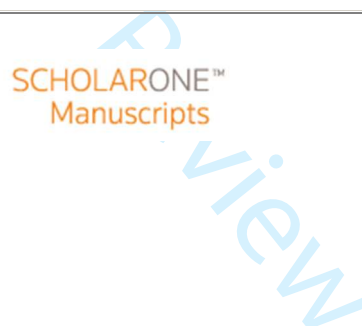


## Towards acoustic condition monitoring for detection and characterisation of laser induced breakdown in a gas turbine laser ignition system

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Keyword:	Condition monitoring, Lasers, Acoustic emission methods (AE)



1 **Towards acoustic condition monitoring for detection and**  
2 **characterisation of laser induced breakdown in a gas turbine**  
3 **laser ignition system**

4

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15

16 **ABSTRACT:**

17 Acoustic detection and characterisation of laser induced breakdown is an attractive  
18 proposition in laser ignition systems in which condition monitoring is necessary but  
19 where optical access for monitoring purposes is impractical. Presented is a signal  
20 processing method based on wavelet decomposition for the non-invasive detection  
21 of acoustic emissions resulting from laser induced breakdown in an atmospheric  
22 pressure combustion test rig, representative of a single combustion chamber in a sub  
23 15 MW industrial gas turbine. The probability and consistency of laser induced  
24 breakdown is determined from the acoustic signal and used to characterize the  
25 operating conditions and identify abrupt and incipient or slowly developing faults.

26

27 **KEYWORDS:**

28 Lasers; Condition monitoring; Acoustic emission methods (AE)

29

30

31 **1. INTRODUCTION**

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1 Laser ignition (LI) offers the potential to address the durability issues associated with  
2 conventional high energy electrical ignition systems by removing the ignition  
3 apparatus from the hot gas path [1,2]. LI typically utilizes tightly focussed visible to  
4 near infrared nanosecond pulsed laser radiation to induce optical breakdown in  
5 combustible mixtures *via* a multi-photon ionization process for the purpose of  
6 initiating combustion [3,4]. In this process, multi-photon ionization of atoms in the  
7 target medium results in the release of electrons which readily absorb more  
8 photons, thereby increasing their kinetic energy. Subsequent collision of these  
9 electrons with neighbouring electrons results in avalanche ionization and the  
10 generation of a plasma in the focal region.

11  
12 Condition monitoring is essential to the development of an LI system for gas  
13 turbines. Unsatisfactory operation of the LI system may be indicative of an incipient  
14 or slowly developing fault such as damage to optical elements in the beam path or  
15 an abrupt fault such as failure of a light guide. Both of the aforementioned fault  
16 types would require the activation of an interlock which is capable of reliably  
17 reducing the beam strength to safe levels within eye protection delay times, as  
18 defined in IEC 60825-2 [5]. Due to the nature of the application and associated  
19 hardware, there is limited optical access to the combustion chamber, making the  
20 effective use of optical means of condition monitoring impractical. There is potential  
21 for use of acoustic emissions to monitor the LI process, as has been applied to laser  
22 peening in recent years, a process with many similarities to LI [9,10]. A component of  
23 the energy within the plasma generated as a result of the multi-photon ionization  
24 process manifests itself as an acoustic emission in the audible frequency range. This  
25 is the result of a shockwave which is formed and expands around the plasma.  
26 Initially, expansion of this shockwave is driven by the high temperature plasma,  
27 whose energy increases due to absorption of laser radiation during the laser pulse  
28 [6]. After the laser pulse ends the temperature of the plasma reduces, resulting in a  
29 deceleration in the expansion of the shockwave. From this point, the blast wave  
30 model of Jones can be employed to describe the propagation of the shockwave into  
31 the acoustic region [7,8].

32

1 The principal challenge in the development of an acoustic emission based condition  
2 monitoring system for detection and characterisation of laser induced breakdown  
3 concerns resolving the acoustic emissions of interest in the relatively noisy  
4 environment associated with engine operation [11]. Relatively little literature exists  
5 concerning detection of acoustic emissions that result from laser induced  
6 breakdown. Yaacob *et al.* proposed utilising changes in the refractive index of  
7 multimode optical fibres to detect acoustic emissions resulting from laser induced  
8 breakdown in isolation oil [12]. It was shown that this method produced a noise free  
9 signal which required no signal processing. The linear dependence of acoustic  
10 pressure on laser pulse energy for optical breakdown in water was characterized by  
11 Bulanov *et al.* using a hydrophone and acoustic receiver [13]. Krasnenko *et al.*  
12 studied the sound generation in the atmosphere resulting from optical breakdown in  
13 aerosol sprays using a microphone, with a view to its practical application as a  
14 diagnostic tool for the influence of atmospheric conditions on laser induced  
15 breakdown regimes [14]. Hosoya *et al.* studied the time responses of sound pressure  
16 generated by laser induced breakdown in air in an anechoic box [15]. The acoustic  
17 signals resembled impulse responses, characterised by a high peak pressures, and  
18 were found to be highly reproducible in terms of pulse width and peak pressure. This  
19 reproducibility was attributed to the consistency of the laser as a source. No  
20 literature exists regarding detection of acoustic emissions from optical breakdown  
21 events in noisy environments associated with engine operation which are typical in  
22 LI applications.

23

24 Proposed in this study is a new approach to the condition monitoring of an LI system  
25 in realistic, engine-like environments. Information regarding the probability and  
26 consistency of laser induced breakdown is discerned from associated acoustic  
27 emissions using wavelet decomposition; a signal processing methodology which is  
28 uniquely suited to the extraction of impulse-like features heavily masked by noise.

