### HIGH TEMPERATURE ELASTICITY OF FLUORIDE

### AND OXIDE ANALOGUES

by

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"Beware of the man who works hard to learn something, learns it and finds himself no wiser than before ..... He is full of murderous resentment of people who are ignorant without having come by their ignorance the hard way."

Kurt Vonnegut, Cat's Cradle.

The experimental programme reported in this thesis was carried out by the author in the Research School of Earth Sciences, A.N.U., from March 1972 to January 1976. Some of the material presented in Chapter 5 is a result of collaboration with Dr. R. C. Liebermann and was published in Jones and Liebermann (1974). All other discussions and interpretations are my own work except as acknowledged.

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#### ABSTRACT

The precise ultrasonic pulse superposition technique has been employed to determine the elastic moduli as a function of temperature from T = 298-650°K for single crystal fluorides crystallising in the rocksalt (LiF and NaF), fluorite (CaF<sub>2</sub>, SrF<sub>2</sub> and BaF<sub>2</sub>), rutile (MgF<sub>2</sub>) and perovskite (KMgF<sub>3</sub>) structures. The pressure derivatives of the elastic moduli were also measured for KMgF<sub>3</sub>. These new data are consistent with low temperature (T < 298°K) data obtained by other ultrasonic pulse techniques and are superior to previous high temperature data from resonance experiments. We employ these new data to consider the fluoride-oxide modelling scheme based on Goldschmidt's crystal chemical considerations and to evaluate the use of fluorides as models for the high temperature elastic behaviour of their oxide analogues.

The elastic moduli, c, are represented by quadratic functions in T over the experimental temperature range; however, the curvature is not in the same sense for all the crystals. For  $CaF_2$ ,  $SrF_2$ ,  $BaF_2$  and  $MgF_2$ , the curvature is consistent with the predictions of classical lattice dynamics that the c-T plot at constant volume should be linear in T at high temperatures. The behaviour of the c' and  $c_{11}$  modes for LiF and NaF contradicts these predictions. The fluorides do not appear to exhibit high temperature elastic behaviour at significantly lower absolute temperatures than their oxide analogues.

The bulk moduli of equivolume oxides and fluorides in a particular structure are scaled as  $4S^2$ , where  $S = Z^0/Z^F$  is the ratio of the effective unit charges and is approximately 75% for all the crystal structures. For the rocksalt-structure fluorides and oxides, the similar values for  $|(\partial c/\partial T)_p|$  for the members of an analogue pair and their decrease with increasing molar volume are explained in terms of nearest neighbour distance in a model incorporating Mitskevich's theory

with K-V systematics. Such similarities do not exist in the values of  $(\partial c/\partial T)_p$  for fluorides and oxides with the fluorite, rutile and perovskite structures and trends are absent for the last two structures. For compounds in all four structures,  $(\partial K_S/\partial T)_p$  is dominated by the extrinsic temperature dependence, whereas for  $(\partial \mu/\partial T)_p$ , the intrinsic is at least as important as the extrinsic contribution.

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### CHAPTER 1

### INTRODUCTION

1.1 Fluoride-oxide modelling scheme and its application to high temperature elasticity

1.2 Outline of thesis

### 1.3 Extent of publication

Laboratory elasticity studies which employ mitrasonic technique to determine the elastic wave velocities are limited in the arthinable competature and pressure range (T < 1200°C, P 5 40 kbar). The approac adopted in this thesis involves the study of analogue compounds under conditions screenible in the inboratory, to estimate the high pressure and high temperature proparties of earth-forming compounds.

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#### CHAPTER 1

#### INTRODUCTION

Seismological studies provide the most direct information on the earth's interior in the form of elastic wave velocities and density as a function of depth. Mineral physics, the application of the concepts and techniques of solid state physics to the study of materials of importance in geophysics, bridges the gap between petrological models of the earth's interior and earth models derived from seismological evidence. Knowledge of the elastic moduli and their pressure and temperature derivatives is important not only for establishing an equation of state for the earth, but also for examining detailed problems, such as the nature of the low-velocity zone and elastic wave velocities in the descending lithospheric slab at plate margins.

Laboratory elasticity studies which employ ultrasonic techniques to determine the elastic wave velocities are limited in the attainable temperature and pressure range (T <  $1200^{\circ}$ C, P < 40 kbar). The approach adopted in this thesis involves the study of analogue compounds under conditions accessible in the laboratory, to estimate the high pressure and high temperature properties of earth-forming compounds.

## 1.1 Fluoride-oxide modelling scheme and its application to high temperature elasticity

The concept of analogue compounds was first introduced on the basis of crystal chemical considerations by Goldschmidt (1927) who demonstrated that ionic size is one of the most important factors governing crystal structure. Ringwood (1970) has made extensive use of the germanates as high pressure models for the physical and crystal chemical properties of their silicate analogues. The larger size of the germanium ion with respect to silicon means that the germanates should transform to high pressure phases at lower pressures than the corresponding silicates. Germanates have also been useful as models for the elasticity of high pressure phases of silicates (e.g., Liebermann, 1972, 1974b, 1975).

Another aspect of Goldschmidt's (1927) modelling concept concerns fluoride and oxide analogue compounds and is also based on crystal chemical considerations: (a) the similarity in ionic radii of  $0^{2^-}$  and  $F^-$ ; (b) the applicability of the rigid ion model to compounds containing the  $0^{2^-}$  and  $F^-$  ions, which have relatively low polarisabilities resulting in their ionic radii being almost independent of co-ordination number; and (c) the correspondence of the crystal structures of oxide and fluoride compounds in which the cations are also of comparable ionic radii, but for which the cationic charge of the fluoride is half that of the oxide.

In the table below we illustrate the central feature of the entire modelling scheme: the similarity of the ionic radii of  $0^{2-}$  and  $F^{-}$  for various co-ordination numbers (after Shannon and Prewitt, 1969, 1970). The comparisons also demonstrate that the ionic radii of  $0^{2-}$  and  $F^{-}$  are almost independent of co-ordination number. Notable examples of simple

Co-ordination number	Ionic r 0 <sup>2-</sup>	adii (Å) F <sup>-</sup>
II	1.35	1.285
III	1.36	1.30
IV	1.38	1.31
VI	1.40	1.33

fluorides which exhibit structural correspondences are LiF-MgO (rocksalt structure),  $CaF_2$ -ThO<sub>2</sub> (fluorite structure),  $MgF_2$ -TiO<sub>2</sub> (rutile structure) and  $BeF_2$ -SiO<sub>2</sub> ( $\alpha$ -quartz and coesite structures). The relative ionic sizes for fluorides and oxides in the rocksalt structure are illustrated













Figure 1.1: Diagram of the cubic face layers for the rocksalt structure illustrating the relative ionic sizes for fluoride-oxide analogue pairs. The ionic radii and the interionic distances are to scale.

in Figure 1.1. In addition, a number of binary compounds with crystal structures of interest to geophysical discussions of the earth's interior are consistent with this modelling scheme and are listed in Table 1.1. Of particular interest is the close correspondence of the ionic radii of  $Be^{2+}$  and  $Si^{4+}$  (0.27Å and 0.26Å, respectively, for 4-fold co-ordination) (Shannon and Prewitt, 1969) which permits the fluoride-oxide modelling system to be extended to include fluoroberyllates and silicates. One disadvantage is that trivalent cations have no place in this scheme, so that it is difficult to model the corundum, ilmenite or garnet structures.

Goldschmidt (1927) also suggested that because of their lower ionic charge, fluorides should be "weakened" models of their oxide analogues, and thus be characterized by lower melting temperature, lower hardness and lower refractive index. In presenting the "weakened" model concept, Goldschmidt (1927) cited the melting points of the phenacites  $Li_2BeF_4$  (470°C) and  $Zn_2SiO_4$  (1510°C) to illustrate the greater temperature sensitivity of the physical properties of the fluorides. We list the ratios of the melting points of other fluorides to those of their oxide analogues,  $T_m^F/T_m^O$ , in Table 1.2; with the exception of MgF<sub>2</sub>-TiO<sub>2</sub>, this ratio is less than 0.6 for all of the analogue pairs. Investigations by Roy et al. (1953,1954) and by Thilo and Lehmann (1949) have demonstrated close similarities in the phase diagrams of binary fluoride and oxide systems at atmospheric pressure with the fluoride systems exhibiting much lower solidus and liquidus temperatures. Recently, Jackson and Liebermann (1974) have shown that the fusion curves of rocksalt fluorides and oxides at high pressure may be correlated in a similar manner. In a study which parallels that reported in this thesis, Jackson (1976) employed fluoride and oxide analogue systems in an investigation of phase equilibria and melting relationships.

The idea that the fluorides might be models for the high temperature elasticity of their oxide analogues was prompted by the

### Table 1.1:

Crystal Structure	Fluoride	Oxide
Olivine	Na <sub>2</sub> BeF <sub>4</sub>	Ca <sub>2</sub> SiO <sub>4</sub>
Phenacite	Li <sub>2</sub> BeF <sub>4</sub>	Zn <sub>2</sub> SiO <sub>4</sub>
Pyroxene	LiBeF <sub>3</sub>	MgSiO <sub>3</sub>
Diopside	LiNaBe <sub>2</sub> F <sub>6</sub>	CaMgSi <sub>2</sub> 0 <sub>6</sub>
Perovskite	KMgF <sub>3</sub>	SrTiO <sub>3</sub>
Spinel	Li <sub>2</sub> NiF <sub>4</sub>	Mg <sub>2</sub> SnO <sub>4</sub>
Strontium plumbate	Na <sub>2</sub> NiF <sub>4</sub>	Ca <sub>2</sub> SnO <sub>4</sub>

### TABLE 1.2: Ratios of Melting Temperatures $(T_m)$ for Fluoride-Oxide Analogue Pairs<sup>†</sup>

Pair	$\frac{T_{m}^{F}/T_{m}^{O}}{T_{m}}$
LiF-MgO	0.36
NaF-CaO	0.44
KF-SrO	0.42
RbF-BaO	0.46
KF-BaO	0.49
CaF <sub>2</sub> -ThO <sub>2</sub>	0.48
MgF <sub>2</sub> -TiO <sub>2</sub>	0.73
MnF <sub>2</sub> -SnO <sub>2</sub>	0.59
KMgF <sub>3</sub> -SrTiO <sub>3</sub>	0.56

<sup>+</sup> The melting temperatures for these fluorides and oxides are listed completely in Table 5.1.

the greater temperature sensitivity of the physical properties of the fluorides and by the fact that germanates have been used as models for the high pressure elasticity of silicates. Classical lattice dynamical theories (e.g., Leibfried and Ludwig, 1961) predict that the elastic moduli should depend linearly on temperature for temperatures greater than the Debye temperature; Anderson (1966) referred to this as the regime of high temperature elastic behaviour. The temperature derivative of the bulk modulus in the high temperature regime is an important input parameter to theoretical equations of state. The evaluation of the use of fluorides to predict the high temperature elastic behaviour of their oxide analogues involves two approaches. (1) Determination of whether the fluorides exhibit high temperature elastic behaviour at lower absolute temperatures than their oxide analogues, which would enable measurement of high temperature derivatives of the elastic moduli at temperatures attainable in laboratory experiments. (2) Examination of the elastic moduli and their temperature derivatives in terms of elastic moduli systematics to determine whether measured values for the fluorides can be used to predict those of the oxides.

The quality and the temperature range of the available elasticity data from the literature precluded evaluation of the high temperature modelling concept. One of the most promising systems for testing the validity of the high temperature modelling concept is the rocksalt analogue pair LiF-MgO. Reliable elasticity data for MgO exist for the temperature range 73°K to 1200°K (Anderson and Andreatch, 1966; Spetzler, 1969, 1970). However the high temperature data for LiF from the resonance experiments of Susse (1961) and Chernov and Stepanov (1961) were not suited to detailed comparison with MgO. The only other fluorides for which single crystal elastic moduli have been determined at high temperatures (T > 300°K) are NaF (rocksalt) and CaF<sub>2</sub> (fluorite), both of which were studied by resonance techniques (Nikanorov and Stepanov,

1963; Nikanorov <u>et al</u>., 1968; Vidal, 1974). The uncertainties in the data for LiF determined by such techniques did not encourage reliance on the data for NaF and  $CaF_2$ .

We have therefore undertaken a programme to determine the elastic moduli of LiF and its isomorph NaF, and of  $CaF_2$  and its isomorphs  $SrF_2$ and  $BaF_2$ , by ultrasonic pulse techniques to temperatures well above room temperature. In addition, we have studied the temperature dependence of the elastic moduli of the rutile-structure MgF<sub>2</sub>, and the perovskite-structure KMgF<sub>3</sub>, which are of great interest as structural analogues of two possible lower mantle phases (see Ringwood, 1970; Liu, 1975, 1976).

### 1.2 Outline of thesis

The purpose of this thesis is to report new and precise values of the single crystal elastic moduli as a function of temperature from 298°K to approximately 650°K for fluorides in the rocksalt, fluorite, rutile and perovskite structures, and to examine the data within the framework of high temperature equations of state and elastic modulus systematics in order to evaluate the fluorides as models for the high temperature elastic behavior of the oxides. In Chapter 2, we describe the experimental techniques employed to determine the elastic wave velocities and hence the elastic moduli as a function of temperature and pressure. The elasticity data versus temperature are presented in Chapter 3 for LiF, NaF,  $CaF_2$ ,  $SrF_2$ ,  $BaF_2$ ,  $MgF_2$  and  $KMgF_3$ . These new data are shown to be internally consistent throughout the temperature range and are compared with existing data from previous investigators. Various high temperature equations of state are employed in Chapter 4 for the discussion of the temperature behaviour of our elastic moduli, and for comparison of the onset of high temperature elastic behaviour

for fluoride and oxide analogues. In Chapter 5, fluoride and oxide elastic moduli and their pressure and temperature derivatives are examined in terms of elastic modulus systematics. Chapter 6 contains a summary and final conclusions on the value of the fluoride-oxide modelling scheme with regard to high temperature elasticity.

### 1.3 Extent of publication

Some of the material in this thesis has been published or submitted for publication while more is being prepared for publication.

- Jones, L. E. A. and Liebermann, R. C., 1974. Elastic and thermal properties of fluoride and oxide analogues in the rocksalt, fluorite, rutile and perovskite structures, Phys. Earth Planet. Interiors., 9:101-107.
- Jones, L. E. A., 1976. High temperature behavior of the elastic moduli of LiF and NaF; comparison with MgO and CaO, submitted to Phys. Earth Planet. Interiors.
- Jones, L. E. A., 1976. High temperature elasticity of the fluorite structure compounds, CaF<sub>2</sub>, SrF<sub>2</sub> and MgF<sub>2</sub>, in preparation.
- 4. Jones, L. E. A., 1976. High temperature elasticity of rutile structure  $MgF_2$ , in preparation.
- 5. Jones, L. E. A., 1976. Elastic moduli of KMgF<sub>3</sub>-perovskite as a function of temperature and pressure, in preparation.

# CHAPTER 2

### EXPERIMENTAL TECHNIQUES

2.1 Introduction

2.2 Sample description and preparation

2.3 Ultrasonic techniques

2.4 Furnace and specimen holder

2.5 Pressure apparatus

For the additions of ontic symmetry (all of the adove except hefp) if was necessary to prepare two sets of crystallographic faces for ultrasonic deusurought to determine and cross-check the three independent elustic moduli. The Lif, heF and Cafe crystals were received as (100) priested cubes which required further orientation and cutting in provide a pair of (110) faces and a pair of (001) faces; the BrF2 and RMgP3 crystals were purchased in this configuration. Due to the appearance of a small crack, the BnP2 crystal was not altered from its original configuration which included a pair of (110) faces and a pair of (11) faces.

The tetragonal MgP2 crystal was purchased as a 1 inch cube with pair of faces perpendicular to the coatin, [001]. To emable the

#### 2.1 Introduction

Ultrasonic pulse techniques were employed in determining the elastic wave velocities in several single crystal fluorides as a function of temperature and pressure. For the temperature measurements, a controlled atmosphere furnace capable of T  $\leq$  1000°C was specially designed and built. Existing apparatus of our laboratory was utilized for the pressure measurements to P  $\leq$  3 kbar.

#### 2.2 Sample description and preparation

Single crystal specimens of LiF, NaF, CaF<sub>2</sub>, BaF<sub>2</sub> and MgF<sub>2</sub> were purchased from Harshaw Chemical Company (Cleveland, Ohio, U.S.A.) while single crystals of  $SrF_2$  and  $KMgF_3$  were obtained from Atomergic Chemetals (Carle Place, New York, U.S.A.). The bulk densities were determined hydrostatically, using toluene as the density reference fluid, and agree to within 0.1% with the X-ray densities (Table 2.1); the former were employed in the calculation of the elastic moduli in Chapter 3.

For the materials of cubic symmetry (all of the above except  $MgF_2$ ) it was necessary to prepare two sets of crystallographic faces for ultrasonic measurement to determine and cross-check the three independent elastic moduli. The LiF, NaF and CaF<sub>2</sub> crystals were received as {100} oriented cubes which required further orientation and cutting to provide a pair of (110) faces and a pair of (001) faces; the  $SrF_2$  and  $KMgF_3$  crystals were purchased in this configuration. Due to the appearance of a small crack, the  $BaF_2$  crystal was not altered from its original configuration which included a pair of (110) faces and a pair of (111) faces.

The tetragonal  $MgF_2$  crystal was purchased as a 1 inch cube with a pair of faces perpendicular to the c-axis, [001]. To enable the determination and cross-checking of the six independent elastic moduli,

### TABLE 2.1: Comparison of bulk and X-ray densities

	Bulk density	X-ray density
Crystal	(gm.cm <sup>-3</sup> )	(gm.cm <sup>-3</sup> )
LiF	2.641±0.003	2.639 <sup>1</sup>
NaF	2.806±0.003	2.8041
CaF <sub>2</sub>	3.183±0.003	3.181 <sup>2</sup>
SrF <sub>2</sub>	4.282±0.004	4.277 <sup>3</sup>
BaF <sub>2</sub>	4.887±0.005	4.886 <sup>2</sup>
MgF <sub>2</sub> (crystal A)	3.178±0.003	3.1784
MgF <sub>2</sub> (crystal B)	3.177±0.003	3.1784
KMgF <sub>3</sub>	3.151±0.003	3.15 <sup>5</sup>

1. Miller and Smith (1964)

2. Wong and Schuele (1968)

3. Gerlich (1964b)

4. Haussühl (1968)

5. Rosenberg and Wigmore (1967)

The pulse superposition technique of McSkimin (1961, 1962) wa ployed in determining the elastic wave velocities as a function of moverature and pressure. A block diagram of the electronic equipment this specimen was oriented and cut to provide the two crystals illustrated in Figure 2.1; crystal A, which consisted of a cube with a pair of (001) faces and a pair of (110) faces; and crystal B, which was a cube with a pair of (100) faces and a pair of faces at 45° to the (001) and (010) crystallographic planes. Since the purchased crystal of  $MgF_2$  was misaligned from the c-axis by 5°, the resultant errors in the orientations of crystals A and B were corrected in the polishing process.

The physical dimensions of the approximately cubical specimens lay between 6.3 mm and 7.5 mm for all crystals except KMgF<sub>3</sub>, for which the edge length was approximately 5 mm. Lengths at room temperature and atmospheric pressure were determined with a micrometer and are accurate to  $\pm 3 \times 10^{-3}$  mm. Opposite faces were polished with 8 µm diamond paste to a flatness of within 0.0005 cm and to a parallelness of better than 0.013°.

The final orientations for LiF and NaF were verified by transmission X-ray techniques to be correct to within  $0.3^{\circ}$ . Back reflection X-ray techniques verified that the orientations were correct to within  $1.5^{\circ}$  for CaF<sub>2</sub>, SrF<sub>2</sub> and the (110) face for BaF<sub>2</sub>. The (111) face of BaF<sub>2</sub> was found to have a misalignment of  $3.5^{\circ}$ . Similar determinations for MgF<sub>2</sub> demonstrated that the orientations were correct to within 1°. The misorientation angles for each of the seven crystals are detailed completely in Appendix A. The effect of these misorientations on the elastic moduli and their temperature derivatives is discussed later in Chapter 3.

### 2.3 Ultrasonic Techniques

The pulse superposition technique of McSkimin (1961, 1962) was employed in determining the elastic wave velocities as a function of temperature and pressure. A block diagram of the electronic equipment





B

<u>Figure 2.1</u>: Diagram showing the orientation of  $MgF_2$  crystals A and B relative to the crystallographic axes for tetragonal crystals.

used is shown in Figure 2.2. The 20 MHz quartz transducers (X-cut for compressional and AC-cut for shear waves, both co-axially-plated and  $\frac{1}{4}$  inch diameter) were bonded directly to the specimens for the temperature and pressure measurements. A high temperature lubricating grease Extemp 9901 (Frisillo and Barsch, 1972) facilitated excellent acoustic coupling at room temperature although a somewhat poorer signal resulted at elevated temperatures (see Figure 2.3). Loss of acoustic coupling due to failure of the bond at high temperatures limited the experimental temperature range to T  $\leq$  400°C. For the pressure measurements, Dow-Chemical Resin 276-V9 was used as the bonding material and provided an excellent signal in the pressure range 0-2.5 kbar. At higher pressures, the signal became highly attenuated and we could not obtain systematic, reproducible data (see Figure 2.4), perhaps due to the increased viscocity of the pressure transmitting fluid or to deterioration of the bonding resin.

In the pulse superposition technique, the "in phase" echo condition is obtained by varying the pulse repetition frequency,  $f_R$ , until a maximum occurs in the amplitude of the successive internal acoustic echoes within the specimen. When this condition is achieved:

$$\delta = (1/f_{\rm p}p) - (1/f_{\rm c})[n/p - \gamma/360]$$
(2.1)

where  $\delta$  is the round trip delay in the specimen alone,  $f_c$  is the carrier frequency (20 MHz) and  $\gamma$  is a phase angle associated with reflections at the transducer-specimen interface. In these experiments, pulses were applied for each round trip in the specimen, corresponding to the p = 1 condition. The value of  $f_R$  associated with n = 0 was determined by measuring the spectrum of repetition frequencies corresponding to integer increments in n for 10 MHz, 20 MHz and 30 MHz transducers. Unresolved ambiguities were eliminated by a pulse transmission technique (Liebermann <u>et al.</u>, 1975). For a thin acoustic bond, the phase angle  $\gamma$  should be of the order of a few degrees (McSkimin, 1961, 1962; Schreiber <u>et al.</u>, 1973).

# PULSE SUPERPOSITION



<u>Figure 2.2</u>: Block diagram of the pulse superposition apparatus in operation with one transducer. The relationship between the pulse repetition frequency  $(f_R)$  and the carrier frequency  $(f_c)$  is illustrated schematically.



(a)

(b)



### Fig.2.3

Photos of typical ultrasonic pulse superposition signals for LiF at room temperature (a) and at high temperature (350°C)(b). The deterioration of the signal with increasing temperature is due to the failure of the Extemp bond. The carrier frequency is approximately 20MHz and the mode of propagation is  $C_{44}$  shear mode in the [001] direction.



(b)

(c)



Photos of typical ultrasonic pulse superposition signals for  $KMgF_3$  at ambient pressure (a), at 1 kbar (b) and at 3 kbar(c). The increased Fig.2.4 attenuation and decrease in the signal quality at 3 kbar are indicative of bonding problems at higher pressures. The carrier frequency is approximately 20 MHz and the mode of propagation is the  $C_{44}$  shear mode in the [110] direction

The resultant errors in  $\delta$  would lie between 1 x 10<sup>-3</sup> and 1 x 10<sup>-4</sup> for the compressional and shear modes measured. The variation of the phase angle  $\gamma$  with pressure and temperature was minimized by maintaining the transducer-bond assemblage at its resonant frequency (McSkimin, 1961). Herein lies the advantage of the pulse superposition technique in its sensitivity to small changes in the elastic wave velocities due to changing environmental conditions (P, T, etc.).

Ambiguities in the measurement of pulse repetition frequencies were observed due to extraneous interference effects which produced multiple maxima in pulse amplitudes instead of the ideal single maximum. In addition, not all the displayed echoes peaked in amplitude at the same frequency, a condition we refer to as "phasing". The uncertainties in  $f_R$ , which tended to be larger for the compressional modes, were estimated on the basis of the separation of the multiple peaks and were comparable to the errors in  $\delta$  due to phase changes at the transducerbond-sample interfaces. Uneven bond thicknesses resulting in varying phase angles across the transducer could be one explanation for the multiple peaking and "phasing". This is supported by the fact that the pattern of peaks does vary with temperature.

Non-parallellism and departure from flatness of the acoustically reflecting faces could also result in extraneous interference effects. Another contributing factor could be diffraction which results in beam spreading and possible side wall reflections as well as reflection of a non-planar wave front from the far end of the sample. The choice of 20 MHz transducers is a tradeoff between minimising the effects of nonparallelism (less significant at lower frequencies) and those of diffraction (less significant at higher frequencies). At the carrier frequency of 20 MHz the previously quoted parallelism figures of better than 0.013° and flatness of better than 0.0005 cm lie on the borderline of detectable effect (Truell <u>et al.</u>, 1969, chapter 2.2). The effects of

diffraction are small for  $a/\lambda >> 1$ , where a is the transducer radius and  $\lambda$  is the wavelength of the carrier (McSkimin, 1964). For compressional waves,  $a/\lambda \sim 12$  and for shear waves,  $a/\lambda \sim 25$ . Hence diffraction effects are more likely to be non-negligible for compressional than for shear waves. The small departures of the echo pattern from exponential decay at room temperature are typical of the effects of non-parallelism and diffraction (Truell <u>et al</u>., 1969, chapters 2.1, 2.2). That the extraneous interferences could be due to the side wall reflections allied with diffraction is supported by the fact that the occurrence of multiple peaking was greatly reduced with the change of boundary conditions upon immersion of the sample in the pressure medium.

The observed multiple peaking and "phasing" probably arise from a combination of diffraction and bond effects. However, despite the errors ascribed to  $f_R$  on the basis of peak separation, it was, in general, possible to track a particular peak as a function of temperature, resulting in a much more systematic data set than the errors would imply. The absolute accuracy of  $f_R$  at any P, T is better than  $\pm 1 \ge 10^{-3}$ ; however the relative precision of  $f_R$  at successive T or P in a particular run is better than  $\pm 1 \ge 10^{-4}$ .

### 2.4 Furnace and specimen holder

A small furnace was specially constructed to our design for the measurement of elastic wave velocities as a function of temperature. One requirement was a thermal inertia low enough to facilitate a flexible range of heating rates, yet high enough to prevent short term temperature fluctuations. The stipulation that the temperature gradient across the sample be as small as possible demanded the provision of a large uniform "hot spot" at the centre of the furnace. Provision also had to be made for the maintenance of an inert gas atmosphere.

A schematic drawing of the furnace is shown in Figure 2.5, illustrating the furnace casing built by our workshop, the furnace core and the packing arrangement. The furnace core consisted of a mullite tube of 5/8 inch internal diameter which we wound with platinum 20% rhodium wire of 0.020 inch diameter. The windings were spaced closer at the ends (approximately 13 turns per inch) than at the centre (approximately 10 turns per inch) and were anchored in place with alumina cement. This gradation in winding was intended to produce a large uniform "hot spot". The ends of the mullite tube extended beyond the furnace so that gas seals could be easily made with the specimen holder and opposing end piece in place. We completed assembly of the furnace by packing in powdered alumina and magnesium oxide as thermal insulation.

The specimen holder (Figures 2.6, 2.7) was designed to support the sample, to supply the electrical signal to the co-axial transducer bonded directly to the sample, and to provide spring loading on the transducer-sample interface. This last was necessary to maintain good acoustical coupling as a function of temperature. The opposing end piece was employed as a thermal and gas seal as well as a means of introducing the platinum-platinum 10% rhodium thermocouple which was seated directly against the specimen. A schematic drawing of both the specimen holder and end piece is shown in Figure 2.6 which also illustrates their placement in the furnace core. Figure 2.7 is a photograph of the assembled specimen holder while Figure 2.8 is a photograph of the furnace with both specimen holder and opposing end piece in place.

The temperature distribution along the axis of the furnace and the exact position of the "hot spot" were determined with the complete assemblage shown in Figure 2.8, but with the introduction of a second thermocouple down the axis of the signal pin. The difference between the fixed reference thermocouple and the movable one enabled precise determination of the temperature distribution. For the final determination, a dummy specimen with a hole for the thermocouple bored





Figure 2.5: Vertical section through the furnace showing the furnace casing, the furnace core and the packing arrangement of the insulating material.



Figure 2.6: Schematic drawing of the specimen holder and opposing end piece in situ in the furnace bore. The drawing is to scale except where broken in the vertical dimension, and except for schematic representation of the transducer, springs, screw-thread and 0-rings.




Fig. 2.8 Photo of the furnace assembly with the specimen holder and opposing end piece in place. The signal cable can be seen at the very top of the photo. Gas input and output tubes are attached to horizontal tubes on the assembly. The thermocouple leads enter from the bottom. along its axis was employed as this simulated the experimental arrangement more closely. Figure 2.9 demonstrates that the hot spot is indeed very uniform, the variation in temperature being less than 1°C over a distance of 12.5 mm at 800°C. At lower temperatures, the hot spot should be even larger. Determinations of the effect of inert gas flow at 400°C, 600°C and 800°C demonstrated that for very slow gas flow, the "hot spot" was unaltered from the position determined at 800°C.

For a temperature run, inert gas (either argon or dry nitrogen) was flushed through the system and then reduced to a very slow flow before the furnace was switched on. The reference junction of the platinum-platinum 10% rhodium thermocouple remained at room temperature which was known to  $\pm 1^{\circ}$ C for the runs for LiF and NaF and to  $\pm 0.2^{\circ}$ C for subsequent runs. The e.m.f. associated with the thermocouple was measured by either a potentiometer or a digital voltmeter; the uncertainty in measurement of e.m.f. corresponded to a temperature difference of  $0.5^{\circ}$ C. The thermocouples used were calibrated against the melting point of gold and against the boiling point of water (see Appendix B) and were found to be correct to within 2°C. It was decided that corrections need not be made to the measured values of temperature.

### 2.5 Pressure apparatus

The pressure dependence of the elastic wave velocities was determined by placing the specimen in a standard specimen holder in a liquid medium apparatus (Figure 2.10) built by Harwood Engineering Company according to the specifications of this laboratory (Liebermann <u>et al.</u>, 1975). Silicone oil (Dow-Corning DC-200, 5 centistoke viscosity) was the pressure medium and the pressure was determined from the millivolt output of a manganin pressure gauge with a precision of  $\pm 0.01$  kbar. Temperature was not controlled but was monitored by a copper-constantan thermocouple with a reference of 0°C in an ice-water slurry. With each



Figure 2.9: The axial temperature distribution across the centre of the furnace. The position of the specimen is indicated.

# ANU Mineral Physics Pressure System (P≤14 kbar)



Figure 2.10: Block diagram of the pressure vessel system.

increase in pressure, the temperature also increased and time to reach equilibrium was allowed before measurements were taken. Since the equilibrium values of temperature also increased with pressure, the data were corrected to 298°K (see also Chapter 3.6).

### CHAPTER 3

TEMPERATURE AND PRESSURE DEPENDENCE OF THE ELASTIC MODULI OF SEVERAL FLUORIDES: EXPERIMENTAL RESULTS

### 3.1 Introduction

3.2 Data analysis for the elastic moduli (c) as a function of temperature (T) and pressure (P)

3.3 Rocksalt-structure fluorides: LiF and NaF. c(T).

3.4 Fluorite-structure fluorides:  $CaF_2$ ,  $SrF_2$  and  $BaF_2$ . c(T).

3.5 Rutile-structure fluorides: MgF<sub>2</sub>. c(T).

3.6 Perovskite-structure fluorides: KMgF<sub>3</sub>. c(T), c(P).

3.7 Conclusion

(12) direction (Table 3.1). The six independent electic moduli is of , together with crosschecks to 370°K, were determined by the supagation of shear and compressional waves in the [100], [110] and [01] directions, and in a direction at 45° to the [001] and [010]

Data analysis for the elastic moduli (c) as a function of feature (T) and pressure (P)

#### CHAPTER 3

TEMPERATURE AND PRESSURE DEPENDENCE OF THE ELASTIC MODULI OF SEVERAL FLUORIDES: EXPERIMENTAL RESULTS

### 3.1 Introduction

The single crystal elastic moduli were determined as a function of temperature using the experimental techniques described in Chapter 2, for fluorides which crystallize in the rocksalt, fluorite, rutile and perovskite structures. Measurements were performed in the range  $298^{\circ}$ K to approximately  $650^{\circ}$ K for LiF and NaF (rocksalt), CaF<sub>2</sub>, SrF<sub>2</sub> and BaF<sub>2</sub> (fluorite), and MgF<sub>2</sub> (rutile). The temperature range of the measurements for KMgF<sub>3</sub> (perovskite) lay between  $298^{\circ}$ K and approximately  $550^{\circ}$ K. The single crystal elastic moduli of KMgF<sub>3</sub> were also determined as a function of pressure from 1 bar to 2.5 kbar.

Propagation of shear and compressional waves in the [110] and [001] directions for the cubic crystals LiF, NaF, CaF<sub>2</sub> and SrF<sub>2</sub> enabled the determination and cross-checking of the three independent elastic moduli (Table 3.1) as a function of temperature. For BaF<sub>2</sub> and KMgF<sub>3</sub>, the three independent elastic moduli were determined by the propagation of compressional and shear waves in the [110] direction, with the room temperature crosschecks for BaF<sub>2</sub> being provided by measurements for the [111] direction (Table 3.1). The six independent elastic moduli for MgF<sub>2</sub>, together with crosschecks to  $370^{\circ}$ K, were determined by the propagation of shear and compressional waves in the [100], [110] and [001] directions, and in a direction at 45° to the [001] and [010] directions (Table 3.2).

## 3.2 Data analysis for the elastic moduli (c) as a function of temperature (T) and pressure (P)

The elastic wave velocities as a function of temperature are determined from the primary data, the pulse repetition frequencies,  $f_{R}$ ,

Mode	velocity	Elastic Constant	Direction	Mode
	v <sub>1</sub>	c <sub>ll</sub>	[001]	Р
	v <sub>2</sub>	C 4 4	[001]	S random polarisation
	v <sub>3</sub>	<sup>1</sup> c'	[110]	S pol [110]
	v <sub>4</sub>	c44	[110]	S pol [001]
	v <sub>5</sub>	<sup>2</sup> c''	[110]	Р
	v <sub>6</sub>	<sup>3</sup> c <sub>L</sub>	[111]	Р
	v <sub>7</sub>	<sup>4</sup> c <sub>T</sub>	[111]	S random polarisation

Table 3.1: Modes of propagation in cubic crystals used for determiningthe single crystal elastic constants

1.  $c' = (c_{11} - c_{12})/2$ 2.  $c'' = (c_{11} + c_{12} + 2c_{44})/2$ 3.  $c_L = (c_{11} + 2c_{12} + 4c_{44})/3$ 4.  $c_T = (c_{11} - c_{12} + c_{44})/3$ 

Mode	velocity	Elastic constant	Direction	Mode
	v <sub>1</sub>	c <sub>11</sub>	[100]	Р
	v <sub>2</sub>	c <sub>66</sub>	[100]	S pol. [010]
	v <sub>3</sub>	с <sub>44</sub>	[100]	S pol. [001]
	v <sub>4</sub>	<sup>1</sup> c <sub>Ĺ1</sub>	[110]	Р
	v <sub>5</sub>	<sup>2</sup> c'	[110]	S pol. [111]
	v <sub>6</sub>	C1414	[110]	S pol. [001]
	v <sub>7</sub>	c <sub>33</sub>	[001]	Р
	v <sub>8</sub>	Сцц	[001]	S random polarisation
	v <sub>9</sub>	<sup>3</sup> c <sub>L2</sub>	45° to [001] and [010]	P (quasi)
	v <sub>10</sub>	<sup>4</sup> c <sub>T2</sub>	45° to [001] and [010]	S (quasi)
	v <sub>11</sub>	<sup>5</sup> c <sub>T1</sub>	45° to [001] and [010]	S pol. [100]
	$= (c_{11} + c_{22})$	a + 2ccc)/2		

1. 
$$c_{L_1} = (c_{11} + c_{12} + 2c_{66})/2$$

2.  $c' = (c_{11} - c_{12})/2$ 

3.  $c_{L_2} = \frac{1}{4} \{ c_{11} + c_{33} + 2c_{44} + [(c_{11} - c_{33})^2 + 4(c_{13} + c_{44})^2]^{\frac{1}{2}} \}$ 

4.  $c_{T_2} = \frac{1}{4} \{ c_{11} + c_{33} + 2c_{44} - [(c_{11} - c_{33})^2 + 4(c_{13} + c_{44})^2]^{\frac{1}{2}} \}$ 

5. 
$$c_{T_1} = (c_{44} + c_{66})/2$$

(8+) - (2+) - 101- 102 - 100

which are measured during very slow heating (less than  $0.5^{\circ}$ C per minute). The values of  $f_R$  thus obtained are indistinguishable from equilibrium measurements. The inherent precision of the pulse superposition technique is reduced by other experimental uncertainties, in particular those associated with bond and diffraction effects (Chapter 2). For the purposes of a least squares analysis, it is assumed that the uncertainties in the pulse repetition frequency are instrumental and are all equal (relative error =  $1 \times 10^{-4}$  for most of the measured modes), and that the random errors in the measurement of temperature can be neglected.

The pulse repetition frequencies,  $f_R$ , the elastic wave velocities, v, and the elastic moduli, c, at any temperature are related by

$$v = 2\ell f_R$$

$$c = \rho v^2 = 4\rho \ell^2 f_R^2$$
(3.1)

For cubic crystals,  $\rho$ , the specimen density, and l, the specimen length in the direction of propagation, are related to their respective room temperature values,  $\rho_{\circ}$  and  $l_{\circ}$ , by

$$\rho = \rho_{o} \left( \frac{\ell_{o}}{\ell} \right)^{3}$$
(3.2)

$$l = l_{o}(a_{1} + a_{2}T + a_{3}T^{2} + a_{4}T^{3})$$
(3.3)

The coefficients  $a_i$  in the polynomial expression for the length, together with the bulk density used in the calculation of the elastic moduli, are given in Table 3.3 for LiF and NaF, and in Table 3.4 for CaF<sub>2</sub>, SrF<sub>2</sub> and BaF<sub>2</sub>. For tetragonal crystals for which the thermal expansion is anisotropic, the corresponding relationships between l and  $l_{\circ}$  for the [100] and [110] directions is given by

$$\left(\frac{\ell}{\ell_{o}}\right) = \left(\frac{\ell^{a}}{\ell_{o}^{a}}\right) = (a_{1} + a_{2}T + a_{3}T^{2})$$
(3.4)

and for the [001] direction by

Data	LiF	NaF
Molecular Weight	25.94	41.99
Molar Volume, cm <sup>3</sup>	9.83	14.98
Bulk Density, gm.cm <sup>-3</sup>	2.641	2.806
X-ray Density, gm.cm <sup>3</sup>	2.639 <sup>1</sup>	2.804 <sup>1</sup>
<sup>a</sup> 1	0.9925 <sup>2</sup>	0.99242
$a_2, deg^{-1} \times 10^{-4}$	0.1845 <sup>2</sup>	0.18962
$a_3, deg^{-2} \times 10^{-7}$	0.2360 <sup>2</sup>	0.22632

- 1. Miller and Smith (1964)
- 2.  $\ell(T) = \ell(298) [a_1 + a_2T + a_3T^2]$ , where  $a_1$ ,  $a_2$ , and  $a_3$ are calculated from  $b_1$ ,  $b_2$  and  $b_3$  of Srivastava and Merchant (1973) where  $a^*(T) = b_1 + b_2T + b_3T^2$ ,  $a^*$  being the lattice parameter.

### Table 3.4: Basic data for CaF2, SrF2 and BaF2

Data	CaF <sub>2</sub>	SrF <sub>2</sub>	BaF <sub>2</sub>
Molecular Weight	78.08	125.62	175.34
Molar Volume, cm <sup>3</sup>	24.55	29.37	35.89
Bulk Density, gm.cm <sup>-3</sup>	3.183	4.282	4.887
X-ray Density, gm.cm <sup>-3</sup>	3.181 <sup>1</sup>	4.2772	4.886 <sup>1</sup>
$a_1$ equation in the direction as	0.9957 <sup>3</sup>	0.9943 <sup>3</sup>	0.9950 <sup>3</sup>
$a_2, deg^{-1} \times 10^{-4}$	0.0727	0.2616	0.1371
$a_3^{-2}$ , deg <sup>-2</sup> x 10 <sup>-7</sup>	0.2863	- 0.3509	0.090
$a_4$ , deg <sup>-3</sup> x 10 <sup>-10</sup>	- 0.1567	0.390	0.050

1. Wong and Schuele (1968)

2. Gerlich (1964b)

3.  $\ell(T) = \ell(298) (a_1 + a_2T + a_3T^2 + a_4T^3)$  where  $\ell$  is the length and the  $a_i$  are determined from the thermal expansion data of Sirdeshmukh and Deshpande (1964).

2.1), versus temperature were fitted by polynomials in T using the stand of least squares. The standard F-test (Bewington, 1969, chapter 5.1) was applied in determining the Statistical significance of adding artikes terms to the fitted polynomials. This was used in conjunction it a mandard  $g^2$ -test (Bevington, 1959, chapter 10-1) to determine the artes of the polynomial that should be fitted to the c-T date. In moral, it was found that the statistical significance of adding a utilize term to the polynomial became marginal at the point where the abuved  $g^2$ -value became approximately equal to unity, indicating that the "state of the date about the fitted polynomial cas comparable with the "finited experimental uncertainties. In the manance of the mall

$$\left(\frac{\ell}{\ell_{o}}\right) = \left(\frac{\ell^{c}}{\ell_{o}^{c}}\right) = (c_{1} + c_{2}T + c_{3}T^{2})$$
(3.5)

and between p and po by

$$(\rho/\rho_{\circ}) = \left(\frac{\ell^{a}}{\ell^{a}}\right)^{2} \left(\frac{\ell^{c}}{\ell^{c}}\right)$$
(3.6)

where  $l^a$  and  $l^c$  are lengths along the a and c axes respectively. For propagation in the direction at 45° to the [001] and [010] directions, the relationship between l and  $l_o$  is

$$\left(\frac{\ell}{\ell_{o}}\right)^{2} = \frac{1}{2} \left[ \left(\frac{\ell^{a}}{\ell_{o}}\right)^{2} + \left(\frac{\ell^{c}}{\ell_{o}}\right)^{2} \right]$$
(3.7)

The coefficients  $a_i$  and  $c_i$ , and the bulk density are given in Table 3.5 for MgF<sub>2</sub>. The raw pulse repetition frequency data and the elastic moduli calculated from equation (2.1) at each temperature data point are listed in Appendix C for each of the measured modes for LiF, NaF, CaF<sub>2</sub>, SrF<sub>2</sub>, BaF<sub>2</sub> and MgF<sub>2</sub>. For KMgF<sub>3</sub>, only the pulse repetition frequencies and corresponding temperatures are listed in Appendix C.

