

Forthcoming in Earth and Planetary Science Letters

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2 **Modelling Shear Bands in a Volcanic Conduit:**

3 **Implications for Over-Pressures and Extrusion-Rates.**

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7 Received 20<sup>th</sup> December 2006; Accepted 28 August 2007.

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22

23 **Abstract**

24 Shear bands in a volcanic conduit are modelled for crystal-rich magma flow using simplified conditions  
25 to capture the fundamental behaviour of a natural system. Our simulations begin with magma  
26 crystallinity in equilibrium with an applied pressure field and isothermal conditions. The viscosity of the  
27 magma is derived using existing empirical equations and is dependent upon temperature, water content  
28 and crystallinity. From these initial conduit conditions we utilize the Finite Element Method, using axi-  
29 symmetric coordinates, to simulate shear bands via shear localisation. We use the von Mises visco-  
30 plasticity model with constant magma shear strength for a first look into the effects of plasticity. The  
31 extent of shear bands in the conduit is explored with a numerical model parameterized with values  
32 appropriate for Soufrière Hills Volcano, Montserrat, although the model is generic in nature. Our model  
33 simulates shallow (up to approximately 700m) shear bands that occur within the upper conduit and  
34 probably govern the lava extrusion style due to shear boundaries. We also model the change in the over-  
35 pressure field within the conduit for flow with and without shear bands. The pressure change can be as  
36 large as several MPa at shallow depths in the conduit, which generates a maximum change in the  
37 pressure gradient of 10's of kPa/m. The formation of shear bands could therefore provide an alternative  
38 or additional mechanism for the inflation/deflation of the volcano flanks as measured by tilt-metres.  
39 Shear bands are found to have a significant effect upon the magma ascent rate due to shear-induced flow  
40 reducing conduit friction and altering the over-pressure in the upper conduit. Since we do not model  
41 frictional controlled slip, only plastic flow, our model calculates the minimum change in extrusion rate  
42 due to shear bands. However, extrusion rates can almost double due to the formation of shear bands,  
43 which may help suppress volatile loss. Due to the paucity of data and large parameter space available for  
44 the magma shear strength our model results can only allow for a qualitative comparison to a natural  
45 system at this stage.

46

47

48 **Key words:**

49 Magma flow

50 Finite element method

51 Shear bands

52 Lava dome

53 Computational volcanology

54 Soufrière Hills Volcano

55

56 **1. Introduction**

57 Lava domes form when the extruded lava is so viscous it cannot flow freely away from the vent. Such  
58 structures can grow slowly for many weeks to years without being a threat to the surrounding  
59 population, but occasionally, a lava dome may collapse or explode. The main risk from collapse events  
60 are pyroclastic flows, concentrated dispersions of hot volcanic fragments that move rapidly down the  
61 volcano flanks in response to gravity [1]. Collapse events are a regular occurrence on Soufrière Hills  
62 Volcano (SHV), Montserrat, and can take the form of repeated destruction and reconstruction of the  
63 dome, often with the locus of new growth switching over time.

64  
65 Lava dome emplacement morphology ranges from near solid structures to more fluid flows, and is  
66 dominated by the degree of magma crystallisation [2, 3]. Crystal growth in intermediate composition  
67 magma occurs primarily due to the exsolution of volatiles, due to a decrease in pressure during ascent  
68 that acts to lower the liquidus temperature of the melt. Consequently, magma undergoes profound  
69 rheological stiffening during ascent, which can change the magma from a Newtonian fluid into a hot  
70 crystalline solid with only small amounts of residual melt [4]. Crystallisation is also time-dependent and  
71 for SHV, and lava domes generally, the morphology of the dome exhibits a high degree of correlation  
72 with the lava extrusion rate [2]. At the lowest extrusion rates lava is highly crystalline (85 to 95% solid  
73 fraction) within the upper conduit. During these conditions lava dome growth occurs in a predominantly  
74 extrusive (exogenous) fashion, producing crystal-rich structures such as spines and whalebacks [2]. At  
75 higher extrusion rates the magma has less time to crystallize in the conduit, resulting in more fluid-like  
76 behaviour including intrusive (endogenous) inflation and exogenous low aspect ratio flows.

77

78 During exogenous dome growth, lava is extruded directly to the free surface of the dome, implying some  
79 form of internal structure capable of channelling the magma. During emplacement the lava often  
80 extrudes in a stick-slip manner along curved structures, interpreted as ductile shear boundaries,  
81 suggesting that the conduit wall provides the main detachment surface. Spines, whalebacks and other  
82 crystal-rich exogenous structures commonly exhibit sub-parallel groves running along their length  
83 parallel with the direction of extrusion, that indicate some form of shear process [4]. Observational  
84 evidence of these structures also identifies cataclasites, suggesting the development of brittle shear  
85 bands [5]. The lava extrusion style is therefore to some degree controlled by shear bands, their presence  
86 being fundamental in crystal-rich exogenous emplacement.

87

88 Three types of seismic signal are commonly observed during silicic volcanic eruptions: Volcano-  
89 Tectonic (VT) events thought to be indicative of rock fracture, Long-Period (LP) events characterized  
90 by their harmonic signature and interpreted as oscillations in a fluid-filled resonator, and Hybrids which  
91 have a high-frequency onset (VT) followed by a low-frequency ringing (LP) [6, 7]. For SHV, the depth  
92 at which these seismic signals occur is anywhere between the free surface and 3000m below it [8]. VT  
93 events represent the deeper conduit system and spikes in activity have generally been linked to  
94 significant changes in eruption activity, although they are more commonly recorded during periods of  
95 dormancy [9]. Hybrid and LP events represent upper conduit and dome processes, commonly with the  
96 source location remaining relatively stable over-time [9]. For SHV LP seismicity is calculated to  
97 originate approximately 1500 m below the surface of the dome [10].

98

99 Cyclic behaviour at SHV during 1997 was observed for seismicity, deformation of the volcano flanks as  
100 recorded by tilt-meters, as well as lava dome growth. During this period cycles ranged from 4 – 36 hours

101 (not including the Vulcanian explosion cyclic events) [3, 11, 12]. During a typical (4 – 36 hours) cyclic  
102 period on SHV, lava dome growth would stagnate, as measured by the seismic network signifying the  
103 accompanying rockfall activity from the dome was reduced [1]. A reduction in the lava extrusion rate is  
104 indicative of crystal growth in the upper conduit, the time-scales of which are comparable to the  
105 deformation cycles, leading to the formation of an impeding dense viscous plug [11]. Pressurisation of  
106 magma and gas under the viscous plug can then result in the inflation of the volcano flanks. An  
107 acceleration in extrusion rate, observed by an increase in the amount of rockfalls from the advancing  
108 lava, signifies the formation of a new pathway for the lava and the removal of the viscous plug [2]. This  
109 permits the pressure in the upper-conduit to decrease, leading to the deflation of the volcano flanks.  
110 Typically dome growth is more pronounced at the peak of volcano flank tilt deformation and during  
111 deflation, commonly with extrusion rates approximately doubling and lava extrusion being  
112 accommodated by slip on ductile shear faults [3, 12]. The volcano flank deflations were generally more  
113 rapid than flank inflation, and hybrid earthquakes were observed to coincide with the point at which  
114 volcano flank inflation started to decelerate (the point of inflexion), suggesting that seismicity may be  
115 initiating the depressurisation process [13].

116

117 The above evidence, along with additional observational data [5], has led some research groups to  
118 postulate that hybrid and LP seismic events originate from stick-slip processes along the conduit margin  
119 [10]. Shear bands, as observed at the surface of the dome during cyclic activity, could generate such  
120 stick-slip behaviour, suggesting that shear bands could penetrate to the depths where LP seismicity  
121 originates. Using an isotropically pressurised conduit model [14], an elastic half-space model [12], or  
122 shear stresses at the wall of the conduit [15], the depth of the pressure source is calculated to be less than  
123 1000 m below the surface of the dome for SHV. Since the depth of LP events is approximately 1500 m

124 below the surface of the dome, this means that the tilt and seismic hypocentres don't appear to correlate,  
125 however the calculated depths are strongly model dependent.

