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# Characterization of the Coating and Tablet Core Roughness by Means of 3D Optical Coherence Tomography

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## ABSTRACT

This study demonstrates the use of optical coherence tomography (OCT) to simultaneously characterize the roughness of the tablet core and coating of pharmaceutical tablets. OCT is a high resolution non-destructive and contactless imaging methodology to characterize structural properties of solid dosage forms. Besides measuring the coating thickness, it also facilitates the analysis of the tablet core and coating roughness. An automated data evaluation algorithm extracts information about coating thickness, as well as tablet core and coating roughness. Samples removed periodically from a pan coating process were investigated, on the basis of thickness and profile maps of the tablet core and coating computed from about 480,000 depth measurements (i.e., 3D data) per sample. This data enables the calculation of the root mean square deviation, the skewness and the kurtosis of the assessed profiles. Analyzing these roughness parameters revealed that, for the given coating formulation, small valleys in the tablet core are filled with coating, whereas coarse features of the tablet core are still visible on the final film-coated tablet. Moreover, the impact of the tablet core roughness on the coating thickness is analyzed by correlating the tablet core profile and the coating thickness map. The presented measurement method and processing could be in the future transferred to in-line OCT measurements, to investigate core and coating roughness during the production of film-coated tablets.

**Keywords:** Optical coherence tomography, solid oral dosage form, coating, roughness, 3D thickness map

## 1. INTRODUCTION

Although tablet coating is a well-established unit operation in the pharmaceutical industry, the achievable quality of coating is still limited by the fact that it is a highly complex process, which depends on many parameters. Slight changes of the coating equipment and process parameters may impact the physicochemical properties of the film, and consequently, affect the coating quality. The key descriptors of coating quality, particularly for functional coatings, are film coating thickness and its uniformity. Another important parameter of the dosage form is the roughness of the tablet core and of the coated tablet. It is well known that the roughness of uncoated tablets affects friability (Riippi et al., 1998) and polymer adhesion (Felton, 2013; Rowe, 1978). Surface roughness is further related to the porosity (Bawuah et al., 2014; Rowe, 1978), and thus to the disintegration and dissolution behavior of the tablets. Moreover, the roughness of a film-coated tablet influences the gloss and permeability of the film. The roughness of the tablet core, as well as of the coated tablet, thus impact the dosage form's properties and its performance. Therefore, measuring the roughness of the uncoated and coated tablet will help to better understand the impact of changes to process parameters and modifications of the formulation on the performance of the solid dosage form.

Surface roughness was previously investigated using stylus instruments (Rowe, 1979; 1978), optical microscopy (Seitavuopio et al., 2003), laser profilometer (Seitavuopio et al., 2003), scanning electron microscopy (SEM) (Riippi et al., 1998; Seitavuopio et al., 2006), atomic force microscopy (AFM)

47 (Seitavuopio et al., 2003) and UV imaging (Klukkert et al., 2015). However, these techniques do not  
48 allow the characterization of the roughness of the uncoated, and of the coated, tablet simultaneously  
49 at the same position. The simultaneous measurement of the roughness of both interfaces enables the  
50 analysis of the impact of the tablet core roughness on the coating uniformity, as well as on the  
51 roughness of the film coated tablet. Moreover, most techniques are time-consuming and do not  
52 facilitate the measuring of a large number of tablets, which is required to calculate significant statistical  
53 parameters.

54 The most promising methods to study the roughness of tablet cores and film coatings are optical  
55 imaging methods, such as confocal laser scanning microscopy (CLSM) and optical coherence  
56 tomography (OCT). Ruotsalainen et al. (Ruotsalainen et al., 2003) used CLSM to study the tablet  
57 core/coating interface and the surface of the film-coated tablet. They investigated the effects of  
58 spraying air pressure and short-term storage on aqueous hydroxypropyl methylcellulose (HPMC)-  
59 coated tablets containing an auto-fluorescent agent in the coating solution in order to achieve a good  
60 contrast of the coating layer when using CLSM. Recently, we and other research groups have  
61 demonstrated how OCT can be applied to measure the coating thickness of tablets (Lin et al., 2015;  
62 Markl et al., 2015a; 2015b; Zeitler et al., 2007) and pellets, (Li et al., 2014; Markl et al., 2015c) as well  
63 as to study the roughness of uncoated tablets (Juuti et al., 2009). OCT is a high-resolution imaging  
64 methodology to produce cross-sectional images of film coatings, in a non-destructive and contactless  
65 manner. This modality allows the direct measurement of the coating thickness, based on the  
66 knowledge of the refractive index of the coating. The very high acquisition rate of OCT (up to MHz  
67 depth scan rates (Wieser et al., 2010)) renders this method a promising tool for the in-line monitoring  
68 of coating processes. This has been reported for the coating of tablets in a pan coater (Markl et al.,  
69 2015a; Lin et al., 2017) as well as the coating of pellets in a fluid-bed coater (Markl et al., 2015c).  
70 Different data processing procedures have been developed to rapidly analyze the OCT measurements  
71 and to determine the coating thickness at several positions of individual tablets (Markl et al., 2015b,  
72 Lin et al., 2015). These data yield significant statistics about the uniformity of the coating as it facilitates  
73 the analysis of the intra- and inter-tablet coating variability besides the average coating thickness.

74 This study shows, for the first time, how to analyze the topography of a tablet core and its film-coating  
75 at the same location using OCT in a 3D mode. Such an analysis cannot be performed with traditional  
76 surface profilometers as they are not capable of providing information about structures below the  
77 surface. We employed OCT to investigate the correlation between the uncoated and coated tablet, as  
78 well as the coating thickness. This was performed by analyzing 3D OCT data of 11 samples (each  
79 consisting of 6 tablets) from different stages of a lab-scale pan coating process.