The values of the elastic moduli, c, calculated from equation (2.1), versus temperature were fitted by polynomials in T using the method of least squares. The standard F-test (Bevington, 1969, chapter 10-2) was applied in determining the statistical significance of adding further terms to the fitted polynomials. This was used in conjunction with a standard  $\chi^2$ -test (Bevington, 1969, chapter 10-1) to determine the degree of the polynomial that should be fitted to the c-T data. In general, it was found that the statistical significance of adding a further term to the polynomial became marginal at the point where the reduced  $\chi^2$ -value became approximately equal to unity, indicating that the scatter of the data about the fitted polynomial was comparable with the estimated experimental uncertainties. In the absence of thermal expansion data for KMgF<sub>3</sub>, the polynomial fitting procedure was applied

Data	
Molecular Weight	62.31
Molar Volume, cm <sup>3</sup>	19.61
Bulk Density, gm.cm <sup>-3</sup> crystal A crystal B	3.178 3.177
X-ray Density, gm.cm <sup>-3</sup>	3.178 <sup>1</sup>
a <sub>1</sub>	0.997019 <sup>2</sup>
$a_2, deg^{-1} \times 10^{-4}$	0.0877942
$a_3, deg^{-1} \times 10^{-7}$	0.040547 <sup>2</sup>
c1 fect of crystal strenged at los	0.995842
$c_2, deg^{-1} \times 10^{-4}$	0.125943 <sup>2</sup>
$c_3, deg^{-1} \times 10^{-7}$	0.0439682

- 1. Haussühl (1968)
- 2.  $l_a(T) = l_a(298) [a_1 + a_2T + a_3T^2]$  and  $l_c(T) = l_c(298) [c_1 + c_2T + c_3T^2]$  where  $l_a, l_c$  are lengths along the a-axes and c-axis respectively. The  $a_i$  and  $c_i$  are determined from the thermal expansion data of Bailey <u>et al</u>. (1975).

directly to the  $f_R^-T$  data.

The values of the elastic moduli and their temperature derivatives were evaluated at 298°K from the polynomial equations in T. The associated errors were determined from the uncertainties in the polynomial coefficients (Bevington, 1969, chapters 6-5, 8-1) together with the uncertainties in  $\rho_{\circ}$  ( $\sim$  0.1%) and  $\ell_{\circ}$  ( $\sim$  0.05%). Since the uncertainties in the polynomial coefficients are not independent, the calculated errors in the elastic moduli and their temperature derivatives probably overestimate the actual uncertainties.

The effect of crystal misorientations (Chapter 2) on the elastic moduli and their temperature derivatives was calculated from the expressions for the orientation dependence of the elastic wave velocities given by Waterman (1959). The expression used in conjunction with Waterman's equations for calculating the error in the temperature derivatives is given in Appendix A.

The primary pressure data are the pulse repetition frequencies,  $f_R$ , measured as a function of pressure under equilibrium and quasiisothermal conditions and corrected to 298°K, using data for the temperature dependence of the  $f_R$ . The precision of the measurement of  $f_R$  is 2 x 10<sup>-4</sup> for the compressional mode and 1 x 10<sup>-4</sup> for the shear modes. The uncertainties can also be roughly estimated from the degree of reproducibility attained in different runs. For the purposes of a least squares analysis, it is assumed that the uncertainties in  $f_R$  are instrumental and are all equal, and that the random errors in the measurement of pressure can be neglected.

The pulse repetition frequencies versus pressure were fitted by straight lines using the method of least squares. The linear relationship for  $f_R$ -P simplified the application of the formula introduced by Cook (1957) for the relative length change with pressure,

$$\left(\frac{\ell}{\ell_{o}}\right) = 1 + \frac{(1+\Delta)}{12\rho_{o}\ell_{o}^{2}} \int_{0}^{P} \frac{dP}{f_{5}^{2} - f_{4}^{2} - f_{3}^{2}/3}$$
(3.8)

where  $f_3$ ,  $f_4$ ,  $f_5$  are the pulse repetition frequencies corresponding to  $v_3$ ,  $v_4$  and  $v_5$  in Table 3.1 and where  $\Delta$  is given by

$$\Delta = \alpha_V \gamma T \tag{3.9}$$

In (3.9),  $\alpha_{V}$  is the volumetric thermal expansion and  $\gamma$  is the thermal Grüneisen parameter

$$\gamma = \frac{\alpha_V K_S}{\rho C_P}$$
(3.10)

 $\rm K_S$  being the adiabatic bulk modulus and  $\rm C_p,$  the specific heat per gram at constant pressure. Since the  $\rm f_R$  depend linearly on P, equation (3.8) can be rewritten as

$$\left(\frac{\&}{\&_{\circ}}\right) = 1 + \frac{(1 + \Delta)}{12\rho_{\circ}\&_{\circ}^{2}} \int_{0}^{P} \frac{dP}{AP^{2} + BP + C}$$
(3.11)

The integral in equation (3.11) can be evaluated (e.g., see Abramowitz and Stegun, 1965) as follows:

$$\int \frac{dP}{AP^{2} + BP + C} = \frac{1}{(B^{2} - 4AC)^{\frac{1}{2}}} \ln \left| \frac{2AP + B - (B^{2} - 4AC)^{\frac{1}{2}}}{2AP + B + (B^{2} - 4AC)^{\frac{1}{2}}} \right|$$

$$(B^{2} - 4AC > 0)$$

$$= \frac{-2}{2AP + B} \qquad (B^2 - 4AC = 0)$$
$$= \frac{2}{(4AC - B^2)^{\frac{1}{2}}} \arctan \frac{2AP + B}{(4AC - B^2)^{\frac{1}{2}}}$$

 $(B^2 - 4AC < 0)$  (3.12)

The elastic moduli were calculated at 1 bar and the maximum experimental pressure from equations (3.1), (3.2), (3.11) and (3.12) using the values of  $f_R$  derived from the linear fits to the  $f_R$ -P data.

The bulk density used in the calculation is listed in Table 3.6. In (3.11),  $(1 + \Delta)$  was replaced by unity for KMgF<sub>3</sub>. This has a negligible effect on  $\ell/\ell_0$  since  $\Delta \sim 0.05$  and the second term in (3.11) is of the order 1 x  $10^{-3}$  at 2.5 kbar. The pressure derivatives of the elastic moduli were determined by assuming a linear dependence on pressure for the elastic moduli. The errors in the elastic moduli and their pressure derivatives were estimated from the uncertainties in the coefficients of the linear equations satisfying the  $f_{\rm R}$ -P data.

### 3.3 Rocksalt-structure fluorides: LiF and NaF. c(T).

The elastic moduli calculated from equation (3.1) for LiF and NaF are plotted for all five modes in Figures 3.1 and 3.2 respectively. Also shown are the fitted polynomial equations (see also Table 3.7). For all modes except c" for LiF and NaF, the addition of a quadratic term to the fitted polynomial equation was statistically significant at the 99.9% confidence level. For c", a cubic polynomial was required for LiF although a linear fit was sufficient for the NaF data. However, the uncertainty for c" is larger than that for the other modes due to difficulties in identifying the correct peak as a function of temperature. In view of this it was decided that only a second degree polynomial was justified by the data for LiF.

The values of the elastic moduli and their temperature derivatives, calculated by evaluating the polynomials at 298°K, are listed in Table 3.8 for LiF and NaF, together with the associated errors. The effects of misorientation were found to be negligible. The crosschecks are provided by comparing  $c_{44}$  from  $v_2$  and  $v_4$  and by comparing c" (measured) and c" (calculated from  $c_{11}$ , c' and  $c_{44}$ ); in all cases the agreement for the elastic moduli is better than 0.5% and for the temperature derivatives is within 5%. These differences for  $c_{44}$  and c" and their temperature derivatives are well within the calculated uncertainties for the

### Table 3.6: Basic data for KMgF3

Data

Molecular Weight	120.41
Molar Volume, cm <sup>3</sup>	38.23
Bulk Density, gm.cm <sup>-3</sup>	3.151
X-ray Density, gm.cm <sup>-3</sup>	3.15 <sup>1</sup>

1. Rosenberg and Wigmore (1967)



and c' for LIF. The solid lines represent the fitted second degree pelynomials. For the cas shown made, the pelynomial curve for the [001] direction cannot be distinguished from the plotted curve for the [110] direction. But points for the crosschool for cas from the [001] direction are indicated by X. For remains of clarity, not all the data points used in the fitting procedure are plotted.



Figure 3.1: Elastic moduli versus temperature for the modes  $c_{11}$ , c",  $c_{44}$ and c' for LiF. The solid lines represent the fitted second degree polynomials. For the  $c_{44}$  shear mode, the polynomial curve for the [001] direction cannot be distinguished from the plotted curve for the [110] direction. Data points for the crosscheck for  $c_{44}$  from the [001] direction are indicated by X. For reasons of clarity, not all the data points used in the fitting procedure are plotted.



Figure 3.2: Elastic moduli versus temperature for the modes  $c_{11}$ , c'',  $c_{44}$ and c' for NaF. The solid lines represent the fitted polynomials (quadratics for  $c_{11}$ , c' and  $c_{44}$  and a straight line for c''). For the  $c_{44}$  shear mode, the polynomial curve for the [110] direction cannot be distinguished from the plotted curve for the [001] direction. Data points for the crosscheck for  $c_{44}$  from the [110] direction are indicated by X. For reasons of clarity, not all the data points used in the fitting procedure are plotted.

for	LiF and NaF		
	A (kbar)	B (kbar.deg <sup>-1</sup> )	C (kbar.deg <sup>-2</sup> x 10 <sup>-3</sup> )
LiF			
c <sub>11</sub>	1377	-0.810	+0.102
c′	457	-0.464	+0.140
c <sub>44</sub> (v <sub>2</sub> )	687	-0.142	-0.063
c <sub>44</sub> (v <sub>4</sub> )	687	-0.149	-0.056
c″	1615	-0.552	-0.038
NaF			
c11	1166	-0.672	+0.080
c ′	474	-0.380	+0.074
$c_{44}(v_2)$	297	-0.045	-0.022
$c_{44}(v_4)$	299	-0.046	-0.021
c "	994	-0.351	- E

Mode	Velocity	c (kbar)	$(\frac{\partial c}{\partial T})_{P}$ (kbar.deg. <sup>-1</sup> )	C (kbar)	$^{\mathrm{aF}}$ $\left(\frac{\partial c}{\partial T}\right)_{\mathrm{p}}$ (kbar.deg. <sup>-1</sup> )
c <sub>11</sub>	v <sub>1</sub>	1144 ± 3	-0.749 ± 0.005	973 ± 3	-0.624 ± 0.006
c ′	v <sub>3</sub>	331 ± 1	$-0.380 \pm 0.002$	368 ± 1	-0.336 ± 0.002
c <sub>44</sub>	v <sub>2</sub>	639 ± 3	-0.179 ± 0.002	282 ± 2	-0.058 ± 0.003
	v <sub>4</sub>	637 ± 2	-0.183 ± 0.004	284 ± 2	-0.059 ± 0.004
c ″	v <sub>5</sub>	1447 ± 7	$-0.575 \pm 0.012$	890 ± 3	-0.354 ± 0.003
	calc.	1453 ± 4	-0.555 ± 0.009	888 ± 5	-0.347 ± 0.008
к <sub>S</sub>	calc.	704 ± 4	-0.242 ± 0.008	483 ± 4	$-0.177 \pm 0.009$

Table 3.8: Single crystal elastic moduli and their temperature derivatives at 298°K for LiF and NaF

respective modes.

In Table 3.9, values of the elastic moduli from other investigations are listed for comparison with our data for LiF and NaF at 298°K. For LiF, the agreement is good with the exception of the values of Briscoe and Squire (1957) and Susse (1961) which tend to be very much lower. Similarly for NaF the agreement is generally good with the exception of the elastic moduli data of Nikanorov and Stepanov (1963).

Also compared in Table 3.9 are the values of the temperature derivatives of the elastic moduli  $(\partial c/\partial T)_p$  at 298°K. For both LiF and NaF the agreement between our values and those of Haussühl (1960) is remarkably good, the discrepancy being less than 1%. The agreement with the NaF data of Vallin et al. (1966) and Bensch (1972) is only fair.

The comparison of our elastic moduli with those of other investigators can be carried out over a wider range of temperatures in Figures 3.3 and 3.4 which are plots of adiabatic bulk modulus,  $K_S$ , versus temperature from 0-1000°K for LiF and 0-800°K for NaF, respectively. The data of Briscoe and Squire (1957) for LiF define a smooth curve offset to lower  $K_S$  values than ours but with a compatible gradient at 298°K. The data point at 298°K from Haussühl (1960) is in agreement with our curve both in absolute value and indicated gradient. The resonance data of Chernov and Stepanov (1961) and Susse (1961) deviate markedly from our curve at higher temperatures even though the former intersects our curve in the neighbourhood of 300°K.

For NaF, there is good agreement between our data  $(300-650^{\circ}K)$  and those of Vallin <u>et al</u>. (1966)  $(0-300^{\circ}K)$  and Lewis <u>et al</u>.(1967)  $(0-300^{\circ}K)$ . In addition the room temperature value of  $K_{\rm S}$  and the temperature gradient of Haussühl (1960) are in agreement with our curve. The values of the bulk modulus from the resonance experiments of Nikanorov and Stepanov (1963) are consistently lower at all temperatures and the absolute value

Table 3	.9: Comp	arison o	f room t	emperatu	re values of	f c and (dc	/aT) from	various invest	igators for LiF and NaF
	°11	c' (kb	ar) <sup>c</sup> 44	К <sub>S</sub>	$\left(\frac{\partial c_{11}}{\partial T}\right)_{p}$	$\left(\frac{\partial c'}{\partial T}\right)_{P}$ (kbar	$\frac{\left(\frac{\partial c_{44}}{\partial T}\right)_{p}}{(deg^{-1})}$	$\left(\frac{\partial K_{\rm S}}{\partial T}\right)_{\rm P}$	Reference
LiF	1144	331	639	704	-0.749	-0.380	-0.183	-0.242	This work
	1137	331	637	696					Miller and Smith (1964)
	1136	330	635	696	-0.749	-0.377	-0.178	-0.247	Haussühl (1960)
	1130	327	637	694					Chernov and Stepanov (1961)
	1111	345	630	651					Briscoe and Squire (1957)
	913	276	598	622					Susse (1961)
NaF	973	368	282	483	-0.624	-0.336	-0.059	-0.177	This work
	970	366	282	482					Miller and Smith (1964)
	970	364	283	485	-0.618	-0.331	-0.059	-0.177	Haussühl (1960)
	970	367	282	481	-0.60	-0.325	-0.085	-0.166	Vallin et al. (1966)
	963	359	279	485					Lewis et al. (1967)
	963	362	276	482	-0.584	-0.308	-0.045	-0.173	Bensch (1972)
	943	372	283	447					Nikanorov and Stepanov (1963



Figure 3.3: Bulk modulus versus temperature for LiF. The dashed curve will be discussed later, when this figure is presented again as Figure 4.10.



Figure 3.4: Bulk modulus versus temperature for NaF. The dashed curve will be discussed later, when this figure is presented again as Figure 4.11.

of their gradient is 50% higher than that of other investigators.

Of particular note in Table 3.9 is the good agreement between our room temperature data and those of Miller and Smith (1964) and Haussühl (1960), both of whom used ultrasonic pulse techniques. The comparisons in Table 3.9 support the accuracy and reliability of our data in the region of 298°K and promote confidence in the elastic moduli data at higher temperatures.

### 3.4 Fluorite-structure fluorides: $CaF_2$ , $SrF_2$ and $BaF_2$ . c(T).

The elastic moduli calculated from equation (3.1) for the five individual modes for CaF<sub>2</sub> and SrF<sub>2</sub> are plotted in Figures 3.5 and 3.6 respectively, while those for the three individual modes for BaF2 are plotted in Figure 3.7. The fitted polynomials are also plotted in Figures 3.5, 3.6 and 3.7. The addition of a quadratic term to the linear fit was statistically significant (at the 99.9% confidence level) for all modes except for  $c_{44}$  ( $v_4$ ) for  $CaF_2$ . For consistency and comparison with the  $c_{4\,4}$   $(v_2)$  mode, the quadratic term for  $c_{4\,4}$   $(v_4)$  was retained. For some modes, the addition of a cubic term was marginally significant; however, simultaneous application of the  $\chi^2$ -test indicated that the reduced  $\chi^2$  value was less than unity for the quadratic fit, which implies that the average scatter of the data about the fitted polynomial was less than the estimated experimental uncertainty. In view of this it was decided that the data required only a second degree polynomial. The polynomial coefficients for all three crystals are listed in Table 3.10.

The values of the elastic moduli and their temperature derivatives calculated by evaluating the polynomials at 298°K are given in Table 3.11 for  $CaF_2$  and  $SrF_2$ . In Table 3.12 are listed the calculated values (from the polynomial) of the elastic moduli and their temperature



Figure 3.5: Elastic moduli versus temperature for the modes  $c_{11}$ , c'',  $c_{44}$ and c' for CaF<sub>2</sub>. The solid lines represent the fitted second degree polynomials for  $c_{11}$ , c'',  $c_{44}$  ( $v_2$ ) and c'. For the  $c_{44}$  shear mode, the polynomial curve for the [110] direction cannot be distinguished from the plotted curve for the [001] direction. Data points for the crosscheck for  $c_{44}$  from the [110] direction are indicated by X. For reasons of clarity, not all the data points used in the fitting procedure are plotted.







Figure 3.7: Elastic moduli versus temperature for the modes c", c' and  $c_{44}$  ( $v_4$ ) for BaF<sub>2</sub>. The fitted polynomials are represented by the solid lines. For reasons of clarity, it was not possible to plot all the data points used in the fitting procedure.

	for Cal	$F_2$ , $SrF_2$ and	BaF <sub>2</sub>	
		A (kbar)	B (kbar.deg <sup>-1</sup> )	C (kbar.deg <sup>-2</sup> x 10 <sup>-3</sup> )
CaF <sub>2</sub>	c <sub>11</sub>	1743.5	-0.2774	-0.1144
	c'	633.1	-0.0846	-0.0439
	$c_{44}(v_2)$	374.2	-0.1184	-0.0046
	c <sub>44</sub> (v <sub>4</sub> )	374.7	-0.1214	-0.0021
	c''	1486.4	-0.3135	-0.0732
SrF <sub>2</sub>	c <sub>11</sub> c'	1310.5 415.4	-0.1873 -0.0422	-0.0810 -0.0253
	c <sub>44</sub> (v <sub>2</sub> )	345.7	-0.0848	-0.0130
	$c_{44}(v_4)$	345.7	-0.0857	-0.0123
	с''	1241.5	-0.2318	-0.0678
BaF <sub>2</sub>	c'	262.2	-0.0279	-0.0161
	С44	278.5	-0.0706	-0.0094
	c''	996.5	-0.2296	-0.0351

Table 3.10: Coefficients of the fitted polynomials,  $c = A + BT + CT^2$ ,

		(	CaF <sub>2</sub>	SrF <sub>2</sub>	
		с	$\left(\frac{\partial c}{\partial T}\right)_{p}$	с	$\left(\frac{\partial c}{\partial T}\right)_{P}$
Mode	Velocity	(kbar)	(kbar.deg <sup>-1</sup> )	(kbar)	(kbar.deg <sup>-1</sup> )
c <sub>11</sub>	v <sub>1</sub>	1650.7±3	-0.346±0.004	1247.5±2	-0.236±0.002
c'	v <sub>3</sub>	604±1	-0.111±0.001	400.6±0.7	-0.0573±0.0007
c <sub>44</sub>	v <sub>2</sub>	338.5±0.6	-0.1212±0.0007	319.3±0.8	-0.0925±0.001
	v <sub>4</sub>	338.3±1	-0.1226±0.0015	319.1±0.7	-0.093±0.0008
c''	v <sub>5</sub>	1386.5±1	-0.357±0.003	1166.4±2	-0.272±0.002
	calc.	1385±5	-0.356±0.006	1166.2±4	-0.271±0.004
KS	calc.	845.4±4	-0.198±0.005	713.4±3	-0.159±0.003

Table 3.11: Single crystal elastic moduli and their temperature derivatives at 298°K for CaF2 and SrF2

		clonen, the column	$\left(\frac{\partial c}{\partial T}\right)_{D}$
Mode	Velocity	(kbar)	(kbar.deg <sup>-1</sup> )
	as shen significant a	252 4+0 5	0.0776±0.006
C.	v	256 7+0 5	-0.0761+0.0005
c''	4 V _	925.0±2	-0.251±0.002
c <sub>I.</sub>	v <sub>6</sub>	927.5±1.4	da stastic andri
Ц	calc.	926.4±2	entation engin of a
с <sub>т</sub>	v <sub>7</sub>	253.8±0.4	of tess Than 0.0
	calc.	253.8±0.5	s, while the offer
ĸs	calc.	581.2±3	-0.162±0.005

Table 3.12: Single crystal elastic moduli and their temperature

derivatives at 298°K for BaF<sub>2</sub>

derivatives for  $BaF_2$ , together with the measured values of  $C_L^{}(v_6)$  and  $C_{}_{}(v_7)$  at room temperature.

The effect of misorientation on the elastic moduli and their temperature derivatives was determined as described in Appendix A, and these errors when significant were incorporated into those listed in Tables 3.11 and 3.12. For CaF<sub>2</sub>, the misorientation errors were comparable with other experimental uncertainties for the elastic moduli (0.2%) and very much less for the derivatives (0.1%). For SrF<sub>2</sub>, the errors arising from misorientation were negligible (< 0.03% for the elastic moduli and < 0.05% for their derivatives). The large misorientation angle of 3.5° for the [110] direction in BaF<sub>2</sub> resulted in errors of less than 0.03% for the elastic moduli and 0.5% for the derivatives, while the effect of misorientation in the [11] direction was negligible. The insensitivity of the elastic wave velocities of BaF<sub>2</sub> to misorientation results from its near isotropy (i.e., c'  $\frac{1}{2}$  c<sub>44</sub>).

For  $CaF_2$  and  $SrF_2$ , the crosschecks are provided by comparing  $c_{44}$ from  $v_2$  and  $v_4$  and by comparing c" (measured) and c" (calculated from  $c_{11}$ , c' and  $c_{44}$ ); the agreement is better than 0.1% for the elastic moduli and 2% for the derivatives, well within the calculated uncertainties. For  $BaF_2$ , the room temperature crosschecks are provided by comparing the calculated and measured values of  $C_L$  and  $C_T$  which agree to approximately 0.1%. Crosschecks for the temperature derivatives were not possible because development of the crack in the specimen prevented further hightemperature measurements.

In Table 3.13, values of the elastic moduli from other investigators are listed for comparison with our new data for  $CaF_2$ ,  $SrF_2$  and  $BaF_2$  at  $^{298}$ °K. For  $CaF_2$  and  $SrF_2$ , the value tabulated for  $c_{44}$  is the average of the values from  $v_2$  and  $v_4$  in Table 3.11. The agreement is good for  $CaF_2$ with the exception of the values of Nikanorov <u>et al</u>. (1968) and Huffman

	c <sub>11</sub>	c'	С44	ĸ <sub>s</sub>	$\left(\frac{\partial c_{11}}{\partial T}\right)_{p}$	$\left(\frac{\partial c'}{\partial T}\right)_{P}$	$\left(\frac{\partial c_{4,4}}{\partial T}\right)_{p}$	$\left(\frac{\frac{\partial K_{S}}{\partial T}}{\frac{\partial T}{\partial T}}\right)_{p}$	
		(kbar)				(kbar.deg <sup>-1</sup> )		<u>e 4 I</u>	Reference
CaF <sub>2</sub>	1651 1642 1635.7 1649.4 1652 1652.6 1700 1640	604 601.2 597.8 601.6 599 599 590 555	338 337.0 339.2 338.0 337 337.5 341 337.0	845 841 838.6 847.3 853.3 854 913.3 900	-0.346 -0.318 -0.335	-0.111 -0.107 -0.104	-0.122 -0.122 -0.116	-0.198 -0.176 -0.197	This work Wong and Schuele (1968) Haussühl (1963) Ho and Ruoff (1967) Brielles and Vidal (1975) Vidal (1974) Nikanorov <u>et al.</u> (1968) Huffman and Norwood (1960)
SrF <sub>2</sub>	1247.5 1236 1246.1	400.6 402.3 399.9	319 313.2 318.74	713.7 699.6 713.0	-0.236 -0.198 -0.239	-0.057 -0.017 -0.057	-0.093 -0.085 -0.092	-0.159 -0.175 -0.162	This work Gerlich (1964b) Alterovitz and Gerlich (1970)
BaF <sub>2</sub>	920.8 919.9 912.2 894.8 891.5	252.4 252.1 248.7 254.7 245.7	256.7 256.8 255.1 249.5 253.5	581.2 583.8 580.6 555.2 594.3	-0.212 -0.204 -0.206	-0.0375 -0.0368 -0.0359	-0.076 -0.0734 -0.0735	-0.162 -0.155 -0.158	This work Wong and Schuele (1968) Haussühl (1963) Gerlich (1968) Gerlich (1964a)

<u>Table 3.13:</u> Comparison of room temperature values of c and  $(\partial c/\partial T)_p$  from various investigators for CaF<sub>2</sub>, SrF<sub>2</sub> and BaF<sub>2</sub>
and Norwood (1960). Similarly for  $BaF_2$ , the agreement is generally good with the exception of the values of Gerlich (1964a, 1968). Our values of the elastic moduli for  $SrF_2$  agree very well with those of Alterovitz and Gerlich (1970), but not as well with those of Gerlich (1964b).

Also compared in Table 3.13 are the values of the temperature derivatives of the elastic moduli,  $(\partial c/\partial T)_p$  at 298°K. Our values of  $(\partial c_{44}/\partial T)_p$  for CaF<sub>2</sub> and SrF<sub>2</sub> are obtained by averaging the values from  $v_2$  and  $v_4$  listed in Table 3.11. For CaF<sub>2</sub>, there is good agreement between our values and those of Wong and Schuele (1968) and Haussühl (1963); in particular, there is striking agreement between our value of  $(\partial K_S/\partial T)_p$  and that of Haussühl (1963). The values of Alterovitz and Gerlich (1970) for SrF<sub>2</sub> agree exceptionally well with all of our values for  $(\partial c/\partial T)_p$ ; the agreement is much better than for the earlier data of Gerlich (1964b). For BaF<sub>2</sub>, there is good agreement among the values of  $(\partial c/\partial T)_p$  from the present work and those of Wong and Schuele (1968) and Haussühl (1963).

As for LiF and NaF, the available high T data from various sources may be readily compared in Figure 3.8 which is a plot of adiabatic bulk modulus,  $K_S$ , versus temperature from different investigators from 0-1123°K for CaF<sub>2</sub>, and from 0-650°K for SrF<sub>2</sub> and BaF<sub>2</sub>. The low temperature values of  $K_S$  for CaF<sub>2</sub> calculated from c<sub>11</sub> and c<sub>12</sub> of Huffman and Norwood (1960) do not follow a smooth curve and are offset to higher  $K_S$  values than ours, as are the high temperature resonance data of Nikanorov <u>et al</u>. (1968). The  $K_S$  values from both these studies were considerably higher than those of all other investigators at 298°K in Table 3.13. However the  $K_S$ -T data of Nikanorov <u>et al</u>. (1968) does follow the general trend of the present  $K_S$ -T data. The  $K_S$ -T data from Vidal (1974) obtained by resonance techniques is considerably different in gradient from our curve (approximately 50% difference in  $(\partial K_S/\partial T)_p$ ) although there is agreement with our curve at room temperature. However,





the agreement of our values for  $(\partial c/\partial T)_p$  at 298°K with other data obtained by ultrasonic pulse techniques in Table 3.13 support the reliability of the trend of our high temperature data for CaF<sub>2</sub>.

Also plotted in Figure 3.8 are the low temperature  $K_S^{-T}$  data for  $SrF_2$  calculated from 4-280°K from the single crystal elastic moduli of Gerlich (1964b) as well as our high temperature  $K_S^{-T}$  data from 300°-650°K. The low temperature curve is slightly offset from our curve and slightly steeper at room temperature; however, as pointed out in the earlier discussion of Table 3.13, Gerlich's (1964b) values differ from the present values and those of Alterovitz and Gerlich (1970), evaluated at 298°K.

The low temperature  $K_S^{-T}$  data for  $BaF_2$  from 0-280°K plotted in Figure 3.8 were calculated from the values of  $c_{11}$  and  $c_{12}$  read from Figure 1 of Gerlich (1964a). Even though such values are not likely to be very accurate they are sufficient to indicate the trend of the low temperature data curve which is offset from our curve at 298°K and also somewhat steeper in slope. Comparisons of the various data in Table 3.13 indicate that the room temperature value and gradient for our  $K_S^{-T}$ curve is reliable and promote confidence in the high temperature data for  $BaF_2$ .

#### 3.5 Rutile-structure fluorides: $MgF_2$ . c(T).

The elastic moduli calculated from equation (3.1) for MgF<sub>2</sub> are plotted in Figure 3.9 for all eleven modes in Table 3.2 together with the fitted polynomials (Table 3.14). The primary modes for  $c_{11}$ ,  $c_{66}$ , c',  $c_{33}$ ,  $c_{44}$  ( $v_8$ ) and  $C_{L_2}$  were measured from 298-650°K while the modes for the crosschecks,  $c_{44}$  ( $v_3$  and  $v_6$ ),  $C_{L_1}$ ,  $C_{T_1}$ , and  $C_{T_2}$  were measured from 298-370°K. The fitted polynomials were determined to be quadratics in T at a confidence level of better than 99.9% for all modes by the simultan-





Table 3.14: Coefficients of the polynomials,  $c = A + BT + CT^2$ ,

Mode	A (kbar)	$(\text{kbar.deg}^{-1})$	$(kbar.deg^{-2} \times 10^{-3})$
	louisted as the VRH (	olgt-Kmss-H11() a	vertage, i.e. the
c11	1455.9	-0.1294	-0.1053
c <sub>66</sub>	1038.0	-0.2650	-0.0206
С44	581.5	-0.0296	-0.0651
c <sub>L1</sub>	2237.3	-0.3449	-0.2144
с'	251.9	+0.0137	-0.0214
C44	582.5	-0.0307	-0.0625
c33	2141.8	-0.2775	-0.0741
C44	586.7	-0.0571	-0.0292
c <sub>L2</sub>	1839.4	-0.2092	-0.0713
c <sub>T2</sub>	544.0	-0.0297	-0.0974
C <sub>T</sub>	808.4	-0.1312	-0.0641

fitted to the c-T data for  $MgF_2$ 

eous application of the F-test and  $\chi^2$ -test described previously.

The values of the elastic moduli and their temperature derivatives calculated by evaluating the polynomial equations at 298°K are listed in Table 3.15 for  $MgF_2$  together with the appropriate errors. The value of  $K_{c}$  is calculated as the VRH (Voigt-Reuss-Hill) average, i.e. the arithmetic mean of the Voigt and Reuss averages for the moduli of a polycrystalline aggregate (Hill, 1952). In the absence of a theoretical formulation for the P and T derivatives of the aggregate moduli, it was assumed that  $(\partial K_{c}/\partial T)$  could be represented by the arithmetic mean of the values of ( $\partial K_{\rm S}^{}/\partial T)$  calculated from the Voigt and Reuss formulae. The upper and lower bounds for  $\rm K_S$  and ( $\rm \partial K_S/\partial T)$  are respectively 1023 and 1015 kbar, and 0.1604 and 0.1599 kbar. deg<sup>-1</sup>. The errors due to misorientation were calculated as described in Appendix A and when significant were incorporated into the errors listed in Table 3.15. For the [001] direction the errors were insignificant (< 0.04% for the elastic moduli and < 0.1% for their temperature derivatives). The errors for the [100] direction are less than 0.2% for the elastic moduli and less than 0.5% for their temperature derivatives. For the [110] direction, the errors in the elastic moduli were less than 0.2% and in their temperature derivatives less than 0.02% except for  $(\partial c'/\partial T)_p$  for which the error is 13% (which appears large only because  $(\partial c'/\partial T)_p$  is near zero). Consequently, the misorientation of less than 0.3° for the propagation direction at 45° to the [100] and [010] directions was assumed to have negligible effect on the elastic moduli and their temperature derivatives.

For MgF<sub>2</sub>, the crosschecks are provided by the comparison of  $c_{44}$ from  $v_3$ ,  $v_6$  and  $v_8$ , and by the comparison of the measured values of  $C_{L_1}$ ,  $C_{T_1}$  and  $C_{T_2}$  with those calculated from the six primary modes. The crosschecks for the elastic moduli are good to within 0.25%. For  $(\partial c_{44}/\partial T)_p$  the values from  $v_3$  and  $v_6$  agree to within 0.6% whereas the

		С	$\left(\frac{\partial c}{\partial T}\right)_{D}$
Mode	Velocity	(kbar)	$(kbar.deg^{-1})$
c <sub>11</sub>	v <sub>1</sub>	1408±6	-0.192±0.007
c <sub>66</sub>	v <sub>2</sub>	957±5	-0.277±0.007
c'	v <sub>5</sub>	254±1	+0.0009±0.0004
c33	v <sub>7</sub>	2053±6	-0.322±0.006
c <sub>44</sub>	v <sub>8</sub>	567±1	-0.0746±0.0007
c <sub>L2</sub>	v <sub>9</sub>	1771±5	-0.252±0.005
c <sub>12</sub>	calc.	900±5	-0.194±0.007
c <sub>13</sub>	calc.	635±11	-0.086±0.025
ĸ <sub>s</sub>	calc.	1019±7	-0.160±0.015
c <sub>44</sub>	v <sub>3</sub>	567±3	-0.0683±0.007
	v <sub>6</sub>	568±2	-0.0679±0.004
c <sub>L1</sub>	v <sub>4</sub>	2115±21	-0.473±0.071
	calc.	2111±9	-0.470±0.012
c <sub>T2</sub>	v <sub>10</sub>	527±8	-0.088±0.026
	calc.	527±13	-0.080±0.019
c <sub>T1</sub>	v <sub>11</sub>	764±7	-0.169±0.017
	calc.	762±3	-0.176±0.004

Table 3.15: Single crystal elastic moduli and their temperaturederivatives at 298°K for MgF2

where enloyinged from their lingur equations in T for the everyon dynamic and shear valueities of a number of polycrystalline the the values of K<sub>5</sub> are the VBH averages colouisted at each which from the single crystal robbil. The difference batters the oblication aggregate averages is indicated in Figure 1.10. Also values from  $v_6$  and  $v_8$  agree to within 10%. The calculated and measured values of  $(\partial C_{L_1}/\partial T)_p$ ,  $(\partial C_{T_1}/\partial T)_p$  and  $(\partial C_{T_2}/\partial T)_p$  all agree to within 10%. The errors associated with the measured crosscheck modes are large due to the limited temperature range and the small number of data points used in the polynomial fitting procedure; the large errors in the calculation of these elastic moduli and their temperature derivatives result from the propagation of errors, since these elastic moduli are complicated functions of the six independent elastic moduli. In view of this, the crosschecks are quite satisfactory.

In Table 3.16, values of the elastic moduli from other investigators are listed for comparison with our new data for  $MgF_2$  at 298°K. The agreement is generally good with the exception of the values of Cutler <u>et al.</u> (1968) which are all too low (except for c' and  $c_{66}$ ). Our value of the isotropic bulk modulus (VRH average) compares favourably with the polycrystalline data of Bailey <u>et al.</u> (1975).

Also compared in Table 3.16 are the values of  $(\partial c/\partial T)_p$  at 298°K from various investigators. The values attributed to Aleksandrov <u>et al</u>. (1969) are determined from their values at 20°C and -100°C together with their statement that the elastic moduli depend linearly on temperature in this range. The agreement between the various values is generally satisfactory.

In Figure 3.10, the present values of  $K_S$  versus T are compared with those of Bailey <u>et al</u>. (1975). The values of  $K_S$  for Bailey <u>et al</u>. (1975) were calculated from their linear equations in T for the average compressional and shear velocities of a number of polycrystalline samples. Our values of  $K_S$  are the VRH averages calculated at each temperature from the single crystal moduli. The difference between the Voigt and Reuss aggregate averages is indicated in Figure 3.10. Also plotted in Figure 3.10 are the two data points calculated from the single

	c11	c <sub>33</sub>	c <sub>12</sub>	c <sub>13</sub>	С44	c <sub>66</sub>	с'	ĸ <sub>s</sub>	Reference
С	1408	2053	900	635	567	957	254	1019	This work
(kbar)	1395	2041	897	625	564	951	249	1010	Aleksandrov et al. (1060)
	1237	1770	732	536	552	978	252	869	$\begin{array}{c} \text{AlexSalidiov}  et \ al. \ (1909) \\ \text{Cutler et al} \ (1968) \end{array}$
	1427	2040	922	641	567	935	252	1030	Davies $(1976)$
	1399	2042	893	637	570	954	253	1015	Haussühl (1968)
	-	-	-	-	-	-	-	1035	Bailey <u>et al</u> . (1975)
$\left(\frac{dc}{dT}\right)_{P}$								1	
(kbar.deg <sup>-1</sup> )	-0.192	-0.322	-0.194	-0.086	-0.075	-0.277	+0.0009	-0.160	This work
	-0.233	-0.308	-0.183	-0.050	-0.058	-0.308	-0.025	-0.151	Aleksandrov et al. (1969)
	-0.215	-0.294	-0.223	-0.051	-0.063	-0.267	+0.004	-0.155	Haussühl (1968)
	-	-	-		-	-	-	-0.176	Bailey et al. (1975)

Table 3.16: Comparison of room temperature values of c and  $(\partial c/\partial T)_{P}$  for MgF<sub>2</sub> from various investigators



Figure 3.10: Bulk modulus versus temperature for  $MgF_2$ . The solid curve will be discussed later, when this figure is presented again as Figure 4.13.

crystal elastic moduli of Aleksandrov <u>et al</u>. (1969) at 173°K and 293°K. Except for a slight offset, the present  $K_S$ -T data curve and that from Bailey <u>et al</u>. (1975) agree very well over the entire high temperature range. This agreement between the bulk modulus calculated as a complicated function of the single crystal elastic moduli and that determined from many polycrystalline samples indicates the compatibility of both sets of high temperature data.

#### 3.6 Perovskite-structure fluorides: KMgF<sub>3</sub>. c(T), c(P).

The elastic moduli were not calculated as a function of temperature in the absence of thermal expansion data for KMgF<sub>3</sub>. The pulse repetition frequencies,  $f_R$ , versus T are plotted in Figure 3.11 for the three individual modes for the [110] direction (Table 3.1), together with the fitted straight lines. Only a straight line fit to the  $f_R$ -T data was statistically significant. The coefficients of these linear equations are given in Table 3.17.

The values of the elastic moduli calculated from the linear  $f_R^{-T}$  equations at 298°K are given in Table 3.18. The errors due to misorientation were negligible. The temperature dependence of the elastic moduli was expressed in the form

$$\left(\frac{d \ln c}{dt}\right) = -\alpha + 2\left(\frac{d \ln f_R}{dT}\right)$$
(3.13)

where  $\alpha$  is the linear coefficient of thermal expansion. Equation (3.13) is obtained by differentiating equation (3.1) with respect to T and then by dividing the resultant equation by equation (3.1). The temperature dependence of the elastic moduli at 298°K can then be found directly from equation (3.13), once the value of the thermal expansion coefficient is known. In Table 3.18 are listed the values of ( $\partial \ln f_R / \partial T$ )<sub>p</sub> together with the appropriate errors. If the linear thermal expansion coefficient





	f <sub>R</sub> = A + BT, for KMgF <sub>3</sub>	fitted to the f <sub>R</sub> -T da	ata
	A (kHz)	B (kHz.deg <sup>-1</sup> )	
c'	393.29	0.09708	
c44	404.89	0.02685	
c''	680.61	0.06976	

Table 3.17: Coefficients of the straight lines,

Table 3.18: Room temperature values of the elastic moduli for  $KMgF_3$  and

Mode	Velocity	c (kbar)	$ \begin{pmatrix} \frac{d \ln f_R}{dT} \end{pmatrix}_{P} \\ (10^{-3} \text{ deg}^{-1}) $	$ \begin{pmatrix} \frac{dlnc}{dT} \\ p \\ (10^{-3} \text{ deg}^{-1}) \end{pmatrix}$	$\left(\frac{dc}{dT}\right)_{p}$ (kbar.deg <sup>-1</sup> )
c'	v <sub>3</sub>	471.9±1	-0.4937±0.0006	-0.5313±0.0013	-0.251±0.001
C44	v <sub>4</sub>	500.1±1	-0.1326±0.0003	-0.1702±0.0008	-0.085±0.001
c''	v <sub>5</sub>	1413.3±3	-0.205±0.0008	-0.243±0.002	-0.343±0.004
c11	calc.	1385±5			-0.509±0.006
c <sub>12</sub>	calc.	441±5			-0.007±0.006
ĸ <sub>s</sub>	calc.	756±4			-0.174±0.005

† See Footnote p. 29.

is assumed to be 3.76 x  $10^{-5} \text{ deg}^{-1}$  for KMgF<sub>3</sub><sup>+</sup> (see footnote), values for  $(\partial \ln c/\partial T)_p$  and  $(\partial c/\partial T)_p$  can be calculated at 298°K and these are also tabulated in Table 3.18.

The values of  $f_R$  versus pressure to 2.5 kbar for KMgF<sub>3</sub> are plotted in Figures 3.12, 3.13 and 3.14 for c',  $c_{44}$  and c" respectively, together with the fitted straight lines (Table 3.19). Only a linear fit to the data was justified for the small number of data points which span a limited pressure range. For c', run 2 data was analysed in preference to run 1 data, since the decreasing P data points for run 1 did not exactly follow the trend for increasing P. In addition,  $f_R$  evaluated at 1 bar and 298°K from run 2 is in much better agreement with the corresponding value from the temperature run. The data for run 3 for  $c_{44}$  (see Figure 3.13) were taken as the primary  $f_R$ -P data since these data are more numerous and reproducible than for runs 1 and 2. The data for c" versus pressure are reproducible within the limit of experimental uncertainty in determining  $f_R$ , which was larger for this mode. The above pressure measurements are limited to 2.5 kbars, since at higher pressures the data are not reproducible.

In Table 3.20 are listed values of the elastic moduli and their pressure derivatives for  $KMgF_3$  at 298°K. The elastic moduli at 298°K determined from the pressure runs agree to within 0.06% of those determined from the temperature runs (Table 3.18), which is of the order of the uncertainty expected from the straight line fitting procedure. (The larger errors listed in Tables 3.18 and 3.20 result from the incorporation

This value of  $\alpha$  for KMgF<sub>3</sub> is determined by multiplying by 4 the value of  $\alpha$  for SrTiO<sub>3</sub> (Lytle, 1964). This follows from the thermal expansion studies of Megaw (1939) and Austin (1952) which demonstrated that for compounds with the same structure,  $\alpha$  is proportional to  $Z_c Z_a$ where  $Z_c$ ,  $Z_a$  are the cationic and anionic valence charges respectively.













Table 3.19: Coefficients of the straight lines,  $f_R = A + BP$ ,

		A (kHz)		B (kHz.kbar <sup>-1</sup> )
	an Carlo		100.00	10002.04-0.1
c' (run 1)		393.69		1.18
c' (run 2)		393.40		1.13
c <sub>44</sub> (run 1)		404.71		0.43
c <sub>44</sub> (run 2)		404.76		0.43
c <sub>44</sub> (run 3)		404.75		0.44
c''		680.59		1.6

fitted to the  $f_R$ -P data for KMgF<sub>3</sub>

able	3.20:	Elastic	moduli	and	their	pressure	derivatives	at
aure	5.20.	LIUSCIC	mouull	anu	cherr	pressure	der.	ivatives

Mode	Velocity	c (kbar)	$\frac{dc}{dp}$
c'	v <sub>3</sub>	472.2±1	2.94±0.12
C <sub>44</sub>	v <sub>4</sub>	499.8±1	1.31±0.03
c''	v <sub>5</sub>	1413.2±3	7.3±0.4
c <sub>11</sub>	calc.	1386±5	8.93±0.55
c <sub>12</sub>	calc.	441±5	3.05±0.55
ĸs	calc.	756±4	5.01±0.47

1 bar and 298°K for KMgF3

Diffising the precise technique of prize hepergosition, so have district as a function of temperature (and pressure) the single crystal distic moduli of several fluorides divitabilizing in the rechemit. Therets, sutile and perovskite structures. The teliability of our data supported by its internal consistency and compatability with other dis. In general, crosschecks are good to within 0.25% for the sidetion moduli and 5% for their temperature derivatives for LiF. Saf. CaF2. SrP2 and MgF2. These results are evidence for the seliability of our data for MgF2. These results are evidence for the seliability of our data for

The Agreement between our values of the electic moduli and their Superature derivatives at 298 K and these of other investigators using Straining pulse techniques attents to the religibility of our derivat of the measurement errors for  $\rho_{\circ}$  and  $\ell_{\circ}$ ). It is worth pointing out that the values of  $(\partial c/\partial P)_{T}$  calculated from the less reliable runs for c' and  $c_{44}$  lie within the uncertainty limits on the values of  $(\partial c/\partial P)_{T}$  listed in Table 3.20.

