

---

**CSL** *COORDINATED SCIENCE LABORATORY*

**THE MIXED BOUNDARY-INITIAL  
VALVE PROBLEM FOR  
VLASOV EQUATION**

KENNETH EVANS, JR

**UNIVERSITY OF ILLINOIS - URBANA, ILLINOIS**

THE MIXED BOUNDARY-INITIAL VALUE PROBLEM  
FOR THE VLASOV EQUATION

by  
Kenneth Evans, Jr.

This work was supported in whole by the Joint Services Electronics Program  
(U.S. Army, U.S. Navy & U.S. Air Force) under Contract DAAB 07-67-C-0199.

Reproduction in whole or in part is permitted for any purpose of the United  
States Government.

This document has been approved for public release and sale; its distribution  
is unlimited.

THE MIXED BOUNDARY-INITIAL VALUE PROBLEM  
FOR THE VLASOV EQUATION

Kenneth Evans, Jr.

Coordinated Science Laboratory  
University of Illinois  
Urbana, Illinois

ABSTRACT

The mixed boundary initial value problem for the Vlasov equation is treated by double Laplace transformation. It is found that certain relations must be satisfied by the boundary and initial values in order to have a well-defined problem. The case of a cold beam in a cold plasma is treated as a simple example. An approach to the problem via discrete velocities is treated in an appendix.



## INTRODUCTION

In this paper the combined boundary-initial value problem for the linearized Vlasov equation will be treated. The method used, double Laplace transformation, is naturally suited to such a problem. A similar treatment for systems of linear, partial differential equations has already been given,<sup>1,2</sup> and will be referred to as I. In plasma physics the treatment I is applicable to the hydrodynamic approximation, which consists of the linearized, lower-order, moment equations of the Vlasov equation, along with Maxwell's equations.<sup>3</sup> Although the validity of this approximation is not well established, it is often used because of its simplicity (relative to more rigorous formulations) when there is any hope it might apply. The Vlasov equation, on the other hand, is on better footing as the lowest order of the BBGKY hierarchy.<sup>4</sup> The present paper is an extension of the ideas of I to the Vlasov equation.

The classic treatment of the solutions to the Vlasov equation is that given by Landau<sup>5</sup> and later refined by Jackson.<sup>6</sup> In the first part of Landau's paper the Vlasov equation is treated as an initial value problem by treating each spatial Fourier component separately and Laplace transforming in the time. This is perhaps the most common treatment of the equation. In the second part of the paper the equation is treated as a boundary value problem by treating each temporal Fourier component separately, then obtaining an integral equation and an asymptotic expansion. In the treatment given in this paper, that is, for the mixed boundary-initial value problem, Laplace transformation is made in both the spatial and temporal variables. This treatment is most appropriate for initial disturbances in bounded systems, for example, the beam-plasma system, where there is a natural boundary where the beam enters the plasma.

### FORMALISM

The equations to be considered in this paper are the Vlasov equation for an electron plasma in a fixed positive ion background and Maxwell's equations for the self-consistent electric field. The magnetic field will be neglected, and the one-dimensional, linearized version of these equations will be used. The equations are:

$$\frac{\partial f}{\partial t} + v \frac{\partial f}{\partial x} - \frac{e}{m} E \frac{df_0}{dv} = 0 \quad (1)$$

$$\frac{\partial E}{\partial t} - 4\pi n_0 e \int v f dv = 0 \quad (2)$$

$$\frac{\partial E}{\partial x} + 4\pi n_0 e \int f dv = 0, \quad (3)$$

where  $f_0 = f_0(v)$  is the unperturbed distribution function,  $f = f(x, t, v)$  is the perturbed distribution function,  $E = E(x, t)$  is the perturbed electric field, and  $n_0$  is the unperturbed density. The electrons have mass  $m$  and charge  $(-e)$ .

It can be seen immediately that there is a relation that must be satisfied by the initial conditions:

$$\frac{\partial E(x, 0)}{\partial x} + 4\pi n_0 e \int f(x, 0, v') dv' = 0 \quad (4)$$

This relation is analogous to the relation arising in I as a result of characteristics lying along the line  $t = 0$ . Similarly, there are two relations which must be satisfied by the boundary conditions:

$$\frac{\partial E(0, t)}{\partial t} - 4\pi n_0 e \int v' f(0, t, v') dv' = 0 \quad (5)$$

$$\frac{e}{m} E(0, t) = \left[ \frac{\partial f(0, t)}{\partial t} / \frac{\partial f_0}{\partial v} \right]_{v=0} \quad (6)$$

These are analogous to relations arising in I as a result of characteristics

lying on the line  $x = 0$ . Relations (4-6) are restrictions on the possible choices of boundary and initial values.

As has been stated above, the equations will be Laplace transformed in both  $x$  and  $t$ . Only solutions in the region  $x \geq 0$  and  $t \geq 0$  will be considered. The transforms will be defined as follows:

$$\begin{bmatrix} f(p,q,v) \\ E(p,q) \end{bmatrix} = \int_0^\infty dt \int_0^\infty dx e^{-pt - qx} \begin{bmatrix} f(x,t,v) \\ E(x,t) \end{bmatrix} \quad (7)$$

$$\begin{bmatrix} f^I(p,v) \\ E^I(p) \end{bmatrix} = \int_0^\infty dt e^{-pt} \begin{bmatrix} f(0,t,v) \\ E(0,t) \end{bmatrix} \quad (8)$$

$$\begin{bmatrix} f^{II}(q,v) \\ E^{II}(q) \end{bmatrix} = \int_0^\infty dx e^{-qx} \begin{bmatrix} f(x,0,v) \\ E(x,0) \end{bmatrix} \quad (9)$$

The inverses are given by:<sup>7</sup>

$$\begin{bmatrix} f(x,t,v) \\ E(x,t) \end{bmatrix} = \frac{1}{(2\pi i)^2} \int_{C_p} dp \int_{C_q} dq e^{pt + qx} \begin{bmatrix} f(p,q,v) \\ E(p,q) \end{bmatrix} \quad (10)$$

$$\begin{bmatrix} f(0,t,v) \\ E(0,t) \end{bmatrix} = \frac{1}{2\pi i} \int_{C_p} dp e^{pt} \begin{bmatrix} f^I(p,v) \\ E^I(p) \end{bmatrix} \quad (11)$$

