## Fabrication of long period fiber gratings of subnanometric bandwidth.

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This paper reports on the fabrication of long period fiber gratings having subnanometric bandwidth in the 1500 nm spectral region. Large gratings have been photo-inscribed in a high NA fiber, the grating pitch and the order of the HE cladding mode are optimized to produce gratings with a large number of periods and preventing the coupling to TE, TM or EH modes. Resonances with a FWHM of 0.83 nm and 0.68 nm have been achieved for gratings 15 and 20 cm long respectively, the free spectral range between transmission notches is 125 nm. The polarization effects and the sensitivity of the gratings to temperature and to strain variations are presented as well. © 2015 Optical Society of America

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Gratings in optical fibers are periodic modulations of the fiber structure that couple energy between different modes. They are classified in two categories, Bragg gratings (BG), which have a periodicity of half a guided wavelength [1], and long period gratings (LPG) which have a period much longer than the wavelength [2]. The former couple energy at specific wavelengths between counter propagating modes (core-core, core - cladding, cladding-cladding) [3] and also to radiation modes [4], while the latter couple energy between co-propagating modes (core-core, core-cladding) [5, 6]. The bandwidth of BGs ranges from few pm (for very large gratings) to hundreds of pm [7], however LPGs have much broader spectra because the number of periods of the gratings is much smaller; the bandwidth of LPGs in the S to L telecommunications bands ranges between several nm to a hundred nm [8, 9, 10]. The reduction of the rejection bandwidth below 1 nm is usually achieved by association of gratings in coaxial interferometric configuration or in sampled configuration [11, 12], however the individual gratings have a large bandwidth and the spectral sub-bands cannot be designed or handled independently.

There is still a need of fabricating long period fiber gratings with narrow rejection bands for core-cladding conversion, these gratings would find applications in signal processing [9, 13], DWDM components and rejection filters for telecommunications [14, 15] or multiplexing series of sensors [16]. This paper presents what is, up to our knowledge, the first demonstration of a long period grating written in an optical fiber with a 3 dB bandwidth below the frontier of 1 nm at 1527 nm and more than 100 nm of free spectral range. The paper discusses first the fabrication procedure, then the grating characteristics and finally the sensitivity to thermal and mechanical perturbations.

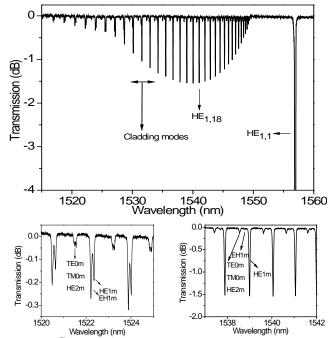
The 3 dB bandwidth of a narrowband LPG can be expressed in following forms:

$$\frac{\Delta \lambda_{3dB}}{\lambda_{res}} \approx 0.8 \frac{\lambda_{res}}{(n_{gc} - n_{gl})L} \approx \frac{0.8\Lambda}{L} = \frac{0.8}{N}$$
 (1)

Where  $\lambda_{res}$  is the coupling wavelength,  $\Lambda$  is the grating period,  $n_{gc}$ and  $n_{al}$  are the group indices of the core mode and the l-th cladding mode, L is the grating length and N is the number of periods. Since  $n_g = n_{eff} - \lambda \partial n_{eff}/\partial \lambda$ , being  $n_{eff}$  the mode effective index, one can assume that  $n_g \cong n_{eff}$  in most cases. The key for bandwidth reduction is the grating length, but fabrication of long gratings requires high precision translation stages, good laser stability and perfect fiber uniformity. The bandwidth scales with the operation wavelength, making more challenging the 1500 nm spectral region than shorter wavelength ranges. The bandwidth decreases as well with the difference of modal indices, fibers of high NA have a higher index core that results in gratings of smaller bandwidth for a given mode order. The order of the cladding mode determines the grating bandwidth as well (the index difference rises with the mode order), but the grating mode is often chosen with other criteria: the dispersion turning point of resonances, the coupling strength or the free spectral range between resonances. The dispersion at the turning point affects the bandwidth as the dispersive term included in the group index of eq. 1 states. Observe that the bandwidth can be reduced as well in conventional (low NA) fibers by using periods of few tens of μm and coupling to very high order modes [17], but very low periods reduce the distance between adjacent resonances (which is given approximately by

 $\lambda_{\text{res}I^{-}} \lambda_{\text{res}I+1} \cong (n_{\text{eff}I+1} - n_{\text{eff}I}) \Lambda)$  despite the higher index difference between modes. Furthermore very large order modes compete with unwanted modes (modes other than the  $\text{HE}_{1m}$ ) which have coupling factors comparable to adjacent  $\text{HE}_{1m}$  modes. Our approach, as it is demonstrated in the paper, overcomes those problems.