In Table 3.21, our values of the elastic moduli at 298°K for  $KMgF_3$  are compared with those of other investigators. There is very good agreement between our values and those of Reshchikova (1969) while the values of Rosenberg and Wigmore (1967) all appear too low.

The values of  $(\partial c/\partial T)_p$  at 298°K are also compared in Table 3.21. The agreement between our values of  $(\partial c/\partial T)_p$  calculated neglecting thermal expansion and those of Reshchikova (1969), who also ignored thermal expansion, is excellent. Table 3.21 also illustrates that the effect of neglecting thermal expansion is an error of approximately 10% in all the  $(\partial c/\partial T)_p$  except for the smaller magnitude  $(\partial c_{44}/\partial T)_p$  for which the error is approximately 25%.

#### 3.7 Conclusion

Utilising the precise technique of pulse superposition, we have measured as a function of temperature (and pressure) the single crystal elastic moduli of several fluorides crystallising in the rocksalt, fluorite, rutile and perovskite structures. The reliability of our data is supported by its internal consistency and compatability with other data. In general, crosschecks are good to within 0.25% for the elastic moduli and 5% for their temperature derivatives for LiF, NaF, CaF<sub>2</sub>, SrF<sub>2</sub> and MgF<sub>2</sub>. These results are evidence for the reliability of our data for KMgF<sub>3</sub> (no crosschecks) and BaF<sub>2</sub> (room temperature crosschecks only).

The agreement between our values of the elastic moduli and their temperature derivatives at 298°K and those of other investigators using ultrasonic pulse techniques attests to the reliability of our data in

Table 3.21:	Comparison	of	the	room	temperature	values	of	С	and	$(\partial c/\partial T)_{p}$
							-			P

## for KMgF<sub>3</sub> from various investigators

c <sub>11</sub>	c' (kb	c' c <sub>44</sub> (kbar)		Reference		
	in precise	inter data wi	11 bit topte	al to the discussions of		
1385	472	500	756	This work		
1380.1	471.8	498.3	751.1	Reshchikova (1969)		
1320	462	485	704	Rosenberg and Wigmore (1967)		

$\left(\frac{\partial c_{11}}{\partial T}\right)_{p}$	$\left(\frac{\partial c'}{\partial T}\right)_{p}$ (kbar	$\left(\frac{\frac{\partial c_{44}}{\partial T}}{\frac{\partial T}{T}}\right)_{p}$ .deg <sup>-1</sup> )	$\left(\frac{\partial K_{S}}{\partial T}\right)_{p}$	
-0.509	-0.251	-0.085	-0.174	This work
-0.46	-0.23	-0.066	-0.153	This work neglecting thermal expansion
-0.47	-0.23	-0.061	-0.163	Reshchikova (1969)

the room temperature region and promotes confidence in our elastic moduli data at higher temperatures. Our high temperature data appear to be superior to the existing high temperature elastic data determined from resonance experiments.

These precise new data will be central to the discussions of high temperature elastic behaviour (Chapter 4) and elastic modulus systematics (Chapter 5).

#### CHAPTER 4

#### HIGH TEMPERATURE ELASTICITY

4.1 Introduction

4.2 Intrinsic and extrinsic temperature dependence of the elastic moduli

4.3  $(\partial c/\partial T)$  versus T for LiF and NaF

4.4 ( $\partial c/\partial T$ ) versus T for CaF<sub>2</sub>, SrF<sub>2</sub> and BaF<sub>2</sub>

4.5 ( $\partial c/\partial T$ ) versus T for MgF<sub>2</sub>

4.6 High temperature equations of state

4.7 Conclusion

#### CHAPTER 4

#### HIGH TEMPERATURE ELASTICITY

#### 4.1 Introduction

Many workers, both in the fields of solid state physics and earth sciences, have been interested in the characterisation of the temperature dependence of the elastic moduli; such studies have involved either experimental determinations or theoretical derivations (or both). There are many reasons for this interest. The parameters in various interatomic force models can be further constrained by information on the behaviour of the elastic moduli, c, versus temperature, leading to a greater understanding of the nature of the short range repulsive forces in the lattice. Such an approach assumes that the elastic behaviour versus temperature is correctly described by the particular lattice dynamical model; for instance, Garber and Granato (1975) expressed the temperature dependence of the second-order elastic constants in terms of second-order, third-order and fourth-order elastic constants. Alternatively, the experimentally determined values of c-T can be employed in testing the validity of certain lattice dynamical approaches as well as in supporting semi-empirical derivations. An understanding of the dynamic lattice is essential in assessing thermal and finite compression effects so that physical properties can be extrapolated to pressures and temperatures beyond the accessible laboratory ranges; these extrapolations have special importance in geophysical discussions of the Earth's interior, where pressures of 3.5 Mbar and temperatures of greater than 3000°K are achieved.

The regimes of low- and high-temperature elasticity have received particular attention in theoretical studies of the solid state. Here "low" temperature refers roughly to the "T<sup>3</sup>" region in the Debye theory of specific heat and "high" temperature refers to temperatures above which all of the lattice vibrational modes are activated and the

classical Dulong-Petit specific heat limit is attained (.i.e., for  $T > \theta_D$ , the Debye temperature). Various formulations of finite strain equations of state depend on the knowledge of the high temperature value of  $(\partial K/\partial T)_p$  in the reference state so that thermal effects can be incorporated (e.g., Thomsen and Anderson, 1969; Thomsen, 1970, 1972; Davies, 1973). The temperature derivatives of the elastic moduli,  $(\partial c/\partial T)_p$ , at high temperatures are also important to discussions of lattice instability theories of melting (e.g., Jackson and Liebermann, 1974).

The dependence of the elastic moduli on pressure and temperature is a direct consequence of lattice anharmonicity. Such behaviour is not predicted by harmonic theories which are based on the assumption that the interatomic potential energy can be expanded as a power series in atomic displacements terminated after the quadratic term. Harmonic theories predict that the elastic moduli should be independent of temperature and pressure and that the thermal expansion should be zero (see Kittel, 1971, chapter 6; Leibfried and Ludwig, 1961).

Anharmonic effects were considered by Grüneisen (1926) in his explanation of the thermal expansion of solids. Born and his co-workers<sup>†</sup> presented a thorough thermodynamical characterisation of solids in which calculations of the elastic moduli versus temperature were carried out for various values of the exponents m and n in the power law potential,  $\Phi = \frac{A}{r^{m}} + \frac{B}{r^{n}}$ . The approaches of both Born and Grüneisen were restricted by the use of such a simple, power law interatomic potential.

Leibfried and Hahn (1958) employed a more generalized approach to arrive at the now commonly accepted result that the elastic moduli are linearly decreasing in temperature at high temperatures (T >>  $\theta_D$ , where  $\theta_D$  is the Debye temperature) and are approximately constant with temperature at low temperatures (T <<  $\theta_D$ ) (see Figure 4.1). This

e.g., Born (1943), Born and Bradburn (1943), Bradburn (1943), Furth (1944), Gow (1944).



# TEMPERATURE, T

<u>Figure 4.1</u>: Plot of  $K_S$  versus T demonstrating the general behaviour of the elastic moduli as a function of temperature. At very low temperatures,  $K_S$  is approximately constant while at high temperatures  $K_S$  is almost linear in T.

The theories of tarper and transits (this) and karperters (the second is a solution of the electric moduli be function of temperature, without the restriction of Leibfried and Hahn with the temperature dependent part of the electric moduli should

results from their expression for the elastic moduli,  $c_{ij}$ , in terms of the internal vibrational energy,  $\bar{\epsilon}$ 

$$c_{ij} = c_o (1 - D\overline{\epsilon}) \tag{4.1}$$

where D is a parameter which depends on the crystal structure and on the model employed. Nevertheless, some doubt has been cast on the ability of this theory to correctly predict the magnitude of the  $(\partial c/\partial T)_p$  (see Slagle and McKinstry, 1967). An extensive treatise on on the theory of anharmonic effects in crystals by Leibfried and Ludwig (1961) arrives at the same conclusion for the behaviour of  $c_{ij}$ versus T as the Leibfried and Hahn (1958) paper. However, this later treatment is more satisfactory in the agreement between the experimental and theoretical curves for the  $c_{ij}$  as a function of temperature.

An important point to note in the discussion of these lattice dynamical theories is that they are couched in terms of volume (strain) and temperature as the independent variables, whereas in the experimental regime the measured variables are pressure (stress) and temperature. It appears, therefore, from the form of the high temperature equations that the predicted linearity should occur at constant volume, rather than at constant pressure (see also Thomsen, 1972). This is supported by Stern's (1958) theory of the anharmonic properties of solids which is formulated in terms of stress and temperature. Stern demonstrated that the temperature derivative of the adiabatic compressibility was proportional to the specific heat at constant pressure which increases with temperature; this implies that the adiabatic bulk modulus should not depend linearly on temperature at constant pressure.

The theories of Garber and Granato (1975) and Mitskevich (1965) also illustrate the high temperature linearity of the elastic moduli as a function of temperature, without the restriction of Leibfried and Hahn (1958) that the temperature dependent part of the elastic moduli should

be proportional to the vibrational energy. Finite strain theories of Thomsen (1970, 1972) and Davies (1973), the so-called 4th order anharmonic theories, extend the considerations of Leibfried and Ludwig (1961) who discussed the effect of temperature and infinitesimal strain. This should obviate the difficulty that classical theories of lattice dynamics are not valid where the strains become larger.

However, all of the preceding theories are limited by their reliance on the quasi-harmonic approximation. This can be illustrated briefly as follows. The isothermal elastic moduli are defined as

$$c_{ijkl}^{T} = \frac{1}{V_{\circ}} \left( \frac{\partial^{2} F}{\partial \eta_{ij} \partial \eta_{kl}} \right)_{T} \qquad i,j,k,l = 1,2,3 \qquad (4.2)$$

where  $n_{ij}$ ,  $n_{kl}$  are measures of the strain and F, the Helmholtz free energy, is given in the quasi-harmonic approximation by

$$F = \Phi_{\circ} + F_{\text{harmonic}} + F_{\text{anharmonic}}$$
(4.3)

 $\Phi_{\circ}$  being the static lattice potential energy. The term  $F_{anharmonic}$  is an explicit function of T only and does not contribute to the elastic moduli in (4.2).  $F_{harmonic}$  is represented by the harmonic expression

$$F_{\text{harmonic}} = \sum_{k} \{ \frac{\hbar\omega}{2} + kT \ln \left[ 1 - \exp \left( - \frac{\hbar\omega}{kT} \right) \right] \}$$
(4.4)

with the proviso that the vibrational frequencies,  $\omega$ , are now explicit functions of volume (strain). The validity of this quasi-harmonic approximation may be subject to doubt at temperatures where the thermal vibrations become large (e.g. Leibfried and Ludwig, 1961).

Semi-empirical equations of state, for example Anderson's (1966) version of Wachtman's equation, avoid the difficulty of correctly describing the anharmonic effects by relating the elastic moduli to the measured values of other properties which reflect the contributions of high temperature anharmonicity (e.g., the enthalpy data). This approach has also been followed by Madan (1971) and will be discussed later in this Chapter.

Our new experimental data for the elastic moduli at high temperatures will be discussed in terms of the theories of high temperature elasticity for the rocksalt, fluorite, rutile and perovskite structures. Particular attention will be paid to the question of the relative onset of the high temperature elastic regime for the fluorides and their oxide analogues.

# 4.2 Intrinsic and extrinsic temperature dependence of the elastic moduli

To evaluate the various theoretical predictions of the high temperature behaviour of the elastic moduli, it is useful to express the measured temperature dependence as a combination of intrinsic and extrinsic components:

$$\begin{pmatrix} \frac{\partial c}{\partial T} \end{pmatrix}_{P} = \begin{pmatrix} \frac{\partial c}{\partial T} \end{pmatrix}_{V} + \begin{pmatrix} \frac{\partial c}{\partial P} \end{pmatrix}_{T} \begin{pmatrix} \frac{\partial P}{\partial V} \end{pmatrix}_{T} \begin{pmatrix} \frac{\partial V}{\partial T} \end{pmatrix}_{P}$$
  
intrinsic extrinsic  

$$= \begin{pmatrix} \frac{\partial c}{\partial T} \end{pmatrix}_{V} - \alpha_{V} K_{T} \begin{pmatrix} \frac{\partial c}{\partial P} \end{pmatrix}_{T}$$

$$= \begin{pmatrix} \frac{\partial c}{\partial T} \end{pmatrix}_{V} - \frac{\alpha_{V} K_{S}}{(1 + \alpha_{V} \gamma T)} \begin{pmatrix} \frac{\partial c}{\partial P} \end{pmatrix}_{T}$$

$$= \begin{pmatrix} \frac{\partial C}{\partial T} \end{pmatrix}_{V} - \frac{\alpha_{V} K_{S}}{(1 + \alpha_{V} \gamma T)} \begin{pmatrix} \frac{\partial c}{\partial P} \end{pmatrix}_{T}$$

$$= \begin{pmatrix} \frac{\partial C}{\partial T} \end{pmatrix}_{V} - \frac{\alpha_{V} K_{S}}{(1 + \alpha_{V} \gamma T)} \begin{pmatrix} \frac{\partial C}{\partial P} \end{pmatrix}_{T}$$

$$= \begin{pmatrix} \frac{\partial C}{\partial T} \end{pmatrix}_{V} - \frac{\alpha_{V} K_{S}}{(1 + \alpha_{V} \gamma T)} \begin{pmatrix} \frac{\partial C}{\partial P} \end{pmatrix}_{T}$$

$$= \begin{pmatrix} \frac{\partial C}{\partial T} \end{pmatrix}_{V} - \frac{\alpha_{V} K_{S}}{(1 + \alpha_{V} \gamma T)} \begin{pmatrix} \frac{\partial C}{\partial P} \end{pmatrix}_{T}$$

where Volume thermal expansion

 $\alpha_{\rm V} = \frac{1}{\rm V} \left(\frac{\partial \rm V}{\partial \rm T}\right)_{\rm P}$ 

 $K_{T} = -V \left(\frac{\partial P}{\partial V}\right)_{T}$ 

Isothermal bulk modulus

Adiabatic bulk modulus

 $K_{S} = K_{T} (1 + \alpha_{V} \gamma T)$  $\gamma = \frac{\alpha_{V} K_{S}}{\rho C_{p}}$ 

Thermal Grüneisen parameter

Specific heat (per gram) at constant P =  $C_p$ 

Values of  $C_p$  and  $\gamma$  for LiF, NaF, CaF<sub>2</sub>, SrF<sub>2</sub>, BaF<sub>2</sub> and MgF<sub>2</sub> are listed in Table 4.1. The extrinsic temperature dependence of the elastic moduli

TABLE 4.1: Thermodynamic Data

	С <sub>р</sub>	
(	cal. deg <sup>-1</sup> mole <sup>-1</sup> )	γ
LiF	9.978	1.63
NaF	2 11.198	1.51
CaF <sub>2</sub>	16.393	1.83
SrF <sub>2</sub>	18.13	1.31
BaF <sub>2</sub>	17.0204	1.80
MgF <sub>2</sub>	14.73	1.21

- Douglas (1959) 1.
- JANAF (1971) 2.
- Touloukian (1967) 3.
- Wicks and Block (1963) 4.

in (4.5) arises through their dependence on volume and its dependence on temperature.

Equation (4.5) is strictly applicable only to solids with cubic symmetry. Fritz (1974) has shown that for the rutile structure the equivalent expression is

$$\left(\frac{\partial c}{\partial T}\right)_{P} = \left(\frac{\partial c}{\partial T}\right)_{V} - \frac{\alpha_{V}^{K}S}{(1 + \alpha_{V}\gamma T)} \left(\frac{\partial c}{\partial P}\right)_{T} + \beta c \qquad (4.6)$$

where  $\beta$  is a correction term involving the axial thermal expansion coefficients, the axial compressibilities and the uniaxial strain derivatives of the elastic moduli. The magnitude of  $\beta$  is discussed in section 4.5 for MgF<sub>2</sub>.

### 4.3 $(\partial c/\partial T)_{P}$ versus T for LiF and NaF

The intrinsic and extrinsic temperature dependence of the elastic moduli for LiF and NaF is illustrated in Figures 4.2 and 4.3 which are plots versus temperature of  $(\partial c/\partial T)_p$ , determined from the polynomial equations (Table 3.7), and  $(\partial c/\partial T)_V$  calculated from equation (4.5), for the moduli  $c_{11}$ , c", c'  $c_{44}$  and  $K_s$ . Our experimental values for  $K_s$  and those of Srivastava and Merchant (1973) for  $\alpha_V$  as a function of temperature were used in the calculations in equation (4.5). For simplicity, it was assumed that  $\gamma$  and  $(\partial c/\partial P)_T$  are independent of temperature, the values for the latter being taken from Miller and Smith (1964). Figure 4.2 and Figure 4.3 also demonstrate that the crosschecks described earlier (Chapter 3) for c" and  $c_{44}$  are valid over the entire temperature range, T =  $300^\circ - 650^\circ K$ .

The linear temperature dependence of  $(\partial c/\partial T)_p$  for all moduli is a direct consequence of fitting the data by a second degree polynomial. For both LiF and NaF,  $|(\partial c_{11}/\partial T)_p|$  and  $|(\partial c'/\partial T)_p|$  decrease with T while







Figure 4.3: -  $(\partial c/\partial T)$  versus temperature for NaF. The values of  $(\partial c/\partial T)_p$ , represented by the solid lines, are determined from the fitted polynomial equations. The dashed lines represent the values of  $(\partial c/\partial T)_V$  calculated from equation (4.5). The crosscheck for  $(\partial c_{44}/\partial T)_p$ obtained from the [110] direction cannot be distinguished from the plotted line for the [001] direction.

 $|(\partial c_{44}/\partial T)_p|$ ,  $|(\partial c''/\partial T)_p|$  and  $|(\partial K_S/\partial T)_p|$  either increase or (in the case of c'' for NaF) remain approximately constant. There is no doubt that this observed curvature is a real feature of our experimental data and is statistically significant. Neither errors in the thermal expansion data used in equations (3.1)-(3.3) nor uncertainties due to bond effects are large enough to account for the deviation of the c vs T curves from linearity; in any case, these effects would cause curvature in the same sense for all the modes.

For comparison,  $(\partial c/\partial T)_p$  and  $(\partial c/\partial T)_V$  for MgO are plotted versus temperature in Figure 4.4 using Spetzler's (1969) data, for which  $(\partial c/\partial P)_T$  does depend on temperature.  $|(\partial c/\partial T)_p|$  increases initially (except for c'), becomes approximately constant for K<sub>S</sub> and c<sub>44</sub>, but thereafter decreases for c<sub>11</sub>, c' and c''.

The reduction to constant volume for LiF and NaF lowers the curves of  $(\partial c/\partial T)_p$  versus temperature in Figures 4.2 and 4.3 and also alters their temperature dependence;  $|(\partial c''/\partial T)|$  now decreases with increasing temperature. In the above reduction it is assumed that  $(\partial c/\partial P)_T$  is independent of temperature. Comparison of the curves of  $(\partial c/\partial T)_p$  and  $(\partial c/\partial T)_V$  versus temperature for MgO in Figure 4.4 demonstrates that the term involving  $(\partial c/\partial P)_T$  in equation (4.5) increases with increasing temperature. It is assumed as a first approximation that this behaviour reflects that of LiF and NaF. Application of this result to the  $(\partial c/\partial T)$ -T curves in Figure 4.2 and Figure 4.3 for LiF and NaF indicates that although the temperature dependence of  $(\partial c/\partial T)_V$  may be eliminated for the modulus  $c_{4,4}$  (resulting in a linear c-T plot at constant volume), that for the moduli  $c_{11}$ , c' and c'' will be accentuated.

Several interesting comparisons emerge from Figures 4.2-4.4. Firstly,  $|(\partial c_{11}/\partial T)_V|$  and  $|(\partial c'/\partial T)_V|$  for MgO decrease with temperature as they did for LiF and NaF. Secondly, the reduction to



Figure 4.4:  $-(\partial c/\partial T)$  versus temperature for MgO. The values of  $(\partial c/\partial T)_p$ , represented by the solid lines, are taken from Spetzler (1969). The dashed lines represent the values of  $(\partial c/\partial T)_V$  calculated from equation (4.5) using Spetzler's (1969) data.
constant volume reduces the  $|(\partial c/\partial T)_p|$  for all modes for each compound to more comparable values; this results from the large extrinsic effect for the modes  $c_{11}$ , c" and c'. Thirdly, the decrease of  $K_S$  with T is entirely an extrinsic effect as  $K_S$  in fact increases slowly with temperature at constant volume. Similar behaviour was pointed out by Roberts and Smith (1970a) for the sodium and potassium halides. Comparisons of ( $\partial c/\partial T$ ) for LiF, NaF and MgO will be discussed further in Chapter 5.

## 4.4 ( $\partial c/\partial T$ ) versus T for CaF<sub>2</sub>, SrF<sub>2</sub>, and BaF<sub>2</sub>

The intrinsic and extrinsic temperature dependence of the elastic moduli for CaF<sub>2</sub>, SrF<sub>2</sub> and BaF<sub>2</sub> is illustrated in Figures 4.5-4.7 respectively. The values of  $\alpha_V(T)$  from Sirdeshmukh and Deshpande (1964) and the experimental values of K<sub>S</sub>(T) were used in the calculations in equation (4.5). We have assumed that  $\gamma$  is independent of temperature and will show later that this assumption is valid. In any case, the expression (4.5) is not sensitive to minor variations in  $\gamma$ . For CaF<sub>2</sub> and BaF<sub>2</sub>, values of  $(\partial c/\partial P)_T$  at 298°K were taken from Wong and Schuele (1968); estimates of  $(\partial^2 c/\partial T\partial P)$  were also made from their data at 298°K and 195°K. For SrF<sub>2</sub>, only the room temperature value of  $(\partial c/\partial P)_T$  from Alterovitz and Gerlich (1970) was available. Figures 4.5 and 4.6 also demonstrate the crosschecks described earlier (Chapter 3) for c" and c<sub>44</sub> for CaF<sub>2</sub> and SrF<sub>2</sub> to be valid over the entire temperature range, T = 300-650°K.

The linearity of the  $(\partial c/\partial T)_p$  curves in T for all moduli is again a direct consequence of fitting the data by second degree polynomials (Table 3.10). For all of the moduli for CaF<sub>2</sub>, SrF<sub>2</sub> and BaF<sub>2</sub>,  $|(\partial c/\partial T)_p|$ either increases with T or remains approximately constant. This is in contrast to the behaviour for LiF and NaF (section 4.3) where  $|(\partial c/\partial T)_p|$ for some moduli actually decreases with temperature. As discussed



<u>Figure 4.5</u>:  $-(\partial c/\partial T)$  versus temperature for CaF<sub>2</sub>. The values of  $(\partial c/\partial T)_p$ , represented by the solid lines, are determined from the fitted polynomial equations. The dashed lines represent the values of  $(\partial c/\partial T)_V$  calculated from (4.5). The dotted line for K<sub>S</sub> illustrates the effect of a constant value for  $(\partial c/\partial P)_T$ . The crosschecks for  $(\partial c_{44}/\partial T)_p$  (v<sub>4</sub>) and  $(\partial c''/\partial T)_p$  (calculated) cannot be distinguished from the respective plotted lines.







<u>Figure 4.7</u>: -  $(\partial c/\partial T)$  versus temperature for BaF<sub>2</sub>. The values of  $(\partial c/\partial T)_p$ , represented by the solid lines, are determined from the fitted polynomial equations. The dashed lines represent the values of  $(\partial c/\partial T)_V$  which are calculated from (4.5).

earlier, the observed curvature is a real feature of the data and cannot be explained by uncertainties in either the experimental or analysis procedures.

The reduction to constant volume for  $CaF_2$ ,  $SrF_2$  and  $BaF_2$  lowers the curves of  $(\partial c/\partial T)_p$  versus temperature in Figures 4.5, 4.6 and 4.7 and also alters their temperature dependence. The above reduction for  $CaF_2$  and  $BaF_2$  took account of the variation of  $(\partial c/\partial P)_T$  with temperature, albeit at somewhat modest temperatures. For  $CaF_2$ , the values of  $|(\partial c/\partial T)|$  at constant volume do not increase as rapidly with temperature as those at constant pressure. This indicates that the curvature in the c-T plot can be partly removed by the conversion to constant volume. In Figure 4.5 for  $\mbox{CaF}_2,$  we have plotted constant volume curves for  $\mbox{K}_S$  for two cases; (i)  $(\partial c/\partial P)_T$  a function of T and (ii)  $(\partial c/\partial P)_T$  independent of T. The curvature in the c-T plot for case (i) is much more nearly eliminated than for case (ii). For  $BaF_2$  and  $SrF_2$ ,  $(\partial c_{44}/\partial T)_V$  and  $(\partial c'/\partial T)_V$ are almost independent of temperature, whereas  $|\left(\partial c''/\partial T\right)_V|$  and  $|(\partial c_{11}/\partial T)_V|$  now decrease with temperature. Additional information on the variation of  $(\partial c/\partial P)_T$  with T is required before more definite conclusions can be drawn from these plots of  $(\partial c/\partial T)_V$  versus temperature; however it does appear that the curvature observed in the c-T plots at constant pressure for these compounds is compatible with linearity in the c-T plots at constant volume, since the correction term  $\alpha_V K_T ~(\partial c/\partial P)_T$ becomes larger with increasing temperature.

Several other interesting features can be seen in Figures 4.5-4.7. Firstly, the curvature in the c-T plot, as indicated by the gradient of the  $(\partial c/\partial T)_p$ -T plots, is largest for CaF<sub>2</sub> and smallest for BaF<sub>2</sub>. This behaviour is in accord with the magnitude of the Debye temperatures (514°K for CaF<sub>2</sub>, 380°K for SrF<sub>2</sub> and 282°K for BaF<sub>2</sub>) since the predicted linear behaviour of c vs T should occur for temperatures greater than the Debye temperature. Secondly, the magnitudes of  $(\partial c'/\partial T)_p$  and  $(\partial c_{44}/\partial T)_p$ 

are very similar, indicating that the degree of anisotropy should not be very temperature sensitive. This is in contrast to the alkali fluorides, LiF and NaF, where  $|(\partial c'/\partial T)|_{p}$  is much larger than  $|(\partial c_{44}/\partial T)_{p}|$ . Thirdly, the reduction to constant volume reduces the  $|(\partial c/\partial T)_{p}|$  for all modes to much more comparable values; the results from the large extrinsic effect for the modes  $c_{11}$  and c". Fourthly, the decrease of  $K_{S}$  with T is entirely an extrinsic effect as  $(\partial K_{S}/\partial T)_{V}$  is actually small and positive.

## 4.5 ( $\partial c/\partial T$ ) versus T for MgF<sub>2</sub>

The intrinsic and extrinsic temperature dependence for MgF<sub>2</sub> is illustrated in Figure 4.8, which is a plot of  $(\partial c/\partial T)_P$  and  $(\partial c/\partial T)_V$  versus T for the independent single crystal elastic moduli and K<sub>S</sub>. The values of  $(\partial c/\partial T)_P$  were determined from the polynomial equations (Table 3.14); values of  $(\partial c/\partial T)_V$  were calculated via equation (4.5) using our experimental values of K<sub>S</sub> vs T, the values of  $\alpha_V$  vs T from Bailey <u>et al</u>. (1975) and the values of  $(\partial c/\partial P)_T$  at 298°K from Davies (1976).  $\gamma$  was assumed to be independent of temperature.

As mentioned earlier, equation (4.6) is the appropriate equation for the approximate separation of  $(\partial c/\partial T)_p$  into intrinsic and extrinsic components for the rutile structure. Fritz (1974) has shown that if the axial strain derivatives of the elastic modulus are of the same sign, then the magnitude of  $\beta$  can be bounded in the following inequality,

$$0 \leq \left| \frac{c\beta}{\alpha_{V}K_{S}(\partial c/\partial P)_{T}} \right| \leq \left| 2 \frac{(\alpha_{a}\chi_{c} - \alpha_{c}\chi_{a})K_{S}}{\alpha_{V}} \right|$$
(4.7)

where  $\alpha_a$ ,  $\alpha_c$  are the coefficients of axial thermal expansion, and  $\chi_a = -(\partial \ln \ell^a / \partial P)_T$ ,  $\chi_c = -(\partial \ln \ell^c / \partial P)_T$ , are the axial compressibilities. From the stress-strain relationship involving the single crystal elastic constants (e.g. Musgrave, 1970, chapter 4.4), it can be shown that



<u>Figure 4.8</u>:  $-(\partial c/\partial T)$  versus temperature for MgF<sub>2</sub>. The values of  $(\partial c/\partial T)_p$ , represented by the solid lines, are determined from the fitted polynomial equations. The dashed lines represent the values of  $(\partial c/\partial T)_V$  which are calculated from (4.5).

$$\chi_{a} = \frac{c_{33} - c_{13}}{c_{33}(c_{11} + c_{12}) - 2c_{13}^{2}}$$

$$\chi_{c} = \frac{c_{11} + c_{12} - 2c_{13}}{c_{33}(c_{11} + c_{12}) - 2c_{13}^{2}}$$
(4.8)

Evaluation of the r.h.s. of equation (4.7) using values of  $\alpha_a$  and  $\alpha_c$ from Bailey <u>et al</u>. (1975) demonstrates that the possible error of the correction term relative to the extrinsic term could be as large as 14 per cent. The error in determining  $(\partial c/\partial T)_V$  will thus be larger when the extrinsic term represents a large fraction of the temperature dependence. The foregoing analysis only applies for the case where the uniaxial strain derivatives of the elastic moduli are of the same sign; it is conceivable that they could be of opposite sign and the errors in neglecting  $\beta$  could be even larger in this case. In the absence of measured uni-axial strain derivatives which would permit a rigorous separation of  $(\partial c/\partial T)_p$  into intrinsic and extrinsic components, equation (4.5) is used as a first approximation, with the possible errors kept in mind.

Figure 4.8 for MgF<sub>2</sub> illustrates that for all the moduli,  $|(\partial c/\partial T)_p|$ either increases with temperature or remains approximately constant. This is similar to the behaviour for CaF<sub>2</sub>, SrF<sub>2</sub> and BaF<sub>2</sub>, but in contrast to that for LiF and NaF. For TiO<sub>2</sub>, Manghnani <u>et al</u>. (1972) reported values of  $|(\partial c/\partial T)_p|$  which decreased with increasing temperature. The behaviour of  $(\partial c/\partial T)_V$  versus temperature for MgF<sub>2</sub> supports the possibility of linearity in the c-T plots at constant volume, particularly if account could be taken of the temperature dependence of  $(\partial c/\partial P)_T$ . As discussed earlier in sections 4.3 and 4.4, an increase in the correction term with temperature would tend to reduce the slope of the  $(\partial c/\partial T)$ -T curves.

The remarks made previously for the rocksalt and fluorite fluorides regarding the similarity in magnitude of the  $(\partial c/\partial T)_V$  vs T curves do not

apply for MgF<sub>2</sub>. There seems to be no simple trend relating  $(\partial c/\partial T)_p$  and  $(\partial c/\partial T)_V$  for the various moduli. However, as noted for the other structures, the temperature dependence of K<sub>S</sub> is entirely an extrinsic effect, as K<sub>S</sub> actually increases very slowly at constant volume.

#### 4.6 High temperature equations of state

The predictions of many classical lattice dynamical theories that  $c_{ij}$  should exhibit linear dependence on T for T >  $\theta_D$  were discussed earlier (4.1). However, although the expressions for  $c_{ij}$  vs T reduce to simple analytical expressions in the high temperature and low temperature limits, none of the theories is able to furnish a simple analytical expression for the  $c_{ij}$  vs T that is valid for the entire temperature range from  $0^{\circ}$ K to the melting temperature.

In the absence of an exact theoretical equation of state, recourse may be made to equations derived on a semi-empirical or approximate theoretical basis. For example, Varshni (1970) has claimed some theoretical justification for the following equation

$$c = c_{o} + s/(e^{t/T} - 1)$$
 (4.9)

where  $c_{\circ}$ , s and t are parameters determined by fitting the equation to the c-T data. Equation (4.9) is based on the result of Leibfried and Hahn (1958) that the temperature dependent part of the elastic moduli is proportional to the internal vibrational energy  $\bar{\epsilon}$  (equation 4.1), as obtained from the Einstein model,

$$\bar{\epsilon} = \frac{1}{2}\hbar\omega + \frac{\hbar\omega}{e^{\hbar\omega/kT} - 1}$$
(4.10)

where h is Planck's constant,  $\hbar = \frac{h}{2\pi}$  and k is Boltzmann's constant. Varshni demonstrated good agreement of (4.9) with the experimental data for metals and ionic compounds (some alkali halides and BaF<sub>2</sub>). Attempts to fit equation (4.9) to the present c-T data for LiF and NaF indicated that it was incompatible with the data for the modes  $c_{11}$  and c'. Analysis of the functional form of equation (4.9) revealed that it cannot accommodate data for which ( $\partial c/\partial T$ ) is negative and increasing, i.e., data for which the c-T plot is concave upward. Equation (4.9) is functionally compatible with the c-T data of CaF<sub>2</sub>, SrF<sub>2</sub>, BaF<sub>2</sub> and MgF<sub>2</sub>; however it was decided not to fit the data by this equation since the parameters are not well constrained by the c-T values in the high temperature region and are extremely sensitive to small differences in slope. This occurs in the absence of constraining data on the parameters at lower temperatures (T <<  $\theta_D$ ) where a significant fraction of the curvature occurs (see Figure 4.1 for the general shape of c-T curves).

Another semi-empirical equation of state has been proposed by Wachtman et al. (1961)

$$E = E_0 - bT \exp(-T_0/T)$$
 (4.11)

where E is Young's modulus and b and T<sub>0</sub> are the parameters to be determined from the data. Anderson (1966) has placed this equation on a firmer theoretical basis for K<sub>S</sub> and has demonstrated that K<sub>S</sub> is linear in T for  $T > \theta_D/2$  (which he defines as the regime of high temperature elastic behaviour). Anderson's final form of the Wachtman equation (Soga, Schreiber and Anderson, 1966) is expressed in terms of the enthalpy data  $H^T$  and is given by

$$K_{\rm S}^{\rm T} - K_{\rm S}^{\rm 298} = -\frac{\gamma\delta}{v^{298}} ({\rm H}^{\rm T} - {\rm H}^{\rm 298}) (1 - \frac{\alpha_{\rm V}^{\rm T}}{2})$$
 (4.12)

where  $V^{298}$  is the volume at 298°K and  $\delta$  is another dimensionless Grüneisen parameter defined by

$$\delta = -\left(\frac{\partial \ln K_{S}}{\partial T}\right) / \left(\frac{\partial \ln V}{\partial T}\right)_{P} = -\frac{1}{\alpha_{V}K_{S}} \left(\frac{\partial K_{S}}{\partial T}\right)_{P}$$
(4.13)

On theoretical grounds (Anderson, 1966; Madan, 1971), δ should lie approximately between 3 and 4 for alkali halides; this is verified in Figure 4.9 for some of our fluoride compounds. These theoretical

derivations depend on assumptions on the nature of the interatomic potential; nevertheless their advantage is that equation (4.12) can be used to extrapolate  $K_S$  to high temperatures in the absence of a value for ( $\partial K_S / \partial T$ ).

The derivation of (4.12) assumes that  $\gamma$  and  $\delta$  are independent of temperature, an assumption which has been demonstrated to be valid for MgO, Mg<sub>2</sub>SiO<sub>4</sub> and MgSiO<sub>3</sub> (Anderson, 1966; Soga and Anderson, 1967). In Figure 4.9, we have illustrated the temperature dependence of  $\gamma$  and  $\delta$  for several fluorides of the present study, and demonstrated that  $\gamma$  and  $\delta$  are indeed approximately constant over the range T = 300-650°K. The product  $\gamma\delta$  varies even less over this temperature range, perhaps since the product is independent of both K<sub>S</sub> and  $\alpha_V$ . This observation is particularly interesting since it is sufficient in deriving (4.12) that  $\gamma\delta$  be independent of temperature.

Figures 4.10 and 4.11 compare the experimental values of  $\rm K_S$  for LiF and NaF with those calculated from 0°K to the melting point from the enthalpy data via equation (4.12). The calculated curves are matched in value and slope to our data curves at 298°K, since  $K_{\rm S}^{-298}$  and  $(\partial K_{\rm S}^{}/\partial T)_{\rm p}$ are input parameters to (4.12). Figures 4.10 and 4.11 demonstrate the excellent agreement between our data and the calculated curve for T > 300°K. This provides additional support for the reliability of our high temperature data, particularly since our values of  $K_{\rm S}$  and  $(\partial K_{\rm S}/\partial T)_{\rm P}$ at 298°K were earlier demonstrated to be in excellent agreement with the most reliable results of other investigators (Chapter 3). For LiF, the calculated curve between 0°K and 300°K follows the general trend of the offset Briscoe and Squire (1957) data (Figure 4.10). The agreement between the low temperature curves is better illustrated by adjusting Briscoe and Squire's data to agree with ours at 298°K. For NaF, the calculated low temperature curve agrees remarkably well with the low temperature data of Lewis et al. (1967) and Vallin et al. (1966). This







Figure 4.10: Bulk modulus versus temperature for LiF. The dashed curve represents values of the bulk modulus calculated from the enthalpy data (Douglas, 1959) via equation (4.12).



Figure 4.11: Bulk modulus versus temperature for NaF. The dashed curve represents values of the bulk modulus calculated from the enthalpy data (JANAF, 1971) via equation (4.12).

further supports our earlier claim (Chapter 3) that our high temperature data for LiF and NaF are in accord with the low temperature data of other experimenters using ultrasonic pulse techniques and lends credence to the construction of composite  $(\partial K_S/\partial T)$ -T curves using experimental data from the low and high temperature regions.

In Figures 4.12 and 4.13, values of  $K_S$  versus T are plotted for comparison with the values determined from the enthalpy data for CaF<sub>2</sub> and MgF<sub>2</sub>, respectively. For both CaF<sub>2</sub> and MgF<sub>2</sub>, there is excellent agreement between the present data and the calculated curves for T > 300°K. The non-systematic behaviour of the low temperature data of Huffman and Norwood (1960) for CaF<sub>2</sub> and its offset from ours at 298°K make further comparisons with the calculated curve impossible. For MgF<sub>2</sub>, the two data points from Aleksandrov <u>et al</u>. (1969) are in quite good accord with the calculated curve at low temperature. The absence of very low temperature data for MgF<sub>2</sub> and the poor quality of the existing data for CaF<sub>2</sub> preclude construction of a composite ( $\partial K_S/\partial T$ )-T curve using experimental data.

Plots of  $(\partial K_{\rm S}/\partial T)_{\rm P}$  versus temperature provide a much more sensitive way of examining the temperature behaviour of the bulk modulus since the high temperature linearity of the K<sub>S</sub>-T plot is reflected by  $(\partial K_{\rm S}/\partial T)_{\rm P}$  attaining a constant value (e.g., Anderson and Andreatch, 1966). In Figure 4.14, the measured  $(\partial K_{\rm S}/\partial T)_{\rm P}$  is plotted versus temperature for LiF, NaF, and MgO in order to determine the onset of high temperature elastic behaviour. For comparison,  $(\partial K_{\rm S}/\partial T)_{\rm P}$  calculated from the enthalpy data for LiF and NaF are also given in Figure 4.14 and the acoustic Debye temperatures,  $\theta_{\rm D}$ , are indicated (see Chapter 5.6 for  $\theta_{\rm D}$ ).

The combined measured and calculated data in Figure 4.14 for LiF and NaF exhibit a very rapid increase of  $|(\partial K_S/\partial T)_p|$  with temperature at low temperatures followed by a levelling out to constant values at high







Temperature , °K

<u>Figure 4.13</u>: Bulk modulus versus temperature for  $MgF_2$ . The dashed curve represents values of the bulk modulus calculated from the enthalpy data (Douglas, 1959) via equation (4.12).



Figure 4.14:  $-(\partial K_S/\partial T)_p$  versus temperature for LiF, NaF and MgO. Values of  $(\partial K_S/\partial T)_p$  for LiF and NaF for T > 300°K were determined from the polynomial fit to our data. For T < 300°K,  $(\partial K_S/\partial T)_p$  for LiF and NaF are determined stepwise from the data of Briscoe and Squire (1957) and Lewis <u>et al</u>. (1967) respectively, the temperature intervals being selected to eliminate large scatter. For MgO the  $(\partial K_S/\partial T)_p$  values for T < 300°K are listed by Anderson and Andreatch (1966) and  $(\partial K_S/\partial T)_p$  for T = 300°K to 1200°K are taken from Spetzler (1969). The values of  $(\partial K_S/\partial T)_p$  calculated from the enthalpy data (Douglas, 1959 for LiF and JANAF, 1971 for NaF) via equation (4.12) are indicated by +. The Debye temperatures,  $\theta_D$ , are indicated on the temperature axis for LiF, NaF and MgO. temperature, similar to the behaviour of MgO (Figure 4.4). Our experimental curves for T = 298-650°K demonstrate that  $|(\partial K_S/\partial T)_p|$  increases from its value for T < 300°K but does not attain a constant value at high temperatures since the data are fitted by only a second degree polynomial in temperature in the experimental range. Fitting the C-T data by a third degree polynomial permits  $|(\partial K_S/\partial T)_p|$  to increase to an approximately constant value and thereafter decrease.

If we arbitrarily define the onset of the high temperature regime to occur at that temperature T\* for which  $|(\partial K_S / \partial T)_p|$  attains 90% of its maximum experimental value we find that

	T*	θ
	°K	°K
iF	400	734
laF	300	441
lgO	420	955

N

Comparison of the experimental curves with the calculated data points indicates that the values of T\* are likely to be too large for LiF and NaF. Nevertheless, these values of T\* are in fair agreement with the theoretical prediction that the high temperature regime commences for  $T > \theta_D/2$ , although we might have anticipated a greater contrast in T\* for LiF and MgO.

Similar comparisons based on high temperature elastic data are not able to be made for the fluorite structure fluorides and oxides. High temperature data exist only for polycrystalline ThO<sub>2</sub> specimens of varying degrees of porosity (Spinner <u>et al</u>., 1963) and are not presented in a suitable form for analysis or comparison. The low temperature data curves for CaF<sub>2</sub>, SrF<sub>2</sub> and BaF<sub>2</sub> are not sufficiently continuous with our data curves at 298°K (see Figure 3.8) to permit the construction of composite  $(\partial K_S / \partial T)_P$ -T curves.