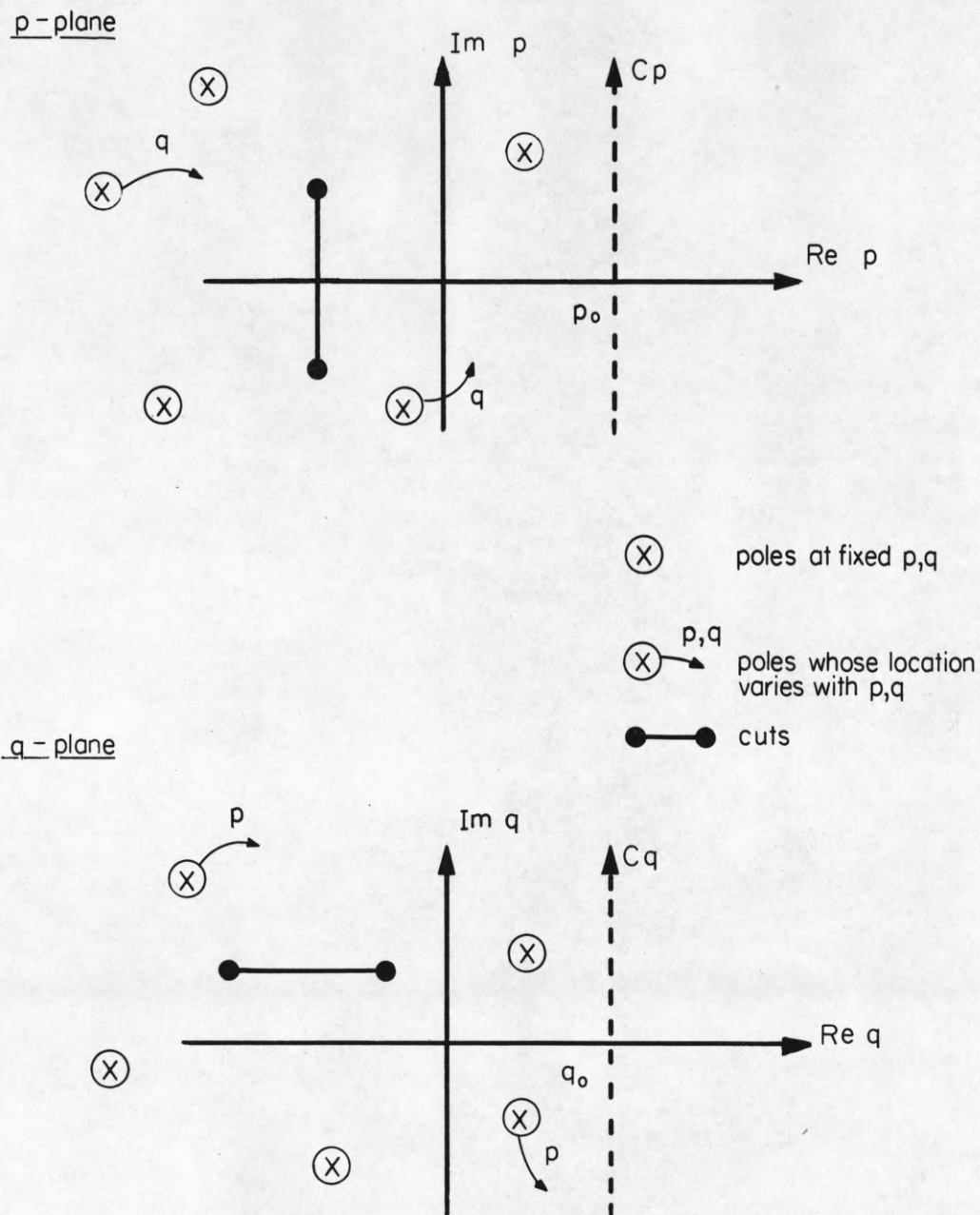
$$\begin{bmatrix} f(x,0,v) \\ E(x,0) \end{bmatrix} = \frac{1}{2\pi i} \int_{C_q} dq e^{qx} \begin{bmatrix} f^{II}(q,v) \\ E^{II}(q) \end{bmatrix} \quad (12)$$

The contours  $C_p$  and  $C_q$  are straight lines  $p = p_0 + ip_i$  and  $q = q_0 + iq_i$ , where  $p_i$  and  $q_i$  vary from  $-\infty$  to  $+\infty$ , and  $p_0$  and  $q_0$  are chosen so that the contours lie to the right of all singularities in the  $p$  and  $q$  planes respectively.

These contours are shown in Fig. 1.

To find the Laplace transformed solution to Eqs. (1-3), the equations are multiplied by  $\exp(-pt - qx)$  and integrated on  $x$  and  $t$  from 0 to  $\infty$ . After integrating by parts, the equations become:





PR-690

Figure 1. Typical singularities and contours of integration for inversion of Laplace transforms.

$$(p + vq)f(p, q, v) - \frac{e}{m} \frac{df_0}{dv} E(p, q) = f^{II}(q, v) + vf^I(p, v) \quad (13)$$

$$pE(p, q) - 4\pi n_0 e \int v' f(p, q, v') dv' = E^{II}(q) \quad (14)$$

and:

$$pE^I(p) - 4\pi n_0 e \int v' f^I(p, v') dv' = E(0, 0) \quad (15)$$

$$qE^{II}(q) + 4\pi n_0 e \int f^{II}(q, v') dv' = E(0, 0) \quad (16)$$

The solution for the electric field is easily found to be:

$$E(p, q) = \frac{N(p, q)}{D(p, q)} \quad (17)$$

where:

$$\begin{aligned} N(p, q) &= \frac{E^I(p)}{q} - \frac{4\pi n_0 e}{q} \int dv' \frac{[f^{II}(q, v') + v' f^I(p, v')]}{p + v'q} \\ &= \frac{E^{II}(q)}{p} + \frac{4\pi n_0 e}{p} \int v' dv' \frac{[f^{II}(q, v') + v' f^I(p, v')]}{p + v'q} \end{aligned} \quad (18)$$

$$\begin{aligned} D(p, q) &= 1 + \frac{\omega_p^2}{q} \int \frac{df_0}{dv'} \frac{dv'}{p + v'q} \\ &= 1 - \frac{\omega_p^2}{p} \int \frac{df_0}{dv'} \frac{v' dv'}{p + v'q} \end{aligned} \quad (19)$$

and  $\omega_p$  is the plasma frequency. The solution for  $f(p, q, v)$  is then easily found from Eq. (13).

