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ORIGINAL PAPER



A theoretical model of inflammation- and mechanotransductiondriven asthmatic airway remodelling

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Abstract

2 Inflammation, airway hyper-responsiveness and airway remodelling are well-established hallmarks of asthma, but their

- inter-relationships remain elusive. In order to obtain a better understanding of their inter-dependence, we develop a
- ⁴ mechanochemical morphoelastic model of the airway wall accounting for local volume changes in airway smooth muscle
- (ASM) and extracellular matrix in response to transient inflammatory or contractile agonist challenges. We use constrained
- mixture theory, together with a multiplicative decomposition of growth from the elastic deformation, to model the airway wall
 as a nonlinear fibre-reinforced elastic cylinder. Local contractile agonist drives ASM cell contraction, generating mechanical
- stresses in the tissue that drive further release of mitogenic mediators and contractile agonists via underlying mechanotransduc-
- successes in the disside that drive further refease of introgene inculators and confidence agoinsts via underlying incentational data
 tive signalling pathways. Our model predictions are consistent with previously described inflammation-induced remodelling
- within an axisymmetric airway geometry. Additionally, our simulations reveal novel mechanotransductive feedback by which
- hyper-responsive airways exhibit increased remodelling, for example, via stress-induced release of pro-mitogenic and pro-
- ¹² contractile cytokines. Simulation results also reveal emergence of a persistent contractile tone observed in asthmatics, via
- ¹³ either a pathological mechanotransductive feedback loop, a failure to clear agonists from the tissue, or a combination of both.
- ¹⁴ Furthermore, we identify various parameter combinations that may contribute to the existence of different asthma phenotypes,
- and we illustrate a combination of factors which may predispose severe asthmatics to fatal bronchospasms.

Keywords Morphoelastic · Bronchoconstriction · Hyper-responsiveness · Mechanochemical · Airway smooth muscle ·
 Multiphase

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18 1 Introduction

Asthma is a chronic lung disease characterized by inflamma tion, airway hyper-responsiveness (excessive bronchocon-

striction in response to relatively low doses of contractile 21 agonist; AHR) and airway remodelling. The last of these 22 involves a series of structural changes, including thickening 23 of the epithelial layer and subepithelial basement membrane 24 (SBM; the collagen-dominated inner layer of the airway) 25 and of airway smooth muscle (ASM) bundles (Holgate 2011; 26 Brightling et al. 2012; James et al. 2012; Berair et al. 2013). 27 While each of these three features contributes to asthma 28 severity, how they interact is poorly understood. Most impor-29 tantly, it is not clear whether AHR or remodelling are causes 30 or consequences of the disease. 31

We hypothesize that while airway remodelling is initiated 32 by inflammatory mediators, it is perpetuated by mechani-33 cal factors. The complexity of the underlying biochemical 34 and mechanical processes, which span multiple length and 35 timescales, makes identification of key interactions solely 36 from biological experiments on isolated processes partic-37 ularly challenging. Our aim is, therefore, to investigate 38 the combined effect of repeated, short timescale, inflam-39 matory episodes and associated mechanical forces, arising 40 from ASM cell (ASMC) contraction, on long-term airway 41 remodelling. To this end, we present a novel, quantita-42 tive mechanochemical modelling framework (informed by 43 appropriate in vitro and in vivo studies) that integrates these processes for the first time. We use this model to elucidate 45 emergent system dynamics and thereby identify key under-46 lying pathogenic processes. 47

Although inflammation is considered to be the main pro-48 cess by which airway remodelling occurs, based on in vitro 49 (Brightling et al. 2012; Dekkers et al. 2012; Noble et al. 2014 50 and references therein) and animal (Sjöberg et al. 2017; Alri-51 fai et al. 2014; Silva et al. 2008; Zhu et al. 1999) studies, the 52 causative effects of inflammation on remodelling are not fully 53 supported by clinical trial or epidemiological data. For exam-54 ple, controlling inflammation with inhaled corticosteroids 55 does not change the extent of airway remodelling or the 56 decline of lung function with age (Guilbert et al. 2006; Strunk 57 2007). Moreover, airway remodelling may occur in early life 58 in the absence of inflammation (James et al. 2012, 2009). 59 Bronchoconstriction, in the absence of inflammation, can 60 also promote airway remodelling (Kistemaker et al. 2014; 61 Oenema et al. 2013; Ge et al. 2012; Grainge et al. 2011; Tatler 62 et al. 2011). In addition to the structural changes present in 63 asthmatic airways, there is increasing evidence of altered 64 baseline contractile tone that is thought to be the result of 65 the chronic presence of contractile agonist or inflammatory 66 mediators (Brightling et al. 2002). 67

It is not clear how this persistent tone arises, but it could enhance AHR (Bossé et al. 2009). Additionally, intra-subject 70

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heterogeneity of tone in asthmatics has been proposed as a cause of AHR (Brown and Togias 2016). Given that the area fraction of ASM in human biopsies has been shown to increase with the degree of asthma severity (Hassan et al. 2010), altered tone and ASM mass are likely interrelated. Furthermore, airway remodelling is also associated with extracellular matrix (ECM) changes (Kuo et al. 2011) and SBM thickening (Benayoun et al. 2003).

Inflammation in the airways is the protective response to allergen challenges, and is characterized by the recruitment of inflammatory cells (such as eosinophils), activation of resident mast cells, and over-expression of cytokines and chemokines (Brightling et al. 2003). Some of the latter interact directly with ASM to trigger contraction, and/or interact with mast cells causing them to degranulate, producing histamine and other contractile agonists (Kostenis and Ulven 2006). Inflammatory cells release mediators that also have the ability to induce remodelling (e.g. TGF- β ; Halwani et al. 2011). Subsequently, the inflammatory cells and cytokines are gradually cleared from the tissue. Allergen challenges in humans are typically random, but in mouse models of asthma, inflammatory and contractile agonist challenges are administered and controlled artificially.

Tissue mechanics plays a significant role in airway remod-94 elling and bronchoconstriction. For example, mechanical 95 strain increases ASMC proliferation (Smith et al. 1994) and 96 contractile protein expression (Smith et al. 1997, 1995). In 97 addition, TGF- β is a cytokine that mediates remodelling by 98 inducing both cell proliferation and ECM protein produc-99 tion (Halwani et al. 2011), as well as having a potential 100 contractile agonist role (Desmoulière et al. 2005; Grinnell 101 and Ho 2002; Montesano and Orci 1988). It is activated 102 by ASMCs (Tatler et al. 2011), likely during bronchocon-103 striction (Oenema et al. 2013; Tatler and Jenkins 2012) via 104 mechanical stretch from latent complexes that are tethered to 105 the ECM and to the ASMC (Froese et al. 2016; Noble et al. 106 2014; Wipff et al. 2007). Moreover, bronchial epithelial cells 107 under mechanical compression shed growth factors such as 108 endothelin-1 (ET-1), early growth response-1 (EGR-1) and 109 TGF- β (Tschumperlin and Drazen 2006, 2001; Tschumper-110 lin et al. 2004) as well as to signal lung fibroblasts to express 111 ECM proteins in vitro (Swartz et al. 2001). 112

The heterogeneous micro-mechanical stress environment, 113 generated by ASM contraction, can be quantitatively and 114 qualitatively very different in normal versus remodelled air-115 ways (Hiorns et al. 2016). Associated mechanotransductive 116 processes may influence ECM deposition and ASM pro-117 liferation and migration. While it is recognized that these 118 mechanisms play a crucial role in numerous developmental, 119 physiological and pathological processes in other diseases 120 (Hoffman et al. 2011; Martinez-Lemus et al. 2009), we have 121

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yet to understand how these mechanisms contribute to AHRand airway remodelling in asthma.

A significant body of work focusses on models of bron-124 choconstriction (e.g. Hiorns et al. 2014; Eskandari et al. 125 2013; Politi et al. 2010; Wang et al. 2008; Latourelle et al. 126 2002; Lambert and Paré 1997; Macklem 1996; Lambert 127 et al. 1993), with much less attention paid to modelling 128 of inflammation in the airways. Of particular relevance to 129 this work are two of our previous models: firstly, our finite-130 thickness continuum-based model (Hiorns et al. 2014) of 131 agonist-initiated contraction of the airway (represented as a 132 nonlinear fibre-reinforced elastic material), which accounts 133 for contractile force generation at the cell-level; secondly, 134 our spatially-averaged (ordinary differential equation; ODE) 135 model (Chernyavsky et al. 2014) of inflammation-driven 136 switching of ASMCs from a contractile to a proliferative 137 phenotype. The former predicts airway calibre changes and 138 spatial stress heterogeneities, as a result of ASM contrac-139 tion and in response to pressure fluctuations that mimic tidal 140 breathing. In the latter, resolution of inflammation is impli-141 cated as the key factor in driving ASM mass accumulation; 142 however, this model does not account for mechanotrans-143 ductive feedback from mechanical stresses arising in the 144 constricted remodelled airway wall. Thus, we combine and 145 extend these two models by: (i) recasting our biomechanical 146 model of the contractile airway into a well-established mor-147 phoelastic framework, that has been widely applied to growth 148 and remodelling of soft tissues; and (ii) coupling this to the 149 evolution of individual tissue constituents, using a multiphase 150 description, governed by underlying biochemical processes 151 such as inflammation-induced ASM phenotype switching, 152 ASM cell proliferation or recruitment and ECM deposition, 153 all of which can depend on mechanical stresses. Importantly, 154 this coupled model accounts for two-way feedback between 155 inflammation-driven changes in volume fractions of individ-156 ual airway constituents and their resulting mechanochemical 157 environment. 158

159 2 Methods

160 2.1 Mathematical formulation

We model the airway wall as a two-layered cylinder, repre-161 senting the inner collagenous SBM and an outer (predom-162 inantly) smooth muscle layer, within which accumulation 163 of ASM mass and ECM deposition is driven by both bio-164 chemical and mechanical stimuli (Figs. 1, 2), neglecting (for 165 simplicity) the sub-mucosal epithelial layer. We first outline 166 a description of the elastic deformation (Fig. 1), consist-167 ing of the balance of linear momentum together with the 168 constitutive specification of a hyperelastic mechanical law 169 (Sect. 2.1.1). We then define the model inputs representing 170

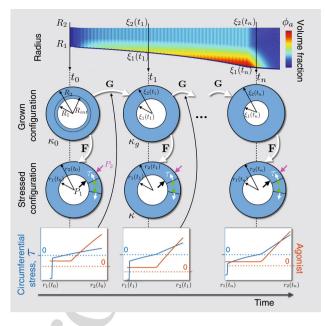


Fig. 1 Configurations during finite growth of the airway wall. Top row: Schematic of the evolution of the airway wall geometry with time, with the colours correspoding to tissue constituent volume fraction. Middle rows: Schematics of the airway geometry in the grown and stressed configurations, at the indicated time. At initial time t_0 , the airway wall is defined by inner radius R_1 , interface radius R_{int} , and outer radius R_2 in κ_0 , the original, stress-free reference configuration. Airway wall growth is described by the mapping, G, from the original configuration to κ_{ρ} , the grown, zero-stress configuration, defined by grown radii ξ_1, ξ_{int} (not shown), and ξ_2 at time t_1 . The airway is deformed via **F** to configuration κ , the current, stressed configuration, defined by radii r_1 , r_{int} , and r_2 , subject to pressure boundary conditions P_1 and P_2 . Bottom row: Schematics of transmural mechanical stress distributions, generated from the active contraction and/or the elastic deformation, and contractile agonist. The mechanical stress, τ , modulates certain rates in the constitutive mass balance equations, e.g. (2.18, 2.21), to influence growth, G

biochemical stimulation (Sect. 2.1.2). Finally (Sect. 2.1.3), we construct the mass balance equations, incorporating suitable biochemical and mechanotransductive processes (Fig. 2).