Comparisons of the relative onset of high temperature elasticity can also be made for the rutiles, MgF<sub>2</sub> and TiO<sub>2</sub>. The single crystal elastic data of Manghnani <u>et al</u>. (1972) for TiO<sub>2</sub> permit the calculation of K<sub>S</sub> and  $(\partial K_S / \partial T)_P$  in the range, 298°-573°K, via the Voigt-Reuss-Hill averaging procedure (Hill, 1952). In Table 4.2,  $(\partial K_S / \partial T)_P$  is listed at various temperatures above 298°K for MgF<sub>2</sub> and TiO<sub>2</sub>. The values of  $(\partial K_S / \partial T)_P$  for TiO<sub>2</sub> vary little over the temperature range. For MgF<sub>2</sub>, the values of  $|(\partial K_S / \partial T)_P|$  increase gradually with T; as discussed earlier for LiF and NaF, the fitting of a second degree polynomial prevents detection of any levelling off in the value of  $(\partial K_S / \partial T)_P$  with T. We can conclude at least from the data in Table 4.2 that the onset of high temperature elastic behaviour does not occur at lower temperatures for MgF<sub>2</sub> than for TiO<sub>2</sub>.

## 4.7 Conclusion

The prediction from lattice dynamical theories of the high temperature linearity of the c-T plot is more valid in constant volume rather than constant pressure space. The experimental results for CaF<sub>2</sub>,  $SrF_2$ ,  $BaF_2$  and  $MgF_2$  support this interpretation; at constant pressure, the c-T curves exhibit concave downward curvature, which can be largely eliminated by the correction to constant volume. However, since the curvature is in the opposite sense for the c<sub>11</sub> and c' modes for LiF and NaF, correction to constant volume merely increases the deviation from linearity and accentuates the variance with the theory. A similar concave upward curvature in the c-T plot appears in the results of Slagle and McKinstry (1967) for NaCl, KCl and KBr and Manghnani <u>et al</u>. (1972) for TiO<sub>2</sub>. Slagle and McKinstry fitted their data with polynomials in T, with the justification that the elastic moduli can be expanded as power series in the vibrational energy (equal to kT at high temperatures). The quadratic and higher order terms in this expansion were neglected by

	Т	(2K <sub>S</sub> /2T) <sub>P</sub>
	(°K)	(kbar deg <sup>-1</sup> )
1		
MgF <sub>2</sub>	298	-0.160
	348	-0.165
	398	-0.170
	448	-0.174
	498	-0.179
	548	-0.184
teneters, the downed	598	-0.189
	648	-0.194
2		
TiO <sub>2</sub>	300.5	-0.571
	313	-0.517
	333	-0.495
	358	-0.525
	423	-0.501
	523	-0.458

- 1. This work
- 2. Manghnani <u>et al</u>. (1972)

a the accessible experimental temperature range. However, the comparisons the model pairs LIF-MgO and MgF2-TIO2 indicate that the onest of MgS emperature elastic behaviour done not occur at significantly lower.

The precision of our data for the temperature dependence of the mattic moduli for LiF, NaF, CaF<sub>2</sub>, SeF<sub>2</sub>, BaF<sub>2</sub> and NgF<sub>2</sub> embles predictions " equations of state at high temperature to be tested. These data are less important in providing information on the elastic moduli and their reperature derivatives for crystal structures of interest in the arth's mantle. In Chapter 5, we will examine the possibility of sploying our data for the fluorides to predict the elastic properties of here or or one of the fluorides to predict the elastic properties of Leibfried and Hahn (1958).

Detailed studies of the behaviour of the elastic moduli as a function of temperature have important implications for lattice dynamical theories. In particular, in the high temperature regime, the validity of the quasi-harmonic approximation requires further evaluation in the light of our new experimental data. For geophysical discussions of the earth's interior, the high temperature value of  $(\partial K_S / \partial T)_p$  is an important parameter. The deviations from the predicted linear behaviour will result in some uncertainty in  $(\partial K_S / \partial T)_p$ ; however since  $|(\partial K_S / \partial T)_p|$  is a small quantity numerically, and since the extrapolations in equations of state are carried out over a pressure range which is very much larger than the temperature range, the resultant uncertainties will be of secondary importance.

Our rationale in measuring the temperature dependence for fluorides was the expectation that the fluorides would exhibit high temperature elastic behaviour at lower absolute temperatures than their oxide analogues; this would enable evaluation of high temperature derivatives in the accessible experimental temperature range. However, the comparisons for the model pairs LiF-MgO and  $MgF_2$ -TiO<sub>2</sub> indicate that the onset of high temperature elastic behaviour does not occur at significantly lower temperatures for the fluorides.

The precision of our data for the temperature dependence of the elastic moduli for LiF, NaF, CaF<sub>2</sub>, SrF<sub>2</sub>, BaF<sub>2</sub> and MgF<sub>2</sub> enables predictions of equations of state at high temperature to be tested. These data are also important in providing information on the elastic moduli and their temperature derivatives for crystal structures of interest in the earth's mantle. In Chapter 5, we will examine the possibility of employing our data for the fluorides to predict the elastic properties of their oxide analogues.

# CHAPTER 5

# SYSTEMATIC RELATIONSHIPS GOVERNING THE ELASTIC MODULI AND THEIR TEMPERATURE AND PRESSURE DERIVATIVES

5.1 Introduction

5.2 Bulk modulus - volume systematics

5.3 Shear modulus - volume systematics

5.4 (ac/aT) systematics

5.5 (∂c/∂P) systematics

5.6 Debye temperature systematics

is number of possible variables, e.g., composition, structure, bondin is etc., it is a rather surprising result that the velocity can be when in terms of only two parameters. Eirch also conjectured that is chemically homogeneous securicit, the velocity should depend only when it, irrespective of shother density variations were due to introd in temperature, pressure or separatilographic phase. The recent which solution on the comperature and pressure dependence of the introduction of various phase transformations has enabled evaluation of only hypothesis (D. L. Anderson <u>et al.</u>, 1071; Michemann and Ringwood is hypothesis (D. L. Anderson <u>et al.</u>, 1071; Michemann and Ringwood is hypothesis (D. L. Anderson <u>et al.</u>, 1071; Michemann and Ringwood is hypothesis (D. L. Anderson <u>et al.</u>, 1071; Michemann and Ringwood is hypothesis (D. L. Anderson <u>et al.</u>, 1071; Michemann and Ringwood is hypothesis (D. L. Anderson <u>et al.</u>, 1071; Michemann and Ringwood is hypothesis (D. L. Anderson <u>et al.</u>, 1071; Michemann and Ringwood

#### CHAPTER 5

SYSTEMATIC RELATIONSHIPS GOVERNING THE ELASTIC MODULI AND THEIR TEMPERATURE AND PRESSURE DERIVATIVES

#### 5.1 Introduction

Systematic relationships between the elastic properties and crystallographic parameters of minerals have been useful in geophysics in estimating the elasticity of unmeasured phases, in relating seismic velocities to density in order to draw compositional inferences about the earth's mantle, and in elucidating the nature of the interatomic forces in the crystalline lattice.

One of the first examples of such a relationship was the demonstration by Birch (1960, 1961a, 1961b) that the compressional velocity,  $v_p$ , is a function only of density,  $\rho$ , and mean atomic weight,  $\overline{M}$ . For many minerals and rocks, the following linear relationship holds:

$$v_{\rm p} = a(\overline{\rm M}) + b\rho \tag{5.1}$$

where a is a function only of  $\overline{M}$  and b is a constant. In view of the large number of possible variables, e.g., composition, structure, bonding type, etc., it is a rather surprising result that the velocity can be described in terms of only two parameters. Birch also conjectured that for a chemically homogeneous material, the velocity should depend only on density, irrespective of whether density variations were due to changes in temperature, pressure or crystallographic phase. The recent availability of data on the temperature and pressure dependence of the elastic moduli, and on the elasticity of the low- and high-pressure polymorphs of various phase transformations has enabled evaluation of Birch's hypothesis (D. L. Anderson <u>et al.</u>, 1971; Liebermann and Ringwood, 1973; Liebermann, 1974b, 1975). Birch's initial formulation of the linear law (5.1) has been developed further by many workers; including its recent formulation as a power law in which the parameters are derived from crystallographic and thermodynamic considerations (e.g., D. L. Anderson, 1967; Shankland, 1972; O. L. Anderson, 1973; Shankland and Chung, 1974).

Much recent interest has also centred on systematics cast in terms of elastic moduli and volume, V, rather than velocity and density. Several studies have demonstrated that the relationship KV = constant holds for isostructural series of halides, oxides, sulphides, selenides and tellurides (O. L. Anderson and Nafe, 1965; O. L. Anderson and Soga, 1967; D. L. Anderson and O. L. Anderson, 1970; and O. L. Anderson, 1972). In addition to the isostructural trends, O. L. Anderson and Soga (1967) have demonstrated that for compounds with the same mean atomic weight,  $\overline{M}$ , the relationship  $KV^4$  = constant is appropriate and that this is merely a restatement of Birch's law.

Isostructural relationships for the shear modulus,  $\mu$ , as a function of volume have been discussed by Davies (1975) who demonstrated that the relationship  $\mu V^{4/3}$  = constant holds for many simple compounds. Davies also examined possible systematics in the pressure derivatives  $(\partial K/\partial P)_T$ and  $(\partial \mu/\partial P)_T$ . Such systematics are also of interest in providing constraints for the interpretation of shock wave data for high pressure phases of rocks and minerals (e.g., D. L. Anderson and Kanamori, 1968; Davies and Gaffney, 1973).

The relationship between the bulk moduli of fluorides and their oxide analogues is examined in the existing framework of bulk modulusvolume systematics. Relationships are also investigated for the temperature and pressure derivatives of the elastic moduli as a function of volume, structure and composition. The earlier observation (Chapter 4) that the Debye temperatures of oxides and fluorides do not differ so markedly as the melting temperatures is explained in terms of systematics

### in the Debye temperatures.

## 5.2 Bulk modulus-volume systematics

The empirical relationship KV = constant is consistent with a simple Born-Mie interatomic potential with a power law repulsion leading to  $KV^{4/3}$  = constant, which is indistinguishable from the empirical result. 0. L. Anderson (1972) has demonstrated that for a general repulsive potential v(r), the following equation is true,

$$K_0 = \frac{2}{9V_0} \frac{A}{r_0} \left[ 1 + \frac{v''(r_0)r_0}{2v'(r_0)} \right]$$
(5.2)

where  $A = A_m^Z c_a^Z e^2$ ,  $A_m$  is the Madelung constant and  $Z_c$ ,  $Z_a$  are the valence charges of the cation and anion respectively. The zero subscripts refer to values for the lattice in equilibrium. For a suitable definition of the Madelung constant,  $A_m$  is essentially independent of structure and the variation in A is contained in the valence product  $Z_c^Z Z_a$ . Taking the logarithm of equation (5.2) gives

$$\ln K_0 = \ln Z_2 Z_2 - x \ln V_0 + \text{constant}$$
(5.3)

where x empirically is close to one. If the term in brackets in equation (5.2) were independent of  $r_0$ , then x would equal 4/3 (the result for the Born-Mie potential). Equation (5.3) leads directly to the result (dropping the zero subscripts for convenience)

$$\frac{KV^*}{Z_c Z_a e^2} = \text{constant}$$
(5.4)

Following Anderson and Nafe (1965), the data of Table 5.1 are presented in Figure 5.1 as a log-log plot of bulk modulus versus molar volume per ion pair (V\* =  $2\overline{M}/\rho$  =  $2\overline{V}$ , where  $\overline{M}$  and  $\overline{V}$  are the mean atomic weight and volume, respectively) for oxides and fluorides crystallising in the rocksalt, fluorite and rutile structures. For clarity the data for the perovskite oxides and fluorides are plotted in Figure 5.2.

Structure	Compound	CN	Ionic Rac Å	lii <sup>1,2</sup>	$z_c z_a$	Molar Volume	м	ρ	Elasti M	c Moduli bar	ψ <sup>a</sup>	Tm	θ <sub>D</sub>	Ab
	12.51	3.5	Cation(s)	Anion	283	cm <sup>3</sup>		gm/ cm <sup>3</sup>	ĸs	μ <sub>s</sub>		°K	°K	
			0.74	1 77	1	0.97	25 94	2 6393	0.70440	0.49140	0.270	112031	73434	57
Rocksalt	Lif	6-0	0.74	1.55	1	14 09	41 00	2 8043	0 48340	0.31440	0.283	126932	49135	56
	NaF		1.02			23 00	58 10	2 5264	0.3234	0.1644	0.289	113031	3274	50
	KF		1.38			23.00	104 47	3 84345	0.2805	0.1275	0.297	104833	2215	48
B	RDF		1.49	1 40		11 25	40 31	3 5836	1 6286	1.3116	0.178	312532	95536	96
	MgO		0.72	1.40	4	16.76	56.08	3 3467	1 147	0.8147	0.186	288732	670*	91
	CaO		1.00			10.70	103 62	5 0097	0 887	0.5917	0.177	269332	45737	90
	SrO		1.13			20.69	103.02	5 0028	0.618	0 3558	0.152	229132	291*	75
	BaO		1.36	8 8 8		25.59	155.54	5.992	0.01	0.000	0.101			
					2	24.55	70 00	7 1919	0 84540	0 42740	0.270	169132	51438	67
Fluorite	CaF <sub>2</sub>	8-4	1.12	1.31	2	24.55	10.00	1 27710	0 71340	0 35040	0 273	167331	38010	66
	SrF <sub>2</sub>		1.25			29.37	125.02	7 7011	0.61111	0 23011	0.250	109731	22111	55
	PbF <sub>2</sub>		1.29			51.47	245.19	1.19	0.59140	0.25540	0 272	159331	28239	62
	BaF <sub>2</sub>		1.42			35.89	175.34	4.880-	2 1712	0 87412	0.170	315132	394*	95
	U02		1.00	1.38	8	24.62	270.03	10.97	1 0714	0.07214	0.165	349332	424*	103
	Th0 <sub>2</sub>		1.04			26.38-5	264.04	10.01	1.95	0.372	0.100	0.000		
				1 70	2	10 (1	62 71	7 17015	1 01940	0 54740	0.260	153632	62644	67
Rutile	MgF <sub>2</sub>	6-3	0.72	1.30	2	19.61	02.31	J. 170	1 10743	0 45243	0.312		459*	62
	NiF <sub>2</sub>		0.69			20.08	96.71	4.015	0 87516	0 30216	0 229	147531	428*	59
	CoF <sub>2</sub>		0.735			21.11	96.93	4.592	0.0033	0 3015	0 271	112931	393*	55
	MnF <sub>2</sub>		0.82			23.67	92.93	3.920	2 4041	2 0441	0 114		1144*	108
	Si0 <sub>2</sub>		0.40	1.36	8	14.01	60.08	4.28/	2.49	1 50018	0 140	+111647	774*	102
	Ge02		0.54			16.64	104.59	0.200	2.305	1 124419	0 132	210332	782*	94
	Ti0 <sub>2</sub>		0.605			18.80	/9.90	4.25	2.155	1 01020	0 149	190332	555*	96
	Sn0 <sub>2</sub>		0.690			21.56	150.69	6.990-*	2.123	1.010	0.145	1000	000	
							100 41	7 1 5 2 1	0 75640	0 18040	0 301	107047	57049	65
Perovskite	KMgF3	12-6-6	1.60 0.72	1.33	1.5	38.23	120.41	3.15	0.750	0.465	0.344	113047	479*	6
	KNiF <sub>3</sub>		1.60 0.69			38.8445	154.81	3.985	0.851	0.430	0.334	87547	438*	6
	KZnF <sub>3</sub>		1.60 0.75	"	"	40.1345	161.47	4.023	0.800	0.392	0.333	075	435*	6
	KCoF <sub>3</sub>		1.60 0.745			40.5845	155.03	5.82	0.78746	0.309	0.333		397*	6
	RbCoF <sub>3</sub>		1.73 0.745		"	42.3445	201.40	4.756	0.80140	0.39/13	0.355	103248	418*	61
	KMnF <sub>3</sub>		1.60 0.82			44.16	151.04	3.4222	0.64920	0.325-	0.298	08648	38623	6
	RbMnF <sub>3</sub>		1.73 0.82			45.73	197.40	4.31724	0.6/524	0.341-	0.321	900	590*	9
	CdTiO <sub>3</sub>		1.31 0.605	1.40	6	32.9025	208.30	6.331	2.1220	0.9820	0.182		489*	91
	CdSnO <sub>3</sub>		1.31 0.69		"	36.6527	279.09	7.615	1.8928	0.8/20	0.180	101048	601*	10
	SrTi0 <sub>3</sub>		1.40 0.605			35.87	183.52	5.11629	1.74450	1.1/00	0.102	1910	031	101

Table 5.1: Summary of elastic and thermal properties of fluorides and oxides

a.  $\psi = KV^*/Z_c Z_a e^2$  where  $V^* = 2\overline{M}/\rho = 2\overline{V}$  b.  $A = a\theta_D \overline{M}^{1/2}$  where  $a = V^{*1/3}$  = mean lattice parameter

\*  $\theta_D$  calculated from room temperature values of the elastic constants. +  $T_m$  for the quartz polymorph of GeO<sub>2</sub>

### Table 5.1 (Continued)

Shannon and Prewitt (1969). 1. 2. Shannon and Prewitt (1970). 3. Miller and Smith (1964). 4. Marshall and Miller (1967). 5. Cleavelin et al. (1972). 6. Spetzler (1969). 7. Son and Bartels (1972). 8. Vetter and Bartels (1973). 9. Wong and Schuele (1968). 10. Gerlich (1964b). 11. Wasilik and Wheat (1965). 12. Wachtman et al. (1964). 13. Robie et al. (1966). 14. Macedo, Capps and Wachtman (1964). 15. Haussühl (1968). 16. Hart and Stevenson (1970). 17. Mizutani et al. (1972). 18. Wang and Simmons (1973). 19. Manghnani, Fisher and Brower (1972). 20. Chang and Graham (1975). 21. Reshchikova (1969). 22. Beckman and Knox (1961). 23. Aleksandrov, Reshchikova and Beznosikov (1966). 24. Melcher and Bolef (1969). 25. Roth (1967). 26. Liebermann (1976). 27. Smith (1960). 28. Liebermann (1974a). 29. Swanson, Fuyat and Ugrinic (1954). 30. Bell and Rupprecht (1963). 31. Wicks and Block (1963). 32. Robie and Waldbaum (1968). 33. Weast (1972). 34. Briscoe and Squire (1957). Lewis, Lehoczky and Briscoe (1967). 35.  $\theta_{\rm D}$  calculated from elastic moduli of Anderson and Andreatch (1966). 36. 37. Johnston, Thrasher and Kearney (1970). 38. Huffman and Norwood (1960). 39. Gerlich (1964a). 40. This work. 41. Liebermann et al. (1976). 42. Calculated from lattice parameters in Wyckoff (1963). 43. Wu (1974). 44.  $\theta_{\rm D}$  calculated from elastic moduli of Aleksandrov et al. (1969) at  $^{173}{}^{\circ}{\rm K}.$ 45. Molar volume calculated from the lattice parameter given in Rousseau et al. (1974). 46. Rousseau et al. (1974). 47. Levin et al. (1964). 48. Levin et al. (1969).

49.  $\theta_{\rm D}$  calculated from elastic moduli of Reshchikova (1969) at 120°K.

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Figure 5.1: Log-log plot of bulk modulus (K) versus molar volume per ion pair  $(2\overline{M}/\rho)$  for oxides and fluorides in the rocksalt, fluorite and rutile structures. The KV\* = constant lines for oxides and fluorides in the three structures are indicated by dashed lines of gradient -1. The solid line of gradient -4 represents the constant mean atomic weight relationship KV\*<sup>4</sup> = constant for  $\overline{M}$  = 20-21.



Figure 5.2: Log-log plot of bulk modulus (K) versus molar volume per ion pair  $(2\overline{M}/\rho)$  for oxides and fluorides in the perovskite structure. The dashed lines represent the KV\* = constant and KV\*<sup>4</sup> = constant relationships, and are labelled accordingly.

Three important trends emerge from these data:

- (1) The relationship KV\* = constant holds for fluorides and oxides in the rocksalt, fluorite, rutile and perovskite structures. For the perovskite and rutile compounds, the scatter of the data points about the line of gradient -1 is much greater than for fluorides and oxides in the other structures.
- (2) From the values of  $\psi = KV^*/Z_c Z_a e^2$  in Table 5.1 we observe that the isostructural lines are scaled approximately as  $Z_c Z_a$  for the fluoride compounds and also for the oxide compounds. Slight variations of  $\psi$  with structure for both the fluorides and the oxides reflect some sensitivity of the effective charges in the Born-Mie interatomic potential to the details of atomic packing and co-ordination number (see also D. L. Anderson and O. L. Anderson, 1970).
- (3) The fact that the  $\psi$ -values for the fluoride and oxide compounds within each isostructural group are not the same can be attributed to differences in the effective charge. If  $S = Z^0/2Z^F$  is defined as the ratio of the effective unit charges of the oxides with respect to the fluorides (following 0. L. Anderson, 1972), then the KV\* = constant lines for the fluorides and oxides of a given structure are scaled as  $4S^2$ . The values of S determined by comparing the KV\* lines for each isostructural group in Figures 5.1 and 5.2 are 0.80 for the rocksalt, 0.78 for the fluorite, 0.70 for the rutile and 0.73 for the perovskite structure. Thus the effective unit charge of an oxide is approximately 75% of that of its fluoride analogue for all the structures considered.

It is interesting to compare our values of S with those derived from the more rigorous lattice dynamical calculations. Using a shell model, Axe (1965) and Axe and Pettit (1966) derived values of S = 0.73 for the fluorite structure (CaF<sub>2</sub> and ThO<sub>2</sub>). Katiyar and Krishnan (1969) employed a rigid ion model and concluded that S = 0.77 for the rutile structure (MgF<sub>2</sub> and TiO<sub>2</sub>). Recent determinations of the effective charges for rutile fluorides (Striefler and Barsch, 1973) and rutile oxides (Striefler and Barsch, 1975) from a least squares fit over all the available elastic and optical data lead to values of S in the range 0.57-0.74.

Since the relative effective charges do not appear to depend on structure for the rocksalt, fluorite, rutile and perovskite structures, it should thus be possible to predict the bulk modulus of an oxide from the bulk modulus of a fluoride of the same crystal structure. In particular the bulk moduli of the corresponding fluoride-oxide pairs in the Goldschmidt modelling scheme (for which the molar volumes are comparable) are related by  $(K^0/K^F) = 4S^2$ . A similar idea was suggested by Haussühl (1968) in considering MgF<sub>2</sub>-TiO<sub>2</sub> and LiF-MgO as analogue pairs. A word of caution is warranted here though; even though the scaling factor  $4S^2$  is virtually the same for all the structures considered, the prediction of bulk moduli is bound to be uncertain for those structures which exhibit large scatter about the lines of gradient (-1) in the log-log K-V\* plot.

From Figures 5.1 and 5.2 we can conclude that the rutile and perovskite isostructural groups do not fit the KV\* = constant systematics as well as we suggested previously (Jones and Liebermann, 1974). For the perovskites, this may be due to the fact that the lattice potential energy involves two types of cation-anion interaction, each characterised by its own repulsive potential. The requirement that the bracketed term in equation (5.2) be a slowly varying function of  $r_0$  (Anderson, 1972) might not be satisfied and deviation from the systematics would occur.

For the rutile-structure oxides, a rigid ion model with central forces only is not satisfactory, and the effects of bond bending must

be incorporated into the model (Striefler and Barsch, 1975). Striefler and Barsch's theoretical values of the bulk modulus agree very well with the experimental values for  $GeO_2$ ,  $TiO_2$  and  $SnO_2$ , and their model predicts reasonable values for the pressure derivatives of the elastic moduli. We can thus assume that it provides a reasonable explanation for the deviations of the rutile oxides on a log-log K-V plot. In general, the deviations from the predicted systematics result from the non-applicability of a simple model rather than from experimental uncertainties. Stishovite (rutile  $SiO_2$ ) is an exception to this in that a wide range of experimental values of bulk modulus have been reported. Ultrasonically-determined values for polycrystalline samples range from 3.46 Mbar (Mizutani <u>et al</u>., 1972) to 2.49 Mbar, the value used here (Liebermann <u>et al</u>., 1976) while Striefler and Barsch (1976) predict a value of 3.145 Mbar on the basis of their lattice dynamical calculations.

The rigid ion model has also been applied to the rutile fluorides (Striefler and Barsch, 1973), although the predicted and experimental values of bulk modulus are not in such good agreement in this case. In particular the model predicts that  ${\rm K}_{\rm S}$  should decrease monotonically with increasing molar volume for the sequence of fluorides MgF2, NiF2, CoF2 and  $MnF_2$  which is not observed (see Figure 5.1). It is possible that the effects of bond bending may also be important in the rutile fluorides. Another complication is introduced for the rutile and perovskite fluorides containing transition metal ions, since these compounds undergo magnetic transitions at low temperatures (e.g., Aleksandrov et al., 1966; Melcher and Bolef, 1969; Melcher, 1970). The "non-magnetic" compounds  ${\rm MgF}_2$  and  $KMgF_2$  have very similar values of  $\psi$  to those of the rocksalt and fluorite fluorides. Despite these discrepancies, our earlier discussion demonstrated that the relative effective charge of the oxides with respect to the fluorides appears to be virtually independent of structure, co-ordination number and details of the atomic interactions.

Another aspect of bulk modulus-volume systematics is given by 0. L. Anderson and Nafe (1965) (see also O. L. Anderson and Soga, 1967) who proposed that oxides and silicates of common mean atomic weight  $\overline{M}$  = 20-21 would be characterized by the relationship  $KV^{*4}$  = constant. In Figure 5.1, the bulk moduli of compounds with  $\overline{M} = 20-21$  (SiO<sub>2</sub>, MgF<sub>2</sub>, MgO, NaF) are indeed scaled as the inverse fourth power of the volume; this is an important result since this group of compounds contains both oxides and fluorides of different crystal structures. For other values of  $\overline{M}$  the KoV\*<sup>-4</sup> scaling is not as evident. However, for the rocksalt structure pairs MgO-NaF ( $\overline{M}$  = 20-21), CaO-KF ( $\overline{M}$  = 28-29), and SrO-RbF  $(\overline{M} = 52)$  this relationship holds very well as indicated in Table 5.2; the members of each pair have comparable  $\overline{M}$  since they are composed of adjacent elements in the Periodic Table which are very close in atomic weight. This alternative modelling scheme, on the basis of common  $\overline{M}$ rather than ionic radii, is implicit in the approach of Son and Bartels (1972) who chose their pairs on the basis of the same closed shell ion core configuration.

## 5.3 Shear modulus-volume systematics

There is no simple theoretical basis for shear modulus-volume systematics as there is for the bulk modulus, which can be described in terms of thermodynamic variables. Davies (1975) has demonstrated that the empirical relationship  $\mu V^n$  = constant holds for the alkali halides, rocksalt oxides and fluorite fluorides, where n is a constant approximately equal to 4/3. According to Davies, oxides in the rutile and corundum structures are also consistent with this relationship.

In Figure 5.3 we have plotted shear modulus,  $\mu$ , versus volume on a log-log plot for oxides and fluorides in the rocksalt, fluorite, rutile and perovskite structures. In addition to the features pointed out by Davies we can make some further comments on Figure 5.3 in the framework

Table 5.2: KV** Systematics for Rocksalt Fluorides and Ox	Oxide	es
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Compound	M	<u>KV*4</u>
LiF	13.0	0.06
MgO	20.2	0.26
NaF	21.0	0.24
CaO	28.0	0.90
KF	29.1	0.90
SrO	51.8	1.61
RbF	52.2	1.53
BaO	76.7	2.62

(2.5.3) Log-log plot of shear modulus (u) versus molar volume per ion pair (20/a) for origins and fluorides in the rockshit, fluorite, cutile and perovative structures. The data of Table 5.1 for a particular structure are plotted in order of increasing molar volume The dashed lines of gratient -4/3 represent the relationship ...4/3



<u>Figure 5.3</u>: Log-log plot of shear modulus ( $\mu$ ) versus molar volume per ion pair ( $2\overline{M}/\rho$ ) for oxides and fluorides in the rocksalt, fluorite, rutile and perovskite structures. The data of Table 5.1 for a particular structure are plotted in order of increasing molar volume. The dashed lines of gradient -4/3 represent the relationship  $\mu V^{4/3}$  = constant.
of the fluoride-oxide modelling scheme: (1) the perovskite fluorides follow a well defined trend which is steeper than the lines of gradient -4/3, while the perovskite oxide data is too scattered to be conclusive. The rutile fluorides describe a much steeper trend than their oxide counterparts which are consistent with  $\mu V^{*4/3}$  = constant. (2) Following an analogous procedure to that used in 5.2 for the bulk modulus-volume systematics, we can evaluate the relative effective charges from the best fitting lines for a particular structure, assuming that the  $V^{*}$ dependence is valid. Values of S are 0.88, 0.75, 0.81 and 0.72, respectively, for the rocksalt, fluorite, rutile and perovskite structures. For the fluorite and perovskite structures, these values of S are very close to those determined from the bulk modulus-volume systematics. This correspondence does not hold as well for the rocksalt and rutile structures for which the values of S derived from  $\mu$ -V systematics are higher than those determined from K-V systematics. The larger spread in these values of S is reflected in Figure 5.3 where the oxides tend to cluster much more closely along a single trend than do the fluorides. The uncertainties in slope and relative effective charge are larger for the shear modulus systematics than for the bulk modulus systematics.

Since the values of S do appear to be structure sensitive, it seems better to rely on isostructural trends within an isochemical group for predicting shear moduli of unmeasured high pressure phases. For example, extrapolation along a line of gradient -4/3 through the perovskite oxide data leads to a shear modulus of 1.7 Mbar for the high pressure perovskite phase of MgSiO<sub>3</sub> (V\* = 9.84 cm<sup>3</sup>, Liu, 1975). Liebermann (1976) obtained a value of 2.8 Mbar for the bulk modulus of MgSiO<sub>3</sub> - perovskite through application of the K-V systematics described in 5.1. These results indicate the value of systematics in elastic moduli in characterising the elasticity of unknown phases.

An uncertainty implicit in Figure 5.3 relates to the problem of

calculating the elastic moduli of polycrystalline aggregates from the single crystal elastic moduli. Values of the isotropic bulk and shear moduli in Table 5.1 were calculated by the Voigt-Reuss-Hill (VRH) averaging scheme (Hill, 1952) for which the uncertainties measured by the difference between the Voigt and Reuss bounds can be quite large, particularly for highly anisotropic materials (e.g., rutiles). However, in general it is found that the arithmetic average (VRH average) of the upper and lower bounds is a fair approximation (e.g., Meister and Peselnick, 1965, for tetragonal crystals).

In view of the fact that  $\mu$  is a complicated average of single crystal elastic moduli, it is perhaps surprising that the shear modulus exhibits any systematic behaviour at all. On a very qualitative level, the shear modulus-volume systematics for the rocksalt structure can be understood in terms of calculations of the elastic moduli from a central force model (e.g., O.L. Anderson and Liebermann, 1970). For the cubic structure,  $\mu$  is a function of c' and c<sub>44</sub> which for the rocksalt structure are given by

$$c' = \frac{z^2 e^2}{v_0^{4/3}} \{An + B\}$$

$$c_{44} = \frac{z^2 e^2}{v_0^{4/3}} D$$
(5.5)

where n is the exponent in the repulsive term in the Born-Mie potential and A, B and D are constants. Gilman (1963) has demonstrated that  $c_{44}$ exhibits a  $d^{-4}$  dependence for alkali halides, where d is the interatomic distance. The V<sup>-4/3</sup> dependence of the shear modulus arises naturally in this model.

5.4  $(\partial c/\partial T)$  systematics

Following the discussion of systematics in the elastic moduli

for fluorides and oxides in the rocksalt, fluorite, rutile and perovskite structures, it is of particular interest to investigate the relationship of  $(\partial c/\partial T)$  to crystallographic parameters. Table 5.3 presents the breakdown of  $(\partial c/\partial T)_p$  into intrinsic and extrinsic components according to equation (4.5), for the alkali fluorides LiF, NaF, KF and RbF, and for the alkaline earth oxides MgO, CaO, SrO and BaO. We decided to investigate the relationships between  $(\partial c/\partial T)$  for these compounds rather than  $(\partial \ln c/\partial T) = \frac{1}{c}(\partial c/\partial T)$  used by other authors (e.g., Bartels and Vetter, 1972), since  $(\partial c/\partial T)_p$  can be discussed in terms of explicit theoretical expressions derived by Mitskevich (1965).

Some important trends and relationships emerge from Table 5.3: (1) In general, for the fluoride series LiF-NaF-KF-RbF, and for the oxide series MgO-CaO-SrO-BaO,  $|(\partial c/\partial T)_p|$  decreases with increasing molar volume for the elastic moduli  $c_{11}$ , c',  $c_{44}$ ,  $K_{S}$  and  $\mu$ . The trends for  $(\partial c/\partial T)_{V}$  are not nearly so uniform;  $|(\partial c/\partial T)_{V}|$  decreases with increasing molar volume for the moduli c',  $c_{4\,4},~K^{}_{\rm S}$  and  $\mu$  for the fluorides and for the moduli  $c_{11}$ , c' and  $\mu$  for the oxides, but increases with increasing molar volume for  $c_{44}$  and  $K_{S}$  for the oxides.  $(\partial c_{11}/\partial T)_{V}$  for the series LiF-NaF-KF-RbF remains approximately constant. (2) The large extrinsic temperature dependence for the moduli,  $c_{11}$ ,  $K_{\rm S}$  and c' was noted previously for LiF, NaF and MgO in the discussion of Figures 4.2-4.4. The same behaviour is borne out in general for the alkali fluorides and alkaline earth oxides in Table 5.3. For the shear modulus,  $\mu$ , the intrinsic and extrinsic components of the temperature dependence are approximately equal for both the fluorides and the oxides. (3) The "weakened model" concept introduced by Goldschmidt (1927) suggests that the elastic properties of fluorides should be more temperature sensitive than those of their oxide analogues. For the fluoride-oxide analogue pairs, LiF-MgO, NaF-CaO, KF-SrO, RbF-BaO, Table 5.3 illustrates that for the moduli c11, c',  $c_{44}$  and  $K_{S}$ ,  $|(\partial c/\partial T)_{p}|$  for the fluoride member of a pair is generally

			Intrinsic	Extrinsic	
		$-\left(\frac{\partial c}{\partial T}\right)_{P}$	$-\left(\frac{\partial c}{\partial T}\right)_{V}$	$+ \alpha_V K_T \left(\frac{\partial c}{\partial P}\right)_T$	$\left(\frac{\partial c}{\partial P}\right)_{m}$
		(kbar.deg <sup>-1</sup> )	(kbar.deg <sup>-1</sup> )	(kbar.deg <sup>-1</sup> )	( ).I.
c <sub>11</sub>	LiF MgO NaF CaO KF SrO RbF BaO	0.749 <sup>1</sup> 0.606 <sup>3</sup> 0.624 <sup>1</sup> 0.547 <sup>4</sup> 0.481 <sup>4</sup> ,6 0.352 <sup>4</sup> 0.433 <sup>4</sup> ,6 0.32 <sup>9</sup>	0.094 0.166 0.102 0.085 <sup>4</sup> 0.093 <sup>4</sup> ,6 -0.065 <sup>4</sup> 0.123 <sup>4</sup> ,6	0.655 0.44 <sup>3</sup> 0.522 0.462 <sup>4</sup> 0.388 <sup>4</sup> ,6 0.417 <sup>4</sup> 0.310 <sup>4</sup> ,6	9.97 <sup>2</sup> 8.697 <sup>3</sup> 11.56 <sup>2</sup> 10.53 <sup>5</sup> 12.26 <sup>7</sup> 11.33 <sup>5</sup> 12.14 <sup>8</sup>
c'	LiF MgO NaF CaO KF SrO RbF BaO	0.38 0.34 0.336 0.266 0.26 0.21 0.225 0.19	0.144 0.145 0.120 0.115 0.094 0.064 0.099	0.236 0.195 0.216 0.148 0.167 0.147 0.126	2.73 3.64 1.985 3.4 5.25 4.0 4.93
С44	LiF MgO NaF CaO KF SrO RbF BaO	0.183 0.103 0.058 0.072 0.027 0.027 0.057 0.017 0.16	0.092 0.048 0.049 0.049 0.040 0.062 0.034	0.091 0.055 0.009 0.024 -0.013 -0.005 -0.017	1.38 1.09 0.205 0.6 -0.43 -0.2 -0.7
ĸ <sub>S</sub>	LiF MgO NaF CaO KF SrO RbF BaO	0.242 0.153 0.177 0.192 0.134 0.07 0.134 0.07	-0.098 -0.042 -0.058 -0.069 -0.032 -0.15 -0.008	0.340 0.195 0.235 0.262 0.166 0.22 0.143	5.14 3.85 5.18 6.0 5.26 6.0 5.57
μ	LiF MgO NaF CaO KF SrO RbF BaO	0.316 0.230 0.153 0.150 0.094 0.119 0.074 0.166	0.169 0.107 0.116 0.075 0.061 0.070 0.057	0.147 0.123 0.037 0.075 0.033 0.049 0.017	2.24 2.44 0.814 1.70 1.043 1.32 0.668

TABLE 5.3:Intrinsic and extrinsic components of  $\left(\frac{\partial c}{\partial T}\right)_p$ for the alkalifluorides and alkaline earth oxides at room temperature

#### TABLE 5.3 (Continued)

- 1. This work
- 2. Miller and Smith (1964)
- 3. Spetzler (1969)
- 4. Bartels and Vetter (1972)
- 5. Son and Bartels (1972)
- 6. Haussühl (1960)
- 7. Roberts and Smith (1970a)
- 8. Roberts and Smith (1970b)
- 9. Vetter and Bartels (1973)

larger than that for the oxide. However, the  $(\partial c/\partial T)_p$  for a particular analogue pair are not as dissimilar as one would expect from other evidence of the "weakened model" concept, e.g., the ratio of the bulk moduli (Jones and Liebermann, 1974). (4) An alternative modelling scheme (Son and Bartels, 1972) based on the same closed shell ion core configuration would pair MgO-NaF, CaO-KF and SrO-RbF;  $(\partial c/\partial T)_p$  for a pair chosen on this basis are more comparable but not demonstrably more systematic than for pairs with similar ionic radii. A modelling scheme based on ionic radii considerations has more theoretical appeal since properties dependent on geometrical configuration such as the relative effect of nearest neighbour and next nearest neighbour interactions ought to be similar for the members of an analogue pair.

In Table 5.4 we present the intrinsic and extrinsic components of  $(\partial c/\partial T)_p$  for the alkaline earth fluorides CaF<sub>2</sub>, SrF<sub>2</sub> and BaF<sub>2</sub>. Temperature derivatives of the single crystal elastic moduli are not available for their oxide analogues,  $ThO_2$  and  $UO_2$ . However we can note some features of the dependence of  $(\partial c/\partial T)$  on crystallographic parameters for the fluorides alone. (1) For the fluoride series  $CaF_2$ -SrF<sub>2</sub>-BaF<sub>2</sub>,  $|(\partial c/\partial T)_p|$  decreases with increasing molar volume for all the elastic moduli. The  $(\partial c/\partial T)_{V}$  data do not exhibit systematic behaviour except for the modulus c', for which  $|(\partial c/\partial T)_{V}|$  decreases with increasing molar volume. (2) The large extrinsic temperature dependence for the moduli  $c_{11}$  and  $K_{\rm S}$  was noted previously in the discussion of Figures 4.5, 4.6 and 4.7. For the single crystal (c' and  $c_{44}$ ) and isotropic ( $\mu$ ) shear moduli, the intrinsic temperature dependence comprises at least half of the total temperature dependence. (3) For the fluorite structure, the value of  $|(\partial c_{11}/\partial T)_p|$  is very much lower than for the rocksalt structure.  $|(\partial c'/\partial T)_p|$  and  $|(\partial c_{44}/\partial T)_p|$  are comparable in value for the fluorites in contrast to the rocksalt structure where  $|(\partial c'/\partial T)_p|$  is much larger than  $|(\partial c_{44}/\partial T)_p|$ . For the two structures, the values of  $|(\partial c_{44}/\partial T)_p|$  are similar.

# TABLE 5.4: Intrinsic and extrinsic components of $\left(\frac{\partial c}{\partial T}\right)_p$ for the alkaline

earth f.	luorides	at	room	temperature
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			Intrinsic	Extrinsic	
		$-\left(\frac{\partial c}{\partial T}\right)_{P}$	$-\left(\frac{\partial c}{\partial T}\right)_{V}$	$+ \alpha_v^1 K_T \left(\frac{\partial c}{\partial P}\right)_T$	$\left(\frac{\partial c}{\partial P}\right)_{T}$
		$(kbar.deg^{-1})$	(kbar.deg <sup>-1</sup> )	$(kbar.deg^{-1})$	
c11	CaF <sub>2</sub> SrF <sub>2</sub> BaF <sub>2</sub>	$\begin{array}{c} 0.346^{2} \\ 0.236^{2} \\ 0.212^{2} \end{array}$	0.0461 0.0630 0.0452	0.300 0.173 0.167	$6.05^{3}$ 5.25 <sup>4</sup> 4.82 <sup>3</sup>
c' .	CaF <sub>2</sub>	0.1108	0.0686	0.042	0.852
	SrF <sub>2</sub>	0.0573	0.0453	0.012	0.365
	BaF <sub>2</sub>	0.0376	0.0437	-0.006	-0.177
С44	CaF <sub>2</sub>	0.1212	0.0563	0.0649	1.31
	SrF <sub>2</sub>	0.0925	0.0574	0.0351	1.07
	BaF <sub>2</sub>	0.0761	0.0492	0.0269	0.777
ĸs	CaF <sub>2</sub>	0.198	-0.0454	0.243	4.92
	SrF <sub>2</sub>	0.159	0.002	0.157	4.76
	BaF <sub>2</sub>	0.156	-0.0191	0.175	5.05
μ	CaF <sub>2</sub>	0.118	0.058	0.060	1.218
	SrF <sub>2</sub>	0.084	0.058	0.026	0.795
	BaF <sub>2</sub>	0.061	0.047	0.014	0.39

1. Sirdeshmukh and Deshpande (1964)

2. This work

actions action

- 3. Wong and Schuele (1968)
- 4. Alterovitz and Gerlich (1970)

The intrinsic and extrinsic temperature dependence for the rutilestructure compounds are given in Tables 5.5 and 5.6. Several important features emerge from Tables 5.6 and 5.7. (1) The trend that was observed for the rocksalt and fluorite structures for  $|(\partial c/\partial T)_p|$  to decrease with increasing molar volume is evident here for neither the rutile fluorides nor oxides; in particular, the values of  $(\partial c/\partial T)_p$  for TiO<sub>2</sub> seem anomalously high in comparison with  $GeO_2$  and  $SnO_2$ . (2) For the rutile fluorides, the extrinsic temperature effect is dominant for the moduli  $c_{11},\;c_{12},\;c_{13}$  and  $K_{_{\rm S}}.$  The intrinsic component dominates the temperature dependence for the shear moduli,  $c_{66}$  and  $\mu_{\rm S}.~$  In general the temperature dependence of the rutile oxides is characterized by similar contributions from the intrinsic and extrinsic components; however, the dominant component is extrinsic for the moduli  $c_{11}$ ,  $c_{12}$ ,  $c_{13}$  and  $K_{s}$ , and intrinsic for the shear moduli  $c_{4\,4},\,c_{6\,6}$  and  $\mu_{\rm S}.~$  (3) As was stated earlier, an underlying concept of the fluoride-oxide modelling scheme was that the physical properties of the fluorides should be more temperature sensitive. From Tables 5.5 and 5.6, we can see that  $|(\partial c/\partial T)_p|$  for the fluorides is in general much lower than the corresponding  $|(\partial c/\partial T)_p|$  for the oxides. An exception to this is  $SnO_2$  for which all the  $(\partial c/\partial T)_p$  are very comparable with those for the fluorides. The major cause of this difference is the fact that the intrinsic temperature dependence for the rutile oxides is much larger than for the fluorides. (4) The temperature behaviour of  $MgF_2$  does however reflect that of TiO<sub>2</sub> in that the ratio of  $(\partial c/\partial T)_p$  for  $TiO_2$  relative to MgF<sub>2</sub> lies between 2.5 and 3 for all modes except  $c_{13}$ . Similar ratios for other fluoride-oxide pairs do not exhibit such constancy.

