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## RESEARCH

# Vertical leaping mechanics of the Lesser Egyptian Jerboa reveal specialization for maneuverability rather than elastic energy storage

Talia Y Moore<sup>1,2\*</sup>, Alberto M Rivera<sup>1</sup> and Andrew A Biewener<sup>1</sup>

## Abstract

**Background:** Numerous historical descriptions of the Lesser Egyptian jerboa, *Jaculus jaculus*, a small bipedal mammal with elongate hindlimbs, make special note of their extraordinary leaping ability. We observed jerboa locomotion in a laboratory setting and performed inverse dynamics analysis to understand how this small rodent generates such impressive leaps. We combined kinematic data from video, dynamic data from a force platform, and morphometric data from dissections to calculate the relative contributions of each hindlimb muscle and tendon to the total movement.

**Results:** Jerboas leapt in excess of 10 times their hip height. At the maximum recorded leap height (not the maximum observed leap height), peak moments for metatarso-phalangeal, ankle, knee, and hip joints were 13.1, 58.4, 65.1, and 66.9 Nmm, respectively. Muscles acting at the ankle joint contributed the most work (mean 231.6 mJ / kg Body Mass) to produce the energy of vertical leaping, while muscles acting at the metatarso-phalangeal joint produced the most stress (peak 317.1 kPa). The plantaris, digital flexors, and gastrocnemius tendons encountered peak stresses of 25.6, 19.1, and 6.0 MPa, respectively, transmitting the forces of their corresponding muscles (peak force 3.3, 2.0, and 3.8 N, respectively). Notably, we found that the mean elastic energy recovered in the primary tendons of both hindlimbs comprised on average only 4.4% of the energy of the associated leap.

**Conclusions:** The limited use of tendon elastic energy storage in the jerboa parallels the morphologically similar heteromyid kangaroo rat, *Dipodomys spectabilis*. When compared to larger saltatory kangaroos and wallabies that sustain hopping over longer periods of time, these small saltatory rodents store and recover less elastic strain energy in their tendons. The large contribution of muscle work, rather than elastic strain energy, to the vertical leap suggests that the fitness benefit of rapid acceleration for predator avoidance dominated over the need to enhance locomotor economy in the evolutionary history of jerboas.

**Keywords:** jerboa; inverse dynamics; muscle-tendon stresses; ricochetal bipedal locomotion

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## 1 **Background**

2 Jerboas are small bipedal rodents native to the deserts of northern Africa and  
3 Eurasia that use erratic hopping locomotion, often called ricochetel saltation, to  
4 navigate their arid habitat, forage for scarce resources, and escape from predators.  
5 They constantly switch between hopping, running, turning, and leaping vertically as  
6 they move on the shifting sand [1, 2]. The inherently variable locomotion of jerboas  
7 presents a challenge for biomechanical analyses commonly designed for steady-state  
8 locomotion [2, 3]. Fortunately, jerboas perform a pronounced vertical leap to escape  
9 predation that can be elicited in a laboratory setting [4]. These escape leaps enable  
10 jerboas to forage in open areas where the risk of avian predation is higher [2,  
11 5]. Vertical leaping is therefore a broadly useful behavior to examine in jerboas,  
12 since leaps to escape predators likely approach maximal performance, and leaping  
13 is relevant to jerboa survival.

14 Understanding how animals use their musculoskeletal system to generate a broad  
15 range of locomotor behaviors informs our understanding of how evolution has  
16 shaped locomotor performance. Since muscles require metabolic energy to actively  
17 contract, whereas tendons are passively elastic, determining the relative mechani-  
18 cal energy contributions of muscles and tendons to locomotor movements can help  
19 to inform predictions of locomotor endurance. Cursorial animals adapted for sus-  
20 tained and repetitive locomotion tend to have greater tendon elastic energy storage  
21 [6]; energy recovered from tendons offsets the amount of muscle work required over  
22 the course of a stride, significantly lowering cost of transport. For example, elastic  
23 energy recovery provides 40%–70% of the total center of mass (CoM) mechanical  
24 energy during sustained hopping in bipedal red kangaroos (*Macropus rufus*) [7] and  
25 36% of CoM mechanical energy during galloping in horses (*Equus ferus caballus*)  
26 [8]. Both of these animals are able to sustain high speed locomotion over long time  
27 periods because the passive energy storage in tendons decreases the need for muscle  
28 work to move the animal’s body during each step.

29 Although tendon energy storage and recovery can provide more economical loco-  
30 motion, the lengthening of compliant tendons likely slows the ability of muscles to  
31 produce limb movement. Therefore, small prey animals requiring quick accelerations  
32 to escape predator threats tend to use less tendon energy storage in their locomo-  
33 tion, allowing muscle-tendon units in their hindlimbs to shorten more quickly. For

34 example, the kangaroo rat, *Dipodomys spectabilis*, which reflexively leaps in response  
35 to the vibrations emitted by their predators [9], elastically recovers only 14% of the  
36 mechanical energy in tendons during forward hopping [10] and 21% during leaping  
37 [11]. Despite considerable phylogenetic distance between kangaroo rats and jerboas  
38 [12], the morphological and behavioral similarity between the species lead us to hy-  
39 pothesize that jerboas, as exemplified by *J. jaculus*, similar to kangaroo rats, store  
40 only a small amount of elastic energy in their tendons during vertical leaping.

41 For non-steady-state locomotion, elastic energy can be gradually stored in tendons  
42 as muscles contract and returned rapidly to amplify a muscle-tendon unit's capacity  
43 to produce power [13]. Because this mechanism requires preparation time to preload  
44 the tendons, power amplification is most often associated with isolated jumps from  
45 a stationary position. Several invertebrates use power amplification and specialized  
46 ratcheting morphology to achieve incredible leaps, up to 100x body length (summa-  
47 rized in [14]). Power amplification has also been demonstrated to enable frog leaps  
48 of up to 8x their body length [15]. However, it is unknown whether jerboas are able  
49 to use power amplification to enhance their vertical leaping performance.

50 In this study, following similar methods used to study red kangaroos [7], we used  
51 joint moment analysis based on measurements of 2D limb kinematics and ground  
52 reaction forces (GRFs) to calculate the relative contributions of jerboa hindlimb  
53 muscles and tendons to produce the energy of vertical leaping. In this study we build  
54 upon previous descriptions of jerboa hindlimb morphology [4, 16], with detailed  
55 dissections of hindlimb muscle and tendon architecture to determine the role of  
56 each hindlimb muscle-tendon element in the execution of vertical leaping.

## 57 **Methods**

### 58 **Animals**

59 We tested five *J. jaculus* (four males, one female) from the colony at the Concord  
60 Field Station that were originally captured from the wild in Egypt. Their masses  
61 ranged from 53g to 74g. More animals were tested, but were non-responsive to  
62 the stimulus and refused to leap, possibly due to lack of motivation. To estimate  
63 the morphological measurements of each subject, we dissected three other jerboas  
64 that were euthanized for other studies and assumed geometric scaling between in-  
65 dividuals. Before experimentation, we shaved the jerboas' legs and used a non-toxic

66 marker to indicate joint positions. All animal care and use protocols were approved  
67 by the Harvard Faculty of Arts and Sciences Institutional Animal Care and Use  
68 Committee (IACUC) and the United States Department of Agriculture.

