

Determinants of workplace exposure and release of ultrafine particles during atmospheric plasma spraying in the ceramic industry

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Abstract

Atmospheric plasma spraying (APS) is a frequently used technique to produce enhanced-property coatings for different materials in the ceramic industry. This work aimed to characterise and quantify the impact of APS on workplace exposure to airborne particles, with a focus on ultrafine particles (UFPs, <100 nm) and nanoparticles (<50 nm). Particle number, mass concentrations, alveolar lung deposited surface area concentration, and size distributions, in the range 10 nm – 20 µm were simultaneously monitored at the emission source, in the worker breathing zone, and in outdoor air. Different input materials (known as feedstock) were tested: (a) micro-sized powders, and (b) suspensions containing submicron- or nano-sized particles. Results evidenced significant UFP emissions (up to $3.3 \times 10^6/\text{cm}^3$) inside the projection chamber, which impacted exposure in the breathing zone outside the projection chamber (up to $8.3 \times 10^5/\text{cm}^3$). Environmental release of UFPs was also detected and quantified ($3.9 \times 10^5/\text{cm}^3$). Engineered nanoparticle (ENP) release to workplace air was also evidenced by TEM microscopy. UFP emissions were detected during the application of both micro-sized powder and suspensions containing submicron- or nano-sized particles, thus suggesting that emissions were process- (and not material-) dependent. An effective risk prevention protocol was implemented, which resulted in a reduction of worker UFP exposure in the breathing zone. These findings evidence the potential risk of occupational exposure to UFPs during atmospheric plasma spraying, and raise the need for further research on UFP formation mechanisms in high-energy industrial processes.

Keywords: process-generated particles, engineered nanoparticles, pristine nanoparticles, mitigation strategies, occupational health, indoor air quality, thermal plasma spraying.

1. Introduction

Thermal spraying in general, and atmospheric plasma spraying (APS) in particular, are frequently used technologies to produce high-performance surfaces required in industrial processes. APS is used to deposit different coatings on a number of surfaces in order to achieve enhanced properties such as wear, corrosion, electrical insulation or heat resistance, while maintaining the structural properties of the underlying material (Fauchais et al., 2014; Rosso et al., 2001; Stöver and Funke, 1999). Atmospheric plasma spraying is commonly employed because of its versatility and wide applicability in diverse technologies such as coating of stainless steel components (e.g., pistons) to prevent wear and corrosion in pump applications, coating of metal structures (e.g., turbine engines and blades) to obtain ceramic thermal barriers in aero-spatial and energy-generation applications, or rapid manufacturing of metal molds without limitation of pattern size, among others (Carpio et al., 2015a,b,c; Huang et al., 2016; Khor and Gu, 2000; Montanari et al., 2002; Olding et al., 2001; Tamulevičius and Dargis, 1998; Zhang et al., 2001).

During thermal spray deposition, the feedstock (starting material) is molten (or partially molten) and accelerated to impact onto the substrate surface, where the deposited material is cooled forming the coating. In the case of APS, the energetic source is a thermal plasma which achieves high impact velocities and very high temperatures (> 10000K). Plasma spraying can provide coatings with varying thickness over a large area at high deposition rate, which makes it advantageous with regard to other coating processes such as physical or chemical vapour deposition (Papyrin et al., 2007; Pawlowski, 1995). Another advantage is that the coated surface does not heat up significantly, allowing the coating of flammable substances. Furthermore, the high energy density and high temperature of plasma flow facilitate the deposition of coatings of refractory materials which are difficult to melt using other conventional thermal spraying techniques (Fauchais et al., 2014). Coating materials available for plasma spraying include metals, alloys, ceramics, plastics and composites, which are typically fed in micro-sized powder form. The use of nanoparticles (<50 nm, NPs) as a feedstock can improve the properties of the coatings (Pawlowski, 2009). However, nanoparticles cannot be injected directly inside the plasma plume because of their poor flowability and low specific weight. For this reason, the injection of suspensions (containing submicron- or nano-sized particles) instead of micro-sized powders has been implemented in recent years. This modification is named suspension plasma spraying (SPS) and the phenomena (fusion, evaporation, particle trajectory, etc.) which occur inside the plasma plume change significantly with respect to the APS technique. (Pawlowski, 2009).

High-energy industrial processes similar to plasma spraying are known to release NPs and ultrafine (<100 nm, UFP) particles into workplace air (Fonseca et al., 2015, 2016a). These particles are usually referred to as process-generated particles (Broekhuizen et al., 2012), and they have the potential to impact indoor air quality, workplace exposure and human health (Li et al., 2016). Studies have shown that one thermal spraying technique similar to plasma spraying, high velocity oxy-fuel (HVOF) spraying, may even generate emissions of large dust particles above 10 µm in size (Huang et al., 2016). In addition to process-generated particles, workplace exposure may be affected by the unintentional release of engineered NPs (ENPs). The use of nanomaterials in

94 state-of-the-art industrial processes such as APS has increased in recent years, and it
95 is expected that this trend will continue in the near future (Savolainen et al., 2013).
96 Consequently, it is critical to identify any potential risks they may pose to human health
97 in indoor, workplace and outdoor environments in the vicinity of the industrial emission
98 source. The evaluation and characterisation of exposure scenarios and risks to
99 airborne UFPs (whether process-generated or engineered) is addressed by the
100 emerging field of research of nanosafety (Savolainen et al., 2013). The need for
101 effective risk governance, which is crucial when developing new technologies and
102 industrial processes, has been evidenced (Read et al., 2016).

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104 In this framework, the present work aimed to assess UFP emissions and their potential
105 impact on workplace exposure during atmospheric plasma spraying of ceramic
106 coatings in an industrial setting. UFP release to the environment was also assessed.
107 Moreover, a prevention protocol was implemented and the exposure levels reduction
108 was quantified. Because of the different terminologies used in the air quality and the
109 nanotechnology research fields, for the purpose of this work the following terms will be
110 used: ultrafine particles (<100 nm), and nanoparticles (<50 nm). Particle diameters
111 measured in this work are mainly submicron, but given that approximately 80% of
112 particle number concentrations (N) is generally <100 nm, the term UFP will be used as
113 equivalent to N even if they are not exactly the same.