## 80 **2. MATERIALS AND METHODS**

### 81 **2.1 Materials**

82 350 g of round bi-convex tablets were coated in a laboratory-scale pan coater (ProCepT, Zelzate,  
83 Belgium), equipped with a 1-L drum and a Schlick spray nozzle, with a 0.8 mm tip. The tablet cores  
84 consisted of 50 mg acetylsalicylic acid, lactose monohydrate, microcrystalline cellulose, highly  
85 dispersed silicone dioxide (SiO<sub>2</sub>), starch, talc, and triacetin. The tablet cores (n = 20) had an average  
86 tablet diameter of 7.14 mm, thickness of 3.75 mm, curvature radius of 7.56 mm, and weight of 149.7  
87 mg. The enteric coating was composed by 42.3% Eudragit L30 D-55, 1.2% triethyl citrate, 6.2% talc and  
88 50.3% water. Pan speed, spray rate, inlet air flow rate and inlet air temperature were kept constant  
89 throughout the entire coating process at 40 min<sup>-1</sup>, 1.40 g/min, 0.4 m<sup>3</sup>/h, and 42°C, respectively. The  
90 process ran for 88 minutes, until a total mass of 120 g of coating material was sprayed onto the tablets,  
91 yielding a total coating thickness of 51.2 ± 2.8 μm (the standard deviation corresponds to the inter-  
92 tablet coating variability of 6 samples). The coating thickness as a function of process time is provided  
93 in Figure S.1 in the supplementary information. Tablet samples (each sample consists of 6 tablets) were  
94 drawn every 8 min, yielding 11 samples in total. The samples are from the coating process (B01)  
95 presented in Markl et al. (Markl et al., 2015a), whereas all tablets were measured again with the 3D  
96 OCT setup.

## 97           2.2 Optical coherence tomography

98       In OCT an optical beam emitted by a broadband light source (i.e., high spatial but low temporal  
99       coherence) is focused onto the surface of the sample. The main part of the light is directly reflected by  
100       the surface of the sample. A substantial fraction of the light penetrates into the coating structure and  
101       is then reflected back by subsequent interfaces, separating two media with different indexes of  
102       refraction, i.e., the coating and the core material. Therefore, coating/tablet core interface is visible if  
103       the coating layer is (i) thicker than the resolution limit of the used system ( $> 10 \mu\text{m}$ ), (ii) the coating  
104       does not exhibit high scattering losses due to particles in a size range of the operating wavelength, and  
105       (iii) there is a change in refractive index between adjacent media (i.e., air/coating and coating/tablet  
106       core). Measuring the optical path length difference between the reflections of the coating surface and  
107       the coating/material core interface allows the determination of the coating thickness, based on the  
108       knowledge of the refractive index of the coating material.

109       The base OCT system presented previously in Markl et al., 2015a allows the use of two different probes,  
110       namely a 1D and 3D imaging probe. The latter was employed in this study in order to acquire 3D data  
111       of a sample of interest, in an off-line configuration. The light source operates at a central wavelength  
112       of 832 nm and has a spectral bandwidth of 75 nm, which provides a theoretical axial resolution of 4.1  
113        $\mu\text{m}$ . The 3D imaging probe allows the reconstruction of depth-resolved cross-sections, or volumes, by  
114       scanning the probing beam laterally across the sample, with the aid of galvanometer mirrors GM1 and  
115       GM2 (Cambridge Technologies), and sub-sequent acquisition of depth scans at successive lateral  
116       positions (see Figure 1). The light emerging from the fiber is split at a non-polarizing bulk beam splitter  
117       BS (splitting ratio 50/50, Thorlabs) into a reference and a probe beam. The probe beam is focused by  
118       an achromatic lens L1 (Thorlabs, focal length,  $f = 36 \text{ mm}$ ). This setup provides a theoretical lateral  
119       resolution of  $10 \mu\text{m}$  and a depth of focus of  $171 \mu\text{m}$ . The spectrometer consists of a fiber collimator FC  
120       (OZ Optics, diameter = 20 mm), a transmissive diffraction grating DG (Wasatch Photonics Inc., Logan,  
121       Utah, USA, 1200 lines/mm), an achromatic lens L3 (Thorlabs, focal length = 100 mm) and a line scan  
122       camera with a 2048 pixel CCD array (Atmel Aviiva,  $14 \times 28 \mu\text{m}^2$  pixel size, 12 bit resolution). The output  
123       voltage of each CCD pixel is proportional to the number of photons hitting an individual pixel,  
124       accumulated during the CCD exposure time of  $30 \mu\text{s}$ .

125       Single depth scans and cross-sections are labelled as A- and B-scans, respectively. Cross-sectional  
126       images are synthesized from successive A-scans. Moreover, three-dimensional volumetric data can be  
127       created by acquiring sequential B-scans. Throughout this study we analyzed only 3D OCT data  
128       consisting of 512 B-scans, which covers a volume of  $3.12 \times 3.12 \times 1.6 \text{ mm}^3$ ; each 2D image has a  
129       dimension of  $1024 \times 1024$  ( $3.12 \times 1.6 \text{ mm}^2$ ). The total acquisition time per volume lasts for about 1  
130       minute.

131       An automated data evaluation algorithm extracts information about coating thickness, as well as tablet  
132       core and coating roughness. This analysis can be carried out either on the basis of cross-sectional  
133       images or by using 3D data of the samples. The focus in this study is the analysis of 3D images of the  
134       samples removed periodically from a pan coating process. A thickness map and profile maps of the  
135       tablet core and coating are computed from about 480,000 depth measurements per sample. This data  
136       enables, among others, the calculation of statistical roughness parameters of the assessed profiles.

