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_Title: Phase analysis in maximal sprinting: an investigation of step-to-step technical changes between the initial acceleration, transition and maximal velocity phases.

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1 **Abstract**

2 The aim of this study was to investigate spatiotemporal and kinematic changes between the
3 initial acceleration, transition and maximum velocity phases of a sprint. Sagittal plane
4 kinematics from five experienced sprinters performing 50 m maximal sprints were collected
5 using six HD-video cameras. Following manual digitising, spatiotemporal and kinematic
6 variables at touchdown and toe-off were calculated. The start and end of the transition phase
7 were identified using the step-to-step changes in centre of mass height and segment angles.
8 Mean step-to-step changes of spatiotemporal and kinematic variables during each phase were
9 calculated. Firstly, the study showed that if sufficient trials are available, step-to-step changes
10 in shank and trunk angles might provide an appropriate measure to detect sprint phases in
11 applied settings. However, given that changes in centre of mass height represent a more
12 holistic measure, this was used to sub-divide the sprints into separate phases. Secondly,
13 during the initial acceleration phase large step-to-step changes in touchdown kinematics were
14 observed compared to the transition phase. At toe-off, step-to-step kinematic changes were
15 consistent across the initial acceleration and transition phases before plateauing during the
16 maximal velocity phase. These results provide coaches and practitioners with valuable
17 insights into key differences between phases in maximal sprinting.

18

19 Key Words: acceleration phase; kinematics; sprint technique; coaching

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26 **Introduction**

27 The sprint running events have traditionally been sub-divided into acceleration, constant
28 velocity and deceleration phases (e.g. Volkov & Lapin, 1979). Due to the multidimensional
29 structure of the acceleration phase (Delecluse, 1997), the scientific (e.g. Delecluse, Van
30 Coppenolle, Willems, Diels, Goris, Van Leemputte & Vuylsteke, 1995; Nagahara,
31 Matsubayashi, Matsuo & Zushi, 2014b) and coaching (e.g. Dick, 1987; Seagrave, 1996;
32 Crick, 2014a) literature have further sub-divided the acceleration phase. For the purposes of
33 this paper, the naming convention used by Delecluse et al. (1995) will be adopted, where the
34 first and second acceleration phases will be referred to as the initial acceleration phase and the
35 transition phase, respectively. The transition phase is then followed by the maximal velocity
36 phase.

37

38 With performance-related factors differing between the phases in a sprint, Delecluse, Van
39 Coppenolle, Diels and Goris (1992) suggested that a good performance in one phase does not
40 guarantee good performance in other phases. An increased understanding of the
41 characteristics of the different phases in sprinting can provide important insights for coaches
42 and applied sport scientists of the changes in mechanics between phases of a maximal sprint.
43 However, with the specific length of each phase dependent on the athletes' ability (Delecluse,
44 1997), it is challenging to tailor training sessions to individual athletes. Recently, scientific
45 (e.g. Nagahara et al., 2014b) and coaching literature (e.g. Crick, 2014a) identified the use of
46 step-to-step progressions of postural measures to identify phases in maximal sprinting.

47

48 Using the step-to-step changes of the centre of mass height (CM-h), Nagahara et al. (2014b)
49 identified two breakpoint steps (approximately steps 4 and 14) which were used to subdivide
50 the sprint into three phases. Distinct changes were reported in spatiotemporal and kinematic

51 variables (Nagahara et al., 2014b) and external kinetics (Nagahara, Mizutani & Matsuo, 2016;
52 Nagahara, Mizutani, Matsuo, Kanehisa & Fukunaga, 2017a) as sprinters crossed from one
53 phase to the next. Similarly, coaching literature proposed that step-to-step progressions of
54 shank and trunk angles at touchdown are specific to each phase of a maximal sprint (Crick,
55 2014a). It is suggested that the initial acceleration phase ends when step-to-step changes in
56 shank angles end as the shank becomes perpendicular to the ground at touchdown (suggested
57 to be: steps 5-7; Crick, 2014b), while the transition phase ends when step-to-step changes in
58 trunk angle cease as the trunk becomes upright (suggested to be: step 17; Crick, 2014c).
59 However, considering that changes in CM-h represent a holistic measure of whole-body
60 changes it is unknown whether the first and second acceleration phases identified by
61 Nagahara et al. (2014b) will align with the initial acceleration and transition phases described
62 by Crick (2014a). This may have important practical implications to ensure the appropriate
63 alignment of information that is shared between researchers, coaches and applied sport
64 scientists.

65

66 Performance during sprint acceleration depends on the net anteroposterior force generated
67 during ground contact, which directly influences the anteroposterior centre of mass (CM)
68 acceleration (Rabita, Dorel, Slawinski, Sàez de Villarreal, Couturier, Samozino & Morin,
69 2015). Theoretically, the orientation of the sprinter (i.e. the vector connecting the sprinter's
70 CM to the contact point with the ground (CM-angle) is mechanically related to their
71 acceleration (di Prampero, Fusi, Sepulcri, Morin, Belli & Antonutto, 2005). As sprinters
72 assume a more forward-inclined CM-angle during the initial acceleration phase,
73 anteroposterior CM acceleration is larger compared with the later phases of a sprint when
74 sprinters adopt a less forward-inclined posture. However, the CM-angle depends on both the
75 CM-h and the anteroposterior distance between the contact point and the CM, which in turn

76 are dependent on the orientation of the segments of the stance leg and trunk. Thus, knowledge
77 of the step-to-step changes in segment angles of the stance leg and trunk are important to
78 understand how sprinters' orientation and CM acceleration changes to address the
79 requirements of the different sprint phases.

80

81 An understanding of the evolution whole-body posture and segment orientations during
82 acceleration can have important implications for developing technical models of sprinting and
83 informing technical interventions. Therefore, the aim of this study was to investigate
84 spatiotemporal and kinematic changes between the initial acceleration, transition and
85 maximum velocity phases of a sprint. Two research questions were formulated; the first
86 research question – *‘how comparable are the sprint acceleration phases when identified using*
87 *different measures?’* aimed to compare and critically appraise the use of either CM-h
88 (Nagahara et al., 2014b) or shank and trunk angles (Crick, 2014a) to identify breakpoint steps
89 in sprint acceleration. The second research question – *‘how do step-to-step progressions of*
90 *spatiotemporal and kinematic variables differ between the initial acceleration, transition and*
91 *maximal velocity phases?’* aimed to characterise the technical changes throughout a maximal
92 sprint. It was hypothesised that; a) the sprint acceleration phases identified using changes in
93 CM-h will align with the phases identified using shank and trunk angles and b) there will be
94 large differences in step-to-step changes of the orientation of sprinters (i.e. CM-angle)
95 between the initial acceleration, transition and maximal velocity phases.