## 69 Experimental Setup

70 At the start of each trial we placed the animal in a wood and plexiglas structure  
71 (103 x 15 x 15 cm) on a force platform. Data were initially collected from a 2-  
72 axis (vertical and fore-aft) custom-made (6 x 12cm) strain gauge force platform  
73 [17], which fed into a data acquisition system (BioPac MP150). Due to damage of  
74 this force platform, subsequent recordings comprising an additional dataset were  
75 collected with a rigid plate mounted on a load cell with 6 degrees of freedom (ATI  
76 Nano43). A meter stick attached to the back of the enclosure indicated the maximum  
77 height of each leap. We used quick bursts of compressed air to motivate the animals  
78 to leap. An additional file shows a representative trial (Additional file S1).

79 To film each trial, we lit the area with a 500W light (Omni Lowell) and placed two  
80 high speed cameras in front of the enclosure to film the leaps in lateral view. In the  
81 original dataset, one camera (Casio ZR100) with a wide angle lens was positioned  
82 to film the entirety of each leap at 240 fps and provided maximum leap height of  
83 each trial. The other camera (IDT NR5) equipped with a zoom lens was positioned  
84 to provide a smaller field of view that allowed detailed motion of joint positions to  
85 be determined at 250 fps during limb contact and takeoff from the force platform.  
86 In the additional trials, one camera (GoPro Hero 3+) recorded at 120 fps and  
87 provided a view of how the feet are placed on the force platform. The other camera  
88 (Photron SA3) equipped with the zoom lens recorded at 250 fps to capture both  
89 detailed motion of joint positions and maximum jump height. For this analysis, we  
90 selected only leaps in which one or both feet were in contact with only the force  
91 platform, with the animal's mediolateral body axis oriented parallel to the camera  
92 filming axis. We assumed that the animal leapt with equal force on both legs, and  
93 divided total ground reaction force in half to compute single limb forces for trials  
94 with both feet on the force platform. Positions of the joints (metatarso-phalangeal,  
95 ankle, knee, and hip), eye, and base of tail were tracked using custom tracking  
96 software (DLTdv5 Matlab program) [18].

## 97 Inverse Dynamics

98 We used an inverse dynamics approach that ignored inertial and gravitational seg-  
 99 mental moment effects to calculate the total agonist muscle force required at each  
 100 joint (from distal to proximal, using a linked-segment model) to resist the moment  
 101 produced by the ground reaction force (GRF) in each frame of video. The GRF  
 102 moment is the cross-product of the GRF originating from the center of pressure  
 103 (CoP) at the base of the foot measured by the force platform with respect to the  
 104 joint's center of rotation, which defines the GRF moment arm [17]. Because ground  
 105 reaction forces had negligible mediolateral and fore-aft horizontal components, we  
 106 estimated each GRF moment arm to be a horizontal distance between the joint and  
 107 CoP.

108 Due to vibrations arising from resonance of the fore and aft vertical force sensors,  
 109 we were unable to obtain reliable CoP measurements for the initial force platform.  
 110 High-speed video showed that the foot lifted off and lost contact with the ground  
 111 incrementally from the MTP (metatarso-phalangeal) joint to the toes, indicating  
 112 that anterior movement of the CoP is greatest near the end of takeoff. We therefore  
 113 estimated the position of the CoP as initially being 25% of the distance from the  
 114 MTP to the toes and moving exponentially in the x-direction towards the distal end  
 115 of digit III over the course of leap takeoff. The data presented here are based on a  
 116 model in which CoP distance from the MTP,  $c$ , is defined as  $c_t = r/4 + (3r/4) * e^{d_t - d}$ ,  
 117 where  $r$  is the distance between the MTP and the toe,  $d$  is the duration of the takeoff  
 118 in frames of high-speed video, and  $d_t$  is the given frame for which  $c_t$  is calculated  
 119 (Figure S2). Although changing the CoP movement model has some effect on joint  
 120 torques (Table S1), especially at the MTP and hip, the general pattern of joint  
 121 torques remains robust (Figure S3).

122 GRF moments at each joint are resisted by the contraction of muscles that cross  
 123 the joint, creating a counteracting muscle joint moment. At each joint, we as-  
 124 sumed that each agonist muscle exerts a force proportional to its physiological  
 125 cross-sectional area (PCSA), or similar peak stress. We calculated PCSA using the  
 126 equation

$$127 \quad PCSA = \frac{mass * \cos(\phi)}{\rho_m * fiberlength} \quad (1)$$

128 where  $\phi$  is pennation angle, and  $\rho_m$  is the density of muscle ( $1060\text{kg}/\text{m}^3$  according  
 129 to [19]). Additionally, we assumed no co-contraction of antagonistic muscle pairs,  
 130 except in the cases of biarticulate muscles spanning two joints.

131 The muscles counteracting the GRF moment at the most distal joint, the MTP,  
 132 are the digital flexors and plantaris (Figure 1, in green); whereas, plantarflexor  
 133 muscles — the plantaris, soleus, and gastrocnemius (Figure 1, in blue) — resist  
 134 the ankle GRF joint moment (in jerboas, the moment arm of the digital flexors is  
 135 close to zero at the ankle). Because the plantaris muscle exerts a moment at both  
 136 the MTP and ankle joints, plantaris muscle-tendon force was first calculated at  
 137 the MTP joint, then subtracted from the total ankle plantarflexor muscle moment  
 138 ( $M_A - F_{plant} \times r_{plant}$ ), leaving the remainder of the moment to be generated by  
 139 the gastrocnemius and the soleus. At the knee joint, rectus femoris, vastus lateralis,  
 140 vastus medialis, and vastus intermedius (i.e. quadriceps) all resist the GRF knee  
 141 flexor moment (Figure 1, in purple), in addition to flexor moments produced by  
 142 the bi-articular gastrocnemius and tri-articular plantaris that have origins from the  
 143 femoral epicondyles. Thus, the quadriceps knee extensors balance the sum of the  
 144 GRF moment at the knee and the opposing flexor moments from the gastrocnemius  
 145 and plantaris: ( $M_K + F_{gast} \times r_{gast} + F_{plant} \times r_{plant}$ ). Similarly, the rectus femoris  
 146 applies an opposing flexor moment at the hip. The hip extensors considered to resist  
 147 hip flexor moments were the biceps femoris, gluteus muscles (medius, medialis, and  
 148 minimus), adductor magnus, and semitendinosus (Figure 1, in red). These muscles  
 149 resist the GRF flexor moment at the hip, in addition to that produced by rectus  
 150 femoris at the knee ( $M_H + F_{recF} \times r_{recF}$ ).

151 Joint angles (Figure 3 a) as defined in Figure 1 (labeled  $\theta$ ) were obtained using  
 152 the following equation:

$$153 \quad \theta_{1,2} = \text{abs}(\text{acos}(\text{limb element}_1 \cdot \text{limb element}_2)) \quad (2)$$

154 where  $\cdot$  indicates the dot product. Joint angles were differentiated to obtain an-  
 155 gular velocity and multiplied by the joint moment to calculate joint power. Joint  
 156 power was integrated over time to calculate net joint work over the takeoff phase  
 157 of the leap. Hip angle was not available during the entirety of all trials, due to the  
 158 anterior portion of the animal occasionally leaving the field of view near the end

159 of the trial. Trials with complete hip angle data showed that hip angle remained  
 160 relatively constant throughout the trial. Therefore, to obtain hip joint work values,  
 161 the hip joint angle was assumed to remain constant (i.e. no additional joint work)  
 162 throughout the remainder of the trial once it disappeared from the camera’s field  
 163 of view.