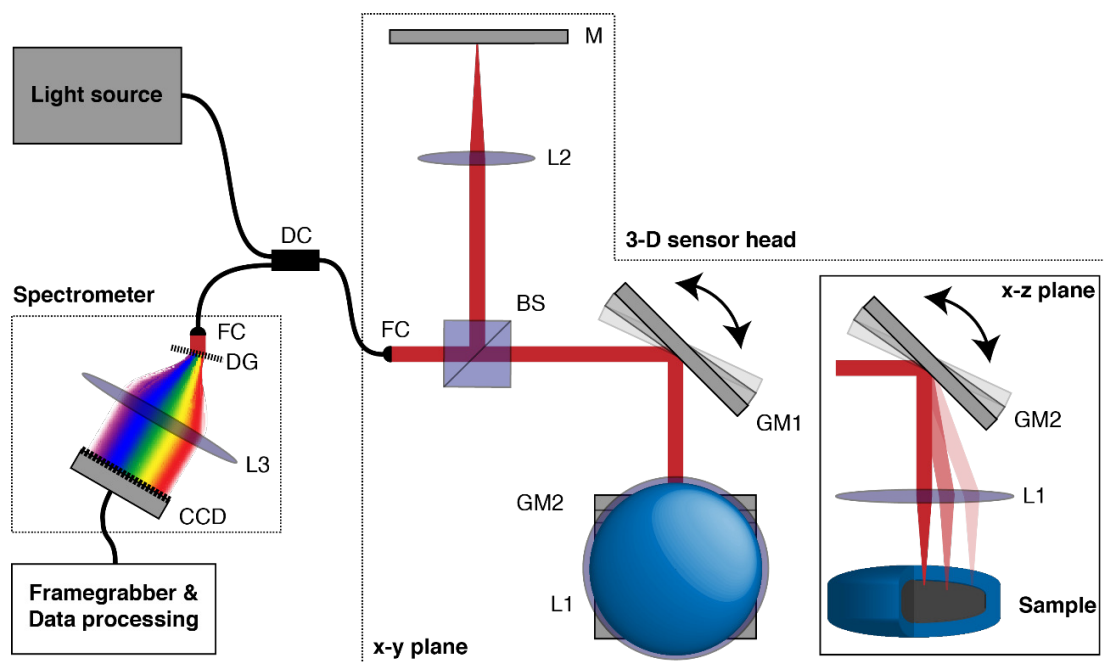


Figure 1: Schematic of OCT system for a 3D and 1D sensor head. DC – directional coupler, FF – fiber focuser, BS – beam splitter, M – mirror, FC – fiber coupler, DG – diffraction grating, Lx – lens, CCD – charged coupled device, GMx – galvanometer mirror. This schematic was modified from Markl et al., 2015a.

137

138

### 2.3 Roughness Analysis

139 A surface profile is in general defined as the result of an intersection between the surface and a defined  
 140 plane (Figure 2). In the case of OCT, this plane is a B-scan, which was acquired perpendicular to the  
 141 tablet face. The data evaluation procedure developed for the coating thickness analysis of 2D OCT  
 142 images was applied on the 3D volume data. This algorithm was presented in Markl et al. and consists  
 143 of four stages: (1) converting the raw spectra to image data by applying a non-uniform Fourier  
 144 transform (Markl et al., 2015b), (2) detecting the air/coating and coating/core interfaces, (3) correcting  
 145 the coating/core interface from distortions induced by the refraction of the beam on the air/coating  
 146 interface, and (4) determining the coating thickness. The application of the algorithm on each B-scan  
 147 of the 3D data allows the generation of a coating thickness map. Moreover, these data facilitate the  
 148 determination of coating and core profiles from the detected coating interfaces. The coating and core  
 149 profiles represent the deviations of the air/coating and coating/core interfaces from their respective  
 150 mean lines. The mean lines of both interfaces are assumed to follow a circle due to the bi-convex shape  
 151 of the tablets. Consequently, analyzing the roughness of bi-convex tablets requires the determination  
 152 of the deviations of the actual surface from a circle with a specified radius and center. A circle was  
 153 therefore fitted in each detected interface and each point on the interface was represented by a polar  
 154 coordinate, as schematically shown in Figure 2 for the air/coating interface. The radius of the fitted  
 155 circle was then subtracted from the radial coordinate, yielding the coating and core profiles.

156 The calculated deviation in height of the interfaces from the fitted circle is the surface roughness of  
 157 the interface. Roughness is typically expressed by statistical parameters, as defined in international  
 158 standards (e.g., DIN EN ISO 4287). One of the most common descriptors is the root mean squared  
 159 deviation, which can be expressed as

$$Rq = \sqrt{\frac{1}{N} \sum_{i=1}^N y_i^2} \quad (2.1)$$

160 with  $y_i$  as the surface height at measurement position  $i$  (see Figure 2) and  $N$  as the total number of  
 161 measurements. Other statistical parameters are skewness ( $Rsk$ ) and kurtosis ( $Rku$ ), which are defined  
 162 as

$$Rsk = \frac{1}{Rq^3 N} \sum_{i=1}^N y_i^3, \quad (2.2)$$

$$Rku = \frac{1}{Rq^4 N} \sum_{i=1}^N y_i^4. \quad (2.3)$$

163 Skewness measures the profile symmetry about the mean line and kurtosis is a descriptor of the  
 164 sharpness of the profile. A negative  $Rsk$  represents a surface which mainly consists of valleys, whereas  
 165 a positive value indicates that the surface is predominantly peaks. The kurtosis is a measure for the  
 166 sharpness of the profile, where a spiky surface will have a high kurtosis value.