29 The results of this investigation reveal significant potential for the practical  
30 application of acoustic-based condition monitoring techniques in LI systems.

31

32 **2. METHODOLOGY**

1 In this section, details of the experimental arrangement used to record acoustic  
2 signals are given followed by a description of the signal processing technique used to  
3 analyse the data.

4

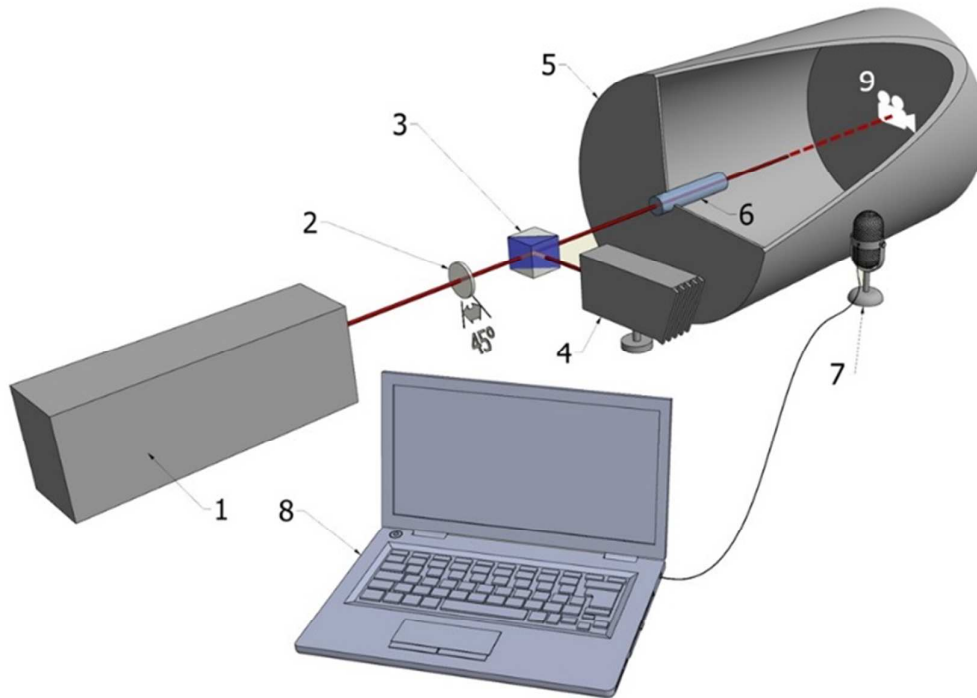
## 5 **2.1 Experimental arrangement**

6 An atmospheric pressure combustion test rig was utilized in this study, which could  
7 be fitted with a single combustor can from a range of Siemens industrial gas  
8 turbines. For the purpose of this investigation, the rig was fitted with a combustion  
9 can and pilot burner from a small to medium (that is, sub 15 MW output power)  
10 Siemens industrial gas turbine.

11

12 A laser ignition system was developed utilizing a Q-switched Nd:YAG TEM<sub>00</sub> laser  
13 (Brilliant; Quantel, Ltd.) with an M<sup>2</sup> of 1.84, pulse duration of 4 ns and operating at  
14 10 Hz repetition rate and 1064 nm wavelength. The output pulse energy ( $E_p$ ) of the  
15 laser source was limited from its maximum of 360 mJ to approximately 21 mJ using  
16 by flashlamp/Q-switch delay time to avoid damage to optical elements in the  
17 system. With the flashlamp/Q-switch delay kept constant, a polarization based  
18 optical attenuator consisting of a ½ wave plate and polarizing beam splitting cube  
19 was used to control the laser pulse energy. The laser pulse energy for a given ½ wave  
20 plate rotation was measured (UP19K-VR; Gentec Electro-Optics, Inc.) and averaged  
21 over 100 pulses. The experimental arrangement is shown in Figure 1.

22

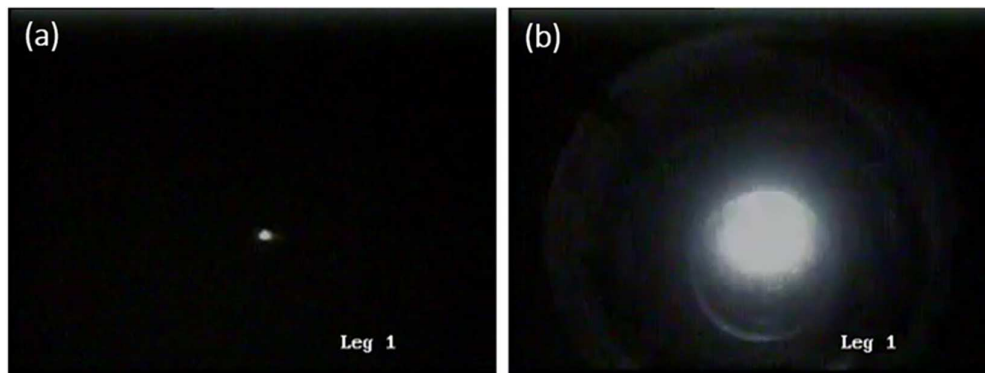


1  
 2 **Figure 1: Experimental arrangement with 1) laser source, 2)  $\frac{1}{2}$  wave plate, 3) polarizing beam**  
 3 **splitting cube, 4) beam dump, 5) combustion chamber, 6) laser igniter assembly, 7) microphone, 8)**  
 4 **data acquisition computer and 9) camera.**

5  
 6 A custom laser igniter assembly was utilized, consisting of a clear aperture for  
 7 transmission of the laser beam, a plano-convex focusing optic with an effective focal  
 8 length of 27 mm and an anti-reflective coated N-BK7 output window. The optical  
 9 path length from the laser source to the igniter assembly was approximately 3 m.  
 10 The tip of the igniter assembly was sealed with red silicone around the edge of the  
 11 output window.

