from the fact that the reflections disappear when rotating the crystal away from the perfect orientation around the corresponding axis. Figure 1f shows the diffraction pattern of a crystal with 60° -rotation twins, oriented along the $[401]$ direction in the structure.

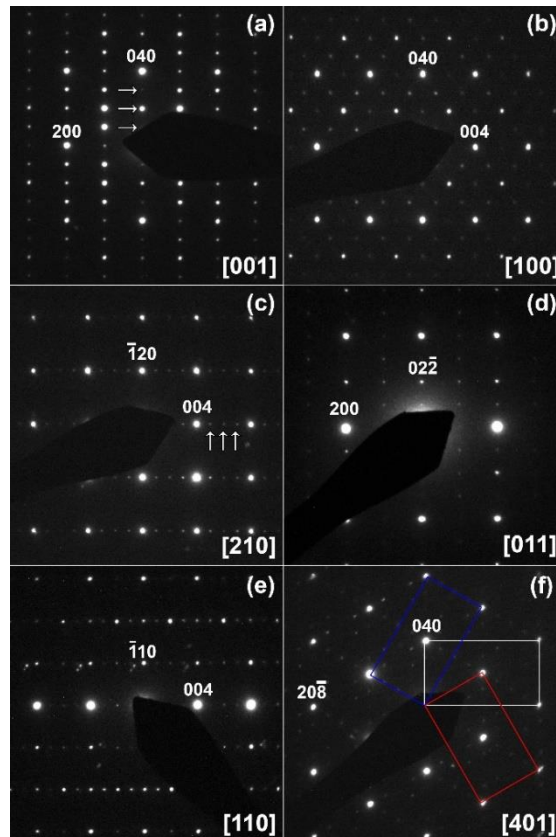


Figure 1. SAED patterns of BSF15 taken along main zone axis (a) [001], (b) [100], (c) [210], (d) [011], (e) [110] and (f) [401] from 60°-rotation twins; white arrows mark $\frac{1}{4}(hh0)$ and $\frac{1}{4}(00l)$ in the cubic sub-cell in patterns (a) and (c), respectively. Red, blue and white rectangles mark unit cells of three rotational twins.

The fitted diffraction profile of the BSF15 powder calcined at 910 °C is shown in Figure S3. Gil-González *et al.* reported a *Pbam* single phase in BSF15 ceramics prepared by mechanochemical synthesis [18], while Levin *et al* showed that the differences between the *Pbam* and *Pnam* structures could not be identified through Rietveld refinement, as both phases produced comparable fitting quality [38]. However, the best fit achieved here was obtained using a three-phase structural model with FE *R3c*, AFE *Pnam* and PE *Pnma* phases. The refined parameters are summarized in Table S1. Figure S4 shows the refined weight fractions of the *R3c*, *Pnam* and *Pnma* phases as a function of the calcination temperature for BSF15 powder. The weight fractions confirm that the calcination conditions affect the phase separation and homogeneity of the samples, as proposed by Khomchenko *et al.* [23] and Walker *et al.* [39]. The weight fraction of the *R3c* phase generally decreases, while that of the *Pnam* phase increases with increasing calcination temperature. The weight fraction of the *Pnma* phase does not show significant variations over the calcination temperature range studied. It is suggested that the *Pnma* phase corresponds to a samarium-rich phase with a similar structure to that of SmFeO_3 . Indeed, the cell dimensions of this phase (Table S1) are very similar to those of SmFeO_3 [40]. An increase of the calcination temperature is seen to favour the *Pnam* phase over the *R3c* phase. Since the *R3c* phase is stable within the Sm-deficient side of the morphotropic phase boundary,

its presence in the samples calcined at lower temperatures suggests that these temperatures are insufficient for significant samarium diffusion. This would result in an inhomogeneous samarium distribution, with samarium-rich areas of the *Pnam* and/or *Pnma* symmetry and samarium-deficient regions with the rhombohedral *R3c* symmetry.