In Table 5.7, we have listed the intrinsic and extrinsic components of the  $(\partial c/\partial T)_p$  for the perovskites KMgF<sub>3</sub> and SrTiO<sub>3</sub>. The comparisons must be viewed as being rather tentative since the value of  $\alpha_V$  is only an estimate for KMgF<sub>3</sub> (see Footnote, p. 29). However some comments can

		fluorides at room	n temperature		
		$-\left(\frac{\partial c}{\partial T}\right)_{P}$	$\frac{\operatorname{intrinsic}}{-\left(\frac{\partial c}{\partial T}\right)_{V}}$	$\begin{array}{c} \text{extrinsic} \\ +\alpha_{V}^{1} K_{T} \left(\frac{\partial c}{\partial P}\right)_{T} \end{array}$	$\left(\frac{\partial c}{\partial P}\right)_{T}$
		$(kbar.deg^{-1})$	$(kbar.deg^{-1})$	(kbar.deg <sup>-1</sup> )	
C <sub>11</sub>	MgF <sub>2</sub>	0.1922	0.0107	0.181	4.83
	NiF <sub>2</sub> MnF <sub>2</sub>	$0.16^4$ $0.216^6$	0.037	0.123	4.45
C <sub>33</sub>	MgF <sub>2</sub> NiFa	0.322	0.110	0.212	5.6
	MnF <sub>2</sub>	0.32	0.100	0.134	5.5
C <sub>12</sub>	MgF <sub>2</sub> NiFa	0.194	-0.0366	0.231	6.1
	MnF <sub>2</sub>	0.220	-0.005	0.243	0.5
C <sub>13</sub>	MgF <sub>2</sub>	0.086	-0.0574	0.143	3.8
	MnF <sub>2</sub>	0.163	0.048	0.002	2.2
С44	MgF <sub>2</sub>	0.0745	0.0443	0.119	0.8
	MnF <sub>2</sub>	0.02	0.010	0.009	0.33
С <sub>66</sub>	MgF <sub>2</sub>	0.277	0.160	0.117	3.1
	MnF <sub>2</sub>	0.26	0.176	0.084	3.0
ĸ <sub>s</sub>	MgF <sub>2</sub>	0.160	-0.0213	0.181	4.8
	MnF <sub>2</sub>	0.18	0.046	0.134	4.8
μ	MgF <sub>2</sub>	0.079	0.059	0.020	0.6
	MnF <sub>2</sub>	0.028	0.045	-0.017	-0.6

 $\alpha_{\rm V}$  for NiF<sub>2</sub> taken from RaO (1973).

2. This work.

3. Davies (1976).

4. Wu (1974).

5. Jamieson and Wu (1974).

6. Haussühl (1968).

Table 5.6:	Intrinsic	and	extrinsic	components	of	$\left(\frac{\partial c}{\partial T}\right)$	for	the	rutile
						\ 01/P			

oxides at room temperature

		$-\left(\frac{\partial c}{\partial T}\right)_{P}$	$\frac{\operatorname{intrinsic}}{-\left(\frac{\partial c}{\partial T}\right)_{V}}$	$\begin{array}{c} \text{extrinsic} \\ +\alpha_{v}^{1}K_{T}\left(\frac{\partial c}{\partial P}\right)_{T} \end{array}$	$\left(\frac{\partial c}{\partial P}\right)_T$
		(kbar.deg <sup>-1</sup> )	(kbar.deg <sup>-1</sup> )	(kbar.deg <sup>-1</sup> )	
C <sub>11</sub>	GeO <sub>2</sub> TiO <sub>2</sub> SnO <sub>2</sub>	$0.42^{2}$ $0.51^{3}$ $0.20^{4}$	$0.187 \\ 0.184^3 \\ 0.084$	$0.233 \\ 0.326^3 \\ 0.116$	6.65 <sup>2</sup> 6.47 <sup>3</sup> 5.25 <sup>4</sup>
C <sub>33</sub>	GeO <sub>2</sub>	0.38	0.148	0.232	6.63
	TiO <sub>2</sub>	0.90	0.484	0.416	8.34
	SnO <sub>2</sub>	0.37	0.236	0.134	6.10
C <sub>12</sub>	GeO <sub>2</sub>	0.46	0.178	0.282	8.05
	TiO <sub>2</sub>	0.58	0.123	0.457	9.10
	SnO <sub>2</sub>	0.21	0.062	0.148	6.73
C <sub>13</sub>	GeO <sub>2</sub>	0.23	0.087	0.143	4.10
	TiO <sub>2</sub>	0.33	0.077	0.253	5.02
	SnO <sub>2</sub>	0.132	0.030	0.102	4.65
С44	GeO <sub>2</sub>	0.15	0.088	0.062	1.78
	TiO <sub>2</sub>	0.22	0.168	0.052	1.10
	SnO <sub>2</sub>	0.059	0.04	0.019	0.889
С <sub>66</sub>	GeO <sub>2</sub>	0.38	0.237	0.143	4.10
	TiO <sub>2</sub>	0.78	0.457	0.323	6.43
	SnO <sub>2</sub>	0.256	0.187	0.069	3.18
ĸ <sub>s</sub>	GeO <sub>2</sub> TiO <sub>2</sub> SnO <sub>2</sub>	$0.36 \\ 0.41 \\ 0.19$	0.145 0.067 0.077	0.216 0.343 0.113	6.15 6.80 5.13
μ	GeO <sub>2</sub>	0.12	0.077	0.043	1.22
	TiO <sub>2</sub>	0.27	0.226	0.044	0.78
	SnO <sub>2</sub>	0.067	0.054	0.013	0.61

1.  $\alpha_{V}$  for GeO<sub>2</sub> and SnO<sub>2</sub> taken from RaO (1973).

2. Wang and Simmons (1973).

3. Manghnani et al. (1972).

4. Chang and Graham (1975).

## TABLE 5.7: Intrinsic and extrinsic components of $\left(\frac{\partial c}{\partial T}\right)_p$ for the perovskites

 $\underline{KMgF_3}$  and  $\underline{SrTiO_3}$  at room temperature

		$-\left(\frac{\partial c}{\partial T}\right)_{\rm P}$	Intrinsic $-\left(\frac{\partial c}{\partial T}\right)_{V}$	Extrinsic + $\alpha_v^1 K_S \left(\frac{\partial c}{\partial P}\right)_T$	$\left(\frac{\partial c}{\partial P}\right)_{T}$
		(kbar.deg <sup>-1</sup> )	(kbar.deg <sup>-1</sup> )	(kbar.deg <sup>-1</sup> )	
c <sub>11</sub>	KMgF <sub>3</sub> RbMnF <sub>3</sub> SrTiOa	$0.509^{2}$ $0.44^{5}$ $0.867^{3}$	0.255	0.254	8.932
с'	KMgF <sub>3</sub> RbMnF <sub>3</sub> SrTiO <sub>2</sub>	0.251 0.217 0.367	0.168	0.083	2.94
с <sub>44</sub>	KMgF <sub>3</sub> RbMnF <sub>3</sub> SrTiO <sub>2</sub>	0.085 0.028 0.161	0.048	0.0372	1.31
ĸ <sub>s</sub>	KMgF <sub>3</sub> RbMnF <sub>3</sub> SrTiO <sub>3</sub>	0.174 0.151 0.377	0.032	0.142	5.01
μ	KMgF <sub>3</sub> RbMnF <sub>3</sub> SrTiO <sub>3</sub>	0.159 0.095 0.295	0.104 	0.055 - 0.141	1.93

1.  $\alpha_v$  for SrTiO<sub>3</sub>taken from Lytle (1964)

 $\alpha_{_{\rm V}}$  for  ${\rm KMgF}_3$  estimated in Footnote p. 29.

2. This work

- 3. Bell and Rupprecht (1963)
- 4. Beattie and Samara (1971)
- 5. Melcher and Bolef (1969)

still be made on the nature of the temperature dependence of the elastic moduli. (1) For both KMgF<sub>3</sub> and SrTiO<sub>3</sub>, the intrinsic temperature effect is greater than or equal to the extrinsic effect for the modes  $c_{11}$ , c' and  $c_{44}$ . For  $(\partial K_S/\partial T)_P$ , the dominant effect is extrinsic, although not as marked as for the rocksalt and fluorite structure. (2) The values of  $(\partial c/\partial T)_P$  for a particular mode are larger for SrTiO<sub>3</sub> than for KMgF<sub>3</sub>; similar behaviour was noted for  $(\partial c/\partial T)_P$  for the rutile-structure compounds. For the fluorides KMgF<sub>3</sub>-RbMnF<sub>3</sub>,  $|(\partial c/\partial T)_P|$  decreases with increasing molar volume for all moduli; however more data are required to establish a trend.

It is worth re-stating the most striking conclusions of the preceding comparisons of  $(\partial c/\partial T)$  for oxides and fluorides in the rocksalt, fluorite, rutile and perovskite structures. (1) Trends of decreasing  $|(\partial c/\partial T)_p|$  with increasing molar volume are observed for the rocksalt and fluorite structure compounds. (2)  $(\partial c/\partial T)_p$  values are very similar for the members of a rocksalt-structure fluoride-oxide analogue pair; these similarities are not exhibited by the rutile and perovskite-structure compounds. (3) For all of the compounds considered,  $(\partial K_S/\partial T)_p$  is dominated by extrinsic temperature dependence; for  $(\partial \mu/\partial T)_p$ , the intrinsic component is greater than or equal to the extrinsic component.

The existence of the above trends and similarities for the rocksalt fluorides and oxides prompted us to seek a theoretical explanation for this behaviour. From theoretical lattice dynamical considerations, Mitskevich (1965) derived the following expressions for the temperature dependence of the c<sub>ii</sub>,

$$\left(\frac{\partial c_{11}}{\partial T}\right)_{P} = -\frac{k}{d_{0}^{3}} \quad (0.411\Lambda^{2} + 3.25\Lambda - 4.8)$$

$$\left(\frac{\partial c_{12}}{\partial T}\right)_{P} = -\frac{k}{d_{0}^{3}} \quad (0.038\Lambda^{2} + 0.46\Lambda - 4.0) \quad (5.6)$$

$$\left(\frac{\partial c_{44}}{\partial T}\right)_{P} = -\frac{k}{d_{0}^{3}} \quad (-0.06\Lambda + 4.8)$$

where k is Boltzmann's constant and  $\Lambda$  is the repulsive parameter in the Born-Mayer potential

dn

$$\Phi(d) = -\frac{A_m^2 c_a^2 a^2}{d} + Be^{-\Lambda d/d_0}$$
(5.7)

where  $d_0$  is the equilibrium value of the nearest neighbour distance d,  $A_m$  is the Madelung constant and  $Z_c$ ,  $Z_a$  are the valences of the cation and anion respectively. By invoking equilibrium conditions it is easy to show that

$$\Lambda = 2 + \frac{9 V d_0 K}{A_m Z_c Z_a e^2}$$
(5.8)

where V is the molecular volume. We demonstrated earlier that the relationship  $KV^*/Z_cZ_ae^2$  = constant holds for isostructural series of fluorides and oxides in the rocksalt, fluorite, rutile and perovskite structures (also for halides, sulphides, selenides and tellurides, D. L. Anderson and O. L. Anderson, 1970). We have applied this result to equation (5.8) which leads to

$$\Lambda = 2 + \phi d \tag{5.9}$$

where  $\phi$  is a constant for the members of an isostructural series. Hence from equations (5.6) and (5.9),  $(\partial c_{ij}^{}/\partial T)_{p}$  should be a function of nearest-neighbour distance only.

In Figure 5.4 we have plotted on a log-log diagram,  $|(\partial c/\partial T)_p|$ versus molar volume per ion pair for the moduli  $c_{11}$ , c' and  $c_{44}$  for the alkali fluorides and the alkaline earth oxides. Both the fluorides and



<u>Figure 5.4</u>: Log-log plot of  $|(\partial c/\partial T)|_p$  (from Table 5.3) versus molar volume per ion pair for the modes  $c_{11}$ , c' and  $c_{44}$  for the alkali fluorides and alkaline earth oxides (rocksalt structure). The data points from left to right are LiF-NaF-KF-RbF and MgO-CaO-SrO-BaO respectively. The solid curves are calculated from equations (5.6) and (5.9) using  $\phi = 2.63$  for the alkali halides.

the oxides describe nearly linear and remarkably similar trends. Also plotted in Figure 5.4 are the theoretical curves for the alkali fluorides calculated from equations (5.6) and (5.9) using a  $\phi$  value of 2.63 (the average of the values for LiF and NaF). The agreement with the theoretical prediction is quite satisfactory in view of the experimental uncertainties in  $(\partial c/\partial T)_p$  and the simplifications in the theory. Strictly, equations (5.6) apply to the high temperature regime whereas we have plotted  $(\partial c/\partial T)_p$  at 298°K in Figure 5.4. The failure of the theory to describe the behaviour of  $(\partial c_{44}/\partial T)_p$  versus volume for the alkali fluorides might result from the use of the simple Born potential which neglects next-nearest neighbour interactions.

In Table 5.8, our high temperature values for  $(\partial c/\partial T)_p$  for LiF and NaF are compared with those calculated from equations (5.6). The agreement is very good for NaF (except for  $c_{44}$ ) but poorer for LiF. Mitskevich's (1965) derivation applied to alkali halides; however Figure 5.4 demonstrates that  $(\partial c/\partial T)_p$  for the fluorides and oxides behave in a similar manner. Therefore we have calculated  $(\partial c/\partial T)_p$  for MgO for comparison with Spetzler's (1969) high temperature data as well as  $(\partial c/\partial T)_p$  for CaO to compare with Bartels and Vetter's (1972) room temperature data. The values of  $\Lambda$  were calculated from equation (5.8) for two cases: (i)  $Z_c = Z_a = 2$  and (ii)  $Z_c = Z_a = 1.6$ . Table 5.8 indicates that for case (ii) the agreement between the observed and calculated values of  $(\partial c/\partial T)_p$  for MgO and CaO is very good (except for  $c_{44}$ ) whereas for case (i) the agreement is very poor.

The concept of an effective charge governing the Coulombic interaction has been discussed by many authors. Son and Bartels (1972) pointed out that the effective charge model made the decomposition of the elastic properties and the repulsive parameters for the oxides appear more like those of the fluorides. Sirdeshmukh and Rao (1975) demonstrated that the use of an effective charge in the calculation of the Gruneisen

	Table 5.8: Comparison of calculated and measured values of $(\partial c/\partial T)_p$ for LiF, NaF, MgO and CaO.							
	d (A <sup>O</sup> )	K <sub>S</sub> (kbar)	Z	Λ	$\left(\frac{\partial c_{11}}{\partial T}\right)_{P}$	$\left(\frac{\partial c}{\partial T}'\right)_{p}$ (then	$\left(\frac{\partial c_{44}}{\partial T}\right)_{P}$	$\left(\frac{\partial K_{S}}{\partial T}\right)_{P}$
LiF	2.0132 <sup>2</sup>	704 <sup>2</sup>	1	7.17	-0.70	-0.36	-0.073	-0.22
					(-0.67)4	(-0.27)	(-0.22)	(-0.30)
NaF	2.3165 <sup>2</sup>	483 <sup>4</sup>	1	8.22	-0.55	-0.29	-0.048	-0.17
					(-0.56)4	(-0.28)	(-0.075)	(-0.19)
Mg0	2.1065 <sup>3</sup>	1628 <sup>5</sup>	2	5.53	-0.38	-0.19	-0.067	-0.13
			1.6	7.51	-0.63	-0.33	-0.064	-0.19
					(-0.59) <sup>5</sup>	(-0.30)	(-0.122)	(-0.20)
Ca0	2.4055 <sup>3</sup>	1140 <sup>3</sup>	2	6.26	-0.31	-0.16	-0.044	-0.10
			1.6	8.66	-0.54	-0.28	-0.043	-0.16
					(-0.55) <sup>6</sup>	(-0.27)	(-0.072)	(-0.19)

1.  $(\partial c/\partial T)_p$  measured at room temperature for CaO and at high temperatures for LiF, NaF and MgO.

- 2. Miller and Smith (1964)
- 3. Son and Bartels (1972)
- 4. This work
- 5. Spetzler (1969)
- 6. Bartels and Vetter (1972)

parameter  $\gamma$  for the alkaline earth oxides resulted in agreement with the thermal values of  $\gamma$ . Following Anderson's (1972) discussion of bulk modulus systematics, we have shown earlier in this Chapter that a relative effective charge of the oxides with respect to the fluorides of  $S = \frac{Z^0}{2Z^F} = 0.80$  for the rocksalt structure made  $KV/Z_cZ_ae^2$  the same constant for all of the rocksalt fluorides and oxides. The good agreement between the observed and calculated values of  $(\partial c/\partial T)_p$  for MgO and CaO for  $Z_c = Z_a = 1.6$  supports the application of the above result to equation (5.9) where  $\phi$  is now the same constant for both the oxides and fluorides. Equations (5.6) and (5.9) demonstrate that  $(\partial c/\partial T)_p$  should be similar for the members of a fluoride-oxide analogue pair chosen on the basis of similar ionic radii (e.g. LiF-MgO, NAF-CaO), the differences arising from the fact that the nearest neighbour distances are not exactly equal (Table 5.8).

While Mitskevich's (1965) theory is limited by its very simple lattice potential, particularly in the description of  $(\partial c_{44}/\partial T)_p$ , it can be applied in conjunction with the observed bulk modulus systematics to describe some of the observed trends and relationships in a semiquantitative manner. In particular, this theory demonstrates the importance of the nearest neighbour distance as a parameter controlling the temperature dependence of the elastic moduli.

Following the success of our model incorporating Mitskevich's theory and K-V systematics for the rocksalt structure, it is of interest to investigate its validity for the fluorite structure. No simple equations such as (5.6) have been derived for this structure due to the complexity of evaluating the lattice sums in the potential energy. An added complication is introduced by the fact that the fluorite lattice is non-centrosymmetric. However, the qualitative behaviour of  $(\partial c/\partial T)_p$  as a function of nearest neighbour distance can be illustrated in Figure 5.5 which is a log-log plot of  $(\partial c/\partial T)_p$  versus molar volume per ion pair.



<u>Figure 5.5</u>: Log-log plot of  $|(\partial c/\partial T)|_p$  (from Table 5.4) versus molar volume per ion pair for the modes  $c_{11}$ , c' and  $c_{44}$  for the alkaline earth fluorides (fluorite structure). The data points from left to right are CaF<sub>2</sub>-SrF<sub>2</sub>-BaF<sub>2</sub>. For comparison, the calculated curves for the alkali halides (Figure 5.4) are shown as dashed lines.

We can see that for the modes  $c_{11}$ , c' and  $c_{44}$  the data for the series  $CaF_2-SrF_2-BaF_2$  are monotonically decreasing with increasing volume and describe roughly linear trends. The theoretical trends calculated for the rocksalt structure are drawn in for comparison. The fluorite and rocksalt lattices are qualitatively similar in the dependence of  $(\partial c/\partial T)_p$  on interionic distance.

For the rutile and perovskite structures, there are neither obvious trends nor theoretical calculations to elucidate the important parameters controlling the temperature dependence of the elastic moduli. We commented previously on the absence of simple trends for the rutile fluorides and oxides in the discussion of Tables 5.5 and 5.6. The theoretical lattice calculations of Striefler and Barsch (1973, 1974, 1975) for the rutile structure do not include estimates of  $(\partial c/\partial T)_p$ . The rutile lattice is complicated by the presence of second nearest neighbour interactions, anion-anion repulsion and non-central forces in general (including bond-bending for the oxides). For the perovskite structure, the tractability of its cubic symmetry to theoretical treatment is outweighed by the complication of two types of cation-anion interaction.

Despite the absence of systematic behaviour for the temperature derivatives of the single crystal elastic moduli for the rutile and perovskite structures, it is nevertheless of interest to compare the temperature derivatives of the isotropic elastic moduli,  $K_S$  and  $\mu$ , for oxides and fluorides in all four structures studied. In Figure 5.6, we have plotted  $(\partial K_S / \partial T)_p$  versus molar volume per ion pair on a log-log plot. We can note several features of Figure 5.6. (1) The rocksalt and fluorite-structure fluorides follow a monotonically decreasing trend with increasing molar volume, which is consistent with the earlier discussions involving Mitskevich's theory. The rocksalt oxides scatter quite widely about a similar trend; however, the errors for SrO and BaO are large (50%) (Bartels and Vetter, 1972; Vetter and Bartels, 1973).



<sup>&</sup>lt;u>Figure 5.6</u>: Log-log plot of  $|(\partial K_S/\partial T)|_p$  versus molar volume per ion pair  $(2M/\rho)$  for fluorides and oxides in the rocksalt, fluorite, rutile and perovskite structures. The data are taken from Tables 5.3-5.7; the molar volumes are listed in Table 5.1. The fluorite and perovskite oxides plot much higher than their fluoride counterparts, so that use of the same symbols for oxides and fluorides causes no confusion.  $(\partial K_S/\partial T)_p$  for ThO<sub>2</sub> is taken from Spinner <u>et al.</u> (1963).

(2) Except for the rocksalts and SnO<sub>2</sub>, the oxides are characterised by high values of  $(\partial K_S / \partial T)_P$ ,  $\cong$  -0.36 to -0.41 kbar. deg<sup>-1</sup>. In general, values of  $(\partial K_S / \partial T)_P$  for the fluorides lie between -0.15 and -0.20 kbar. deg.<sup>-1</sup>.

Values of  $(\partial \mu / \partial T)_p$  are plotted versus molar volume per ion pair on a log-log diagram in Figure 5.7. (1) We can note a fairly well defined trend for the rocksalt fluorides and oxides in which  $|(\partial \mu / \partial T)_p|$ decreases with increasing molar volume. Similar behaviour occurs for the fluorite-structure fluorides. The rutile-structure compounds do not exhibit systematic behaviour. (2)  $(\partial \mu / \partial T)_p$  appears to be much more sensitive to volume than does  $(\partial K_S / \partial T)_p$ ; at small molar volumes (e.g., LiF and MgO),  $|(\partial \mu / \partial T)_p|$  is larger than  $|(\partial K_S / \partial T)_p|$ , while at larger molar volumes the reverse is true.

It should be pointed out here that the values of  $(\partial \mu/\partial T)_p$  are the average of the values calculated for the Voigt and Reuss bounds. For the rutile-structure compounds,  $(\partial K_S/\partial T)_p$  is determined in a similar manner. The validity of this approach is supported by the comparison of our calculated  $(\partial K_S/\partial T)_p$  and  $(\partial \mu/\partial T)_p$  for MgF<sub>2</sub> with the measured values for polycrystalline samples of Bailey <u>et al</u>. (1975) and Rai and Manghnani (1976).

(2K <sub>S</sub> /2T) <sub>P</sub>	(20/9L)		
(kbar deg <sup>-1</sup> )	(kbar deg <sup>-1</sup> )		
0.160	0.079		This work
0.154	0.098		Bailey <u>et al</u> . (1975)
0.160	0.092	А	
0.155	0.088	В	Rai and Manghnani (1976)

Thus we can perhaps expect that the values of  $(\partial K_S / \partial T)_p$  and  $(\partial \mu / \partial T)_p$  for polycrystalline aggregates should reflect any existing trends for the derivatives of the single crystal moduli.

We can examine Figure 5.6 and 5.7 in the framework of the fluoride-



Figure 5.7: Log-log plot of  $|(\partial \mu / \partial T)|_p$  versus molar volume per ion pair  $(2\overline{M}/\rho)$  for fluorides and oxides in the rocksalt, fluorite, rutile and perovskite structures. The data are taken from Tables 5.3-5.7; the molar volumes are listed in Table 5.1.  $(\partial \mu / \partial T)_p$  for ThO<sub>2</sub> is taken from Spinner et al. (1963).

oxide modelling scheme. We concluded earlier for the rocksalt structure that the temperature dependence of the elastic moduli for the fluorides and oxides was governed by the same relationship in terms of nearest neighbour distance only. In this model, the simple concept of effective charge seemed sufficient to account for the more covalent nature of the oxides; this was also true for all the structures considered in the discussion of K-V systematics and to a lesser extent for µ-V systematics. The extreme difference between  $(\partial K_S / \partial T)_P$  of the fluorides and oxides for the other three structures prompts us to look at scaling laws for  $(\partial K_{g}/\partial T)_{p}$ , analogous to the considerations for K-V systematics. We can examine values of  $(\partial \ln K_S / \partial T)_p = \frac{1}{K_S} (\partial K_S / \partial T)_p$ , which tend to fall into two groups, one for the fluorite and perovskite-structure compounds, and one for the rutile structure compounds. This would seem to indicate that for a particular structure the scaling parameter is approximately  $S^2 Z_2 Z_3$ . However, in the absence of any theoretical foundation, it is difficult to justify a predictive approach such as that discussed for the bulk moduli of fluorides and oxides.

An alternative approach is to employ isostructural compounds of similar chemical composition to predict the elasticity of unmeasured phases. Such an approach has been used by Chang and Graham (1975) who plotted  $(\partial K_S/\partial T)_P$  versus cationic radius for the rutile-structure oxide series  $SiO_2-GeO_2-TiO_2-SnO_2$ . Examination of Figures 5.6 and 5.7 in this light indicates that a reasonable value for  $(\partial K_S/\partial T)_P$  of stishovite should be  $-0.38\pm0.1$  kbar. deg<sup>-1</sup>. This is certainly consistent with the value of -0.35 kbar. deg<sup>-1</sup> for  $(\partial K_S/\partial T)_P$  obtained by Graham (1973) from the reduction of shock wave data for stishovite. A similar estimate can be made for  $(\partial K_S/\partial T)_P$  for the perovskite-structure polymorph of MgSiO<sub>3</sub>. The systematics for  $(\partial \mu/\partial T)_P$  for the rutile and perovskite structures are too inconclusive to enable predictions to be made for stishovite and MgSiO<sub>3</sub>-perovskite.

#### 5.5 $(\partial c/\partial P)$ systematics

The study of the relationship of  $(\partial c/\partial P)_T$  to crystallographic parameters has been furthered by the discussion of Davies (1975). Davies demonstrated for the alkali halides that K' =  $(\partial K/\partial P)_{T,P=0}$  is remarkably constant, and that  $K\mu'/\mu$  where  $\mu' = (\partial \mu/\partial P)_{T,P=0}$  decreases monotonically with increasing cationic radius. K' does not vary systematically for the oxides and silicates, although a tendency of  $K\mu'/\mu$  for a particular structure to decrease with increasing cationic radius was noted by Davies. In view of the results of central force models (e.g., 0. L. Anderson and Liebermann, 1970) that account for the behaviour of  $(\partial c'/\partial P)_T$  and  $(\partial c_{4\mu}/\partial P)_T$  for simple cubic lattices, Davies postulated that the trends he observed for  $K\mu'/\mu$  were probably a simple, though as yet undetermined, function of crystal structure.

We will now consider our new pressure data for the perovskite  $\mathrm{KMgF}_3$  in the context of the above relationships, together with the values of K' and  $K\mu'/\mu$  for oxides and fluorides in the rutile and perovskite structures. In Figure 5.8 we have plotted K' and Kµ'/µ versus a mean lattice spacing per ion pair. For K', no systematic trend can be discerned except that, in general, K' is larger for the oxides than for the fluorides. We can at least conclude that K' should lie between 5 and 7 for stishovite and the perovskite phase of MgSiO<sub>3</sub>. The trend for  $K\mu'/\mu$ for the rutile oxides is approximately linear as described by Davies.  $MgF_2$  lies fairly close to this trend, in contrast to NiF<sub>2</sub> for which  $\mu'$  is negative. The low values of  $\mu$ ' seem to be characteristic of the rutile structure (see Tables 5.5 and 5.6). Extrapolation along the rutile oxide trend leads to a value between 2 and 3 for  $K\mu'/\mu$  for stishovite. In the absence of sufficient data to define a trend for the perovskites and in view of the fact that  $K\mu'/\mu$  appears to decrease with increasing interionic distance, we can place a lower limit of 3 on  $K\mu'/\mu$  for the perovskitestructure MgSiO<sub>3</sub>.



Figure 5.8: Plot of K' and Kµ'/µ versus mean atomic spacing,  $V^{1/3}$ , where V is the volume per ion pair, for fluorides and oxides in the rutile and perovskite structures. Values of K' and µ' are listed in Tables 5.5-5.7, while those for K and µ appear in Table 5.1. The volume per ion pair is calculated from the molar volume listed in Table 5.1.

It is wise to be cautious in the application of the above systematics to the prediction of the pressure derivatives of the elastic moduli for unmeasured high pressure phases. There is as yet no theoretical justification for such relationships and the extrapolated values along near-linear trends depend on the method of extrapolation (i.e. linear or power law). Within the experimental scatter, either a straight line or a curve can satisfactorily fit the data over the range of interionic distances. Thus, the estimates of K' and  $K\mu'/\mu$  for stishovite and MgSiO<sub>3</sub>perovskite must be regarded as rather tentative.

#### 5.6 Debye temperature systematics

In Chapter 4, we pointed out that an important parameter controlling the temperature dependence of the elastic moduli was the Debye temperature  $\theta_{\rm D}$ . The elastic moduli data of Table 5.1 may be used to calculate the elastic Debye temperatures from the following equation, which holds for isotropic solids (Debye, 1912):

$$\theta_{\rm D} = \frac{\rm h}{\rm k} \frac{\rm 9\rho N}{4\pi \rm M} \frac{1/3}{\rm v_m} \tag{5.10}$$

where:  $3v_{\rm m}^{-3} = \frac{2}{v_{\rm s}^3} + \frac{1}{v_{\rm p}^3}$ (5.11)

and h and k are Planck's and Boltzmann's constants, N is Avogadro's number, and  $v_{p}$  and  $v_{s}$  the compressional and shear wave velocities. The values of  $v_{p}$  and  $v_{s}$  have been calculated from the single crystal elastic moduli c<sub>ii</sub> by the Voigt-Reuss-Hill averaging scheme; O. L. Anderson (1963) has shown that this method of calculating the elastic  $\boldsymbol{\theta}_{D}$  is equivalent to the more rigorous method of averaging the eigenfrequencies over all possible normal modes and directions of the crystal. Wherever possible, the Debye temperatures given in Table 5.1 have been calculated using the elastic constant data near 0°K; in the other cases, room temperature elastic data were employed so that the values of  $\boldsymbol{\theta}_D$  will be underestimated. In Table 5.9 we also list the ratios of the Debye temperatures for the corresponding fluorides and oxides. With the exception of the pairs containing BaO and ThO<sub>2</sub>, the  $\theta_{\rm D}$  of the fluorides are 65-80% of those for their oxide analogues.

Gmelin (1970) proposed a systematic relationship between the Debye temperature and certain crystallographic parameters:

$$\theta_{\rm D} = \frac{A}{a\overline{M}^{1/2}} \tag{5.12}$$

where a = V\*<sup>1/3</sup> is a mean lattice parameter, A is an empirical constant, and  $\overline{M}$  is the mean atomic weight. In Table 5.1 we list the values of A =  $a\theta_{\overline{D}}\overline{M}^{1/2}$  for the compounds under discussion. For each of the fluoride and oxide isostructural groups, the values of this product are approximately constant, especially for the rocksalt structure. Some of the scatter in this product for the other structures may be attributable to the necessity of using room temperature elastic constant data to calculate  $\theta_{\overline{D}}$ . For the corresponding pairs of fluorides and oxides, the Debye temperatures should thus be related by:

$$\theta_{\mathrm{D}}^{\mathrm{F}}/\theta_{\mathrm{D}}^{\mathrm{O}} = (\mathrm{A}^{\mathrm{F}}/\mathrm{A}^{\mathrm{O}}) (\overline{\mathrm{M}}^{\mathrm{O}}/\overline{\mathrm{M}}^{\mathrm{F}})^{1/2}$$
(5.13)

where  $(A^{F}/A^{O}) \approx 0.6$ . We might expect from this relationship that the Debye temperatures of a particular analogue pair could be very similar, depending on the relative mean atomic weights. For LiF-MgO, for instance,  $\overline{M}^{O}/\overline{M}^{F} = 1.55$  so that (5.13) predicts  $\theta_{D}^{F}/\theta_{D}^{O} = 0.75$  compared to 0.77 in Table 5.9. Thus for some analogue pairs, the fluoride might not be expected to exhibit high temperature elastic behaviour at substantially lower temperatures than the oxide.

Table 5.9:	Ratios	of	Melting	(T <sub>m</sub> )	and	Debye	<u>(θ</u> )	Temperatures	for
							D		

### Oxide-Fluoride Analogue Pairs

Pair 	$\frac{T_m^F/T_m^O}{T_m^O}$	$\theta_{\rm D}^{\rm F}/\theta_{\rm D}^{\rm O}$
LiF-MgO	0.36	0.77
NaF-CaO	0.44	0.73
KF-SrO	0.42	0.72
RbF-BaO	0.46	0.76
KF-BaO	0.49	1.12
CaF <sub>2</sub> -ThO <sub>2</sub>	0.48	1.21
MgF <sub>2</sub> -TiO <sub>2</sub>	0.73	0.79
MnF <sub>2</sub> -SnO <sub>2</sub>	0.59	0.72
KMgF <sub>3</sub> -SrTiO <sub>3</sub>	0.56	0.79

#### CHAPTER 6

#### SUMMARY OF CONCLUSIONS

6.1 Introduction

- 6.2 High temperature elasticity
- 6.3 Systematics in elastic moduli and their pressure and temperature derivatives
- 6.4 Final conclusions on the fluoride-oxide modelling scheme

#### CHAPTER 6

#### SUMMARY OF CONCLUSIONS

#### 6.1 Introduction

Goldschmidt's modelling scheme based on crystal chemical considerations is the origin of both the germanate-silicate and fluorideoxide analogue concepts. The success of the germanate modelling scheme in predicting the high pressure phases of silicates and in examining their elasticity prompted investigation of the fluoride-oxide modelling scheme in the context of high temperature elasticity. There were two aspects to our approach. The first involved examination of the temperature dependence of the elastic moduli in the framework of equations of state to determine whether the fluorides exhibited "high temperature" elastic behaviour at lower absolute temperatures than the oxides. This would enable evaluation of high temperature derivatives at accessible laboratory temperatures, using fluoride models. Our second aim was to determine the relationship between the temperature derivatives of the elastic moduli for the fluorides and oxides, with a view to predicting the high temperature elastic behaviour of the oxides.

The scarcity of data and the dubious quality of some of the existing data made the above comparisons impossible. We therefore developed the capacity to measure the elastic moduli as a function of temperature, using the precise pulse superposition technique, for single crystal fluorides crystallising in the rocksalt, fluorite, rutile and perovskite structures. Our new data are in good agreement with data from other investigators at room temperature and are demonstrably superior to existing high temperature data. Evaluation of our data in the context of high temperature equations of state and systematics in the elastic moduli and their pressure and temperature derivatives lead to the following conclusions.

#### 6.2 High temperature elasticity

Classical lattice dynamic theories predict that the elastic moduli should exhibit a linearly decreasing dependence on temperature for temperatures greater than the Debye temperature,  $\theta_D$ . These theories are couched in terms of volume and temperature as the independent variables so that the prediction of high temperature linearity applies strictly to constant volume rather than constant pressure space. Examination of our new high temperature data demonstrates:

(1) The fluorides do not appear to exhibit "high temperature" elastic behaviour at substantially lower absolute temperatures than do the oxides. This was illustrated for the fluoride-oxide analogue pairs, LiF-MgO and  $MgF_2-TiO_2$ . This result is not inconsistent with the relative magnitude of the Debye temperatures.

(2) In the experimental temperature range, the c-T data at constant pressure (1 bar) continue to exhibit curvature, rather than the predicted linearity. For CaF<sub>2</sub>, SrF<sub>2</sub>, BaF<sub>2</sub> and MgF<sub>2</sub>, the deviation from linearity is consistent with the experimental variables being P and T, and can be largely eliminated by the correction to constant volume. However, for the c' and  $c_{44}$  modes for LiF and NaF, the curvature is in the opposite sense, and correction to constant volume merely accentuates the deviation from linearity. This demonstrated concave upward curvature in the c-T plot must have important implications for lattice dynamical theories.

#### 6.3 <u>Systematics in elastic moduli and their pressure and temperature</u> derivatives

Our new data were combined with data from the literature in order to examine established and postulated elasticity systematics in terms of the fluoride-oxide modelling scheme. (1) Fluorides are excellent models for the oxides using bulk modulus-volume systematics. A uniform relative effective charge of S = 0.75 of the fluorides with respect to the oxides for all of the structures considered permits the prediction of the bulk modulus of an oxide from that of its fluoride analogue. The data for the more complex rutile and perovskite structures do not fit the KV = constant systematics quite as well as the data for the rocksalt and fluorite structures.

(2) A systematic trend of  $\mu V^{*}^{4/3}$  = constant is evident in a shear modulus-volume plot, although there is no theoretical foundation for such a trend. An analogous evaluation of the relative effective charge leads to values of S which are more structure sensitive, thus disallowing the fluoride-oxide predictive approach for shear moduli. Consideration of the isostructural trends for the oxides leads to a value of  $\mu$  of 1.7 Mbar for the perovskite-structure polymorph of MgSiO<sub>3</sub>.

(3) Several very interesting features emerge from the examination of the temperature derivatives of the elastic moduli for the fluorides and oxides. (a) The rocksalt fluorides and oxides and the fluorite fluorides exhibit trends of decreasing  $|(\partial c/\partial T)_p|$  with increasing molar volume; such trends are not in evidence for the rutile-structure compounds. (b) The values of  $(\partial c/\partial T)_p$  are very similar for the members of a rocksalt fluoride-oxide analogue pair; analogue pairs for the other structures do not exhibit such similarity. (c) For all the structures considered,  $(\partial K_S/\partial T)_p$  is dominated by extrinsic temperature dependence; in some cases e.g., the alkali fluorides,  $K_S$  actually increases very slowly with temperature at constant volume. In contrast, for  $(\partial \mu/\partial T)_p$ , the intrinsic component is at least as important as the extrinsic component. The above result leads us to speculate that static lattice models which describe the effect of volume change on the elastic moduli might provide reasonable values for  $(\partial K_S/\partial T)_p$ . A simple model incorporating Mitskevich's theory with K-V systematics was employed to explain the observed behaviour for  $(\partial c/\partial T)_p$  for the rocksalt fluorides and oxides in terms of nearest-neighbour distance only. The values of  $(\partial K_S/\partial T)_p$  and  $(\partial \mu/\partial T)_p$  were plotted versus molar volume for all the structures considered. As expected from our model, the rocksalt fluorides and oxides and fluorite fluorides exhibited systematic trends in these plots. In general, and excluding the rocksalt structure, values of  $|(\partial K_S/\partial T)_p|$  are very much higher for the oxides than for the fluorides and appear to be scaled as  $S^2 Z_c Z_a e^2$ . Using an isostructural, isochemical predictive approach, values of  $(\partial K_S/\partial T)_p = 0.38\pm0.1$  kbar. deg<sup>-1</sup> were estimated for both stishovite and the perovskite-phase of MgSiO<sub>3</sub>.

#### 6.4 Final conclusions on the fluoride-oxide modelling scheme

The fluoride-oxide modelling scheme centred on the structural correspondences between fluoride-oxide analogue pairs with similar ionic radii. The "weakened model" concept suggested that the difference in physical properties could be attributed to the fact that the valence charges of the fluorides were half those for the oxides. This model was shown to give a good representation of the bulk moduli of the fluorides relative to those of the oxides, although an effective charge was invoked to account for the partial covalency of the oxides. The shear moduli of fluorides and oxides also appear to be related in an analogous manner.

The similarity in the temperature derivatives of the elastic moduli for fluoride-oxide analogue pairs in the rocksalt structure can be explained in terms of a simple model where the interionic distance is the only parameter. Here again, the simple concept of an effective charge is sufficient to account for the more covalent nature of the oxides. However, for the fluorite, rutile and perovskite structures, such similarities in the values of  $(\partial c/\partial T)_p$  for a fluoride-oxide analogue pair do not appear. It must be assumed for these structures that the

higher degree of covalency for the oxides plays a much more important role in determining  $(\partial c/\partial T)_p$ . In the absence of a theoretical basis for these differences in  $(\partial c/\partial T)_p$  for the fluorides and oxides, it is wiser to examine isostructural, isochemical relationships for predicting the elasticity of unmeasured phases.

As a predictive tool for the high temperature elasticity of the oxides, the fluoride-oxide analogue scheme is limited. Only for the rocksalt structure can we estimate values of  $(\partial c/\partial T)_p$  for the oxides from those of the fluorides. In addition, we have shown that the fluorides do not exhibit high temperature elastic behaviour at significantly lower absolute temperatures than their oxide analogues. However, in the absence of good single crystals of oxides and silicates, measurement of fluoride structural analogues does provide information on the relationship of elasticity to crystallographic parameters for a particular structure. The study of simple ionic compounds in which the forces are fairly well understood is a particularly useful one in increasing our understanding of the behaviour of solids as a function of temperature and pressure. The value of our results for the temperature dependence of the elastic moduli lies in the fact that we have measured structural analogues of important mantle phases.

The limited success of the fluoride-oxide modelling scheme prompts suggestions for the direction of future research: (1) The study of analogue compounds isostructural and isochemical with high pressure phases, to avoid difficulties raised in the fluoride-oxide modelling scheme by the difference in bonding type. (2) Development of the theoretical basis for systematics in the pressure and temperature derivatives of the elastic moduli. In particular, the modified rigid ion models of Striefler and Barsch (1973, 1974, 1975) might be extended to provide theoretical estimates of  $(\partial c/\partial T)_p$ . (3) Development of

experimental techniques to measure the elasticity of high pressure phases of analogue compounds in situ after synthesis as a function of pressure and temperature. A further possibility is the extension of the temperature range of measurement of the elastic moduli at constant pressure by the use of improved bonding techniques.

#### APPENDIX A

#### CALCULATION OF CRYSTAL MISORIENTATION EFFECTS

The relationship between the misoriented axes and the crystallographic axes is illustrated in Figure A.1, where, following Waterman (1959),  $\{y_i\}$  are the pure mode axes and  $\{x_i\}$  are the misoriented axes. The polar misorientation angle  $\theta$  together with the angle  $\phi$  are given in Table A.1 for the propagation directions of interest for each crystal.

Waterman has derived expressions for the fractional change in velocity,  $(\Delta v/v)$ , arising from the misorientation, in terms of the angles  $\theta$  and  $\phi$ . We have used these expressions directly in calculating the relative change in the elastic moduli, c, for crystals with cubic and tetragonal symmetry.