2.1.1 Geometry and kinematics

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The airway tissue is modelled as a mixture (Ateshian 2007; 176 Humphrey and Rajagopal 2002; Bowen 1976; Truesdell and 177 Toupin 1960) consisting of four phases: ASMCs in either a 178 contractile (c) or a proliferative (p) phenotype; a collagen-179 dominated ECM (e); and an extracellular fluid (w) that also 180 transports soluble nutrient (not modelled) for tissue main-181 tenance. The outer layer is composed of multiple phases 182 (predominantly ASMCs), and the inner layer, representing 183 the SBM, is composed entirely of the ECM phase. Follow-184 ing the traditional continuum mechanics approach (Holzapfel 185 2000; Truesdell and Noll 1965), we assume initially (at time 186 t_0) that each constituent a in the airway is in a (common) 187

spatial, unstressed and unstrained reference configuration 188 denoted κ_0 , in which the position of a particle is given by **X**. 189 We assume that the airway is an axisymmetric thick-walled 190 cylinder of fixed length. We define fixed polar cylindri-191 cal co-ordinates R, Θ, Z in the radial, circumferential and 192 axial directions, respectively, with the inner layer occupying 193 $R_1 \leq R \leq R_{\text{int}}$, and the outer layer $R_{\text{int}} \leq R \leq R_2$ (Fig. 1). 194 In Fig. 1, **G** is a topological mapping from κ_0 to an interme-195 diate "grown" configuration κ_g , in which the position of a 196 particle originally at **X** is given by $\boldsymbol{\xi}(\mathbf{X}, t)$, with cylindrical 197 co-ordinates: 198

¹⁹⁹
$$\xi = \xi (R, t), \vartheta = \Theta, \zeta = Z,$$
 (2.1)

where we have assumed the airway maintains axisymmetry 200 and zero axial growth. The airway in the grown configura-201 tion κ_g is deformed to a stressed configuration κ , and the 202 position of a particle originally at $\boldsymbol{\xi}$ is now at $\mathbf{x}(\boldsymbol{\xi})$, with 203 the mapping given by the deformation gradient tensor \mathbf{F} . 204 The total deformation is given by using the standard mul-205 tiplicative decomposition, $\mathbf{H} = \mathbf{FG}$. For concision, explicit 206 dependence on time is suppressed here and throughout. 207

For simplicity, we impose a plane-strain approximation, 208 axisymmetry, and zero axial displacement. Thus, the defor-209 mation from κ_g to κ is given by 210

$$r = r(\xi), \theta = \vartheta, z = \zeta, \qquad (2.2)$$

so that the elastic deformation gradient tensor is given by 212

²¹³
$$\mathbf{F} = \operatorname{diag}\left[\frac{\partial r}{\partial \xi}, \frac{r}{\xi}, \lambda_z\right].$$
 (2.3)

Assuming incompressibility, $det(\mathbf{F}) = 1$ thus gives 214

$$r^{2} = r_{\text{int}}^{2} + \xi^{2} - \xi_{\text{int}}^{2}, \qquad (2.4)$$

where $r_{\text{int}} = r(\xi_{\text{int}})$. The initial airway geometry (Online 216 Resource 2) is chosen to match the bovine airways used in 217 LaPrad et al. (2010), from which the mechanical properties 218 are obtained. These are similar in size and structure to gen-219 eration 4 human airways (Harvey et al. 2013; Coxson et al. 220 2008; Williamson et al. 2011). The interface radius is chosen 221 based on human airway histology (Benayoun et al. 2003). 222

Mechanical properties We assume the tissue is a nonlinear 223 hyperelastic heterogeneous (multiphase) anisotropic mate-224 rial (Bowen 1976; Truesdell and Noll 1965; Truesdell and 225 Toupin 1960). The formulation for obtaining the constitu-226 tive mechanical relation for this type of material is given in 227 detail by Ateshian and Ricken (2010) and Ateshian (2007). 228 We neglect dissipative stresses and assume: that all solid 229 constituents are constrained to move together (Humphrey 230 and Rajagopal 2002); isothermality; electroneutrality; tissue 231

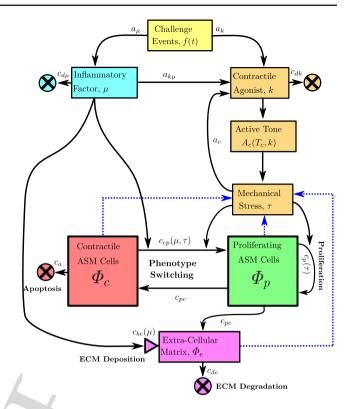


Fig. 2 Overview of the biochemical mechanisms. Allergen or contractile agonist challenges, f(t), specified to occur at times t_i , drive evolution of an inflammatory factor, μ , and contractile agonist concentration, k. The magnitude and rate of clearance of μ and k are determined by constants a_{μ} , a_k , and $c_{d\mu}$, c_{dk} , respectively. Inflammation leads to global release of contractile agonist at rate $a_{k\mu}$. Contractile agonist induces local ASMC contraction, and the resulting increased mechanical stress τ releases further cytokines, with contractile agonist properties, at rate a_c . Contractile ASMCs undergo apoptosis (c_a) and switching to a proliferative phenotype (c_{cp}) . The proliferative ASMCs divide (c_p) and switch to a contractile phenotype at a (high) constant rate (c_{pc}) . Both inflammation and mechanical stress drive increases (from a baseline) in the contractile to proliferative switching rate $(c_{cp}(\mu, \tau))$, and increasing mechanical stress drives increases in the proliferation or recruitment rate $(c_{\rm p}(\tau))$. ECM proteins degrade (c_{de}) and are deposited $(c_{be}(\mu))$ at baseline rates during normal tissue maintenance, with the latter increasing with inflammation. Proliferating ASMCs produce additional ECM proteins (with rate cpe). Blue dotted arrows indicate how constituent volume fractions are required for computation of the mechanical stress (τ), as illustrated in Fig. 1. Rate constants are given in Online Resource 2

incompressibility; that stress arises from the elastic deforma-232 tion only (i.e. the growth mapping does not impart stress); 233 and that viscous stresses are negligible. 234

Following Hiorns et al. (2014), we apply the commonly used additive de-coupling of the active and passive Cauchy stress tensors: 237

$$\mathbf{T} = -p\mathbf{1} + \mathbf{T}_{\text{passive}} + \mathbf{T}_{\text{active}}, \qquad (2.5) \quad {}_{23}$$

where **1** is the identity tensor and *p* is a Lagrange multiplier 239 enforcing incompressibility, with the passive stress given by 240

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$$\mathbf{T}_{\text{passive}} = 2\mathbf{F} \frac{\partial \Psi}{\partial \mathbf{C}} \mathbf{F}^{\mathrm{T}},$$
 (2.6)

²⁴² in which we highlight that, since the mixture is constrained, ²⁴³ $\mathbf{F}_{a} = \mathbf{F}$. In (2.6), Ψ is the strain energy function per unit ²⁴⁴ volume of the mixture,

$$_{245} \Psi = \sum_{a=p,c,e} \Phi_a W_a,$$
 (2.7)

²⁴⁶ and W_a is the strain energy function per unit constituent vol-²⁴⁷ ume of constituent *a* (Ateshian 2007; Huyghe and Janssen ²⁴⁸ 1997), noting that the fluid phase (*w*) does not contribute to ²⁴⁹ the mechanical response of the tissue.

The contractile ASMCs and collagen-dominant ECM form continuous fibre-like structures (Ijpma et al. 2017) and therefore are modelled as two sets of helical fibres wrapped symmetrically about the airway axis (to avoid torsion). The active stress in (2.5) is given by

255
$$\mathbf{T}_{\text{active}} = \Phi_{c} A_{c} \mathbf{m}_{c}^{(j)} \otimes \mathbf{m}_{c}^{(j)},$$
 (2.8)

where A_c is the contractile force density, defined as the force generated by the contractile ASMCs per unit area of constituent (Brook et al. 2010) and $\mathbf{m}_c^{(j)}$ is the contractile ASMC fibre orientation vector (see Online Resource 1.1 for further details).

Specification of the constitutive mechanical response for 261 the airway wall constituents In our previous work (Hiorns 262 et al. 2014), the airway wall is modelled as a composite mate-263 rial of ASMCs and ECM, in which two families of fibres 264 are embedded in an isotropic ground matrix, thus giving 265 an anisotropic response. Fibre recruitment is modelled phe-266 nomenologically with an exponential dependence on stretch. 267 Here, we de-couple the mechanical responses of the pro-268 liferating ASMCs, modelled as an isotropic neo-Hookean 269 material; the contractile ASMCs, modelled as the fibre-270 embedded material described above, and the ECM, modelled 271 similarly under the additional assumption that collagen fibres 272 bear load only after being extended beyond the recruitment 273 stretch, λ_u (Hiorns et al. 2014; Hill et al. 2012; Robertson 274 et al. 2011; Holzapfel and Ogden 2010). The strain energy 275 functions for each of the constituents are given in Online 276 Resource 1.2. 277

We introduce a scalar quantity τ representing the mechanical stress along the contractile ASMC fibre directions, given by

$$\tau = \frac{1}{2} \sum_{j=1,2} \mathbf{T} : \mathbf{m}_{c}^{(j)} \otimes \mathbf{m}_{c}^{(j)}, \qquad (2.9)$$

which is used in the mass balance equations in Sect. 2.1.3
to elicit the mechanotransductive responses. The degree of
contraction is directly related to the amount of agonist bound

to the relevant contractile ASMC receptors. We therefore 285 assume that the contractile force density, A_c in (2.8), is a function of contractile agonist concentration, k, saturating as follows: 286

$$A_{\rm c} = T_{\rm c} \frac{k^n}{K_d + k^n},\tag{2.10}$$

where T_c is a measure of hyper-responsiveness, K_d represents the ratio of the dissociation rate of the ligand-receptor complex to its association rate, and n is the Hill coefficient, describing cooperativity.

Balance of linear momentum In addition to the assumptions stated above, we further assume that body forces are negligible and inertial terms may be neglected due to slow timescales associated with quasi-static deformation. Therefore, in mechanical equilibrium, conservation of linear momentum requires 299

Under the assumption of no torsion and plane strain, (2.11) reduces to 300

$$\frac{\partial T_{rr}}{\partial r} + \frac{T_{rr} - T_{\theta\theta}}{r} = 0, \qquad (2.12) \quad {}_{303}$$

where T_{rr} is the radial component and $T_{\theta\theta}$ the circumferential component of the Cauchy stress.

Boundary conditions for the elastic deformation For the elastic deformation, pressure boundary conditions are specified at the inner and outer radii, and continuity of radial displacements and stress at the interface, so that

$$T_{rr}(r_1) = -P_1,$$
 (2.13a) 310

$$r^{(i)}(\xi_{\text{int}}) = r^{(0)}(\xi_{\text{int}}) \equiv r_{\text{int}}.$$
 (2.13b) ³¹

$$T_{rr}^{(t)}(r_{\text{int}}) = T_{rr}^{(0)}(r_{\text{int}}),$$
 (2.13c) 312

$$T_{rr}(r_2) = -P_2.$$
 (2.13d) 313

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2.1.2 Model inputs

We assume that a series of transitory allergen challenges drives a global inflammatory response that represent an influx of inflammatory cells, such as eosinophils, into the airway tissue, resulting in a cumulative inflammatory status denoted μ . The challenges may be administered (e.g. in chronic asthma mouse models), or occur naturally. Therefore, μ evolves according to

$$\frac{\mathrm{d}\mu}{\mathrm{d}t} = a_{\mu}f(t) - c_{\mathrm{d}\mu}\mu, \qquad (2.14) \quad {}_{323}$$

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where $c_{d\mu}$ is the inflammation decay rate representing clearance of inflammatory cytokines or inflammatory cell apoptosis, and a_{μ} the magnitude, and f(t) denotes the timing of events given by (2.16).

Inflammation drives a local activation of mast cells and 328 bronchoconstrictive mediators (represented by the concen-32 tration k) such as histamine or acetylcholine (Pelaia et al. 330 2008). The agonist induces active contraction of the ASM. 331 which leads to airway narrowing together with associated 332 local airway wall stresses. We assume that the local ten-333 sile stress, τ (2.9), induces activation of latent TGF- β ; this 334 cytokine also acts as a contractile agonist and therefore 335 contributes to k. We also consider cases where local com-336 pressive stress drives remodelling. These cases represent 337 compression-induced epithelial-cell-mediated expression of 338 EGR-1 or ET-1, noting that, here, we do not model the epithe-339 lial cells directly. 340

As with inflammation, the frequency of contractile agonist challenges may be specified as model input to represent, for instance, artificial methacholine challenges in animals (Lauzon and Bates 2000; Gunst et al. 1988) or humans (Grainge et al. 2011). Contractile agonist, k, thus evolves over time according to

³⁴⁷
$$\frac{\mathrm{d}k}{\mathrm{d}t} = a_k f(t) - c_{\mathrm{d}k}k + a_{k\mu}\mu + a_\mathrm{c}\tau H(\tau),$$
 (2.15)

where c_{dk} is the agonist clearance rate, a_k the magnitude of administered agonist stimuli, $a_{k\mu}$ the rate of inflammationinduced agonist activation, and a_c the rate at which the stress τ induces agonist release. The Heaviside step function *H* ensures that only tensile stresses release *k* (Wipff et al. 2007).

By setting $a_{\mu} = 0$ or $a_k = 0$ in 2.14 and 2.15, f(t)represents either contractile agonist- or inflammatory-only challenges, respectively. The challenges are represented by a series of Gaussian peaks

358
$$f(t) = \frac{1}{\sqrt{2\pi\sigma^2}} \sum_{i=1}^{N} \left[\exp^{-d(t-t_i)^2/2\sigma^2} \right],$$
 (2.16)

where t_i is a vector of *N* event times, and *d* and σ are constants (Chernyavsky et al. 2014).

361 2.1.3 Tissue growth

³⁶² Under the assumption of axisymmetry, in cylindrical polar ³⁶³ co-ordinates, the local density, ρ_a , of each constituent (a =³⁶⁴ c, p, e, w) evolves according to:

$$_{365} \quad \frac{\partial \rho_{a}}{\partial t} + v \frac{\partial \rho_{a}}{\partial \xi} + \rho_{a} \frac{1}{\xi} \frac{\partial (\xi v)}{\partial \xi} = s_{a} \tag{2.17}$$

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where ρ_a and the (constrained mixture) radial growth velocity, v, are functions of the grown radius, ξ (Fig. 1), and time, t; $s_a = s_a (\rho_c, \rho_p, \rho_e)$ represents the constituent-dependent source/sink terms, specified in detail below.