A fiber with NA=0.29 supplied by Fibercore was used in this experiment (product number SM1500-4.2/125). The fiber had a cutoff wavelength of 1387 nm, a modal field diameter of 4.2µm and an attenuation of 1.95 dB/Km at 1550 nm. A Bragg grating was written to get information about the effective indices of the cladding modes. The BG was inscribed scanning a UV beam over the fiber through a phase mask. A CW laser at 244 nm was used with a power of 83 mW, the beam was focused by a cylindrical lens and the flux of energy in the fiber core was estimated to be 160 I/mm<sup>2</sup>. The grating spectrum is shown in Fig.1. The core mode HE<sub>11</sub> is reflected at 1556.9 nm and its resonance depth exceeds -38 dB. Several couplings to cladding modes appear at shorter wavelengths, the main series of resonances have a depth of -1.7 dB around 1540 nm, this series corresponds to cladding modes HE<sub>1m</sub> and EH<sub>1m</sub> [18]. A secondary series of notches of about -0.1 dB deep appears between the notches of the main series, this series corresponds to modes TE<sub>0m</sub>, TM<sub>0m</sub> and HE<sub>2m</sub> [19, 20], these resonances usually appear in strong gratings because of the fiber imperfections or fabrication inaccuracies (i.e. core eccentricity or beam misalignment).



**Fig. 1.** Bragg grating spectrum, the vertical scale is magnified to highlight cladding modes resonances. Full wavelength range (top), detail at 1522 nm (bottom left) and detail at 1540 nm (bottom right).

The coupling to  $HE_{1m}$  and  $EH_{1m}$  modes can be resolved in the first series of resonances as it is shown in the bottom details of Fig. 1. Around 1522 nm the coupling to  $EH_{1m}$  modes is stronger than to  $HE_{1m}$  modes, however the  $EH_{1m}$  modes reduce their coupling

strength to near zero around 1540 nm while the  $HE_{1m}$  modes reach maximum coupling (see the bottom right detail of Fig. 1). No splitting is observed for the  $HE_{1m}$  resonances around 1540 nm, which indicates that other modes ( $EH_{3m}$ ,  $HE_{3m}$ ) are either quasi-degenerated or weakly coupled. The  $HE_{1m}$  modes experience a polarization dependent shift of 4 pm in the 1540 nm region (not shown in graphs) that can be due to the birefringence induced by UV radiation or to the residual birefringence of the fiber.

The effective indices of the core and cladding modes can be calculated from the resonant wavelengths of the BG assuming that the fundamental core mode has little variation in the wavelength range of the cladding modes. Although this is an approximation, it gives sufficient precision for the lowest order modes, allowing for the design of LPGs whose resonance has to lie in the spectral region of the BG resonances (this will be verified later). The refractive indices and the resonant wavelengths of  $\rm HE_{1m}$  modes are presented in Fig. 2. The index difference between the core and cladding modes is large for this particular fiber; therefore, the period of the LPGs will be short: tens of microns to couple in S or C bands.

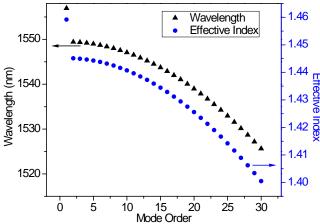


Fig. 2. Resonant wavelengths and refractive indices of HE<sub>1m</sub> modes.

The effective indices of the modes were numerically calculated by solving the Maxwell equations in a realistic fiber. This calculation allows us to make sure that the cladding resonances of lowest order ( $HE_{1,2}$  and  $HE_{1,3}$ ) have been correctly identified in Fig. 1. The results of the simulation are in good agreement with experimental data as it is shown in Fig. 3.

The maximum coupling strength corresponds to  $HE_{1m}$  modes between m=15 and m=20 as can be observed in Fig. 1. On the contrary, the relative strength of their neighboring  $EH_{1m}$  modes is much smaller; therefore, LPGs based on this set of modes ( $HE_{1,15}$  to  $HE_{1,20}$ ) will have a large free spectral range between resonances and will be less likely to present unwanted resonances caused by EH, TE or TM modes that might appear due to fabrication inaccuracies. Additionally, the  $\lambda_{res}$  versus  $\Lambda$  diagram of Fig. 3 does not show the dispersion turning point for this set of modes, therefore the resonances of the LPG will not experience the ultrawide spectral broadening that other modes of higher order could have. The free spectral range between consecutive resonances expected from Fig. 3 is larger than 100 nm.