The effect of crystal misorientation on the temperature derivatives of the elastic moduli, c, can be calculated as follows:

$$\frac{\Delta \dot{c}}{\dot{c}} = \frac{\dot{c} \cdot \dot{c}_{\circ}}{\dot{c}} = \frac{\frac{\partial}{\partial T} (\rho (v + \Delta v)^{2}) - \frac{\partial}{\partial T} (\rho v^{2})}{\frac{\partial}{\partial T} (\rho (v + \Delta v)^{2})}$$
(A.1)

Neglecting terms of order  $(\Delta v)^2$ , equation (A.1) becomes

$$\frac{\Delta \dot{\mathbf{c}}}{\dot{\mathbf{c}}} = \frac{\frac{\partial}{\partial T} [\rho v^2 + 2\rho v \Delta v - \rho v^2]}{\frac{\partial}{\partial T} (\rho (v + \Delta v)^2)}$$
$$= \frac{2\rho v^2 \frac{\partial}{\partial T} \left(\frac{\Delta v}{v}\right)}{\frac{\partial}{\partial T} (\rho + \Delta v)^2)} + 2 \left(\frac{\Delta v}{v}\right) \frac{\frac{\partial}{\partial T} (\rho v^2)}{\frac{\partial}{\partial T} (\rho (v + \Delta v)^2)}$$
$$\approx \frac{2 \dot{\mathbf{c}}}{\dot{\mathbf{c}}} \frac{\partial}{\partial T} \left(\frac{\Delta v}{v}\right) + 2 \left(\frac{\Delta v}{v}\right) \qquad (A.2)$$

Waterman's equations for  $(\Delta v/v)$  can then be differentiated with respect to T to evaluate  $\frac{\partial}{\partial T} \left(\frac{\Delta v}{v}\right)$  in (A.2).


Figure A.1: Relationship between the misoriented axes and the crystallographic axes for crystals of cubic and tetragonal symmetry.

ABLE A.1: Misorientation angle	for each	of the	seven	crystals	studied
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Compound	Direction	θ	φ
LiF	[001]	0.3°	45°
	[110]	0.3°	0
NaF	[001]	0.3°	45°
	[110]	0.3°	60°
CaF <sub>2</sub>	[001]	1.5°	45°
	[110]	1.5°	0
SrF <sub>2</sub>	[001]	1.3°	45°
	[110]	0.5°	0
BaF <sub>2</sub>	$\begin{bmatrix} 110 \\ 1\overline{11} \end{bmatrix}$	3.5° 0.3°	70° 45°
MgF <sub>2</sub>	[100] [110] [001] 45° to [001] and [010]	1.0° 0.7° 0.7° 0.3°	56° 90° 45°
KMgF <sub>3</sub>	[110]	0.5°	33°

 $\theta$  and  $\phi$  are defined in Figure A.1

emocouple temperature (see taken to to 1054.470 (dem

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### APPENDIX B

### CALIBRATION OF THERMOCOUPLES

The melting point of gold and the boiling point of water were used as calibration points for the platinum-platinum 10% rhodium thermocouples. The initial and final calibration of thermocouple 1 were made against the gold melting point; thermocouple 2 was calibrated with thermocouple 1 as a reference. Thermocouple 2 was used for the measurements for  $SrF_2$  and  $BaF_2$  and thermocouple 1 for the remainder of the crystals.

The calibration at the melting point of gold involved placement of two adjacent thermocouples in a furnace: one, the uncalibrated thermocouple and one, a thermocouple with a gold wire completing the junction. As the assembly was heated slowly through the gold melting point, evidence of melting was provided by the levelling out of the "gold" thermocouple temperature (see Figures B.1 and B.2). This temperature was taken to be 1064.4°C (Weast, 1972) and the corresponding temperature as measured by the unknown thermocouple was noted. Thermocouple 1 was estimated to be correct to within 2°C. Subsequent calibration indicated that thermocouples 1 and 2 agreed almost exactly with each other. Figures B.1 and B.2 illustrate that thermocouple 1 was not contaminated during the experimental runs.

Both thermocouples were calibrated against the boiling point of distilled water and were found to be correct to within 1°C. The barometric pressure was taken into account in estimating the corrected boiling point of water according to the tabulations in Weast (1972).

79







Figure B.2: Final calibration of thermocouple 1 against the melting point of gold.

### APPENDIX C

### RAW DATA

The primary data, the measured pulse repetition frequencies, are listed as a function of temperature for each compound. The corresponding elastic moduli are also given for all compounds except  $KMgF_3$ . The data appear in the following order:

LiF NaF CaF<sub>2</sub> SrF<sub>2</sub> BaF<sub>2</sub> MgF<sub>2</sub> KMgF<sub>3</sub>

For LiF, NaF, CaF<sub>2</sub> and SrF<sub>2</sub>, the data are presented (in order) for the modes  $c_{11}$ ,  $c_{44}$  ( $v_2$ ), c',  $c_{44}$  ( $v_4$ ) and c"; for BaF<sub>2</sub> and KMgF<sub>3</sub>, the data are listed for the modes c',  $c_{44}$  ( $v_4$ ) and c". The data for MgF<sub>2</sub> appear in the order of the modes given in Table 3.2.

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### C = CII , MODE IS P [001]

# LENGTH (298) = +2894 INCHES + DENSITY(298) = 2+6413 GM/CC

			TEMPERATURE	FREQUENCY	MODULUS, C
TEMPERATURE	FREQUENCY	MODOLOSIC		(247)	(MUAR)
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	
IDEGREED AT	1.26.22				1.051753
		1 147258	424.6	430 • 21	1.051040
294.3	448.29	1.17/300	424 • 1	430.08	1.452296
309.4	446.31	1.130007	423.2	430.31	1.051882
312.4	445.88	1.134332	422.6	430.22	1.052950
319.9	444.78	1.128435	422.2	430.44	1.032730
321.9	444.49	1.126863	422.1	430.49	1.053225
323.1	444.35	1.126133	421.9	430.50	1.053200
324.5	444.15	1.125741	421-9	430.53	1.053755
325.4	443.94	1.123986	421.0	430.56	1.053555
324.4	443.88	1.123627	421.0	4311.56	1.053000
374.5	443.83	1.123370	721 • /	430.57	1.053035
320.5	443.78	1.123106	421.0	430.56	1.053010
326.0	443.76	1.123641	421.0	429.78	1.049551
326.7	443.72	1.122790	427 • 1	427.76	1.039152
327.1	443.69	1.122660	440.9	427.37	1.037120
327.2	443.49	1.122646	443.7	427.28	1.036700
327.3	443.66	1.122479	444.3	427.22	1.030400
327.3	443.60	1.122349	444.7	127022	1.035911
327.4	443.05	1,122283	445.4	42/013	1.034080
327.6	443.02	1,121976	446.9	420075	1.034617
327.9	443.50	1.122(52	447.4	420.00	1.033848
327.9	443.50	1,121976	448.4	420.14	1.032735
327.9	443.50	1 121054	450.2	420.01	1.032081
327 · B	443.50	1.119263	450.2	426.51	1.032002
332 • 1	443.00	1.117.60	450.2	428.50	1.032675
334.9	442.65	1.114053	449.9	420.50	1.032075
337.9	442.20	1 112508	449.9	426.50	1.011125
341.2	441.79	1 1 1 2 3 1 7	480.4	422.28	1.004493
344.5	441.38	109774	489.9	420.98	1.003373
346.7	441.59	1.107/06	491.6	420.76	1.001621
348.3	440.83	1.164923	494.2	420.42	1.000713
349 • 1	440.74	1.100725	495.4	420.24	.998145
356.5	440.5/	1.100.115	498.8	419.72	996400
351.5	440.42	1.105170	501.3	419.38	.996234
352 • 1	440.31	1.107625	501.4	419.35	996155
352.2	440.28	1.104474	501.5	419.33	996111
352.5	440.25	1.104332	501.4	419.32	.996115
352.5	440.21	1.104131	501.3	419.32	.996115
352.5	440.19	1.104050	501.3	419.32	.996180
352.6	440.17	1.103952	500.9	419.33	
352.6	440.15	1.103851	506.1	418.78	
352.6	440.15	1.103851	506.7	418.67	0015118
352.6	440.13	1.103751	508.8	418.42	017076
352.6	440.13	1.103751	513.4	417.71	0
352.5	440.13	1.103755	515.9	417.36	000210
352.3	440.14	1.103/88	514.4	417.31	.785737
352.3	446.15	1.103813	5.0.1		

351.6	440.33	1.104793	518.3	416.99	•984370
355.1	439.88	1.102376	520.0	416.77	.983260
357.8	439.50	1.100367	520.8	416.65	.982684
369.6	437.50	1.000075	520.0	414-49	. 9 8 1 8 3 7
357.5	437.24	1.0707/5	522.0	410.47	0.1.6.3.1
359.8	439.19	1.198/38	522.3	416.44	.761031
363.2	438.70	1.096156	528.4	415.73	. 9/8008
363.6	438.65	1.095865	533.5	414.99	.974291
366.3	438.22	1.093613	540.0	414.06	.969050
366.6	428.18	1.193426	543.6	413.53	.967023
370.3	437 49	1 090019	544.5	412.25	966190
370.3	437.07	1.070830	544.5	413.35	
3/2.5	437.3/	1.089182	54/.3	412.99	. 767373
312.0	437.34	1. 189114	549.5	412.63	. 702010
3/2.8	437.33	1.088971	549.4	412.65	. 962690
3/2.8	437.33	1.088922	549.0	412.65	. 962684
372.6	437.30	1.088865	548.7	412.67	.962813
312.6	427.31	1.11888311	548.3	412.72	. 9 . 30 . 4
372.5	437.30	1 099909	554.3	411.97	. 959336
3/2.3	437.30	1.00000	554.3	411.47/	
372.3	437.31	1.088841	554.3	411.94	• 757177
3/2.2	437.32	1.088920	554.3	411.94	• 959197
371.6	437.38	1.089243	554.3	411.94	.959197
371.5	437.40	1.089371	560.5	411.12	• 955119
371.3	437.42	1.089478	566.0	410.36	.951335
371.3	437.44	1.089528	569.6	409.79	.948541
371.5	437.44	1.089520	570.4	409.72	.948206
371.5	427.44	1 000/520	576.4	407.72	044617
371.4	437 42	1.007520	575.0	400.77	• 7 - 7 - 5 1 /
377.2	43/ . 42	1.007407	5/6.0	408.92	• 7 9 9 2 2 3
377.2	436.12	1.085763	5/6.2	408.90	. 744145
381.3	436.16	1.782795	576.3	408.88	. 944071
384 • 1	435.77	1.080749	593.2	406.49	.932326
387.3	435.29	1.078244	593.2	406.50	.932372
391.5	434.72	1.075231	593.3	406.47	.932253
394.2	434.37	1.073394	612.0	403.90	.919705
397.9	433.82	1.070555	612.0	403.90	.919659
398.4	433.74	1.070145	612.2	403.89	
398.6	473.77	1.070109	612.2	403.87	000074
399.7	433.72	1.070007	03/00	400.01	• 700774
300.7	433.07	1.009907	038.8	399.94	• 700593
378./	433.69	1.069857	640.0	399.78	.899844
398.6	433.69	1.069861	640.5	399.72	.899552
398.4	433.69	1.069894	641.2	399.62	.899049
397.6	433.78	1.070394	642.6	199.44	.898201
397.5	433.81	1.070497	643.6	199.12	. 897596
397.5	433.81	1.170546	644.6	109.19	. 894991
347.6	433.81	1.070542	645.4	377.17	
307.4	133.07	1.070542	013.0	370.74	• 075025
401.2	733.02	1.0/050/	070.2	398.93	.075/31
407.0	433.42	1.000420	070.3	398.90	. 875572
107.9	432.40	1.063432	646.8	398.84	.895301
03/.8	400.66	.901154	647.4	398.78	.894984
911.7	431.86	1.060356	647.8	398 . 74	.894832
413.9	431.65	1.059237	648.7	398.60	. 894165
414.3	431.57	1.058828	650.4	398.38	.893104
420.8	430.81	1.054842	485.3	421.45	1.007884
423.6	431.41	1	10313	721.03	1.00,004
	150.10	1.002/22			

### C = C44, MODE IS S E0013 RANDOM POL.

### LENGTH (298) = .2894 INCHES , DENSITY(298) = 2.6413 GM/CC

TEMPERATURE	FREQUENCY	MODULUS, C	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
294.0	334.79	. 639903	400.5	129.42	18544
299.0	334.56	. 4 3 8 9 0 8	414.1	329.57	. 617478
304.5	334.37	-638042	415.1	327.57	617286
307.3	334.24	.637547	415.7	329.49	.617160
313.2	333.99	.636429	431.3	328.95	614398
321.8	333.62	. 6 3 4 9 3 7	432.3	320.00	614149
322 • 1	333.60	. 6 3 4 7 7 4	434.4	320.00	613708
324.9	333.51	634774	435.0	328.07	.013/00
325 . 7	333.49		435.0	328.67	
326.7	333.46	6034240	433.0	320.02	+13950
338.6	333.92	.031135	438.0	328.51	.012750
339.4	332.72	.031/90	441.2	328.33	.012202
340.0	332.70	.031/03	441.5	328.34	• 612232
343.1	332.07	.0315/0	441.7	328.31	.612134
344.4	332.17	.631015	442.0	328 • 31	.612090
346.6	332.00	. 630703	443.0	328.26	.611917
349	332.59	.630275	443.7	328 • 22	•611714
349.5	332.47	. 6 2 9 9 0 0	444.9	328 • 17	.611498
349.4	332.45	29/95	446.2	328 • 11	•611262
349.9	332.44	. 6 2 9 7 7 4	446.5	328.08	.611143
350.00	332.44	.629729	446.9	328.06	.611059
350.2	332.42	.629689	447.7	328 • 02	.610891
35.0.4	332.40	.629609	448 • 1	327.99	.610770
362.4	332.34	.629548	449.3	327.94	.610555
355.00	332.33	.629272	450 • 2	327.87	•610291
367.0	332.23	• 6 2 8 8 4 0	450.9	327.85	.610181
359.1	332.15	.628493	451.3	327.83	.010097
369.0	332.10	• 6 2 8 2 6 1	453.2	327 • 76	.609809
340.7	332.90	.628109	463.0	327 • 33	.607936
341.1	331.98	.627768	466.0	327 • 21	.607417
345 . 1	331.96	.627665	466.4	327 . 17	.607296
345.7	331.79	.626952	466.9	327 • 17	.607246
344.9	331.74	.626750	468 • 6	327.07	.606852
349.6	331.70	.626572	470.0	326.99	.606540
349-1	331.63	.626290	471.3	326.93	.606267
370.1	331.60	.626164	472.7	326 • 85	.605917
371-1	331.56	.625990	474.7	326 . 74	.605479
372.0	331.49	.625654	484.6	326 . 26	.603457
372.5	331.4/	.625638	484.7	326 . 26	.603436
373.3	331.40	.625291	485.1	326.22	.603297
374.2	331.38	.625211	485.2	326.22	.603276
374.5	331.36	.625122	492.7	325.88	.601870
374.5	331.35	.625077	494.6	325.81	.601564
374.7	331.34	• 6 2 5 0 4 2	498.7	325.60	.600668
381.3	331.33	.625019	501.6	325.47	.600134
501.3	331.07	.623870	506 • 2	325.22	.599060

388399 388399 399 399 399 399 399 399 39	52 • 3 54 • 3 56 • 3 57 • 6 70 • 9 71 • 9 72 • 4 79 • 1 79 • 7 79 • 7 79 • 7 79 • 6 50 2 • 5 50 3 • 1 50 4 • 3 50 7 • 6	331.03 330.99 330.83 330.67 336.62 330.56 330.56 330.56 330.56 330.22 330.22 330.21 330.11 330.11 330.71 330.88	. 6 2 3 6 9 7 6 2 3 5 2 3 6 2 2 8 7 1 6 2 2 1 9 4 6 2 1 9 38 6 2 1 8 5 9 6 2 1 6 9 9 6 2 1 6 9 9 6 2 1 6 9 6 2 0 3 7 8 6 2 0 2 3 2 6 2 0 2 1 6 6 1 9 7 7 3 6 1 9 3 7 5 6 1 8 8 1 1	508.5 513.9 520.5 524.9 530.6 531.0 532.2 533.4 534.2 534.2 534.2 536.8 548.6 562.6 563.6	325 • 15 324 • 85 324 • 51 324 • 30 324 • 01 324 • 00 323 • 94 323 • 85 323 • 81 323 • 69 323 • 69 323 • 69 323 • 67 323 • 67 323 • 14 322 • 49 322 • 38	.598744 .597541 .596086 .595222 .594030 .5936965 .593387 .593387 .592870 .592607 .592607 .592607 .590364 .587627 .587218
	n.					

# C = (C11-C12)/2 , MODE 15 5 L1103 POL. [1-10]

	LENGTH (298)	= .2837 INCHES .	DENSITY(298) = 2.6	413 GM/CC	
			TEMPERATURE	FREQUENCY	MODULUS, C
FMPERATURE	FREQUENCY	MODULUS	TENTERATE E		(MBAR)
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	
					.252497
		331774	521.8	215.45	.252551
295.0	245.92	328986	521.7	215.47	.252581
303.2	244.88	327209	521.7	215.47	.252599
307.6	244.27	324255	521.6	215.77	.252618
313.2	243.19	322468	521.5	215.50	.252629
320.3	242.55	321454	521.6	215.50	.252629
322.5	242.17	321481	521.6	215.50	.252630
322.5	242.18	. 321474	521.5	215.50	.252526
322.5	242.18	. 321409	521.9	215.46	. 247297
322.5	242.18	. 321400	538.7	213.30	. 245495
325.6	241.85	. 320505	544.3	212.55	. 245220
333.9	246.73	.31/520	545.2	212.43	244797
346 • 1	239.11	.313110	546.5	212.25	244147
347.1	238.69	.312020	548.5	211.98	244089
346.9	238.71	.312065	548.5	211.95	244084
346.8	238.73	.312114	548.5	211.95	.244064
346.4	238.92	.312635	548.5	211.95	.244004
345.9	238.95	.312719	557.1	210.91	.241003
345.6	239.51	.312873	557.5	210.83	.241378
345.5	239.03	.312927	559.4	210.73	.241105
345.4	239.06	.312987	550.7	210.17	• 23705/
345.2	239.08	.313048	563.6	210.00	.237753
344.0	239.10	.313116	503.8	209.69	.238/17
344.4	239.14	.313211	500.2	209.18	.23/525
344.3	239.17	.313313	507 7	208.44	.235//3
344.5	239.21	.313407	5/5 7	208.42	.235/20
31711	236.75	.306789	5/5•5	208.42	.235/2/
303.1	235.99	.304761	5/5•1	205.87	.229/82
300.0	235.14	.302497	575 • /	205.76	.229532
374.7	235.12	.302443	576.0	205.48	.228880
3/5 1	231.67	.293389	578 • /	205.45	.228812
421.1	228.78	.285870	578.0	205.41	.228/22
721 1	228.78	.285869	578 • 7	205.41	.228720
721.2	227.95	.283719	577.1	205.41	.228/1/
727.7	227.91	.283629	578 • 7	205.41	.228/29
128.2	227.87	.283521	578.8	204.76	.227234
120.1	227.17	.281731	004.0	204.71	.22/105
433.0	227.15	.281661	605.2	204.04	.225571
733.0	227.09	.281534	610.5	203.76	.224930
439.9	226.37	.279688	012.0	202.90	.222957
456.5	224.95	.276157	617.1	202.75	.222615
150.5	224.91	.275958	620.5	202.58	.222240
450.6	224.91	.275952	621.5	202.37	.221755
450.0	224.90	.275946	623.3	202.37	.221760
450.4	224.90	.275946	623.5	202.36	.221732
450.6	224.90	.275946	023.7	202.02	

					. 221732
		. 268185	623.4	202.30	720961
4/4.3	221.02	268066	626.5	202.02	220701
474.7	221.1/	247431	629.1	201.72	. 220201
476.4	221.52	.20/431	624.6	201.61	. 220032
477.9	221.26	.266/81	(30) 0	201.47	.219698
477.9	221.26	.266781	030.0	201.32	.219377
477.9	221.27	.266811	631.8	201.52	.218946
477.9	221.28	.266831	633.4	201.13	.218524
4//•0	221 20	265885	634.8	200.94	217863
481.1	220.70	264006	637.2	200.65	.217000
483.8	220.50	-204700	637.9	200.53	.21/000
465.8	220.23	.204230	439.3	200.37	.21/228
561.2	218.29	.259418	637.3	200.26	.216992
562.4	218.10	.258971	040.1	200.03	.216476
505.1	217.72	.258034	041.0	200.05	.216353
5(.5.1	217.69	.257969	642.2	199.70	.215983
505.1	217.72	258017	643.5	199.82	215964
505.1	217.72	258013	643.8	199.78	.215/01
504.9	21/•/1	258033	645.5	199.58	.215443
504.7	21/./2	.250035	645.8	199.51	.215294
504.6	217.73	.258040	444.4	199.44	.215151
504.5	217.74	.258088	640.0	199.09	.214362
503.8	217.85	.258351	677.7	199.07	.214314
503.7	217.86	.258370	649.4	177.07	.214281
503.7	217.86	.258370	649.5	199.00	214260
509.4	217.30	.256990	649.4	199.05	214243
508.0	21/ . 50	255777	649.3	199.06	• 21 4205
512.1	210.00	255442	649.2	199.07	.214310
513.1	216.00	• 2 3 3 4 4 6	449.2	199.14	.214461
515.7	216.34	.254660	440.5	199.09	.214361
516.6	216.21	.254332	617.5	199.01	.214180
517.5	216.07	.254005	650.4	100.05	.214040
520.9	215.60	.252871	650.9	170.75	.213619
522.1	215.45	. 252494	652.6	198.10	212642
522-1	215 25	252521	655 • 7	198.32	.212072
523.6	215.25	251989	657.7	198.00	• 211720
523.3	215.24	252449	658.4	197.99	.211902
521.9	215.43	. 2 3 2 4 4 7	00000		

THE REAL FILMING ETACHIOF

# C = C44 , MODE IS S E1103 POL. [001]

# LENGTH (298) = .2999 INCHES , DENSITY(298) = 2.6413 GM/CC

		NOD111 115 C	TEMPERATURE	FREQUENCY	MODULUS, C
TEMPERATURE	FREQUENCY	HODOLOGIC			(MBAR)
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	11120021
294.0 294.0 340.4 340.4 374.6 374.6 422.6 482.1	3 2 2 • 5 8 3 2 2 • 5 8 3 2 2 • 5 7 3 2 0 • 7 0 3 2 0 • 6 7 3 1 9 • 1 7 3 1 9 • 1 7 3 1 7 • 0 3 3 1 4 • 3 3	.637931 .637931 .637911 .629560 .629458 .622836 .622797 .613398 .601577	482.8 525.0 524.9 579.7 616.6 629.2 629.8 630.2 630.2	314 • 37 312 • 38 312 • 33 309 • 63 307 • 74 307 • 12 307 • 10 307 • 08 307 • 06	• 601732 • 593069 • 592863 • 581270 • 573218 • 570571 • 570481 • 570377 • 570340
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		RAW DATA FOR LITH	HIUM FLUORIDE		
	с.	(C11+C12+2C44)/2	, MODE IS P [110]		
	LENGTH (298)	2837 INCHES . [	DENSITY(298) = 2.64	13 GM/CC	
MPERATURE	FREQUENCY	MODULUS	TEMPERATURE	FREQUENCY	MODULUS

TEMPERATURE	FREQUENCY	MODULUS, C	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
294.3	513.65	1.447466	495 . 2	494.67	1.332517
297.1	513.46	1.446292	496.4	494.53	1.331/24
298.4	513.32	1.445414	497.5	494.41	1.331016
304.3	512.87	1.442631	497.5	494.38	1.330855
308.3	512.49	1.4417249	497.5	494.37	1.330828
310.3	512.32	1 . 439226	497.5	494.37	1.330828
312.9	512.11	1.437051	497.4	494.38	1.330887
319.3	511.53	1.434333	496 • 1	494.40	1.331067
322.4	511.23	1.432530	509.3	493.24	1.324043
323.6	511.29	1.431488	510.6	493.08	1.323138
323.6	511.10	1.431716	515.3	492.55	1.320033
323.4	511.09	1 431498	519.7	492.03	1.317001
323.7	511.09	1.431/93	521.2	491.88	1.316140
323.8	511.08	1.431/22	571.5	491.84	1.315883
323.9	511.07	1.431642	521.3	491.81	1.315733
324.1	511.34	1 431404	571.3	491.81	1.315760
324.3	511.04	1.431374	521.1	491.83	1.315878
374.4	511.02	1 431357	520.8	491.87	1.316109
326.9	510.90	1 430495	520.8	491.87	1.316109
343.4	509.36	1.421051	520.6	491.92	1.316388
345.5	509.17	1.419016	520.5	491.94	1.316447
360.0	509.17	1.717910	520.3	491.94	1.316512
351.4	508.51	1.415008	520.5	491.94	1.316495
351.8	500.49	1 415759	520.7	491.94	1.316463
351.8	500.47	1 415764	520.7	491.92	1.316356
351.0	508.47	1.415713	520.8	491.90	1.316270
361.6	508.47	1.415704	521.2	491.88	1.316140
351.6	500.47	1 415717	525.3	491.44	1.313530
351.6	500.49	1.415797	534.9	490.33	1.307089
351.5	509.49	1.415.907	542.6	489.65	1.303030
351.5	508.50	1.415058	544.6	489.43	1.301719
353.4	568.36	1.414084	544.6	489.43	1.301719
358.4	507.88	1.412065	544.4	489.44	1.301783
359.9	507.72	1.411100	544.3	489.46	1.301869
361.7	507.56	1.410094	543.9	489.47	1.301998
364 . 1	507.29	1.408502	543.1	489.53	1.302336
365.0	507.12	1.407510	542.3	489.58	1.302648
367.8	566.91	1.406207	544.8	489.47	1.301893
368.9	506.79	1.405486	551.7	488.79	1.247938
369.8	506.68	1.404830	552.6	488.74	1.297568
384 . 11	505.63	1.398296	562.6	487.74	1.291744
384.4	505.63	1.398296	564.6	487.55	1.290596
304.3	505.60	1.398087	565.3	487.49	1.290239
384.9	505.51	1.397614	567.7	487.17	1.288407
2.2.5 11	5.05 4.0	1 207205	E 7 0 . 2	494.99	1.286723

305.1					
305.0	505.42	1.397026	57(1+2	486.88	1.286756
396.7	504.35	1.390549	570.2	10000	1 201702
394.4	501055	1.570517	570.2	400.07	1.200/02
370.7	504.30	1.390785	5/0.2	486.90	1.286809
395.6	504.46	1.391240	570.2	484.90	1.286809
395.4	504.49	1 201210	5.0.0	400070	
305.0	504.40	1.371380	201.0	485.82	1.280462
375.4	504.49	1.391388	585.2	485.50	1.278578
395.3	504.49	1, 191 191	589.1	105.50	1 174334
196.4		1.5/15/5	307.1	405.12	1.2/0327
375.4	564.49	1.391388	591.9	484.79	1.274451
394.5	504.54	1.391738	593.9	494.54	1.273204
426.1	E.C. 1 44	1 373034		101.30	
424	21.1.4.4	1.3/3020	573.5	484.54	1.2/3069
726.3	5(1.36	1.372604	592.9	484.58	1.273262
426.3	5(1.36	1.372404	E 9 2 . 4		1 272712
474.7	501155	1.072001	572.4	201102	1.2/3/12
20.2	501.35	1.3/2555	571.4	484.73	1.274165
425 • 7	561.36	1.372636	591.2	494.74	1.274308
422.7	501 42	1 274245	501 1	1011/0	1.2/1000
4 2 4 0	201.02	1.074245	571.1	484.77	1.274392
721.0	501.69	1.374676	591.1	484.79	1.274498
420 • 1	501.87	1.375497	591.2	404 70	1 274412
419.9	501 00	1.3/307/	271.2	4840/8	1.2/4413
4.0	501.70	1.3/5899	591.2	484.78	1.274465
414.8	501.92	1.375987	591.4	484.78	1.274401
419.8	501.92	1 374047	F 9 1 /	401070	
410.0	501 72	1.3/0042	571.6	484.77	1.2/4363
11700	561.93	1.376069	591.6	484.75	1.274258
419.8	501.92	1.376042	591.0		1 271027
419.9	501 02	0750012	570.7	404.38	1.2/17//
444	501.72	1.3/5982	602 • 3	483.78	1.268512
796.8	499.37	1.360673	605.8	483.49	1.266838
447.1	409.15	1 3400.20	(0) 0	403.47	1.200030
447.7	477.55	1.300520	008+8	483.12	1.264/23
	499.28	1.360107	612.3	482.78	1.262737
448.1	499.19	1.359622	614.5	102 10	1 241444
448.9	100 17	350022	01403	402.00	1.201000
440.4	477.17	1.357443	616.5	482.29	1.259901
	499.20	1.359612	617.7	482.22	1.259465
448.6	499.22	1.359759	414.2	102.122	1 25 7 105
448.4	100 25	1.357737	010.3	482.10	1.228802
	477.20	1.359906	618.3	482.10	1.258776
778.4	499.24	1.359851	617.9	482.10	1.759857
471.3	494.92	1, 3440.28		402.10	1.220022
470.9	170	1.340030	01/09	482.12	1.258957
	496.93	1.346087	618.5	482.12	1.258895
4/0•/	496.97	1.346342	4 2 7 . E		1 25 4 3 7 0
47.0.6	494.99	344454	027.00	481.35	1.2543/0
470	770.77	1.340450	629.3	481.16	1.253247
170.0	497.00	1.346483	630.8	480.99	1.252298
470 • 4	497.01	1.344575	( ) ) 7	400.77	
470.4	497.01	34/575	032.1	480.78	1.251065
47	77/061	1.3465/5	634.9	480.53	1.249608
1/0.0	497.02	1.346591	637.3	490.25	1.2481124
470.4	497.03	1.344129	124.2	400.25	1.240034
470.6	407 02	1.010021	030.2	480.15	1.247487
470 7	777.02	1.346591	639.7	480.00	1.246592
7/0./	497.01	1.346559	641.1		1 DUE DE D
470.7	497.01	1.3445.54	01111	4/7.0/	1.245057
470.8		1.370504	642.5	479.70	1.244867
170.0	497.00	1.346472	643.4	479.58	1.244216
4/5+5	496.64	1.344266	442.5	177.50	1.241210
475.9	494.42	1.0011200	0-3-5	4/9.56	1.244106
471.0	970.02	1.344104	643.5	479.58	1.244158
7/0.4	496.53	1.343648	643.6	479.64	1.244100
476.7	496.52	1.343661	443 4	1// 50	1.244100
476.7		1.373551	073.6	479.55	1.244023
474.9	496.50	1.343443	643.6	479.53	1.243945
1/0.0	496.48	1.343329	643.7	479.54	1, 143801
476.7	496.47	1, 343307	0.5.7	4/7.54	1.243791
476.6	101 10	1.343307	643.7	479.54	1.243965
	496.49	1.343421	643.7	479.53	1.243930
4/6.4	496.49	1.343432	443 7	4/7.55	1.273737
476 • 1	494.52	1 3435.04	013./	4/7.54	1.243765
474.9	770.52	1.343584	645.9	479.35	1.242873
	496.62	1.344218	647.5	479.17	1.241814
4/5.6	496.62	1.344179	(4) 0	4/7 1/	1.241018
477.3	494.44		018.4	479.01	1.240905
470.4	770.70	1.343166	652 • 8	478.62	1.238651
17.0	496.24	1.341850	65441	470.10	1 234303

486.4495.601.338019657.2477.991.235154488.6495.371.336710658.4477.801.234074480.3495.191.335591661.2477.431.231995490.3494.911.3339701.3339701.3339701.333970

NaF

### C = CII, MODE IS P EUOID

# LENGTH (298) = .3731 INCHES , DENSITY(298) = 2.8062 GM/CC

TEMPERATURE FREQUENCY		MODULUS,C	TEMPERATURE	FREQUENCY	MODULUS,C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
293.6 305.5 318.7 326.6	311 • 12 310 • 10 308 • 85 308 • 09 307 - 79	• 975825 • 969062 • 960846 • 955870 • 953922	527 • 4 528 • 8 528 • 5 540 • 4 547 • 4	289.00 288.78 288.81 287.73 287.06	.834673 .833353 .833537 .826894 .822798 .822793
329 • 4 329 • 4 337 • 5 346 • 7 348 • 1 360 • 4	307 • 78 307 • 05 306 • 13 305 • 99	• 953857 • 949076 • 943099 • 942191 • 934964	558•7 568•7 569•9 572•2 572•0	286.00 285.02 284.89 284.89 284.68	810390 809607 808445 808339 808392
368 • 3 376 • 7 376 • 9 394 • 7 395 • 5	304 • 11 303 • 29 303 • 26 301 • 57	• 929989 • 924703 • 924513 • 913647 • 913075	572+1 581+9 589+3 575+8 575+8 576+2	284.87 283.78 283.06 282.45 282.45	802882 798547 794875 794579 794579
400 • 7 408 • 5 413 • 1 452 • 5	301.02 300.33 299.87 296.05	.910116 .905687 .902759 .878576 .878444	598.5 607.0 609.5 609.9 610.3	282•15 281•36 281•10 281•05 281•02	788349 786802 786508 786525
462 · 9 475 · 8 481 · 7 492 · 4	295 • 14 293 • 98 293 • 31 292 • 34	.872825 .865531 .861386 .855325 .847379	611 • 2 618 • 3 619 • 6 622 • 8 624 • 1	280 • 92 280 • 28 280 • 15 279 • 83 279 • 70	• 781901 • 781901 • 781128 • 779229 • 778458
512 · 6 514 · C 515 · 6	290.41 290.26 290.13	.843356 .842443 .841632	627•0 631•1	279•41 279•02	• 7 7 4 4 2 4

### RAW DATA FOR SUDIUM FLUORIDE

### C = C44, MODE IS S LOUIJ RANDOM PUL.

### LENGTH (298) = .3731 INCHES . DENSITY(298) = 2.8062 GM/CC

TEMPERATURE FREQUENCY		MODULUS, C	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
			542.5	162.94	.264910
298.3	167.23	.281889	503.5	162.97	.264831
310.7	167.07	.281236	504./	102072	.264718
318.2	166.96	.280796	500.0	162.07	.264639
323.0	166.88	.280482	50/ 12	162-07	.264246
342.5	166.58	.279289	5/3.1	102010	.203864
343.2	166.58	.279282	5/8.1	102.01	.263741
347.9	166.50	.278969	580.1	102.07	.203030
351.2	166.46	.278803	590.4	102.10	-262920
355.0	166.40	.278565	592.0	102.43	.262765
363.7	166.27	.278645	594.1	162.37	-262527
369.3	166.17	.277655	597.8	162.33	202521
380.4	166.00	.276977	606 • 7	162.15	221722
395 • 1	165.77	.276063	608 • 3	162.12	261491
405.4	165.61	. 275425	611.4	162.00	240949
420.6	165.37	.274471	618 • 3	161.93	200,0,
438.2	165.39	.273358	623.3	161.85	2000/1
447.0	164.95	.272802	624.4	161.82	-200301
450.3	164.89	.272568	627 • 3	161.1/	.200301
468.9	164.59	.271378	628.7	161.74	.260251
473.1	164.52	.271101	630.8	161.70	.200070
488.0	164.28	.270148	632.6	161.67	• 2577/0
498.5	164.09	.269468	636.3	161.60	.257/00
505.2	163.96	.268906	637.4	161.57	.257578
530.0	163.55	.267285	642.4	161.49	.257214
536.4	163.43	.266819	666.1	161.04	.25/544
539.0	163.38	.266626	649.0	161.37	.258813
545.6	163.26	.266159	649.9	161.34	.258700
547.5	163.22	.266017	653.2	161.28	.2584/3
547.3	163.22	.266009	654.4	161.26	.258394
546.5	163.23	.266051	657 • 2	161.21	.258144
546.7	163.23	.266049	659.0	161 • 17	.258048
553.3	163.12	.265614	660.3	161.15	.25/768
559.0	163.01	.265190	661 • 4	161.12	.25/859
562.4	162.96	.2649.88	662.7	161 • 10	.257778

# C = (C11-C12)/2 , MODE IS S C1103 POL. C1-103

# LENGTH (298) = .2485 INCHES , DENSITY(298) = 2.8062 GM/CC

TEMPERATURE FREQUENCY		MODULUS,C	TEMPERATURE	FREQUENCY	MODULUS, C
Incluses vi	14471	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
IDEGREES KI	(KHZ)	(			
			510 1	253.57	.284631
294.2	287.10	.368631	500.4	255.57	.284129
310.3	285.13	.363386	562.0	253.35	.243/02
310.3	203-40	. 359361	563.4	253.1/	243234
342.1	283.00	359709	565.0	252.97	.203231
321.1	283.17	35.97.44	568.4	252.51	.2021/7
324.7	283.33	. 350670	571.4	252.13	.2812//
336 • 7	281.84	.354727	572.4	252.01	.280997
346.9	280.65	. 351619	272.7	251.57	.279971
359.8	278.87	.347025	5/6.0	201.07	.279909
345.2	278.25	.345411	576.1	251.54	. 278028
341.0	276.26	. 340290	582.6	250.73	274120
301.0	276 23	. 337458	587.0	249.89	270120
384.1	2/5.25	337533	593.1	249.37	. 2/4701
389.3	2/5.10		597.9	248.75	.2/3455
440.8	268.69	• 3211/1	407.4	247.57	.270760
450.5	267.45	.318105	007.4	246.92	.269271
451.4	267.31	.317755	014.5	244.30	.267853
453.2	267.08	.317192	61/.5	240.30	.267054
462.8	265.87	.314217	618.2	270.21	. 267427
466.1	265.47	.313220	619.0	240.11	247124
4 7	245.40	.313653	620.2	245.98	2011469
47.5.0	203.40	311705	621.0	245.86	.200057
7/0.9	204.05	308055	621.9	245.73	.200000
480.0	263.07	. 300833	622.8	245.60	• 266287
486.6	262.92	. 300900	621.3	245.55	.266164
492.0	262.17	.305162	625.5	245.26	.265503
493.8	261.94	.304616	023.3	245 . 17	.265286
499.3	261.25	.302939	627.3	244.97	.264506
504.7	260.57	.301291	629.1	277.02	.264101
506.3	260.35	.300762	630 • 4	244.04	263064
513.1	259.48	. 298665	634 • 1	244.18	. 2 . 2952
517.0	259.91	. 297346	634.4	244.13	262/32
21/ . 7	200.05	. 297163	636 • 1	243.90	.20211/
518.3	258.05	294755	636.7	243.88	.262385
519.3	258.00	270/33	637.1	243.79	• 262192
519.6	258.66	. 270677	437.2	243.70	.262126
517.5	258.96	. 29/417	447-1	243.05	.260529
530.4	257.31	.293493	073 • 1	242.87	.260134
533.9	256.92	. 292538	644.3	242.81	.259987
535.1	256.76	. 292182	644.9	272.01	.259579
536.7	256.53	.291632	646 • 3	242.02	259772
566.4	254.19	.286105	647.5	242.47	268979
555.5	254.16	286036	648.6	242.36	250777
555.5	257.10	284772	649.3	242.25	.250/40

# C = C44 , MODE IS S E1163 POL. E0013

# LENGTH (298) = .253C INCHES , DENSITY(298) = 2.8062 GM/CC

	ENFOUENCY	MODULUS	TEMPERATURE	FREQUENCY	100020310
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
$296 \cdot 3$ $318 \cdot 4$ $322 \cdot 9$ $328 \cdot 4$ $341 \cdot 0$ $346 \cdot 6$ $350 \cdot 1$ $357 \cdot 5$ $364 \cdot 7$ $365 \cdot 6$ $365 \cdot 5$ $365 \cdot 9$ $372 \cdot 1$ $376 \cdot 6$ $380 \cdot 5$ $380 \cdot 5$ $383 \cdot 9$ $386 \cdot 1$ $387 \cdot 1$	247.44 246.97 246.85 246.73 246.48 246.25 246.25 246.11 245.92 245.90 245.90 245.90 245.76 245.57 245.67 245.57 245.49 245.49 245.47 245.47 245.47 245.47 245.97	283798 282504 282210 281877 281169 280835 280556 280556 280170 279673 279635 279610 279247 278975 278708 278504 278504 278302 278302 278179 277610 275726	$431 \cdot 6$ $437 \cdot 7$ $442 \cdot 4$ $446 \cdot 3$ $456 \cdot 7$ $460 \cdot 3$ $460 \cdot 3$ $460 \cdot 1$ $471 \cdot 1$ $479 \cdot 2$ $480 \cdot 1$ $480 \cdot 1$ $480 \cdot 1$ $480 \cdot 1$ $485 \cdot 2$ $510 \cdot 0$ $518 \cdot 5$ $523 \cdot 8$ $547 \cdot 2$ $571 \cdot 1$ $574 \cdot 7$ $575 \cdot 5$ $575 \cdot 0$	$244 \cdot 36$ $244 \cdot 23$ $244 \cdot 09$ $244 \cdot 00$ $243 \cdot 74$ $243 \cdot 66$ $243 \cdot 51$ $243 \cdot 18$ $243 \cdot 18$ $243 \cdot 18$ $243 \cdot 18$ $242 \cdot 42$ $242 \cdot 42$ $242 \cdot 42$ $242 \cdot 42$ $242 \cdot 66$ $241 \cdot 65$ $241 \cdot 65$ $241 \cdot 65$ $240 \cdot 74$ $240 \cdot 73$ $240 \cdot 72$	<ul> <li>275461</li> <li>275098</li> <li>274733</li> <li>274494</li> <li>273798</li> <li>273580</li> <li>272862</li> <li>272291</li> <li>272254</li> <li>271856</li> <li>269292</li> <li>269292</li> <li>269735</li> <li>268192</li> <li>268192</li> <li>267755</li> <li>265775</li> <li>265719</li> <li>265717</li> </ul>

# RAW DATA FOR SUDIUM FLUORIDE

# C = (C11+C12+2C44)/2 , MODE IS P [110]

# LENGTH (298) = .2418 INCHES , DENSITY(298) = 2.8062 GH/CC

		MODULUS	TEMPERATURE	FREQUENCY	MODULUSIC
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
297 • 2 318 • 6 328 • 6 345 • 6 369 • 1 361 • 4 397 • 9 440 • 3 440 • 3 440 • 7 441 • 4 452 • 1 460 • 6	458.60 456.87 455.94 454.44 452.60 451.49 449.97 449.97 446.42 446.42 445.47 445.47 445.47 445.47	. 8 9 0 4 0 2 . 8 8 3 0 9 5 . 8 7 9 2 0 8 . 8 7 2 9 0 6 . 8 6 5 1 3 9 . 8 6 0 5 4 0 . 8 3 9 6 2 0 . 8 3 9 4 7 6 . 8 3 9 2 0 8 . 8 3 5 5 3 5 . 8 3 2 7 4 5 . 8 2 6 3 3 8	496.6 500.7 516.3 518.6 532.1 553.3 557.6 570.2 573.4 592.1 622.1	441.67 441.33 440.26 440.46 438.67 438.29 438.77 436.77 436.37 435.40 435.09 433.48 431.00	.819675 .818475 .813963 .814624 .807573 .806036 .799843 .798210 .794261 .794261 .795000 .766482 .776439