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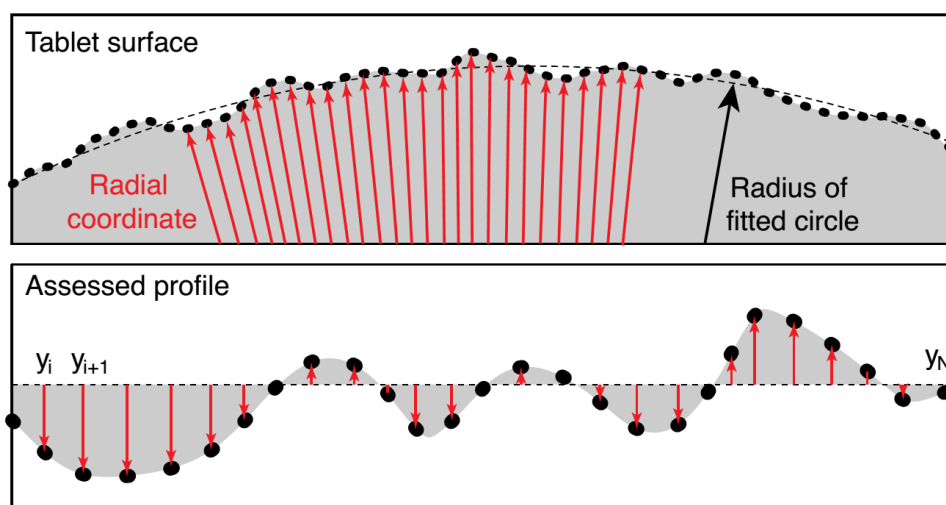


Figure 2: Schematic of the coating profile generation from the detected air/coating interface.  $y_i$  is the height of the surface profile at position  $i$  for a total of  $N$  measurements. Each point on the tablet surface is represented by a radial coordinate. The profile is assessed by subtracting the radius of the fitted circle from the radial coordinate.

168

## 169 2.4 Validation of OCT profile measurements

170 The OCT roughness analysis was validated by roughness maps generated by a contact profilometer  
 171 (Veeco DEKTAK 150), using a  $0.9 \mu\text{m}$  radius tip which can provide a vertical resolution of up to  $1 \text{ \AA}$ . The  
 172 contact profilometry measurements were performed on the tablet surface covering a range of  $3 \times 3$   
 173  $\text{mm}^2$  ( $250 \times 3000 \text{ px}$ ). The acquisition time per profile map was about 1 hour.

### 174 3. Results and discussion

#### 175 3.1 Comparison of OCT and contact profilometry

176 Figure 3 shows 2D roughness maps of one film-coated tablet, by means of contact profilometry and  
 177 OCT. Both measurements are in very good agreement, which is also indicated by the statistical  
 178 roughness parameters listed in Table 1 and by the frequency distribution in Figure 4. Slight deviations  
 179 between the profilometer and OCT measurements are due to the different instrument settings (i.e.,  
 180 scanning range, vertical and horizontal resolution) and due to a slight rotation of the tablet between  
 181 the two measurements. Moreover, the OCT data suffers from minor distortions which are mainly due  
 182 to the so-called fan distortion, which is related to the rastering of the surfaces using optical scanners  
 183 (e.g. galvanometer mirrors). This effect curves the OCT image deeper and it is stronger the farther  
 184 away from the center. Fan distortion can be corrected by a three-dimensional distortion correction  
 185 algorithm as proposed by Ortiz et al., 2010.

186 Table 1: Statistical roughness parameters from contact  
 187 profilometry and OCT of the same tablet (sample from  
 process time 88 mins). The data is shown in Figure 3.

	Contact profilometry	OCT
$Rq$ $\mu\text{m}$	3.98	4.09
$Rsk$ -	-0.23	-0.23
$Rku$ -	3.95	4.32

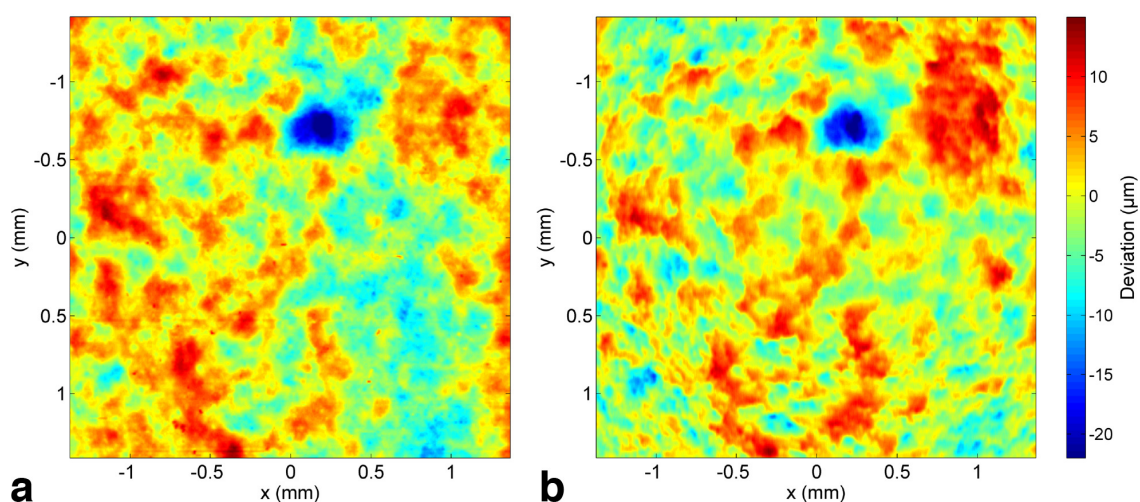


Figure 3: 2D roughness maps of a final film-coated tablet at the same position using (a) contact profilometry and (b) 3D OCT. The color bar is valid for both figures. The statistical roughness parameters of both measurements are given in Table 1.