96

97 **Methods**

98 *Participants and procedures*

99 Following institutional ethical approval, three male and two female national-level sprinters
100 (Table 1) gave written informed consent to participate. Data were collected in March (after

101 the indoor season) and eight weeks later in May (early outdoor season) during participants'
102 regular training sessions.

103

104 ****Insert table 1 near here****

105

106 Prior to data collection, the participants performed a coach-led warm-up. The warm-up
107 incorporated; dynamic stretching, sprint specific drills, and was concluded with 3-5 runs of
108 increasing intensity. The participants then performed up to three practice starts from the
109 starting blocks, before commencing with the data collection. Following the warm-up, data
110 were collected from five maximal 50 m sprints from blocks, with at least five minutes rest
111 between trials to ensure a full recovery. One sprinter (P3) only completed three sprints at the
112 second collection. Each sprint was started with '*on your marks*' and '*set*' commands,
113 followed by a manually triggered auditory starting signal. All participants wore sprinting
114 shoes and the testing was done on a Mondo track surface.

115

116 *Data collection set-up*

117 Five HDV digital cameras (1×Sony Z5; 2×Sony Z1; 2×Sony A1E, Sony, Tokyo, Japan) were
118 mounted on tripods at a height of 1.80 m and 19 m from the running lane (Cameras 1 – 5;
119 Figure 1). The cameras recorded in HD (1440 × 1080 pixels) at 50 Hz with an open iris and a
120 shutter speed of 1/600 s.

121

122 ****Insert figure 1 near here****

123

124 A sixth camera (Sony Z5) was set up perpendicular to the 25 m mark and 40 m away from the
125 running lane was panned during trials and used to identify touchdown and toe-off events. It

126 recorded in HD (1440×1080 pixels) at 200 Hz with an open iris and a shutter speed of
127 $1/600$ s. Two sets of 20 sequentially illuminating LEDs (Wee Beastie Electronics,
128 Loughborough, UK), which were synchronised to the starting signal, were used to
129 synchronise cameras 1 to 4 with the 200 Hz panning camera to within 0.001 s (Irwin &
130 Kerwin, 2006). Camera 5 was subsequently synchronised to camera 4 through calculation of a
131 time offset, which was based on the participants' CM position data from the overlap between
132 cameras 4 and 5. First, the time difference between cameras 4 and 5 was determined. Using
133 linear interpolation between two successive CM positions (0.020 s apart) from camera 4, the
134 time at the closest corresponding CM position from camera 5 was estimated. Secondly, the
135 time difference between cameras 4 and 5 was added to the camera 4's synchronisation data
136 from the LED synchronisation lights. This provided the necessary timing data needed to
137 synchronise camera 5 with the 200 Hz panning camera.

138

139 *Data reduction*

140 Videos were manually digitised in Matlab (The MathWorks Inc., USA, version R2014a)
141 using an open source package (DLTdv5, Hedrick, 2008). The data required for calibration
142 was obtained by digitising recordings of a vertical calibration pole with three spherical control
143 points (diameter of 0.100 m) which was moved sequentially through three to five known
144 locations across each camera's field of view (Figure 1). This allowed a $10.00 \text{ m} \times 2.17 \text{ m}$
145 plane to be calibrated for cameras 1 to 5 using an open source eight parameter 2D-DLT
146 (Meershoek, 1997) which was edited to include a ninth parameter to account for lens
147 distortion (Walton, 1981). The accuracy of spatial reconstruction was assessed by calculating
148 horizontal and vertical root-mean-squared differences (RMSD) between reconstructed and
149 known points within the calibrated plane. Across both days, reconstruction errors were
150 suitably low, ranging from 0.002 - 0.005 m.

151

152 From the panning camera videos, the touchdown and toe-off events were identified.
153 Touchdown was defined as the first frame when the foot was visibly on the ground, while toe-
154 off was defined as the first frame when the foot was visibly off the ground. The identification
155 of touchdown and toe-off was repeated three times for each trial with at least five days
156 between repetitions. The events identified consistently on at least two separate occasions were
157 used in subsequent processing as the touchdown and toe-off events. Static camera videos were
158 digitised for two frames around each touchdown (last frame before and the first frame of
159 ground contact) and toe-off (last frame before and the first frame of flight) (Bezodis, Kerwin
160 & Salo, 2008). Sixteen body landmarks were digitised: vertex and seventh cervical vertebra
161 (C7), then both hips, shoulders, elbows, wrists, knees, ankles and metatarsophalangeal (MTP)
162 joint centres. Furthermore, the distal end of the contact foot (i.e. the toe) was digitised for
163 three consecutive frames while the foot was on the ground. These three consecutively
164 digitised frames were later averaged during data processing to provide a measure for the
165 position of the front of the shoe during ground contact. To better approximate spatiotemporal
166 data at touchdown and toe-off, event times from the 200 Hz panning camera were
167 synchronised to the data from the static cameras using the LED synch lights (Figure 1) or a
168 least squares fit to the touchdown and toe-off events. Overall, data from all cameras could be
169 synchronised to the nearest 0.002 s. The coordinate positions of each of the digitised points at
170 the 200 Hz touchdown and toe-off events were calculated via linear interpolation between the
171 two frames digitised around touchdown and toe-off.

172

173 To evaluate the reliability of digitising, one trial was re-digitised three times. Variables of
174 interest were calculated from the three sets of digitisations. The absolute and relative
175 (expressed as a percentage of the absolute RMSD relative to variables range across the trial)

176 RMSDs between all re-digitisations were calculated for the variables measured. A relative
177 RMSD below 5% was selected as a cut-off for a variable to be deemed reliable. The reliability
178 analysis revealed acceptably low uncertainties with RMSDs of $0.03 \text{ m}\cdot\text{s}^{-1}$ (relative RMSD:
179 0.6%) for step velocity, between 0.005 - 0.010 m (relative RMSD: 0.0% - 2.9%) for height
180 and distance variables, 0.02 Hz (relative RMSD: 2.0%) for step frequency and between 1° - 2°
181 (relative RMSD: 0.8% - 3.9%) for angular variables. The reliability of the variables was
182 therefore deemed acceptably low to identify step-to-step changes during the sprinting trials.

183

184 *Data processing*

185 The CM at touchdown and toe-off was calculated using segmental inertia data from de Leva
186 (1996) apart from the foot segment for which Winter's (2009) data were used, with the added
187 mass of each athlete's running shoe. Event times, and CM and joint centre locations at
188 touchdown and toe-off were used to calculate the following variables:

189

190 *Sprint Performance [s]*: Time at 50 m minus reaction time. The 50 m time was calculated as
191 the time when the participants' CM reached 50 m, using a fourth-order polynomial, which
192 was fit through all consecutive touchdown and toe-off CM locations from step 1 onwards.
193 Reaction time was determined from the 200 Hz panning camera as the moment when the
194 participants showed the first visible movement in the starting blocks following the start signal.