126

127 We develop a visco-plastic axi-symmetrical Finite Element Method (FEM) model to simulate the  
128 generation of shear bands, localised regions of high strain, in a conduit via shear-localization. The  
129 formation of a zone or band of localised shear along the conduit wall occurs within our conduit domain  
130 when the material enters the plastic limit, i.e. when the shear stress experienced equals the shear strength  
131 of the magma. We neglect any potential frictional slip after shear bands have been generated,  
132 considering only plastic flow and therefore the minimum change in extrusion rate. We neglect the  
133 influence that bubbles have upon the viscosity and density, which may alter the flow properties. We also  
134 neglect departures from isothermal conditions and the evolution of shear bands once they form, instead  
135 considering the slow mode components of lava rheology, making the assumption that the timescales for  
136 shear band evolution occur more rapidly than the rheology can change. Instead, we focus our attention  
137 on a magma crystallinity in equilibrium with the pressure field and the influence this has upon viscosity  
138 and shear stress, which is found to be more significant than for bubbles for this style of volcanism [16,  
139 17]. For this paper we use constant magma shear strength because it is unknown which constitutive  
140 relationship controls the mode of deformation at depth. This means that the extent of the shear bands is  
141 controlled by the magma shear stress, which is effectively governed by the viscosity. Our model is  
142 intended to be simplified to capture the fundamental behaviour of a natural system, such as changes in  
143 extrusion rate and pressure. In section 2 we briefly discuss existing models that consider shear bands in  
144 conduit flow. We follow this with the description of our conduit model in section 3, including the field  
145 equations and initial conditions used. Section 4 provides results from our model and in section 5 we  
146 discuss these results.

147

148 **2. Existing Models**

149 Modelling efforts have been limited by the complexities of the magma rheology, for which no complete  
150 mathematical model currently exists [18]. Costa [17] recently developed an advanced model for the  
151 viscosity of magma containing very high solid fractions, although this model remains Newtonian.

152 Existing numerical models have offered important insights into the fundamental characteristics of lava  
153 flow in a conduit due to gas exsolution and crystallisation and how this may promote cyclic behaviour.

154 Melnik and Sparks [18 - 21] conduit models demonstrate that the major flow regimes depend upon the  
155 relative time scales of magma ascent and crystallisation, and that some cyclic behaviour can be

156 attributed to the time-scales involved with crystallisation kinetics. The observation of complex

157 oscillatory behaviour in the high-pressure extrusion of industrial polymer melts led Denlinger and

158 Hoblitt [22] to develop a simple dynamic model for conduit flow. They model compressible magma

159 flow through a cylindrical conduit undergoing stick-slip motion to extract characteristic oscillatory time-

160 periods, and relate this to the cyclic periods experienced by silicic volcanoes. While Wylie et al. [23]

161 modelled volatile exsolution as magma nears the surface, the corresponding increase in magma viscosity

162 within an elastic medium, and how this promotes oscillatory flow. In all these models the oscillatory and

163 seismic behaviour is related to the magma flow instability. However, none of the models consider the

164 lateral variations across the conduit which will modify the flow properties and promote the development

165 of shear bands [24, 25].

166

167 Neuberg et al. [10] combined seismological clues, field evidence and numerical modelling to suggest a

168 trigger mechanism for LP seismicity based upon the brittle failure of magma in the glass transition. They

169 model magma flow in a conduit using the FEM. Shear bands develop at the conduit wall where loss of



170 heat and gas is modelled, consequently resulting in a high viscosity gradient. Although they base their  
171 model upon the SHV, they use a very low crystallinity of 30% and this means they have to rely upon  
172 very high extrusion rates to force the generation of shear bands to appropriate depths. Gonnermann and  
173 Manga [26] use bubble growth and plastic failure to model the point at which magma fragmentation  
174 occurs within a conduit and the influence it has upon the resulting eruption style. For their model they  
175 are primarily interested in how magma melt and bubbles control viscous shearing, but do not specifically  
176 consider the depth that fragmentation (intense shear) occurs, or how it then changes the extrusion rate or  
177 pressure within the conduit. This is our motivation, and as for Neuberg et al. [10] and Gonnermann and  
178 Manga [26] we use an empirical well-studied viscosity and constant magma shear strength for a first  
179 look into the effects of plasticity.

180

### 181 **3. Conduit Model**

182 We model the conduit as a vertical cylinder of uniform radius between the magma chamber and the  
183 volcano free surface, as shown in Figure 1. The conduit is 15 metres in radius and has a length of 5km  
184 [27]. Magma ascent is driven by an over-pressure existing within the magma chamber, defined as the  
185 total pressure minus magma-static pressure, and the pressure at the free surface is atmospheric. Model  
186 equations are discussed in this section and Table 1 lists the parameters used in the model.

187

188 [Location of figure 1]

189 [Location of table 1]

190

#### 191 **3.1 Momentum Equations**

192 Magma is modelled as an isotropic, incompressible viscous fluid. The relationship between the  
 193 deviatoric part of the stress tensor  $\sigma'_{ij}$ , and the symmetric part of the velocity gradient or stretching  $D'_{ij}$ ,  
 194 reads:

$$196 \quad \sigma'_{ij} = 2\eta D'_{ij}, \quad i, j = (1,2,3), \quad (1)$$

197 where

$$198 \quad \begin{aligned} \sigma'_{ij} &= \sigma_{ij} + P\delta_{ij} \quad \text{and} \quad P = -\frac{1}{3}\sigma_{kk}, \\ D'_{ij} &= D_{ij} - \frac{1}{3}D_{kk}\delta_{ij}. \end{aligned} \quad (2)$$

199 Here  $\sigma_{ij}$  are components of the stress tensor,  $\eta$  the viscosity,  $\delta_{ij}$  is the Kronecker delta and  $P$  the  
 200 pressure. In general the viscosity depends on the pressure, temperature and other state variables. Here  
 201 we focus on the dependency of  $\eta$  on the crystal content as described in sections 3.4 and 3.5. We also  
 202 assume that any dilatancy effects associated with the crystallisation processes do not affect the  
 203 qualitative features of the flows considered here; i.e. we assume:

$$204 \quad D_{ij} = \text{div} \mathbf{v} = 0, \quad (3)$$

205 where  $\mathbf{v}$  is the velocity vector. The stress-equilibrium equations in axi-symmetrical coordinates, read,

$$206 \quad \begin{aligned} (r\sigma_{rr})_{,r} + r\sigma_{rz,z} - \sigma_{\theta\theta} + rf_r &= 0 \\ r\sigma_{zz,z} + (r\sigma_{rz})_{,r} + rf_z &= 0 \end{aligned} \quad (4)$$

207

208 where  $f$  is the body force and  $r$  is the radial coordinate. Insertion of equations 1 and 2 into 4 yields the  
 209 equations of motion in the following form:

210

$$\begin{aligned}
 211 \quad & \left( r(2\eta v_{r,r} - P) \right)_{,r} + r \left( \eta (v_{r,z} + v_{z,r}) \right)_{,z} - 2\eta \frac{v_r}{r} + P + r f_r = 0 \\
 & r(2\eta v_{z,z} - P)_{,z} + \left( r \eta (v_{r,z} + v_{z,r}) \right)_{,r} + r f_z = 0.
 \end{aligned} \tag{5}$$

212

### 213 **3.2 Generating Shear Bands**

214 Shear bands are weak regions stressed under high strain rates that are prone to failure. Localized shear  
 215 bands form if the underlying flow or deformation experiences a particular type of instability in the  
 216 constitutive relationship [28]. This instability expresses itself mathematically as a change in the type of  
 217 the tangential boundary value problem. In pressure-sensitive materials the instability may arise because  
 218 of a mismatch between the pressure sensitivity and the dilatancy factor and/or strain softening, for  
 219 example due to micro-cracking. Another important shear-band generating mechanism is related to shear  
 220 heating and thermal feedback due to a strongly temperature-dependent viscosity. However, this  
 221 mechanism is generally only relevant for high Péclet number flows (adiabatic shear banding) and is not  
 222 likely to be important in our study due to the low flow rates experienced at SHV [25]. Model results are  
 223 extremely mesh sensitive since the thickness of shear bands is undetermined in standard continuum  
 224 models. Strategies to overcome this ill-posedness have been developed mainly by the engineering  
 225 community [29]. Here we accept this mesh sensitivity so that the shear band width will be set by the  
 226 length scale provided by the discretisation scheme, i.e. the characteristic element width, which equals  
 227 the thickness of shear bands observed at SHV [4].

228

229 Magma flow rates can be highly variable due to complex feed-back processes such as time-dependent  
230 crystallisation [19]. However we need an initial crystallinity, pressure and viscosity within our conduit  
231 from which to initialise our model. The simplest starting point is to assume that the magma is initially  
232 stationary, and that the crystal content is in equilibrium with a pressure field. Stationary magma also  
233 implies that no shear bands currently exist within the conduit at the start of the simulation. From this  
234 initial magma state we need to initiate flow by changing the pressure field. Over time-scales associated  
235 with magma ascent in the conduit, magma chamber key variables such as over-pressure are likely to be  
236 approximately constant due to its large volume with respect to the lava-dome and conduit. Since our  
237 model is not transient at this stage we need to make the necessary simplification that a rapid over-  
238 pressure change occurs that is large enough to force magma flow and to generate shear bands. A  
239 significant and rapid pressure change within the conduit can be achieved by removing a flow-inhibiting  
240 lava dome, existing at the conduit exit, by means of a collapse event. Therefore our model begins with a  
241 pressure field that represents a lava dome at the conduit exit, providing a resisting pressure equal to the  
242 magnitude of the over-pressure in the magma chamber. The initial pressure gradient from which to  
243 evaluate the magma properties in the conduit for one simulation thus comprises of a component from the  
244 magma-static pressure, plus a constant over-pressure from the weight of the lava dome. Mathematically  
245 we instantaneously remove the dome and set the conduit exit pressure to be equal to atmospheric  
246 pressure. The over-pressure existing within the magma chamber can then be transferred to the magma in  
247 the conduit enabling flow. The velocity and pressure fields within the conduit are then calculated  
248 iteratively, using the initialised viscosity field and conduit exit and magma chamber pressures as  
249 boundary conditions.