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115 **2. Experimental setup**

116 Atmospheric plasma spraying was carried out in an industrial-scale pilot plant located
117 in the facilities of the Institute of Ceramic Technology (ITC) in Castellón, Spain. The
118 APS system consisted in a mon cathode plasma torch (F4-MB, Oerlikon-Metco,
119 Switzerland) operated by a six-axes robot arm (IRB 1400, ABB, Switzerland). Due to
120 standard occupational health and safety considerations, plasma spraying in the pilot
121 plant is performed inside a closed chamber, with no direct interaction by the worker
122 (Figure S1 in Supporting Information). The projection chamber (3x3x2.5 m³) was
123 located inside the worker's room (approximate dimensions 6x6x3 m³), where the
124 breathing zone was located at approximately 1.5 m from the projection chamber.

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126 A total of 14 APS processes were carried out, 9 of which using micro-sized powders
127 and 5 using aqueous suspensions containing submicron- or nano-sized particles as
128 feedstock (Table 1). The following particle monitoring instrumentation was deployed:

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- 130 • In the worker's room, outside the projection chamber (Figure S1 and S2; Zone
131 A): a DiscMini particle counter (Testo) monitoring particle number
132 concentrations (N) between 10-700 nm and mean particle diameter (D_p) was
133 deployed next to the worker's desk, at breathing height. Appropriate conductive
134 tubing (Asbach et al., 2015; Viana et al., 2015) was used. A butanol
135 condensation particle counter (CPC, TSI Model 3775), monitoring particles
136 between 4 and 1500 nm, was also used. Particle mass concentrations were
137 monitored by means of a Grimm 1107 laser spectrometer, measuring PM₁₀,
138 PM_{2.5} and PM₁ concentrations. Particle samples for TEM-EDX analysis were
139 collected on Au grids using SKC cassettes attached to a Leland Legacy pump
140 operating at 6 L/min.

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- Inside the projection chamber (Figure S1 and S2; Zone B): N concentrations were monitored using a second DiscMini unit. Particle number size distributions between 10-420 nm were monitored by means of a portable SMPS NanoScan (Fonseca et al., 2016b; Stabile et al., 2014; Tritscher et al., 2013), which was placed for safety reasons outside of the projection chamber and connected with conductive tubing (Tygon conductive tubing, 1.5 m in length) to the inside of the chamber. The authors are aware that the length of the tubing may result in particle losses and is thus a limitation of the study. Samples for the characterisation of particle morphology and composition by TEM-EDX were collected using a 3-stage rotating impactor (1 - 2.5 μm , 2.5 - 10 μm , and > 10 μm) using Au grids as collection substrates.
 - Outdoor air: a third DiscMini unit and a second Grimm 1107 unit were deployed outdoors on the building's roof and at approximately 1 m from the ventilation exhaust originating from the worker's room, to monitor N, D_p , PM_{10} , $\text{PM}_{2.5}$ and PM_1 . The instruments were located as close as possible to the exhaust (taking into account the operational limitations) while avoiding interference from other exhaust systems. The inlets were not located inside the exhaust to avoid instrumental failures, since these instrument are not adapted to work in duct streams.

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163 All DiscMini and Grimm 1107 units were intercompared prior to the experiments at the

164 IDAEA-CSIC urban background air quality monitoring station in Barcelona, monitoring

165 outdoor air. One DiscMini was identified as the internal reference, and the other units

166 were corrected (with slope and intercept) with regard to it. Correlation coefficients (R^2)

167 between the different units were always >0.8. The Grimm 1107 spectrometers were

168 corrected individually by comparison with EU reference high-volume samplers for PM_{10}

169 and $\text{PM}_{2.5}$ mass concentrations. The DiscMini particle counters were also compared

170 with a TSI SMPS3080 system coupled with a CPC3772 and showed a $R^2 > 0.88$

171 correlation with regard to N and a 12-18% relative difference with regard to D_p (Viana et

172 al., 2015). The particle number concentration data were not corrected with regard to

173 the SMPS given the different lower cutoff sizes of the DiscMini units and SMPS

174 system. Finally, the butanol CPC was intercompared with the DiscMini units on site

175 during a non-activity period (night-time), obtaining a correlation of $R^2 = 0.87$. The CPC

176 data were not corrected with regard to the DiscMini units due to their different cutoff

177 sizes, as in the case of the SMPS. The different particle size ranges of the instruments

178 (10-700 nm for DiscMini, 4 nm to 1.5 μm for CPC) should be taken into account when

179 intercomparing the different types of instruments.

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181 Different feedstock types were tested in order to assess their influence on UFP

182 emissions (Table 1), including:

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184 Powders:

- Feedstock P1: ceramic glass powders made up of Na_2O , SiO_2 , CaO , and P_2O_5 . Its size distribution was micro-sized (<63 μm) with 1% of fluidized SiO_2 NPs (Cañas et al., 2016).
- Feedstock P2: commercial micro-scaled powder of a Ni-based superalloy (AMDRY 997, Oerlikon-Metco, Switzerland) with a mean particle size of 40 μm .

190 Suspensions:

- 191 • Feedstock S1: aqueous suspension containing a mix of lab-synthesized nano-
192 sized particles of $Gd_2Zr_2O_7$ (60nm) and submicron-sized particles of $ZrO_2-Y_2O_3$
193 (Tosoh TZ-3YS, 400nm).
- 194 • Feedstock S2: aqueous suspension containing nano-sized particles ($Gd_2Zr_2O_7$).
- 195 • Feedstock S3: aqueous suspension containing submicron-sized particles (ZrO_2-
196 Y_2O_3).