195

196 *Spatiotemporal variables*: A step was defined from touchdown to the subsequent contralateral
197 touchdown. Step velocity (m/s) was the anteroposterior CM displacement between two
198 consecutive touchdowns divided by the time between the touchdown events. Step length (m)
199 was the anteroposterior displacement of the CM between two consecutive touchdowns, while
200 step frequency (Hz) was the inverse of step time from the panning camera touchdown events.

201 Contact time (s) was calculated by subtracting the touchdown time from the subsequent toe-
202 off time. Flight time (s) was calculated by subtracting the toe-off time from the subsequent
203 touchdown time. Contact distance (m) was calculated as the difference between the
204 anteroposterior positions of the CM at touchdown and subsequent toe-off. Touchdown
205 distance (TD distance, m) was the anteroposterior distance between the MTP and CM at
206 touchdown while toe-off distance (TO distance, m) was the anteroposterior distance between
207 the CM at toe-off and the average toe position during contact. Negative touchdown and toe-
208 off distances represented the CM in front of the contact point. The flight distance (m) was
209 calculated by subtracting the CM position at touchdown from the CM position at the
210 preceding toe-off event.

211

212 *Kinematics:* Segment angles [$^{\circ}$] were defined between the horizontal forward line and the
213 vector created from the distal to proximal segment endpoints. CM, trunk (θ_{trunk}), thigh (θ_{thigh})
214 and shank (θ_{shank}) angles at touchdown and toe-off were calculated.

215

216 Data from each camera were combined into the full 50 m sprint trial. Since all participants
217 performed at least 25 steps within the 50 m sprint, steps 1-25 were analysed further.

218

219 *Phase identification*

220 Phase identification was based on identifying breakpoint steps at the start of transition (T_{start})
221 and maximal velocity (MV_{start}) phases, respectively. The initial acceleration phase occurred
222 between step one and the step preceding T_{start} , while the transition phase occurred between
223 T_{start} and the step preceding MV_{start} . The maximal velocity phase was defined from MV_{start} to
224 step 25. It must be acknowledged that this study will define the maximal velocity phase based
225 on kinematic characteristics generally associated with this phase of the events (i.e. upright

226 posture; e.g. Crick. 2014c) and therefore running velocity may show a small change during
227 this phase. In order to address the first research question, T_{start} and MV_{start} were both identified
228 using multiple approaches.

229

230 T_{start} : This breakpoint step was identified from step-to-step increases in touchdown CM-h (TD
231 CM-h) and touchdown shank angle (TD shank angle). Based on previous literature (e.g.
232 Delecluse et al., 1995; Nagahara et al., 2014b; Crick, 2014b), T_{start} was predicted to occur
233 within the first 10 steps. Therefore, to remove the influence of subsequent data, only the first
234 10 steps of the sprint were used. A modified method involving multiple straight-line
235 approximation was used to identify T_{start} (see Nagahara et al., 2014b for further details).

236

237 MV_{start} : This breakpoint step was identified based on step-to-step increases in TD CM-h and
238 touchdown trunk angle (TD trunk angle). To remove the influence of data points from the
239 start of the trial, only data from step eight onwards were used (Nagahara et al., 2014b). A
240 method using two first order polynomials was used to identify MV_{start} (see Nagahara et al.,
241 2014b for further details).

242

243 *Data analysis*

244 To address the first research question, and identify breakpoints during maximal sprint
245 acceleration, all trials from both days were used. This allowed a more robust and thorough
246 comparison of the measures used to subdivide the acceleration phase across a range of
247 athletes, trials and sessions. The differences in T_{start} (calculated using either TD CM-h or TD
248 shank angle) and MV_{start} (calculated using either TD CM-h or TD trunk angle) were quantified
249 by calculating an RMSD between respective measures for each participant on each day.

250

251 To address the second research question, each participant's best trial from each day was
252 selected based on 50 m times. This allowed the investigation of the step-to-step technical
253 changes associated with only the best performances from each sprinter in the sample. The
254 measure identified as 'most appropriate' from research question 1 was then used to identify
255 T_{start} and MV_{start} breakpoint steps to address research question 2. T_{start} and MV_{start} breakpoint
256 steps identified from the best trials were used to identify the steps occurring in the initial
257 acceleration, transition and maximal velocity phases of the most successful sprints. Following
258 the identification of T_{start} and MV_{start} , the step-to-step data profiles were smoothed using a
259 Hanning three-point moving averages algorithm (Grimshaw, Fowler, Lees & Burden, 2004).

260

261 Mean step-to-step changes across the steps within the initial acceleration (IAP), transition
262 (TP) and maximal velocity phases (MVP) were calculated for each variable, across each trial.
263 Magnitude-based inferences (MBI; Batterham & Hopkins, 2006) were used to quantify
264 meaningful differences between each participants' mean step-to-step changes between the
265 phases. Differences between means (phases: TP-IAP; MVP-IAP; MVP-TP) were calculated
266 using the post-only crossover spreadsheet (Hopkins, 2006) with a confidence interval (CI) of
267 97%. The smallest worthwhile change was an effect size of 0.2 (Hopkins, 2004; Winter, Abt
268 & Nevill, 2014). Effect sizes were quantified using the following scale: <0.19 (trivial), 0.20-
269 0.59 (small), 0.60-1.19 (moderate), 1.20-1.99 (large), 2.00-3.99 (very large) and >4.00
270 (extremely large; Hopkins, Marshall, Batterham & Hanin, 2009). The probability (percentage
271 and qualitative description) that the differences were larger than 0.20 was defined as; possibly
272 25-75% (*); likely: 75-95% (**); very likely: 95-99.5% (***) and most likely >99.5% (****;
273 Hopkins et al., 2009). When the outcome of the effect had a >5% chance of being positive and
274 negative, the effect was described as unclear. Median, interquartile range and range of

275 step-to-step changes within each phase were calculated across all ten trials and presented in
276 box and whisker plots.

277

278 **Results**

279 Ranges of performance (50 m time) and the identified breakpoint steps are presented in Table
280 2. Only P1 (6.13-6.07 s) and P3 (5.90-5.89 s) improved on their best performance from day 1
281 to 2. The RMSD between T_{start} identified using TD CM-h or TD shank angles ranged from
282 0.8-2.1 steps, whilst the RMSD between MV_{start} identified using TD CM-h or TD trunk angles
283 ranged from 1.3-2.3 steps (Table 2). The within-participant ranges of T_{start} steps identified
284 averaged 1.9 steps using TD CM-h and 2.2 steps using TD shank angles. Ranges of MV_{start}
285 steps identified averaged 2.8 steps using TD CM-h and 2.6 steps using TD trunk angles.