In order to achieve both high weight fraction of the *Pnam* phase and low dielectric loss, the powders $x = 0.150, 0.160, 0.165$ were calcined at $910\text{ }^{\circ}\text{C}$ and that for $x = 0.180$ at $950\text{ }^{\circ}\text{C}$. The ceramics were sintered at $800\text{ }^{\circ}\text{C}$ to avoid Bi_2O_3 evaporation and achieved relative densities above 95% in all cases. The XRD patterns of the $\text{Bi}_{1-x}\text{Sm}_x\text{FeO}_3$ powders and ceramics are shown in Figure S5a and Figure S5b, respectively. All the patterns were fitted using a multi-phase structural model considering the coexistence of the *R3c*, *Pnam* and *Pnma* phases. The variation of the weight fractions of the three phases as a function of Sm concentration for $\text{Bi}_{1-x}\text{Sm}_x\text{FeO}_3$ powder is shown in Figure 2a. The weight fraction of the *R3c* phase decreases with increasing Sm concentration and in BSF18 the rhombohedral phase is absent. The fraction of the *Pnam* phase decreases and that of the *Pnma* phase increases with increasing Sm concentration. This indicates that in the compositional range studied, Sm substitution favours the formation of the *Pnma* phase at the expense of the *R3c* and *Pnam* phases. The variation of the weight fraction in each phase as a function of the Sm substitution level for the ceramics (Figure 2b) showed similar trends to those in powder samples, but with a larger fraction of the *Pnma* phase and a lower fraction of the *Pnam* phase. It is suggested that SPS sintering further promotes the formation of the *Pnma* phase.

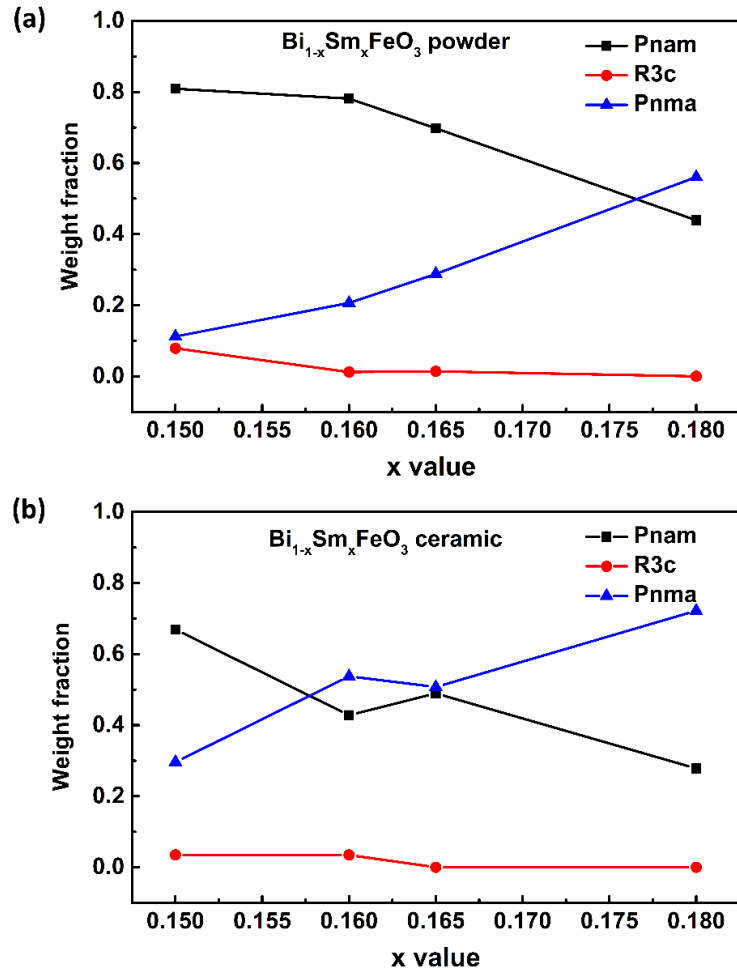


Figure 2. Weight fractions of the *R3c*, *Pnam* and *Pnma* phases as a function of Sm content in (a) $\text{Bi}_{1-x}\text{Sm}_x\text{FeO}_3$ powders; (b) $\text{Bi}_{1-x}\text{Sm}_x\text{FeO}_3$ ceramics ($x = 0.150, 0.160, 0.165$ and 0.180). Error bars are smaller than the symbols used.