We assume that the density of contractile ASMCs, ρ_c , 370 evolves through switching to and from a proliferative pheno-371 type, ρ_p (Fig. 2; Naveed et al. 2017; Wright et al. 2013; Hirota 372 et al. 2009). The definition of ASMC phenotype is based on 373 the observable function of the cells arising from expression 374 of intracellular proteins, e.g. proliferative ASMCs exhibiting 375 decreased expression of contractile proteins (Wright et al. 376 2013). As in our previous model (Chernyavsky et al. 2014), 377 the rate of switching is governed by the inflammatory status, 378 μ , but here we additionally assume that switching can also 379 be driven by the local fibre mechanical stress τ . Thus, 380

$$s_{\rm c} = c_{\rm pc}\rho_{\rm p} - c_{\rm a}\rho_{\rm c}^2 - c_{\rm cp}(\mu,\tau)\rho_{\rm c}, \qquad (2.18) \quad {}_{38}$$

where c_{pc} and c_{a} are positive constants, the first two terms representing switch back from the proliferative phenotype and apoptosis, respectively, the combination of which provides a logistic growth representation. c_{cp} represents the inflammation- and stress-modulated rate of switching to the proliferative phenotype given by 387

$$c_{\rm cp}(\mu,\tau) = c_{\rm c0} + (c_{\rm c1} - c_{\rm c0}) H(\mu - \mu_1) + (c_{\rm c2} - c_{\rm c1}) H(\mu - \mu_2) + c_{\rm c\tau}(\tau)\tau,$$
(2.19) 388

where c_{c0} , c_{c1} , c_{c2} and $c_{c\tau}$ are positive constants. The Heaviside functions are used to divide the inflammation into three levels: healthy, mild, and severe, which are characterized by the thresholds μ_1 and μ_2 (Fig. 3). The final term represents local mechanical stress-induced switching:

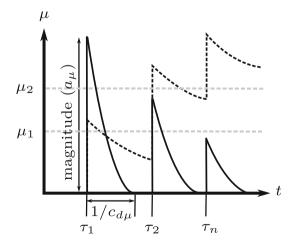


Fig. 3 Inflammation levels. Inflammatory status dynamics induced by a series of environmental stimuli, illustrating the parameters $\mu_1, \mu_2, a_{\mu}, c_{d\mu}$, and t_i , noting that for periodic events, $t_{i+1} - t_i = \Delta t$ and $\omega = 1/\Delta t$. The solid line represents relatively fast inflammatory clearance (high $c_{d\mu}$), while the dotted line represents slow clearance

$$c_{c\tau}(\tau) = \begin{cases} c_{cp}^{f} H(\tau) & \text{if tension induces switching,} \\ c_{cp}^{f} H(-\tau) & \text{if compression induces switching.} \end{cases}$$

$$(2.20)$$

Increases in proliferative ASMC density, ρ_p , arise via proliferation and phenotype switching. Thus, proliferative ASMC turnover, s_p , is represented by

³⁹⁹
$$s_{\rm p} = (c_{\rm p}(\tau) - c_{\rm pc}) \rho_{\rm p} + c_{\rm cp}(\mu, \tau) \rho_{\rm c},$$
 (2.21)

where the proliferation rate $(c_p(\tau))$ is modulated directly by the local stress τ according to

402
$$c_{\rm p}(\tau) = c_{\rm p0} + c_{\rm p\tau}\tau,$$
 (2.22)

representing baseline and a (tensile or compressive) stressdriven proliferation, of identical form to (2.20) but with rate constant c_p^f .

406 ECM turnover is modelled via

407
$$s_{\rm e} = c_{\rm pe}\rho_{\rm p} + c_{\rm be}(\mu) - c_{\rm de}\rho_{\rm e},$$
 (2.23)

where the first term represents ECM synthesis by the proliferative ASMCs, e.g. via ASMC-mediated release of active TGF- β that induces ASMCs to synthesize collagen (Coutts et al. 2001); the second term represents modification of ECM by inflammatory mediators, e.g. via mast cell activation mediated by MMP-1; and the third term, linear degradation. The inflammation-driven ECM deposition is given by

$$c_{be}(\mu) = c_{e0} + (c_{e1} - c_{e0}) H(\mu - \mu_1) + (c_{e2} - c_{e1}) H(\mu - \mu_2),$$
(2.24)

where, again, the Heaviside function is used to separate thethree inflammation levels.

For simplicity, each of the constituents is considered 419 intrinsically incompressible, i.e. their true densities $(\rho_a^{\rm T})$ 420 remain constant in space and time (Ateshian 2011), and we 421 assume that the true densities of the ASMCs and ECM are 422 equal, a reasonable assumption in general (Gleason et al. 423 2004). In the following, we work in terms of the volume 424 fraction, defined by $\Phi_a = \rho_a / \rho_a^T$, and correspondingly write 425 the source/sink terms as $S_a = s_a / \rho_a^T$. Assuming no voids, we 426 obtain 427

$$_{428} \quad \sum_{a} \Phi_{a} = 1.$$
 (2.25)

Equation (2.17), together with the definition of volume fraction and the source/sink terms, is re-expressed as

$$_{431} \quad \frac{\partial \Phi_{a}}{\partial t} + v \frac{\partial \Phi_{a}}{\partial \xi} + \Phi_{a} \left(\frac{1}{\xi} \frac{\partial}{\partial \xi} \left(\xi v \right) \right) = S_{a} \tag{2.26}$$

where the volume fractions, Φ_a , are functions of the grown radius, ξ (Fig. 1), and time, t, and a = c, p, e. As in Gleason et al. (2004), we assume that a constant and uniform tissue hydration is maintained, such that $\Phi_w = 0.70$. Summation of (2.26), together with (2.25), gives the mass balance equation for the entire mixture as

$$\frac{1}{\xi}\frac{\partial}{\partial\xi}\left(\xi\upsilon\right) = \left(S_{\rm c} + S_{\rm p} + S_{\rm e}\right) / \left(1 - \Phi_w\right) = q. \tag{2.27}$$
⁴³⁸

We note that: Φ_e is obtained using (2.25); S_c , S_p and S_e ⁴³⁹ are functions of Φ_c , Φ_p and Φ_e . Thus (2.25), (2.27) and ⁴⁴⁰ (2.26), together with initial conditions on Φ_a (see Online Resource 2), ξ and boundary conditions on v, completely specify the time-evolving growth mapping **G**, provided that the mechanical stress state can be computed (Fig. 1; Sect. 2.1.1). ⁴⁴⁵

Initial and boundary conditions on tissue growth During normal tissue maintenance, in the absence of inflammation or administered contractile agonist, we assume that ASM proliferation, recruitment and apoptosis, and ECM degradation and deposition in the airway wall balance to generate a homeostatic state. The non-trivial homogeneous steady state for (2.26), for which v = 0, is given by

$$\boldsymbol{P}_{p}^{*} = \frac{c_{p}c_{c0}^{2}}{c_{a}(c_{pc} - c_{p0})^{2}\rho_{p}^{T}},$$
(2.28a) 453

$$\Phi_{\rm c}^* = \frac{c_{\rm p0}c_{\rm c0}}{c_{\rm a}(c_{\rm pc} - c_{\rm p0})\rho_{\rm c}^{\rm T}},\tag{2.28b}$$

$$\Phi_{\rm e}^* = \frac{c_{\rm e0} + c_{\rm pe} \Phi_{\rm p}^* \rho_{\rm p}^{\rm I}}{c_{\rm de} \rho_{\rm e}^{\rm T}},$$
(2.28c) 455

where we have made use of (2.18), (2.21), and (2.23). A linear stability analysis of (2.26) ensures *a priori* that the steady state (2.28) is stable. Hence, we impose this homeostatic steady state as the initial condition 459

$$\Phi_{\rm a}(\xi,0) = \Phi_{\rm a}^*, \qquad a = c, \, p, e. \tag{2.29} \quad {}_{\rm 460}$$

A zero flux condition is imposed at the inner wall and at the interface between the two layers, which in cylindrical polar co-ordinates is given by 463

$$v(\xi_1) \frac{\partial \Phi_a}{\partial \xi} \Big|_{\xi_1} = 0, \qquad (2.30a) \quad {}_{464}$$

$$v(\xi_{\rm int})\frac{\partial \Phi_{\rm a}}{\partial \xi}\Big|_{\xi_{\rm int}} = 0.$$
(2.30b) 46

In order to solve the ODE (2.27) representing growth in each layer, a boundary condition must be specified on the velocity. However, because (2.27) is first order, one is unable to specify the velocity at both the inner and outer boundaries

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466

of each layer. We therefore set the radial velocity to zero on
the outer wall, so that all growth occurs inwardly (this choice
is discussed further in Sect. 4). Additionally, we require the
velocity and displacement at the interface of the two layers
to be continuous. Hence, we have

476
$$\xi(R_2) = \xi_2 = R_2,$$
 (2.31a)

477
$$\xi(R_{\text{int}}^{(l)}) = \xi(R_{\text{int}}^{(o)}) = \xi_{\text{int}},$$
 (2.31b)

478 $v(\xi_2) = 0,$ (2.31c)

479
$$v(\xi_{\text{int}}^{(l)}) = v(\xi_{\text{int}}^{(o)}),$$
 (2.31d)

where the superscripts (*i*) and (*o*) denote limiting values
taken from the inner and outer layers, respectively.

Inflammatory or agonist challenge protocol Episodes 482 of inflammation-inducing allergen or contractile agonist 483 challenges are represented by (2.16) in (2.14) or (2.15), 484 respectively. Simulations are performed over a 1000 day 485 interval, with the challenges confined to the first 50 days, 486 thereby allowing a long resolution period to investigate the 487 effects of the challenges on long-term airway remodelling 488 post-challenge. The numerical solution method is outlined 489 in Online Resource 1.3. 490

491 **2.2 Determination of material parameters**

The passive material parameters are determined by fit-492 ting (2.12) to the quasi-static pressure-radius inflation data 493 in LaPrad et al. (2010) via nonlinear regression using 494 lsgcurvefit.min MATLAB, with termination tolerances 495 set to default values. Material parameters are given in Online 106 Resource 2, and the fit to the data ($R^2=0.9978$) is depicted 497 in the results below. The active response is determined 498 by selecting values for T_c that qualitatively matched the 499 active pressure-radius curves given in the work of Hiorns 500 et al. (2014) for similar values of contractile agonist, k. All 501 model parameter values and their descriptions are provided 502 in Online Resource 2. 503

504 3 Results

To investigate the behaviour of our novel mechanochemical 505 morphoelastic model, we first performed a one-at-a-time sen-506 sitivity study (Online Resource 3) on selected parameters of 507 most relevance to airway remodelling. The analysis showed 508 that remodelling was most sensitive to the magnitude and 509 resolution rate of inflammation, during inflammatory chal-510 lenges. However, due to the possible effect of combination 511 of the large number of parameters in this model (see Online 512 Resource 2) and the large differences in remodelling that 513 occur between inflammation and contractile agonist chal-514 lenges, we chose to perform a series of paired parameter 515

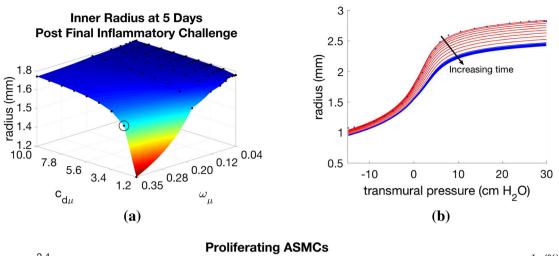
explorations. These are used to investigate the effect of 516 repeated inflammatory episodes, and mechanical forces that 517 arise from repeated ASM contractions, on long-term airway 518 remodelling and effective mechanical properties of the air-519 way. Parameters are set to default values unless varied in 520 the simulations. Results are discarded for parameter choices 521 that lead to airway growth or contraction completely into 522 the lumen, i.e. the inner radius decreases to zero. Unless 523 otherwise specified, remodelling occurs in the outer layer 524 only. 525

Effect of inflammatory challenges In our first set of sim-526 ulations, we apply only inflammatory challenges $(a_k =$ 527 0), mimicking regular allergen exposures in experimental 528 studies, and explore the response to changes in challenge 529 frequency, ω_{μ} , and inflammation resolution rate, $c_{d\mu}$. From 530 an initial inner radius of 1.8mm, we observe inward airway 531 remodelling towards the lumen, as depicted in Fig. 4a, show-532 ing the inner radius at 5 days post-final challenge for each 533 parameter pair. In particular, we observe a "switch" effect, 534 in which the response is insensitive to increases in ω_{μ} and 535 decreases in $c_{d\mu}$ for a large region of parameter space, but 536 dramatic increases in remodelling occur beyond a thresh-537 old parameter set. Contractile agonist retention time, defined 538 as the number of days between the final inflammatory or 539 agonist challenge and the reduction in the total amount of 540 agonist in the airway cross-section to near zero ($< 1 \times 10^{-6}$), 541 remains rather low for relatively high ω_{μ} and low $c_{d\mu}$, and 542 is relatively insensitive to ω_{μ} , but we observe a threshold 543 in $c_{d\mu}$ below which the agonist resolution time increases 544 abruptly to 15 days from a baseline of approximately 10 545 days. 546

Detailed results for a specific parameter choice (high-547 lighted by circles in Fig. 4a) are shown in Fig. 4b-e. Static 548 pressure-radius curves are computed for time points dur-549 ing and following inflammatory challenges (Fig. 4b). For 550 these parameter choices, the contractile agonist concentra-551 tion remains low, since the rate of inflammation-induced 552 agonist release is relatively low, and very little ASMC con-553 traction occurs. During challenges, the pressure-radius curve 554 shifts downward as the airway thickens due to inflammation-555 induced remodelling. Following challenges, the curves con-556 tinue to shift slightly downwards, due to a small amount of 557 post-challenge remodelling, prior to a return to the steady 558 state. 559

The total amount of ASM and ECM increases during 560 inflammatory challenges as ASMCs switch from contrac-561 tile to proliferative phenotype, and their volume fractions 562 relative to that of ECM increase over time (Fig. 4c, d). Rela-563 tively low mechanical stresses arise during challenges for this 564 parameter set, as inflammation induces only a small amount 565 of contractile agonist release, and hence contraction is also 566 minimal. We observe compressive radial stresses in the air-567 way mid-wall. In the circumferential direction, the stresses 568

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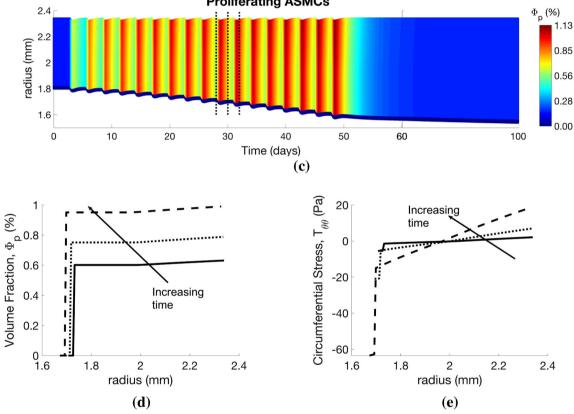
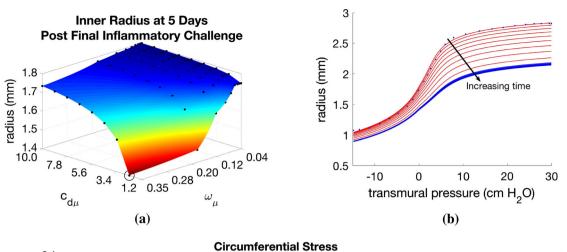


Fig. 4 Effect of inflammatory challenges on airway remodelling and mechanics. Variation in **a** remodelled geometry with inflammation frequency (ω_{μ}) and resolution ($c_{d\mu}$) parameter values. Illustrative results are evaluated at the circled point on the surface: **b** pressure–radius curve (red lines correspond to points during challenge; blue lines indicate res-

olution period; blue dots indicate data of LaPrad et al. 2010); **c** volume fraction of proliferative ASMCs (Φ_p) as a function of radius and time, **d** Φ_p and **e** $T_{\theta\theta}$ as functions of radius at days 28, 30, and 32 (indicated by dotted lines in **c**). Additional plots are provided in Online Resources 4 and 5

are found to be tensile towards the outer edge of the airway
 wall and compressive near the lumen (Fig. 4e). Mechanical
 stresses in the axial direction are compressive due to tissue
 incompressibility (Online Resource 5).