164 From the muscle-tendon force data, we calculated the strain energy storage in  
 165 the digital flexor, plantaris, and Achilles tendons. Tendon stress was calculated by  
 166 dividing the force by tendon cross-sectional area. Tendon cross-sectional area was  
 167 calculated using the following equation:

$$168 \quad CSA = \frac{mass}{\rho_t * length} \quad (3)$$

169 where the density of tendon ( $\rho_t$ ) is  $1120kg/m^3$  [20]. Strain is stress divided by the  
 170 tendon elastic modulus. We used a value of 1.0 GPa [21, 22, 23], which approximates  
 171 the average modulus over a tendon strain range of 0–5% [8]. Overall tendon length  
 172 change was calculated as strain multiplied by resting tendon length (measured dur-  
 173 ing dissection from muscle-tendon unit as origin to insertion minus muscle fascicle  
 174 length). Tendon elastic energy was then calculated assuming Hookean behavior as:  
 175  $W = \frac{1}{2}F\Delta L$ . Although this assumption ignores the “toe” region of the J-shaped  
 176 tendon elasticity curve, our use of a lower elastic modulus (1.0 GPa) compared  
 177 with the modulus for the linear stress-strain region ( $\approx 1.2$  GPa) helps to correct  
 178 for overestimates based on an assumption of linear elasticity [8]. Because tendon  
 179 resilience is  $\approx 93\%$  [24, 25], we multiplied tendon energy storage by 0.93 to estimate  
 180 the energy recovered that could help to power the animal’s leap. We compared the  
 181 tendon energy in both limbs to the total energy of the leap, as determined by po-  
 182 tential energy at maximum leap height, to compute tendon energy recovery for each  
 183 trial. To provide a conservative estimation of the CoM location, we recorded the  
 184 location of the rump behind the hip at maximum leap height to calculate potential  
 185 energy. Unless noted otherwise, data are reported as mean  $\pm$  SD.

## 186 **Results**

187 We analyzed 36 trials from five jerboas (2–14 leaps per animal). 11 trials from three  
 188 individuals involved no contact with the sides of the enclosure, could therefore be



189 used to determine maximum leap height and total energy of the leap. In each figure,  
190 data points for each individual have the same shape.

### 191 Leap Patterns

192 Jerboas leapt to a mean recorded height of 0.37 m, with a maximum leap height  
193 exceeding 0.60 m (Leap height vs peak GRF was not included for the highest tri-  
194 als, as jerboas truncated their leaps by gripping onto the wall and escaping from  
195 the enclosure. Experimenters chose to recapture the animal in lieu of being able to  
196 save the recorded data for those trials). The highest leaps were approximately 10  
197 times hip height at mid-stance during forward locomotion (6.1 cm, calculated from  
198 forward locomotion data collected for [26]). Average peak single-leg GRF was 2.6  
199 (N/body weights) with a maximum of 4.5 (N/body weights). A positive correla-  
200 tion between maximum leap height and peak vertical GRF was observed ( $p=0.03$ ,  
201  $R^2=0.42$ , Figure 2). Few leaps were immediate takeoffs from a previous landing. Of-  
202 tentimes jerboas would perform multiple leaps in succession. However, due to there  
203 being a few seconds between each leap (see Additional file S1), countermovement  
204 leaps were rarely observed. The highest leaps, both in our dataset and those not  
205 saved and analyzed, were often the first or the only leap in a series.

### 206 Muscle-tendon architecture

207 Muscle and tendon measurements are presented in Tables 1 and 2. MTP (plantar)  
208 flexors accounted for 5.4% of the total hindlimb “extensor” muscle mass (for multi-  
209 articular muscles, muscle mass distribution was categorized based on the more distal  
210 joint across which the muscle acts), with ankle extensors being 14.1%, knee exten-  
211 sors 24.1%, and hip extensors 56.5% of total extensor muscle mass. As expected  
212 for fast-moving limbs, muscle mass decreased in the more distal limb segments, de-  
213 creasing the moment of inertia of the limb with respect to the hip. In contrast, the  
214 cross-sectional area of the MTP flexors, ankle, knee, and hip extensors accounted for  
215 9.0%, 33.9%, 25.8%, and 31.2% of the total hindlimb muscle cross-sectional area, re-  
216 spectively. Because force generation is proportional to muscle cross-sectional area,  
217 ankle and MTP plantarflexors would be expected to contribute more force with  
218 respect to their mass.

219 Joint work, muscle stress, and force

220 MTP joint angle decreased (dorsi-flexed) throughout takeoff from the ground (Fig-  
221 ure 3 a), indicating negative MTP joint work during jump takeoff ( $-52.4 \pm 31.6$  mJ  
222 /kg body mass, Figure 3 e). MTP plantar-flexor muscles exerted mean peak stresses  
223 of 132.8 kPa; much higher than the stresses exerted by muscles at other joints. The  
224 maximum muscle stress recorded (317.1 kPa in the plantaris) was less than the peak  
225 muscle stress recorded in kangaroo rat ankle extensors during vertical leaping (350  
226 kPa) [11]. However, greater muscle stresses were likely achieved in the higher leaps  
227 not analyzed (due to animals escaping the leaping enclosure and lost data). Peak  
228 force generated by the plantaris was 3.28 N, which was the highest force produced  
229 by any single muscle belly (Figure 4 a). For a 64 g jerboa weighing 0.6 N, maximum  
230 force generated by the plantaris therefore exceeded five times the animal's weight.

231 Work produced at the ankle joint exceeded work at any other joint, with an aver-  
232 age of  $231.6 \pm 132.0$  mJ/kg body mass (Figure 4 b). Ankle plantarflexors exerted  
233 mean peak stresses of 30.8 kPa, with a maximum stress of 62.2 kPa. Similar PCSA  
234 values for lateral and medial heads of the gastrocnemius resulted in our estimate  
235 of nearly identical forces at these two muscles (Figure 4 b). The maximum force  
236 produced by the lateral gastrocnemius head was 1.9 N, with the maximum force  
237 produced by both heads being 3.8 N. Due to its much smaller PCSA, the soleus  
238 contributed very little to the ankle moment, exerting an estimated maximum force  
239 of 0.1 N.

240 An average of  $175.4 \pm 99.6$  mJ/kg body mass of work was produced at the knee  
241 (Figure 4 c); considerably less than expected based on the cross-sectional area of  
242 the knee flexors relative to the ankle extensors and MTP plantarflexors (Table  
243 1). As a group, the quadriceps produced average peak stresses of 17.0 kPa, with  
244 a maximum of 42.7 kPa. Given its larger size, the vastus lateralis generated the  
245 greatest estimated peak force at the knee (mean 0.7 N, max 1.8 N, Figure 4 c). As  
246 the smallest of the quadriceps, the vastus intermedius contributed the least force to  
247 the knee extensor moment (mean 0.1 N, max 0.2 N, Figure 4 c).