12  
 13 **The presence or otherwise of laser induced breakdown within the combustion**  
 14 **chamber could be verified by monitoring the camera feed.** Figure 2 shows the  
 15 camera feed for both flashlamp operation and laser induced breakdown.

16



1  
2 **Figure 2: Camera feed showing (a) flashlamp operation and (b) laser induced breakdown (10 Hz**  
3 **repetition rate, 1064 nm wavelength).**

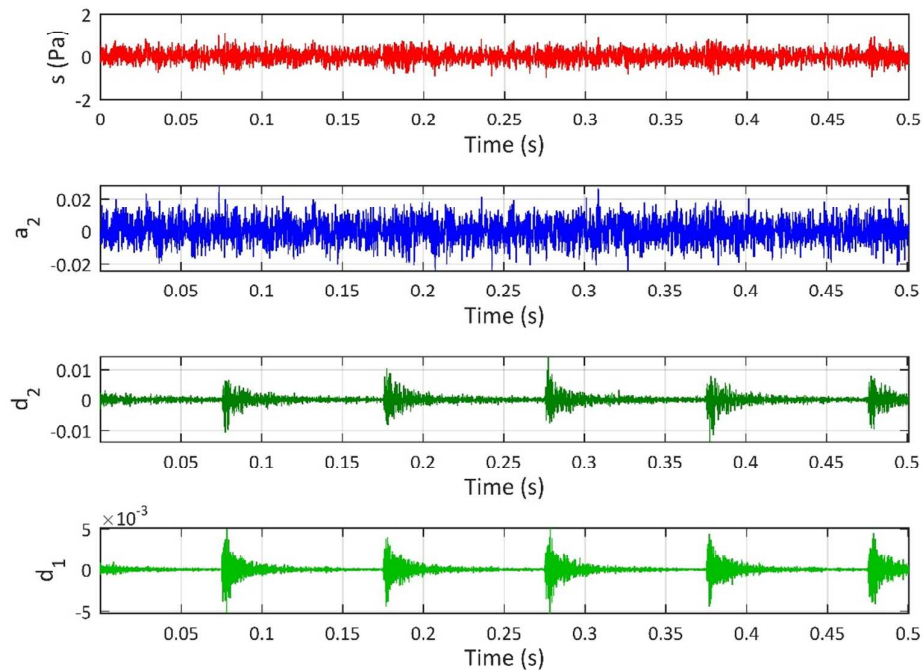
4  
5 A condenser microphone (AT2020, Audio-Technica Ltd.) with a frequency response  
6 of 0.02 to 20 kHz was used to capture the acoustic signal, which was sampled  
7 directly using MATLAB at 48 kHz and 16-bit resolution. The sensor was placed  
8 approximately 2 cm from the combustion chamber's external casing with the  
9 sensitive plane aimed directly at the casing wall. In this investigation, the ambient  
10 conditions were such that no additional steps were required to reduce wind noise on  
11 the microphone.

## 13 **2.2 Signal processing methodology**

14 The signal processing work focused on acoustic identification of laser induced  
15 breakdown in an atmospheric pressure combustion test rig, representative of an  
16 industrial gas turbine during its start-up procedure. Audio recordings of 11 s in  
17 duration were repeated ten times for a given set of experiment parameters. The raw  
18 acoustic signal was sampled and imported directly into MATLAB. Each signal was  
19 clipped to a length of 10 s to remove unwanted artefacts from the beginning and  
20 end of the recording and then processed by two level wavelet decomposition,  
21 allowing for the resolution of information in both the time and frequency domains.  
22 Wavelet decomposition was chosen on the basis of both its sensitivity to abrupt  
23 changes in frequency in the time domain and its computational efficiency. The base  
24 wavelet best capable of resolving the laser induced breakdown events was selected  
25 using energy to Shannon entropy ratio at the first level of decomposition as the  
26 criterion [16]. A total of 131 base wavelet types from the wavelet families

1 Daubechies, symlets, coiflets, biorthogonal, Fejer-Korovkin and reverse biorthogonal  
 2 were considered, with the base wavelet producing the maximum energy to Shannon  
 3 entropy ratio selected as the most appropriate wavelet; in this case, the  
 4 biorthogonal (Bior6.8) wavelet. The wavelet decomposition produced three sets of  
 5 coefficients, representing the approximation of the signal at low frequencies ( $a_1$ ) and  
 6 the detail of the signal at high frequencies ( $d_1$  and  $d_2$ ). Where present, laser induced  
 7 breakdown events are clearly visible at the first level of decomposition in the detail  
 8 coefficients  $d_1$ , as shown in Figure 3 for raw acoustic signal  $s$ , representing consistent  
 9 laser induced breakdown in an atmospheric pressure combustion test rig. As such,  
 10 the  $d_1$  coefficients (henceforth referred to as the detail signal) were extracted for  
 11 further processing.