#### RELATIONS AMONG THE BOUNDARY AND INITIAL CONDITIONS

In order for the inverse Laplace transforms, Eqs. (10-12), to be defined, it must be possible to find contours  $C_p$  and  $C_q$  such that  $E(p, q)$  and

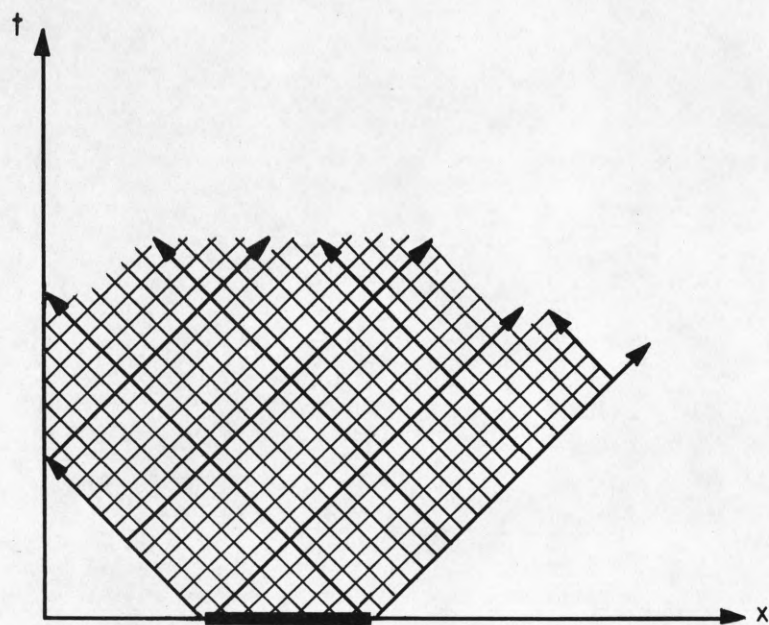


$f(p,q,v)$  are analytic to the right of these contours in the  $p$  and  $q$  planes. It was found in I, on the other hand, that unless the boundary and initial conditions were suitably restricted, that such contours could not in general be found. The lack of the required analyticity occurred when there were characteristics associated with negative characteristic velocities. In that case information specified at  $t = 0$  was propagated to  $x = 0$ . The result was that the boundary conditions were determined by the initial conditions and could not be specified independently. Figure 2 shows how information specified at  $t = 0$  can affect the boundary at  $x = 0$  in this case. The Vlasov equation can be thought of as a system of equations of the type considered in I. (See the appendix at the end of this paper.) There is one equation for each value of the velocity  $v$ , and the characteristic velocities are these values of  $v$ . A number of these characteristic velocities are, then, of course, negative. One would hence expect relations among the boundary and initial conditions to occur for the Vlasov equation in much the same way as they occurred in I when there were negative characteristic velocities. It will be seen that this is, in fact, the case.

Consider the singularities of  $E(p,q)$  in the  $p$ -plane for a given  $q$ . There is, first of all, a cut along the line  $p = -vq$  for  $-\infty < v < \infty$ . See Fig. 3. This is a generalization of the cut which appears along the imaginary  $p$ -axis in the Landau treatment for the value  $q = ik$ . To investigate the discontinuity of  $D(p,q)$  across this cut, it is convenient to define:

$$D^{\pm}(v,q) = \lim_{\substack{-p \rightarrow v \pm i\epsilon \\ q}} D(p,q) \quad (20)$$

Using the relation:



PR-684

Figure 2. Propagation of information specified at  $t = 0$  to the boundary  $x = 0$ .

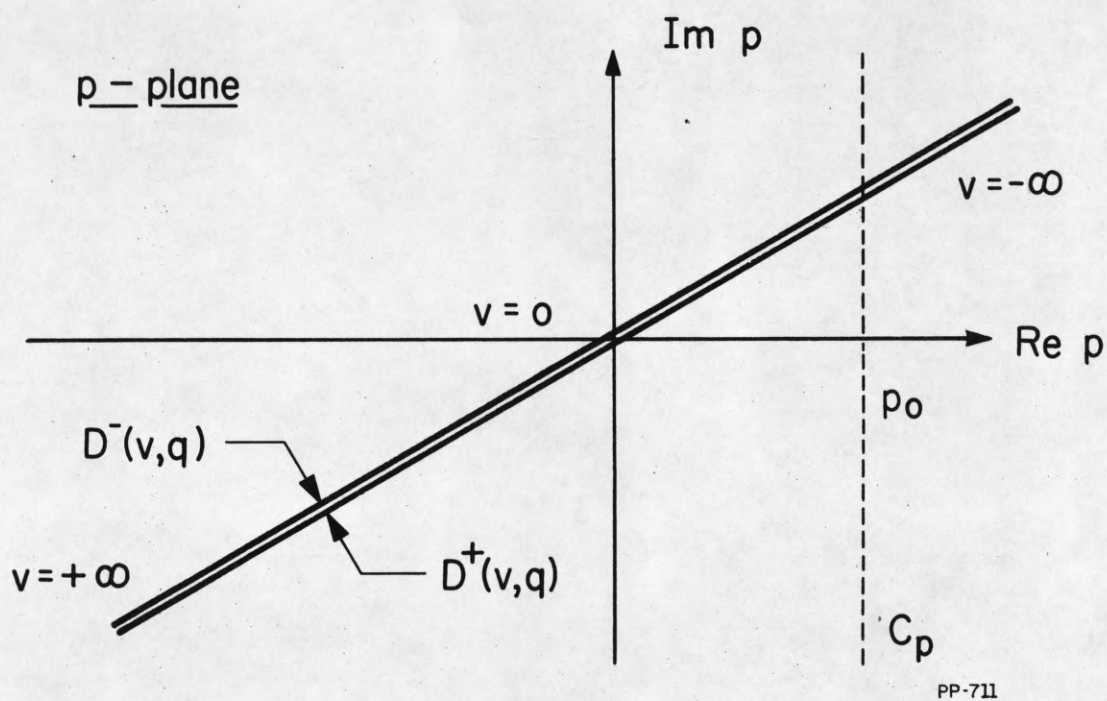


Figure 3. Cut of  $E(p, q)$  in the  $p$ -plane for a given  $q$ . ( $\text{Re } q > 0$ )



$$\lim_{s \rightarrow u + i\epsilon} \left( \frac{1}{t - s} \right) = P \left( \frac{1}{t - u} \right) \pm i\pi\delta(t-u) \quad (21)$$

where P indicates the principal value, it is easy to calculate:

$$D^+(v, q) = 1 + \left( \frac{\omega}{q} \right)^2 P \int \frac{df_o}{dv'} \frac{dv'}{v' - v} \pm i\pi \left( \frac{\omega}{q} \right)^2 \frac{df_o}{dv} \quad (22)$$

or that:

$$D^+ = D^- + \Delta D \quad (23)$$

with:

$$\Delta D = 2\pi i \left( \frac{\omega}{q} \right)^2 \frac{df_o}{dv} \quad (24)$$

Similarly if:

$$N^+(v, q) = \lim_{q \rightarrow v + i\epsilon} N(p, q), \quad (25)$$

then:

$$N^+ = N^- + \Delta N \quad (26)$$

$$\Delta N = - \frac{8\pi^2 \ln_o e}{2q} [f^{II}(q, v) + vf^I(-vq, v)] \quad (27)$$