250

251 The largest dome recorded at SHV was approximately 1116m above sea level, and following a collapse  
252 event the deepest it excavated into the crater was approximately 700m a.s.l., resulting in a dome collapse  
253 of approximately 400m [30]. This, and the estimated maximum tensile strength of the surrounding  
254 country rocks of 20 MPa provides an upper limit for the pressure change in our model [31]. The  
255 assumption of a magma crystallinity in equilibrium with the pressure field is not likely to be appropriate  
256 during periods of sustained magma flow due to crystallisation kinetics [25]. However the largest strain-  
257 rates and shear stresses are likely to be at the conduit walls due to a no-slip boundary condition. At the  
258 conduit wall, where magma is stationary, the crystal volume fraction and water content in the magma  
259 will be in equilibrium with the applied pressure. Hence the viscosity field along the conduit wall, where  
260 shear bands form, would not be expected to change much for transient flow from our unsteady model.

261

### 262 **3.3 Temperature**

263 The low thermal conductivity of magma means that the temperature will not change significantly along  
264 the length of the conduit, enabling us to assume the magma is in thermal equilibrium. The temperature  
265 of the magma and the conduit walls in our models is set to be 1123°K [32] justified by assuming the  
266 eruption is long-lived, the case for SHV, and therefore the conduit walls have been pre-heated. We  
267 assume that shear bands form instantaneously so that isothermal conditions prevail. Temporal offsets  
268 that may affect the flow; i.e., shear heating can further destabilize the flow once shear bands form, but  
269 this effect will be secondary to the onset of shear bands.

270

### 271 **3.4 Physical Properties of Magma**

272 Magma contains crystals, melt and bubbles that vary in proportion during flow and ascent in the conduit.  
273 Variations in the proportions of liquid and non-liquid components will modify the viscosity. The role of

274 bubbles in the magma in the simulation is ignored because its influence upon the viscosity is weak, a  
 275 maximum change in viscosity of approximately 75% [33] and for high viscosity dome forming eruptions  
 276 this value is likely to be much lower [34]. Our model focuses upon representing the crystal volume  
 277 fraction characteristics of the magma since this has by far the strongest influence upon the magnitude of  
 278 the effective viscosity, potentially increasing it to over 4 orders of magnitude [2, 17, 20, 33]. By  
 279 assuming the maximum crystal volume fraction possible in the magma, our model can be considered to  
 280 be an end-member scenario, reflecting very slow magma ascent rates, and will generate the deepest  
 281 shear bands owing to the highest viscosity within the conduit and the highest over-pressures required to  
 282 force flow.

283

284 For SHV the crystallinity in the magma chamber is calculated to be 35 to 45 vol. % phenocrysts and 15-  
 285 20 vol. % microphenocrysts [4] giving a total crystallinity between 50 and 65%. We assume an initial  
 286 crystallinity of 60 vol. % at the conduit entrance (Fig. 1). The degree of crystallisation is modelled by  
 287 considering the effective liquidus temperature  $T_{liq}$  which changes due to the progressive chemical  
 288 change of the melt (Eqn. 6).

289

$$290 \quad T_{liq} = a_T + b_T \ln(P) + c_T \ln(P)^2 + d_T \ln(P)/P^2, \quad (6)$$

291

292 with the coefficients  $a_T, b_T, c_T, d_T$  as given by Melnik and Sparks [21] and listed in Table 1. The  
 293 equilibrium crystallinity  $\phi_{eq}$  in the melt phase is given by (Eqn. 7):

294

$$295 \quad \phi_{eq} = \frac{A(P)(T - T_{liq}(P))}{B(P) - T}, \quad (7)$$

296

297 where  $A(P)$  and  $B(T)$  are functions of the pressure and are described by Melnik and Sparks [21] and  $T$   
 298 is the temperature. The melt viscosity of the magma is calculated using an empirical equation developed  
 299 by Hess and Dingwell [18] (Eqn. 8), where the water content, the primary volatile, is  $c = \alpha_s \sqrt{P}$  with  
 300  $\alpha_s$  the solubility coefficient:

301

$$302 \quad \log \eta_m = -3.545 + \left( 0.833 \ln c + \frac{9601 - 2368 \ln c}{T - (195.7 + 32.25 \ln c)} \right). \quad (8)$$

303

304 The total viscosity is calculated using the equation presented in Melnik and Sparks [21] (Eqn 9)

305 where  $\phi = \phi_{eq}$ :

306

$$307 \quad \eta = \theta(\phi) \eta_m \quad (9)$$

$$308 \quad \log \left( \frac{\theta(\phi)}{\theta_0} \right) = (\arctan(\xi(\phi - \phi_0)) + \pi / 2)$$

309

310 Equation 9 contains the coefficients  $\theta$  and  $\xi$ , and  $\phi_0$  is the critical crystal fraction, and the values used  
 311 are given in Table 1. For our model, this gives a viscosity from  $5 \times 10^5$  Pa s at the magma chamber up to  
 312  $4 \times 10^{10}$  Pa s at the conduit exit, depending upon the magma chamber pressure used.

313

### 314 **3.5 Magma shear strength**

315 The shear strength provides a limit to the acceptable stress states in a material. Laboratory experiments  
 316 show that the critical stress at the onset of yield is a function of pressure, temperature, strain, strain-rate,

317 porosity and sample size [36]. Therefore the physical properties of the magma are likely to affect the  
 318 yield characteristics of the magma. For example, if the magma has only small amounts of crystals then  
 319 the magma may yield in a ductile way as observed for metals. Whilst for cool brittle magma,  
 320 deformation is localized along micro-fractures that amalgamate into a shear surface at failure [4]. Since  
 321 we do not have knowledge of the yield mechanism along the conduit length we must focus on the  
 322 simplest scenario, a constant magma shear strength with a magnitude obtained from the brittle-ductile  
 323 criteria for glasses. For a first look into the effects of plasticity we use the von Mises visco-plastic model  
 324 with the yield criterion given by equation 10, where  $F$  designates the yield function,  $\tau = \sqrt{1/2\sigma'_{ij}\sigma'_{ij}}$  is  
 325 the equivalent shear stress and  $\tau_s$  is the magma shear strength. Prior to yielding the material deforms  
 326 linearly (i.e. Newtonianly), and once the shear strength has been reached some fraction of the  
 327 deformation will be permanent and non-reversible with plastic flow along a shear band.

$$328$$

$$329 \quad F = \tau - \tau_s \leq 0. \quad (10)$$

330

331 For an illustration how the criterion (Eqn. 10) works, consider simple shear with a prescribed  
 332 monotonically increasing strain rate. At sufficiently low strain rates the shear stress is below the magma  
 333 shear strength  $\tau_s$ . As the strain rate increases the shear stress will eventually reach  $\tau_s$ . It is non-physical  
 334 for  $\tau - \tau_s > 0$ , that is to have a stress exceeding the magma shear strength, thus even if the strain rate is  
 335 increased the shear stress will remain constant with  $\tau = \tau_s$ . Hence, shear bands are less likely to develop  
 336 as the magma shear strength increases and the driving force of the process controlling the magnitude of  
 337 the shear stress remains unaltered, because higher shear stresses are required to permit the magma to  
 338 enter the plastic regime. To model plastic flow we define an effective viscosity  $\eta_{eff} = \min[\eta, \eta_s]$  in the



339 solution of the velocity-pressure problem (Eqn. 5),  $\eta$  is the pre-yield viscosity (Eqn. 9) and  $\eta_s = \tau_s / \dot{\gamma}$ ,  
340 where  $\dot{\gamma}$  is the equivalent strain-rate, i.e.  $\dot{\gamma} = \sqrt{2D_{ij}D_{ij}}$ . Since  $\dot{\gamma}$  is unknown initially the solution has to  
341 be determined iteratively. The definition of  $\eta_{eff}$  ensures that after enough iterations  $\tau - \tau_s \leq 0$   
342 everywhere. Although the non-linear problem is solved iteratively using a secant rather a tangent  
343 method, the character and the properties of the solution is determined by the properties of the tangential  
344 problem [37]. During the iterations the plastic zone typically narrows and lengthens continuously until it  
345 is localized in a band of approximately one element size width along the conduit wall. In this particular  
346 case the plastic zone coincides with the domain occupied by the shear band.