Effect of inflammatory challenge-induced ECM changes in the subepithelial basement membrane Next, to model SBM thickening associated with asthma, we allow for ⁵⁷⁵ inflammation-induced ECM deposition and degradation in ⁵⁷⁶ the SBM, as well as in the outer layer, by setting c_{e0} , c_{e1} , c_{e2} ⁵⁷⁷ and c_{de} in the inner layer to the default values given (for ⁵⁷⁸ the outer layer). The addition of inflammation-induced ECM ⁵⁷⁹ deposition results in increased inward remodelling (Fig. 5a), ⁵⁸⁰



2.4 $T_{ heta heta}$ (Pa) 36 2.2 radius (mm) 5 2 -26 1.8 -57 1.6 -87 1.4 0 10 40 50 60 100 20 30 Time (days) (c)

Fig. 5 Effect of inflammatory challenge-induced subepithelial basement membrane thickening on airway remodelling and mechanics. Variation in **a** remodelled geometry with inflammation frequency (ω_{μ}) and resolution $(c_{d\mu})$ parameter values. Illustrative results are evaluated at the circled point on the surface: **b** pressure–radius curve (red lines

correspond to points during challenge; blue lines indicate resolution period; blue dots indicate data of LaPrad et al. 2010) and c circumferential stress ($T_{\theta\theta}$) as a function of radius and time. Results are similar to Fig. 4, except here, inflammation also drives SBM thickening

which, in turn, decreases effective airway compliance, as 581 shown by modified pressure-radius curves (Figs. 5b, c, 582 f, 4b). Compressive circumferential stresses in the SBM 583 are correspondingly reduced (Fig. 5c), due to increased 584 cross-sectional area. In contrast, peak tensile circumferential 585 stresses in the outer layers are greater with SBM thickening, 586 presumably as a result of a thicker, stiffer inner layer and 587 therefore an effectively stiffer airway. 588

Effect of contractile agonist challenges Here, we apply 589 only contractile agonist challenges ($a_{\mu} = 0$), mimicking reg-590 ular methacholine exposures in experimental animal studies. 591 We highlight that, in these simulations, all remodelling is 592 driven by mechanotransduction, i.e. by local, stress-mediated 593 phenotype switching. We find that increasing the agonist 594 challenge frequency (ω_k) and decreasing the contractile ago-595 nist resolution rate (c_{dk}) lead to increased remodelling at 5 596 days post-challenge. As in the inflammatory-only challenges, 597 severe remodelling is observed only beyond a threshold 598 parameter set. Contractile agonist resolution time increases 599 with decreasing agonist resolution rate, c_{dk} , with a thresh-600 old below which there is a dramatic change in resolution 601

time from a baseline of approximately 5 days to over 60 days (Fig. 6a). The dramatic increase in resolution time is a result of the build-up of agonist concentration demonstrated by nonzero agonist concentrations at the end of each challenge (Online Resource 5). Similar to the inflammation-only challenges, the contractile agonist resolution time is relatively insensitive to the challenge frequency, ω_k .

Despite the reduced ECM volume fraction in the outer 609 part of the airway (see Online Resource 5), the overall effec-610 tive stiffness of the remodelled airway is increased during 611 contractile agonist challenges, as indicated by the contin-612 ued downshift in pressure-radius curves at high transmural 613 pressures (Fig. 6b). To inflate the airway, a relatively high 614 transmural pressure is required to overcome the increased 615 contractile forces in the strongly contracted state, with a 616 strong downward shift at all pressures, and the appearance of 617 a significantly more compliant portion that shifts towards the 618 right. When the pressure is great enough to cause stretches 619 that exceed the recruitment threshold (see Sect. 2.1.1 and 620 Online Resource 1.2), there is a very rapid increase in the 621 recruitment of ECM. Tissue growth (increased airway thick-622

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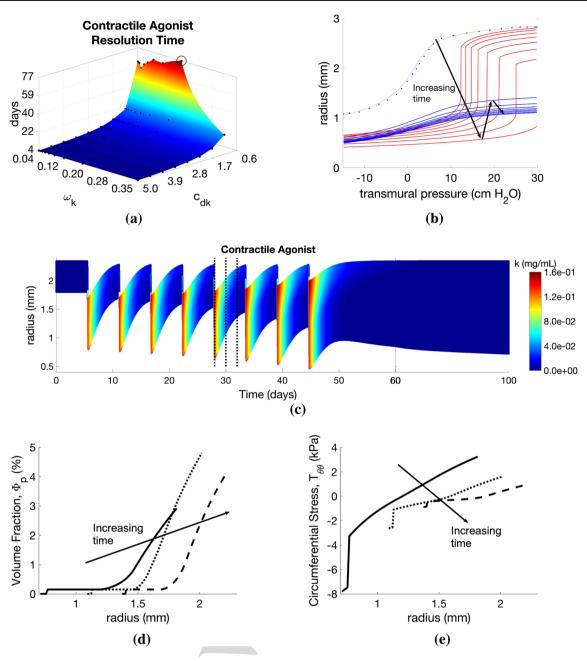


Fig. 6 Effect of contractile agonist challenges on airway remodelling and mechanics. Variation in **a** agonist resolution rate with contractile agonist frequency (ω_k) and resolution (c_{dk}) parameter values. Illustrative results evaluated at the circled point on the surface: **b** pressure-radius curve (red lines correspond to points during challenge;

ness) also contributes to the observed downward shift. The separation of the effects of contractile agonist and tissue growth becomes clear following challenges, where the compliant portion of the curve disappears (first curve following challenges, Fig. 6b), and the high pressure portion of the pressure-radius curves shifts downwards as remodelling continues post-challenge.

blue lines indicate resolution period; blue dots indicate data of LaPrad et al. 2010), **c** contractile agonist concentration (*k*) as a function of radius and time, **d** Φ_p and (e) $T_{\theta\theta}$ as functions of radius at days 28, 30, and 32 (indicated by dotted lines on **c**). Additional plots are provided in Online Resources 4 and 5

As contractile agonist challenges cause the airways to contract (Fig. 6c), local ASMC phenotype switching (Fig. 6d) and local release of contractile agonist increase with increasing tensile circumferential stress in the outer part of the airway wall (Fig. 6e) that arises from the agonist-induced contraction. Small amounts of locally activated residual contractile agonist continue to drive remodelling post-challenge, 636 ⁶³⁷ generating a feedback loop that slows agonist clearance ⁶³⁸ (Fig. 6a), accounting for build-up in agonist concentration.

Effect of changes in intrinsic ASM hyper-responsiveness 639 To simulate the effects of increasing intrinsic responsive-640 ness of ASMCs to contractile agonist, we return to the 641 inflammation-only challenges and investigate the effect of 642 paired changes in responsiveness (T_c) and challenge fre-643 quency (ω_{μ}) . We find that remodelling increases with $T_{\rm c}$ 644 and ω_{μ} (Fig. 7a), but a threshold effect only exists for 645 increasing T_c . Increasing T_c also leads to much slower ago-646 nist clearance. At low values of T_c , the agonist eventually 647 clears (Fig. 7a, b), while at high values, a self-perpetuating 648 feedback loop is established (Fig. 7a, c), due to the local 649 mechanotransduction-driven agonist release, which is not 650 resolved, and the airway eventually grows in to the lumen. 651

Global versus local effects of inflammatory and contrac-652 tile agonist challenges In Figs. 4 and 6, we illustrate the effect 653 of varying frequency and resolution rate of inflammation- and 654 contractile agonist-only challenges, respectively. Here, we 655 compare instead the effects of varying amplitude and resolu-656 tion rate in these globally applied challenges (first and second 657 columns, Fig. 8). Additionally, we compare these effects to 658 changes in rates of inflammation- $(a_{k\mu})$ and stress-mediated 659 (a_c) local contractile agonist release (third column, Fig. 8). 660

Increasing the amplitude (a_{μ}) and decreasing the reso-661 lution rate $(c_{d\mu})$ of inflammatory-only challenges lead to 662 increased remodelling (Fig. 8a), without a clear threshold 663 effect. Additionally, the degree of remodelling becomes less 66 dependent on the inflammation amplitude for sufficiently fast 665 resolution. At the (relatively low) default value of ASMC 666 responsiveness, T_c , employed here, the contractile agonist 667 clears rapidly from the tissue upon cessation of inflamma-668 tory challenges, due to the small amounts of local agonist 669 activated by mechanical stress (Fig. 8d). Low levels of ago-670 nist release during inflammatory challenges results in limited 67 contraction and therefore very low mechanical stresses. 672

In contrast, we observe a very sharp threshold for increas-673 ing contractile agonist magnitude (a_k) and decreasing agonist 674 clearance rate (c_{dk}) (Fig. 8b). Locally activated agonist 675 remains in the tissue longer at lower clearance rates, and 676 its effect is evident in the transmural variations in circumfer-677 ential stress (Fig. 8f) in the time period following cessation 678 of challenges (> day 50). High contractile agonist concen-679 tration induced by the agonist challenge generates significant 680 bronchoconstriction and therefore relatively higher mechan-681 ical stresses than with inflammatory challenges. 682

Increasing the rate at which inflammation induces contractile agonist release $(a_{k\mu})$ exacerbates remodelling, and increasing the rate of stress-induced agonist release (a_c) increases the positive mechanotransductive feedback, leading to additional remodelling (Fig. 8c). With both an increase in stress-mediated feedback and in inflammationinduced contractile agonist release, agonist resolution time

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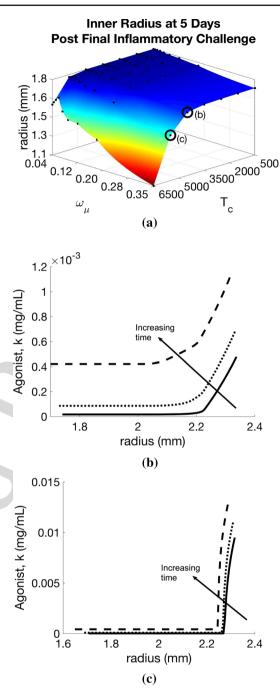


Fig. 7 Effect of airway smooth muscle cell hyper-responsiveness on airway remodelling, active tone, and mechanotransductive feedback. Variation in **a** remodelled geometry with inflammation frequency (ω_{μ}) and hyper-responsiveness (T_c) parameter values. Transmural contractile agonist concentration is plotted as a function of radius at days 28, 30, and 32 for parameter value pairs indicated by the circled points on **a**: **b** where contractile agonist eventually clears from the tissue and **c** where contractile agonist remains in the tissue in an indefinite feedback loop, causing increasing remodelling long after cessation of challenges

is increased, though it remains significantly faster than with direct contractile agonist challenge. Increasing $a_{k\mu}$ and a_c thus leads to an effective combination of inflammatory and contractile agonist challenges, as increased contrac-

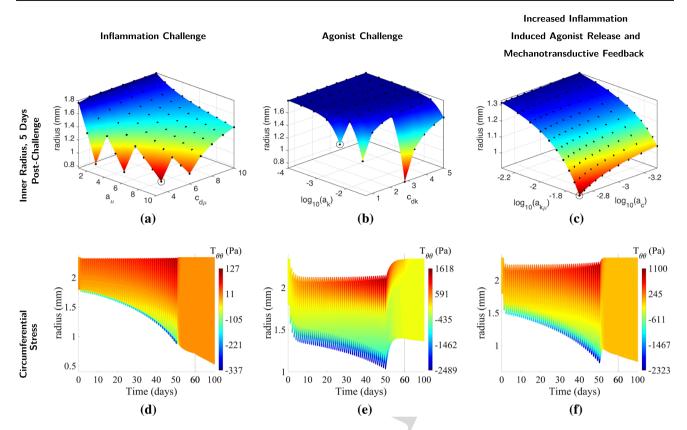


Fig. 8 Global versus local effects on airway remodelling and active tone. Variation in remodelled geometry (1st row) with parameter pairs: inflammation magnitude and resolution ($c_{d\mu}$, a_{μ} ; 1st column), contractile agonist magnitude and resolution (c_{dk} , a_k ; 2nd column), and

inflammation-induced contractile agonist release and mechanotransductive agonist release ($a_{k\mu}$, a_c ; 3rd column). Circumferential stress (2nd row) is plotted as a function of radius and time for parameter value pairs indicated by the circled points on the surfaces

tion is observed during inflammatory challenges, and overall
 remodelling is higher than with agonist challenge alone. The
 higher levels of contractile agonist release during inflamma tory challenges result in greater mechanical stresses (Figs. 8f)
 from agonist-induced bronchoconstriction.