12



13

14 **Figure 3: Two level Bior6.8 wavelet decomposition of raw acoustic sound pressure signal  $s$  with**  
 15 **approximation coefficients  $a_2$ , and detail coefficients  $d_1$  and  $d_2$  (21 mJ pulse energy, 10 Hz repetition**  
 16 **rate, 1064 nm wavelength).**

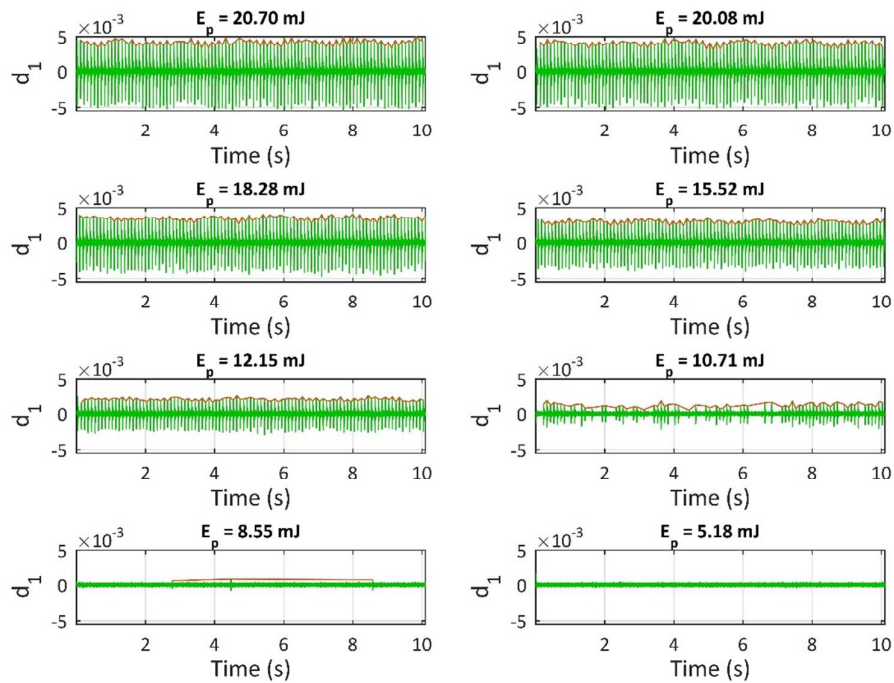
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### 18 **3 RESULTS AND DISCUSSION**



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1 The experimental work focused on (i) identification of abrupt faults and (ii)  
2 identification of incipient or slowly developing faults in a gas turbine laser ignition  
3 system. Acoustic signals were recorded during operation of the laser ignition system  
4 on an atmospheric pressure combustion test rig with a constant air mass flow rate of  
5 0.4 kg/s. It should be noted that this intake of air into the combustion chamber was  
6 the main source of noise when the test rig was in operation. Operation of intake and  
7 exhaust fans also contributed to the noise. No fuel was introduced into the  
8 combustion chamber in this investigation. This effectively recreates the conditions at  
9 the point in the turbine start-up procedure at which the laser ignition system would  
10 be fired for condition monitoring purposes. The acoustic signals were subsequently  
11 processed according to the methodology outlined in Section 2.2. To simulate  
12 unsatisfactory operation of the laser ignition system, the laser pulse energy ( $E_p$ ) was  
13 increased from a minimum to the maximum pulse energy used in this investigation  
14 of 21 mJ by rotating the  $\frac{1}{2}$  wave plate in the experimental arrangement depicted in  
15 Figure 1. A peak detection algorithm was applied to the detail signal to determine  
16 the probability of laser induced breakdown as a function of laser pulses fired over a  
17 given period of time, a representative output of which is shown in Figure 4. The  
18 threshold above which the signal was considered to be a peak was dictated by the  
19 maximum and minimum amplitude values for the detail signal at the first level of  
20 decomposition for an ambient acoustic signal, recorded with test rig in operation  
21 and the laser flashlamps on. The peak-to-peak separation was restricted using a  
22 windowing function in accordance with the 10 Hz repetition rate of the laser source.  
23



1

2 **Figure 4: Representative outputs from the peak detection algorithm applied to the detail signal for**  
 3 **a single 10 s audio recording (10 Hz repetition rate, 1064 nm wavelength).**

4

5 Figure 4 reveals the presence of three distinct energy regions as the pulse energy is  
 6 increased. At an incident pulse energy of 5.18 mJ no laser induced breakdown  
 7 occurred. A second region was observed for incident pulse energies of 8.55 mJ and  
 8 10.71 mJ, characterized by inconsistent laser induced breakdown with a probability  
 9 of 2.7% and 64.6%, respectively. Optical breakdown can only occur when the  
 10 incident laser radiation is above a threshold value; therefore, for pulse energies close  
 11 to this threshold value as opposed to those well in excess of it, a statistically smaller  
 12 fraction of the laser pulse is capable of causing optical breakdown, resulting in a  
 13 reduced probability of laser induced breakdown [17]. A third region of consistent  
 14 laser induced breakdown was observed for incident pulse energies in excess of 12.15  
 15 mJ, in accordance with observations made by Chen *et. al* [18]. **The presence of these**  
 16 **three distinct energy regions was confirmed by reviewing the recorded camera feed.**