# C = CII , MODE IS P [001]

# LENGTH (298) = .2884 INCHES . DENSITY(298) = 3.1830 GH/CC

	6 6 0 2 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7						422.5	422.9	422.2	421.6	410.8	4.004	407.4	349.4	389.3	369.1 4	368.9 4	365.0	4 + + 95	363.7 4	4.59.4	350.1	1.645	348.9 4	348.6	348.6 4	347.7 4	347.0 4	331.2 4	330.3 4	319.3 4	318.0 4	317.7 4	316.2 4	314.7 4	312.7 4	312.6 4	311.2 4	296.8	(DEGREES K)	TEMPERATURE FRE	
193.78	83.83	83.96			Bu 7	84.71	5	B. 47	5.40	5.5	86.09	P6.12	R6.26	R7 . 13	A7 . 15	88.14	88.15	88.35	A8.38	P8.41	88.45	89.12	A9.15	89.15	89.18	89.20	89.21	89.26	A9.97	90.04	90.51	90.59	90.62	90.65	90.74	9C. Al	97.87	90.87	91.53	KHZ )	QUENCY	
1.593459	1.593764	1.594759		1.595212		1.600259	1-605750	1.605871	1-605930	1.606382	1.610389	1.610621	1.611640	1.618103	1.618173	1.625518	1.625592	1.627097	1.627285	1.627510	1.627787	1.632760	1.632929	1.632969	1.633180	1.633334	1.633378	1.633737	1.639032	1.639565	1.643056	1.643670	1.643848	1.644133	1.644754	1.645358	1.645717	1.645811	1.650723	(MBAR)	MODULUS.C	
673.4	+ · 500	662.6	660.4	659.8	659.7	657.8	653.9	651.3	1 - 5+9	639.7	637.5	637.2	634 . 3	633-2	621.0	620.4	619.3	61104	910.9	- B + C		541.4	540.0	2.683	5/8.4	5/7.8	5/6.2	54.3	553.0	548.0	545.5	514.3	514.0	507.6	506.5	506 • 1	497.2	495.9	479.5	(DEGREES K)	TEMPERATURE	
471 • 43	471.91	472.0A	472.22	472.27	472.31	472.40	472.56	472.71	473.10	473.42	473.57	473.59	473.76	473.82	474.51	4/4.00	4/4.62	4 / S - U +	4/0010	4/2.01	4/0.01	4/0.23	10.00	4/0.30	4/0.1/	4/100	11 - / 1	4/8.3/	47.8.44	4/8./1	4/8.85	480.65	480.6/	481.01	481.06	481.10	481.58	481.64	482.54	(КН2)	FREQUENCT	
1.505164	1.505498	1.509715	1.510723	1.511033	1.511311	1.511939	1.513075	1.514164	1.516726	1.51414/	1.520142	1.520331	1.176.1	1.170.1	700070.1	1 . 7	1.07.001			1.511258	1.536092	1.536260	1.539185	1.519788	1.540109			- 545325						1.0/0000	1.07.000	1.0/0/00	1.0/110	1.00//000	1.584404	(MBAR)	muuurus, c	

# C = C44, MODE IS SLOOIJ RANDOM POL.

### LENGTH (298) = .2884 INCHES , DENSITY(298) = 3.1830 GM/CC

TEMPERATURE FREQUENCY		MODULUS, C	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
296.0	222.66	. 338732	536 • 2	213.36	.309338
320.6	221.72	. 335694	538.3	213.27	.309061
321.3	221.69	. 335629	539.1	213.25	.308983
321.5	221.68	.335582	542.9	213.10	.308534
322 • 1	221.67	. 335548	543.1	213.08	.308489
332.7	221.27	. 334278	557.4	212.51	.306734
332.9	221.26	. 334247	558.3	212.48	.306626
343.3	220.87	. 332996	571.3	211.94	.304987
343.4	220.86	. 332965	571.9	211.92	.304925
350.9	220.59	. 332083	581.3	211.56	.303791
351.1	220.58	. 332:36	582.2	211.52	.303684
373.0	219.73	. 329325	587.5	211.30	.302999
374 • 1	219.68	.329182	591.0	211.16	.302586
375 • 4	219.63	. 3291123	591.2	211.15	.302556
376 • 1	219.61	. 328958	598.9	210.83	.301582
380.7	219.42	. 328 370	599.8	210.78	.301447
381.1	219.42	. 328338	606.0	210.53	.300687
394.3	218.92	. 325761	610.2	210.36	.300156
395 . 1	218.70	. 326681	610.3	210.35	.300127
395.6	218.88	. 326632	616.5	210.09	.299340
399.3	218.73	. 326158	617.8	210.06	.299245
399.7	218.72	.326110	624.2	209.79	. 298429
400.3	218.70	. 326076	624.8	209.76	.298339
416.4	218.07	. 3240.66	626.2	209.72	.298215
416.3	218.07	. 324067	627.8	209.65	.298005
431.9	217.48	. 322185	628.6	209.61	.297899
432.5	217.44	. 322192	632.5	209.45	. 297402
434.7	217.35	. 321809	633.1	209.43	.297341
436.5	217.29	.321603	637.3	209.25	. 296785
443.7	217.3	.320780	641.7	209.08	. 296271
443.9	217.2	. 320749	642.6	209.04	.296160
445.0	216.98	.320622	645.5	208.92	.295819
445.3	216.97	. 320591	646.9	208.86	. 295625
463.3	216.25	.318346	649.2	208.77	. 295353
464.4	216.22	.318220	656.5	208.47	. 294436
465 . /	216.16	.3181:49	657.5	208 • 42	. 294290
4/3.2	215.87	.317139	662.8	208 • 22	. 293/02
4/3.6	215.85	. 317092	665.9	208.09	. 293313
4/3.8	215.84	.317061	667.8	208.02	. 293102
7/5.8	215.76	• 316797	6/2 • 3	207.82	. 292507
503.8	214.65	• 31 3 3 2 1	6/3.0	207.80	.272731
575.5	214.50	.313134	0/5 • 1	207.70	• 272163
524.4	213.80	• 310681	0/5.3	207.69	• 292134
527.4	213.75	• 310557	6//•2	207.61	241045
527.0	213./1	.310417	6//•/	207.59	- 271035
535.1	213.40	.309448	6/8.5	207.56	• 27 1 / 1 /
272.0	213.38	.309399			

# C = (C11-C12)/2 , MODE 15 S [110] POL. [1-10]

# LENGTH (298) = •2948 INCHES • DENSITY(298) = 3•1830 GM/CC

HADULUS

	CREAL CNCY	MODULUSIC	TEMPERATURE	FREQUENCY	HODOLOSIC
TEMPERATURE	FREQUENCI	11000020270	IDE OUTET KI	( K H 7 )	(MBAR)
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES N)	(KIL)	
					.574871
		404294	537.9	284.55	674686
295.5	290.94	.01000	539.6	284.51	
324.6	294.25		E 4 2 . 8	284.42	.5/7250
324.6	290.23	.600989	544.7	284.36	.574009
333.0	290.03	.600055		284.35	.573986
334.1	290.00	.599917	544.9	204.24	.573466
336.9	299.96	.599729	548.9	204 19	.573196
353.7	200.56	.597866	550 • 9	204.10	.572993
352.3	207.50	.597774	552.4	284.13	.572676
353.0	287.57	594087	554.9	284.00	572499
317.0	288.74	594941	556.0	284.03	672798
377 • 4	288.94		557.4	283.98	. 5/2270
399.4	288.39	. 57242/	558.9	283.94	.5/2070
399.7	288.38	.572382	570.1	283.60	.5/0570
399.9	288.37	.59231/	570.7	283.53	.570252
430.6	288.35	.592226	57207	283.48	.570050
421.0	287.81	.589756	5/4.2	203.37	.569561
421.4	287.79	.589686	5//.6	203.37	.569133
410.5	287.33	.587518	580.9	283.20	.568890
- 37 - 5	207.29	.587348	582.5	283022	-568579
1.5	207 21	586960	584.6	283.15	548490
444.4	287.21	586467	585 . 2	283.13	C (7368
446.4	28/ • 17	694461	594.5	282.88	
446.8	287.12		599.0	282.74	.560/13
447.0	287.12	.50055/	599.8	282.71	· 5660UZ
467.6	286.55	. 58396/	607.6	282.63	.566243
469.0	286.52	.583820	404.3	282.57	.565979
474.9	286.37	.583113	004.5	282.56	.565956
475.6	286.34	• 5830UI	004.5	282.54	.565866
477.6	286.26	.582627	605.2	202.49	.565599
477.7	286.26	.582626	607.1	202.43	.565351
478.5	286.24	.582581	609 • 1	202.43	.565039
470.9	294.22	.582487	611.4	282.30	.564662
7/8 • 7	200.22	.581889	614 • 1	282.28	- 564593
483.4	280.10	.581571	614.7	282.26	-544085
486.3	286.03	581137	618.2	282.15	643931
489.7	285.73	580772	619.2	282.11	
492.6	285.85	579491	620.9	282.06	. 563/00
500.9	285.61	577601	622.5	282.00	. 503770
501.4	285.59	. 5/7573	623.0	281.95	. 563237
503.8	285.53	.5/7270	427.3	281.85	.562/00
504.9	285.49	• 5/ 415 4	427.8	281.83	.562/14
508.3	285.41	.5/8/6/	428.5	281.81	.562604
522 . 1	285.01	.576953	(20.1	281.76	.562363
527.6	284.86	.576269	630.1	281.74	.562296
529.5	284.81	.576020	030.0	2010/1	
534.9	284.65	.575297			

### C = C44 , MODE IS S LIICJ POL. [001]

# LENGTH (298) = .2948 INCHES , DENSITY(298) = 3.1830 GM/CC

TENREDATIONE	ERFOLIENCY	MODULUS	TEMPERATURE	FREQUENCY	MODULUS, C
TEMPERATURE	FRE OF TE		(DEGREES K)	(KHZ)	(MBAR)
(DEGREES K)	(KHZ)	(MBAR)	TOEGREES WY		
				210.42	.314721
205 5	217.75	.338507	489.4	210.12	.314284
275.5	21/	333205	492.8	210.20	. 112763
346.6	216.17	222144	505.5	209.80	311608
341.0	216.12		514.5	209.44	.311000
341.1	216.12	.333128	514.5	208.98	.310168
343.0	214-28	.332998	526.2	200 . 20	.308020
342.0	210.00	. 332973	543.9	208.30	- 306560
342.3	210.17	332040	555.5	207.84	204011
350.0	215.78	.332040	559.9	207.66	. 300011
350.1	215.78	. 332032	544.0	207.44	. 305302
340.5	215.78	.332035	500.0	207.35	· 30500P
348.5	215.78	.332024	570.0	207.35	. 3114549
349.0	215.70	330784	572.3	207.20	204339
359.0	215.40	330/84	573.9	207.13	. 30 7 3 3 7
359.9	215.37	.330800	580.1	206.90	.303025
359.9	215.34	.330609	500.1	204.51	.302420
344.4	215.18	.330076	294.3	200.01	.301927
304.0	215.05	. 329652	593.6	206.30	201006
368 • 1	215.115	320001	600.6	206.06	.301000
374.1	214.81	. 320801	403.5	205.95	.300050
380.00	214.61	.328211	803.5	205.69	.299857
382.1	214.53	.327966	610.0	205.52	.299346
302 .	214.34	. 327 359	614.0	205.52	.298702
386.8	217.5	326715	619.5	205.32	294402
392.4	214.15	224204	621.7	205 • 22	.270102
394.9	214.05	.320387	423.9	205.13	. 298124
394.3	214.00	. 326221	023 1	204.93	.297524
405.4	213.63	.325041	020.0	204.90	.297400
405.0	213.62	.325716	629.6	204.70	. 297174
405.9	213.02	324967	631.8	204.82	201915
408.5	213.50	324004	633.6	204.75	.270705
407.5	213.50	. 32 4800	434.5	204.72	. 290049
407.5	213.55	. 324791	()	204.70	• 296791
412.5	213.37	.324191	034.5	204.49	.246760
412.6	213.17	. 324191	634.8	204.07	. 296752
12.3	212.24	. 324162	635.0	204.00	244728
414.4	213.30	324042	635.2	204.68	201704
413.6	213.33	. 324502	635.5	204.67	. 290/01
440.3	212.32	.320/95	435.4	204.66	.296661
440.5	212.31	.320763	() ( )	204.65	• 296638
447.6	212.29	.320695	035.1	204 . 44	.296614
440.0	211.96	.319659	636.0	204.04	294583
1 7 7 • 7	211 05	319636	636.2	204.63	201575
450.0	211.95	314570	636.3	204.63	. 2703/3
474.7	211.00	.3105/0	637.1	204.60	. 296504
475.0	210.99	.31053/	137.0	204.57	.296404
477.5	210.94	.316391	63/ • 9	201.50	. 296189
	210.73	.315707	639.6	204.55	
401.0	210.75				

### C = (C11+C12+2C44)/2 , MODE IS P [110]

### LENGTH (298) = .2948 INCHES . DENSITY(298) = 3.1830 GM/CC

<b>IEMPERATURE</b>	FREQUENCY	MODULUS, C	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
301.7	440.46	1.384940	603.5	423.37	1.270534
301.5	440.47	1 384809	607.0	423.15	1.269105
322.9	440.47	1.3772/3	613.5	422.72	1.266355
373.3	437.37	1 377303	415.4	422.60	1.265577
340.7	437.35	1.377207	619.0	422.38	1.264148
340.7	438.40	1.3/1147	017.0	422.50	1.262406
341.0	438.44	1.3/1015	623.1	422.11	1.242198
358.3	437.53	1.364852	624.0	422.08	1. 241881
359.1	437.48	1.364517	624.6	422.03	1.201001
376.6	436.55	1.358200	626 • 3	421.94	1.201200
317.9	436.48	1.357725	629.6	421.72	1.2570/3
396.6	435.46	1.350822	632.5	421.55	1.258/68
397.7	435.40	1.350385	635 • 1	421.37	1.25/643
410.1	434.67	1.345514	635+6	421.35	1.257508
410.6	434.63	1.345251	636.0	421.33	1.257347
411.3	434.59	1.344982	637 • 1	421.26	1.256865
421.0	434.08	1.341498	637 . 4	421.24	1.256737
421.6	434.03	1.341232	641 • 1	421.01	1.255311
435.6	433.24	1.335922	642.0	420.97	1.254985
438.6	433.10	1.334934	644.3	420.81	1.253961
450.6	412.40	1.330281	651.5	420.36	1.251090
452.5	412.13	1.329760	652.2	420.31	1.250741
453.6	412.26	1.329295	457.8	420.28	1.250574
444.9	430.44	1-317147	651.3	420.25	1.250380
485.3	430.42	1.317043	454.5	420.17	1.249838
505.6	429.22	1 309041	455.0	420.14	1.249674
504.3	427022	1.309714	454.4	420.04	1.249125
509.2	429-01	1.307/78	457.9	410.97	1.248577
514.9	427.01	1.305428	450.4	419.94	1.247875
533.1	428.07	1.303427	657.9	417.00	1.247226
533.6	427.02	1 290 1 14	661.2	419.42	1.246360
537.1	42/ 00/	1.270110	663.5	419.52	1.245751
510.7	427.30	1.296/00	664.7	417.53	1.244266
544.2	42/ 04	1.270137	60001	417.30	1.242974
544.5	426.70	1.274(150	671.2	417.10	1.242401
551.2	426.73	1.273887	0/2.0	417.01	1.242229
552.1	426.53	1.291255	0/3.3	418.78	1.242000
552 • 1	426.47	1.290893	0/4.0	418.44	1 240115
335.1	426.30	1.289740	6/8.5	418.65	1.240110
200.0	426.20	1.289439	6/9.5	418.58	1 239071
201.4	425.93	1.28/304	680.3	418.53	1 . 237322
565.7	425.69	1.285688	681.8	418.42	1.230004
569.1	425.65	1.285400	682.8	418.35	1 230240
5/3.2	425 . 22	1.282615	684.8	418.21	1.23/322
2/5.6	425.08	1.281695	687.0	418.05	1.236309
5/9.3	424.83	1.280102	688.9	417.97	1.235/50
584.8	424.51	1.278(.02	689.9	417.90	1.235306
599.4	423.60	1.272103	695 • 0	417.53	1.232968
00103	423.49	1.271323			

. SrF<sub>2</sub>

# C = CII, MODE IS P [001]

# LENGTH (298) = .3619 INCHES . DENSITY(298) = 4.2820 GM/CC

TEMPEDATIOE	EREQUENCY	MODULUS,C	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
$294 \cdot 2$ $294 \cdot 2$ $309 \cdot 7$ $323 \cdot 7$ $349 \cdot 8$ $353 \cdot 3$ $369 \cdot 4$ $378 \cdot 1$ $398 \cdot 5$ $419 \cdot 1$ $423 \cdot 7$ $435 \cdot 9$ $435 \cdot 9$ $435 \cdot 9$ $436 \cdot 4$ $459 \cdot 6$ $460 \cdot 2$ $481 \cdot 8$ $500 \cdot 7$ $519 \cdot 8$	352.06 351.60 351.15 350.22 350.22 349.68 349.40 348.74 348.74 348.75 347.47 347.47 347.47 346.67 345.92 345.26 344.58	$1 \cdot 2 \cdot 4 \cdot 8 \cdot 4 \cdot 1 \cdot 6 \\ 1 \cdot 2 \cdot 4 \cdot 4 \cdot 5 \cdot 4 \\ 1 \cdot 2 \cdot 4 \cdot 4 \cdot 5 \cdot 4 \\ 1 \cdot 2 \cdot 4 \cdot 1 \cdot 3 \cdot 9 \cdot 7 \\ 1 \cdot 2 \cdot 3 \cdot 5 \cdot 0 \cdot 2 \cdot 6 \\ 1 \cdot 2 \cdot 3 \cdot 4 \cdot 2 \cdot 1 \cdot 7 \\ 1 \cdot 2 \cdot 3 \cdot 5 \cdot 2 \cdot 7 \cdot 7 \\ 1 \cdot 2 \cdot 2 \cdot 7 \cdot 7 \cdot 8 \cdot 8 \\ 1 \cdot 2 \cdot 2 \cdot 7 \cdot 9 \cdot 8 \\ 1 \cdot 2 \cdot 2 \cdot 7 \cdot 9 \cdot 8 \\ 1 \cdot 2 \cdot 2 \cdot 7 \cdot 9 \cdot 8 \\ 1 \cdot 2 \cdot 2 \cdot 7 \cdot 9 \cdot 8 \\ 1 \cdot 2 \cdot 2 \cdot 7 \cdot 9 \cdot 8 \\ 1 \cdot 2 \cdot 2 \cdot 7 \cdot 9 \cdot 8 \\ 1 \cdot 2 \cdot 2 \cdot 7 \cdot 9 \cdot 8 \\ 1 \cdot 2 \cdot 1 \cdot 7 \cdot 6 \cdot 8 \\ 1 \cdot 2 \cdot 1 \cdot 7 \cdot 6 \cdot 8 \\ 1 \cdot 2 \cdot 1 \cdot 7 \cdot 6 \cdot 8 \\ 1 \cdot 2 \cdot 1 \cdot 7 \cdot 8 \\ 1 \cdot 2 \cdot 1 \cdot 7 \cdot 8 \\ 1 \cdot 2 \cdot 1 \cdot 7 \cdot 8 \\ 1 \cdot 2 \cdot 1 \cdot 7 \cdot 8 \\ 1 \cdot 1 \cdot 9 \cdot 1 \cdot 9 \\ 1 \cdot 1 \cdot$	$540 \cdot 3$ $559 \cdot 6$ $560 \cdot 4$ $581 \cdot 0$ $601 \cdot 6$ $602 \cdot 1$ $635 \cdot 8$ $629 \cdot 3$ $621 \cdot 5$ $633 \cdot 5$ $633 \cdot 5$ $6446 \cdot 3$ $653 \cdot 2$ $653 \cdot 2$ $654 \cdot 0$ $664 \cdot 0$ $667 \cdot 7$	$343 \cdot 86$ $343 \cdot 16$ $343 \cdot 14$ $342 \cdot 38$ $341 \cdot 61$ $340 \cdot 33$ $340 \cdot 56$ $340 \cdot 87$ $340 \cdot 42$ $340 \cdot 41$ $339 \cdot 92$ $339 \cdot 65$ $339 \cdot 44$ $339 \cdot 37$ $339 \cdot 13$ $339 \cdot 01$	$\begin{array}{c} 1 \cdot 185733\\ 1 \cdot 180390\\ 1 \cdot 180230\\ 1 \cdot 174459\\ 1 \cdot 168536\\ 1 \cdot 1685418\\ 1 \cdot 168744\\ 1 \cdot 160525\\ 1 \cdot 160525\\ 1 \cdot 167325\\ 1 \cdot 157321\\ 1 \cdot 155344\\ 1 \cdot 153496\\ 1 \cdot 151834\\ 1 \cdot 151288\\ 1 \cdot 150907\\ 1 \cdot 149605\\ \end{array}$

# C = C44 , MODE IS S LODIJ RANDOM POL.

# LENGTH (298) = .3019 INCHES , DENSITY(298) = 4.2820 GM/CC

TEMPERATURE	FREQUENCY	MODULUS, C	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
295 • 7 295 • 8 307 • 0 308 • 2 318 • 3 326 • 6 340 • 1 342 • 2 351 • 9 362 • 6 376 • 3 381 • 0 395 • C 399 • 6 412 • 5 425 • 6 433 • 6 436 • 1 451 • 6	$178 \cdot 10$ $178 \cdot 10$ $177 \cdot 83$ $177 \cdot 80$ $177 \cdot 55$ $177 \cdot 34$ $177 \cdot 00$ $176 \cdot 95$ $176 \cdot 71$ $176 \cdot 09$ $175 \cdot 97$ $175 \cdot 61$ $175 \cdot 509$ $175 \cdot 16$ $175 \cdot 09$ $174 \cdot 83$ $174 \cdot 61$ $174 \cdot 29$ $174 \cdot 15$	• 319498 • 319488 • 318465 • 318342 • 317398 • 316615 • 315335 • 315128 • 314235 • 314235 • 314235 • 314235 • 31911 • 311453 • 309687 • 308438 • 308477 • 307191 • 306401 • 305211 • 304673	471.0 472.7 494.4 501.9 519.4 536.4 550.3 588.6 592.7 595.4 611.7 618.6 632.2 640.1 643.5 653.3 655.7 657.9 659.1	$173 \cdot 69$ $173 \cdot 64$ $173 \cdot 07$ $172 \cdot 86$ $172 \cdot 40$ $171 \cdot 93$ $171 \cdot 93$ $170 \cdot 53$ $170 \cdot 43$ $170 \cdot 34$ $169 \cdot 90$ $169 \cdot 72$ $169 \cdot 11$ $169 \cdot 02$ $168 \cdot 58$	• 302956 • 302789 • 300651 • 299911 • 298174 • 296476 • 295118 • 291300 • 290911 • 290609 • 288295 • 286871 • 28670 • 285729 • 284725 • 28475 •

# C = (C11-C12)/2 , MODE 15 S [110] POL, [1-10]

# LENGTH (298) = .3068 INCHES , DENSITY(298) = 4.2820 GM/CC

50-0-54CV	MODULUS	TEMPERATURE	FREQUENCY	MODULUS, C
FREQUENCY	HOUDEUSIE		1847)	(MBAR)
(KHZ)	(MBAR)	(DEGREES K)	((12)	
$196 \cdot 30$ $196 \cdot 30$ $196 \cdot 30$ $196 \cdot 10$ $196 \cdot 10$ $195 \cdot 93$ $195 \cdot 93$ $195 \cdot 82$ $195 \cdot 42$ $195 \cdot 41$ $195 \cdot 41$ $195 \cdot 42$ $195 \cdot 42$ 195	. 400836 . 400835 . 400835 . 399929 . 399861 . 399179 . 399145 . 398622 . 397585 . 396824 . 395183 . 395183 . 395183 . 395183 . 391676 . 391676 . 391629 . 391594 . 390380 . 390019 . 388945 . 388846 . 388945 . 388806 . 387947 . 386031 . 38559	$5 4 3 \cdot 9$ $5 4 4 \cdot 7$ $5 5 5 \cdot 3$ $5 6 5 \cdot 1$ $6 0 1 \cdot 9$ $6 0 1 \cdot 9$ $6 0 1 \cdot 9$ $6 0 2 \cdot 1$ $6 0 3 \cdot 7$ $6 1 2 \cdot 7$ $6 1 2 \cdot 7$ $6 2 4 \cdot 2$ $6 3 9 \cdot 8$ $6 4 4 2 \cdot 4$ $6 5 5 \cdot 2$ $6 5 5 \cdot 2$ $6 5 6 \cdot 2$ $6 5 6 \cdot 2$ $6 5 5 \cdot 2$ $6 5 6 \cdot 2$ $6 5 6 \cdot 2$ $6 5 5 \cdot 2$ $6 5 6 \cdot 2$ $6 5 6 \cdot 2$ $6 5 5 \cdot 2$ $6 5 6 \cdot 2$ $6 5 6 \cdot 2$ $6 5 5 \cdot 2$ $6 5 6 \cdot 2$ $6 5 6 \cdot 2$ $6 5 5 \cdot 2$ $6 5 6 \cdot 2$ $6 5 6 \cdot 2$ $6 5 5 \cdot 2$ $6 5 6 \cdot 2$ $6 5 7 \cdot 7$ $6 6 2 \cdot 7$ $6 6 3 \cdot 9$	$192 \cdot 81$ $192 \cdot 65$ $192 \cdot 64$ $192 \cdot 64$ $192 \cdot 49$ $191 \cdot 91$ $192 \cdot 15$ $192 \cdot 15$ $192 \cdot 15$ $192 \cdot 15$ $191 \cdot 91$ $191 \cdot 91$ $191 \cdot 50$ $191 \cdot 50$ $191 \cdot 50$ $191 \cdot 24$ $191 \cdot 24$ $191 \cdot 24$ $191 \cdot 24$ $191 \cdot 03$ $190 \cdot 96$ $190 \cdot 94$ $190 \cdot 91$	384985 384938 384241 384186 380853 380853 380864 381963 381940 380941 380706 3800841 380706 380189 378968 378968 378968 378968 377962 377765 377765 37769482 377765 377765 37769482 377695 377695 37659447 376352 376230
	FREQUENCY (KHZ) 196.30 196.30 196.30 196.09 196.09 195.93 195.82 195.59 195.42 195.41 195.06 194.75 194.50 194.27 194.27 194.27 194.27 194.68 193.68 193.64 193.00	FREQUENCY         MODULUS, C           (KHZ)         (MBAR)           196.30         .400835           196.30         .400835           196.10         .399929           196.10         .399929           195.94         .399179           195.95         .398622           195.95         .397585           195.94         .397185           195.95         .397585           195.95         .397585           195.92         .396621           195.93         .397185           195.94         .397585           195.95         .397585           195.92         .39769           195.94         .396781           195.95         .39769           195.92         .393769           195.94         .39769           194.75         .392657           194.27         .391629           194.27         .391629           194.27         .391629           193.68         .388945           193.68         .388945           193.68         .388945           193.46         .387947           193.46         .387947	FREQUENCY         MODULUS,C         TEMPERATURE           (KHZ)         (MBAR)         (DEGREES K)           196.30         .400836         543.9           196.30         .400835         554.7           196.30         .400835         554.7           196.10         .399929         555.3           196.10         .399929         555.3           196.10         .399179         601.9           195.93         .399179         601.8           195.93         .399145         585.8           195.93         .399145         601.8           195.94         .399622         585.8           195.959         .397585         586.2           195.42         .396622         585.8           195.94         .397585         586.2           195.959         .397585         602.1           195.42         .3966781         603.7           195.43         .612.7         .612.7           195.94         .3971679         612.7           194.75         .397169         612.7           194.75         .397169         612.7           194.27         .3970300         637.9           1	FREQUENCYMODULUS,CTEMPERATUREFREQUENCY(KHZ)(MBAR)(DEGREES K)(KHZ)196.30.400835543.9192.81196.30.400835554.7192.80196.30.400835554.7192.64196.30.400835554.7192.64196.30.400835555.3192.64196.40.399861565.1192.64196.09.399861565.1192.64195.94.399179601.8191.91195.93.399175601.8192.15195.82.398622585.8192.15195.59.396624602.1191.91195.41.396824602.1191.91195.42.396624603.7191.88195.66.395183612.7191.73194.75.392657626.2191.50194.75.397169632.9191.31194.75.391629639.8191.28194.27.391594639.8191.28194.28.391676632.9191.28194.27.391594655.2191.03194.68.388945655.2191.03193.67.388106659.7190.99193.68.388945655.2191.03193.64.388945655.2191.03193.66.388945655.2191.03193.66.388945655.2190.99193.67.388106659.7190.99193.68<

### C = C44 , MODE 15 5 E110J POL . [001]

LENGTH (298) = .3068 INCHES . DENSITY(298) = 4.2820 GM/CC

TEMPERATURE	FREQUENCY	MODULUS,C	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
$295 \cdot 2$ $318 \cdot 9$ $330 \cdot 0$ $344 \cdot 0$ $353 \cdot 7$ $370 \cdot 4$ $386 \cdot 7$ $404 \cdot 7$ $405 \cdot 4$ $421 \cdot 1$ $421 \cdot 1$ $421 \cdot 1$ $422 \cdot 8$ $432 \cdot 8$ $432 \cdot 8$ $449 \cdot 5$ $449 \cdot 5$ $4463 \cdot 3$ $485 \cdot 3$ $4866 \cdot 7$	175.25 174.66 174.63 174.03 173.78 173.78 172.95 172.95 172.97 172.02 171.80 171.80 171.80 171.39 171.39 171.39 171.03 171.03 171.03 171.03	<pre>. 319462 .317179 .316117 .314789 .313855 .312292 .310630 .308981 .308981 .307446 .307447 .307152 .306321 .306321 .304769 .3047704 .303432 .303472 .303413 .301267 .301172</pre>	$511 \cdot 0$ $512 \cdot 7$ $534 \cdot 1$ $535 \cdot 3$ $552 \cdot 0$ $553 \cdot 9$ $580 \cdot 7$ $590 \cdot 4$ $592 \cdot 1$ $610 \cdot 3$ $611 \cdot 4$ $623 \cdot 9$ $633 \cdot 7$ $643 \cdot 7$ $647 \cdot 3$ $655 \cdot 1$ $656 \cdot 6$ $659 \cdot 9$ $664 \cdot 3$	$169 \cdot 78$ $169 \cdot 75$ $169 \cdot 17$ $169 \cdot 15$ $168 \cdot 71$ $168 \cdot 66$ $167 \cdot 94$ $167 \cdot 67$ $167 \cdot 15$ $167 \cdot 15$ $166 \cdot 62$ $166 \cdot 52$ $166 \cdot 14$ $165 \cdot 89$ $165 \cdot 81$ $165 \cdot 68$	<ul> <li>298731</li> <li>298580</li> <li>296442</li> <li>296338</li> <li>294683</li> <li>294509</li> <li>291848</li> <li>291848</li> <li>29184005</li> <li>290671</li> <li>288864</li> <li>287479</li> <li>286880</li> <li>286487</li> <li>285416</li> <li>285416</li> <li>285416</li> <li>2844141</li> <li>283829</li> <li>283363</li> </ul>

# C = (C11+C12+2C44)/2 , MODE IS P [110]

# LENGTH (298) = .3068 INCHES : DENSITY(298) = 4.2820 GM/CC

	EREQUENCY.	MODULUS	TEMPERATURE	FREQUENCY	MODULUS,C
TEMPERATURE	FREQUENCE	HODOLODIC	IDECREES KI	(KHZ)	(MBAR)
(DEGREES K)	(KHZ)	(MBAR)	IDEGREES NI		
293.8 293.8 293.8 307.0 317.8 334.7 342.8 346.7 359.7 375.3 375.3 375.7 388.6 413.5 413.6 423.3 447.5 452.7 468.4	335 • C 3 335 • C 3 335 • C 3 334 • 55 334 • 16 333 • 51 333 • 51 333 • 51 333 • 51 333 • 21 333 • C 6 332 • 56 331 • 97 331 • 96 331 • 47 330 • 49 330 • 49 330 • 10 329 • 20 328 • 99 328 • 31	$1 \cdot 167598$ $1 \cdot 167598$ $1 \cdot 167598$ $1 \cdot 163980$ $1 \cdot 161072$ $1 \cdot 156287$ $1 \cdot 154025$ $1 \cdot 154025$ $1 \cdot 152915$ $1 \cdot 144889$ $1 \cdot 144889$ $1 \cdot 144778$ $1 \cdot 144778$ $1 \cdot 144125$ $1 \cdot 13982$ $1 \cdot 133911$ $1 \cdot 131116$ $1 \cdot 124439$ $1 \cdot 122933$ $1 \cdot 117935$	503 • 1 505 • 2 532 • 0 548 • 9 565 • 4 571 • 6 587 • 3 603 • 3 629 • 9 6440 • 9 6440 • 9 651 • 9 651 • 9 657 • 1 660 • 4 665 • 0 669 • 2 671 • 6 672 • 6 673 • 6	$326 \cdot 92$ $326 \cdot 83$ $325 \cdot 72$ $325 \cdot 03$ $324 \cdot 05$ $323 \cdot 44$ $322 \cdot 70$ $321 \cdot 57$ $321 \cdot 57$ $320 \cdot 62$ $320 \cdot 26$ $320 \cdot 26$ $320 \cdot 26$ $319 \cdot 87$ $319 \cdot 76$ $319 \cdot 67$	$1 \cdot 107734$ $1 \cdot 107111$ $1 \cdot 098946$ $1 \cdot 093916$ $1 \cdot 088993$ $1 \cdot 086718$ $1 \cdot 086718$ $1 \cdot 076822$ $1 \cdot 068520$ $1 \cdot 068520$ $1 \cdot 0685064$ $1 \cdot 0645064$ $1 \cdot 0645064$ $1 \cdot 056883$ $1 \cdot 057411$ $1 \cdot 055985$ $1 \cdot 0554584$
401 0	227.58	1.1125/6			


#### RAW DATA FOR BARIUM FLUORIDE

# C = (C11-C12)/2 , MODE IS S [110] POL. [1-10]

LENGTH (298) = .3131 INCHES , DENSITY(298) = 4.8870 GM/CC

TEMPERATURE	FREQUENCY	MODULUS,C	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
$296 \cdot 5$ $296 \cdot 3$ $311 \cdot 5$ $329 \cdot 3$ $341 \cdot 2$ $346 \cdot C$ $360 \cdot 3$ $360 \cdot 3$ $366 \cdot C$ $381 \cdot 2$ $382 \cdot 1$ $394 \cdot 9$ $410 \cdot 6$ $445 \cdot 1$ $460 \cdot 8$ $473 \cdot 8$ $502 \cdot 5$ $519 \cdot 1$ $533 \cdot 5$ $541 \cdot C$ $562 \cdot 8$ $575 \cdot 5$	$1 4 2 \cdot 9 2$ $1 4 2 \cdot 9 2$ $1 4 2 \cdot 7 7$ $1 4 2 \cdot 6 7$ $1 4 2 \cdot 6 0$ $1 4 2 \cdot 4 0$ $1 4 2 \cdot 4 4$ $1 4 2 \cdot 3 0$ $1 4 2 \cdot 2 5$ $1 4 2 \cdot 5 0$ $1 4 0 \cdot 6 6$ $1 4 0 \cdot 6 6$ $1 4 0 \cdot 4 2$ $1 4 0 \cdot 17$ $1 4 0 \cdot 0 2$	252525 252526 251953 251527 251251 250782 250597 25026 249793 249793 249150 248621 248008 247594 246551 245889 2455889 2455889 245330 244080 243340 2242692 242292 242357 2241373 2240769	$581 \cdot 5$ $586 \cdot 5$ $590 \cdot 0$ $595 \cdot 8$ $599 \cdot 2$ $600 \cdot 3$ $604 \cdot 1$ $605 \cdot 0$ $607 \cdot 2$ $611 \cdot 3$ $617 \cdot 0$ $618 \cdot 1$ $620 \cdot 2$ $633 \cdot 2$ $633 \cdot 2$ $633 \cdot 2$ $633 \cdot 2$ $643 \cdot 3$ $6448 \cdot 5$ $6455 \cdot 2$ $655 \cdot 2$ $655 \cdot 3$ $658 \cdot 7$ $663 \cdot 1$	$139 \cdot 96$ $139 \cdot 92$ $139 \cdot 88$ $139 \cdot 79$ $139 \cdot 79$ $139 \cdot 70$ $139 \cdot 70$ $139 \cdot 60$ $139 \cdot 61$ $139 \cdot 61$ $139 \cdot 50$ $139 \cdot 50$ $139 \cdot 31$ $139 \cdot 27$ $139 \cdot 16$ $139 \cdot 05$ $139 \cdot 03$ $139 \cdot 03$ $138 \cdot 97$	<ul> <li>240495</li> <li>240314</li> <li>240178</li> <li>239828</li> <li>239667</li> <li>239625</li> <li>239460</li> <li>239403</li> <li>239284</li> <li>239284</li> <li>239284</li> <li>238845</li> <li>238786</li> <li>238786</li> <li>238786</li> <li>238786</li> <li>238786</li> <li>237728</li> <li>237542</li> <li>237542</li> <li>237290</li> <li>236925</li> <li>236754</li> <li>236754</li> <li>236754</li> <li>236754</li> <li>236754</li> <li>236754</li> <li>236533</li> </ul>
575.5	140.02	.240769	663 • 1	138.97	• 2 3

### RAW DATA FOR BARIUM FLUORIDE

# C = C44 , MODE IS S E116J POL. E0013

# LENGTH (298) = .3131 INCHES , DENSITY(298) = 4.8870 GM/CC

TEMPERATURE	FREQUENCY	MODULUS, C	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
298.7	144.06	.256585	534.2	139.18	• 238166
298.7	144.07	.256594	541.1	139.02	.236441
321.3	143.85	255780	565.7	138.50	.235620
327.3	143.59	.254780	580.9	138 • 17	.234379
329.5	143.46	.254271	594.3	137.86	• 233253
341 • 1	143.22	.253376	600 • 3	137.73	.232632
347 • 1	143.09	.2528/5	607.2	137.58	.232218
367.5	142.68	.251332	611.3	137.49	.231869
371.1	142.59	.250995	616.7	137.36	• 23142/
380.3	142.42	.250327	618 • 7	13/ . 32	.230892
-00.3	142.00	247998	628.3	137.11	.230487
411.7	141.76	.247841	634.7	136.96	.229946
420.3	141.59	.247197	636.3	136.93	• 2 2 9 8 2 5
433.1	141.33	.246188	640.9	136.83	.229312
436.4	141.25	245924	644.6	136.74	.229137
461.3	140.74	.243993	649.3	136.64	.228751
480.5	140.33	.242438	651.9	136.58	• 228532
495 • 2	140.01	.241267	653.6	136.54	. 228359
511.7	139.89	.240790	655 • 1	136.50	.228266

#### RAW DATA FOR BARIUM FLUORIDE

#### C = (Ci1+C12+2C44)/2 , MODE IS P [110]

#### LENGTH (298) = .3131 INCHES . DENSITY(298) = 4.8870 GM/CC

TEMPERATURE	FREQUENCY	MODULUS, C	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
296.3 296.3 309.2 320.5 331.9 346.1 355.9 375.7 397.1 423.1 423.1 423.0 436.1 440.1 440.1	273.60 273.65 273.16 272.77 272.35 271.84 271.53 271.26 270.81 270.06 270.61 270.06 269.13 269.14 268.67 268.53 267.79	• 925514 • 925514 • 922295 • 919447 • 916430 • 912689 • 910388 • 908430 • 905192 • 899747 • 899747 • 893080 • 889716 • 888669 • 8883364 • 883322	477.5 478.0 493.2 539.4 559.6 576.2 593.2 601.4 609.9 620.3 632.8 640.0 642.5 651.9 651.9	$267 \cdot 19$ $267 \cdot 17$ $266 \cdot 60$ $264 \cdot 89$ $264 \cdot 84$ $264 \cdot 24$ $263 \cdot 53$ $262 \cdot 85$ $262 \cdot 21$ $261 \cdot 81$ $261 \cdot 31$ $261 \cdot 05$ $260 \cdot 94$ $260 \cdot 58$ $260 \cdot 53$	<ul> <li>878966</li> <li>87856</li> <li>874798</li> <li>862509</li> <li>862434</li> <li>857901</li> <li>852788</li> <li>848004</li> <li>845704</li> <li>843429</li> <li>840561</li> <li>837065</li> <li>835214</li> <li>834477</li> <li>831931</li> <li>831580</li> </ul>



## C = CII , MODE IS P EIOD]

# LENGTH (298) = .2727 INCHES , DENSITY(298) = 3.1770 GM/CC

TEMPERATURE	FREQUENCY	MODULUS, C	TEMPERATURE	FREQUENCY	MODULUS.C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
297.0 297.2 309.3 310.8 326.0 326.0 342.7 358.1 358.1 358.1 370.9 371.6	480.56 480.55 480.24 480.20 479.76 479.72 479.47 479.22 478.74 478.65 478.33 478.31	$1 \cdot 408040$ $1 \cdot 408006$ $1 \cdot 405960$ $1 \cdot 405664$ $1 \cdot 402520$ $1 \cdot 402520$ $1 \cdot 400878$ $1 \cdot 399213$ $1 \cdot 39551$ $1 \cdot 395551$ $1 \cdot 393300$	479.9 496.8 498.7 508.1 518.1 530.5 535.4 543.5 552.0 570.1 578.9 583.3	474 • 60 473 • 99 473 • 92 473 • 61 473 • 22 472 • 80 472 • 60 472 • 30 472 • 00 472 • 00 472 • 00 472 • 00	1 • 369378 1 • 365472 1 • 365024 1 • 362993 1 • 360546 1 • 357815 1 • 354641 1 • 354641 1 • 354641 1 • 354671 1 • 345790 1 • 345790
385•7 391•7 395•7	477 • 81 477 • 54 477 • 47	1 • 3 9 0 0 7 7 1 • 3 8 8 4 0 2 1 • 3 8 7 8 7 7	587•8 599•7 603•3	470 • 55 470 • 10 469 • 95	1 • 3 4 3 5 7 9 1 • 3 4 0 7 2 8 1 • 3 3 9 7 8 6
408.0 444.4 445.9	477•13 477•03 475•90 475•87	1 • 385685 1 • 385075 1 • 377645	608 • 3 618 • 6 620 • 7	469 • 77 469 • 29 469 • 19	1 • 3 3 8 6 4 1 1 • 3 3 5 6 6 0 1 • 3 3 5 0 6 9
446 • 8 448 • 5 469 • 2 474 • 5 479 • 1	475 • 83 475 • 77 474 • 96 474 • 79	1 • 377243 1 • 376828 1 • 371673 1 • 370599	632 • 1 632 • 8 642 • 3 643 • 5	468,99 468,62 468,53 468,22 468,17	1 • 3 3 3 8 6 9 1 • 3 3 1 5 5 4 1 • 3 3 0 9 7 8 1 • 3 2 9 0 3 7 1 • 3 2 8 7 2 4

# C = C66 , MODE IS 5 [100] POL. [010]

# LENGTH (298) . 2727 INCHES , DENSITY(298) . 3.1770 GM/CC

TEMPERATURE	FREQUENCY	MODULUS, C	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
297.0 297.0 297.2 312.2 318.1 325.7 339.3 365.3 380.5 392.8 414.0 414.0	$396 \cdot 24$ $396 \cdot 24$ $395 \cdot 45$ $395 \cdot 12$ $394 \cdot 72$ $393 \cdot 26$ $392 \cdot 60$ $392 \cdot 60$ $391 \cdot 62$ $389 \cdot 83$ $389 \cdot 83$	• 957318 • 957318 • 957315 • 953259 • 951559 • 945669 • 945669 • 945669 • 945669 • 933886 • 930892 • 924895 • 924895	448.0 448.0 451.0 451.0 500.2 524.1 533.0 548.0 554.8 569.0 580.2 597.6	387 • 89 387 • 89 387 • 69 387 • 13 386 • 07 384 • 84 383 • 46 382 • 91 382 • 06 381 • 67 380 • 94 380 • 19 379 • 18	• 915180 • 915156 • 914214 • 914399 • 906144 • 90058 • 893251 • 890554 • 886352 • 8864462 • 880886 • 877203 • 872302
435.3	388.56	.918559	629.9	377.26	.863015

# C = C44 , MODE IS S [100] POL. [001]

# LENGTH (298) = .2727 INCHES , DENSITY(298) = 3.1770 GH/CC

TEMPERATURE	FREQUENCY	MODULUS, C	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
295 • 3 295 • 3 306 • 4 309 • 7 322 • 1 329 • 3 339 • 6	304.98 304.99 304.81 304.75 304.54 304.42 304.24	• 567130 • 567149 • 566402 • 566151 • 565263 • 564755 • 564015	3 4 5 * 3 3 5 3 * 0 3 6 1 * 0 3 6 6 * 4 3 6 9 * 0 3 7 1 * 0 3 7 1 * 7	304 • 14 303 • 86 303 • 76 303 • 71 303 • 67 303 • 67	• 563576 • 563008 • 562400 • 561964 • 561774 • 561627 • 561584