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198 In order to reduce the exposure levels after they were detected (section 3), mitigation
199 strategies were implemented according to a hierarchical prevention protocol:

- 200 • Stage 0: The APS system worked as it was set up by the manufacturer. Plasma
201 spraying took place inside a cabin (projection chamber) with an air ventilation
202 system where the air entrance was by a single point from the breathing zone.
- 203 • Stage 1: Corrective measures were applied in the emission zone (APS
204 projection chamber; Figure S1 and S2 at Zone B).
- 205 • Stage 2: Corrective measures were applied to the air extraction system.
- 206 • Stage 3: Corrective measures were applied in the breathing zone (Figure S1
207 and S2; Zone A).

208 Detailed information of the applied corrective measures is provided in section 3.2. A
209 summary of the APS experiments carried out may be found in Table 1, showing the
210 feedstocks used, the number of replicas available, and the specific characteristics of
211 the experimental setup.

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213 **3. Results and discussion**

214 *3.1. UFP emissions during plasma spraying*

215 Particle number concentrations and size distribution were monitored inside the plasma
216 chamber during the application of different feedstock as coatings. Background UFP
217 number concentrations were representative of typical concentrations in an urban area
218 ($1.6 \times 10^4/cm^3$; Pérez et al., 2010; Reche et al., 2011), with D_p ranging between 40-70
219 nm characteristic of aged diesel exhaust aerosols (Brines et al., 2016; Dall'Osto et al.,
220 2012). The influence of outdoor aerosols was high given that the doors of the pilot plant
221 were open and connected directly to outdoor air.

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223 Inside the chamber, results evidenced intense UFP emissions (Figure 1) coinciding
224 with the spraying events. Particle number concentrations increased by up to 3 orders of
225 magnitude inside the chamber (in the order of $10^6/cm^3$) with respect to background
226 concentrations ($10^3-10^4/cm^3$, Table 2) inside the chamber prior to spraying. This pattern
227 was consistent across the different replicas (Figure 1). In the example shown in Figure
228 1, as the spraying process was initiated (after closing the chamber doors) UFP
229 concentrations increased coinciding with the ignition of the plasma plume. During this
230 stage, average 10-second UFP concentrations reached $2.1 \times 10^4/cm^3$ in the projection
231 chamber, to subsequently peak at $6 \times 10^6/cm^3$ with a D_p of 25-30 nm during spraying of
232 the feedstock. The emission pattern and measured UFP concentrations and D_p were
233 mostly consistent across replicas. UFP formation may occur during three stages of
234 thermal spray: (a) heating and melting of the feedstock, (b) acceleration of the droplets,
235 and (c) impact and deposition stage. During these stages, UFPs are likely to be formed
236 through vaporisation and subsequent nucleation of emission gases, or through

237 mechanical impaction (Huang et al., 2016). They may also be formed by nucleation
238 linked to the emission of sulphur-containing gaseous precursors if these are present in
239 the feedstock (Fonseca et al., 2016a). As shown in Figure 1, the data monitored by the
240 two particle counters deployed inside the chamber (DiscMini and NanoScan) were also
241 consistent, thus confirming the high absolute concentration values measured despite
242 the fact that the peak concentrations were outside the concentration range
243 recommended by the instrument manufacturers ($>10^6/\text{cm}^3$).

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245 The results from this study evidence the formation and release of UFPs during plasma
246 spraying. A previous study focusing on a different kind of high velocity spraying (HVOF)
247 reported coarse particle emissions ($>10\ \mu\text{m}$ in size) with a unique morphology of
248 polygonal or irregular block of crushed powder, and finer dust particles ($2.5\ \mu\text{m}$) in the
249 form of irregular or flocculent agglomerates (Huang et al., 2016). The authors
250 monitored particle mass concentrations (PM, as opposed to N in this work) reaching
251 maximum concentrations of $140\ \text{mg}/\text{m}^3$, with time-weighted average concentrations of
252 $34\ \text{mg}/\text{m}^3$. In such a highly polluted scenario PM concentration should be the preferred
253 exposure metric. Due to the particle concentration levels monitored in the scenario
254 assessed in the present work, N was considered a more targeted metric for emissions
255 and exposure monitoring (Vogel et al., 2014). To the authors' knowledge, Huang et al.
256 (2016) is the only previous publication available monitoring particle release and
257 exposure due to plasma spraying.

258

259 The experimental setup described above was replicated for the different kinds of
260 feedstock shown in Table 1, with the results shown in Figure 2 and Table 2. Plasma
261 spraying generated high UFP emission concentrations under all scenarios, which
262 ranged between 2.6×10^6 and $3.3 \times 10^6/\text{cm}^3$ for experiments #1 to #3, and between
263 1.1×10^6 and $2.5 \times 10^6/\text{cm}^3$ for experiments #4 to #7. This relative decrease was probably
264 linked to the implementation of mitigation strategies which will be discussed below. The
265 mean D_p distribution monitored during experiments carried out at different stages of
266 the prevention protocol is shown in Figure S3 in Supporting Information, including the
267 following experiments: #2 and #3 (stage 1), #4 (stage 2) and #7 (stage 3). Aside from
268 the differences obtained owing to the mitigation strategies, results evidence that major
269 UFP emissions were generated during the application of both nano- and micro-sized
270 suspensions and powders, thus suggesting that the emissions are related to the
271 process and not only to the grain size distribution of the input material. This is
272 consistent with previous results (Huang et al., 2016). The feedstocks applied during
273 experiments #4, #6 and #7 were characterised by mean D_p of 60 and 400 nm
274 ($\text{Gd}_2\text{Zr}_2\text{O}_7$, and $\text{ZrO}_2\text{-Y}_2\text{O}_3$, respectively), whereas the remaining materials were
275 predominantly micro-sized ($<63\ \mu\text{m}$) with only minor contributions (1%) from
276 nanomaterials in the case of ceramic glass powders. As shown in Figure 2, mean D_p
277 inside the chamber did not vary significantly across experiments and ranged between
278 28 nm in experiment #2 (micro-scaled feedstock) and 45 nm in experiment #6 (nano-
279 scaled feedstock), and showed no consistent pattern for either type of material. As a
280 result, it may be concluded that UFP emissions from APS are process-related. No
281 statistically relevant conclusions can be drawn with regard to N emitted with the
282 different types of coatings due to the fact that the measurements were carried out
283 under different exhaust ventilation conditions inside the chamber.