17

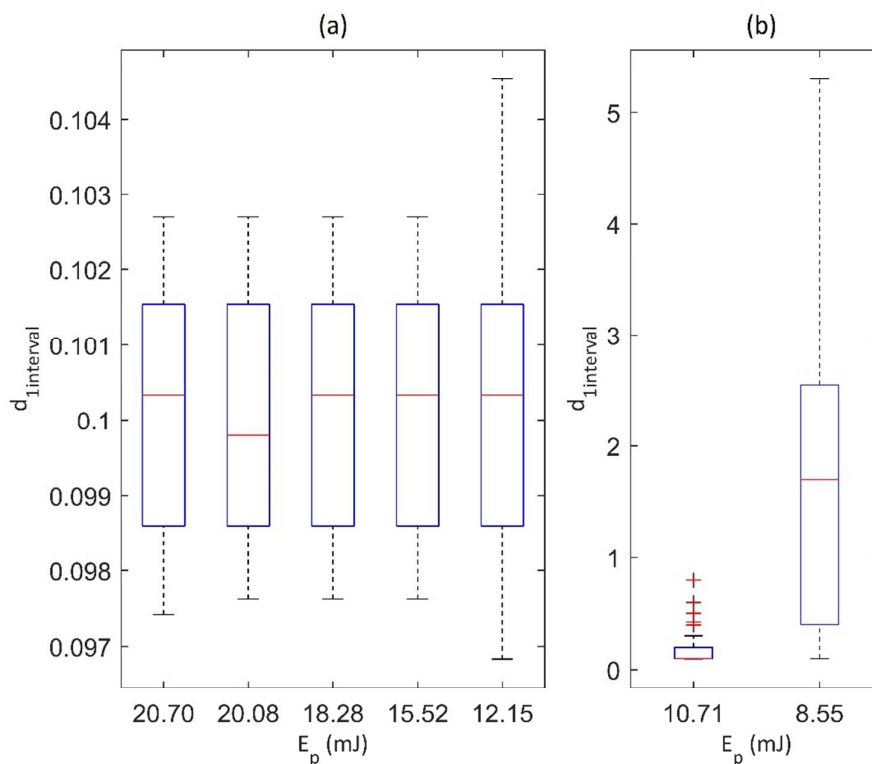
1 In addition to the probability of laser induced breakdown, information relating to the  
 2 consistency of laser induced breakdown can be inferred from the detail signal. The  
 3 following sections detail methods for the identification of abrupt and incipient or  
 4 slowly developing faults from this information.

5

### 6 **3.1 Abrupt fault detection**

7 An abrupt fault would result in unsatisfactory operation of the laser ignition system  
 8 immediately after the fault develops. Possible causes for such a fault may include  
 9 misalignment, severe damage to an optical element in the beam path or failure of  
 10 the laser source to operate correctly. In the event of an abrupt fault, inconsistent or  
 11 no laser induced breakdown will occur. As such, the time interval between the peaks  
 12 detected in the detail signal is a useful parameter to consider. Figure 5 presents a  
 13 box plot of the peak intervals for those incident pulse energies which resulted in  
 14 laser induced breakdown.

15



16

17 **Figure 5: Box plot of the peak intervals ( $d_{\text{interval}}$ ) from the peak detection algorithm applied to the**  
 18 **detail signals in (a) the consistent laser induced breakdown region and (b) the inconsistent laser**  
 19 **induced breakdown region (10 Hz repetition rate, 1064 nm wavelength).**

1

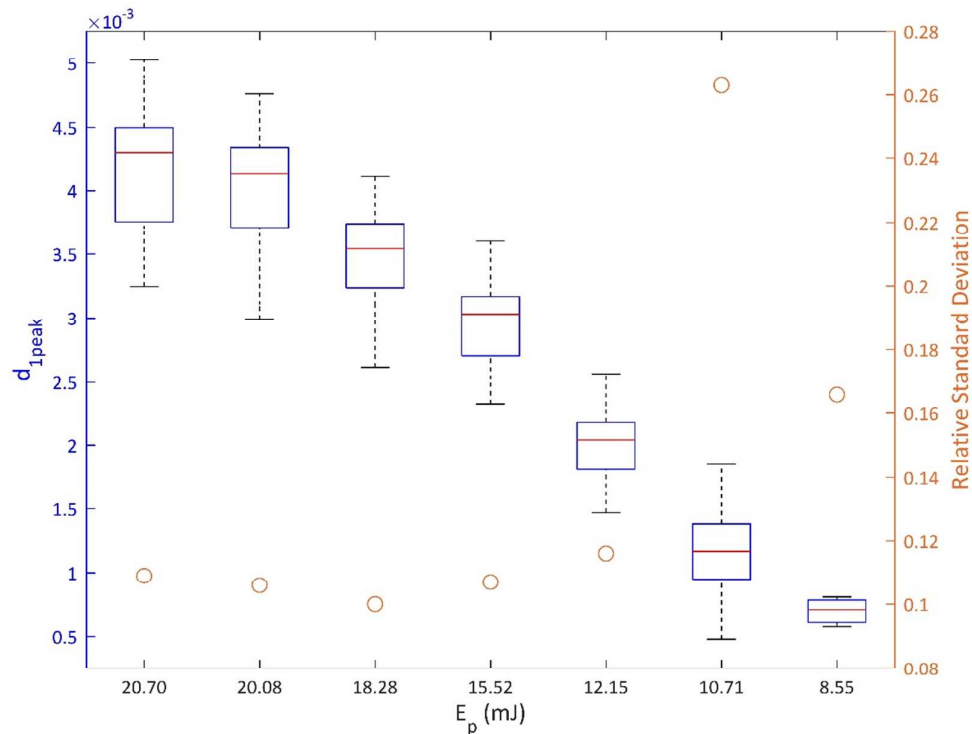
2 Referring to Figure 5, for incident pulse energies in excess of 12.15 mJ (that is, in the  
3 consistent laser induced breakdown region) the peak intervals are centred on 0.1 s,  
4 corresponding to the 10 Hz repetition rate of the laser source. As the incident pulse  
5 energy decreases to 10.71 mJ and 8.55 mJ the median interval and distribution both  
6 increase. This can be attributed to increasingly inconsistent spark formation as the  
7 incident pulse energy decreases, therefore reducing the number of breakdown  
8 events detected.