248 An average of  $132.9 \pm 103.4$  mJ/kg body mass of work was produced at the hip,  
249 contributing the least amount of positive work relative to the knee and ankle joints  
250 to leap potential energy (Figure 4 d). Hip adductors produced an average peak  
251 stress of 6.3 kPa and a maximum stress of 14.1 kPa. The greatest peak forces at

252 the hip were produced by the biceps femoris (mean 0.2 N, max 0.5 N, Figure 4 d).  
253 Although the hip extensors have a greater total cross-sectional area (Table 1) and  
254 a greater number of muscles in comparison to agonist extensor and plantarflexor  
255 groups at more distal joints, the hip extensors contributed less net positive work  
256 toward the vertical leap than the ankle or knee joints due to the hip angle remaining  
257 relatively constant throughout the takeoff of each trial (Figure 4 d).

258 Power produced by muscles acting at each joint peaked at different times during  
259 leap takeoff (Figure 3 b). The MTP moment was small throughout the takeoff, due  
260 to the close proximity of the MTP joint to the CoP. Consequently, the muscles acting  
261 at the MTP produced small amounts of negative power (due to MTP dorsiflexion)  
262 throughout the takeoff (Figure 3 b). The ankle, knee, and hip moments gradually  
263 increased until 60–70% of takeoff, and then decreased rapidly after peak GRF,  
264 toward the end of takeoff, as the animal left the ground and rose into the air  
265 (Figure 3 c). Joint power generated by the ankle and hip exhibited two peaks, one  
266 at 15% takeoff, and one 60% takeoff (Figure 3 b). On the other hand, the joint  
267 power generated by muscles acting at the knee had a single peak, with the knee  
268 occurring at 80% takeoff (Figure 3 b).

#### 269 Tendon energy recovery

270 We analyzed the plantaris, digital flexor, and Achilles tendons for their contribution  
271 to strain energy storage and recovery during leaping, as these are the largest tendons  
272 in the hindlimbs and attach to muscles producing the greatest force. The plantaris  
273 tendon experienced the greatest peak stresses (mean 11.6, max 25.6 MPa), and  
274 the Achilles experienced the least (mean 3.2, max 6.0 MPa), despite transmitting  
275 greater total force from both heads of the gastrocnemius (Figure 5 a, 4 b). All  
276 tendon stresses were well within the tensile strength of vertebrate tendon,  $\approx 100$   
277 MPa [21], and had a minimum safety factor of 3.9.

278 The low tendon stresses resulted in very small amounts of energy being recovered  
279 from the tendons. The maximum energy contribution of a single tendon throughout  
280 a leap was approximately 20 mJ, and the maximum energy recovery throughout a  
281 leap from all tendons in both hindlimbs was 64.2 mJ (Figure 5 c), in a trial without  
282 maximum jump height. The maximum recorded leap energy was estimated to be  
283 314.9 mJ, with the tendons contributing 22.0 mJ (14.3% energy recovery) for that

284 trial. Tendon contributions to total leap energy for both hindlimbs averaged 4.4%  
285  $\pm$  3.1% (Figure 5 d) and showed no significant relationship with peak leap height,  
286 although the lack of significance may be due to small sample size (Figure 5 b).

## 287 **Discussion**

288 Muscle forces in this paper have been analyzed under a number of assumptions,  
289 both to simplify the analysis and to enable direct comparison to previous studies of  
290 jumping mammals. Electromyographic recordings in future studies could determine  
291 whether co-contraction of antagonistic muscles would need to be incorporated into  
292 the model, which would increase the estimated force produced by the muscles. Sim-  
293 ilarly, accounting for force-length (F-L) and force-velocity (F-V) effects in future  
294 analyses of jerboa leaping would be useful, if such analyses were related to the F-L  
295 and F-V measurements of key hindlimb muscles. Based on our study, the gastroc-  
296 nemius and plantaris muscles would be most important to assess, as our inverse  
297 dynamics analysis indicates that these muscles generate the greatest work during  
298 leaping. Finally, it would be of interest to know the fiber type distributions for these  
299 muscles, but such data are not currently available, other than for the soleus [27, 28],  
300 which is comprised of type I fibers. However, our analysis shows that the soleus is  
301 extremely small and cannot contribute much work to leaping. Thus, further exper-  
302 imentation and muscle modeling would enable a more detailed analysis, though we  
303 believe that these additional considerations would minimally affect the significance  
304 of the results presented here.

305 Studying jerboa vertical leaping under controlled laboratory conditions represents  
306 an important first step in understanding how and why these small mammals gen-  
307 erate some of the highest leaps (relative to hip height) of most mammals [29, 30].  
308 Although we observed leaps in excess of 10 times hip height in the laboratory, obser-  
309 vations of jerboas in the wild suggest that jerboas are capable of more extreme leap-  
310 ing maneuvers [31]. Indeed, the low values of mean muscle and tendon stresses we  
311 calculated here suggest a greater capacity for leaping and accelerative maneuvering  
312 than we observed in the laboratory. The restrictive artificial enclosure, including the  
313 solid substrate, likely limited the jerboas' motivation and performance. That field  
314 performance may substantially exceed laboratory performance has been recorded  
315 in other species, and highlights the importance of identifying and quantifying those

316 stimuli that motivate animal locomotion [32, 33]. Despite the somewhat subdued  
317 behaviors exhibited by jerboas in laboratory settings, the mechanistic understand-  
318 ing gained from a biomechanical analysis of leaping performance helps to predict the  
319 limits of their performance for other behaviors and the selective pressures favoring  
320 the evolution of their locomotion.

321 During leaping, we observed a consistent pattern of peak hip extension and work  
322 early in takeoff, with little change throughout the rest of takeoff. This likely ele-  
323 vates the CoM to minimize pitch instability of the trunk during subsequent knee  
324 and ankle power output. The early peak of jerboa hip power matches other leaping  
325 vertebrates, such as frogs, galagos, humans, and cats [34, 29, 35, 36]. Lizards leaping  
326 from substrates with variable friction provide further evidence that trunk pitch is  
327 important to a successful leap — perturbations to trunk pitch during takeoff are  
328 rapidly corrected with inertial movements of the tail [37]. Finally, in contrast to  
329 power generated at the hip, knee, and ankle joints, negative power (energy absorp-  
330 tion) occurs at the MTP joint during leaping. Interestingly, this pattern parallels  
331 MTP energy absorption in wallabies during acceleration [38] and in goats during  
332 incline locomotion [39], and may reflect the biarticular transfer of energy from the  
333 MTP joint via the plantaris tendon to contribute power for ankle extension.

334 The contribution of jerboa tendon elastic energy recovery to CoM work during  
335 leaping is surprisingly low, even when compared to tendon elastic energy recovery  
336 in kangaroo rats during forward hopping and vertical leaping [10, 11], despite these  
337 animals being morphologically and behaviorally convergent. Unlike small bipedal  
338 rodents, kangaroos have thinner tendons (relative to body size) that store and  
339 return substantially more elastic energy, enabling them to perform sustained bouts  
340 of steady-state cursorial locomotion; while simultaneously hindering accelerative  
341 ability, which is likely unnecessary due to their lack of consistent predation pressure  
342 [40, 41]. For both bipedal and quadrupedal cursorial animals, even small stride-to-  
343 stride energy savings can add up to substantial energy savings over time, reducing  
344 the cost of foraging. Dogs, horses, kangaroos, and ostriches can recycle 36–74% of  
345 their total limb mechanical work by storing energy elastically in tendons [42, 8,  
346 7, 43]. In comparison, jerboas and kangaroo rats recover far less energy compared  
347 with the CoM work performed during locomotion and leaping (Figure 5 d), and rely  
348 on acceleration capacity to escape predation [44]. Thus, muscle-tendon morphology

349 suggests a significant difference in the ecological context and selective pressures  
350 encountered by small and large bipedal hopping mammals.