It can be seen from Fig. 3 that this cut makes it impossible to draw a contour  $C_p$  to the right of all singularities. To have a well-defined Laplace transform, then, it is necessary to choose the boundary and initial conditions so as to eliminate this cut, or more exactly, to eliminate that part of it in the right half-plane. As could be expected, the part of the cut in the right half-plane is that due to negative values of  $v$ . To eliminate the cut, it is sufficient to determine the boundary and initial conditions for negative  $v$  so that:

$$\frac{N^+}{D^+} = \frac{N^-}{D^-} = \frac{N^- + \Delta N}{D^- + \Delta D} \quad (28)$$

The expression resulting from substitution of the appropriate quantities into Eq. (28) is:

$$[f^{II}(q,v) + vf^I(-vq,v)] \left[ 1 + \left(\frac{\omega p}{q}\right)^2 P \int \frac{df_o}{dv'} \frac{dv'}{v' - v} \right] = \frac{df_o}{dv} \left\{ \left(\frac{\omega p}{q}\right)^2 P \int dv' \frac{[f^{II}(q,v') + v'f^I(-v'q,v')] - \frac{eE^I(-vq)}{mq}}{v' - v} \right\} \quad (29)$$

provided  $v < 0$ . Eq. (29) is the relation that must be satisfied by the boundary and initial conditions for a well-defined solution  $E(p,q)$ .

It is still necessary to determine if  $f(p,q,v)$  is analytic to the right of the contour  $C_p$ . The function  $f(p,q,v)$  is given by:

$$f(p,q,v) = \frac{1}{p + vq} \left\{ \frac{e}{m} \frac{df_o}{dv} E(p,q) + f^{II}(q,v) + vf^I(p,v) \right\} \quad (30)$$

Provided  $E(p,q)$  is analytic to the right of  $C_p$ ,  $f(p,q,v)$  has only a pole at  $p = -vq$  for negative  $v$  that could be a problem. Explicit calculation can verify, however, that the residue of this pole is zero in virtue of Eq. (29), so that there is, in fact, no pole of  $f(p,q,v)$  at  $p = -vq$  for negative  $v$ .

It has now been demonstrated that in order to have a well-formulated mixed boundary initial value problem for the equations given, the boundary and initial conditions must be chosen to satisfy Eqs. (4-6) and (29). It has been assumed that the boundary and initial conditions are sufficiently well-behaved that the preceding analysis can be carried out. By picking sufficiently singular boundary and initial conditions one can produce arbitrary steady-state plasma oscillations,<sup>8,6</sup> in which case the analysis given in this paper is not relevant.

## SATISFACTION OF THE BOUNDARY AND INITIAL CONDITIONS

It should be determined if the solution, subject to the restrictions on the boundary and initial conditions, does indeed satisfy the specified boundary and initial conditions. In order to do this it will be assumed that the boundary and initial conditions can be expanded as follows:

$$E^I(p) = \frac{1}{p} E(0,0) + \frac{1}{p^2} \frac{\partial E}{\partial t}(0,0) + \dots \quad (31)$$

$$E^{II}(q) = \frac{1}{q} E(0,0) + \frac{1}{q^2} \frac{\partial E}{\partial x}(0,0) + \dots \quad (32)$$

with similar expressions for  $f^I(p,v)$  and  $f^{II}(q,v)$ . To see if the initial conditions are satisfied, one can move the contour  $C_p$  to  $p_0 = \infty$ , keeping it sufficiently small so that  $e^{pt} \simeq 1$ . The inversion integral for  $E(x,t \rightarrow 0)$  then becomes:

$$E(x,t \rightarrow 0) = (2\pi i)^{-2} \int dp dq E(p \rightarrow \infty, q) e^{pt + qx} \quad (33)$$

An analogous expression for  $x \rightarrow 0$  is obtained. This method is described in detail in I.

Examination of the solution, Eqs. (17-19), indicates:

$$E(p \rightarrow \infty, q) = \frac{E^{II}(q)}{p} + \dots \quad (34)$$

so that:

$$\begin{aligned} E(x,t \rightarrow 0) &= (2\pi i)^{-2} \int dp dq \frac{E^{II}(q)}{p} e^{pt + qx} \\ &= (2\pi i)^{-1} \int dq E^{II}(q) e^{qx} \\ &= E(x,0) \end{aligned} \quad (35)$$

(The higher order terms in Eq. (34) do not contribute in the first integration in Eq. (35). Eq. (35) indicates that the solution  $E(x,t)$  satisfies the initial condition. Similarly one can see that:



$$f(p \rightarrow \infty, q, v) = \frac{f^{II}(q, v)}{p} \quad (36)$$

$$E(p, q \rightarrow \infty) = \frac{E^I(p)}{q} \quad (37)$$

$$f(p, q \rightarrow \infty, v) = \frac{f^I(p, v)}{q} \quad (38)$$

and, hence, that  $E(x, t)$  and  $f(x, t, v)$  satisfy all the boundary and initial conditions.

#### EXAMPLE

As a simple example to illustrate the method, the case of a cold electron beam in a cold plasma will be taken. The unperturbed distribution function is:

$$f_0 = \frac{1}{n_0} [n_p \delta(v) + n_b \delta(v - v_b)]$$

The subscript  $p$  refers to plasma quantities, and the subscript  $b$  refers to beam quantities. The following set of boundary and initial conditions will be chosen:

$$\begin{aligned} f(0, t, v) &= 0 & f(x, 0, v) &= \delta(v) \sin kx \\ E(0, t, v) &= 0 & E(x, 0) &= -\frac{m\omega^2}{ek} (1 - \cos kx) \end{aligned} \quad (39)$$

It can be explicitly verified that this set satisfies Eqs. (4-6) and (29).

The relations:

$$x\delta(x) = 0 \quad (40)$$

$$\delta(x) = -x\delta'(x) \quad (41)$$

are useful in showing that Eq. (29) is satisfied.

The transform of the electric field can then be written:

$$E(p,q) = \frac{-4\pi n_0 e \int dv' f^{II}(q,v')}{q \int \frac{dv'}{p + v'q}} \quad (42)$$

$$1 + \frac{\omega_p^2}{q \int \frac{df_0}{dv'} \frac{dv'}{p + v'q}}$$

After the velocity integrations are performed,  $E(p,q)$  becomes:

$$E(p,q) = \frac{-4\pi n_0 e k}{pq(q^2 + k^2)} \quad (43)$$

$$1 + \frac{\omega_p^2}{p^2} + \frac{\omega_b^2}{(p + v_b q)^2}$$

This is the same result as was obtained in a similar calculation using the hydrodynamic approximation.<sup>9</sup> The solution is extensively discussed in that paper.

#### SUMMARY

The mixed boundary-initial value problem for the Vlasov equation has been treated by double Laplace transformation. It has been shown that a well-formulated problem can be obtained only if the boundary and initial conditions are suitably restricted. The restrictions consist of three fairly simple relations which can be considered to determine the electric field boundary and initial conditions if the distribution function boundary and initial conditions are given. Another, more complicated, integral relation between the boundary and initial conditions associated with negative velocities must also be satisfied. It has also been shown that the given solution does satisfy the boundary and initial conditions in general. A simple example for a cold beam in a cold plasma has been shown to give results consistent with previous calculations.