9

### 10 **3.2 Incipient fault detection**

11 An incipient or slowly developing fault may result in unsatisfactory operation of the  
12 laser ignition system at some point after the fault initially develops. A possible cause  
13 for such a fault could be slight damage to an optical element in the beam path,  
14 acting as a nucleation point for further damage upon successive irradiation. In the  
15 event of an incipient fault occurring, it is important to identify and rectify the  
16 underlying issue as it can eventually lead to inconsistent laser induced breakdown  
17 and therefore unsatisfactory operation of the laser ignition system. Figure 6 shows  
18 the distribution of the absolute value of peak amplitudes as a function of incident  
19 pulse energy.

20



1

2 **Figure 6: Box plot of absolute values of peak amplitude from the peak detection algorithm applied**  
 3 **to the detail signal ( $d_{1peak}$ ) and their relative standard deviation (circles) as a function of incident**  
 4 **pulse energy (10 Hz repetition rate, 1064 nm wavelength).**

5

6 Figure 6 reveals a decrease in the median absolute value of peak amplitude with  
 7 decreasing incident pulse energy, following a sigmoidal trend. In the consistent laser  
 8 induced breakdown region (that is, at incident pulse energies of 12.15 mJ and above)  
 9 there is also a narrowing of the distribution with decreasing incident pulse energy.

10 This narrowing can be attributed to the decrease in magnitude of the individual peak  
 11 amplitudes as less energy is deposited in the shock wave. As such, this narrowing is  
 12 not reflected in the relative standard deviation, which remains consistent in this  
 13 region. The transition from consistent to inconsistent laser induced breakdown is  
 14 characterized by an abrupt increase in the relative standard deviation at an incident  
 15 pulse energy of 10.71 mJ, corresponding to a breakdown probability of 64.6%. Long  
 16 term monitoring (that is, at every start-up sequence for the turbine) of the absolute  
 17 value of peak amplitude could be used to monitor for the sigmoidal trend shown in  
 18 Figure 6, indicative of an incipient or slowly developing fault.

19

#### 1    **4        CONCLUSIONS**

2    Noise robust acoustic condition monitoring for detection and characterisation of  
3    laser induced breakdown in a laser ignition system has been demonstrated. Acoustic  
4    detection of laser induced breakdown events under realistic engine-like conditions  
5    was achieved through use of a signal processing method based on wavelet  
6    decomposition using a Bior6.8 mother wavelet and extraction of the detail  
7    coefficients at the first level of decomposition as a de-noised signal.

8

9    The potential for the implementation of an acoustic sensor system for condition  
10    monitoring of a gas turbine laser ignition system has been clearly demonstrated. A  
11    peak detection algorithm was applied to determine the probability of laser induced  
12    breakdown as a function of laser pulses fired over a given period of time.

13    Information relating to the consistency of laser induced breakdown was then used to  
14    identify abrupt and incipient or slowly developing faults, simulated by decreasing the  
15    incident pulse energy. The time interval between peaks was shown to increase from  
16    a base of 0.1 s corresponding to the repetition rate of the laser as the energy region  
17    transitioned from consistent to inconsistent laser induced breakdown with  
18    decreasing incident pulse energy, indicative of an abrupt fault. The absolute value of  
19    peak amplitude was shown to decrease with decreasing incident pulse energy,  
20    following a sigmoidal trend which could be used to identify insipient faults. Further  
21    work is required to address the instrumentation and integration challenges  
22    associated with development of a real-time acoustic condition monitoring system for  
23    gas turbine laser ignition systems.

24

#### 25    **ACKNOWLEDGEMENTS:**

26

27    The authors would like to thank Siemens Industrial Turbomachinery Ltd (SITL) for  
28    funding this investigation as part of a wider investigation into laser ignition for gas  
29    turbines.

30

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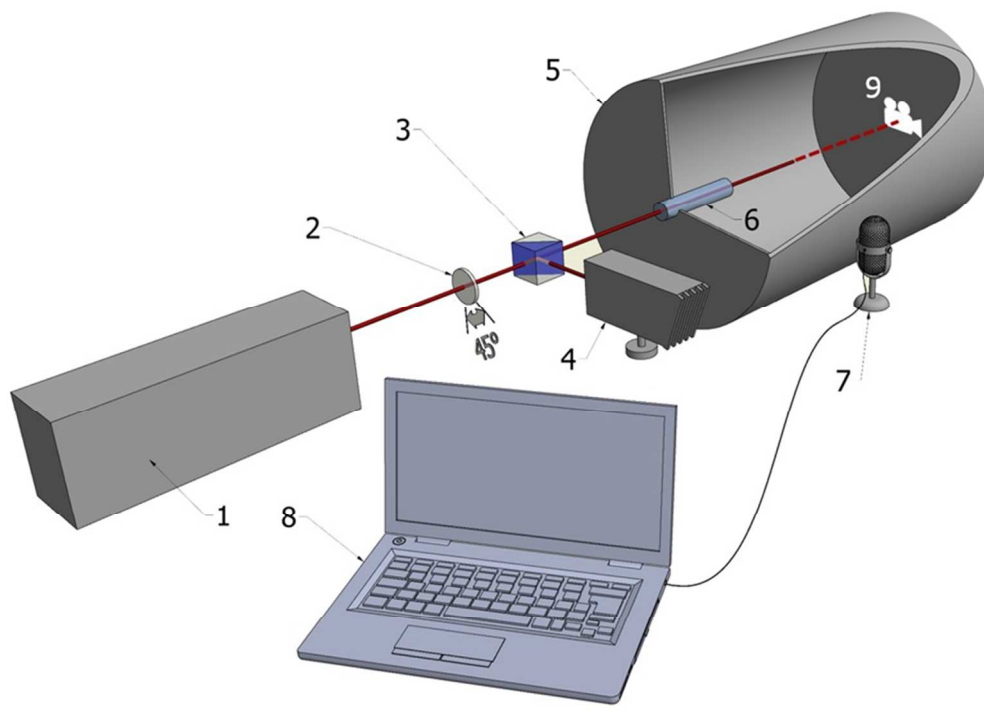


Figure 1: Experimental arrangement with 1) laser source, 2)  $\frac{1}{2}$  wave plate, 3) polarizing beam splitting cube, 4) beam dump, 5) combustion chamber, 6) laser igniter assembly, 7) microphone, 8) data acquisition computer and 9) camera.