347

348 Table 2 gives values for  $\tau_s$  from the literature. Apparent from table 2 is that the magma shear strength is  
349 not well constrained. Some of this scatter is because the physical properties of semi-molten magma are  
350 hard to measure given the technical difficulties involved in deforming samples of lava at the high  
351 temperatures, pressures and strain rates that occur within natural systems.

352

353 [Location of table 2]

354

#### 355 **4. Results**

356 The axi-symmetrical equations (3-5) are solved using the parallelized FEM based PDE solver eScript  
357 and the FE library Finley [38]. More details on the solution process for the velocity and pressure fields  
358 can be found in [39]. The axi-symmetric cylindrical conduit is discretised using 5000 x 15 elements with  
359 quadratic shape functions (8 nodes per element) in conjunction with 4 point Gauss integration for the  
360 element matrices.

361

**362 4.1 Shear band generation**

363 Figure 2 shows results from one simulation with magma shear strength of  $2 \times 10^5 \text{ Pa}$  and a magma  
364 chamber pressure of 132.2 MPa, which required a pressure change of 14.7 MPa at the conduit exit. From  
365 left to right in figure 2 we produce plots of velocity in  $X_3$ -axis, strain-rate, shear stress, and shear stress  
366 divided by the magma shear strength (effectively the plasticity). Where the shear stress divided by the  
367 magma shear strength is exactly equal to unity, shear bands will form. This results in a narrow band one  
368 element wide flush against the conduit wall, and for this simulation corresponds to a shear band length  
369 of 413.5m. In all the models presented, shear bands form a continuous band between the conduit exit  
370 and the maximum depth of the shear band directly against the conduit wall. This is due to the effective  
371 viscosity increasing towards the conduit exit (Fig. 3) and the magma shear strength having a constant  
372 value.

373

374 [Location of figure 2]

375

**376 4.2 Shear band length.**

377 Figure 4 shows the length that shear bands penetrate into the conduit for two different magma shear  
378 strengths over a range of magma chamber pressures, from 2.4 MPa to 25.4 MPa. Using a magma shear  
379 strength of  $10^6 \text{ Pa}$  the result was that no shear bands form in the conduit over the magma chamber  
380 pressures used. By reducing the magma shear strength we can force shear bands to form, because it  
381 effectively decreases the shear-stress required before the magma enters the plastic regime. For a magma  
382 shear strength of  $5 \times 10^5 \text{ Pa}$  shear bands develop to a maximum depth of 130 metres, whilst for a magma  
383 shear strength of  $2 \times 10^5 \text{ Pa}$  shear bands develop to a maximum depth of 703 metres. The length of the  
384 shear band within a conduit will depend upon the magma viscosity and the driving pressure. Although a

385 magma shear strength change from  $2 \times 10^5 \text{Pa}$  to  $5 \times 10^5 \text{Pa}$  is only small, the length that shear bands form to  
386 is significantly affected because the viscosity changes occurs most dramatically in the upper conduit.  
387 Figure 3 shows the relaxed Newtonian viscosity along the length of the conduit at the start of the  
388 simulation as well as the crystal volume fraction of the magma with depth. Figure 4 also shows that  
389 shear bands will not form within the conduit for magma chamber pressure below approximately 130MPa  
390 (an over-pressure of 12MPa) for a magma shear strength of  $5 \times 10^5 \text{Pa}$ , whilst for a magma shear strength  
391 of  $2 \times 10^5 \text{Pa}$  shear bands only form for magma chamber pressures exceeding 120MPa (i.e. an over-  
392 pressure of 2MPa).

393

394

395 [Location of figure 3]

396 [Location of figure 4]

397

398

399 For low magma chamber pressures, corresponding to an initially small change in pressure at the conduit  
400 exit, the viscosity in the upper conduit will be relatively large (Eqns. 7 - 9). However, due to the low  
401 extrusion rate (a consequence of the lower over-pressure), shear bands will not penetrate deep into the  
402 conduit. For increasing magma chamber pressures, i.e. increased dome retarding pressures, the viscosity  
403 in the upper conduit will decrease since crystallinity is a function of pressure. However, a higher over-  
404 pressure will result in a higher extrusion rate allowing the shear band length to increase with increasing  
405 magma chamber pressure. The length that shear bands penetrate into the conduit tends towards an upper  
406 limit, most clearly shown for a magma shear strength of  $5 \times 10^5 \text{Pa}$  (Fig. 4), due to the viscosity decreasing  
407 with increasing depth within the conduit (Fig. 3).

408

409 **4.3 Shear band influence upon extrusion rate.**

410 Shear bands are likely to effect magma ascent rates by reducing conduit friction and consequently the  
411 large over-pressures required to extrude highly crystalline silicic magmas. We calculate the extrusion  
412 rate for magma flow with no shear bands in the conduit (i.e. Hagen-Poiseuille flow), assuming the  
413 magma does not enter the plastic regime. For the same magma chamber pressure we calculate the  
414 extrusion rate for magma flow in the conduit with shear bands permitted to form. Since our model  
415 ignores a possible elastic-brittle contribution to the rheology, frictional slip can not be modelled. As a  
416 consequence we model the minimum change in extrusion rate due to plastic deformation only.

417

418 [Location of figure 5]

419

420 Figure 5 shows the modelled extrusion rate (a) and its relative change (b) with and without shear bands  
421 in the conduit, plotted against the pressure in the magma chamber. For a magma shear strength of  
422  $5 \times 10^5$  Pa shear bands can penetrate to depths of 130 m, which results in a maximum change in extrusion  
423 rate of approximately 3%. Whilst for a magma shear strength of  $2 \times 10^5$  Pa, at the highest magma  
424 chamber pressures shear bands reach a depth of 703 m resulting in a change in the extrusion rate of  
425 almost 100%. Transitions between effusive and explosive volcanic activity are essentially controlled by  
426 volatiles. The ability of gas trapped within the magma melt, from exsolved volatiles, to expand or escape  
427 by permeable flow will determine if the ascending magma will be effusive or explosive. Slowly  
428 ascending magma has time to release this build-up of gas resulting in highly degassed effusive magma.  
429 However, magma ascending rapidly may not be able to release the build-up of gas, and this may result in  
430 explosive activity. Gonnermann and Manga [26] suggest that fragmentation at the conduit wall, from  
431 localised regions of high strain, may act to inhibit explosive behaviour due the enhanced permeability

432 from the fracture network that develops. However, cyclic activity in 1997 at SHV produced numerous  
433 Vulcanian explosions with each episode preceded by a large dome collapse [40]. These collapse events  
434 may have forced the generation of shear bands in the upper conduit due to a large change in pressure as  
435 shown by our models. If these shear bands form rapidly enough, instantaneously in our visco-plastic  
436 model, the enhanced extrusion rate due to shear band formation may be large enough to prevent volatiles  
437 exsolving effusively. This may result in a competition between the processes of enhanced permeability  
438 from fragmentation and reduced gas loss due to enhanced extrusion rates. Therefore deep shear bands  
439 may be more likely to promote explosive activity due to a potentially large increase in extrusion rate.

440

441 The relative increase in extrusion rate due to the formation of shear bands is non-linear (Fig 5b). This is  
442 due to two processes, first the length of shear bands tends towards an upper limit due to the decrease in  
443 viscosity with depth in the upper conduit (Fig. 3). Second, at increasing depths in the conduit the  
444 viscosity is lower, which will result in a smaller decrease from Newtonian to shear viscosity, meaning  
445 that the conduit resistance change is not as significant. At low magma chamber pressures (<130MPa) the  
446 extrusion rate is at the low end of the observed range for SHV (<0.5m<sup>3</sup>s<sup>-1</sup>). Lava is commonly extruded  
447 along shear surfaces at these extrusion rates due to the high degree of crystallinity in the magma. Since  
448 the generation of shear bands at these magma chamber pressures have a relatively minor influence upon  
449 the extrusion rate (changing it by up to 40%) this suggests that shear bands forming at this extrusion rate  
450 may be relatively stable and the crystal content will not vary significantly due to crystallisation kinetics  
451 [20].