351 While energetically costly, locomotion that is predominantly powered by muscular  
352 contraction has the benefit of producing rapid changes in movement, or a high  
353 acceleration capacity. Because compliant tendons result in greater stretch for a  
354 given amount of force, it requires a muscle to shorten a greater distance and (for  
355 a given shortening rate) a longer time to produce movement at a joint. Therefore,  
356 reduced tendon stretch and energy storage can be advantageous, especially for prey  
357 animals that must produce rapid joint movements to change speed or direction  
358 for predator evasion [45]. Because of the high energetic cost, this strategy would be  
359 most appropriate for evading predators that are committed to a single strike, rather  
360 than being pursued over long distances.

361 It is difficult to discern whether the small size of jerboas and kangaroo rats con-  
362 strains their tendon morphology, and thus their capacity for elastic energy storage.  
363 Biewener and Bertram [40] argue that because tendons are generally thicker than  
364 expected based on strength [46], kangaroo tendons have evolved to be thinner than  
365 expected for their body size to favor elastic energy storage at the expense of a re-  
366 duced acceleration ability and control of rapid movements. However, it is unclear  
367 if small jerboa-sized mammals also have the ability to evolve thinner tendons for  
368 enhanced elastic energy recovery. Kangaroo rat tendons are thicker than expected  
369 given geometric similarity, and would require  $\approx 80\%$  reduction in cross-sectional  
370 area to confer elastic energy recovery equivalent to a kangaroo or wallaby [10].  
371 Relatively few biomechanical analyses have examined the terrestrial locomotion of  
372 quadrupedal mammals smaller than 1 kg, because most small mammals (including  
373 the quadrupedal ancestors of jerboas) are ambulatory generalists with fewer less  
374 obvious biomechanical specializations [47, 48]. Elephant shrews (*Elephantulus spp.*,  
375 Macroscelidae) would provide the most informative comparison, as they are the only  
376 identified group of micro-cursorial quadrupedal mammals [49]. Evidence of thinner  
377 tendons than expected by geometric similarity in elephant shrew hindlimbs would  
378 suggest that animals of small size may not be constrained to have stiff tendons with  
379 low elastic energy storage. This would lend support to the argument that, jerboas  
380 and kangaroo rats likely encountered selection favoring greater tendon thickness  
381 and force transmission, allowing for rapid accelerative movements.

382 The low level of tendon strain computed in this analysis suggests that jerboas do  
 383 not rely on power amplification to achieve the leaps that we recorded. Power ampli-  
 384 fication has been indirectly demonstrated to occur in other mammals during jump-  
 385 ing, such as rock wallabies and galagos, which frequently move over irregular and  
 386 discontinuous locomotor substrates [50, 29]. Jumping that is predominantly pow-  
 387 ered by muscle contraction has the advantage of requiring no extra time to preload  
 388 the tendon, thus making it possible to produce a more rapid leaping movement.  
 389 Thus, muscle-powered leaps have the potential to enhance the three-dimensional  
 390 complexity of a trajectory, which is important for evading single-strike predators on  
 391 a continuous locomotor matrix [45, 26]. Since jerboas and kangaroo rats are only  
 392 found in continuous desert environments, leaping that is predominantly powered  
 393 by muscle contraction likely provides a greater advantage to their predator evasion  
 394 ability than leaping via power amplification from their tendons.

## 395 Conclusion

396 Our results show that the hindlimb morphology of jerboas, much like kangaroo  
 397 rats, favors the rapid generation of large ground reaction forces during leaping by  
 398 reliance on muscle work rather than elastic energy recovery to power acceleration  
 399 and movement. Such short bouts of rapid leaping would be particularly well suited  
 400 to evading single-strike predators, especially in desert ecosystems where sympatric  
 401 quadrupedal rodents are at greater risk for predation due to moving with lower  
 402 velocities and less unpredictable trajectories [2]. Future studies of biomechanical  
 403 performance in a field setting will provide important insight into the evolutionary  
 404 and ecological context of this spectacular leaping rodent.

## 405 List of Abbreviations

- 406 • **GRF** Ground reaction force
- 407 • **CoP** Center of pressure
- 408 • **CoM** Center of mass
- 409 • **MTP** Metatarsal-Phalangeal joint
- 410 •  $x_{CoP}$  x-position of the Center of Pressure
- 411 •  $T_y$  Torque in the y-plane measured by the load cell
- 412 •  $F_z$  Force in the z-plane measured by the load cell
- 413 •  $t$  Thickness of the plate, in this case 7.5mm
- 414 • **PCSA** Physiological cross-sectional area of muscle (Equation 1)
- 415 •  $\theta$  Joint angle (Equation 2)
- 416 • **CSA** Cross-sectional area of tendon (Equation 3)
- 417 • **BW** Body weight of jerboa

- 418 •  $\phi$  Muscle pennation angle
- 419 •  $\rho_x$  Density of  $x$
- 420 •  $M_x$  Ground reaction force moment of joint  $x$
- 421 •  $F_x$  Force produced by muscle  $x$
- 422 •  $r_x$  Moment arm of muscle  $x$
- 423 •  $W$  Tendon Spring Energy
- 424 •  $\Delta L$  Change of tendon length

#### 425 Ethics

426 All animal care and use protocols were approved by the Harvard Faculty of Arts and Sciences Institutional Animal  
427 Care and Use Committee (IACUC) and the United States Department of Agriculture.

#### 428 Consent for publication

429 Not applicable

#### 430 Competing interests

431 The authors declare that they have no competing interests.

#### 432 Availability of data and materials

433 The datasets and code analysed during the current study available from the corresponding author on reasonable  
434 request.

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#### 437 Authors' contributions

438 All authors designed the experiment, T.Y.M. and A.M.R. collected data and performed inverse dynamics analysis,  
439 and all authors contributed to writing the manuscript. This work was performed in contribution to an undergraduate  
440 honors thesis to A.M.R at Harvard College.