286

287 ****Insert table 2 near here****

288

289 To address the second research question, the ranges of T_{start} and MV_{start} steps based on the
290 step-to-step changes in TD CM-h were identified from each participants' best trials and used
291 to sub-divide the whole 50 m sprint into three distinct phases, which had no possible overlap
292 (see shaded areas on Figures 2-4). The initial acceleration phase therefore comprised steps
293 one to three, the transition phase steps six to 13, and the maximal velocity phase steps 17 to
294 25. T_{start} was associated with step velocities of 6.06 to 7.83 m/s (65 to 77% V_{max} , which was
295 8.86 to 10.73 m/s), while the MV_{start} was associated with step velocities of 8.19 to 10.07 m/s
296 (92 to 98% V_{max}).

297

298 Over the 25 steps, the largest step-to-step changes in step velocity, step length and step
299 frequency (Figure 2) occurred during the initial acceleration phase (i.e. steps 1 to 3), with

300 extremely large step-to-step increases in step velocity and step length and trivial to very large
301 step-to-step increases in frequency compared to the transition and maximal velocity phases.
302 During the transition phase, mean step-to-step increases in step velocity were extremely large,
303 mean increases in step length were large to very large and mean changes in step frequency
304 were trivial to small compared to the maximal velocity phase.

305

306 ****Insert figure 2 near here****

307

308 The initial acceleration phase was characterised by small to very large changes in contact
309 times, flight times, contact distances, flight distances and touchdown distance compared to the
310 transition and maximal velocity phases (Figure 3). During the transition phase, step-to-step
311 changes in contact distances (Figure 3e) plateaued or started decreasing as increases in
312 touchdown distances (0.01 to 0.02 m per step; Figure 3m&n) were equal to or smaller than
313 decreases in toe-off distances (0.01 to 0.03 m per step; Figure 3o&p). During the maximal
314 velocity phase, flight times and flight distances continued to show small step-to-step
315 increases. Mean step-to-step increases in touchdown and toe-off CM-h were very large to
316 extremely large between the initial acceleration and the transition phases and small to large
317 between the transition and maximal velocity phases.

318

319 ****Insert figure 3 near here****

320

321 Step-to-step changes in touchdown CM-angle were most likely large to very large between
322 the initial acceleration phase and both later phases, but most likely only small between the
323 transition and maximal velocity phases (Figure 4). Changes in toe-off CM-angle were most

324 likely moderate to very large between the maximal velocity phase and both preceding phases,
325 and very likely small to very large between the initial acceleration and transition phases.

326

327 ****Insert figure 4 near here****

328

329 **Discussion and Implications**

330 Increased understanding of the technical changes associated with different phases in sprinting
331 is important to facilitate the development of technical models of sprinting. Therefore, the aim
332 of this study was to investigate spatiotemporal and kinematic changes between the initial
333 acceleration, transition and maximum velocity phases of a sprint. To address this aim, two
334 research questions were developed.

335

336 Firstly, to compare different measures previously proposed in scientific (Nagahara et al.,
337 2014b) and coaching literature (Crick 2014a), the first research question - '*how comparable*
338 *are the sprint acceleration phases when identified using different measures?*' was addressed.

339 The within-trial RMSD analysis revealed differences up to 2.3 steps between for the T_{start} and
340 MV_{start} steps identified using the different variables. Hypothesis a) that the sprint acceleration
341 phases identified using changes in TD CM-h will align with the phases identified using shank
342 and trunk angles was therefore rejected. Although relatively low, these RMSD step
343 differences are ultimately due to other segments than the shank and trunk changing
344 independently and therefore influencing the TD CM-h. Furthermore, bilateral differences,
345 which have previously been reported in maximal sprinting (Exell, Gittoes, Irwin & Kerwin,
346 2012) could have contributed to these RMSD step differences. While the within-trial analysis
347 revealed that different T_{start} and MV_{start} steps were identified when using either TD CM-h or
348 touchdown segments angles, both measures did provide similar ranges of T_{start} and MV_{start}

349 steps across multiple trials. Therefore, using segment angles in applied settings, where the
350 speed of feedback is often an important factor may be an appropriate substitute provided that
351 these data are based on multiple trials (at least three trials per participant). However, since TD
352 CM-h provides a more robust and holistic measure that is more representative of the overall
353 postural changes and changes in CM acceleration, this measure is more appropriate for
354 identifying T_{start} and MV_{start} and was therefore subsequently used to address research question
355 2.

356

357 To understand technical differences between phases, the second research question – ‘*how do*
358 *step-to-step progressions of spatiotemporal and kinematic variables differ between the initial*
359 *acceleration, transition and maximal velocity phases?*’ was examined. Using TD CM-h, steps
360 one to three were defined as the initial acceleration phase, steps 6-13 the transition phase, and
361 steps 17-25 the maximal velocity phase. Standardised differences in mean between-step
362 increases of the CM-angle between the initial acceleration and transition phases were very
363 large (ES confidence interval: 1.30 to 3.80) for touchdown angles and large (ES confidence
364 interval: 0.33 to 2.31) for toe-off angles. Comparing the transition and maximal velocity
365 phases, standardised differences in mean step-to-step increases of CM-angles were small (ES
366 confidence interval: 0.27 to 0.53) for touchdown angles and very large (ES confidence
367 interval: 1.16 to 2.14) for toe-off angles. Based on this, hypothesis b) that there will be large
368 differences in step-to-step changes of CM-angle between the initial acceleration, transition
369 and maximal velocity phases, was only partially accepted. These changes in touchdown and
370 toe-off CM-angles provide some important insight into the initial acceleration and transition
371 phases.

372

373 The more forward-inclined orientation of the participants (i.e. smaller touchdown and toe-off
374 CM-angles; Figure 4a&c) during the initial acceleration phase compared to the transition
375 phase is indicative of the capacity to generate larger net anteroposterior forces (Kugler &
376 Janshen, 2010; Rabita et al., 2015) during this phase. This explains the extremely large
377 step-to-step increases in step velocity during initial acceleration (median 0.88 m/s per step;
378 Figure 2a&b) compared to the transition phase (median 0.24 m/s per step). Additionally, these
379 extremely large increases in step velocity during the initial acceleration phase were achieved
380 through extremely large increases in step length and trivial to very large increases in step
381 frequency, compared to the transition phase. Previous research has reported that across a
382 group of sprinters, performance during the initial acceleration phase is dependent on large
383 increases in step frequency (Nagahara et al., 2014a) and that within athletes, better
384 performances were influenced by larger magnitudes of step frequency throughout the
385 acceleration phase (Nagahara, Mizutani, Matsuo, Kanehisa & Fukunaga, 2017b). Ultimately,
386 the magnitude of the step frequency, which is determined by the sum of contact and flight
387 times, is an important determinant of step velocity. The ability to quickly increase step
388 frequency during the initial acceleration phase (Debaere et al., 2013; Nagahara et al., 2014a)
389 may be an important characteristic of this phase compared to the transition and maximal
390 velocity phases. In the current study, the large step-to-step increases in step frequency
391 (median 0.12 steps·s⁻¹ per step; Figure 3a&b) during the initial acceleration phase were due to
392 larger decreases in contact times (median -0.020 s per step; Figure 3a&b) relative to the
393 increases in flight times (median 0.012 s per step; Figure 3a&b). As contact times are related
394 to running velocity (Hunter et al., 2004), shorter contact times are dependent on larger
395 running velocities which can be achieved by applying larger propulsive impulses during
396 preceding steps (Nagahara et al., 2017b). Therefore, as a sprinter's ability to generate larger
397 propulsive forces during the initial acceleration phase increases, their larger change in running

398 velocity will result in larger decreases in contact times which could allow them to achieve
399 larger increases in step frequency.