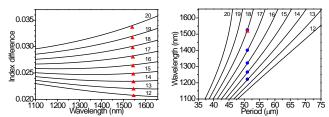
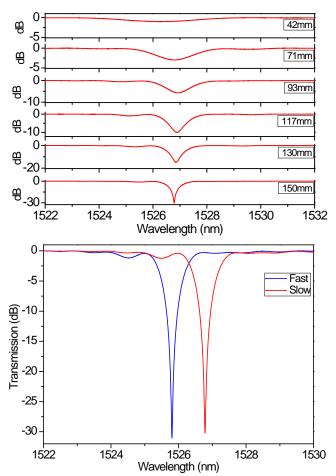


Fig. 3. Left: effective index difference between the  $HE_{11}$  mode and  $HE_{1m}$  modes for m=12 to 20 (lines: theory, dots: experimental data from BG). Right: Resonant wavelength as function of the LPG period for  $HE_{11}$  to  $HE_{1m}$  couplings for m=12 to 20 (lines: theory, triangle: expected form BG, circles: experimental data from LPG).

The LPGs of this experiment were designed to couple the mode HE<sub>1,18</sub>; thus, the grating period was set at  $\Lambda$ =51  $\mu$ m. Taking into account the indices of Fig. 2, the HE<sub>1,18</sub> mode was expected to have a resonance at 1517 nm. Mode 18 was chosen as a balance of large intermodal distance, short period (high N) and moderate slope of the  $\lambda_{res}$  versus period curve; mode 20 with shorter period would have larger free spectral range according to Fig. 3 but it might also have larger bandwidth because it is closer to the dispersion turning point (where  $\partial \lambda_{res}/\partial \Lambda = \infty$  and  $\Delta n_g = n_{gc} - n_{gl} = 0$ ). The grating was made point by point, by irradiating the fiber through a slit 25 um wide. The slit diffracts the UV beam with a far-field divergence of 19.5 mrad, the fiber core lies in Fresnel's diffraction zone. The UV beam was again focused along the fiber axis with a cylindrical lens and its power was 57mW; half a period of the grating was irradiated for a lapse of time of 1000 ms with a flux of energy of 1.5 J/mm<sup>2</sup>, the second half of the period was quickly scanned in about 10 ms. The scan process was controlled by an encoded motor from Physik Instrumente (product M525.22).

The grating growth was monitored during fabrication: the transmission notch as a function of the grating length is shown in Fig. 4. A super-luminescent diode partially polarized was used as light source, light was polarized by an external polarizer with an extinction ratio of 35 dB at 1550 nm. The polarization state had to be carefully adjusted during the grating inscription: the spectral notch is broad when the grating is short and the polarization dependency is undistinguishable; however, when the notch depth exceeds 3 dB, two close transmission notches that correspond to the slow and fast axes of the fiber can be distinguished and the polarization has to be matched to one of them in order to adjust the grating length for optimum coupling. The resulting grating was 150 mm in length.

The grating presents two transmission notches that correspond to the slow and fast axis of the fiber, each resonance has a 3 dB bandwidth of 0.83 nm. The upper band is centered at 1526.78 nm and has a depth of -30.2 dB, the lower band is shifted 0.97 nm and has a depth of -30.9 dB. The spectra were measured with a resolution of 18 pm and the bottom of the notches is well resolved. The insertion loss of the grating measured out of the band is less than 0.1 dB. The suppressed bands have sidelobes -1.2 dB deep, their asymmetry indicates an uneven chirp in the grating. The bandwidth expected from equation 1 is 0.42 nm, the discrepancy is discussed later. The resonant wavelengths of the LPG are 0.7 % higher than expected from the refractive indices of the BG in Fig.2, notice that the LPG was made with lower UV energy and it has smaller average index than the BG, hence, shorter resonant wavelength.



**Fig. 4.** LPG spectrum as function of the grating length (top). Polarization dependency for 150 mm length (bottom).

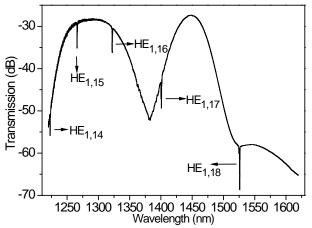


Fig. 5. Spectrum showing resonances of different cladding modes.