SEM images of the BSF15 and BSF18 ceramics are shown in Figure 3 as a representative example, with images for other compositions given in the supporting information as Figure S6. The $\text{Bi}_{25}\text{FeO}_{40}$ phase is mainly present at the grain boundaries, while $\text{Bi}_2\text{Fe}_4\text{O}_9$ is evidenced within the grains, in agreement with previous studies [3]. It has been reported that in the

temperature range 447 °C – 767 °C, $\text{Bi}_{25}\text{FeO}_{40}$ is thermodynamically more stable than BiFeO_3 [3]. While the SPS sintering temperature was 800 °C, the post-sintering annealing temperature was lower (700 °C) and may account for the presence of the $\text{Bi}_{25}\text{FeO}_{40}$ secondary phase.

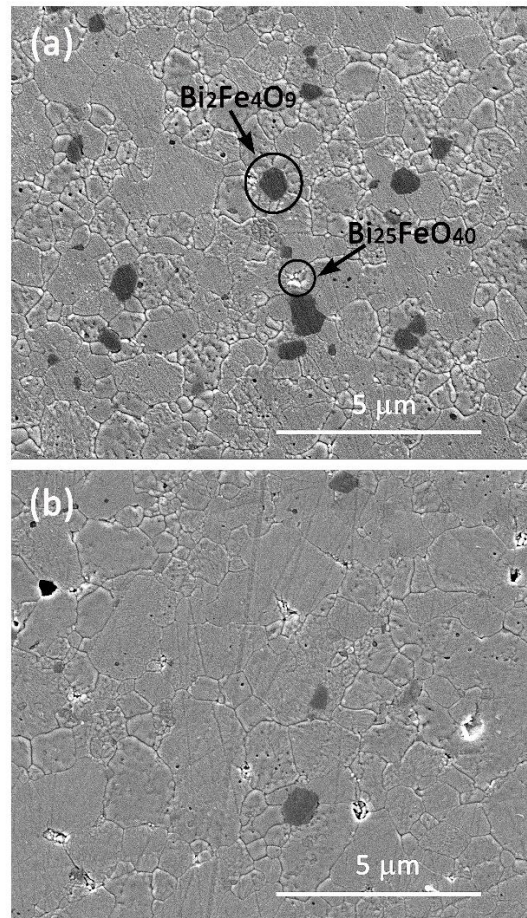


Figure 3 SEM image of (a) BSF15 and (b) BSF18 ceramics. The $\text{Bi}_2\text{Fe}_4\text{O}_9$ (dark grey) and $\text{Bi}_{25}\text{FeO}_{40}$ (bright) phases are highlighted by circles.

Figure 4 shows the frequency dependent dielectric behaviour of the $\text{Bi}_{1-x}\text{Sm}_x\text{FeO}_3$ ($x = 0.150, 0.160, 0.165$ and 0.180) ceramics at room temperature. In general, the measured

permittivity values ϵ_r (Figure 4a) are larger than those of pure BiFeO_3 [41]. This can be attributed to the enhanced polarizability of the MPB compositions [42]. The low values of dielectric loss factor $\tan\delta$ (Figure 4b) suggest a low concentration of oxygen vacancies, *i.e.* iron likely remains in the 3+ oxidation state [6]. The permittivity increases with increasing Sm concentration. The dependence of the dielectric loss on the Sm content varies somewhat with frequency and does not show a clear compositional trend at higher frequencies. Nevertheless, the composition with the highest level of Sm-substitution shows the lowest dielectric loss over the entire studied frequency range. Additionally, all the Sm-substituted compositions show significantly lower dielectric loss than unsubstituted BiFeO_3 , consistent with the reports of Sun *et al.* [19] and Uchida *et al.* [43]. For Sm-substituted BiFeO_3 thin films, the maximum permittivity has been reported to occur at $x = 0.14$ [16]. In the present study, the maximum permittivity of the bulk ceramics is observed at $x = 0.180$.