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285 In order to characterise their morphology and chemical composition inside the chamber
286 particles were sampled on TEM grids. It should be noted that TED-EDX results are not
287 quantitative, and refer to single particles identified. As expected, different particle
288 morphologies were observed. Figure 3a shows an example of spherical particles
289 originating from evaporation and condensation or fusion of the feedstock, in this case
290 originating from the aqueous suspension containing submicron-sized particles (ZrO_2 -
291 Y_2O_3). In addition, release of the pristine (original) ENPs was also identified (Figure
292 3b), in the case of the Gd-based ENPs. Mauer et al. (2015) reported the difficulties in
293 coating with $Gd_2Zr_2O_7$ due to the fact that the material is partly decomposed inside the
294 plasma plume and the Gd_2O_3 is evaporated. Thus, this confirms that the ENPs
295 detected by TEM may have been originated due to a partial evaporation of the
296 feedstock and subsequent condensation of the vapour. Given the high correlation
297 between particle concentrations in the plasma chamber and in the worker breathing
298 zone (Figure 4), it is expectable that exposures to the ENPs detected inside the
299 chamber occur in the breathing zone. Further studies are necessary to confirm this
300 hypothesis. Finally, Ca-rich particles probably sourcing from the feedstock (Figure 3c)
301 were also observed. These results are also consistent with the variety of particle
302 morphologies detected in previous studies (Huang et al., 2016).

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304 3.2. *Impact on exposure*

305 Worker exposure to UFP emissions from the plasma chamber was assessed by
306 placing monitoring instruments on a desk in close proximity to the worker and at
307 breathing height, thus closely simulating breathing zone conditions (Asbach, 2015;
308 Vogel et al., 2014). Plasma spraying activities inside the chamber had an evident and
309 statistically significant impact ($> \text{background} + 3 \cdot \sigma_{\text{background}}$; Asbach et al. 2012) in the
310 breathing zone (Figure 4). Breathing zone UFP concentrations followed an increasing
311 pattern coinciding with the start of the spraying process, but with a 1-2 minute delay
312 due to transport from the chamber towards the breathing zone. In the example shown
313 in Figure 4, representative of experiments #2 to #3 (stage 1), UFP concentrations
314 increased from $2.2 \times 10^4 / \text{cm}^3$ prior to the spraying activity to $7.2 \times 10^5 / \text{cm}^3$ during and
315 after spraying. Mean D_p increased by 10-20 nm (Table 2) with regard to those
316 measured inside the plasma chamber probably due to particle transport and ageing
317 between the two measurement locations (approximately 2 m). The uncertainty of the
318 monitoring instrumentation should evidently be taken into account for this assessment.
319 As a result it may be concluded that, for experiments #1 to #3, the exhaust system in
320 place was able to remove between 68% and 91% of the UFP monitored inside the
321 plasma chamber, resulting in significant exposure concentrations in the breathing zone
322 and with potentially health hazardous D_p (33-51 nm; Table 2).

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324 Aside from the actual spraying periods, worker exposures also occurred during
325 cleaning (by using a vacuum cleaner) of the chamber at the end of each spraying
326 process. As expected, this activity impacted PM_{10} and $PM_{2.5}$ concentrations due to the
327 coarser D_p of the particles re-suspended, with concentrations increasing from 5 to 350
328 $\mu\text{g}PM_{2.5}/\text{m}^3$ (Figure 5). Conversely, emissions from direct APS had only minor impacts
329 on $PM_{2.5}$ mass. Even though these results may seem to contrast with previous studies
330 (Huang et al., 2016), it is probable that the cause are the different concentration and
331 exposure ranges in both plasma spraying scenarios, possibly influenced by the
332 different technologies applied (APS vs. HVOF).

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In order to reduce exposure concentrations, the prevention protocol described in the Methods section was applied by implementing the following measures:

- Stage 1: Improved air circulation in the plasma chamber using a multi-point system surrounding the plasma flame, as well as a delayed door-opening protocol. The air intake into the plasma room was changed from the breathing zone to directly from outdoor air.
- Stage 2: Enhanced sealing of the extraction system ducts from the chamber to the exhaust, to prevent the flow of emissions towards the breathing zone.
- Stage 3: Enhanced air exchange rates through forced ventilation in the breathing zone (to approximately 14 air exchanges per hour, in contrast to the original 2 air exchanges per hour).

Reductions in exposure concentrations in the breathing zone are evident after the implementation of the mitigation strategies (Figure 2). The comparison between experiments #1 and #2 evidences a reduction of UFP concentrations of approximately 70% (from 8.3×10^5 to $2.7 \times 10^5/\text{cm}^3$, monitored with DiscMini). Likewise, the comparison between experiments #3 and #6 shows a 75% reduction of UFP concentrations between stages 1 and 3 (from 1.8×10^5 to $4.4 \times 10^4/\text{cm}^3$, monitored with the CPC). Even though the reductions observed are experiment-dependent and data are not available from the same instrument for all experiments for direct comparison, these results evidence the benefits of the exposure mitigation protocol implemented. Exposure reductions were monitored in the breathing zone, while concentrations remained relatively constant (same order of magnitude) inside the projection chamber.

Finally, UFP concentrations in the breathing zone after the implementation of the mitigation strategies ($1.9 \times 10^4/\text{cm}^3$, measured with the CPC) were comparable to those monitored in urban environments in European cities as such as Barcelona, London or Bern (1.2×10^4 - $2.8 \times 10^4/\text{cm}^3$; Reche et al., 2011). However, it should be taken into account that the exposure risk also depends on the coating chemical composition which in some cases may include potentially health hazardous materials.