## ACKNOWLEDGEMENT

This work was supported in whole by the Joint Services Electronics Program (U. S. Army, U. S. Navy, and U. S. Air Force) under contract DAAB-07-67-C-0199.

## APPENDIX

It is possible to formulate Eqs. (1-3) into a set of linear, first order, hyperbolic, partial differential equations of the type considered in I, provided the velocity  $v$  is assumed to be a discrete parameter. The values of the velocity will be labeled  $v_i$ :  $-N \leq i \leq N$ . The number  $N$  will be very large. Let:

$$f_i(x,t) = f(x,t,v_i) \quad (44)$$

$$\Delta v_i = v_{i+1} - v_i \quad (45)$$

Eqs. (1-3) become:

$$\frac{\partial f_i}{\partial t} + v_i \frac{\partial f_i}{\partial x} - \frac{e}{m} \frac{df_o}{dv_i} = 0 \quad (46)$$

$$\frac{\partial E}{\partial t} - 4\pi n_o e \sum_i v_i f_i \Delta v_i = 0 \quad (47)$$

with the subsidiary condition:

$$\frac{\partial E}{\partial x} + 4\pi n_o e \sum_i f_i \Delta v_i = 0 \quad (48)$$

These are a system of  $2N+2$  equations in  $2N+2$  unknowns, with a subsidiary condition which can be shown to be satisfied in virtue of the other equations, provided it is satisfied at  $t = 0$ .<sup>1</sup> It can easily be seen that relations analogous to Eqs. (4-5) are obtained:

$$\frac{\partial E(x,0)}{\partial x} + 4\pi n_o e \sum_i f_i(x,0) \Delta v_i = 0 \quad (49)$$



$$\frac{\partial E(0,t)}{\partial t} + 4\pi n_0 e \sum_i v_i f_i(0,t) \Delta v_i = 0 \quad (50)$$

$$\left[ \frac{\partial f_i}{\partial t} - \frac{e}{m} \frac{df_0}{dv_i} \right]_{i=0} = 0 \quad (51)$$

These conditions are a result of characteristics lying on the boundaries  $x = 0$  and  $t = 0$ .

If Eqs. (49-50) are Laplace transformed, the result is:

$$(p + v_i q) f_i - \frac{e}{m} \frac{df_0}{dv_i} E = f_i^{II}(q) + v_i f_i^I(p) \quad (52)$$

$$pE - 4\pi n_0 e \sum_i v_i f_i \Delta v_i = E^{II}(q) \quad (53)$$

In Eqs. (52-53)  $f_i = f_i(p,q)$  and  $E = E(p,q)$  are the double transforms of  $f_i(x,t)$  and  $E(x,t)$ ,  $f_i^I(p)$  and  $E^I(p)$  are the single transforms of  $f_i(0,t)$  and  $E(0,t)$ , and  $f_i^{II}(q)$  and  $E^{II}(q)$  are the single transforms of  $f_i(x,0)$  and  $E(x,0)$ . If we take  $f_{N+1}$  to be the electric field  $E$ , the solution is:

$$f_i(p,q) = \frac{[a_{jk} f_k^{II}(q) + b_{jk} f_k^I(p)] d_{ji}(p,q)}{\Delta(p,q)} \quad (54)$$

where:

$$a_{jk} = \delta_{jk} \quad (55)$$

$$b_{jk} = v_j \delta_{jk} \quad (56)$$

$$c_{jk} = \begin{cases} 0 & j, k \neq N+1 \\ 0 & j, k = N+1 \\ -\frac{e}{m} \frac{df_0}{dv_j} & k = N+1 \\ -4\pi n_0 e v_k \Delta v_k & j = N+1 \end{cases} \quad (57)$$

$$\Delta_{jk} = a_{jk} p + b_{jk} q + c_{jk} \quad (58)$$

$$d_{jk} = \text{cofactor of } \Delta_{jk} \quad (59)$$

$$\Delta(p,q) = \det |\Delta_{jk}| \quad (60)$$

The function  $\Delta(p,q)$  can be calculated to be:

$$\Delta(p,q) = p \prod_i (p + v_i q) - \sum_i \omega_i^2 \frac{df_0}{dv_i} v_i \Delta v_i \prod_{j \neq i} (p + v_j q) \quad (61)$$

The  $N+1$  terms are not included in the sums and products. It can be seen that  $\Delta(p,q)$  is related to  $D(p,q)$ :

$$D(p,q) \leftrightarrow \frac{\Delta(p,q)}{p \prod_i (p + v_i q)} \quad (62)$$

The characteristic velocities  $c_i$  are found from the asymptotic values  $p_i(q) = -c_i q$  of the roots of  $\Delta(p,q) = 0$ . The characteristic velocities can be seen from Eq. (61) to be the  $v_i$ . The fact that relations among the boundary and initial conditions only occur for negative characteristic velocities is consistent with the relation derived in Eq. (29).

The singularities of  $E(p,q)$ , apart from the singularities of the boundary and initial conditions, come from the zeros of  $\Delta(p,q)$ . It can be seen then that in the limit  $N \rightarrow \infty$ ,  $D(p,q)$  will have an infinite number of zeros. Evidently some of these are responsible for the cut which appears when  $v$  is treated as a continuous variable.

This approach of treating  $v$  as a discrete parameter has its main value as a bridge from the methods used in I to those treated in this paper. It provides some intuitive understanding of the problem; however, it will not be investigated further.

## REFERENCES

1. K. Evans, Jr., "Double Laplace Transformation in Mixed Boundary-Initial Value Problems and its Application to Multi-component Plasmas" (Thesis, University of Illinois, Urbana, Illinois, 1970), and Coordinated Science Laboratory Report R-450 (1969).
2. K. Evans, Jr. and E. A. Jackson, (to be published).
3. L. Spitzer, Jr., Physics of Fully Ionized Gases (Interscience, New York, 1956), p. 94 ff.
4. D. C. Montgomery and D. A. Tidman, Plasma Kinetic Theory (McGraw-Hill, New York, 1964), p. 41 ff.
5. L. Landau, Journ. of Phys. 10, 25 (1946).
6. J. D. Jackson, J. Nucl. Energy: Pt. C 1, 171 (1960).
7. I. N. Sneddon, Fourier Transforms, (McGraw-Hill, New York, 1951), p. 45 ff.
8. I. B. Bernstein, J. M. Green, and M. D. Kruskal, Phys. Rev. 108, 546 (1957).
9. K. Evans, Jr. and E. A. Jackson, Phys. Fluids (to be published).