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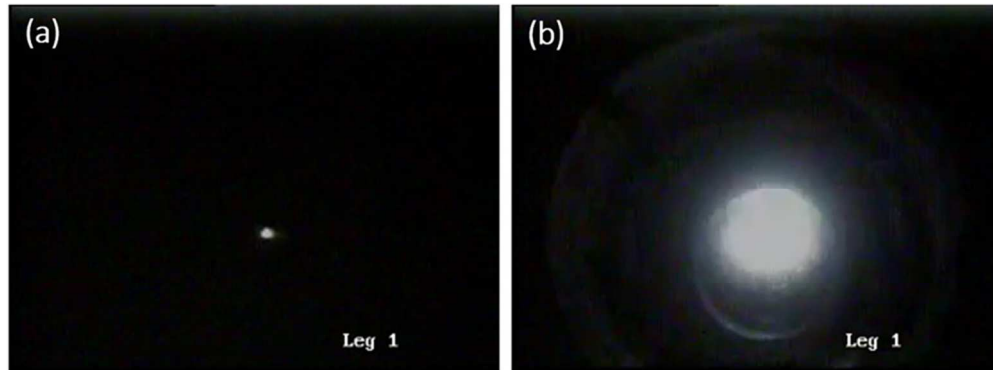


Figure 2: Camera feed showing (a) flashlamp operation and (b) laser induced breakdown (10 Hz repetition rate, 1064 nm wavelength).

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Peer Review

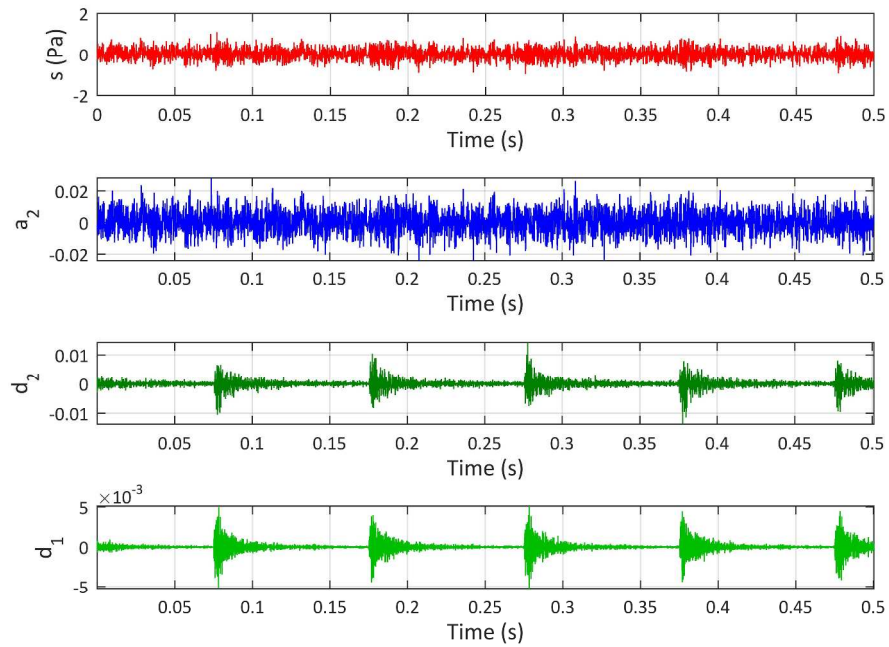


Figure 3: Two level Bior6.8 wavelet decomposition of raw acoustic sound pressure signal  $s$  with approximation coefficients  $a_2$ , and detail coefficients  $d_1$  and  $d_2$  (21 mJ pulse energy, 10 Hz repetition rate, 1064 nm wavelength).

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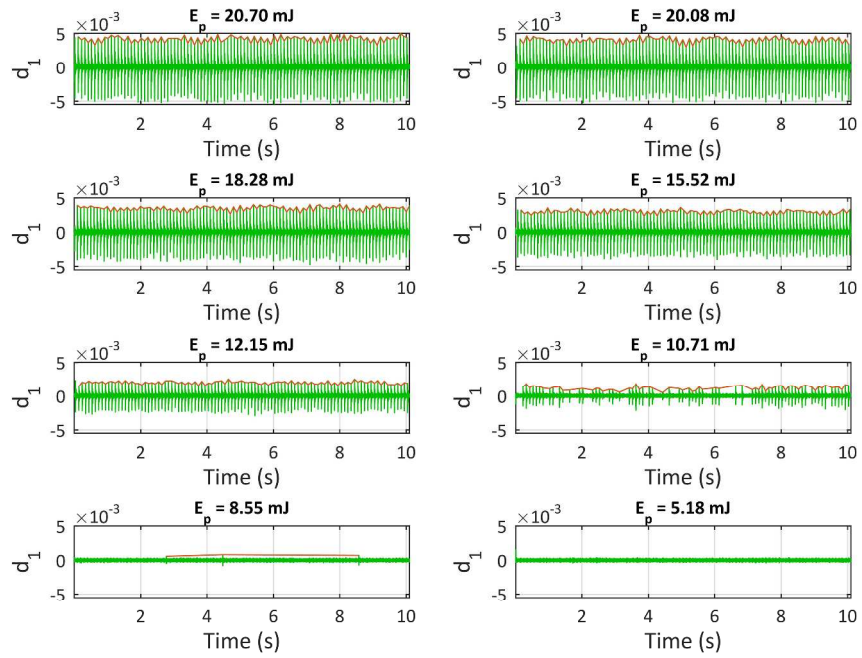


Figure 4: Representative outputs from the peak detection algorithm applied to the detail signal for a single 10 s audio recording (10 Hz repetition rate, 1064 nm wavelength).