3.3. Impact on environmental release

In addition to exposure, APS emissions impacted outdoor air. Environmental release of UFPs, monitored on the rooftop of the pilot plant (5 m above ground) in the vicinity of the exhaust system (1 m), was evidenced through a 1-order of magnitude increase in UFP concentrations ($1.7 \times 10^4/\text{cm}^3$ to $2.5 \times 10^5/\text{cm}^3$; Figure 4), which was again observed across all replicas (Figure 1). As in the case of the breathing zone, this increase should also be considered statistically significant (Asbach et al., 2012). However, no environmental or health impacts should be expected from this specific pilot plant due to (a) the short temporal impact of the emissions (<2 min), (b) their fast dilution in outdoor air, (c) the fast coagulation/agglomeration of particles and thus their increase in particle diameter, and (d) the chemical composition of the feedstock used in these experiments, resembling mineral matter. Despite this, APS may be used to apply a broad variety of coatings which include potentially health hazardous metals (e.g., Cr, Co, W, etc.), in which case environmental release of such metal-rich UFPs should be monitored and prevented (Li et al., 2016) using appropriate gas cleaning systems.

381 4. Conclusions

382 Ultrafine particle emissions and their impact on workplace exposure were monitored
383 during atmospheric plasma spraying (APS) in an industrial-scale pilot plant. Particle
384 diameters monitored ranged between 10-700 nm but are reported as UFP given that
385 80% of total N is generally found in the <100 nm size range. UFP emissions were
386 expected due to the high-energy nature of this industrial process. Results evidenced
387 major UFP emissions during APS reaching up to $3.3 \times 10^6/\text{cm}^3$ inside the projection
388 chamber with D_p ranging between 28-45 nm. Breathing zone concentrations reached
389 up to $8.3 \times 10^5/\text{cm}^3$ (33-51 nm in diameter). These concentrations were statistically
390 significantly higher than the initial background concentrations of 10^3 - $10^4/\text{cm}^3$, and thus
391 evidence the health hazardous potential of this industrial process. The nature of the
392 emissions was investigated by testing micro- and nano-sized feedstocks, including
393 engineered nanoparticles (ENPs). The mean D_p inside the APS chamber did not vary
394 significantly across experiments and showed no consistent differences between the
395 different feedstocks. Thus, it was concluded that UFP emissions were detected
396 irrespective of the presence of ENPs in the feedstock, and that they were therefore
397 process-related. In a minor proportion, release of pristine ENPs to the plasma chamber
398 air was also evidenced by TEM microscopy. New particle formation originating from the
399 evaporation of the feedstock was also detected. A risk prevention protocol was applied
400 to the studied facility, leading to significant reductions in breathing zone UFP
401 concentrations. This work evidences the relevance of process-generated emissions
402 with regard to workplace exposure to nanoparticles, and the need for real-world
403 assessments in order to identify exposure risks and improve indoor air quality in
404 industrial settings by implementing effective prevention protocols.

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534 **Figure captions**

535 Figure 1. Top: Particle number concentrations (N, 10-700 nm with DiscMini; 10-420 nm
536 with NanoScan SMPS) monitored during 3 replicas in experiment #2, using a
537 micrometric powder (Na₂O; SiO₂; CaO; P₂O₅; 1% nano) as feedstock, in the plasma
538 chamber and in outdoor air. Bottom: Particle size distribution monitored during 3
539 replicas in experiment #2. The plasma spraying activity of each replica is shown as a
540 horizontal line between grey circles.

541

542 Figure 2. Mean particle number concentrations (N) and particle diameter (D_p) inside the
543 plasma chamber for each of the experiments performed.

544

545 Figure 3. TEM images of particles collected on TEM grids inside the plasma chamber.
546 (a) spherical particles originating from evaporation of the feedstock (ZrO₂-Y₂O₃
547 nanoparticles), experiment #7; (b) release of pristine Gd-based ENPs, experiment #6;
548 (c) mineral (Ca) particles probably sourcing from the feedstock, experiment #2.

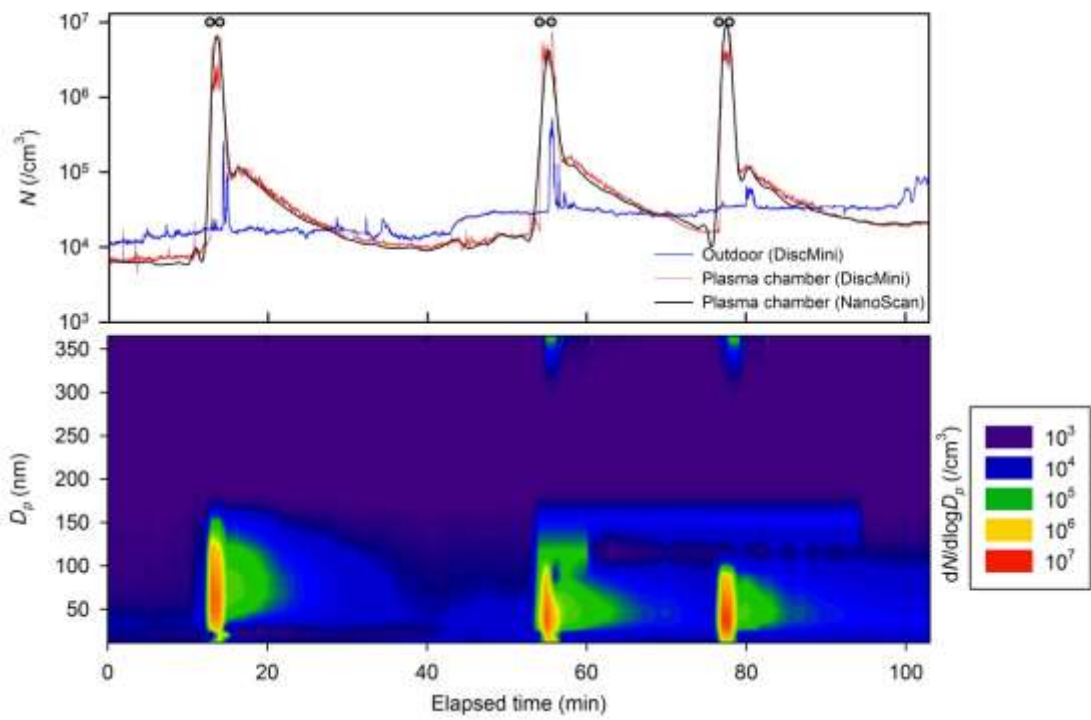
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550 Figure 4. Particle number concentrations (N, 10-700 nm with DiscMini; 4 nm to 1.5 μm
551 with CPC) monitored during one of the replicas in experiment #2, using a micro-sized
552 powder (Na₂O; SiO₂; CaO; P₂O₅; 1% nano) as feedstock. Measurements carried out in
553 the plasma chamber, in the breathing zone, and in outdoor air. The plasma spraying
554 activity is shown as a horizontal line between grey circles.