# Distribution List as of April 1, 1970

ESD (ESTI)  
L. C. Hanscom Field  
Bedford, Mass 01731 2 copies

Defense Documentation Center  
Attn: DDC-TCA  
Cameron Station  
Alexandria, Virginia 22314 50 copies

Commanding General  
Attn: STEMS-RE-L, Technical Library  
White Sands Missile Range  
New Mexico 88002 2 copies

Mr Robert O. Parker, AMSEL-RD-S  
Executive Secretary, TAC/JSEF  
U.S. Army Electronics Command  
Fort Monmouth, New Jersey 07703

Director, Electronic Programs  
Attn: Code 427  
Department of the Navy  
Washington, D.C. 20360 2 copies

Naval Air Systems Command  
AIR 03  
Washington, D.C. 20360 2 copies

Director  
Naval Research Laboratory  
Attn: Code 2027  
Washington, D.C. 20390 6 copies

Naval Electronic Systems Command  
ELEX 03, Room 2046 Munitions Building  
Department of the Navy  
Washington, D.C. 20360 2 copies

Commander  
U.S. Naval Ordnance Laboratory  
Attn: Librarian  
White Oak, Md 20910 2 copies

LTC H. W. Jackson  
Chief, Electronics Division  
Directorate of Engineering Sciences  
Air Force of Scientific Research  
Arlington, Virginia 22209 5 copies

Commander  
Naval Electronics Laboratory Center  
Attn: Library  
San Diego, Calif 92152 2 copies

Dr. L. M. Hollingsworth  
AFCL (CRN)  
L. C. Hanscom Field  
Bedford, Mass 01731

Division of Engineering & Applied Physics  
210 Pierce Hall  
Harvard University  
Cambridge, Mass 02138

Director  
Research Laboratory of Electronics  
Massachusetts Institute of Technology  
Cambridge, Mass 02139

Miss R. Joyce Harman  
Project MAC, Room 810  
545 Technology Square  
Cambridge, Mass 02139

Professor R. H. Rediker  
Elec Engineering Professor  
Mass, Institute of Technology  
Building 13-3050  
Cambridge, Mass 02139

Raytheon Company  
Research Division Library  
28 Seyon Street  
Waltham, Mass 02154

Sylvania Electronic Systems  
Applied Research Laboratory  
Attn: Documents Librarian  
40 Sylvan Road  
Waltham, Mass 02154

Commanding Officer  
Army Materials & Mechanics  
Research Center  
Attn: Dr H. Priest  
Watertown Arsenal  
Watertown, Mass 02172

MIT Lincoln Laboratory  
Attn: Library A-082  
PO Box 73  
Lexington, Mass 02173

Commanding Officer  
Office of Naval Research  
Branch Office  
495 Summer Street  
Boston, Mass 02210

Commanding Officer (Code 2064)  
U.S. Naval Underwater Sound Laboratory  
Fort Trumbull  
New London, Conn 06320

Dept of Eng & Applied Science  
Yale University  
New Haven, Conn 06520

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-CT-A  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-CT-D  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-CT-I  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-CT-L (Dr W.S. McAfee)  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-CT-O  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-CT-R  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-CT-S  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-GG-DD  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-DL  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-KL-D  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-KL-E  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-KL-I  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-KL-SM  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-KL-S  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-KL-T  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-ML-A  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-ML-C  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-ML-D (Dr H. Bennett)  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-ML-P  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-SC  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-VL-D  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-VL-F  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-WL-D  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-XL-DT  
Fort Monmouth, New Jersey 07703

Commanding General  
U.S. Army Electronics Command  
Attn: AMSEL-XL-D  
Fort Monmouth, New Jersey 07703

Mr Norman J. Field, AMSEL-RD-S  
Chief, Office of Science & Technology  
Research and Development Directorate  
U.S. Army Electronics Command  
Fort Monmouth, New Jersey 07703

Project Manager  
Common Positioning & Navigation Systems  
Attn: Harold H. Bahr (AMCPM-NS-IM),  
Building 439  
U.S. Army Electronics Command  
Fort Monmouth, New Jersey 07703

U.S. Army Munitions Command  
Attn: Science & Technology  
Info Br., Bldg 59  
Picatinny Arsenal, SMUPA-RT-S  
Dover, New Jersey 07801

European Office of Aerospace Research  
APO New York 09667

Director  
Columbia Radiation Laboratory  
Columbia University  
538 West 120th ST  
New York, N. Y. 10027

Dr John R. Ragazzini, Dean  
School of Engineering & Science  
New York University  
University Heights  
Bronx, New York 10453

Mr Jerome Fox, Research Coordinator  
Polytechnic Institute of Brooklyn  
333 Jay St.  
Brooklyn, New York 11201

Airborn Instruments Laboratory  
Deerpark, New York 11729

Dr W. R. Lepage, Chairman  
Syracuse University  
Dept of Electrical Engineering  
Syracuse, New York 13210

Rome Air Development Center  
Attn: Documents Library (EMTLD)  
Griffiss Air Force Base, New York 13440

Mr H. E. Webb (EMBSI)  
Rome Air Development Center  
Griffiss Air Force Base, New York 13440

Professor James A. Cadzow  
Department of Electrical Engineering  
State University of New York at Buffalo  
Buffalo, New York 14214

Dr A. G. Jordan  
Head of Dept of Elec Engineering  
Carnegie-Mellon University  
Pittsburgh, Penn 15213

Hunt Library  
Carnegie-Mellon University  
Schenley Park  
Pittsburgh, Penn 15213

Lehigh University  
Dept of Electrical Engineering  
Bethlehem, Penn 18015

Commander (ADL)  
Naval Air Development Center  
Attn: NADC Library  
Johnsville, Warminster, Pa 18974

Technical Director (SMUPA-A2000-107-1)  
Frankford Arsenal  
Philadelphia, Penn 19137

Mr M. Zane Thornton, Chief, Network  
Engineering, Communications and  
Operations Branch, Lister Hill  
National Center/ Biomedical Communications  
8600 Rockville Pike  
Bethesda, Maryland 20014

U.S. Post Office Dept  
Library - Room 6012  
12th & Pennsylvania Ave, N.W.  
Washington, D.C. 20260

Technical Library  
DDR&E  
Room 3C-122, The Pentagon  
Washington, D.C. 20301

Director for Materials Sciences  
Advanced Research Projects Agency  
Department of Defense  
Washington, D.C. 20301

Asst Director (Research)  
Rm 3C128, The Pentagon  
Office of the Sec of Defense  
Washington, D.C. 20301

Chief, R & D Division (340)  
Defense Communications Agency  
Washington, D.C. 20305

Distribution List (cont'd.)