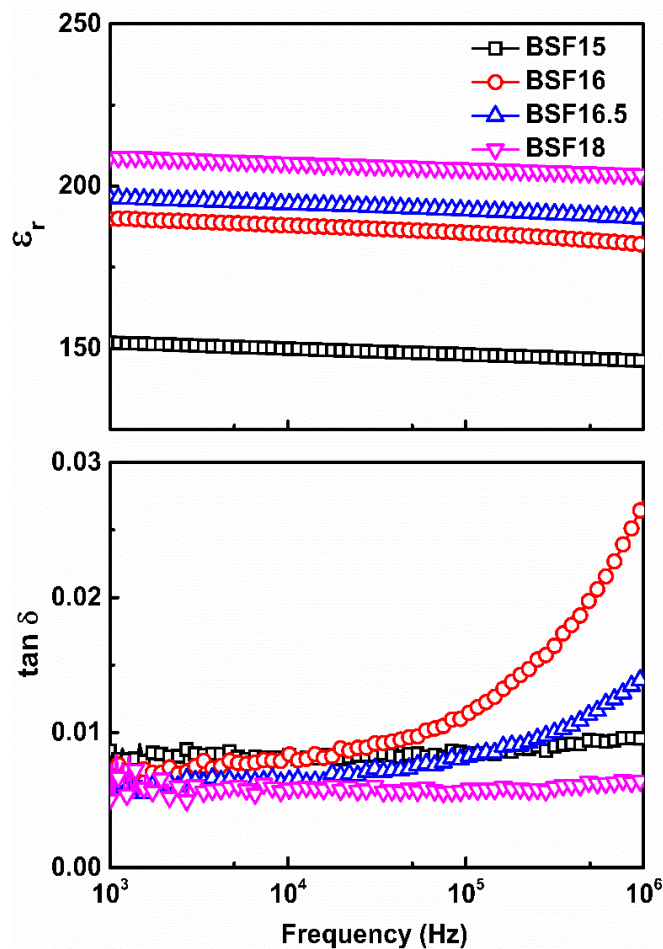


Figure 4. Frequency dependence of (a) relative permittivity ϵ_r and (b) dielectric loss factor $\tan\delta$ for $\text{Bi}_{1-x}\text{Sm}_x\text{FeO}_3$ ceramics at room temperature.

Phase transitions in the $\text{Bi}_{1-x}\text{Sm}_x\text{FeO}_3$ system were investigated by variable temperature XRD. Figure 5 shows detail of the XRD patterns of the BSF15 calcined powder, at selected temperatures over the temperature range 25 °C - 300 °C, on heating and cooling. The intensity of the peaks of the PE *Pnma* phase (at about 25.4°, 41.2°, 47.7° and 52.8° 2 θ) increases with increasing temperature, while the reflections associated with the AFE *Pnam* phase (at about 29.2°, 45.8°, 49.5°, 51.6° and 55.3° 2 θ) show decreasing intensity with increasing temperature.

For the BSF18 calcined powder (Figure S7), the peaks at about 45.8° and 51.6° correspond to the AFE *Pnam* phase and gradually disappear with increasing temperature.