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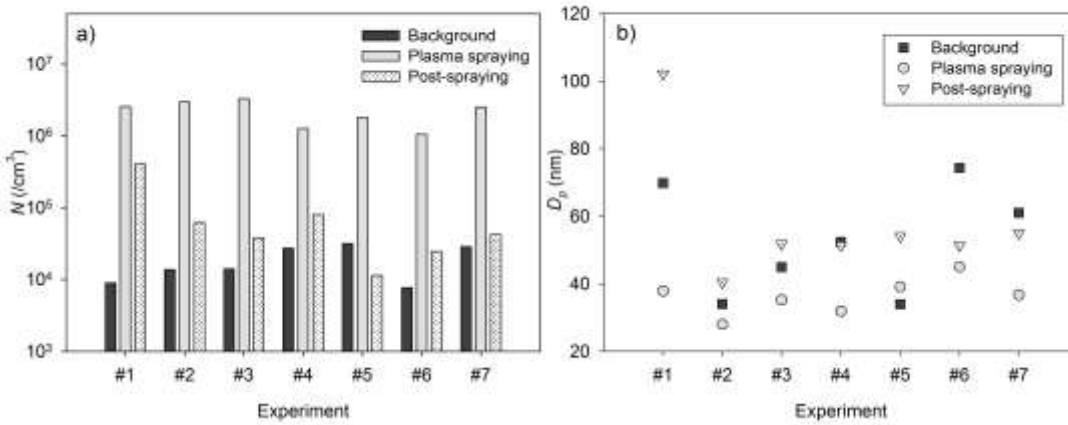
556 Figure 5. Impact of cleaning activities on particle mass concentrations (PM_{2.5}) in the
557 plasma chamber. Work activities such as plasma spraying or cleaning are shown as a
558 horizontal line between grey circles.

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561 Figure 1



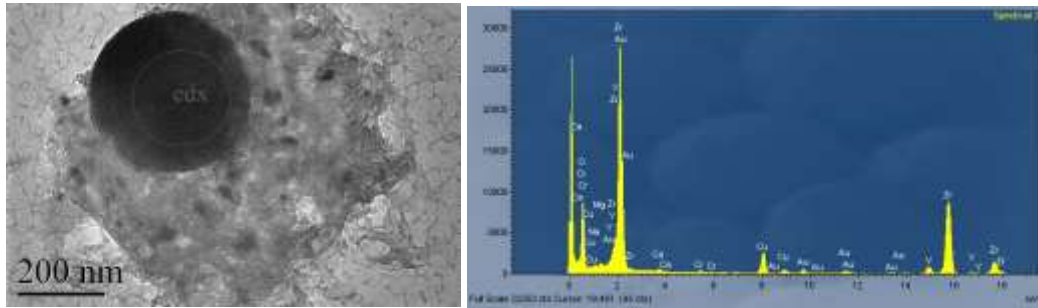
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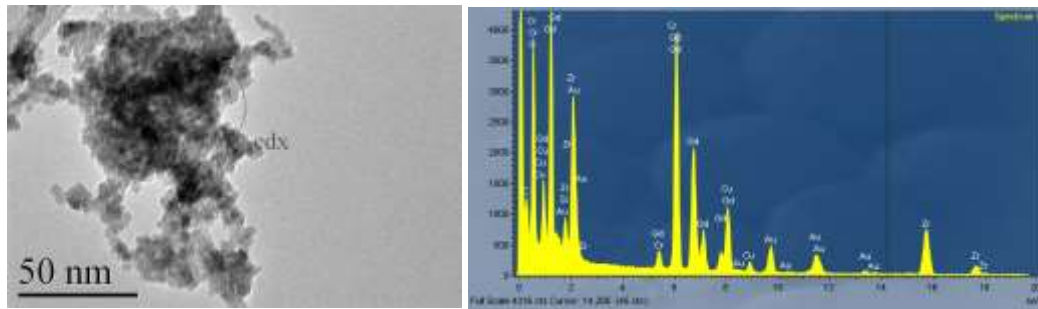
564 Figure 2