Effect of phenotype switching and proliferation rate mod-699 ulation by tensile versus compressive mechanical stress In 700 all of the above simulations, we have assumed that only ten-701 sile stresses can increase phenotype switching (via (2.19) and 702 nonzero c_{cp}^{J} in (2.20)) and that the proliferation rate of the pro-703 liferative ASMCs is unaffected by local stress (default value 704 $c_{\rm p}^{J} = 0$). Here, we investigate the effect of varying these 705 parameters (in inflammatory-only challenges) for both ten-706 sile and compressive stress-modulated phenotype switching 707 and proliferation/recruitment rate. We vary either the stress-708 induced switching rate (c_{cp}^{J}) or the proliferation rate (c_{p}^{J}) and 709 the contractile agonist clearance rate (c_{dk}) . Transmural dis-710 tributions of proliferating ASMC volume fraction at day 51 711 (Fig. 9), selected from the overall results of this parameter 712 exploration (Online Resource 6), illustrate the effects of these 713 parameters on remodelling. 714

We observe similar amounts of remodelling for increases in both tensile and compressive stress-modulated pheno-

type switching rate and decreasing agonist clearance rate 717 with no clear threshold effect (see Online Resource 6). For 718 the same parameter ranges, agonist resolution times are 719 observed to be similar and relatively independent of c_{cp}^{J} for 720 both cases. Distributions of the proliferative ASMC volume 721 fraction significantly differ in the two cases, with larger vol-722 ume fractions at the outer edge of the airway wall in the 723 tensile stress-modulated case and at the inner edge in the 724 compressive stress-modulated case (Fig. 9a), reflecting the 725 observed circumferential stress heterogeneity and contrac-726 tile agonist build-up. For our given initial conditions (Online 727 Resource 2), both tensile and compressive stress-induced 728 increase in phenotype switching results in a greater amount 729 of airway remodelling than stress-induced increase in pro-730 liferation rate (Fig. 9a, cf. b). Agonist retention is similar 731 between the two cases. 732

4 Discussion

The mechanisms underlying the interaction of inflammation, airway hyper-responsiveness and airway remodelling 735 in asthma are poorly understood. Thus, we have devel-736

733

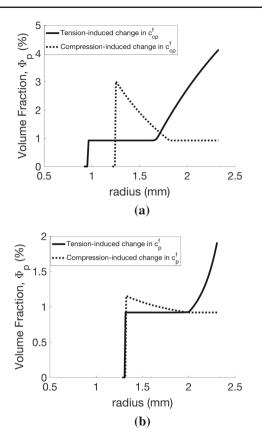


Fig. 9 Effect of mechanotransductive mechanisms on airway mechanics and remodelling. Volume fraction of proliferating airway smooth muscle cells as a function of radius at day 51, for either tensile (solid lines) or compressive (dotted lines) mechanical stress-induced changes in ASMC (**a**) phenotype switching rate or **b** proliferation rate. Parameters for **a** are $c_{dk} = 0.83$ and $c_{cp}^f = 0.05$ and for **b** are $c_{dk} = 0.50$ and $c_p^f = 0.05$. Increased remodelling occurs in the former, even at a higher agonist clearance rate

oped a new computational model of coupled biochemical-737 and mechanotransduction-induced remodelling of the air-738 way wall. In the model, accumulation of ASM and ECM is 739 driven by switching of ASMCs from a contractile to prolifer-740 ative phenotype (which is capable of synthesizing ECM), and 741 also, via a novel mechanotransductive feedback mechanism 742 by which a mechanically stressed tissue releases mitogenic 743 growth factors and contractile agonists. 744

Our results qualitatively match those reported for asth-745 matic airways (as well as results from our previous model; 746 see Online Resource 7). For example, we have predicted 747 narrowing of the lumen and a downward shift in the pressure-748 radius curves that have been previously reported in humans 749 (Williamson et al. 2011). Our model also predicts wall thick-750 ening of airways due to increased ASM volume, which has 751 been reported both in asthmatic patients (James et al. 2012, 752 2009) and in animal models (Alrifai et al. 2014). 753

The inflammatory twitch hypothesis suggests that selflimiting inflammatory events are invoked in the presence of an allergic stimulus and dissipate as the stimulus disappears,

with long resolution periods being a possible explanation for 757 the chronic inflammation characteristic of asthma (Pothen 758 et al. 2016). Our results suggest that these long resolution 759 periods may increase remodelling associated with severe 760 asthma. In animal models of asthma, for example, transitory 761 inflammatory cell recruitment, and increases in thickness of 762 both ASM bundles and the SBM, have been associated with 763 repeated/successive allergen challenges (Johnson et al. 2004: 764 McMillan and Lloyd 2004). This response is thought to be 765 the effect of pro-remodelling growth factors affecting acti-766 vation of mast cells, ASM proliferation and ECM deposition 767 (Naveed et al. 2017; James 2017) or increased recruitment 768 of ASM progenitors such as myofibroblasts into the ASM 769 bundles (Gerarduzzi and Battista 2017; Singh et al. 2014; 770 Saunders et al. 2009). Thicknesses of both ASM bundles and 771 the SBM have been shown to gradually return to control lev-772 els upon cessation of challenges (Alrifai et al. 2014; Leclere 773 et al. 2012), with the resolution periods of inflammation and 774 tissue growth being on the order of days to months (Pothen 775 et al. 2016; Alrifai et al. 2014), which is reflected in our sim-776 ulations, in which inflammatory status, μ , remains elevated 777 with decreased clearance rate, $c_{d\mu}$. 778

Our work broadly follows that of Skalak (1980) and 779 Rodriguez et al. (1994) in which growth and remodelling 780 is treated as a topological mapping from a reference con-781 figuration to a grown configuration followed by an elastic 782 deformation. A key component of this model is the implicit 783 separation of timescales between the growth and the (instan-784 taneous) elastic deformations. This approach has previously 785 been applied to model airway narrowing (in which the folding 786 that occurs during growth was modelled utilizing buck-787 ling theory; Moulton and Goriely 2011a, b), but this was in 788 the context of a single phase, and growth kinematics were 789 prescribed directly. Multiphase or mixture theory has been 790 utilized in numerous cardiovascular studies (e.g. Valentin 791 et al. 2013; Gleason and Humphrey 2005; Gleason et al. 2004; 792 Humphrey and Rajagopal 2003, 2002), where the models 793 were driven by evolution of the growth configuration of each 794 phase, but without consideration of their interactions. To our 795 knowledge, the approach taken here, in which the spatio-796 temporal evolution of the individual tissue constituents is 797 driven by underlying biological and mechanochemical pro-798 cesses, has not been considered in airway remodelling. Thus, 799 the multiphase model proposed here addresses the limitations 800 of previous models by considering in detail the interactions 801 between tissue constituents, as in the studies of Ateshian 802 (2007) and Aparício et al. (2016). We use our model to carry 803 out a series of parameter exploration studies to identify poten-804 tial mechanisms underlying the pathogenesis and evolution 805 of asthma, described below. 806

Impaired resolution of inflammation may explain airway remodelling characteristic of asthma As in our previous model (Chernyavsky et al. 2014), slower resolution of inflam-

mation has a greater effect on airway wall thickening than 810 either challenge frequency or amplitude (Figs. 4a, 8a), as 811 a result of slower clearance of residual pro-remodelling 812 and pro-contractile cytokines (See Online Resource 7). This 813 effect may be responsible for increased remodelling and 814 bronchoconstriction observed in patients with severe asthma 815 that is poorly controlled with anti-inflammatory medications, 816 e.g. corticosteroids. In these cases, inflammation may not be 817 effectively cleared, e.g. by failure to induce inflammatory 818 cell apoptosis (Wenzel 2012; Woolley et al. 1996). 819

Inflammation-independent bronchoconstriction-mediated 820 mechanical stresses could drive airway remodelling Grainge 821 et al. (2011) have demonstrated the possibility of inflam-822 mation-independent airway remodelling in asthmatics 823 through application of methacholine-only challenges. Our 824 model suggests the mechanisms by which this may occur. We 825 show how tensile stresses along (circumferentially-oriented) 826 muscle fibres, arising from agonist-induced contraction of 827 ASMCs, can cause a local release of additional agonist 828 (Fig. 6c). This mechanotransductive pathway may represent 829 stretch-induced activation of latent TGF- β , which has both 830 mitogenic (Halwani et al. 2011) and contractile agonist (Oji-831 aku et al. 2017; Oenema et al. 2013; Desmoulière et al. 2005; 832 Grinnell and Ho 2002; Montesano and Orci 1988) properties. 833 This additional local increase in agonist concentration trig-834 gers a local tensile stress-induced cell phenotype switching, 835 thus driving increases in ASM mass. We have also shown that 836 compressive stress-induced increases in phenotype switching 837 or proliferation rate (Fig. 9), possibly mediated by shed-838 ding of growth factors such as EGFR and ET-1, could also 839 explain the inflammation-independent remodelling observed 840 in Grainge et al. (2011). Contractile agonists alone are insuf-841 ficient to induce physiological changes in mice, as measured 842 with plethysmography (Mailhot-Larouche et al. 2018). Our 843 simulations suggest that very frequent challenges, impaired 844 agonist clearance or increased rate of stress-driven ago-845 nist activation is required to cause significant remodelling 846 (Fig. 8b). It is possible that an intrinsic inability to clear 847 agonist, increased sensitivity of ASM/ECM to stress-driven TGF- β activation or EGFR/ET-1 shedding could place the 849 asthmatic subject in a high-risk region of the parameter space. 850 Interaction of inflammation with intrinsic ASM hyper-851 responsiveness could explain persistent contractile tone and 852 severe remodelling Our simulations show that increased 853 intrinsic hyper-responsiveness causes increased remodelling 854 (Fig. 7a) and significantly increased contractile agonist 855 resolution times. This response is a result of increased bron-856 choconstriction at a given agonist concentration, driving 857 increases in tensile stresses and hence further (mechan-858 otransductive) activation of pro-mitogenic mediators and 859 contractile agonists such as TGF- β . These results high-860 light that the retention of contractile agonist associated with 861 increased hyper-responsiveness is a candidate mechanism 862

accounting for the persistent tone observed in asthmatics 863 (Brightling et al. 2002). As expected, long resolution times 864 are associated with impaired clearance of contractile agonist, 865 c_{dk} (Fig. 6a). Notably, delayed contractile agonist resolution 866 occurs when both the ASMCs are very hyper-responsive and 867 inflammation challenge frequency is high. The combination 868 of identified mechanisms could therefore be responsible for 869 persistent contractile tone and remodelling, post-challenge, 870 in hyper-responsive airways (Kariyawasam et al. 2007). 871

Increased airway remodelling could occur via local 872 mechanotransductive effects An increase in both inflammation- 873 and mechanical stress-induced contractile agonist release 874 (Fig. 8c) leads to a condition that is an effective combination 875 of inflammation-only (Fig. 8a) and agonist-only challenge 876 (Fig. 8b). Increased rates of inflammation-induced agonist 877 release $(a_{k\mu})$ could represent degranulation of the larger num-878 bers of mast cells present in the ASM bundles of asthmatics 879 (Naveed et al. 2017) and hence the production of contractile 880 agonist (e.g. histamine). These released factors ultimately 881 elicit a pro-mitogenic response where (tensile) mechanical 882 stresses arising from ASMC contraction drive tissue remod-883 elling via stress-induced phenotype switching of ASMCs. 88/ Separately, under the assumption of mechanically activated 885 mediators (e.g. TGF- β), increasing stress-activated release 886 $(a_{\rm c})$ increases agonist-induced bronchoconstriction, leading 887 to further agonist release and thus further contraction and 888 stress-induced remodelling in a perpetual feedback loop. The 889 feedback mechanism may explain how coupled inflamma-890 tion and bronchoconstriction lead to increased remodelling 891 in severe asthma. 892

Airway wall thickening may be a normal, local mechano-893 protective response but ultimately becomes detrimental 894 to global lung mechanics and function The increase in 895 cross-sectional area from thickening of the SBM counter-896 intuitively may serve to reduce mechanical stresses, arising 897 during bronchoconstriction (Fig. 5c). This reduction in stress 898 could, in turn, reduce compressive stress-driven shedding of 899 growth factors mediated by epithelial cells. Our model does 900 not allow for buckling of the SBM, due to our imposition 90 of axisymmetry, but reduced compressive stresses as a result 902 of the thicker SBM could also reduce propensity to buckle 903 (Moulton and Goriely 2011a) and hence limit airway nar-904 rowing during bronchoconstriction. 905

Our results also indicate that remodelling-induced changes in functional mechanical properties of the airways may depend on what drove the remodelling. For instance, we show that the pressure–radius curves during inflammationonly challenges have qualitatively different characteristics to those associated with agonist-only challenges (cf. Fig. 4b, 6b).