452

453

454 **4.4 Shear band influence upon the over-pressure field**

455 Cyclic inflation and deflation of the flanks of the volcano as recorded by tilt-meters is indicative of  
456 pressurisation within the upper conduit [12]. Crystal-rich magma forms a viscous cap in the upper  
457 conduit that inhibits flow, leading to pressure build-up at shallow levels and edifice inflation [11]. The  
458 magnitude and direction of tilt of the volcano flanks can be used to infer the magnitude and depth of the  
459 pressure source. Using an isotropically pressurised model [14] or elastic half-space model [12, 41], the  
460 depth of the pressure source is always less than 1000 m below the surface of the dome for SHV. Also,  
461 the pressure source either needs to be very large or distributed over a large area [14]. Green and Neuberg  
462 [13], following research by Beauducel et al. [42], suggest that surface deformations recorded by tilt-  
463 meters could instead, or in addition, be from shear stresses within the upper conduit rather than a single  
464 large pressure source. The SHV flank displacements are then consistent with the generation of shear  
465 stresses beginning within the upper 100's metres of the conduit walls. However, Green and Neuberg  
466 [13] emphasize that the vertical extent of the pressure source is unconstrained because tilt measurements  
467 are insensitive to deep sources. Considering vertical traction along the conduit walls the location for the  
468 tilt hypocentre is calculated to be approximately 400m and 600 m a.s.l., that suggests a shear stress  
469 depth of 160 to 360m below the conduit exit, with traction values between 0.5 and 1.5MPa [13]. For  
470 vertical traction to explain the recorded tilt requires a pressure gradient of  $6.7 \times 10^4 - 2.0 \times 10^5$  Pa/m along  
471 an upper conduit segment 30m in diameter [13].

472

473 [Location of figure 6]

474

475 We use our conduit flow model to calculate the over-pressure within the conduit with shear bands for a  
476 magma shear strength of  $2 \times 10^5$  Pa (Fig. 6). Figure 6a shows the over-pressure profile along the conduit  
477 length for flow in the conduit with shear bands and without shear bands (i.e. Hagen-Poiseuille flow).

478 The pressure difference in figure 6b corresponds to the over-pressure in the conduit for Hagen-Poiseuille  
479 flow minus the over-pressure in the conduit with shear bands for the same magma chamber pressure.  
480 Hence, what figure 6b shows is the redistribution in over-pressure along the conduit length due to the  
481 development of shear bands. A positive pressure difference corresponds to a drop in pressure and  
482 therefore flank deflation. Everywhere the pressure difference is less or equal (at the magma chamber and  
483 conduit exit) to the initial over-pressure field, but the difference is most significant in the upper part of  
484 the conduit. This is more clearly shown in figure 7 which shows the over-pressure gradient along the  
485 conduit length for flow with shear bands minus that for Hagen-Poiseuille flow. Below the depth in the  
486 conduit where shear bands exist, the over-pressure gradient increases due to an increase in extrusion rate  
487 (from the presence of shear bands) but no change in viscosity. Above the depth where shear bands form,  
488 the over-pressure gradient decreases to values of  $4 \times 10^4$  Pa/m. Figure 8 shows a summary of all the  
489 model results for a magma shear strength of  $2 \times 10^5$  Pa showing the pressure difference maximum and the  
490 depth of the maximum against magma chamber pressure. These values for the depth and magnitude of  
491 the pressure change are comparable to those inferred at SHV during cyclic activity.

492

493 [Location of figure 7]

494

495 [Location of figure 8]

496

## 497 **5. Discussion**

498 Shear bands are simulated using a strain-localisation model to occur when the shear-stress equals the  
499 magma shear strength of the magma. This can result in the generation of shear bands to depths of  
500 approximately 700 m for low magma shear strengths ( $2 \times 10^5$  Pa) and high magma chamber pressures

501 (142.9MPa). These shear bands may be responsible for lava effusion along shear boundaries at the free  
502 surface, because they extend directly from the conduit exit, and flank inflation/deflation. Geophysical  
503 evidence for the depth of shear bands at SHV is not well constrained other than from the pressure source  
504 responsible for the inflation and deflation of the volcano flanks. Green and Neuberg, [13] and Voight et  
505 al. [12] calculate the depth of such pressure sources to be between approximately 160 to 510 below the  
506 conduit exit, consistent with our modelled shallow shear bands depths and pressure change maximum.

507

508

509 The over-pressure in the upper conduit is significantly affected by the formation of shear bands, due to a  
510 change in the viscosity and flow field altering the conduit resistance. Our model shows that the over-  
511 pressure decreases in the upper conduit due to the formation of shear bands, corresponding to the  
512 deflation of the flanks. We model a change in over-pressure gradient of up to  $4 \times 10^4$  Pa/m in the upper  
513 conduit and a maximum pressure change of 4.5MPa at depths up to 300m; magnitudes that can be  
514 related to the change in the tilt experienced during inflation and deflation cyclic events. Enhanced  
515 degassing and ash emissions are observed during the inflation maximum and deflation cycle from cracks  
516 on the dome surface [12]. This may be due to the enhanced permeability from the formation of shear  
517 bands that generate micro-fractures. However there may be a competition between the process of  
518 enhanced permeability from fragmentation, and an enhanced extrusion rates suppressing gas-loss from  
519 shear band development. Also, an increase in extrusion rate due to the formation of shear bands may be  
520 the explanation for why the deflation period for the volcano flanks is commonly more rapid than the  
521 inflation period. Given further model constrains/improvements, an observed change in extrusion rate  
522 could be used to infer the shear strength of the magma within the conduit or the greatest depth that shear  
523 bands penetrate to.



524

525 The conduit of a volcano initially begins as a dyke connected to the magma chamber, with cylindrical  
526 conduit geometries only developing at shallow levels where the erosional capabilities of magma are  
527 higher. The radius or width of the dyke for SHV at depth is estimated to be approximately 11 to 12 m  
528 with an uncertainty of 7 m, when considering the ascent rates of hornblende [43]. Our model suggests  
529 that there may be a greatest depth at which upper shear bands can reach, and this will be the greatest  
530 depth at which significant conduit wall erosion will occur, when ignoring explosive decompression  
531 effects. Due to over-simplifications used in our model we can't constrain this depth. But future models  
532 that couple the change in the conduit radius with depth, and the feedback it will have upon magma  
533 viscosity and extrusion rates, will allow for an estimate of the conduit plumbing at depth.

534

535 For lower magma shear strength values the depth of shear bands can be expected to increase, but will  
536 only reach the depths at which LP seismicity occurs (~1500 m) for unrealistically low magma shear  
537 strengths. Thus, it is hard to reconcile LP seismic signals directly to the depth of shear bands simulated  
538 in our model. To form shear bands at the depth where LP events occur requires either a more complex  
539 magma shear strength model, the conduit to narrow at depth allowing the strain-rate to increase, or both.  
540 A magma shear strength model dependent upon pressure and magma crystallinity will be the focus of  
541 future research [44].

542

543 All models have their limitations, and we make several simplifying assumptions that are likely to affect  
544 models results. First, we have to rely upon a pressure change, via a dome collapse event, to trigger flow.  
545 However, in reality the magma is extruded without any large pressure change or dome collapse event in  
546 a continuous manner. Indeed, it was during periods of rapid magma extrusion ( $>5\text{m}^3\text{s}^{-1}$ ) that the cyclic

547 seismic and deformation was primarily observed. Thus a transient model including the temporal  
548 evolution of shear bands is required to fully understand the influence of shear bands upon magma flow,  
549 pressure and the timescales involved in cyclicity. Second, because we consider a maximum crystallinity  
550 in our models, this reflects flows at low extrusion rates. For flow at higher extrusion rates the viscosity is  
551 likely to be lower due to crystallisation growth kinetics [19, 25]. This process may suppress the  
552 development of shear bands, due to a lower viscosity, resulting in lower shear stresses at the conduit  
553 wall although the crystallinity is likely to remain approximately in equilibrium at the wall. Finally,  
554 neglecting vesicularity means that we don't consider a variable density, which is likely to give  
555 quantitatively different results. Introducing vesicularity into the model will decrease the weight of the  
556 magma column which is likely to increase the extrusion rate and push the depth of shear bands to deeper  
557 levels within the conduit. However, simplifications were necessary for this model, but despite this model  
558 results suggest that changes in pressure and velocity fields due to shear bands could be significant,  
559 especially during tilt and seismic cycles in eruptive behaviour.

560

## 561 **6. Acknowledgements**

562 We would like to thank 3 anonymous reviewers for helping to make significant changes and  
563 improvements to the manuscript and thank M. A. O'Brien for proof-reading. Support is gratefully  
564 acknowledged by the Australian Computational Earth Systems Simulator Major National Research  
565 Facility (ACcESS MNRF), The University of Queensland, and support from the ARC discovery grant  
566 DP0771377.

567

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712

713 **Figure captions:**

714 Figure 1: Schematic of a volcano, showing a conduit connecting the magma chamber to the free-surface,  
 715 with lava dome/flow at the conduit exit (not to scale). In reality the conduit may narrow at depth but it is  
 716 assumed to be a constant radius for simplicity in this model. Also shown is the approximate depth at  
 717 which LP seismicity and pressurisation responsible for volcano flank tilt occurs. Shown next to the  
 718 schematic is the model domain. We use axisymmetric coordinates, modelling the conduit between  $r = 0$   
 719 to the conduit wall at  $r = 15\text{m}$ . The length of the conduit is 5000m. Boundary 1 has the condition of an  
 720 applied pressure, the magma chamber pressure, and Boundary 4 is at atmospheric pressure. Boundary 3  
 721 has the condition of no-slip and Boundary 2 is a symmetry boundary, ensuring no flow in the radial  
 722 direction.