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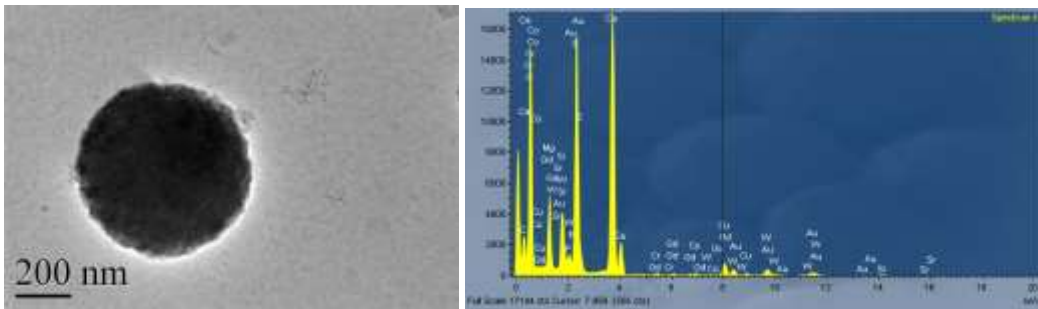
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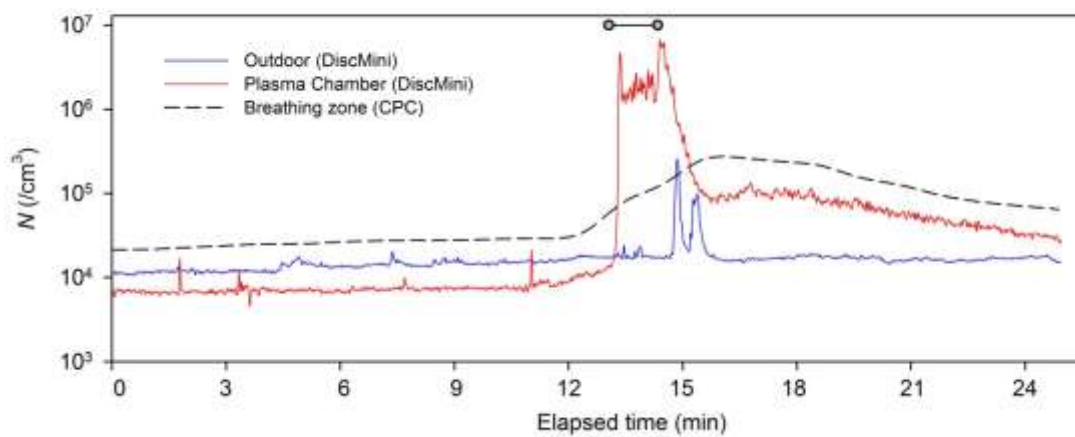


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Figure 3

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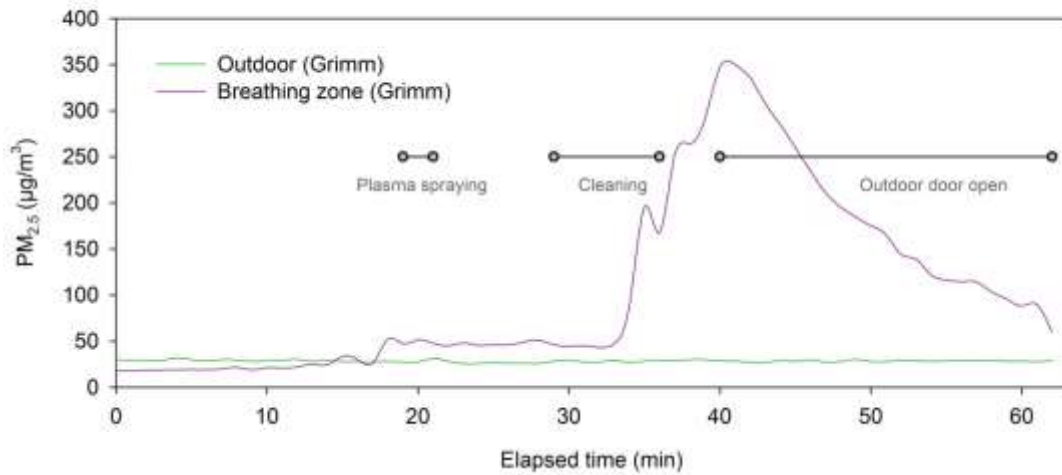


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Figure 4



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577 Figure 5

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581 Table 1. Summary of plasma spraying experiments. Experimental setup: pre- or post-mitigation
582 strategies. P: powder. S: suspension

583

Experiment (date)	Feedstock	Grain size (feedstock)	Composition	Replicas	Setup
#1 (31/10/15)	P1	Micro	Na ₂ O; SiO ₂ ; CaO; P ₂ O ₅ (1% nano)	1	Stage 0
#2 (17/12/16)	P1	Micro	Na ₂ O; SiO ₂ ; CaO; P ₂ O ₅ (1% nano)	4	Stage 1
#3 (17/12/16)	P2	Micro	NiCoCrAlTaY	1	
#4 (17/12/16)	S1	Submicro + Nano	ZrO ₂ -Y ₂ O ₃ + Gd ₂ Zr ₂ O ₇	1	Stage 2
#5 (08/01/16)	P2	Micro	NiCoCrAlTaY	3	Stage 3
#6 (08/01/16)	S2	Submicro	Gd ₂ Zr ₂ O ₇	2	
#7 (08/01/16)	S3	Nano	ZrO ₂ -Y ₂ O ₃	2	

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588 Table 2. Mean UFP number concentrations and particle diameter inside the plasma chamber and in the breathing zone for each of the experiments
 589 performed, prior to and during the spraying activity. Data not available in the breathing zone for experiments #5 to #7 due to instrumental failures.