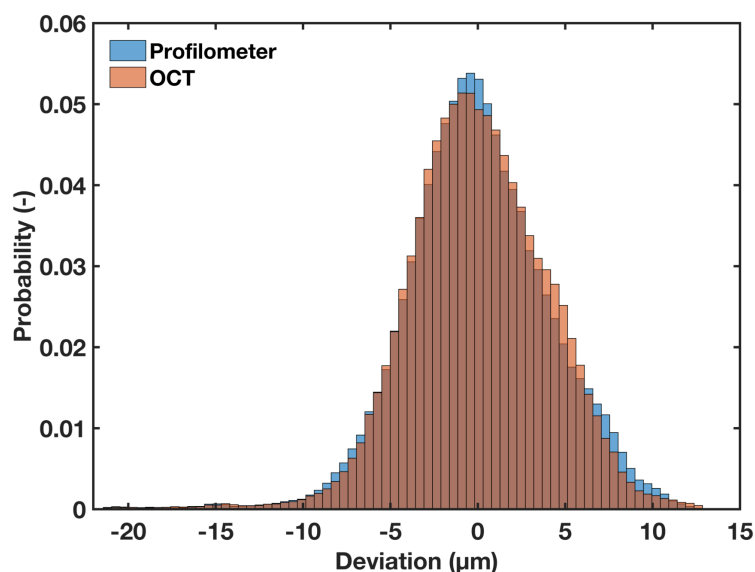


Figure 4: Frequency distributions of the roughness measurements using OCT and the profilometer. The frequency distributions were calculated from the 2D roughness maps as depicted in Figure 3.

194

### 195 **3.2 Correlation between coating profile, tablet core profile and coating thickness**

196 In the following we focus on the results from the OCT measurements, allowing the measurement of a  
197 much larger number of tablets due to the high acquisition rate, as well as due to the advantage of  
198 measuring the coating and the tablet core profile simultaneously (Figure 5). Further results are shown  
199 in Figure S.2 in the supplementary information. Comparing the core and the coating profiles reveals  
200 that small valleys of the tablet core profile are filled with coating. However, larger valleys and peaks in  
201 the core are still present in the coating.



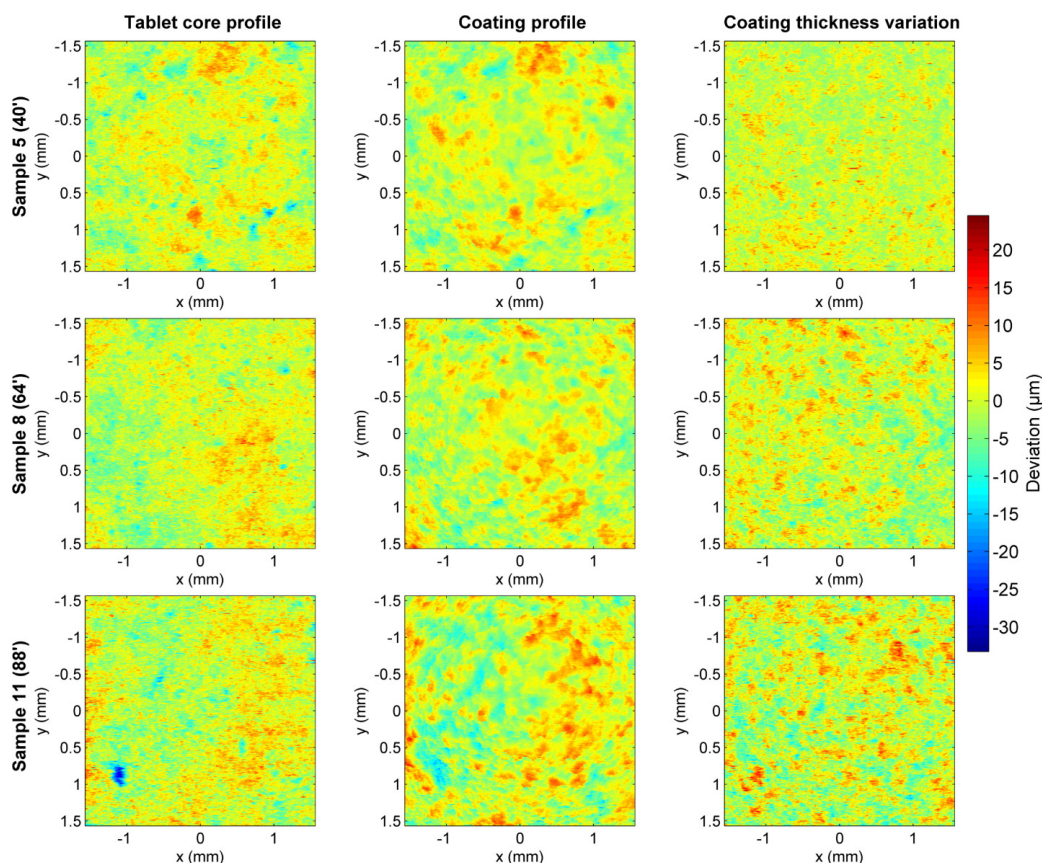


Figure 5: Tablet core and coating profiles, as well as coating thickness variations, of three tablets from different stages of the coating process. Each row corresponds to the same OCT measurement. The dimensions of each map are  $3.12 \times 3.12 \text{ mm}^2$  (512 x 1024 pixels).