400

401 During the transition phase, further increases in step velocity were mainly due to step-to-step
402 increases in step length, which in turn resulted from further increases in flight distance
403 (Figure 3g). Previous research has demonstrated that flight distance is determined by the
404 anterior and vertical CM velocity at toe-off, the latter of which is also the main determinant of
405 flight time (Hunter et al., 2004). Therefore, as step velocities increase, sprinters need to
406 increase the magnitude of vertical force production to facilitate a decrease in contact times
407 (Figure 3a) without impeding step-to-step increases in CM-h (Figure 3i) and flight times
408 (Figure 3c). However, since a more forward-inclined GRF vector (Rabita et al., 2015;
409 Nagahara, Mizutani, Matsuo, Kanehisa & Fukunaga, 2017a) and a smaller vertical impulse
410 predicts better acceleration performance (Nagahara et al., 2017a), there likely exists an ideal
411 magnitude of vertical force that facilitates increases in step velocity without negatively
412 affecting step frequency through excessively long flight times.

413

414 Segmental changes that influence changes in CM-angle can provide an insight into how
415 sprinters adjust force production. During the initial acceleration phase, the relatively large
416 step-to-step increases in touchdown CM-angle, compared to the transition phase, were
417 influenced by increases in shank (median 9° per step) and trunk angles (median 4° per step).
418 These results align with the coaching literature, which suggests that during the initial
419 acceleration phase, experienced sprinters show step-to-step changes in shank angles of
420 between 6 to 8° per step (Crick, 2014b). These increased touchdown variables during the
421 initial acceleration phase could ultimately contribute to the decrease in the anterior forces
422 sprinters can generate during subsequent ground contacts. This may be due to the increases in

423 shank and trunk angles could result in larger touchdown distances, which have been
424 previously linked to larger braking forces (Hunter, Marshall & McNair, 2005). Additionally,
425 the relatively large step-to-step increases in CM-h (Figure 3i&k) and trunk angles (Figure
426 4e&g) during the initial acceleration phase could influence the increasing toe-off CM-angles
427 (Figure 4c) and therefore the capacity to generate large propulsive forces (e.g. di Prampero et
428 al., 2005; Kugler & Janshen, 2010). Although a decreased touchdown distance has been
429 shown to be beneficial during the first step of a sprint (Bezodis, Trewartha & Salo, 2015), the
430 large magnitude of step-to-step increases in TD variables may ultimately reflect a requirement
431 to generate larger magnitudes of vertical force and therefore flight times (Figure 3c) as a
432 sprint progresses. Previous research from the maximal velocity phase of sprinting suggested
433 that sprinters generate larger vertical forces early during ground contact due to their upright
434 trunk and extended hip and knee joint, which provide increased stiffness at touchdown (Clark
435 & Weyand, 2014). Similarly, during earlier sprint phases, the increasing TD CM-angle
436 (Figure 4a), TD CM-h (Figure 3i) and more extended hip and knee joints due to the increasing
437 TD trunk (Figure 4e) and shank (Figure 4m) angles could increase the capacity to generate
438 vertical force early during ground contact and therefore minimise the loss in CM-h
439 immediately following touchdown.

440

441 At toe-off, the CM-angle increased during both the initial acceleration (median 2° per step;
442 Figure 4c&d) and transition phases (median 1° per step; Figure 4c&d). Although smaller CM-
443 angles at toe-off could facilitate larger propulsive force production (Kugler & Janshen, 2010),
444 the step-to-step increases in toe-off CM-angle may be unavoidable given the increases in
445 touchdown CM-angles, CM-h, trunk angles and decreases in contact times. Coaching
446 literature proposed trunk angle and changes in trunk angle as an important factors influencing
447 anterior force production during sprinting (Crick, 2014c), and suggested that better sprinters

448 likely show smaller step-to-step increases in trunk angles (Crick, 2014c). Ultimately, the
449 increasing trunk angle (Figure 4e&g) during the initial acceleration and transition phases may
450 play an important role in influencing the toe-off CM-angle by limiting the anterior rotation of
451 the thigh (Figure 4k) and therefore contribute to the increases in toe-off distances (Figure 3e).
452 This could ultimately contribute to the decreasing magnitude of propulsive forces sprinters
453 can generate as a sprint progresses (e.g. Nagahara et al., 2017a).

454

455 Compared to the initial acceleration and transition phases, the maximal velocity phase was
456 characterised by small to negligible step-to-step changes in many spatiotemporal (Figure
457 2&3) and kinematic variables (Figure 4). At MV_{start} , participants had reached 92-98% of
458 maximal velocity. These results show parity with the British Athletics technical model, which
459 suggests that world-class sprinters reached 95% of maximal velocity at MV_{start} (Crick, 2014c).
460 The participants still showed small increases in step velocity (Figure 2a) which suggests that
461 the participants maintained a positive net anterior impulse during the maximal velocity phase.
462 This was further reflected in the small increases in flight distances (Figure 3g) and therefore
463 step lengths (Figure 2c) which continued throughout the maximal velocity phase. This
464 supports the results by Ae et al. (1992) who reported that step length increases continue
465 throughout a sprint. These results could be explained by the upright trunk and high knee lift,
466 which are associated with this phase of sprinting and allow sprinters a longer path to
467 accelerate their foot down and backwards prior to touchdown. This would contribute to
468 increasing vertical force production earlier during ground contact (Clark & Weyand, 2014)
469 and reduced braking forces (Hunter et al., 2005). The upright posture of sprinters is thought to
470 benefit the mechanics during late swing and early ground contact (i.e. 'front side mechanics';
471 Mann, 2007, p. 86) and vertical force production (e.g. Clark & Weyand, 2014) during the
472 maximal velocity phase. However, the increasing trunk angle as a sprint progresses might

473 provide an unavoidable constraint limiting toe-off distances and therefore the magnitude of
474 propulsive forces sprinters can theoretically generate. Therefore, as a sprint progresses
475 through the initial acceleration, transition and maximal velocity phases, sprinters may have a
476 greater ability to manage touchdown rather than toe-off mechanics in an attempt to influence
477 performance.