After fabrication, the LPGs spectrum was measured in a span of 400 nm to identify couplings to other modes, see Fig. 5. The closest resonance appears at 1400.7 nm and corresponds to mode  $\rm HE_{1,17}$  in good agreement with predictions from Fig. 3. No sign of coupling to  $\rm EH_{1m}$ ,  $\rm HE_{2m}$ ,  $\rm TM_{0m}$  or  $\rm TE_{0m}$  was observed between consecutive

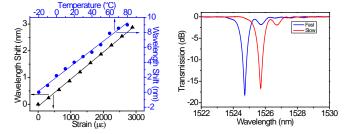
HE resonances; consequently the LPG has a free spectral range of 125 nm available for wavelength multiplexing. The bottom of the resonances in Fig. 5 is not well resolved because the set of diodes used as light source was partially polarized.

We have also written strong gratings impinging the UV beam at a small angle with respect to the fiber axis, the resulting asymmetric LPGs present an additional resonance located 1 nm below the fundamental  $\text{HE}_{1,18}$  resonance; we believe this closest resonance corresponds to a mode  $\text{HE}_{3m}$  which is almost degenerated with the  $\text{HE}_{1,18}$  [19, 20]. It was as well observed in gratings fabricated with different UV powers that the spectral separation between polarization bands remains unalterable, this indicates that polarization splitting is due to the intrinsic birefringence of the fiber rather than induced by the UV radiation (at least for the energy levels of our experiments).

The sensitivity of the LPG to temperature and axial strain was measured after annealing the grating at 90  $^{\circ}$ C for 24h in order to stabilize the refractive index profile photoinduced in the fiber during the grating fabrication. As it is shown in Fig. 6 (left), the sensitivities of this resonance are 91 pm/ $^{\circ}$ C and 1.0 pm/ $^{\circ}$ E.

As it has been commented before, the LPGs have an unwanted chirp due to fabrication inaccuracies. We have identified three causes of error: (1) the stability of the room temperature, (2) the fluctuations of the UV power (laser power or the spatial beam stability) and (3) the axial uniformity of the pristine fiber. A temperature variation of  $\pm 1\,^{0}$ C results in a variation of the resonant wavelength of  $\pm 90\,$  pm. The refractive index modulation of the grating was estimated to be  $2.3\times10^{-5}$ ; assuming a linear dependence on the UV power, a variation of  $\pm 2\,$  mW results in a chirp of  $\pm 40\,$  pm. Furthermore, short pieces of fiber have a random variation of the core radius and refractive indices [21]; these irregularities could change the difference between effective indices up to  $10^{-6}$ , and this random variation results in a chirp of  $\pm 50\,$ pm. The overall effect is an rms error of  $\pm 110\,$  pm along the grating.

Because of this random chirp, the quality of the gratings worsens as the bandwidth is reduced. As an example, we show in Fig. 6 (right) the spectrum of a 200 mm long grating. The spectral bandwidth is 0.68 nm and 0.70 nm for the fast and slow axis; however, the sidelobes are -1.8 dB and -1.9 dB deep and the resonances have -18.0 dB and -16.7 dB for the two polarizations. Attempts to increase the coupling of this grating were made, but we found systematically that sidelobes grew further and invaded the main resonance broadening the spectrum.



**Fig. 6.** Left: LPG response to temperature and strain (lines: linear fit). Right: Spectrum of a 200 mm length LPG. The 3dB bandwidths are  $0.68 \, \text{nm}$  and  $0.70 \, \text{nm}$  for the fast and slow axis.

In summary, we have demonstrated narrowband LPGs fabricated using a high NA fiber whose core and cladding modes have differences between effective indices larger than those of low NA fibers. The period of the gratings is short in this kind of fiber, hence the number of periods for given length is higher; and, as a result, the bandwidth is reduced. Bandwidths of 0.83 nm have been achieved in 15 cm long gratings which have excellent spectral quality; the bandwidth has been reduced to 0.68 nm in gratings 20 cm long, but the spectral quality is slightly poorer. The spectrum has a free spectral range of 125 nm and the suppressed band is polarization split into two bands 0.97 nm apart. The resonance corresponding to the HE<sub>1,18</sub> mode has sensitivities to temperature and strain of 91 pm/°C and 1.0 pm/µs. The main limitations for further improvement are the stability of the UV beam and the room temperature during fabrication, as well as the quality of the pristine fiber.

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