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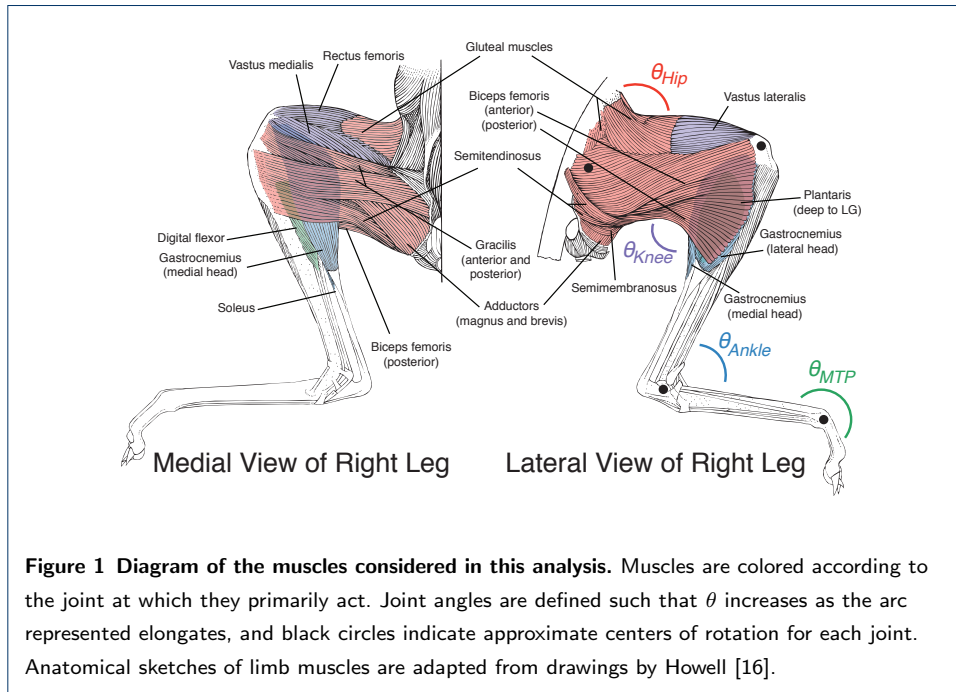
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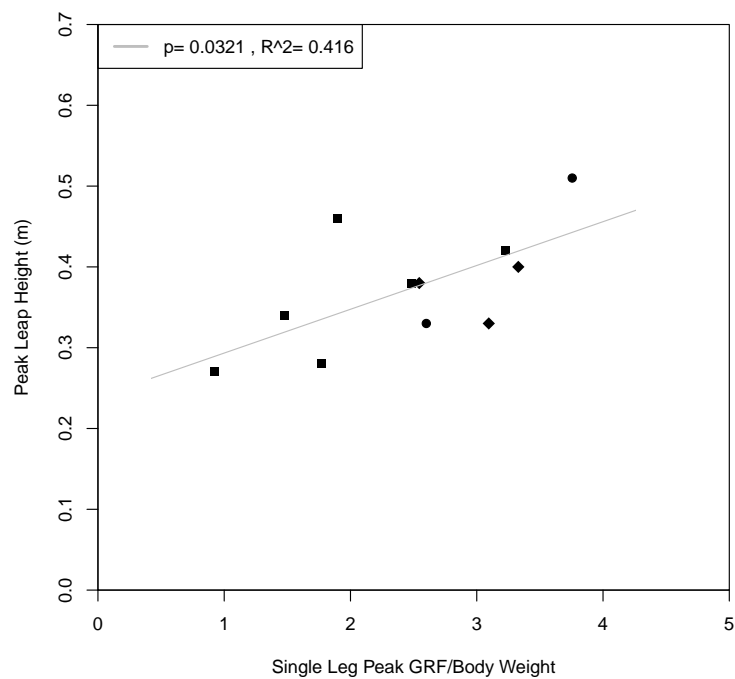


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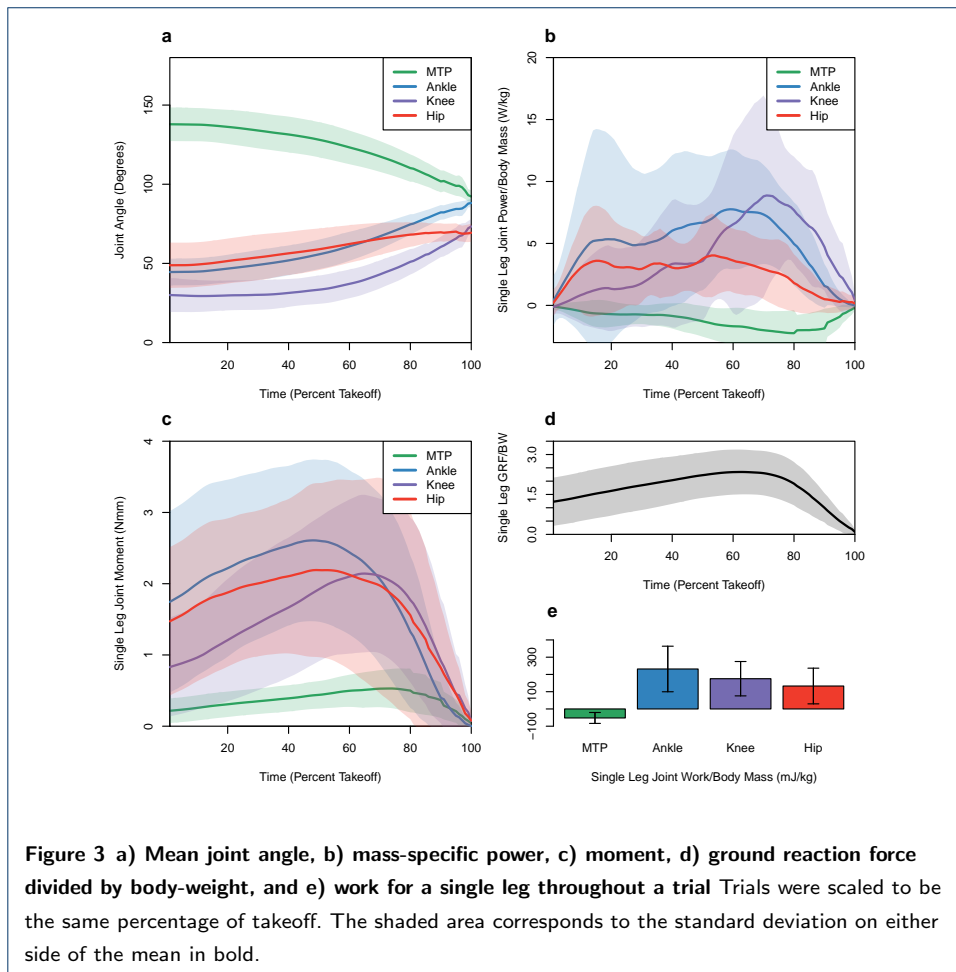
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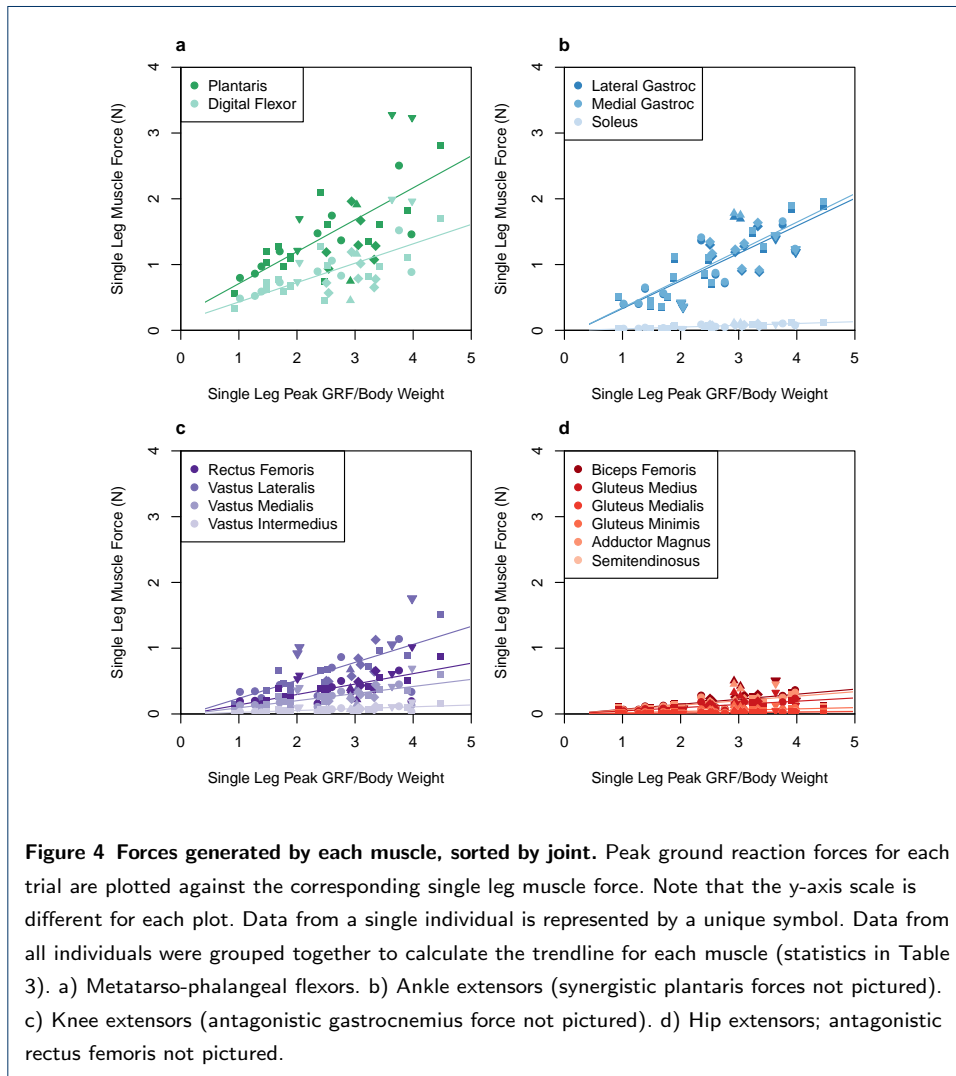
561 **Figures**