478

479 Despite having five participants in this study, the parity of the results with previous scientific
480 and coaching literature as well as the between-participant consistency regarding the step-
481 to-step changes in the different variables provides confidence in the applicability of this data
482 to investigate changes associated with maximal sprinting. The results presented in the current
483 study provide important insights to increase understanding of the differences between phases
484 in maximal sprinting. Overall, the changing spatiotemporal and kinematic variables through
485 the different phases have important implications for the performance of the sprinters. The
486 changes in CM-h and CM-angle suggest that participants increased vertical force production
487 through changes in touchdown mechanics, while changes in toe-off mechanics suggest an
488 unavoidable limiting feature that dictates decreases in propulsive force production as a sprint
489 progresses. Finally, while breakpoints were identified to define the initial acceleration,
490 transition and maximal velocity phases, this study did not investigate how differences in the
491 location of the breakpoint points between different trials were associated with differences in
492 spatiotemporal and kinematic variables. While the aim of this study was to investigate
493 differences between the phases of a sprint, an investigation of how changes in breakpoints are
494 related to spatiotemporal and kinematic variables may represent a future avenue of research.

495

496 **Conclusions**

497 The current study has developed an understanding of the technical changes associated with
498 the different phases of a maximal sprint. As long as a sufficient number of trials are available
499 for analysis (at least three), using shank and trunk angles may represent an appropriate
500 measure to detect breakpoint steps in applied settings. However, CM-h represents a more
501 holistic measure of overall postural changes, which links to the centre of mass acceleration,
502 and therefore provides a more robust measure to identify phases during maximal sprinting.
503 This analysis revealed important changes in whole body posture that may be linked to force
504 production, which would ultimately determine the increases in step velocity associated with
505 the initial acceleration phase compared to the transition and maximal velocity phases. These
506 results provide coaches and practitioners with valuable insights into key differences between
507 phases in maximal sprinting.

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Table 1. Participant characteristics.

ID	Age	Gender	Stature [m]	Body Mass [kg]	60 m/100 m PB [s]
P1	27	Male	1.89	89.1	6.99/10.87
P2	20	Male	1.79	73.5	6.80/10.64
P3	19	Male	1.79	72.0	6.86/10.71
P4	20	Female	1.76	69.4	7.65/12.34
P5	25	Female	1.71	63.3	7.61/11.90

651

Table 2. Ranges of performance times, maximal step velocities and breakpoint steps identified for each participant on each day. RMSD values are presented between T_{start} steps identified using either TD CM-h or TD shank angles, and between MV_{start} steps identified using either TD CM-h or TD trunk angles. Data are based on all available trials for each participant.

Participant	Day	50 m time (s)	Range of maximum Step Velocities (m/s)	T_{start}			MV_{start}		
				TD CM-h	TD θ_{shank}	TD CM-h vs. TD θ_{shank}	TD CM-h	TD θ_{trunk}	TD CM-h vs. TD θ_{trunk}
P1	1	6.13 – 6.21	9.59 – 9.93	5-7	3-6	1.6	14-17	15-18	1.3
	2	6.07 – 6.15	9.82 – 10.20	3-5	3-6	1.5	13-17	15-17	1.4
P2	1	5.86 – 5.94	10.53 – 10.76	3-5	3-5	1.2	14-15	14-16	1.6
	2	5.98 – 6.01	10.35 – 10.56	3-6	3-6	0.8	13-15	12-16	2.0
P3	1	5.90 – 5.96	10.53 – 10.61	3-4	3-6	2.1	15-17	17-18	2.3
	2	5.89 – 5.94	10.40 – 10.63	4-5	4-6	1.3	14-17	14-17	1.3
P4	1	6.78 – 6.90	8.83 – 9.04	3-5	5	1.1	12-17	14-15	1.6
	2	6.83 – 7.06	8.56 – 8.86	5-6	3-5	1.1	13-16	14-19	1.7
P5	1	6.63 – 6.75	8.99 – 9.15	4-7	4-6	1.1	14-16	13-17	2.0
	2	6.75 – 6.78	8.96 – 9.10	5-7	4-6	0.9	14-17	13-15	1.7
All	1			3-7	3-6	1.5	12-17	13-18	1.8
	2			3-7	3-6	1.1	13-17	12-19	1.7

Note: SV: step velocity, TD CM-h: touchdown centre of mass height, TD θ_{shank} : touchdown shank angles, TD θ_{trunk} : touchdown trunk angles, T_{start} : step representing the start of the transition phase, MV_{start} : step representing the start of the maximal velocity phase.

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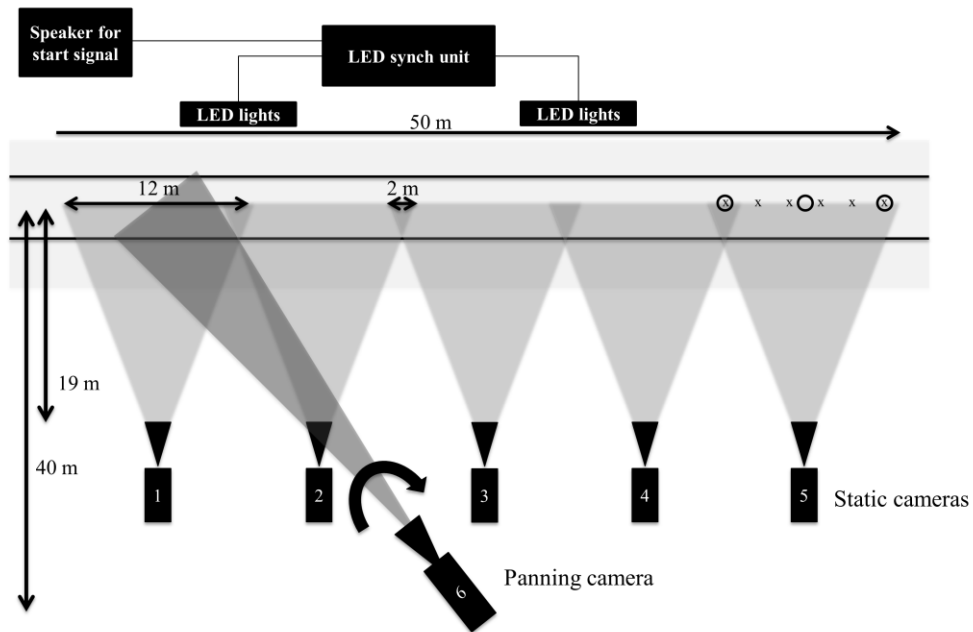


Figure 1. Camera and synchronisation light set-up (not to scale). An example of the camera calibration points for days 1 (O) and 2 (X) are shown in camera 5's field of view. This was repeated for all five static cameras. The direction of travel was from left to right.