Commanding General  
U.S. Army Materiel Command  
Attn: AMGRD-TP  
Washington, D.C. 20315

Director, U.S. Army Materiel  
Concepts Agency  
Washington, D.C. 20315

Hq USAF (AFRDD)  
The Pentagon  
Washington, D.C. 20330

Hq USAF (AFRDDG)  
The Pentagon  
Washington, D.C. 20330

Hq USAF (AFRDS)  
The Pentagon  
Washington, D.C. 20330

AFSC (SCTSE)  
Andrews Air Force Base, Maryland 20331

Dr I. R. Mirman  
Hq AFSC (SGGP)  
Andrews AFB, Maryland 20331

Naval Ship Systems Command  
Ship 031  
Washington, D.C. 20360

Naval Ship Systems Command  
Ship 035  
Washington, D.C. 20360

Commander  
U.S. Naval Security Group Command  
Attn: G43  
3801 Nebraska Avenue  
Washington, D.C. 20390

Director  
Naval Research Laboratory  
Washington, D.C. 20390  
Attn: Dr A. Brodzinsky, Sup. Elec Div

Director  
Naval Research Laboratory  
Washington, D.C. 20390  
Attn: Maury Center Library (Code 8050)

Director  
Naval Research Laboratory  
Washington, D.C. 20390  
Attn: Dr W.C. Hall, Code 7000

Director  
Naval Research Laboratory  
Attn: Library, Code 2029 (ONRL)  
Washington, D.C. 20390

Dr G. M. R. Winkler  
Director, Time Service Division  
U. S. Naval Observatory  
Washington, D.C. 20390

Colonel E.P. Gaines, Jr  
ACDA/FO  
1901 Pennsylvania Ave. N.W.  
Washington, D.C. 20451

Commanding Officer  
Harry Diamond Laboratories  
Attn: Mr Berthold Altman (AMXDO-TI)  
Connecticut Ave & Van Ness St., N.W.  
Washington, D.C. 20438

Central Intelligence Agency  
Attn: CRS/ADD Publications  
Washington, D.C. 20505

Dr H. Harrison, Code RRE  
Chief, Electrophysics Branch  
National Aeronautics & Space Admin  
Washington, D.C. 20546

The John Hopkins University  
Applied Physics Laboratory  
Attn: Document Librarian  
8621 Georgia Avenue  
Silver Spring, Maryland 20910

Technical Director  
U.S. Army Limited War Laboratory  
Aberdeen Proving Ground  
Aberdeen, Maryland 21005

Commanding Officer (AMXRD-BAT)  
US Army Ballistics Research Laboratory  
Aberdeen Proving Ground  
Aberdeen, Maryland 21005

Electromagnetic Compatibility  
Analysis Center (EGAC)  
Attn: ACOAT  
North Severn  
Annapolis, Maryland 21402

Commanding Officer  
U.S. Army Engineer Topographic Laboratories  
Attn: STINFLO Center  
Fort Belvoir, Virginia 22060

U.S. Army Mobility Equipment Research  
and Development Center, Bldg 315  
Attn: Technical Document Center  
Fort Belvoir, Virginia 22060

Director (NV-D)  
Night Vision Laboratory, USAECOM  
Fort Belvoir, Virginia 22060

Dr Alvin D. Schnitzler  
Institute for Defense Analyses  
Science and Technology Division  
400 Army-Navy Drive  
Arlington, Virginia 22202

Director  
Physical & Engineering Sciences Division  
3045 Columbia Pike  
Arlington, Va 22204

Commanding General  
U.S. Army Security Agency  
Attn: IARD-T  
Arlington Hall Station  
Arlington, Virginia 22212

Commanding General  
USACDC Institute of Land Combat  
Attn: Technical Library, Rm 636  
2461 Eisenhower Avenue  
Alexandria, Virginia 22314

VELA Seismological Center  
300 North Washington St  
Alexandria, Virginia 22314

U.S. Naval Weapons Laboratory  
Dahlgren, Virginia 22448

Research Laboratories for the Eng  
Sciences, School of Engineering &  
Applied Science  
University of Virginia  
Charlottesville, Va 22903

Dr Herman Robl  
Deputy Chief Scientist  
U.S. Army Research Office (Durham)  
Box CM, Duke Station  
Durham, North Carolina 27706

Rochard O. Ulsh (CRDARD-IP)  
U.S. Army Research Office (Durham)  
Box CM, Duke Station  
Durham, North  
Durham, North

Richard O. Ulsh (CRDARD-IP)  
U.S. Army Research Office (Durham)  
Box CM, Duke Station  
Durham, North Carolina 27706

ADTC (ADBPS-12)  
Eglin AFB, Florida 32542

Commanding Officer  
Naval Training Device Center  
Orlando, Florida 32813

Technical Library, AFETR  
(ETV,MU-135)  
Patrick AFB, Florida 32925

Commanding General  
U.S. Army Missile Command  
Attn: AMSMI-RR  
Redstone Arsenal, Alabama 35809

Redstone Scientific Information Center  
Attn: Chief, Document Section  
U.S. Army Missile Command  
Redstone Arsenal, Alabama 35809

AUL3T-9663  
Maxwell AFB, Alabama 36112

Hq AEDC (AETS)  
Attn: Library/Documents  
Arnold AFS, Tennessee 37389

Case Institute of Technology  
Engineering Division  
University Circle  
Cleveland, Ohio 44106

NASA Lewis Research Center  
Attn: Library  
21000 Brookpark Road  
Cleveland, Ohio 44135

Director  
Air Force Avionics Laboratory  
Wright-Patterson AFB, Ohio 45433

AFAL (AVTA) R.D. Larson  
Wright-Patterson AFB, Ohio 45433

AFAL (AVT) Dr H.V. Noble, Chief  
Electronics Technology Division  
Air Force Avionics Laboratory  
Wright-Patterson AFB, Ohio 45433

Dr Robert E. Fontana  
Head, Dept of Elec Engineering  
Air Force Institute of Technology  
Wright Patterson AFB, Ohio 45433

Dept of Electrical Engineering  
Clippinger Laboratory  
Ohio University  
Athens, Ohio 45701

Commanding Officer  
Naval Avionics Facility  
Indianapolis, Indiana 46241

Dr John D. Hancock, Head  
School of Electrical Engineering  
Purdue University  
Lafayette, Ind 47907

Professor Joseph E. Rowe  
Chairman,  
Dept of Elec Engineering  
The University of Michigan  
Ann Arbor, Michigan 48104

Dr G. J. Murphy  
The Technological Institute  
Northwestern University  
Evanston, Ill 60201

Commanding Officer  
Office of Naval Research  
Branch Office  
219 South Dearborn St  
Chicago, Illinois 60604

Illinois Institute of Technology  
Dept of Electrical Engineering  
Chicago, Illinois 60616

Deputy for Res. and Eng (AMSE-DRE)  
U.S. Army Weapons Command  
Rock Island Arsenal  
Rock Island, Illinois 61201

Commandant  
U.S. Army Command & General  
Staff College  
Attn: Acquisitions, Library Division  
Fort Leavenworth, Kansas 66027