723

724 Figure 2: Results from one simulation with a magma shear strength of  $2 \times 10^5 \text{Pa}$ , a magma chamber  
 725 pressure of 132.2 MPa requiring a pressure change of 14.7MPa at the free surface. From left to right are  
 726 plots of velocity in the  $X_3$ -axis, strain-rate, shear stress, and shear stress divided by the magma shear  
 727 strength (effectively the plasticity) within the conduit. Shown is only half of the conduit, from the centre  
 728 of the conduit at  $r=0$  (left side of image) to the conduit wall at  $r=15\text{m}$  (right side of image). The conduit  
 729 radius has been stretched in the figures by a factor of 30 to better visualise the results along the entire  
 730 5km length of the conduit. Where the shear stress divided by the magma shear strength is exactly equal  
 731 to unity shear bands develop. This corresponds to a shear band one element wide, flush against the  
 732 conduit wall, within the red zone of the figure. For this simulation a shear band of length of 413.5m  
 733 forms between the conduit exit and a depth of 413.5m.

734

735 Figure 3: A typical modelled crystal volume fraction (a) and viscosity (b) along the length of the  
736 conduit. Most of the change in viscosity and crystallinity occurs in the upper-conduit due to the pressure  
737 field.

738

739 Figure 4: Modelled shear band length against pressure in the magma chamber for magma shear strength  
740 values of  $2 \times 10^5 \text{Pa}$  (filled shapes) and  $5 \times 10^5 \text{Pa}$  (unfilled shapes). For the same magma shear strength the  
741 magma chamber pressure governs the depth of the shear bands due to its influence upon the extrusion  
742 rate and viscosity.

743

744 Figure 5: a) shows the extrusion rate modelled with and without shear bands against the pressure in the  
745 magma chamber. The model uses a magma shear strength of  $2 \times 10^5 \text{Pa}$  for the solid shapes and  $5 \times 10^5 \text{Pa}$   
746 for the unfilled shapes. The initial extrusion rate for no shear bands in the conduit is given by the  
747 crosses. b) shows the modelled change in extrusion rate (given by the extrusion rate with shear bands  
748 divided by extrusion rate without shear bands) using the same symbols for the different magma shear  
749 strengths.

750

751 Figure 6: a) Shows the over-pressure in the conduit with depth for flow in the conduit without shear  
752 bands (i.e. Hagen-Poiseuille flow) and with shear bands for a magma shear strength of  $5 \times 10^5 \text{Pa}$  (Flow  
753 with shear bands). Both flow models have a magma chamber pressure of  $132.55 \text{MPa}$ . Also shown is the  
754 difference in pressure between the two flow regimes with depth in the conduit, a depth of zero  
755 corresponds to the conduit exit. A positive pressure difference corresponds a decrease in the over-  
756 pressure along the conduit length, i.e. flank deflation. b) Difference in over-pressure along the conduit

757 due to the development of shear bands for different magma chamber pressures, shown in the legend, all  
758 for dome collapse events equivalent to 7MPa and a magma shear strength of  $5 \times 10^5$  Pa.

759

760 Figure 7: Change in over-pressure gradient for flow with shear bands minus flow without shear bands  
761 (i.e. Hagen-Poiseuille flow) along the conduit length for different magma chamber pressures, shown in  
762 the legend, for dome collapse events equal to 7MPa and a magma shear strength of  $2 \times 10^5$  Pa. A positive  
763 pressure-gradient corresponds to an increase in the pressure gradient due to the presence of shear bands,  
764 whilst a negative pressure gradient corresponds to a decrease. A depth of zero corresponds to the conduit  
765 exit.

766

767 Figure 8: Summary of a) over-pressure maximum (see Fig. 6) and b) the depth of the maxima (see Fig.  
768 6) against magma chamber pressure for all the model runs for a magma shear strength of  $2 \times 10^5$  Pa.

769

770 Table 1: Parameters used in the model which are appropriate for the magma from Soufrière Hills  
 771 Volcano.

Symbol	Parameter	Reference	Value
T	Initial Temperature	32	1123°K
$\phi$	Crystal volume fraction in chamber	4	0.6
$\rho$	Density	19	2350 kg.m <sup>-3</sup>
P <sub>0</sub>	Maximum over-pressure	31	20 MPa
$\xi$	Parameter in effective viscosity function	21	8.6
$\theta_0$	Parameter in effective viscosity function	21	1.4
$\phi_0$	Parameter in effective viscosity function	21	0.69
$\alpha_s$	Solubility coefficient	19	4.11 x10 <sup>-6</sup> Pa <sup>-1/2</sup>
$a_T$	Liquidus and solidus coefficients	21	1465.4
$b_T$	Liquidus and solidus coefficients	21	-31.4
$c_T$	Liquidus and solidus coefficients	21	-2.8
$d_T$	Liquidus and solidus coefficients	21	-0.41
$R_c$	Conduit radius	27	15 m
$L_c$	Conduit length	27	5000m
$g$	Acceleration due to gravity		10 m.s <sup>-2</sup>

772

773 Table 2: Magma shear strength values quoted in the literature for lavas that are appropriate to our study.

Magma Shear Strength    Reference    Comments

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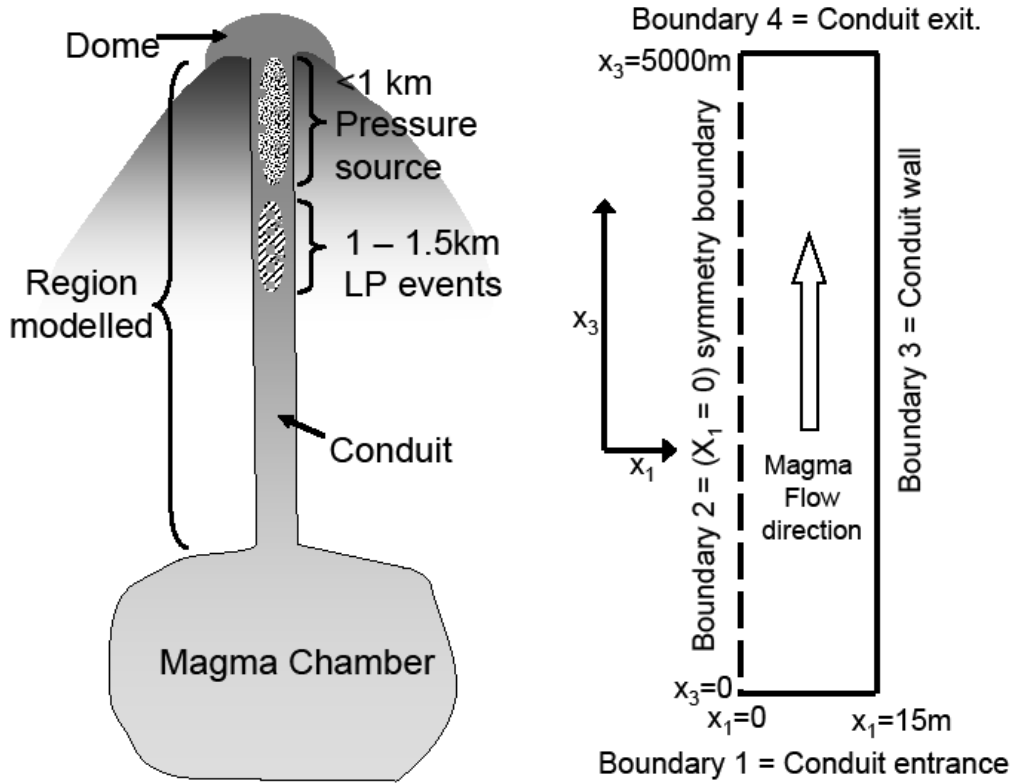
$10^6 - 10^7$ Pa	45	Experimental results from hydrous vesicular glasses.
$10^6$ Pa	12	From estimates for the strength of lava from the height of spines extruded at Soufrière Hills Volcano, Montserrat.
$10^7$ Pa	26	Used in numerical models for magma fragmentation.
$0.5 - 1.5 \times 10^6$ Pa	15	Inferred from numerical models for the amplitude of tilt measured at Soufrière Hills Volcano, Montserrat.
$10^7$ Pa	10	Used in numerical models of magma flow at Soufrière Hills Volcano, Montserrat.
$10^7 - 10^8$ Pa	5	Magma shear strength values from laboratory experiments.