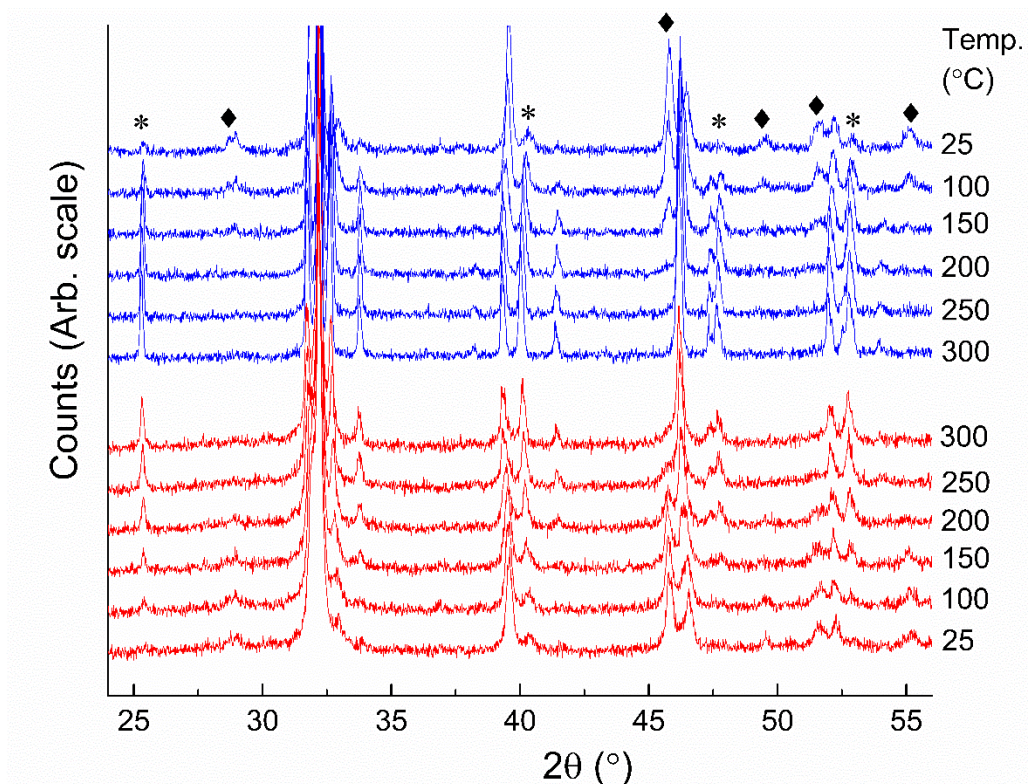


Figure 5. Detail of X-ray diffraction patterns for BSF15 powder (calcined at 910°C) on heating (red) and cooling (blue) at selected temperatures over the range 25°C to 300°C . The peaks belonging exclusively to the *Pnma* phase are marked by asterisks and those of the *Pnam* phase are marked by diamonds.

Figure 6a shows the weight fractions of the *R3c*, *Pnam* and *Pnma* phases as functions of temperature for the BSF15 powder. Both the *Pnam* and *R3c* phases gradually transform to the *Pnma* phase with increasing temperature, confirming that the *Pnma* phase is the high-

temperature stable phase. The *Pnam* phase completely disappears at 450 °C. Figure 6b shows the refined weight fractions of the *Pnam* and *Pnma* phases as functions of temperature for the BSF18 powder. The *Pnam* phase gradually transforms to the *Pnma* phase upon heating; the transition is completed at about 300 °C, which is lower than the transition temperature for BSF15. The weight fraction of each phase before and after the experiment showed some differences, which are associated with the thermal hysteresis around the phase transition.

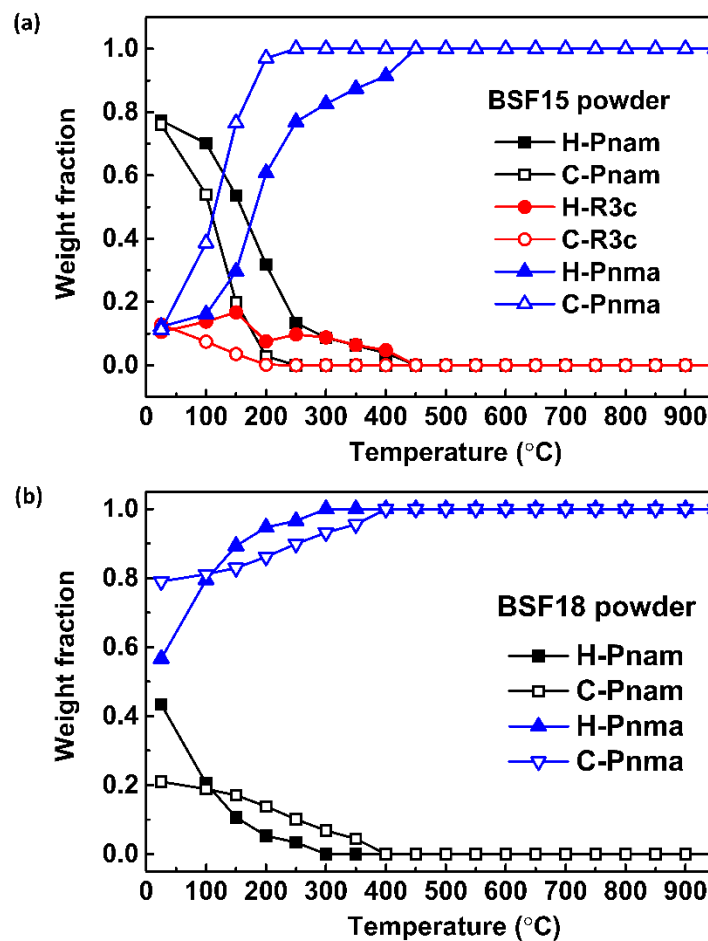


Figure 6. Refined weight fractions of the *R3c*, *Pnam* and *Pnma* phases as functions of temperature for (a) BSF15 powder and (b) BSF18 powder.