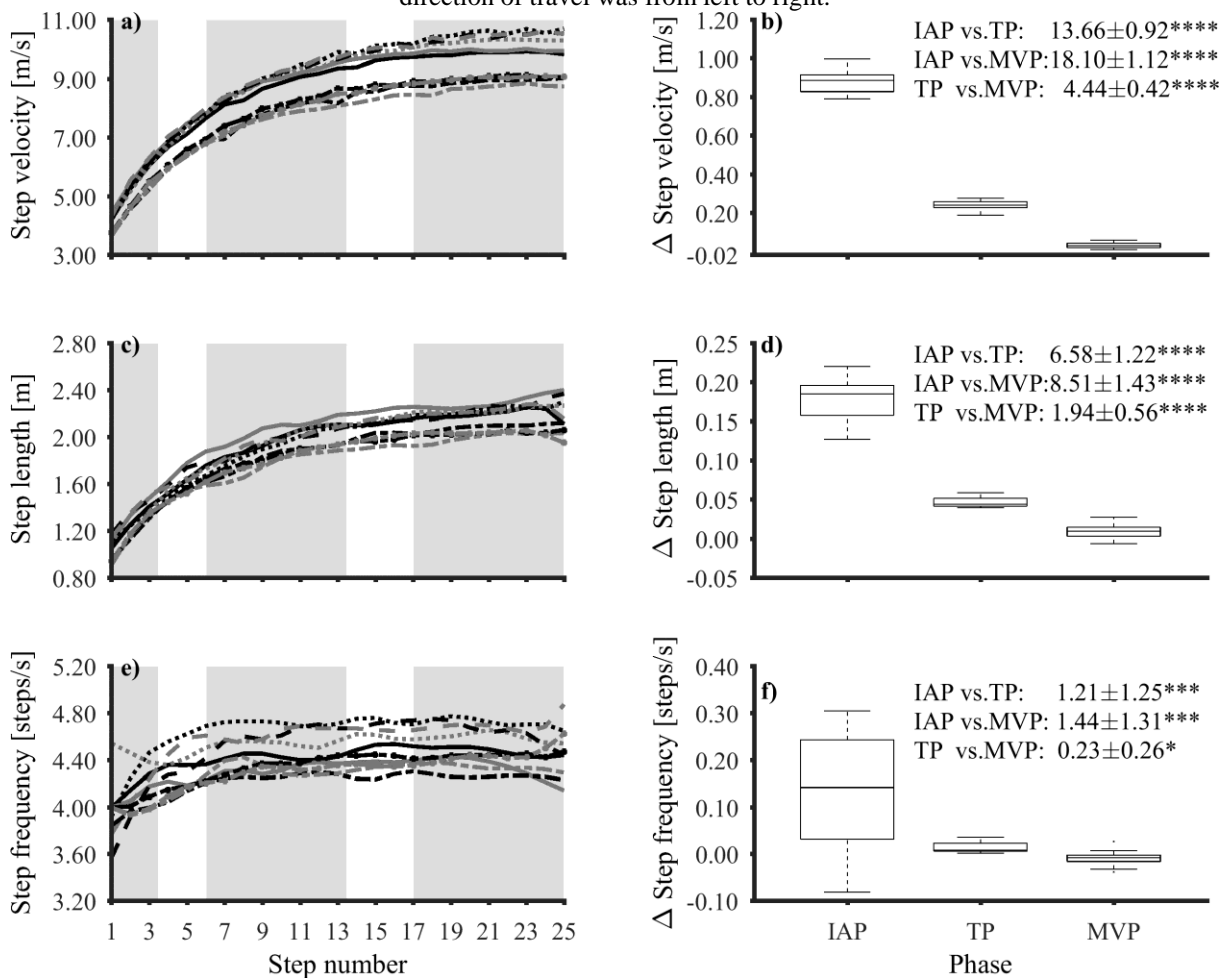


Figure 2. Step-to-step step velocity (a), step length (c) and step frequency (e) profiles of the participants' best 50 m sprints from day 1 (black) and day 2 (grey). Each participant is represented by particular line style. Grey columns highlight the initial acceleration, transition and maximal velocity phases. Box and whisker plots, figures b, d, f show the median, interquartile range and range of between step changes during the initial acceleration,

transition and maximal velocity phases. Magnitude-based inference results presented on figures b, d and f show the mean standardised effect \pm 90% confidence interval. The probability that the differences were bigger than the smallest worthwhile change (i.e. 0.20) was defined by: unclear (no stars), possibly (*); likely (**); very likely (***) and most likely (****).

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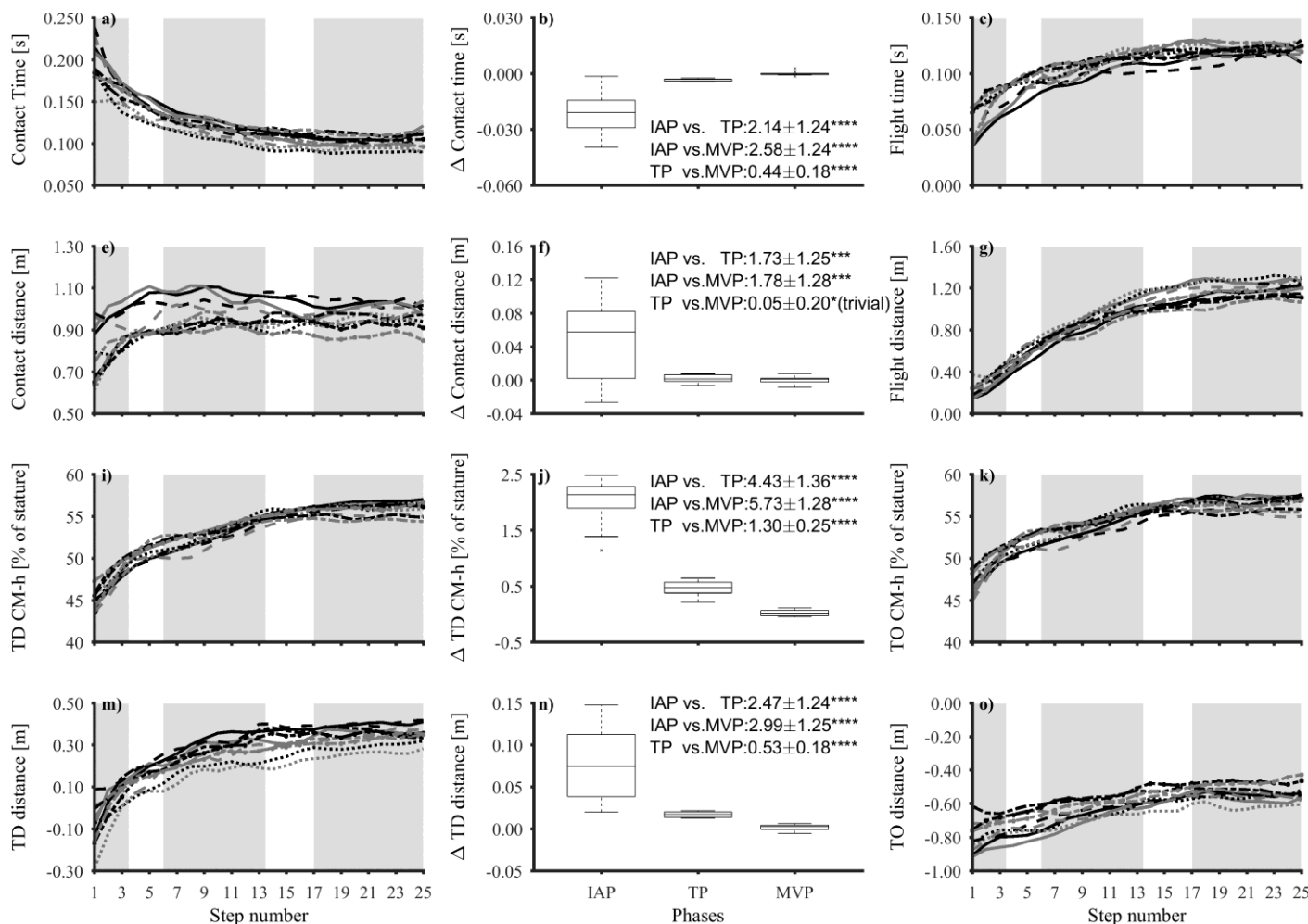