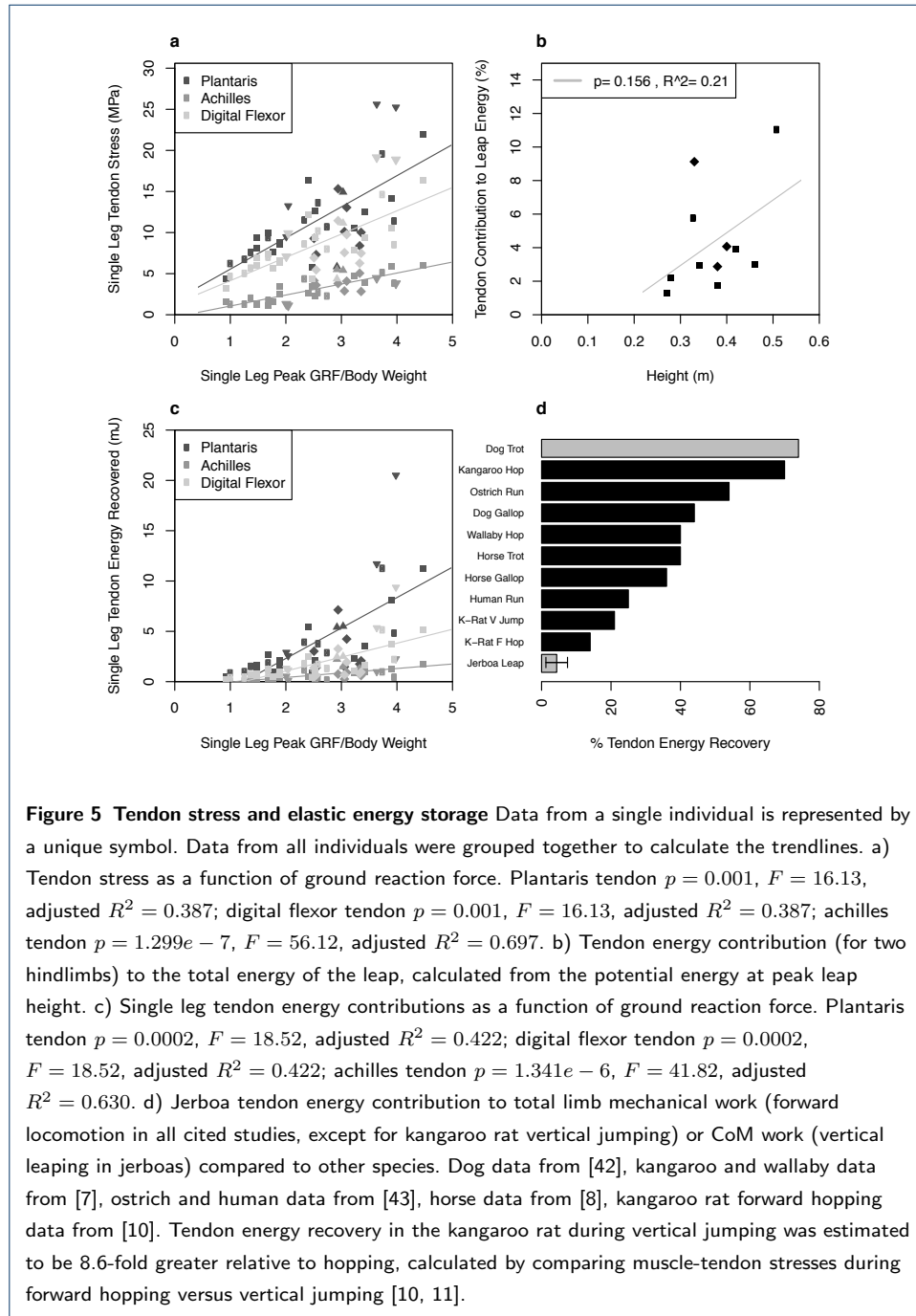




**Figure 2 Height versus normalized force for each trial.** The x-axis represents the maximum force recorded during each leap divided by body weight. The y-axis is a conservative estimate of peak CoM height. Of the data collected, only 11 leaps from three individuals involved no contact with the side walls and are included in this figure.







562 **Tables**

563 See next page



**Table 1 Hindlimb muscle morphometric data geometrically scaled for a jerboa of mass 62.72g.** Muscle masses are shown in grams, fiber length and moment arms are shown in millimeters, and muscle pennation angles are shown in degrees.

Muscle	Mass	Fiber Length	Pennation Angle	MTP Arm	Ankle Arm	Knee Arm	Hip Arm
Plantaris	0.10	7.10	8	1.15	4.52	1.96	-
Digital Flexors	0.06	7.25	15	1.08	1.58	-	-
Medial Gastroc	0.20	4.39	15	-	4.52	2.02	-
Lateral Gastroc	0.22	5.15	18	-	4.52	2.02	-
Soleus	0.02	7.16	5	-	4.47	-	-
Rectus Femoris	0.18	9.35	16	-	-	3.33	5.75
Vastus Lateralis	0.43	13.21	11	-	-	3.33	-
Vastus Medialis	0.13	9.98	10	-	-	3.33	-
Vastus Intermedius	0.02	5.30	5	-	-	3.33	-
Biceps Femoris	0.87	32.26	10	-	-	-	5.79
Gluteus Medius	0.19	11.23	0	-	-	-	3.42
Gluteus Medialis	0.02	6.65	0	-	-	-	3.42
Gluteus Minimus	0.06	8.63	0	-	-	-	3.42
Adductor Magnus	0.56	23.01	3	-	-	-	10.52
Semitendinosus	0.07	23.46	3	-	-	-	11.32

**Table 2 Morphometric data for hindlimb tendons geometrically scaled for a jerboa of mass 62.72g.** Tendon masses are in grams, lengths are in millimeters, cross-sectional area in square millimeters.