Figure 7a shows the temperature dependence of dielectric permittivity ϵ_r and loss factor $\tan\delta$ of the BSF15 ceramic during heating. At around 200 °C, the permittivity shows a peak accompanied by a minimum in dielectric loss, which correlates with the temperature where the highest rate of decrease in the *Pnam* phase content was observed in the X-ray data (Figure 6a). Thus, the peak at 200 °C can be attributed to the transition from the AFE *Pnam* phase to the PE *Pnma* phase. This is mostly likely the same event identified by Gil-González and co-workers at 175 °C by differential scanning calorimetry and X-ray diffraction, which they attributed to a *Pbam-Pnma* transition [18]. As the samarium content increases, the permittivity peak shifts to lower temperatures (the thermal dependencies of dielectric behaviour for BSF16 and BSF16.5 ceramics are shown in Figures S8a and S8b, respectively). In BSF18, this peak is observed at 100 °C (Figure 7b), where the largest drop in the *Pnam* phase fraction was detected (Figure 6b). This temperature is close to the phase transition temperature detected in BSF17.5 by Gil-González *et al.* at 150 °C and attributed to the *Pbam+Pnma/Pnma* transformation [18]. The stabilization of the *Pnma* phase might be attributed to the effect of the substitution of Bi^{3+} ions by smaller Sm^{3+} ions ($r = 1.36 \text{ \AA}$ and 1.28 \AA , respectively for the ions in 12 coordinate geometry [44]), resulting in a lattice distortion and unit cell volume reduction [45, 46]. The peak at about 400 °C, visible in the high frequency curves in all compositions, is probably related to the antiferromagnetic Néel temperature, in agreement with Gil-González *et al.* [18].

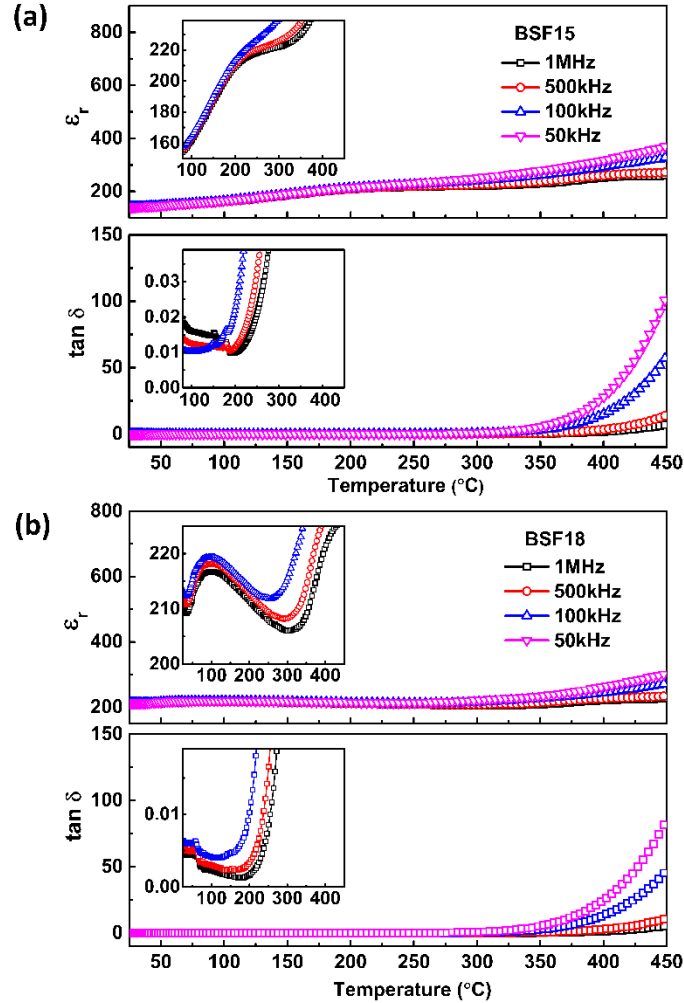


Figure 7. Temperature dependence of relative permittivity ϵ_r and dielectric loss factor $\tan \delta$ at selected frequencies for (a) BSF15 and (b) BSF18 ceramics on heating, with detail shown inset.