590

Experiment	Feedstock Grain size	Setup	UFP (#/cm ³)							
			Plasma chamber				Breathing zone			
			Background		Plasma spraying		Background		Plasma spraying	
DiscMini	NanoScan	Discmini	NanoScan	DiscMini	CPC	DiscMini	CPC			
#1	Micro	Stage 0	9.0×10 ³	9.5×10 ³	2.6×10 ⁶	7.9×10 ⁵	9.8×10 ³	N/A	8.3×10 ⁵	N/A
#2	Micro	Stage 1	1.4×10 ⁴	1.6×10 ⁴	3.0×10 ⁶	2.6×10 ⁶	2.2×10 ⁴	3.3×10 ⁴	2.7×10 ⁵	2.6×10 ⁵
#3	Micro		1.4×10 ⁴	2.0×10 ⁴	3.3×10 ⁶	3.2×10 ⁶	2.8×10 ⁴	2.6×10 ⁴	7.2×10 ⁵	1.8×10 ⁵
#4	Submicro + Nano	Stage 2	2.7×10 ⁴	2.9×10 ⁴	1.3×10 ⁶	1.7×10 ⁶	2.6×10 ⁴	3.2×10 ⁴	2.9×10 ⁵	5.2×10 ⁴
#5	Micro	Stage 3	3.2×10 ⁴	N/A	1.8×10 ⁶	N/A	N/A	1.8×10 ⁴	N/A	4.4×10 ⁴
#6	Submicro		7.8×10 ³	N/A	1.1×10 ⁶	N/A	N/A	9.7×10 ³	N/A	1.9×10 ⁴
#7	Nano		2.9×10 ⁴	2.7×10 ⁴	2.5×10 ⁶	1.3×10 ⁶	N/A	N/A	N/A	N/A
			Size (nm)							
			Plasma chamber				Breathing zone			
			Background		Plasma spraying		Background		Plasma spraying	
			DiscMini	NanoScan	N Discmini	NanoScan	DiscMini	CPC	DiscMini	CPC
#1	Micro	Stage 0	70	64	38	59	61	-	47	-
#2	Micro	Stage 1	34	42	28	47	33		33	
#3	Micro		45	56	35	53	44		45	
#4	Submicro + Nano	Stage 2	52	62	32	48	52		51	
#5	Micro	Stage 3	34	N/A	39	N/A	N/A		N/A	
#6	Submicro		74	N/A	45	N/A	N/A		N/A	
#7	Nano		61	72	37	47	N/A		N/A	

591 N/A: not available

592
593 **Supporting Information**
594

595 **Determinants of workplace exposure and release of ultrafine particles during**
596 **atmospheric plasma spraying in the ceramic industry**
597

598 Viana M.¹, Fonseca A.S.², Querol X.¹, López-Lilao A.³, Carpio P.^{3,4}, Salmatonidis A.¹, Monfort
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603 Figure S1. Projection chamber (left) and worker's room (right)

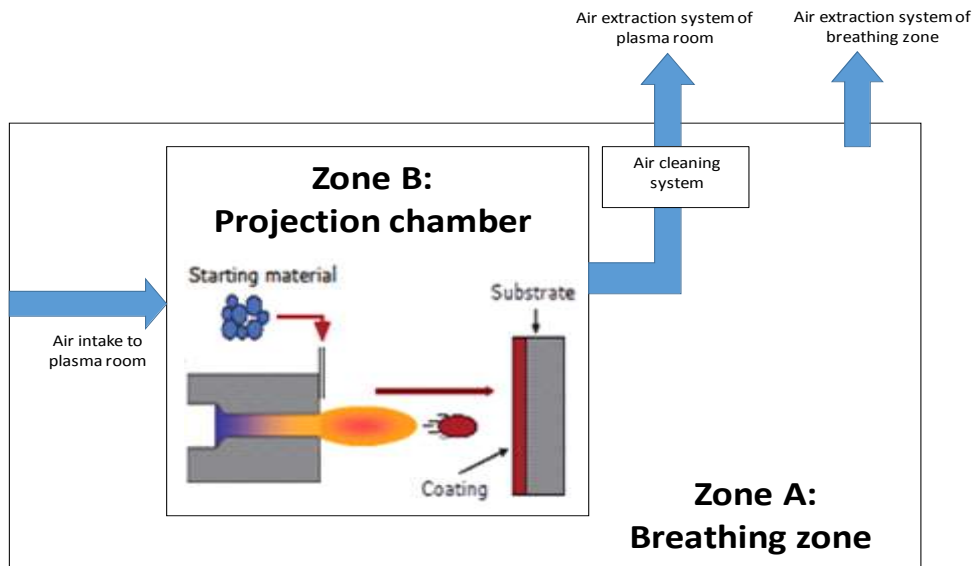
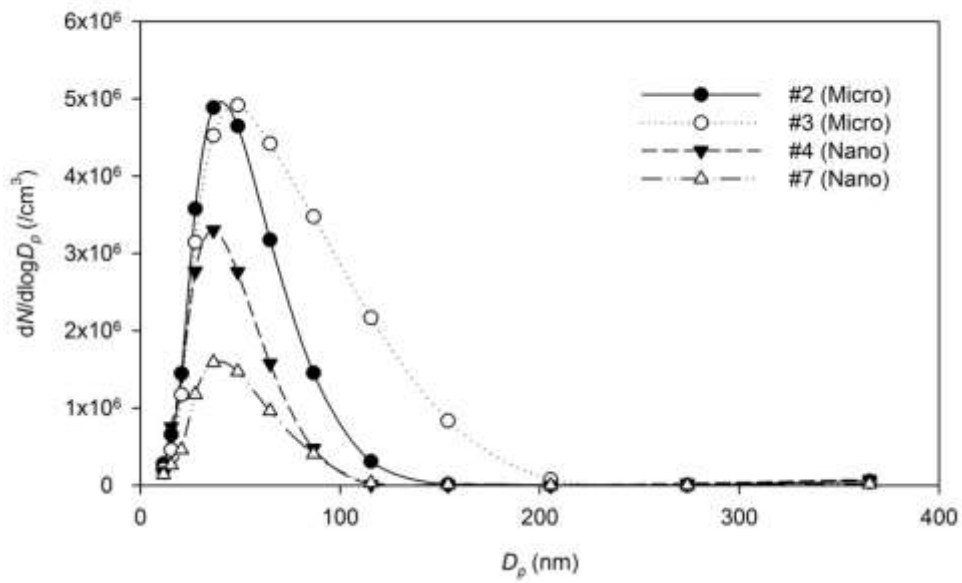


Figure S2. Scheme of plasma projection scenario.



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 607 Figure S3. Particle size distribution measured in the plasma chamber during plasma spraying
 608 activities: experiment #2 (micro size; mean obtained by 4 replicas for spraying activity),
 609 experiment #3 (micro size; 1 replica), experiments #4 (submicron- and nano-sized; 1 replica),
 610 and experiment #7 (submicron- and nano-sized; mean obtained by 2 replicas for spraying
 611 activity). Particle size distribution for experiments #5 and #6 is not available.