Interaction of different underlying mechanisms may contribute to the existence of different asthma phenotypes A combination of various characteristics defines asthma subgroups, 913

or phenotypes (see Wenzel 2012 and references therein). 016 Here, we have identified various parameter combinations that 917 may contribute to the existence of different asthma pheno-918 types. For example, the presence of eosinophils in the lung 919 tissue is associated with thickened SBM, high expression of 920 TGB- β , increased frequency and severity of symptoms, and 921 more near-fatal events (Wenzel 2012; Miranda et al. 2004). 922 Persistent eosinophils, despite corticosteriod treatment (typ-923 ically associated with eosinophil apoptosis), is associated 924 with adult-onset, less allergic severe $(T_H 2)$ asthma (Wen-925 zel 2012). The slower clearance of inflammation leading to 926 increased remodelling (Figs. 4a, 8a) and reduced contrac-927 tile agonist clearance may underlie this type of asthma. Our 928 results (Fig. 5) suggest that a thickened SBM may be associ-929 ated with the increased presence of eosinophils, in agreement 930 with the SBM thickness observed in non-eosinophilic com-931 pared with eosinophilic asthma (Miranda et al. 2004). 932

Our results show that for regular bronchoconstrictive 933 events to induce long-term airway remodelling an extreme 934 set of consequences (Figs. 6, 8b) is required, which may 935 be the reason why, to our knowledge, contractile agonist-936 induced remodelling has not been observed in animal studies 037 (e.g. Mailhot-Larouche et al. 2018). However, the study by 938 Grainge et al. (2011) shows that contractile agonist chal-939 lenges do lead to increased ASM thickness in humans. That 940 mice do not spontaneously develop asthma but that humans 941 do, suggests that the subjects of the Grainge et al. (2011) 942 study may lie in a different region of parameter space, i.e. 943 beyond the relevant thresholds. 944

Methacholine challenges have been shown to increase air-945 way responsiveness in humans over the short term (Gazzola 946 et al. 2017), and increased smooth muscle responsiveness 947 may be independent of inflammation in some asthma phe-948 notypes (e.g. non- $T_H 2$ asthma; Wenzel 2012). Our model 949 suggests a possible mechanism: with intrinsically hyper-950 responsive ASMCs, normal exposure to contractile agonists 951 alone (in the absence of inflammation) may be sufficient to 952 drive further agonist release (Fig. 6b), and increase ASMC 953 responsiveness, thus leading an asthma symptom phenotypes not typically associated with inflammation, such as exercise-, 955 obesity-induced asthma, or non- $T_H 2$ asthma. 956

Increased ASMC hyper-responsiveness (Fig. 7) and/or 957 increased mechanotransduction (Fig. 8c) may exacerbate 958 remodelling, even at normal levels of inflammation (pauci-959 granulocytic asthma; Carr et al. 2017). Thus, these mecha-960 nisms may underlie the degrees of severity associated with 961 inflammation-induced $(T_H 2)$ as thma: mild to moderate as th-962 matics may be characterized by increased inflammation but 963 normal ASMC responsiveness (Fig. 4), while severe asth-964 matics may have increased hyper-responsiveness that leads to 965 pathological remodelling (Fig. 7). Alternatively, mechanisms 966 that reverse influx of inflammatory cells, and hence, return 967 inflammation to normal levels, may have become impaired 968

(Pothen et al. 2016; Brightling et al. 2012). A remodelled air way exhibiting a combination of the characteristics described
 above may be primed for severe or even fatal bronchospasms
 in which airway contraction completely obstructs airflow.

Model limitations and future work Models of this nature 973 necessarily require some simplifying assumptions. In partic-974 ular, we have assumed that the airway remains axisymmetric 975 (and free of shear) during both growth and elastic deforma-976 tion. This simplified approach, in which only radial growth 977 is considered, permits more straightforward analysis of the 978 effects of varying concentrations of tissue constituents and 979 contractile agonists across the airway wall. Nevertheless, our 980 model is novel in accounting for local mechanotransductive 981 effects and these spatial distributions. However, we note that 982 some growth may occur circumferentially and, possibly, axi-983 ally, in vivo. Circumferential growth/atrophy has been shown 984 to underlie the development of residual stresses in arteries 985 (Rodriguez et al. 1994); however, airways have been shown 986 to exhibit little or no residual stresses (McKay et al. 2002), 987 and so we omit this growth mode from the model for sim-988 plicity. Axial growth is similarly neglected, based on a lack 989 of experimental data on axial growth of airways. The growth aan models of Ren (2013) and Grytsan et al. (2017) do account 991 for both isotropic and varying degrees of anisotropic growth 992 but do not consider heterogeneous spatial distributions. A 993 more comprehensive approach would be to extend the mod-994 els analysed herein to 3D. However, the numerical solution 995 of the resulting equations is beyond the scope of the current 99 study. Additionally, our imposition of axisymmetry prevents 007 us from considering buckling of the stiff SBM. Future work 998 could involve utilizing this model to predict regions of high 999 compressive stresses in which buckling could occur (Moul-1000 ton and Goriely 2011a). 1001

To solve (2.27), we specify zero radial velocity at the outer 1002 wall, so that growth occurs inwardly. We note that this choice 1003 is somewhat arbitrary and that the growth velocity could be 1004 specified at any point along the wall thickness. We choose 1005 to specify zero growth on the outer boundary based on evi-1006 dence that airways appear to narrow during asthma. Studies 1007 on human bronchial segments have shown that increased 1008 ASM in asthmatics contributes to exaggerated airway nar-1009 rowing (Noble et al. 2013). 1010

We do not allow for the separate evolution of the individ-1011 ual constituents' reference configurations, as in Humphrey 1012 and Rajagopal (2002). If our assumptions were relaxed so 1013 that these could move independently, interphase drag may be 1014 used to more accurately account for stress-induced activation 1015 of latent TGF- β . Moreover, changes in reference configura-1016 tions, in addition to non-axisymmetric growth, could allow 1017 for the development of residual stresses. Although healthy 1018 airways exhibit negligible or small residual stresses (McKay 1019 et al. 2002), to our knowledge these have not been mea-1020 sured in remodelled airways. Relaxing this constraint would 1021

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present a challenge in the theoretical development and in the
numerical solution that is beyond the scope of the current
work.

We have assumed that collagen fibre recruitment initiates 1025 at stretches above unity, with an exponential function rep-1026 resenting gradually increasing fibre uncrimping. Rigorous 102 experimental analysis of the airway structure-function rela-1028 tionship, through coupled mechanical testing and advanced 1029 microscopic imaging (e.g. Hill et al. 2012; Clifford et al. 1030 2011), would enable incorporation of fibre dispersion and 1031 recruitment to refine our model (e.g. Gasser et al. 2006; 1032 Sacks 2003; Lanir 1983, 1979). Also, we have not accounted 1033 for diffusion of applied contractile agonists, or of activated 1034 cytokines such as TGF- β . Finally, migration of myofibrob-1035 lasts (ASM progenitors) into the muscle bundle has been 1036 hypothesized as a mechanism of increased ASM. Although 1037 this migration (and differentiation into ASMCs) has not 1038 been modelled here explicitly, the ASMC proliferation in 1039 our model could instead represent this recruitment of ASM 1040 progenitors, and the timescale associated with migration is 1041 implicitly accounted for in the proliferation rate (reinter-1042 preted as a 'recruitment' rate of myofibroblasts which then 1043 become ASM). 1044

Notwithstanding these limitations, key advantages of our 1045 model are the ability to generate measurable biological and 1046 mechanical output that may be tested experimentally and the 1047 ability to separate the long-term effects of growth from the 1048 relatively shorter term mechanical effects of pressurization 1049 and active contraction. A study, combining the modelling 1050 approach described here with experimental measurements 1051 of tissue constitution, geometry, and active mechanics, is 1052 required to distinguish between the effects of geometric 1053 remodelling and changes in tissue mechanics. 1054

Therefore, this work forms the theoretical basis of a model 1055 that is currently being tested against data from in vivo animal 1056 experiments, utilizing an ovalbumin model of inflammation-1057 induced asthma in mice. We have shown how the volume 1058 fraction of constituents may be evaluated at any time along 1059 the remodelling process (e.g. Fig. 4). These will be compared 1060 to measurements made on histological sections taken from 1061 animal models of asthma, to infer underlying mechanisms as 1062 discussed above, and also for further model development and 1063 validation. Additionally, we have demonstrated the ability to 1064 assess mechanical properties of the airway as they evolve, 1065 via computed pressure-radius curves (e.g. Fig. 4b) which 1066 are commonly measured experimentally, to show changes in 1067 passive and active tissue mechanics and distinguish between 1068 healthy and diseased airways. 1069

In addition to airway remodelling, the approach outlined in this paper has broad applicability to other areas of tissue mechanics. For example, the mechanotransductive feedback mechanisms described herein likely have direct applications to models of aneurysm growth (Grytsan et al. 2017; Aparício et al. 2016). Moreover, the 1075 coupled biochemical-biomechanical elements are relevant 1076 to inflammation-associated adventitial collagen deposition 1077 observed in arteries under hypertension (Bersi et al. 2016). 1078 Furthermore, the technique we present for modelling a 1079 non-homogeneous spatial distribution of tissue constituents 1080 would be applicable to the myocardium, since local changes 1081 in tissue constitution occur during mechanical overload. 1082 e.g. in hypertension-induced myocyte hypertrophy and col-1083 lagen deposition (Hill et al. 2014) and during remod-1084 elling following myocardial infarction (Gajarsa and Kloner 1085 2011). 1086

Conclusions Our results suggest that mechanical stresses, 1087 arising from bronchoconstriction, initiated by multiple 1088 inflammatory or contractile agonist challenges, and driving 1089 agonist release, generate a mechanotransductive feedback 1090 loop. With this feedback loop, increased ASM hyper-109 responsiveness to contractile agonists and impaired clearance 1092 of inflammatory factors and contractile agonists leads to 1093 increased remodelling, increased bronchoconstriction, and 1094 maintenance of an increased baseline contractile tone due to 1095 the chronic presence of contractile agonists. The key factors 1006 that allow such a state to emerge are (i) increased intrin-1097 sic hyper-responsiveness of ASMCs to contractile agonists, 1098 (ii) delayed contractile agonist clearance from the tissue, 1099 (iii) increased release of contractile agonist by inflamma-1100 tory cells, and (iv) mechanotransductive feedback, in which 1101 active contraction generates increases in mechanical stress 1102 that subsequently initiate the release of additional contractile 1103 agonists and thus exacerbate remodelling. Targeting mechan-1104 otransductive pathways (e.g. TGF- β) and rapid resolution of 1105 inflammation or contractile agonist may have potential for 1106 treating severe forms of asthma. 1107

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Compliance with ethical standards

Conflict of interest The authors declare that they have no conflict of 1112 interest.

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Online Resources: A theoretical model of inflammation- and mechanotransduction-driven asthmatic airway remodelling

1 Additional Mathematical Details

This section provides additional details about the model development and numerical solution techniques.

1.1 Fiber Directions

Considering a cylindrical body composed of an anisotropic material reinforced by two sets of fibers dispersed in the $\theta - z$ plane, the undeformed fibre directions in polar cylindrical co-ordinates are given by

$$\mathbf{m}_{0,a}^{(1)} = \cos \Theta_a \mathbf{e}_{\theta} + \sin \Theta_a \mathbf{e}_z, \tag{S1a}$$
$$\mathbf{m}_{0,a}^{(2)} = -\cos \Theta_a \mathbf{e}_{\theta} + \sin \Theta_a \mathbf{e}_z, \tag{S1b}$$

for a given constituent a, where \mathbf{e}_{θ} and \mathbf{e}_{z} are unit vectors in the circumferential and axial directions, respectively. The current fibre direction, denoted $\mathbf{m}_{a}^{(j)}$, is obtained from the undeformed fibre directions via a push-forward operation,

$$\mathbf{m}_{a}^{(j)} = \frac{\mathbf{F} \cdot \mathbf{m}_{0,a}^{(j)}}{\sqrt{\alpha_{a}^{(j)}}},\tag{S2a}$$

where

$$\alpha_a^{(j)} = \mathbf{m}_{0,a}^{(j)} \cdot \mathbf{C}\mathbf{m}_{0,a}^{(j)}, \qquad j = 1, 2,$$
(S2b)

is the square of the fibre stretch ratio (Holzapfel, 2000), and $\mathbf{C} = \mathbf{F}^T \mathbf{F}$ is the right Cauchy-Green tensor. We further posit that all fibres, including both ASM and collagen fibres in the ECM, are oriented along the circumference (Ijpma et al, 2017), so $\Theta_a = \Theta = 0^\circ$.

1.2 Specific Forms of the Strain Energy Functions

Below we define the forms of the strain energy functions for the tissue constituents a = p, c, e. The neo-Hookean form of the strain energy function for the proliferating (p) airway smooth muscle cells (ASMCs) is given by

$$W_p = \frac{1}{2} \eta_p \left(I_1 - 3 \right),$$
(S3a)

where η_p is a material parameter representing the passive stiffness of proliferating cells, and $I_1 = \text{tr}\mathbf{C}$ is a strain invariant. The form for the contractile (c) ASMCs is given by

$$W_{c} = \frac{1}{2}\eta_{c}\left(I_{1} - 3\right) + \sum_{j=1,2} \frac{C_{c}}{2\beta_{c}} \left(\exp^{\beta_{c}\left(\alpha_{c}^{(j)} - 1\right)^{2}} - 1\right),\tag{S3b}$$

where material parameters are η_c , representing the passive (isotropic) stiffness of contractile cells, C_c , representing their passive (anisotropic) stiffness, and β_c , accounting for nonlinear stiffening with increasing deformation. The form for the extracellular matrix (ECM or e) is modeled similarly, so

$$W_{e} = \frac{1}{2} \eta_{e} \left(I_{1} - 3 \right) + \sum_{j=1,2} H \left(\alpha_{e}^{(j)} - \lambda_{u}^{2} \right) \frac{C_{e}}{2\beta_{e}} \left(\exp^{\beta_{e} \left(\alpha_{e}^{(j)} - \lambda_{u}^{2} \right)^{2}} - 1 \right),$$
(S3c)

with material parameters η_e , representing the passive (isotropic) stiffness of the embedded ECM cells, C_e , representing fibre density, and β_e , parametrizing the gradual recruitment of collagen fibres.

1.3 Numerical Solution Procedure

This section provides specific forms of the model equations that were used in the numerical scheme, as well as the numerical techniques that were used to solve the PDEs. First, we derive the equations governing the growth in each layer of the airway wall. Next, we derive a nonlinear equation that represents the elastic deformation of a two-layer multi-phase cylinder subject to pressure boundary conditions. Finally, we discuss the specific numerical schemes we used to solve these equations and the governing PDEs in the main text.