The room temperature current-electric field (I-E) and the polarization-electric field (P-E) hysteresis loops of the BSF15 and BSF18 ceramics are shown in Figure 8 and those of the BSF16 and BSF16.5 ceramics are shown in Figure S9. According to the I-E curves, the electrical conductivity of Sm-substituted ceramics is significantly lower than that of pure BiFeO_3 (see Ref.1). The current peak (labelled “A”) observed in the I-E loop of BSF15 is indicative of domain

switching in the FE phase, which is consistent with the presence of the $R3c$ structure at room temperature (Figure 2). The lower P-E loop hysteresis and the suppression of the peak in the I-E loops in ceramics with higher Sm content indicates the reduction of the electrical conductivity and the suppression of FE behaviour. Additionally, the breakdown strength of the ceramics has been greatly improved in compositions with higher Sm content, compared to those previously reported [27, 47, 48]. However, double P-E hysteresis loops characteristic of reversible AFE \leftrightarrow FE transitions were not observed, despite the presence of the AFE $Pnam$ phase observed in the TEM images (Figure 1).

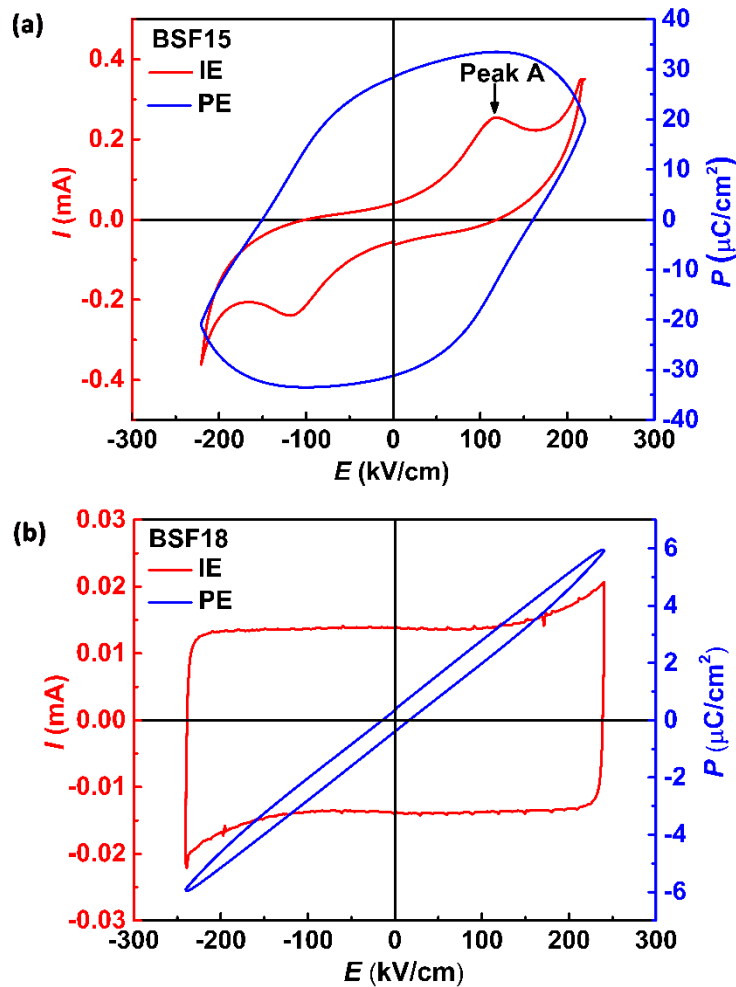


Figure 8. Current-electric field (I-E) and polarization-electric field (P-E) hysteresis loops of (a) BSF15 and (b) BSF18 ceramics.

4. Conclusions

Through a detailed diffraction investigation, the existence of an antiferroelectric phase with *Pnam* symmetry in $\text{Bi}_{1-x}\text{Sm}_x\text{FeO}_3$ ceramics, with compositions close to the morphotropic phase boundary ($0.15 \leq x \leq 0.18$) has been confirmed. The antiferroelectric *Pnam* phase coexists with the ferroelectric *R3c* and paraelectric *Pnma* phases, whose relative fractions vary with the level of Sm substitution and the calcination conditions. In particular, the fractions of both the *R3c* phase and the *Pnam* phases decrease with increasing Sm concentration. The fraction of the *Pnam* phase increases and that of the *R3c* phase decreases with increasing calcination temperature. The fractions of *R3c* and the *Pnam* phases progressively reduce with increasing temperature in favour of the *Pnma* phase, with a rate that strongly depends on the Sm concentration. Sm-substitution increases the dielectric permittivity, reduces electrical conductivity, increases breakdown strength and suppresses ferroelectric switching. The results indicate that it is possible to tailor phase composition and the consequent dielectric properties through careful selection of composition and calcination conditions.

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