202

203 A more detailed investigation of the relation between the core profile, coating profile and the coating  
 204 thickness can be performed by calculating correlation coefficients (Figure 6). As expected, a weak  
 205 linear correlation (coefficient close to 0) at the early stages of the coating process can be observed for  
 206 the core profile/coating thickness. This is also true for the coating profile and coating thickness. On the  
 207 contrary, the coating profile and the core profile are highly correlated, i.e. both profiles are almost  
 208 identical, as the coating is still very thin and thus below the resolution limit of OCT at this stage of the  
 209 process. The most significant changes of the coefficients occur in the first half of the coating process  
 210 ( $< 48 \text{ min}$ ), where the average coating thickness is  $< 28 \mu\text{m}$ . The correlation coefficient between the  
 211 coating and core profile approaches 0.5, which evidences that the final coating profile still represents  
 212 features from the original core profile. The negative correlation coefficient of the core profile and  
 213 coating thickness variation reflects a negative linear dependence between these two variables, which  
 214 indicates that a valley or a peak in the core profile causes a larger or smaller coating thickness,  
 215 respectively.

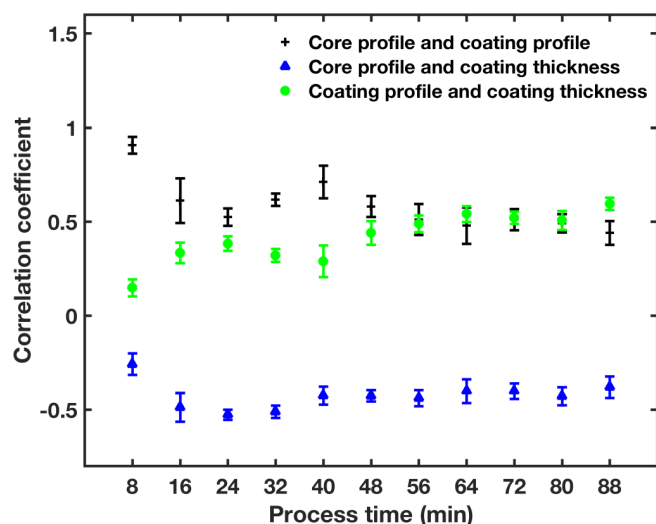


Figure 6: Correlation coefficients between core profile, coating profile and thickness variation maps depending on the process time. Each data point is the average correlation coefficient of 6 tablets and the error bar corresponds to its standard deviation. The size of each map used for the calculation of the correlation coefficients were  $3.12 \times 3.12 \text{ mm}^2$  ( $512 \times 1024$  pixels).

216

217

### 3.3 Statistical roughness parameters

218 The correlation of the different profiles can be further analyzed on the basis of the statistical roughness  
 219 parameters ( $Rq$ ,  $Rsk$  and  $Rku$ ). The root mean square deviation for the coating and the core profile is  
 220 illustrated in Figure 7a.  $Rq$  deviates at the beginning of the process ( $< 24$  min) from the values at the  
 221 end of the process, even though the roughness of the tablet cores should be similar throughout all  
 222 measurements. We want to remind the reader at this point that tablets were drawn from the process  
 223 at each stage for the analysis and they were not returned to the process. Although the tablet cores are  
 224 from the same batch, the roughness of the tablet cores clearly varies as indicated by the standard  
 225 deviation of the tablet core  $Rq$  as well as by the difference in average  $Rq$  between each process stage.  
 226 The coating roughness is constant towards the end of the process in contrast to the tablet core  
 227 roughness, which indicates that the coating process compensates, to a certain extent, the roughness  
 228 variations of the tablet cores. Moreover, the timely deviation of the tablet core  $Rq$  is primarily due to  
 229 the thin coating layer ( $15 \mu\text{m}$  at 24 min) at the beginning of the process, which cannot be accurately  
 230 resolved by the OCT system in use, causing a misdetection of the tablet core interface. The large  
 231 standard deviation at process time 40 min is due to a defect, which is discussed below on the basis of  
 232 the kurtosis.

233 However, the roughness of the tablet at process times  $< 48$  min is higher than that of the coating  
 234 surface, as the coating droplets preferentially fill in irregularities in the tablet core which causes a  
 235 smoother surface (Figure 7). On the contrary, the coating is slightly rougher than the core towards the  
 236 end of the process. The roughness of the coating surface strongly depends on the coating application  
 237 conditions, as was shown by Twitchell et al., 1995. The authors stated, on the basis of light section  
 238 microscope measurements, that increasing the spray gun-to-bed distance, changing the spray shape  
 239 from a narrow cone to a wide flat spray or decreasing the atomizing air pressure produce rougher  
 240 surfaces.