Dept of Electrical Engineering  
Rice University  
Houston, Texas 77001

HQ AMD (AMR)  
Brooks AFB, Texas 78235

USAFSAM (SMKOR)  
Brooks AFB, Texas 78235

Mr B. R. Locke  
Technical Adviser, Requirements  
USAF Security Service  
Kelly Air Force Base, Texas 78241

Director  
Electronics Research Center  
The University of Texas as Austin  
Eng-Science Bldg 110  
Austin, Texas 78712

Department of Elec Engineering  
Texas Technological University  
Lubbock, Texas 79409

Commandant  
U.S. Army Air Defense School  
Attn: Missile Sciences Div., C&S Dept  
P.O. Box 9390  
Fort Bliss, Texas 79916

Director  
Aerospace Mechanics Sciences  
Frank J. Seiler Research Laboratory (OAR)  
USAF Academy  
Colorado Springs, Colorado 80840

Director of Faculty Research  
Department of the Air Force  
U.S. Air Force Academy  
Colorado Springs, Colorado 80840

Major Richard J. Gowen  
Tenure Associate Professor  
Dept of Electrical Engineering  
U.S. Air Force Academy  
Colorado Springs, Colorado 80840

Academy Library (DFSLB)  
U.S. Air Force Academy  
Colorado Springs, Colorado 80840

M.A. Rothenberg (STEPD-SC(S))  
Scientific Director  
Desert Test Center  
Bldg 100, Soldiers' Circle  
Fort Douglas, Utah 84113

Utah State University  
Dept of Electrical Engineering  
Logan, Utah 84321

School of Engineering Sciences  
Arizona State University  
Tempe, Ariz 85281

## Distribution List (cont'd.)

Commanding General  
U.S. Army Strategic Communications  
Command  
Attn: SCC-CG-SAE  
Fort Huachuca, Arizona 85613

The University of Arizona  
Dept of Electrical Engineering  
Tucson, Arizona 85721

Capt C. E. Baum  
AFWL (WLRE)  
Kirkland AFB, New Mexico 87117

Los Alamos Scientific Laboratory  
Attn: Report Library  
P. O. Box 1663  
Los Alamos, N.M. 87544

Commanding Officer  
(AMSEL-BL-WS-R)  
Atmospheric Sciences Laboratory  
White Sands Missile Range  
New Mexico 88002

Commanding Officer  
Atmospheric Sciences Laboratory  
White Sands Missile Range  
New Mexico 88002

Chief, Missile Electronic Warfare  
Technical Area, (AMSEL-WL-M)  
U. S. Army Electronics Command  
White Sands Missile Range  
New Mexico 88002

Director  
Electronic Sciences Lab  
University of Southern California  
Los Angeles, Calif 90007

Eng & Math Sciences Library  
University of California at Los Angeles  
405 Hilgred Avenue  
Los Angeles, Calif 90024

Aerospace Corporation  
P. O. Box 95085  
Los Angeles, California 90045  
Attn: Library Acquisitions Group

Hq SAMSQ (SMITTS/Lt Belate)  
AF Unit Post Office  
Los Angeles, Calif 90045

Dr Sheldon J. Wells  
Electronic Properties Information Center  
Mail Station E-175  
Hughes Aircraft Company  
Culver City, California 90230

Director, USAF PROJECT RAND  
Via: Aif Force Liaison Office  
The RAND Corporation  
Attn: Library D  
1700 Main Street  
Santa Monica, California 90406

Deputy Director & Chief Scientist  
Office of Naval Research Branch Office  
1030 East Green Street  
Pasadena, California 91101

Aeronautics Library  
Graduate Aeronautical Laboratories  
California Institute of Technology  
1201 E. California Blvd  
Pasadena, California 91109

Professor Nicholas George  
California Institute of Technology  
Pasadena, California 91109

Commanding Officer  
Naval Weapons Center  
Corona Laboratories  
Attn: Library  
Corona, California 91720

Dr F. R. Charvat  
Union Carbide Corporation  
Materials Systems Division  
Crystal Products Dept  
8888 Balboa Avenue  
P. O. Box 23017  
San Diego, California 92123

Hollander Associates  
P. O. Box 2276  
Fullerton, California 92633

Commander, U.S. Naval Missile Center (56322)  
Point Mugu, California 93041

W.A. Eberspacher, Associate Head  
Systems Integration Division  
Code 5340A, Box 15  
U.S. Naval Missile Center  
Point Mugu, California 93041

Sciences-Engineering Library  
University of California  
Santa Barbara, California 93106

Commander (Code 753)  
Naval Weapons Center  
Attn: Technical Library  
China Lake, California 93555

Library (Code 2124)  
Technical Report Section  
Naval Postgraduate School  
Monterey, California 93940

Glen A. Myers (Code 52Mv)  
Assoc Professor of Elec Eng  
Naval Postgraduate School  
Monterey, California 93940

Dr Leo Young  
Stanford Research Institute  
Menlo Park, California 94025

Lenkurt Electric Co., Inc.  
1105 County Road  
San Carlos, California 94070  
Attn: Mr E.K. Peterson

Director  
Microwave Laboratory  
Stanford University  
Stanford, California 94305

Director  
Stanford Electronics Laboratories  
Stanford University  
Stanford, California 94305

Director  
Electronics Research Laboratory  
University of California  
Berkeley, California 94720



## DOCUMENT CONTROL DATA - R &amp; D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate author) University of Illinois Coordinated Science Laboratory Urbana, Illinois 61801		2a. REPORT SECURITY CLASSIFICATION	
		2b. GROUP	
3. REPORT TITLE THE MIXED BOUNDARY-INITIAL VALUE PROBLEM FOR THE VLASOV EQUATION			
4. DESCRIPTIVE NOTES (Type of report and inclusive dates)			
5. AUTHOR(S) (First name, middle initial, last name) EVANS, Kenneth, Jr.			
6. PERIOD June 1970		7a. TOTAL NO. OF PAGES 17	7b. NO. OF REFS 9
8a. CONTRACT OR GRANT NO. DAAB 07-67-C-0199		9a. ORIGINATOR'S REPORT NUMBER(S) R-473	
b. PROJECT NO.			
c.		9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report) UILU-ENG 70-218	
d.			
10. DISTRIBUTION STATEMENT This document has been approved for public release and sale; its distribution is unlimited.			
11. SUPPLEMENTARY NOTES		12. SPONSORING MILITARY ACTIVITY Joint Services Electronics Program thru U.S. Army Electronics Command Fort Monmouth, New Jersey 07703	
13. ABSTRACT The mixed boundary initial value problem for the Vlasov equation is treated by double Laplace transformation. It is found that certain relations must be satisfied by the boundary and initial values in order to have a well-defined problem. The case of a cold beam in a cold plasma is treated as a simple example. An approach to the problem via discrete velocities is treated in an appendix.			