Growth. The radial growth of the airway is determined as follows. Integrating (2.27) with respect to ξ gives the velocity in the outer layer as

$$\xi v(\xi)^{(o)} = \int_{\xi_{int}}^{\xi} \xi' q^{(o)} d\xi' + K_1, \qquad \xi_{int} \le \xi \le \xi_2.$$
(S4a)

Similarly, the velocity in the inner layer is given by

$$\xi v(\xi)^{(i)} = \int_{\xi_1}^{\xi} \xi' q^{(i)} d\xi' + K_2, \qquad \xi_1 \le \xi \le \xi_{int}.$$
(S4b)

The constants K_1 and K_2 are determined by applying the zero velocity boundary condition (2.31c) and continuity of velocity at ξ_{int} (2.31d), respectively. The interface velocity is then given by (S4a) evaluated at $\xi = \xi_{int}$ to give

$$v(\xi_{int}) = \frac{d\xi_{int}}{dt} = -\frac{1}{\xi_{int}} \int_{\xi_{int}}^{R_2} \xi q^{(o)} d\xi,$$
(S4c)

which is solved numerically for ξ_{int} . It is then used with (S4b) to obtain an expression for the velocity at the inner wall, given by

$$v(\xi_1) = \frac{d\xi_1}{dt} = \frac{1}{\xi_1} \left[\xi_{int} v(\xi_{int}) - \int_{\xi_1}^{\xi_{int}} \xi q^{(i)} d\xi \right],$$
(S4d)

which is again solved numerically for ξ_1 .

Elastic deformation. Integrating (2.12) and applying (2.13a) gives the radial stress for the inner layer

$$T_{rr}^{(i)} = \int_{r_1}^r \frac{1}{r'} \left(T_{\theta\theta}^{(i)} - T_{rr}^{(i)} \right) dr' - P_1, \qquad r_1 \le r \le r_{int},$$
(S5a)

and applying (2.13d) gives the radial stress for the outer layer

$$T_{rr}^{(o)} = T_{rr}^{(i)}(r_{int}) + \int_{r_{int}}^{r} \frac{1}{r'} \left(T_{\theta\theta}^{(o)} - T_{rr}^{(o)} \right) dr' - P_2, \qquad r_{int} \le r \le r_2.$$
(S5b)

Applying continuity of stress (2.13c) thus gives

$$P_1 - P_2 = \int_{r_1}^{r_{int}} \frac{1}{r} \left(T_{\theta\theta}^{(i)} - T_{rr}^{(i)} \right) dr + \int_{r_{int}}^{r_2} \frac{1}{r} \left(T_{\theta\theta}^{(o)} - T_{rr}^{(o)} \right) dr,$$
(S5c)

wherein r_1 and r_2 can be expressed in terms of r_{int} via (2.4), since ξ_1 and ξ_{int} are known from the solution of (S4), and (i) denotes variables computed in the inner layer and (o) those in the outer layer. Together with the radial and circumferential stress components of the Cauchy stress specified by (2.5) and (S3), (S5c) is therefore an algebraic equation in the unknown r_{int} . At each time step, a root finding algorithm (fzero.m), is used to solve the equilibrium equation (S5c) for r_{int} . All other variables can be evaluated once this is known.

Parameter	Definition	Inner layer	Outer layer	Units
$\mu _{t_0}$	Inflammatory factor, μ	0	0	${ m mg}~{ m mm}^{-3}$
$k _{t_0}$	Contractile agonist, \boldsymbol{k}	0	0	${ m mg}~{ m mm}^{-3}$
$arPsi_c _{t_0}$	Contractile ASMC volume fraction	0	0.20	
$\Phi_p _{t_0}$	Proliferating ASMC volume fraction	0	$1.50 \mathrm{x} 10^{-3}$	
$arPsi_e _{t_0}$	ECM volume fraction	0.30	$9.85 \text{x} 10^{-2}$	
R_1	Inner radius	1.800		mm
R_{int}	Interface radius	1.818		mm
R_2	Outer radius		2.340	mm

Table 1: Initial Conditions and Airway Geometry

Numerical techniques. Numerical solutions to the system of coupled PDEs, given by (2.26), with (2.18-2.25), were obtained via the method of lines as follows. A finite difference spatial discretisation, with upwinding applied to convective terms, was employed. For simplicity, we fixed with the number of nodes at 10 in the (thin) inner layer and 100 in the outer layer, noting that, as the airway grows, Δr is not constant¹. The resulting system, along with (S4), was time-stepped in MATLAB using an ODE solver (ode45.m or ode15s.m; the latter is used when inflammatory or agonist challenge frequency is very high resulting in a stiff system of equations), with the integrals evaluated using trapz.m. This method was applied separately to the inner and outer layers and solutions matched at r_{int} .

2 Model Parameters and Initial Conditions

Initial conditions for inflammatory factor, μ , contractile agonist concentration, k, and volume fractions, Φ_a , a = p, c, e, along with the initial geometry of the airway, are given in Table 1. Rate constants for the mass balance equations and material parameters, consistent between the two layers, are given in Table 2. Model parameters differing between the layers are given in Table 3.

3 Sensitivity Study

We performed a one-at-a-time sensitivity study by varying parameters a_{μ} , $c_{d\mu}$, a_k , c_{dk} , T_c , $a_{k\mu}$, and a_c (Fig. S1). For each parameter, simulations were performed for a range of 100 values, with inflammatory challenges (except for parameter a_k , in which the airways were challenged with contractile agonists) at a frequency of one per day for 50 days, followed by a resolution period. Change in inner radius, from the initial value ($R_1=1.8$ mm), at 5 days post final challenge was used to assess the results. The model is highly sensitive to a_{μ} and $c_{d\mu}$, as increased remodelling (represented by decreased inner radius) is associated with increasing magnitude (a_{μ}), decreasing clearance ($c_{d\mu}$) of inflammatory factor μ , with the former exhibiting a linear response above a certain threshold and the latter a nonlinear response. Moreover, the model is highly sensitive to contractile agonist magnitude (a_k) in the agonist-challenge simulations. Note that the curve for a_k in Fig. S1 does not pass through zero. The reason for this is that, at the default value of a_k and c_{dk} (Table 2), the simulations with contractile agonist challenges at a frequency of 1 per day over 50 days results in contraction into the lumen. A nonlinear decrease in radius is associated with decreasing clearance of contractile agonist concentration, k, with a strong threshold effect observed with decreasing c_{dk} . The model is less sensitive to this parameter than magnitude, clearance of μ (subject to inflammatory challenges).

¹ Remark: Initially, $\Delta r = 0.002mm$ in the inner layer and 0.005mm in the outer layer. For all times, $\Delta r < 0.2mm$, even in the extreme (unrealised) case in which only the airway inner layer grows into the lumen.

Parameter	Definition	Value	Units
Constants			
$egin{aligned} & ho_c^T \ & ho_p^T \ & ho_p^T \ & ho_f^T \ & ho_f^T \ & \Phi_w \end{aligned}$	Contractile ASMC density	1.050	${ m mg}~{ m mm}^{-3}$
$ ho_p^T$	Proliferative ASMC density	1.050	${ m mg}~{ m mm}^{-3}$
$ ho_e^T$	Extracellular matrix density	1.050	${ m mg}~{ m mm}^{-3}$
$ ho_f^T$	Fluid mass density	1.000	$\mathrm{mg}~\mathrm{mm}^{-3}$
$\check{\Phi_w}$	Fluid volume fraction	0.70	
Inflammatic	on and Agonist Rate Constants		
$\overline{a_{\mu}}$	Stimulus amplitude for inflammatory factor, μ	3	$\mathrm{mg} \mathrm{mm}^{-3} \mathrm{day}^{-1}$
$c_{d\mu}$	Decay rate of inflammatory factor, μ	5	day^{-1}
μ_1	First inflammatory threshold	1	$mg mm^{-3}$
μ_2	Second inflammatory threshold	2.5	${ m mg}~{ m mm}^{-3}$
a_k	Stimulus amplitude for contractile agonist, k	$4.64 \mathrm{x} 10^{-2}$	$mg mm^{-3} day^{-1}$
c_{dk}	Decay rate of contractile agonist, k	2	day^{-1}
$a_{k\mu}$	Inflammation-induced agonist release coefficient	0.001	day^{-1}
a_c	Contraction-induced agonist release coefficient	0.001	$\mathrm{mg} \mathrm{mm}^{-3} \mathrm{cmH}_{2}\mathrm{O}^{-1} \mathrm{day}^{-1}$
Event Para	-		
\overline{d}	Duration of inflammation/agonist administration	1/3	
σ	Event parameter	0.01	
ω	Inflammation, μ , or contractile agonist, k ,	1	day^{-1}
	challenge frequency		C C
T	Time scale	1000	days
Mechanical	Material Parameters		
$\overline{\eta_p}$	Proliferative ASMC passive isotropic stiffness	51.84	$\rm cm H_2 O$
η_c	Contractile ASMC passive isotropic stiffness	51.84	cmH_2O
$\overset{\prime c}{C_c}$	Contractile ASMC passive anisotropic stiffness	1.14×10^{-3}	cmH_2O
β_c	Contractile ASMC passive anisotropic exponential parameter	2.74	-
η_e	ECM passive isotropic stiffness	51.84	$\rm cm H_2 O$
C_e	ECM passive anisotropic stiffness	18.1	cmH_2O
β_e	ECM passive anisotropic summess ECM passive anisotropic exponential parameter	1.48	chilli 20
T_c	Agonist-induced active contraction parameter	1000	$\mathrm{cmH}_{2}\mathrm{O}$
λ_{act}	Collagen recruitment stretch	1	5 <u>.</u> 5
λ_{act} λ_z	Axial stretch ratio	1	
Θ	Fiber angle	0	radians
P_1	Lumen pressure	0	cmH_2O
P_1	External pressure	0	cmH_2O
- 4	problem	~	

Table 2: Default Model Parameters Consistent Between the Two Layers

Also, the model is not very sensitive to changes in ASMC responsiveness to contractile agonist (T_c) , inflammationinduced contractile agonist release $(a_{k\mu})$, and mechanical-stress induced contractile agonist release (a_c) , as each of these result in only small (nonlinear) changes in inner radius.

4 Volume Fractions

In order to compare results more directly from the simulations in Figs. 4 and 6, we plot the volume fractions of the airway wall constituents (proliferating, contractile ASMCs and ECM) as functions of the radius in Fig. S2. The left column depicts the constituent volume fractions taken at 3 separate days (increasing in time, moving down the column) from the simulation using the parameters corresponding to the circled point on the surfaces of Fig. 4a,b, while the right column depicts those corresponding to the circled point on the surfaces of Fig. 6a,b. The volume fractions of the constituents remain flat and only slightly increase during inflammation challenges (moving down

Parameter	Definition	Inner layer	Outer layer	Units
c_{p0}	Baseline cell proliferation rate constant	0	1/3	day^{-1}
c_{pc}	Proliferative to contractile ASMC switching rate constant	0	2/3	day^{-1}
c_{c0}	Basline (low) contractile to proliferative switching rate constant	0	2.50×10^{-3}	day^{-1}
c_{c1}	Medium contractile to proliferative switching rate constant	0	$5.0 \mathrm{x} 10^{-3}$	day^{-1}
c_{c2}	High contractile to proliferative switching rate constant	0	$5.0 \mathrm{x} 10^{-2}$	day^{-1}
c_a	Contractile cell apoptosis rate constant	0	$1.19 \mathrm{x} 10^{-2}$	day^{-1}
c_{de}	Baseline ECM degradation rate constant	0	9.70×10^{-3}	day^{-1}
c_{e0}	Baseline (low) ECM deposition rate constant	0	$1.0 \mathrm{x} 10^{-3}$	$\mathrm{mg} \mathrm{mm}^{-3} \mathrm{day}^{-1}$
c_{e1}	Medium ECM deposition rate constant	0	$1.0 \mathrm{x} 10^{-3}$	$\mathrm{mg} \mathrm{mm}^{-3} \mathrm{day}^{-1}$
c_{e2}	High ECM deposition rate constant	0	$1.0 \mathrm{x} 10^{-3}$	$\mathrm{mg} \mathrm{mm}^{-3} \mathrm{day}^{-1}$
c_{pe}	ECM deposition, via proliferative cells, rate constant	0	$1.0 \mathrm{x} 10^{-3}$	day^{-1}
c_p^f	Stress-induced cell proliferation rate constant	0	0	day^{-1}
c^f_{cp}	Stress-induced contractile to proliferative ASMC switching rate constant	0	$5.0 \text{x} 10^{-3}$	day^{-1}

Table 3: Default Model Parameters Differing Between the Two Layers

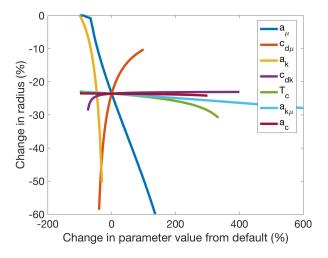


Fig. S1: Sensitivity Study. Change in inner radius, at 5 days post final challenge, from original radius $R_1=1.8$ mm, as a function of change in parameter from default value (Table 2). The airway was challenged every day for a 50 day period with inflammation challenges, except for the study varying a_k , in which contractile agonist challenges were used. The default value for a_k was chosen so that low frequency challenges led to non-trivial remodelling, but at higher frequencies used here (one per day for 50 days), growth/contraction into the lumen results with this default value.

the left column). The increase in proliferating ASMCs towards the outer wall of the airway is due to the tensile mechanical stress-induced increase in phenotype switching rate. Thus, the figures in the right column depict the local increase in proliferative, and associated decrease in contractile, ASMCs during phenotype switching. Also, the airway geometry shifts to the right from day 28 to day 32, as the contractile agonist gradually clears from the tissue and the airway relaxes.