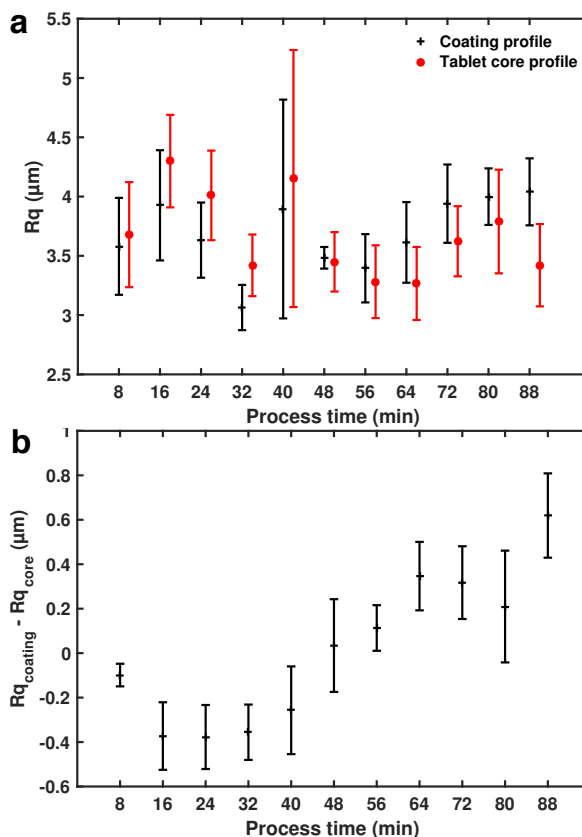


Figure 7: Analysis of the root mean square deviation as a function of process time. (a) Average  $Rq \pm$  standard deviation (errorbar) for each profile. The process time of the tablet core profile was shifted by 2 min in order to enhance the visibility of all data points. (b) The average and standard deviation values are calculated from the differences between  $Rq$  of the coating and the core profile of each tablet.

241

242 The roughness difference between coating and core profile can also be characterized by the skewness  
 243 and kurtosis of both profiles (Figure 8). Similar to the changes in  $Rq$ , we also observe a change in  $Rsk$   
 244 and in  $Rku$ , at the middle of the process. A smoother surface of the coated tablet is also supported by  
 245 the kurtosis values. We would like to remind the reader at this point that kurtosis is a measure for  
 246 sharpness and a spiky surface will have a high kurtosis value. The kurtosis difference, as shown in Figure  
 247 8b, thus highlights that the tablet surface is smoother (less spiky surface) after coating ( $Rku_{\text{coating}} <$   
 248  $Rku_{\text{core}}$ ). However, it may be preferable to have a rough tablet core surface, which would provide  
 249 greater interfacial contact between coating solution and tablet. A rougher surface, and thus a larger  
 250 surface area, causes stronger adhesion bonds between the tablet and the film (Nadkarni et al., 1975).

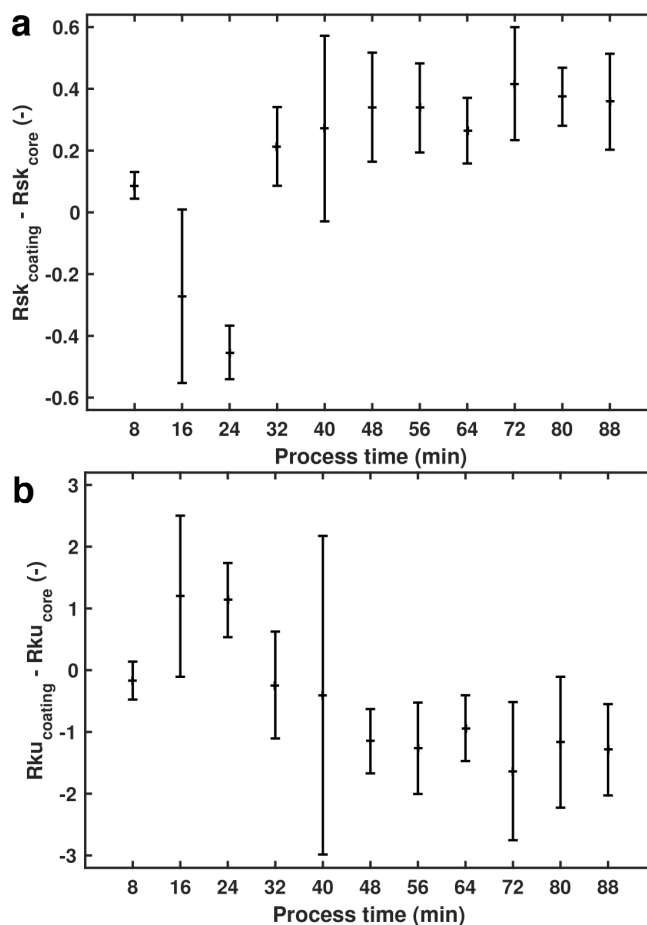


Figure 8: Difference in (a) skewness and (b) kurtosis between coating and core profile.

251

252 Figure 9 depicts the skewness of individual tablets drawn from the process at 24 min and 88 min  
 253 (process end). The skewness of the tablet core is larger at the beginning of the process than that of the  
 254 coating, whereas the absolute value of the tablet core skewness is closer to 0 (see data of process time  
 255 24 min in Figure 9). In contrast to the beginning of the process, the data follows a normal distribution  
 256 at the end of the process and is thus more symmetrical (i.e. skewness value is closer to 0). Therefore,  
 257 at the early stages of the process the coating negatively impacts the surface symmetry by forming  
 258 additional valleys ( $Rsk_{\text{coating}} < Rsk_{\text{core}} < 0$ ). The coating positively impacts the roughness symmetry  
 259 at the end of the coating process, as indicated by the skewness of the coating, which is closer to 0 than  
 260 that of the core profile.

261 The large standard deviation at process time 40 min is due to a defect in the tablet core, as illustrated  
 262 in Figure 10. Since the tablets are not the same for different process stages, this defect can only be  
 263 observed in the results from one tablet drawn from the process at 40 min. The tablet with this defect  
 264 is also an outlier in the  $Rsk$  and in the  $Rq$  analysis. However, the kurtosis is highly sensitive to such  
 265 local and small defects, which could have a major impact on the performance of this tablet. It can be  
 266 clearly observed, by comparing the tablet core and coating profiles, that the defect is in the tablet core.  
 267 The core profile has a higher value than the coating profile, meaning that negative spikes are filled with  
 268 coating. However,  $Rq$  of the coating and of the core (Figure 7) showed that the final coated surface is  
 269 in general rougher than the surface of the tablet core, but it is more symmetric and less spiky than the  
 270 original surface, as indicated by  $Rsk$  and  $Rku$ .