## C = (C11+C12+2C66)/2 , MODE 15 P E1103

#### LENGTH (298) = .2456 INCHES , DENSITY(298) = 3.1780 GM/CC

TEMPERATURE	FREQUENCY	MODULUS, C	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
298.0 298.0 308.2 312.7 314.0 326.4 333.6	653.92 653.93 653.25 652.93 652.82 651.93 651.46	2 • 1 1 5 3 7 7 2 • 1 1 5 4 4 2 2 • 1 1 0 7 8 0 2 • 1 0 8 5 6 8 2 • 1 0 7 7 8 3 2 • 1 0 1 6 0 6 2 • 0 9 8 3 4 3	335 • 6 349 • 0 355 • 1 357 • 9 373 • 5 373 • 5	651•32 650•36 649•93 649•72 648•57 648•57	2 • 0 9 7 4 0 B 2 • 0 9 0 7 9 3 2 • 0 8 7 8 2 9 2 • 0 8 7 8 2 9 2 • 0 7 8 4 9 7 2 • 0 7 8 5 2 9

# C = (C11-C12)/2, MODE IS S [110] POL. [1-10]

# LENGTH (298) = .2456 INCHES , DENSITY(298) = 3.1780 GM/CC

TEMPERATURE	FREQUENCY	MODULUS, C	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
295 • 5 294 • 9 328 • 9 336 • 1 340 • 6 347 • 7 362 • 6 368 • 1 384 • 6 398 • 0 410 • 6 425 • 4 433 • 6 448 • 0	226.64 226.64 226.69 226.70 226.71 226.72 226.73 226.73 226.75 226.75 226.75 226.75 226.77 226.77 226.76 226.76 226.76	254108 254123 254122 254122 254122 254116 254109 254115 254078 254078 254023 254023 254023 254002 253850 253844 253844 253762	471.9 485.2 500.9 512.0 534.8 541.5 560.9 563.8 586.0 591.0 599.7 603.1 614.5 624.3 637.0	226 • 7 4 226 • 7 2 226 • 69 226 • 68 226 • 64 226 • 62 226 • 58 226 • 58 226 • 57 226 • 50 226 • 48 226 • 48 226 • 43 226 • 41 226 • 36 226 • 36	.253616 .253515 .253403 .253322 .253060 .252885 .252885 .252885 .252595 .252595 .252595 .252595 .2522422 .252374 .252255 .252122 .251275 .251795

# C = C44 , MODE IS S CIIDJ POL. COOIJ

# LENGTH (298) = .2456 INCHES . DENSITY(298) = 3.1780 GH/CC

TEMPERATURE	FREQUENCY	MODULUS, C	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
294 • 8 295 • 0 294 • 8 306 • 4 309 • 5 320 • 7 322 • 6 331 • 0 337 • 2	338 • 83 338 • 83 338 • 83 338 • 64 338 • 58 338 • 37 338 • 37 338 • 33 338 • 18 338 • 18	• 567993 • 567991 • 567993 • 567239 • 567211 • 566227 • 566060 • 565485 • 565029	344.7 353.3 356.4 367.6 370.6 377.1 383.3 389.0 393.6	337.92 337.75 337.68 337.46 337.40 337.26 337.13 337.01 336.92	564479     563852     563590     562530     562022     561083     560742

#### C = C33 , MODE IS P [001]

# LENGTH (298) = +2794 INCHES , DENSITY(298) = 3+1780 GM/CC

TEMPERATURE	FREQUENCY	MODULUS,C	TEMPERATURE	FREQUENCY	MODULUS,C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
294.4	544.29	2.053108	514.3	556 • 62	1.980155
305.2	545.89	2.050052	515.6	556.53	1.9/945/
313.3	545.53	2.047324	527 • 4	556.00	1.9/5483
321.3	565.22	2.045033	529.8	555.87	1.974588
323.3	565.22	2.041054	538.4	555 • 32	1.9/0531
333+3	507.70	2.037858	541.1	555 • 18	1.969490
343.7	564.20	2.037221	562.7	554.17	1.961877
345.4	507.17	2.034744	562.7	554.18	1.961947
352.6	563.07	2 030436	571.1	553.72	1.958612
365.3	563.32	2.030533	592.9	552.82	1.951785
365.6	563.31	2.030525	599.0	552.42	1.948885
380.0	562.07	2 025071	602.3	552.26	1.947696
381.1	562.64	2.023407	617.3	551.51	1.942168
391.4	562.21	2.022195	624.1	551.16	1.939543
405 • 8	561.54	2.01/184	425.4	551.10	1.939061
406.4	561.51	2.010957	125.9	551.08	1.938948
419.0	560.93	2.012519	025.0	551.00	1.934847
420.0	560.89	2.012215	030.4	550.55	1.934629
435.6	560.21	2.007120	636.8	550.32	1.933376
436 • 1	560 • 18	2.006897	639.9	550.32	1.933374
436 • 4	560 • 17	2.006785	870.0	550 52	1.929777
442 • 1	559.93	2.00500/	652.0	547.05	1.929411
455.5	559.33	2.000491	652.8	547.79	1.979796
456 . 9	559.26	1.999966	653.3	5470/8	1.928518
476.5	558.36	1.993205	655.5	547.08	1.928405
477.8	558.29	1.992684	655 • 9	549.00	027507
489.9	557.60	1.987520	657 • 8	547.55	1.925130
492.0	557.49	1.986700	664.0	549.21	1.024463
506.8	556.78	1.981424	665 • 9	549.12	1.023534
509.8	556.63	1.980305	668 • 7	549.00	1.723334

### C = C44 , MODE IS S EDDIJ RANDOM POL.

### LENGTH (298) = .2794 INCHES , DENSITY(298) = 3.1780 GM/CC

TEMPERATURE	FREQUENCY	MODULUSIC	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
301.7	207.56	566831	472.3	294.17	.553249
300.5	297.57	544994	484.1	293.91	.552235
296.6	297.64	567176	500.5	293.54	.550787
296.6	297.64	567176	500.9	293.53	.550747
309.0	207.44	544344	516.9	293.21	.549433
311.4	207.37	544105	517.2	293.19	-549356
317.0	297.37	545403	531.9	292.95	548049
317.2	297.27	646403	549.2	272005	-546543
325.0	297.27	. 505883	547.2	272.17	546106
325.0	297.10		534.5	272.37	C 4 4 4 2 4
335+3	296.92		570 . 7	271.77	544036
330.3	296.91	. 50 7 2 3 7	5/6.7	271.04	
34/•3	296.70	. 563387	580.2	291.76	
358.1	296.49	. 562565	572.4	291.49	.542052
358.3	296.49	.562545	596.0	291.40	.542299
371.4	296.23	.561502	599.2	291.33	.542004
383.9	295.99	.560520	609 • 6	291.06	• 5 4 0 9 8 3
400.3	295.65	.559198	616.4	290.90	.540335
400.5	295.65	.559160	620 • 7	290.81	.539960
415 • 3	295.35	.557978	632.2	290.56	•538991
415.8	295.33	.557919	635 • 0	290.49	.538699
434.0	294.96	.556421	640.3	290.36	.538207
434.4	294.96	.556400	643.0	290 . 28	.537915
448.8	294.67	.555241	644.8	290.25	.537776
450.5	294.63	.555101	648.2	290.17	.537462
467.5	294.26	.553610	654 • 1	290.02	.536875
467.3	294.27	.553668	656 • 8	289.95	.536602

#### C = [C11+C12+2C44+SQRT[(C11-C33)++2+4+((C13+C44)++2)]]/4

#### MODE IS P E45 DEGREES TO COOLJ AND CIOOJ J

#### LENGTH (298) = .2752 INCHES , DENSITY(298) = 3.1770 GM/CC

TEMPERATURE	FREQUENCY	MODULUS,C	TEMPERATURE	FREQUENCY	MODULUS.C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
295 • 8 295 • 8 307 • 3 309 • 5 317 • 8 328 • 9 337 • 4 350 • 6 362 • 3 375 • 0 5 6 0 • 5 400 • 4 413 • 9 421 • 1 436 • 0 440 • 1 453 • 1	534 • C8 534 • C8 533 • 69 533 • 69 533 • 35 532 • 96 532 • 21 531 • 79 531 • 31 531 • 31 530 • 32 529 • 76 529 • 76 528 • 93 528 • 81 528 • 34	$1 \cdot 771197$ $1 \cdot 771197$ $1 \cdot 768383$ $1 \cdot 765987$ $1 \cdot 765987$ $1 \cdot 765987$ $1 \cdot 763116$ $1 \cdot 750717$ $1 \cdot 757717$ $1 \cdot 751244$ $1 \cdot 751244$ $1 \cdot 749581$ $1 \cdot 749581$ $1 \cdot 749581$ $1 \cdot 749297$ $1 \cdot 740297$ $1 \cdot 738043$ $1 \cdot 734347$ $1 \cdot 733440$ $1 \cdot 7304114$	489.0 507.5 512.4 515.8 539.9 549.6 571.6 588.4 588.7 598.7 604.5 616.2 620.4 625.1 647.9 650.3 3653.3	526 • 90 526 • 22 526 • 04 525 • 89 524 • 91 524 • 50 523 • 62 522 • 93 522 • 93 522 • 25 522 • 53 522 • 25 521 • 71 521 • 52 520 • 38 520 • 27 520 • 13	1 • 7 1 9 9 5 2 1 • 7 1 5 0 7 8 1 • 7 1 3 7 6 4 1 • 7 1 3 7 6 4 1 • 7 1 3 7 6 4 1 • 7 0 5 8 3 1 1 • 7 0 5 8 3 1 1 • 6 9 6 7 7 7 1 • 6 9 1 8 2 3 1 • 6 8 9 0 3 9 1 • 6 8 7 1 2 8 1 • 6 8 7 1 2 8 1 • 6 8 2 0 4 9 1 • 6 7 3 3 0 2 1 • 6 7 2 3 3 1 1 • 6 7 1 0 6 1 • 6 7 3 0 0 2 1 • 6 7 2 3 3 1 1 • 6 7 1 0 6 1 • 6 7 3 0 0 2 1 • 6 7 2 3 3 1 1 • 6 7 1 0 6 1 • 6 7 3 0 0 2 1 • 6 7 2 3 3 1 1 • 6 7 1 0 6 1 • 6 0

# C = LC11+C12+2C44-SQRTE(C11-C33)++2+4+((C13+C44)++2)]/4

# MODE IS S C45 DEGREES TO COOLD AND CLODE D

## LENGTH (298) = .2752 INCHES . DENSITY(298) = 3.1770 GM/CC

TEMPERATURE	FREQUENCY	MODULUS,C	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
295.7 295.5 311.4 317.7 338.6 338.4 348.4	291.25 291.24 290.88 290.72 290.22 290.22 290.22 289.99	• 526728 • 526711 • 525298 • 524665 • 522755 • 522756 • 521867	353•1 357•4 360•7 366•7 372•1 374•0	289.87 289.76 289.67 289.49 289.35 289.31	•521407 •520985 •520860 •519958 •519440 •519249

# C = EC44+C66J/2, MODE IS S E45 DEGREES TO E0013 AND E1003 POL. E0103

LENGTH (298) = .2752 INCHES . DENSITY(298) = 3.1770 GM/CC

TENRICATION	EREQUENCY	MODULUS	TEMPERATURE	FREQUENCY	MODULUS, C
(DEGREES K)	(KHZ)	(MBAR)	(DEGREES K)	(KHZ)	(MBAR)
296.2 296.0 311.9 312.8 327.2 327.2 327.5	350.76 350.76 350.18 350.15 349.60 349.59 349.58	• 7 6 3 9 6 3 • 7 6 3 9 6 5 • 7 6 1 3 0 4 • 7 6 1 1 6 6 • 7 5 8 6 5 2 • 7 5 8 6 0 9 • 7 5 8 5 8 5	335 • 9 344 • 1 354 • 3 363 • 9 368 • 3 372 • 9 373 • 3	349 • 27 348 • 95 348 • 56 348 • 20 348 • 01 347 • 83 347 • 81	• 757145 • 755687 • 753910 • 75269 • 751469 • 751469 • 750613 • 750502

KMgF<sub>3</sub>

## KAW DATA FOR POTASSIUM MAGNESIUM FLUORIDE

### C = (C11-C12)/2 , MODE IS S [110] POL. [1-10]

LENGTH (298)	= .1937 INCHES	• DENSITY(298) = 3.151	GM/CC
TEMPERATURE	FREQUENCY	TEMPERATURE	FREQUENCY
(DEGREES K)	(KHZ)	(DEGREES K)	(KHZ)
294.0 294.0 303.3 312.5 320.4 323.1 332.1 343.7 354.6 356.7 368.4 373.4 385.7 386.9 390.1 401.5 405.6 419.1 422.5	$393 \cdot 66$ $392 \cdot 82$ $391 \cdot 90$ $391 \cdot 10$ $390 \cdot 87$ $389 \cdot 97$ $387 \cdot 53$ $387 \cdot 53$ $385 \cdot 94$ $385 \cdot 94$ $384 \cdot 81$ $384 \cdot 63$ $383 \cdot 24$ $383 \cdot 23$ $386 \cdot 153$ $381 \cdot 17$	423.3 425.9 434.7 439.0 448.6 451.8 460.8 460.8 460.8 475.0 478.0 478.0 478.5 491.6 495.4 498.7 511.6 518.8 539.7 543.0	$3 \ 6 \ 1 \cdot 1 \ 3 \\ 3 \ 6 \ 0 \cdot 8 \ 8 \\ 3 \ 8 \ 0 \cdot 0 \ 1 \\ 3 \ 7 \ 0 \cdot 6 \ 4 \\ 3 \ 7 \ 0 \cdot 6 \ 3 \\ 7 \ 8 \cdot 4 \ 4 \\ 3 \ 7 \ 7 \ 0 \cdot 5 \ 3 \\ 3 \ 7 \ 7 \ 0 \cdot 5 \ 3 \\ 3 \ 7 \ 7 \ 0 \cdot 5 \ 3 \\ 3 \ 7 \ 6 \ \cdot 1 \ 6 \\ 3 \ 7 \ 5 \ \cdot 5 \ 3 \\ 3 \ 7 \ 6 \ \cdot 1 \ 6 \\ 3 \ 7 \ 5 \ \cdot 6 \ 0 \\ 3 \ 7 \ 4 \ 4 \ 9 \\ 3 \ 7 \ 4 \ 4 \ 9 \\ 3 \ 7 \ 4 \ 4 \ 9 \\ 3 \ 7 \ 4 \ 4 \ 1 \ 1 \\ 3 \ 7 \ 2 \ 5 \ 2 \\ 3 \ 7 \ 1 \ 7 \ 8 \ 8 \ 1 \\ 3 \ 7 \ 2 \ 5 \ 2 \\ 3 \ 7 \ 1 \ 7 \ 7 \ 8 \ 8 \ 1 \\ 3 \ 6 \ 9 \ \cdot 8 \ 3 \\ 3 \ 6 \ 9 \ \cdot 4 \ 0 \\ 3 \ 6 \ 9 \ \cdot 4 \ 0 \\ $

#### RAW DATA FOR POTASSIUM MAGNESIUM FLUORIDE

### C = C44 , MODE IS S L1103 POL. L0013

LENGTH (298)	• .1937 INCHES	, DENSITY(298) = 3.151	GM/CC
TEMPERATURE	FREQUENCY	TEMPERATURE	FREQUENCY
(DEGREES K)	(KHZ)	(DEGREES K)	(KHZ)
294.3 294.3 302.2 319.0 326.4 336.6 345.6 357.9 361.4 370.9 373.4 376.1 381.2 398.4 400.9 411.9 425.3 429.8 435.6	$\begin{array}{c} 404.95\\ 404.97\\ 404.81\\ 404.33\\ 404.16\\ 403.78\\ 403.53\\ 403.27\\ 403.27\\ 403.15\\ 402.84\\ 402.84\\ 402.84\\ 402.84\\ 402.84\\ 402.19\\ 402.19\\ 402.19\\ 401.33\\ 401.49\\ 401.33\\ 401.35\end{array}$	467.8 468.3 478.2 481.0 484.9 494.2 498.3 499.5 513.7 521.1 531.2 533.0 543.5 551.2 552.9 555.0	$400 \cdot 39$ $400 \cdot 37$ $400 \cdot 04$ $399 \cdot 92$ $399 \cdot 53$ $399 \cdot 54$ $399 \cdot 54$ $399 \cdot 12$ $398 \cdot 63$ $398 \cdot 63$ $398 \cdot 58$ $398 \cdot 26$ $398 \cdot 09$ $398 \cdot 97$ $398 \cdot 97$ $397 \cdot 97$ 397
440.0 440.5 443.4 450.9 456.6	401 • 12 401 • 11 400 • 96 400 • 84 400 • 84	563•3 565•6 571•9 578•2 578•2	397.77 397.72 397.52 397.33
456.9 459.8 460.2	400.69 400.60 400.58	589.2 597.4	397.01 396.79

#### RAW DATA FOR POTASSIUM MAGNESIUM FLUORIDE

C = (C11+C12+2C44)/2 , MODE 15 P [110]

LENGTH (298) = .1937 INCHES , DENSITY(298) = 3.151 GM/CC TEMPERATURE FREQUENCY FREQUENCY TEMPERATURE (DEGREES K) (KHZ) (DEGREES K) (KHZ) 670.17 444.8 298.0 680.66 448.0 670.00 679.84 308.6 669.59 312.6 679.60 454.0 473.0 679.14 666.05 667.74 478.6 327 . 3 678.64 497.7 666.37 678.22 332.6 666.28 500.1 677.55 343.0 676.98 665.25 350.3 516.3 521.6 665.01 350.7 352.9 676.78 534.4 664.16 539.7 663.78 676.25 362.7 662.82 675.59 555.4 372.3 675.60 558.1 662.55 372.7 662.41 563.0 382.0 674.98 660.19 391.4 674.00 593.6 659.58 672.92 601.4 407.6 659.37 428.5 603.1 671.53

620.5

624.8

658.11 657.84

671.44

670.95

435.3

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#### ERRATA

Page 5, line 18	"behavior" should be "behaviour".
Page 9, line 14	"viscocity" should be "viscosity"
Table 5.1, Ref. 12	"1964" should be "1965".
Ref. 25	"1967" should be "1957".
Table 5.8	"d" should be "d $_{\circ}$ ".

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# ELASTIC AND THERMAL PROPERTIES OF FLUORIDE AND OXIDE ANALOGUES IN THE ROCKSALT, FLUORITE, RUTILE AND PEROVSKITE STRUCTURES

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(Submitted for publication March 19, 1974; accepted May 31, 1974)

Fluorides are considered as models for the physical properties of oxides on the basis of Goldschmidt's crystal chemical arguments. The well-established bulk modulus (K)-volume (V) relationship KV = constant is shown to hold for fluorides and oxides belonging to the four isostructural series. The bulk moduli of equivolume oxides and fluorides are scaled as  $4S^2$ , where  $S = Z^0/2Z^F$  is the ratio of the effective unit charges and is approximately 77% for all of the crystal structures. The fluorides have distinctly lower melting and Debye temperatures which offers the possibility of using these compounds as models for the high-temperature elastic behaviour of their oxide analogues.

# 1 Introduction

The concept of fluoride and oxide analogue compounds was first introduced by Goldschmidt (1927) on the basis of a number of crystal chemical considerations: (a) the similarity in ionic radii of  $O^2$  and  $F^-$ ; (b) the applicability of the rigid ion model to compounds containing the  $O^2^-$  and  $F^-$  ions, which have relatively low polarizabilities resulting in their ionic radii being almost independent of coordination number; and (c) the correspondence of the crystal structures of oxide and fluoride compounds in which the cations are also of comparable ionic radii. Notable examples of this modelling concept are LiF-MgO (rocksalt structure)  $CaF_2$ -ThO<sub>2</sub> (fluorite structure), MgF<sub>2</sub>-TiO<sub>2</sub> (rutile structure), and BeF<sub>2</sub>-SiO<sub>2</sub> ( $\alpha$ -quartz and coesite structures).

Goldschmidt (1927) also suggested that because of their lower ionic charge fluorides should be "weakened" models of their oxide analogues and thus be characterized by lower melting temperature. lower hardness and lower refractive index. Subsequent investigations by Roy et al. (1953, 1954) and Thilo and Lehmann (1949), have demonstrated close similarities in the phase diagrams of binary fluoride and oxide systems at atmospheric pressure with the fluoride systems exhibiting much lower solidus and liquidus temperatures. Recently, Jackson and Liebermann (1974) have shown that the fusion curves of rocksalt fluorides and oxides at high pressure may be correlated in a similar manner. The purpose of this paper is to examine the elastic and thermal properties of fluoride and oxide compounds crystallizing in the rocksalt, fluorite, rutile, and perovskite structures in the framework of systematics proposed by previous investigators. We also compare the melting and Debye temperatures of the model pairs to evaluate the possibility of using fluoride data to predict the high-temperature elasticity of their oxide analogues.

### 2. Data and discussion

The central feature of the entire modelling scheme is the similarity of the ionic radii of  $O^{2-}$  and  $F^{-}$  for various coordination numbers listed below (after Shannon and Prewitt, 1970).

Coordination number	Ionic radii	(Å)	
	0 <sup>2-</sup>	F <sup>-</sup>	
II	1.35	1.285	-
III	1.36	1.30	
IV	1.38	1.31	
VI	1.40	1.33	2.0

Simple fluoride and oxide compounds whose cations have comparable ionic radii and ionic charge ratios of 1/2 exhibit the same crystal structure. In addition, a number of binary compounds which obey this model-

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TABLE I Crystal structures of som	ie fluorides and	oxides
Crystal structure	Fluoride	Oxide

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er, otar stracture	ridonae	Oxide
Olivine	Na <sub>2</sub> BeF <sub>4</sub>	Ca <sub>2</sub> SiO <sub>4</sub>
Phenacite	Li2 BeF4	Zn <sub>2</sub> SiO <sub>4</sub>
Pyroxene	LiBeF <sub>3</sub>	MgSiO <sub>3</sub>
Diopside	LiNaBe <sub>2</sub> F <sub>6</sub>	CaMgSi <sub>2</sub> O <sub>6</sub>
Perovskite	KMnF <sub>3</sub>	BaTiO <sub>3</sub>
Spinel	Li <sub>2</sub> NiF <sub>4</sub>	Mg <sub>2</sub> SnO <sub>4</sub>
Strontium plumbate	Na <sub>2</sub> NiF <sub>4</sub>	Ca <sub>2</sub> SnO <sub>4</sub>

ling formula and whose crystal structures are of interest in geophysical discussions of the earth's interior are listed in Table I. Of particular interest is the close correspondence of the ionic radii of  $Be^{2+}$  and  $Si^{4+}$  (0.27Å and 0.26Å, respectively, for 4-fold coordination (Shannon and Prewitt, 1970)) which permits the fluoride oxide model system to be extended to fluoroberyllates and silicates. One disadvantage is that trivalent cations have no place in this scheme, so that it is difficult to model the corundum and garnet structures.

In Table II we list all the fluorides and oxides of the rocksalt, fluorite, rutile and perovskite structures for which elastic constant data are available. Table II also contains coordination numbers, ionic radii, densities  $(\rho)$ , molecular weights (M), molar volumes (V), and the isotropic elastic bulk (K) and shear  $(\mu)$  moduli, all determined at room temperature and atmospheric pressure.

### 2.1. Elastic properties systematics

Several previous studies have demonstrated that the relationship KV = constant holds for isostructural series of halides, oxides, sulfides, selenides, and tellurides (O.L. Anderson and Nafe, 1965; D.L. Anderson, 1967; O.L. Anderson and Soga, 1967; D.L. Anderson and O.L. Anderson, 1970; and O.L. Anderson, 1972). This behaviour is consistent with a simple Born-Mie interatomic potential with power law repulsion leading to  $KV^{4/3}$  = constant, which is indistinguishable from the empirical result. Following O.L. Anderson and Nafe (1965), we present in Fig. 1 the data of Table II as a log-log plot of bulk modulus versus molar volume per ion pair ( $V^*$  =



Fig. 1. Log-log plot of bulk modulus (K) versus molar volume per ion pair  $(2\overline{M}/\rho)$  for oxides and fluorides in the rocksalt, fluorite and rutile structures. (To avoid confusion, the perovskite structure is excluded.) The  $KV^*$  = constant lines for oxides and fluorides in the three structures are indicated by dashed lines of gradient -1. The solid line of gradient -4 represents the constant mean atomic weight relationship  $KV^{*4}$  = constant for  $\overline{M}$  = 20-21.

 $2\overline{M}/\rho = 2\overline{V}$ , where  $\overline{M}$  and  $\overline{V}$  are the mean atomic weight and volume, respectively).

Three important trends emerge from this data:

(1) The relationship  $KV^*$  = constant holds for fluorides and oxides crystallizing in the rocksalt, fluorite, rutile and perovskite structures.

(2) From the values of  $\psi = KV^*/Z_cZ_ae^2$  in Table II we observe that the isostructural lines are scaled as  $Z_cZ_a$ for the fluoride compounds and also for the oxide compounds, where  $Z_c$  and  $Z_a$  are the valence charges of the

#### PROPERTIES C

cation and ani 10%) for each crystal structu the Born-Mie sitive to coord atomic packin derson, 1970) (3) The fac oxide compou not the same effective chars of the effectiv to the fluoride the KV = ccof a given stru determined by tural group in the fluorite, C kite structure oxide is appro ogue for all th

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cation and anion. The constancy of the values (within 10%) for each set of chemical compounds in different crystal structures implies that the effective charges in the Born-Mie interatomic potential are relatively insensitive to coordination number and to the details of the atomic packing (see also D.L. Anderson and O.L. Anderson, 1970).

(3) The fact that the  $\psi$ -values for the fluoride and oxide compounds within each isostructural group are not the same may be attributable to differences in the effective charge. If  $S = Z^{O}/2Z^{F}$  is defined as the ratio of the effective unit charges of the oxides with respect to the fluorides (following O.L. Anderson, 1972), then the  $KV^*$  = constant lines for the fluorides and oxides of a given structure are scaled as  $4S^2$ . The values of S determined by comparing the  $KV^*$  lines for each structural group in Fig. 1 are 0.80 for the rocksalt, 0.78 for the fluorite, 0.74 for the rutile and 0.74 for the perovskite structures. Thus the effective unit charge of an oxide is approximately 77% of that of its fluoride analogue for all the structures considered.

It is interesting to compare our values of S with those derived from the more rigorous lattice dynamical calculations. Using a shell model, Axe (1965) and Axe and Pettit (1966) derived values of S = 0.73 for the fluorite structure (CaF2 and ThO2). Katiyar and Krishnan (1969) employed a rigid ion model and concluded that S =0.77 for the rutile structure (MgF<sub>2</sub> and TiO<sub>2</sub>). Recent determinations of the effective charges for rutile fluorides (Striefler and Barsch, 1973) and rutile oxides (M.E. Striefler and G.R. Barsch, private communication, 1974) from a least-squares fit over all the available elastic and optical data lead to values of S in the range 0.57 - 0.74.

Since the relative effective charges of the fluorides and oxides do not appear to depend on coordination number or crystal field, it should thus be possible to predict the bulk modulus of an oxide from the bulk modulus of a fluoride of the same crystal structure. In particular the bulk moduli of the corresponding fluoride-oxide pairs in the Goldschmidt modelling scheme (for which the molar volumes are comparable) are related by  $(K^{O}/K^{F}) = 4S^{2}$ . A similar idea was suggested by Haussühl (1968) in considering  $MgF_2$ -TiO<sub>2</sub> and LiF-MgO as analogue pairs.

Another aspect of bulk modulus systematics is given by O.L. Anderson and Nafe (1965) (see also O.L. Anderson and Soga, 1967) who proposed that data for

oxides and silicates of common mean atomic weight  $\overline{M}$  = 20–21 would be characterized by the relationship  $KV^{*4}$  = constant. In Fig. 1, the bulk moduli of compounds with  $\overline{M} = 20-21$  (SiO<sub>2</sub>, MgF<sub>2</sub>, MgO, NaF) are indeed scaled as the inverse fourth power of the volume; this is an important result since this group of compounds contains both oxides and fluorides of different crystal structures. For other values of  $\overline{M}$ , the  $K \sim V^{*-4}$  scaling is not as evident. However, for the rocksalt structure pairs MgO-NaF ( $\overline{M}$  = 20-21), CaO-KF ( $\overline{M}$  = 28-29), and SrO-RbF ( $\overline{M}$  = 52) this relationship holds very well as indicated in Table III; the members of each pair have comparable  $\overline{M}$  since they are composed of adjacent elements in the Periodic Table which are very close in atomic weight. This alternative modelling scheme, on the basis of common  $\overline{M}$  rather than ionic radii, is implicit in the approach of Son and Bartels (1972) who chose their pairs on the basis of the same closed shell ion core configuration.

#### 2.2. High-temperature elasticity

In presenting the concept of fluorides as "weakened" models of oxides, Goldschmidt (1927) cited the melting points of the phenacites Li2BeF4 (470°C) and Zn2SiO4 (1510°C) to illustrate the greater temperature sensitivity of the physical properties of the fluorides. We list in Table II the melting temperatures at atmospheric pressure for the compounds under consideration in this paper. The ratios of the melting points of the fluorides to those of their oxide analogues  $T_{\rm m}^{\rm F}/T_{\rm m}^{\rm O}$  are given in Table IV; with the exception of  $MgF_2$ -TiO<sub>2</sub>, this ratio is less than 0.6 for all of the analogue pairs.

In discussing the temperature dependence of the elastic properties, the Debye temperature  $\theta_{\rm D}$  is a significant parameter since Leibfried and Ludwig (1961) have shown that for  $T > \theta_{\rm D}$  the bulk modulus should decrease linearly with increasing temperature. The elastic moduli data of Table II may be used to calculate the elastic Debye temperatures from the following equation, which holds for isotropic solids (Debye, 1912):

$$\theta_{\rm D} = \frac{h}{k} \left(\frac{9\rho N}{4\pi M}\right)^{1/3} v_{\rm m}$$
  
where:  $3v_{\rm m}^{-3} = \left(\frac{2}{v^3} + \frac{1}{v^3}\right)$ 

Structure	Compound	CN	Ionic radii <sup>1,2</sup>	2 (Å)	$Z_{c}Z_{a}$	Molar	М (g)	$\rho$ (g/cm <sup>3</sup> )	Elastic m	noduli (Mbar)	$\psi^{a}$	T <sub>m</sub>	θ <sub>D</sub>	Ab
			cation(s)	anion		(cm <sup>3</sup> )		(8) **** /	K <sub>s</sub>	μ <sub>s</sub>		( <sup>°</sup> K)	( <sup>°</sup> K)	
Rocksalt	LiF	6-6	0.74	1.33	1	9.83	25.94	2.639 <sup>3</sup>	0.696 <sup>3</sup>	0.490 <sup>3</sup>	0.267	1120 <sup>31</sup>	73434	57
	NaF		1.02	1.33	1	14.98	41.99	$2.804^{3}$	$0.482^{3}$	0.3133	0.281	126932	49135	56
	KF		1.38	1.33	1	23.00	58.10	2.5264	0.3234	0.1644	0.289	$1130^{31}$	3274	50
	RbF		1.49	1.33	1	27.18	104.47	3.84345	0.2805	0.1275	0.297	$1048^{33}$	2215	48
	MgO		0.72	1.40	4	11.25	40.31	3.5836	1.6286	1.3116	0.178	312532	95536	96
	CaO		1.00	1.40	4	16.76	56.08	3.3467	1.147	0.8147	0.186	288732	670*	91
	SrO		1.13	1.40	4	20.69	103.62	5.0097	0.887	0.5917	0.177	269332	45737	90
	BaO		1.36	1.40	4	25.59	153.34	5.992 <sup>8</sup>	0.618	0.355 <sup>8</sup>	0.152	2291 <sup>32</sup>	291*	75
Fluorite	CaF <sub>2</sub>	8-4	1.12	1.31	2	24.55	78.08	3.1819	0.8419	0.4269	0.268	169132	51438	67
	SrF <sub>2</sub>		1.25	1.31	2	29.37	125.62	4.27710	$0.699^{10}$	0.34610	0.267	1673 <sup>31</sup>	$380^{10}$	66
	PbF <sub>2</sub>		1.29	1.31	2	31.47	245.19	7.7911	0.611111	0.230 <sup>11</sup>	0.250	$1097^{31}$	22111	55
	BaF <sub>2</sub>		1.42	1.31	2	35.89	175.34	4.8869	0.5849	0.2559	0.272	1593 <sup>31</sup>	282 <sup>39</sup>	62
	UO2		1.00	1.38	8	24.62	270.03	$10.97^{12}$	2.13 12	$0.874^{12}$	0.170	3151 <sup>32</sup>	394*	95
	ThO <sub>2</sub>		1.04	1.38	8	26.3813	264.04	10.01	1.93 <sup>14</sup>	$0.972^{14}$	0.165	3493 <sup>32</sup>	424*	103
Rutile	MgF <sub>2</sub>	6-3	0.72	1.30	2	19.61	62.31	3.17815	1.01515	0.546 <sup>15</sup>	0.258	1536 <sup>32</sup>	621*	67
	CoF <sub>2</sub>		0.735	1.30	2	21.11	96.93	4.59216	$0.835^{16}$	0.392 <sup>16</sup>	0.229	$1475^{31}$	428*	59
	MnF <sub>2</sub>		0.82	1.30	2	23.67	92.93	3.92615	0.88315	0.30 <sup>15</sup>	0.271	$1129^{31}$	393*	55
	SiO <sub>2</sub>		0.40	1.36	8	14.01	60.08	4.28717	3.46 <sup>17</sup>	1.29 <sup>17</sup>	0.157		930*	88
	GeO <sub>2</sub>		0.54	1.36	8	16.64	104.59	$6.286^{18}$	2.58918	1.50918	0.140		774*	102
	TiO <sub>2</sub>		0.605	1.36	8	18.80	79.90	4.2513	2.155 19	1.124 <sup>19</sup>	0.132	2103 <sup>32</sup>	782*	94
	SnO <sub>2</sub>		0.69	1.36	8	21.55	150.69	6.992 <sup>20</sup>	2.0320	$0.98^{20}$	0.142	1903 <sup>32</sup>	545*	94
Perovskite	KMgF <sub>3</sub>	12-6-6	1.60 0.72	1.33	1.5	38.23	120.41	3.15 <sup>21</sup>	0.75321	0.47121	0.299		548*	67
	KMnF <sub>3</sub>		1.60 0.82	1.33	1.5	44.16	151.04	3.4222	0.649 <sup>23</sup>	0.325 <sup>23</sup>	0.298		418*	60
	RbMnF <sub>3</sub>		1.73 0.82	1.33	1.5	45.73	197.40	4.31724	0.67524	0.34124	0.321		386 <sup>23</sup>	64
	CdTiO <sub>3</sub>		1.31 0.605	1.40	6	32.90 <sup>25</sup>	208.30	6.331	2.00 <sup>26</sup>	$0.98^{26}$	0.171		589*	90
	CdSnO <sub>3</sub>		1.31 0.69	1.40	6	36.6527	279.09	7.615	1.8926	0.87 <sup>26</sup>	0.180		489*	90
	CaSnO <sub>3</sub>		1.35 0.69	1.40	6	36.4728	206.77	5.673	1.1526	0.8526	0.109		555*	87
	SrTiO <sub>3</sub>		1.40 0.605	1.40	6	35.87	183.52	5.11629	1.744 30	1.1730	0.162		691*	102

TABLE II Summary of elastic and thermal properties of fluorides and oxides

<sup>a</sup>  $\psi = KV^*/Z_c Z_a e^2$ ;  $V^* = 2\overline{M}/\rho = 2\overline{V}$ <sup>b</sup>  $A = a\theta_D \sqrt{M}$ ;  $a = V^{1/3}$  = mean lattice parameter. <sup>\*</sup>  $\theta_D$  calculated from room temperature values of the elastic constants.

1. Shannon and Prewitt (1969) 2. Shannon and Prewitt (1970)

3. Miller and Smith (1964)

4. Marshall and Miller (1967)

21. Reshchikova (1969) 22. Beckman and Knox (1961) 23. Aleksandrov et al. (1966) 24. Melcher and Bolef (1969)

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 $\theta_{\rm D}$  calculated from room temperature values of the elastic constants.

1. Shannon and Prewitt (1969) 2. Shannon and Prewitt (1970) 3. Miller and Smith (1964) 4. Marshall and Miller (1967) 5. Cleavelin et al. (1972) 6. Spetzler (1969) 7. Son and Bartels (1972) 8. Vetter and Bartels (1973) 9. Wong and Schuele (1968) 10. Gerlich (1964b) 11. Wasilik and Wheat (1965) 12. Wachtman et al. (1965) 13. Robie et al. (1966) 14. Macedo et al. (1964) 15. Haussühl (1968) 16. Hart and Stevenson (1970) 17. Mizutani et al. (1972) 18. Wang and Simmons (1973) 19. Manghnani et al. (1972) 20. Liebermann (1973)

#### TABLE III

 $KV^{*4}$  systematics for rocksalt fluorides and oxides

Compound	$\overline{M}$	KV <sup>*4</sup>
LiF	13.0	0.06
MgO NaF	20.2 21.0	0.26 0.24
CaO KF	28.0 29.1	0.90 0.90
SrO RbF	51.8 52.2	1.61 1.53
BaO	76.7	2.62
BaO	76.7	2.62

21. Reshchikova (1969) 22. Beckman and Knox (1961) 23. Aleksandrov et al. (1966) 24. Melcher and Bolef (1969) 25. Roth (1957) 26. Liebermann (1974) 27. Smith (1960) 28. Coughanour et al. (1955) 29. Swanson et al. (1954) 30. Bell and Rupprecht (1963) 31. Wicks and Block (1963) 32. Robie and Waldbaum (1968) 33. Weast (1972) 34. Briscoe and Squire (1957) 35. Lewis et al. (1967) 36.  $\theta_{\rm D}$  calculated from elastic constants of Anderson and Andreatch (1966) 37. Johnston et al. (1970) 38. Huffman and Norwood (1960) 39. Gerlich (1964a)

#### TABLE IV

Ratios of melting  $(T_m)$  and Debye  $(\theta_D)$  temperatures for oxide-fluoride analogue pairs

Pair	$T_{\rm m}^{\rm F}/T_{\rm m}^{\rm O}$	$\theta_{\rm D}^{\rm F}/\theta_{\rm D}^{\rm O}$
LiF-MgO	0.36	0.77
NaF-CaO	0.44	0.73
KF-SrO	0.42	0.72
RbF-BaO	0.46	0.76
KF-BaO	0.49	1.12
CaF <sub>2</sub> -ThO <sub>2</sub>	0.48	1.21
$MgF_2 - TiO_2$	0.73	0.79
$MnF_2 - SnO_2$	0.59	0.72
KMgF <sub>3</sub> -SrTiO <sub>3</sub>		0.79

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(c) Their lower melting temperatures facilitate the fabrication of hot-pressed polycrystalline aggregates of the binary fluorides with crystal structures of interest to geophysics; in lieu of single crystals of these compounds, these aggregate specimens may be used for hightemperature elasticity measurements by ultrasonic techniques.

#### 3. Summary

Goldschmidt's (1927) crystal chemical modelling scheme has been employed to examine the relationship of elastic and thermal properties of fluoride and oxide compounds with the rocksalt, fluorite, rutile and perovskite structures. The bulk moduli are inversely proport tional to volume for the fluorides and oxides of each crystal structure. The approximate constancy of th relative effective charge as a scaling factor for the bulk moduli of fluorides and oxides of a particular structure offers the possibility that the elasticity of oxide compounds with other crystal structures could be predicted from the data for the corresponding fluorides. In addition, the lower elastic moduli of the fluorides may enable us to measure the second-order pressure derivatives which are difficult to obtain for the oxides even with the most sophisticated ultrasonic techniques.

The lower melting and Debye temperatures of the fluorides and fluoroberyllates support our interest in utilizing these compounds as models for the high-temperature elasticity of their oxide and silicate analogues. An ultrasonic program is currently underway in our laboratory to measure the elastic properties of LiF to high temperatures; these data will permit a detailed comparison with the MgO data of Spetzler (1969), as well as evaluation of the higher order terms in various finite strain equations of state (e.g. Thomsen, 1972; Davies, 1973).

By model studies of this type, we are endeavouring to estimate the high-temperature properties of oxides and silicates, just as others (see Ringwood (1970) for a comprehensive review) have employed germanates as high-pressure models for the physical and crystal chemical properties of their silicate analogues.

#### Acknowledgements

We thank A.E. Ringwood for suggesting that the oxide-fluoride modelling scheme of Goldschmidt might

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and h and k are Planck's and Boltzmann's constants, N is Avogadro's number, and  $v_p$  and  $v_s$  the compressional and shear wave velocitites. The values of  $v_{p}$  and  $v_{\rm c}$  have been calculated from the single crystal elastic moduli  $c_{ii}$  by the Voigt-Reuss-Hill averaging scheme; O.L. Anderson (1963) has shown that this method of calculating the elastic  $\theta_{\rm D}$  is equivalent to the more rigorous method of averaging the eigenfrequencies over all possible normal modes and directions of the crystal. Wherever possible, the Debye temperatures given in Table II have been calculated using the elastic constant data near 0°K; in the other cases, room temperature elastic data were employed so that the values of  $\theta_{\rm D}$ will be underestimated. In Table III we also list the ratios of the Debye temperatures for the corresponding fluorides and oxides. With the exception of the pairs containing BaO and ThO<sub>2</sub>, the  $\theta_{\rm D}$  of the fluorides are 65-80% of those for their oxide analogues.

Gmelin (1970) proposed a systematic relationship between the Debye temperature and certain crystallographic parameters:

# $\theta_{\rm D} = \frac{A}{a\overline{M}^{1/2}}$

where  $a = V^{*1/3}$  is a mean lattice parameter, A is an empirical constant, and  $\overline{M}$  is the mean atomic weight. In Table II we list the values of  $A = a\theta_D \overline{M}^{1/2}$  for the compounds under discussion. For each of the fluoride and oxide isostructural groups, the values of this product are approximately constant, especially for the rocksalt structure. Some of the scatter in this product for the other structures may be attributable to the necessity of using room temperature elastic constant data to calculate  $\theta_D$ . For the corresponding pairs of fluorides and oxides, the Debye temperatures should thus be related by:

# $\theta_{\mathrm{D}}^{\mathrm{F}}/\theta_{\mathrm{D}}^{\mathrm{O}} = (A^{\mathrm{F}}/A^{\mathrm{O}}) (\overline{M}^{\mathrm{O}}/\overline{M}^{\mathrm{F}})^{1/2}$

so that  $\theta_{\rm D}$  for the oxide may be predicted from  $\theta_{\rm D}$  for its fluoride analogue.

The scaling of the thermal properties of the fluoride and oxide analogues offers several distinct advantages in studying fluoride models:

(a) It is experimentally possible to measure the elastic properties of fluoride compounds to much greater fractions of their melting temperatures.

(b) Their lower Debye temperatures imply that the fluorides should exhibit the linear K vs T high-temperature behaviour at lower absolute temperatures.
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## PROPERTIES OF FLUORIDE AND OXIDE ANALOGUES

be applicable to discussions of high-temperature elasticity, and l.N.S. Jackson and A.E. Ringwood for comments on this paper. We are grateful to M.E. Striefler and G.R. Barsch for permission to use their data on the rutile oxides prior to publication.

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