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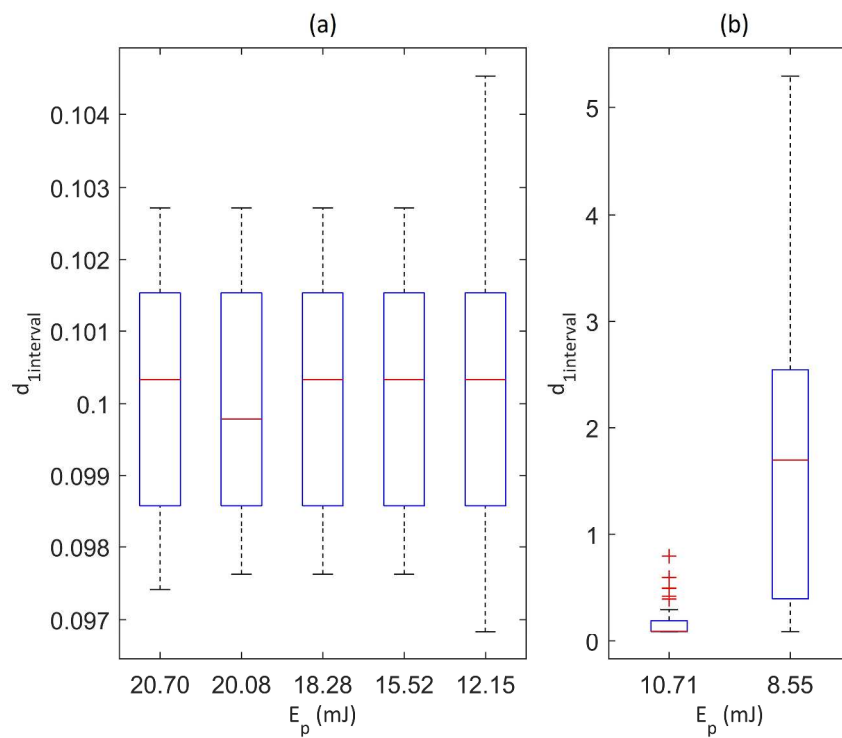


Figure 5: Box plot of the peak intervals ( $d_{1interval}$ ) from the peak detection algorithm applied to the detail signals in (a) the consistent laser induced breakdown region and (b) the inconsistent laser induced breakdown region (10 Hz repetition rate, 1064 nm wavelength).

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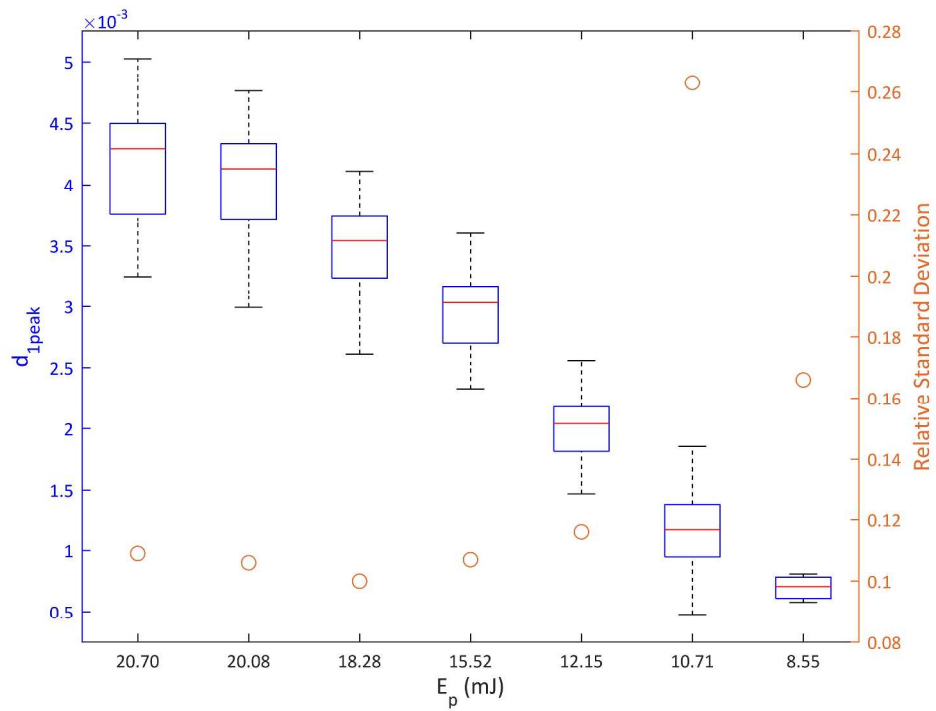


Figure 6: Box plot of absolute values of peak amplitude from the peak detection algorithm applied to the detail signal ( $d_{1peak}$ ) and their relative standard deviation (circles) as a function of incident pulse energy (10 Hz repetition rate, 1064 nm wavelength).

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