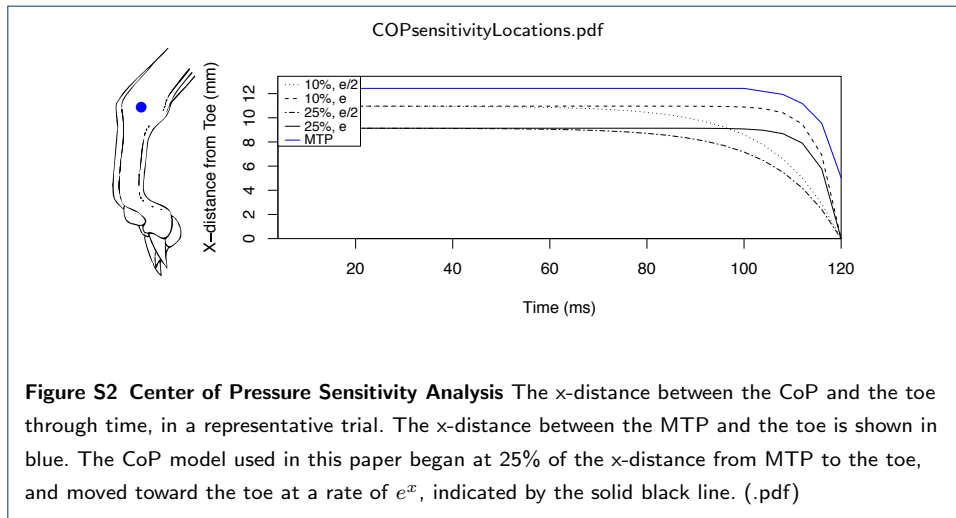
Tendon	Mass	Length	CSA	Flexor Moment Arm	Extensor Moment Arm
Plantaris	0.006	46.688	0.119	1.900	-
Digital Flexor	0.014	47.050	0.271	1.900	-
Achilles	0.017	19.906	0.784	-	4.820

**Table 3 Statistics for trendlines in Figure 4.**

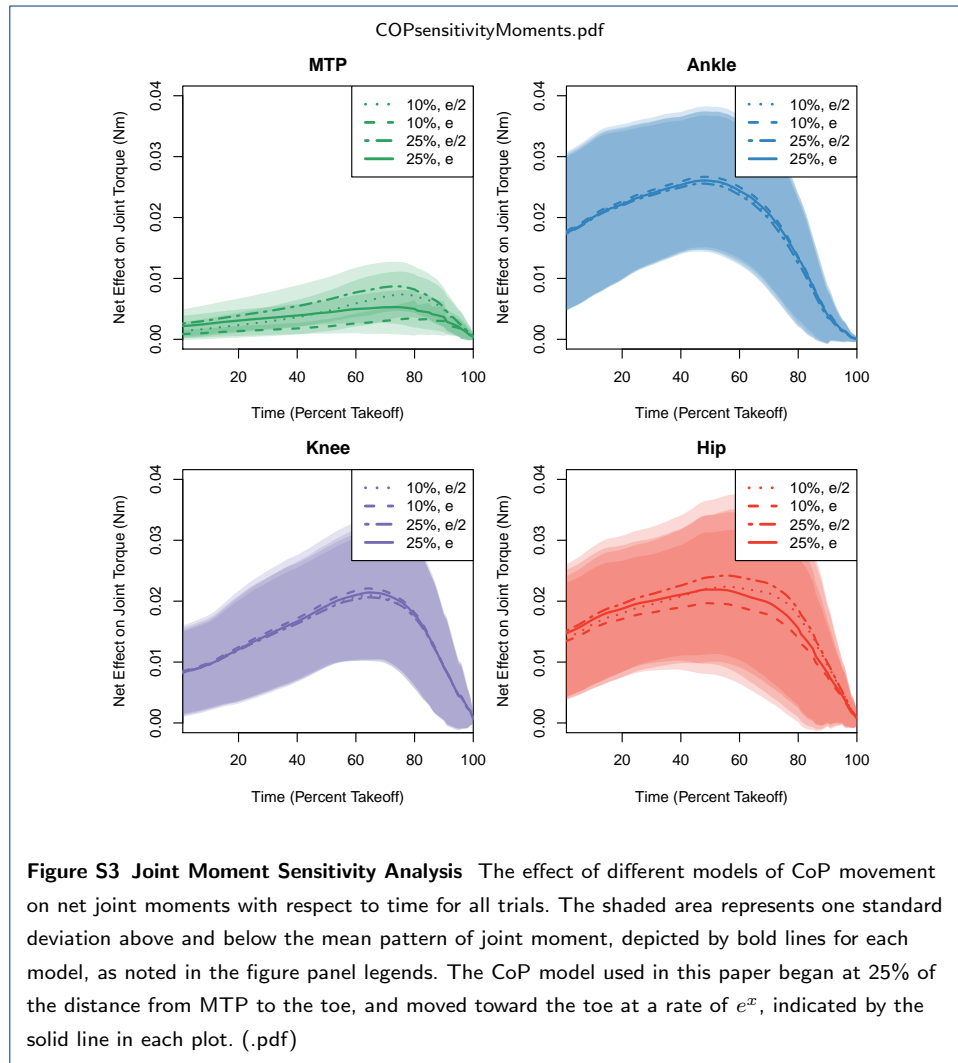
Muscle	<i>p</i> value	<i>F</i> statistic	Adjusted <i>R</i> <sup>2</sup>
Plantaris	0.012	7.48	0.213
Digital Flexor	0.012	7.48	0.213
Lateral Gastrocnemius	3.350e-8	65.86	0.730
Medial Gastrocnemius	1.347e-8	73.09	0.750
Soleus	1.347e-8	73.09	0.750
Rectus Femoris	0.001	14.86	0.366
Vastus Lateralis	0.001	14.86	0.366
Vastus Medialis	0.001	14.86	0.366
Vastus Intermedius	0.001	14.86	0.366
Biceps Femoris	1.052e-5	31.42	0.559
Gluteus Medius	1.052e-5	31.42	0.559
Gluteus Medialis	1.052e-5	31.42	0.559
Gluteus Minimus	1.052e-5	31.42	0.559
Adductor Magnus	1.052e-5	31.42	0.559
Semitendinosus	1.052e-5	31.42	0.559

564 Additional Files

**Figure S1 Video of jerboa leap** A video of a sample vertical leap. The jerboa is standing upon a 2-axis force plate, inside of a vertical trap. In the presence of increased air flow, the jerboa leaps vertically. (.avi)



**Figure S2 Center of Pressure Sensitivity Analysis** The x-distance between the CoP and the toe through time, in a representative trial. The x-distance between the MTP and the toe is shown in blue. The CoP model used in this paper began at 25% of the x-distance from MTP to the toe, and moved toward the toe at a rate of  $e^{-x}$ , indicated by the solid black line. (.pdf)



**Table S1 Effect of CoP model on muscle stress by joint.** Stresses for each model are shown as a proportion of the model used (25% initial location, exponential movement).

Joint	10%, $e/2$	10%, $e$	25%, $e/2$
MTP	2.01	1.31	2.35
Ankle	0.98	1.00	0.96
Knee	0.96	0.98	0.94
Hip	1.10	1.01	1.18