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777 Figure 1:

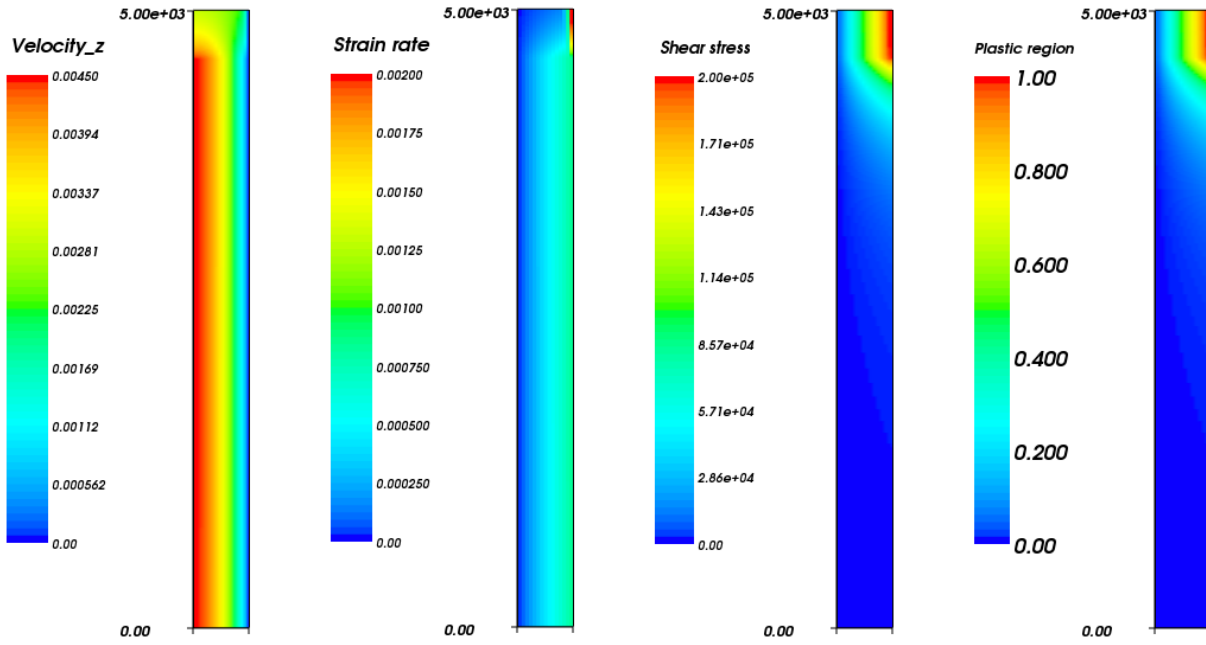


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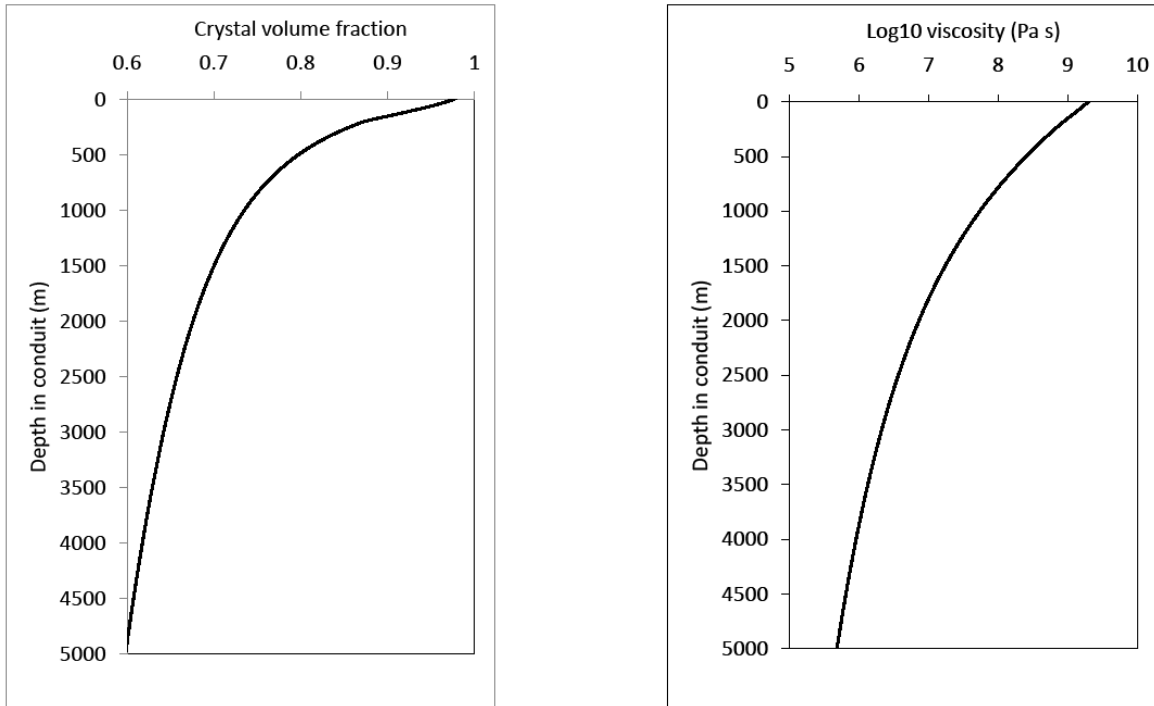