Figure 3. Step-to-step contact times (a), flight times (c), contact distance (e), flight distance (g), TD CM-h (i), TO CM-h (k), TD distance (m), and TO distance (o) for the participants best 50 m sprint from day 1 (black) and day 2 (grey). Each participant is represented by particular line style. Grey shaded regions indicate transition and maximal velocity phases. Box and whisker plots, figures b, d, f, h, j, l, n and p show the median, interquartile range and whiskers for the initial acceleration, transition and maximal velocity phases. Magnitude-based inference results presented on figures b, d, f, h, j, l, n and p show the effect \pm 90% confidence interval. The probability that the differences were bigger than the smallest worthwhile change (i.e. 0.20) were: not likely (*); likely (**); very likely (***) and most likely (****).

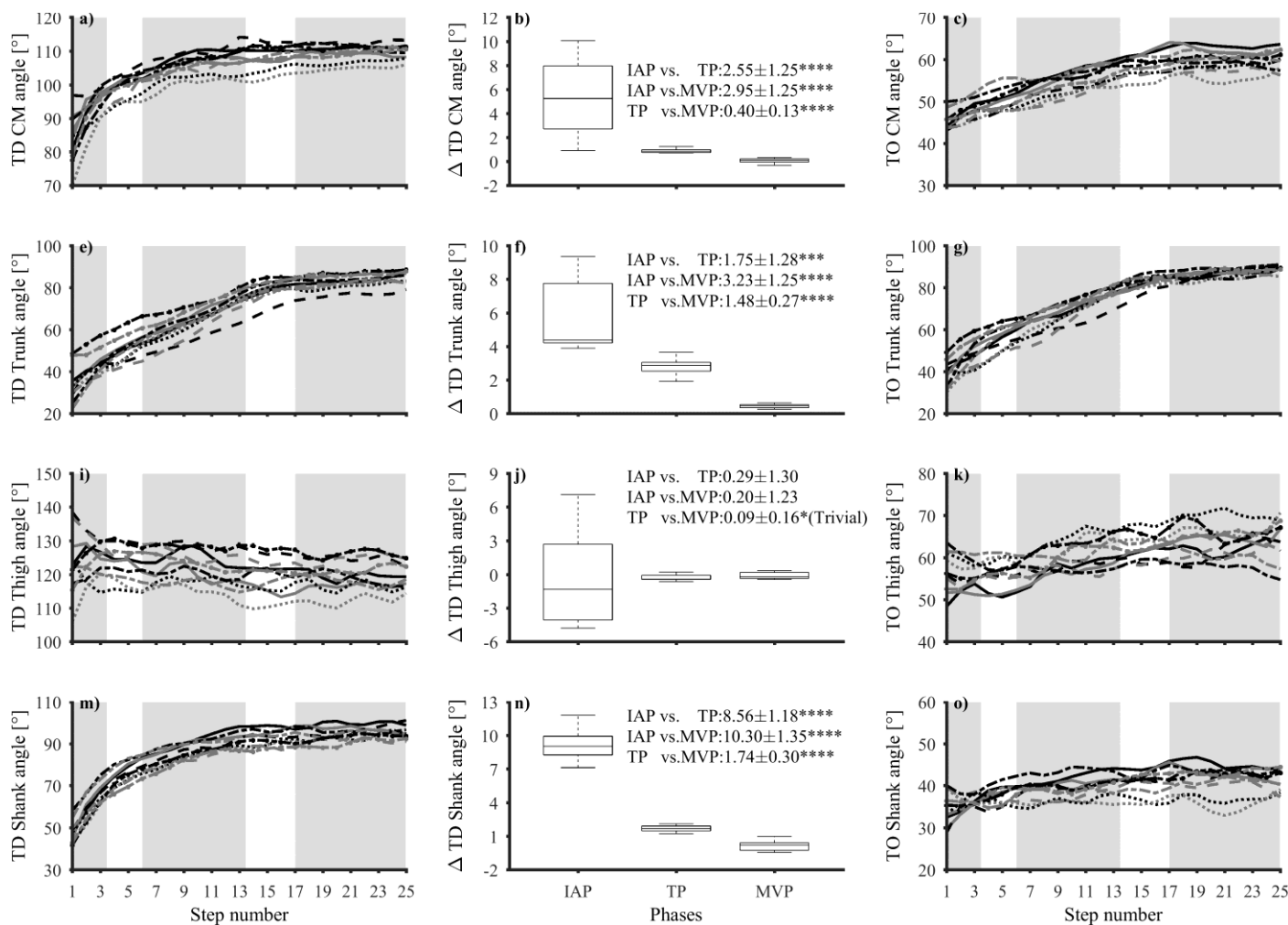


Figure 4. Step-to-step TD CM-angle (a), TO CM-angle (c), TD trunk angle (e), TO trunk angle (G), TD thigh angle (i), TO thigh angle (k), TD Shank angle (m), TO Shank angle (o) profiles of the participants best 50 m sprints from days 1 (black) and 2 (grey). Each participant is represented by particular line. Shaded grey vertical bars indicate the transition phases. Box and whisker plots, figures b, d, f, h, j, l, n and p show the median, 25th and 75th percentiles and whiskers represent the range of the data. Magnitude-based inference results presented on the right of the box plots show the mean standardised effect \pm 90% confidence interval. The probability that the differences were bigger than the smallest worthwhile effect (no stars), possibly (*); likely (**); very likely (***) and most likely (****).