271 Such data can be used to gain more insight into the impact of the core roughness on the overall coating  
 272 uniformity. In particular, analyzing how closely the coated tablet surface follows the uncoated tablet  
 273 surface strongly depends on the process conditions. It is thus of great interest to have a fast and non-

274 destructive tool, such as OCT, to investigate the roughness of the tablet core and coating, on the basis  
 275 of statistical roughness parameters.

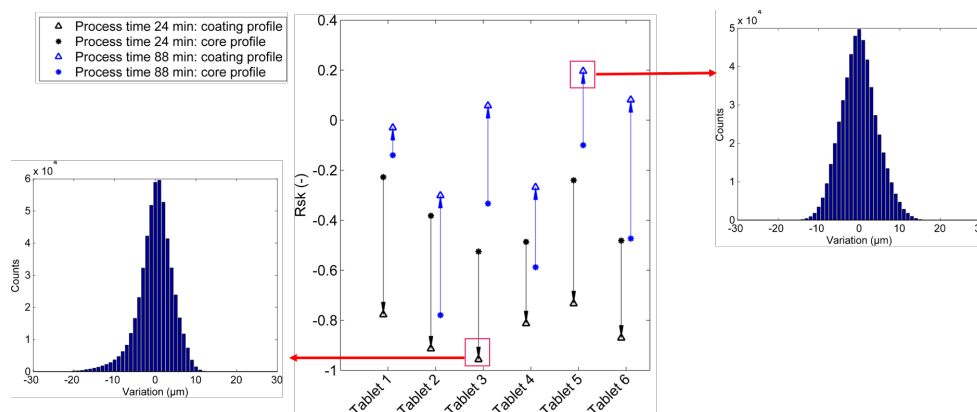


Figure 9: Skewness of six tablets which were randomly drawn from the process after 24 min (black) and after 88 min (blue). The arrows point from the core to the coating value of the same tablet.

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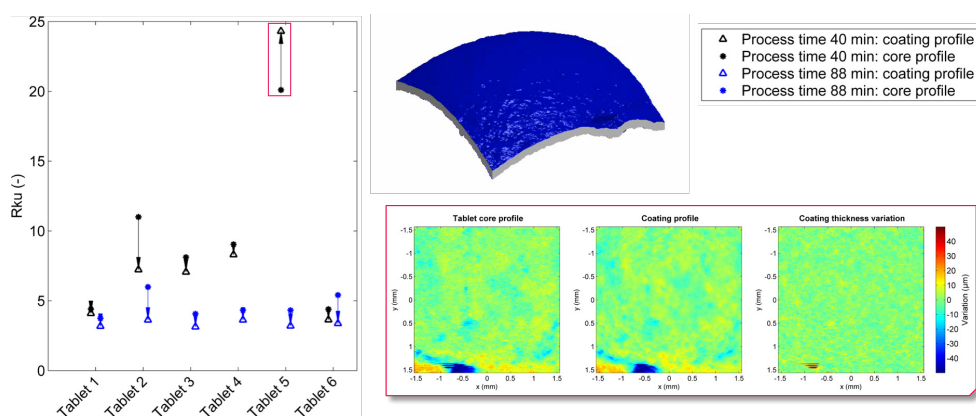


Figure 10: Analysis of a defect in the tablet core and the coating surface. Left figure: Kurtosis of 6 tablets randomly drawn from the coating process after 40 min and at the process completion (88 min). The 3D rendering, as well as the tablet core profile, coating profile and coating thickness variation are data from the tablet highlighted in the red square in the left figure. The arrows point from the core to the coating value of the same tablet.

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#### 4. Conclusion

281 This study reports how the surface roughness evolves during a tablet coating process, by comparing  
 282 tablet core profile and coating profile using 3D OCT measurements of a part of a tablet face. The data  
 283 reveal that small valleys are filled with coating, whereas coarse features of the tablet core are visible  
 284 on the final film-coated tablet. This clearly affects the coating uniformity, as observed in the correlation  
 285 between the coating thickness variation and the core profile. In addition, the presented concept could  
 286 be used to detect defects and irregularities in the tablet core, as well as in the coating surface, with  
 287 one single measurement. Such a detailed investigation cannot be performed with a contact  
 288 profilometer, which only provides data on the final dosage form surface. In this study we focused on  
 289 investigating the tablet faces and the results may vary for the tablet band or the surface close to the

290 edges as it is well known that the coating thickness differs between the tablets faces, the edges and  
291 the tablet band. OCT is capable of measuring the tablet band, but it may provide inaccurate  
292 measurements of the coating close to the edges.

293 Moreover, the presented concept could be further transferred to in-line OCT measurements (Markl et  
294 al., 2015a), allowing the investigation of core and coating roughness during production. Specifically,  
295 for functional and active coatings, slight changes of the coating equipment and process parameters  
296 may impact the physicochemical properties of the film, and may thus affect the coating quality. The  
297 applicability of OCT to measure functional or active coatings primarily depends on the used coating  
298 formulation, which may cause strong scattering losses leading to a reduced penetration depth and  
299 limiting the maximum detectable coating thickness.

300 However, monitoring and controlling coating quality is of great importance to prevent output risks,  
301 including batch reprocessing, batch reject and product recall. Characterizing coating properties such  
302 as coating thickness, coating uniformity as well as roughness is therefore critical for the purpose of  
303 quality control and quality assurance.

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