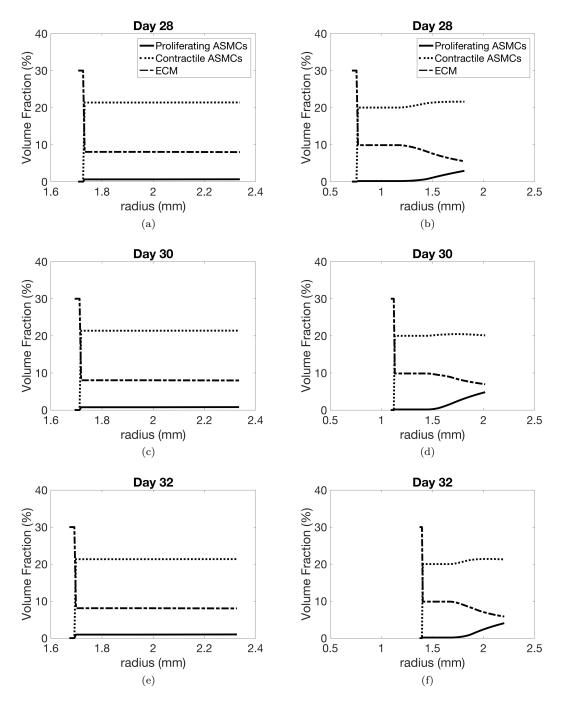


Fig. S2: Volume Fractions vs. Radius. Volume fractions of proliferating, contractile airway smooth muscle cells (ASMCs) and extracellular matrix (ECM) plotted as a function of radius taken at days 28, 30, and 32, corresponding to (left column) the circled point on the surfaces of Fig. 4a,b and (right column) the circled point on the surfaces of Fig. 6a,b. The inner radius shifts to the left more dramatically moving down the right column compared with the left column, as contractile agonist is cleared from the tissue following the challenge. Clearly, contractile agonist-induced deformation is dominant in the agonist-challenge simulations.

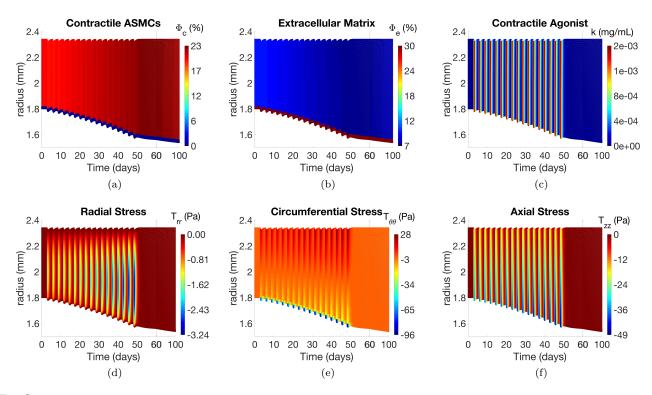


Fig. S3: Volume Fractions, Contractile Agonist Concentration, and Mechanical Stresses during Inflammatory Challenges. Illustrative results are evaluated at the circled point on the surface of Fig. 4a: volume fractions of (a) contractile ASMCs, (b) extracellular matrix, and concentration of (c) contractile agonist; Cauchy stresses in the (d) radial, (e) circumferential, and (f), (f) axial directions

5 Volume Fractions, Contractile Agonist Concentration, and Mechanical Stresses

The volume fractions, local contractile agonist concentrations, and mechanical stress distributions for the selected points (not already included) in Figs. 4 and 6 are depicted in Figs. S3 and S4, respectively. During inflammationonly challenges, the gradients of the constituents and agonists across the airway radius (Figs. S3a-c and 4c) are low compared to contractile agonist challenges (Figs. S4a-c and 6c), in which the local mechanotransduction-induced ASMC phenotype switching leads to local increases in ASM towards the outer wall (associated with regions on increased circumferential tensile stress), and thus relatively higher volume fractions of proliferating ASMCs and lower volume fractions of contractile ASMCs and ECM. For both inflammation (Fig. S3d-f) and agonist (Fig. S4d-f) challenges, radial stresses are compressive in the mid-wall and zero at the boundaries (thus matching the zero pressure boundary conditions), circumferential stresses are tensile in the outer potion of the wall and compressive in the inner portion, and axial stresses are compressive (due to incompressibility), with agonist challenges resulting in much higher stress magnitudes due to the active contraction.

6 Effect on Remodelling of Changes in Phenotype Switching Rate or Intrinsic Proliferation Rate Modulated by Mechanical Tensile or Compressive Stresses

Similar amounts of remodelling are observed for increases in both tensile and compressive stress-modulated phenotype switching rates, c_{cp}^{f} and decreasing agonist clearance rate, c_{dk} , with no clear threshold effect (Fig. S5a,b). For the same parameter ranges, agonist resolution times are also observed to be similar (note some simulation results are not plotted due to contraction/growth into the lumen during challenges). Moreover, agonist resolution time appears to be relatively independent of c_{cp}^{f} for both cases (Fig. S5c,d). For a selected parameter set (shown as circles on the surfaces in Figs. S5a–d), distributions of the proliferative ASMC volume fraction are significantly different in the two cases. Larger volume fractions are observed at the outer edge of the airway wall in the tensile stress-modulated case (Fig. S5e) and at the inner edge in the compressive stress-modulated case (Fig. S5f).

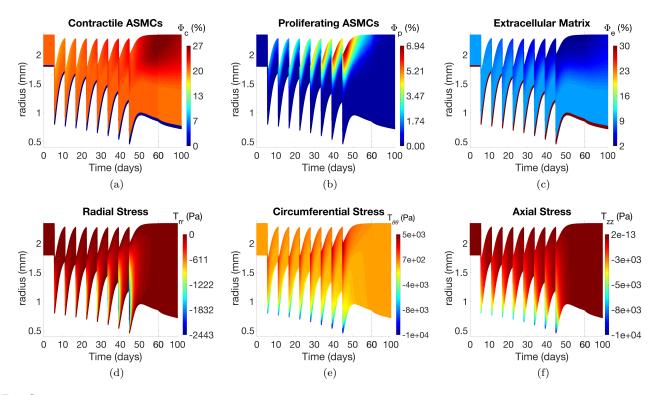


Fig. S4: Volume Fractions, Contractile Agonist Concentration, and Mechanical Stresses during Contractile Agonist Challenges. Illustrative results are evaluated at the circled point on the surface of Fig. 6a: volume fractions of (a) contractile, (b) proliferating ASMCs, and (c) extracellular matrix; Cauchy stresses in the (d) radial, (e) circumferential, and (f) axial directions

For our given initial conditions, both tensile and compressive stress-induced phenotype switching (c_{cp}^f) results in a greater amount of airway remodelling (Fig. S5a,b) than stress-induced increase in proliferation rate (c_p^f) ; Fig. S6a,b); again, note that some simulation results are not plotted due to contraction/growth into the lumen during challenges. Agonist retention is similar between the two cases (cf. Figs. S5c,d, S6c,d). Slightly less contraction is observed during challenges with increasing c_{cp}^f compared with increasing c_p^f . In the former case (Fig. S5e, S5f), contractile cells are lost due to phenotype switching, and in the latter case (Fig. S6e, S6f), the intrinsic proliferation rate of the current (lower) population of proliferating ASMCs is increased.

7 Comparison to Previous Modelling Results

Qualitatively, very similar results were obtained between the current study and our previous study (Chernyavsky et al (2014); Fig. S7). Severe remodelling in the former (red colour in Figs. S7a,b) corresponds to increased remodelling towards the lumen in the latter (red colour in Figs. S7c,d, respectively corresponding to the inward remodelling shown in Figs. 8a, 4a).

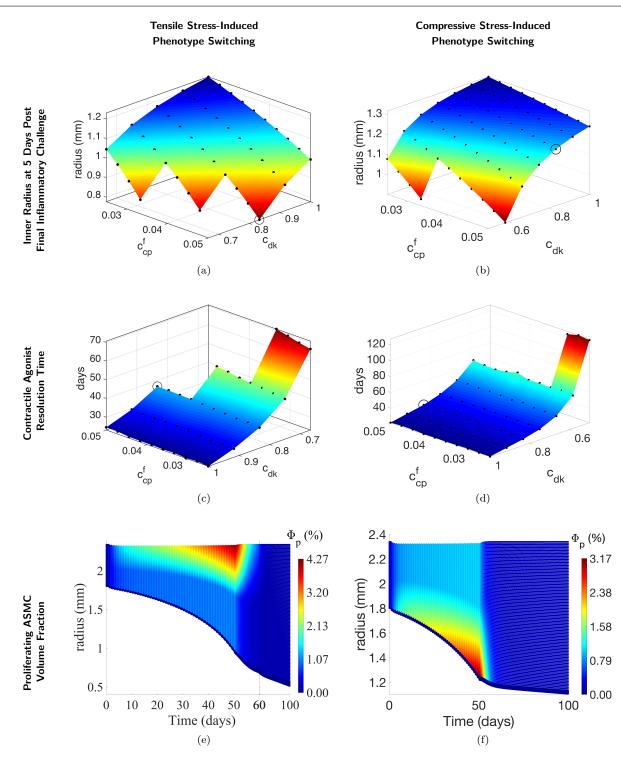


Fig. S5: Effect of phenotype switching rate modulated by tensile vs compressive stress: Variation in (a), (b) remodelled geometry $(1^{st}$ row) and (c), (d) agonist resolution rate (2^{nd} row) with selected parameter values of stress-induced phenotype switching (c_{cp}^f) and agonist resolution rate (c_{dk}) . The proliferating airway smooth muscle cell volume fraction (e), (f) is plotted as functions of radius and time for parameter value pairs indicated by the circled points on the surfaces.

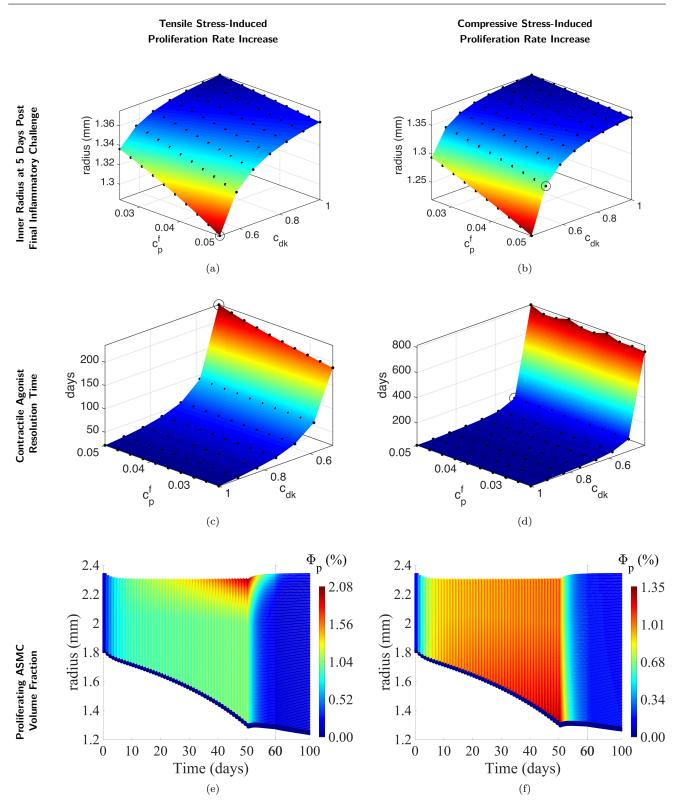


Fig. S6: Effect of proliferation rate modulated by tensile vs compressive stress: Variation in (a), (b) remodelled geometry (1^{st} row) and (c), (d) agonist resolution rate (2^{nd} row) with selected parameter values of stress-induced proliferation rate increase (c_p^f) and agonist resolution rate (c_{dk}) . The proliferating airway smooth muscle cell volume fraction (e), (f) is plotted as functions of radius and time for parameter value pairs indicated by the circled points on the surfaces.

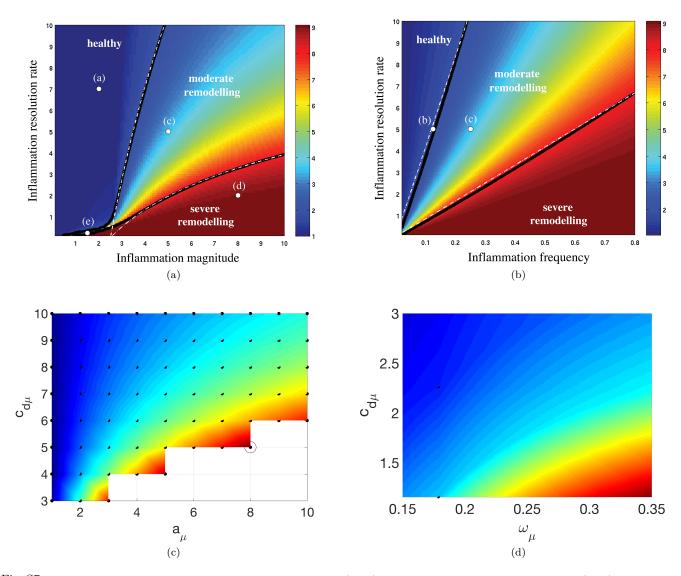


Fig. S7: Comparison of Current Model Results to Chernyavsky et al (2014). Top row: results from Chernyavsky et al (2014), showing fold-increase in ASM population size after 300 days (colour scale) as a function of the inflammation resolution rate and the (a) inflammation magnitude or (b) inflammation challenge frequency; Bottom row: results from current study, showing inner radius at 5 days post final inflammatory challenge (colour scale) as a function of the inflammation resolution rate and the (c) inflammation magnitude (rotated view of Fig. 8a) or (d) challenge frequency (rotated and zoomed view of Fig. 4a).

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