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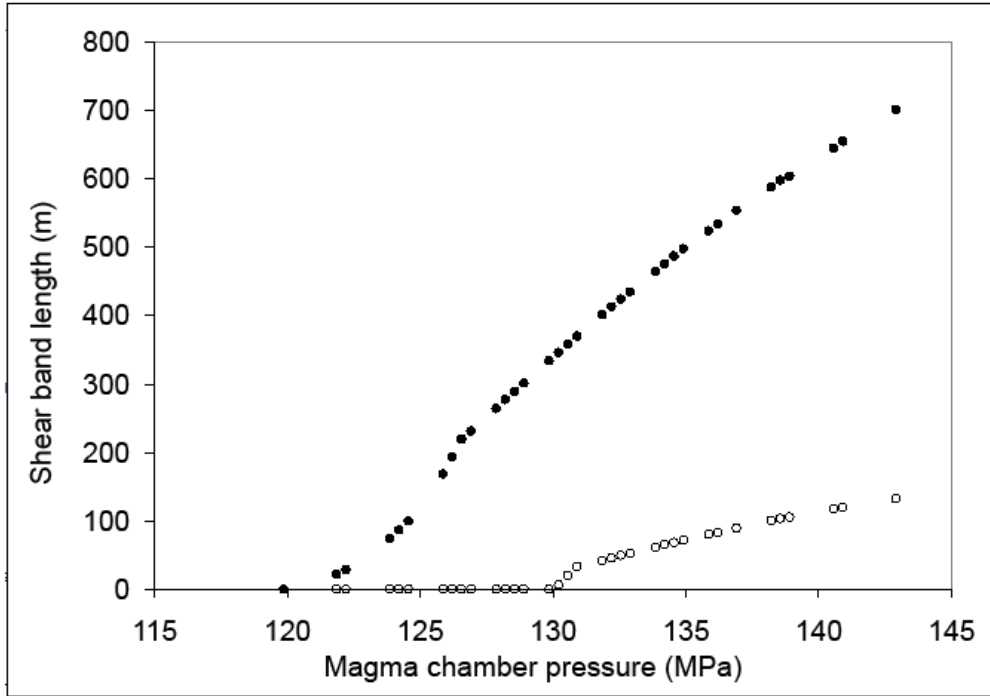
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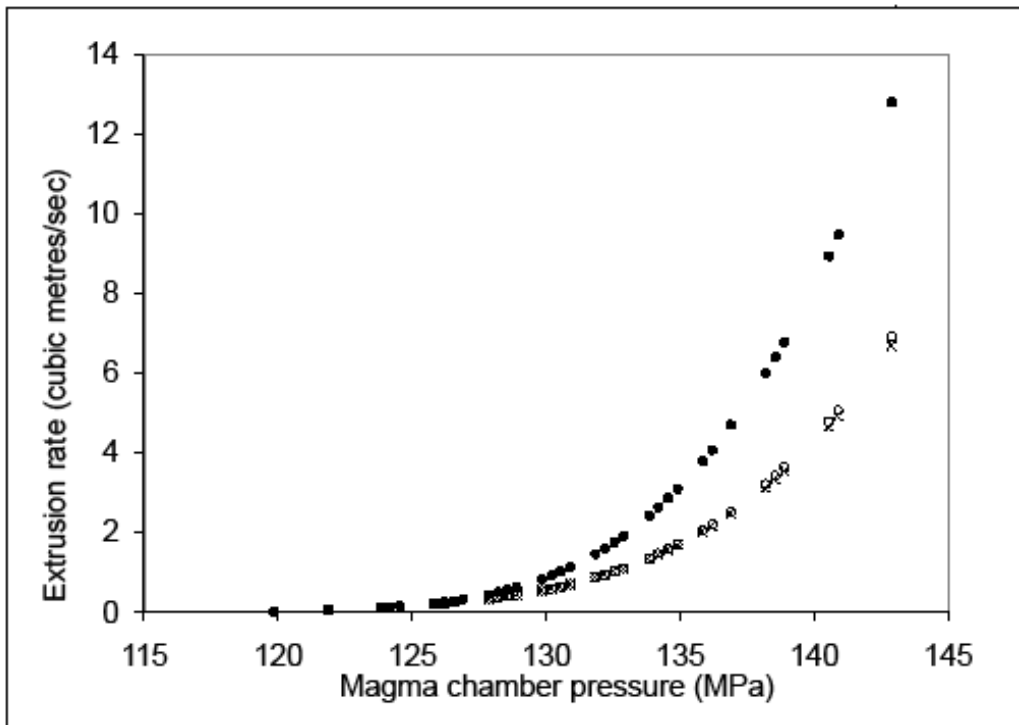
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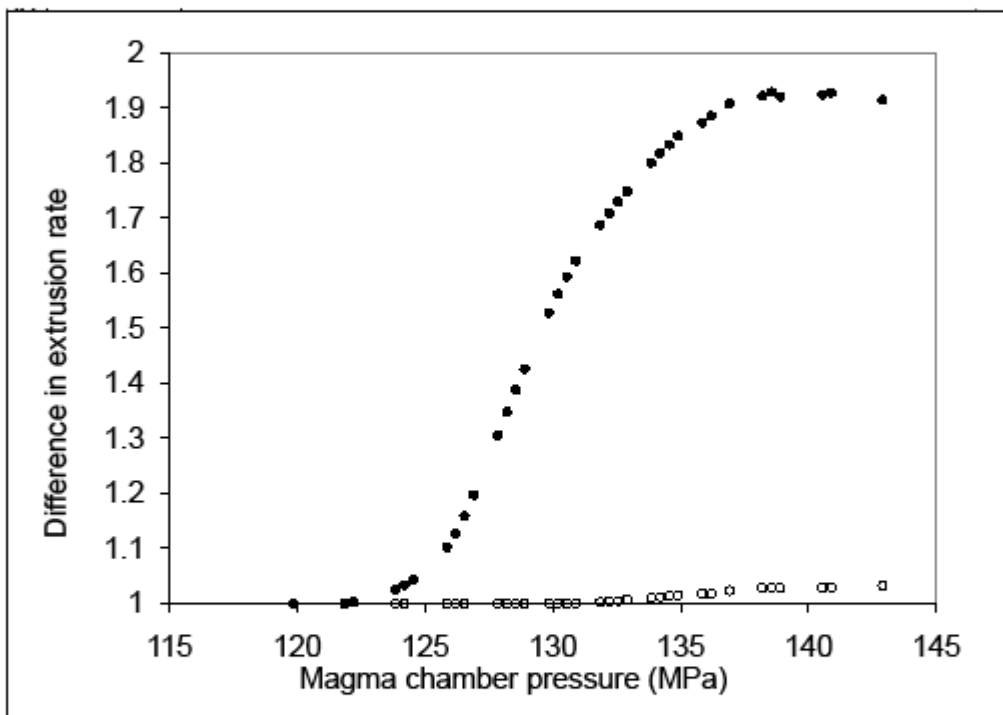
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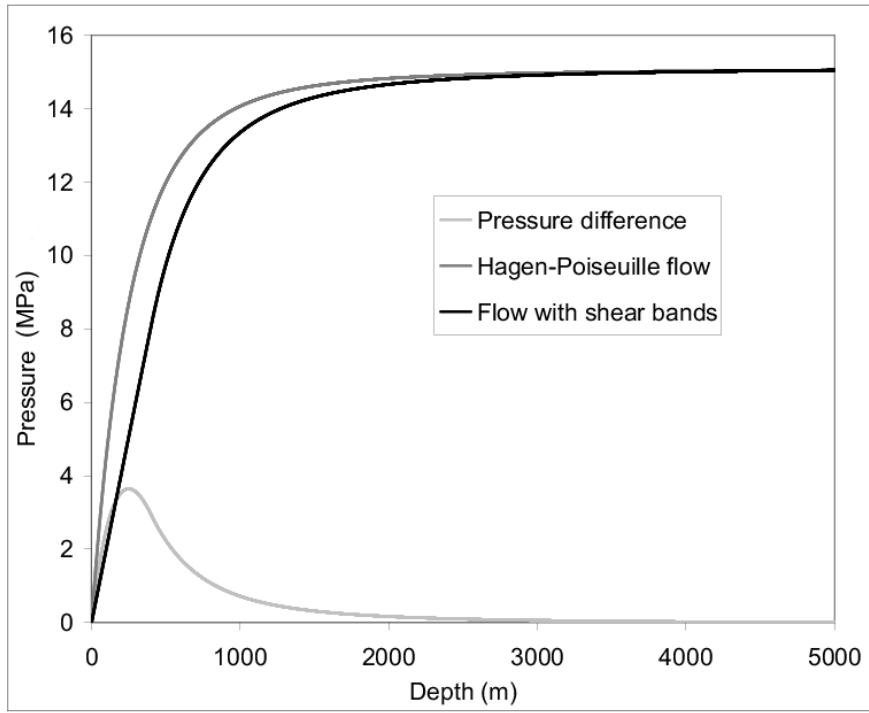


792 Figure 5b:



794 Figure

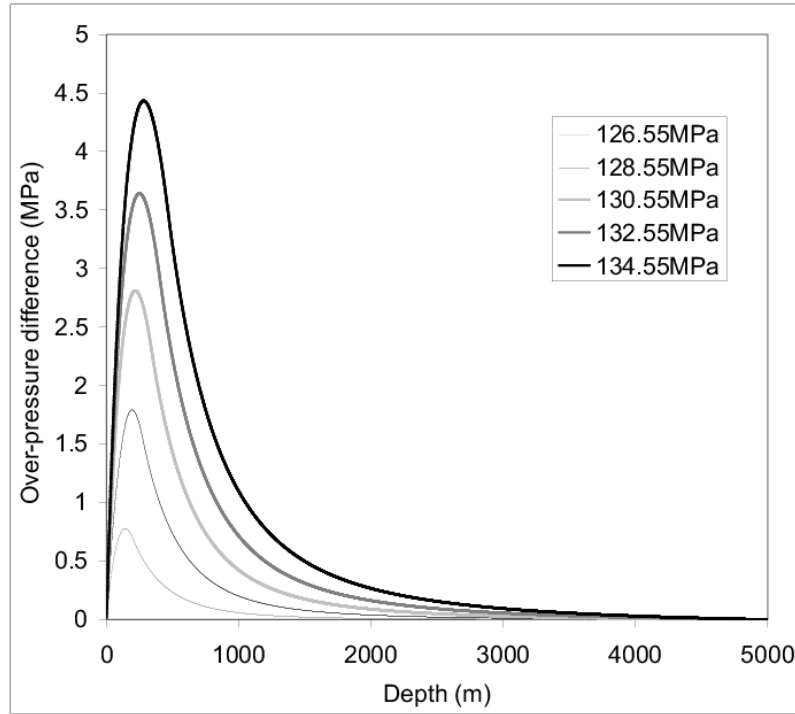
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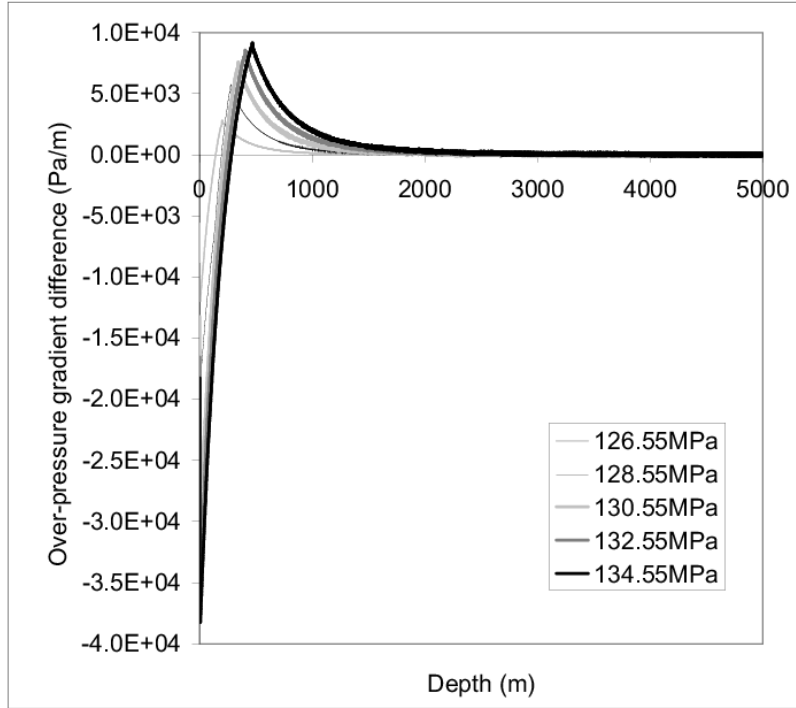
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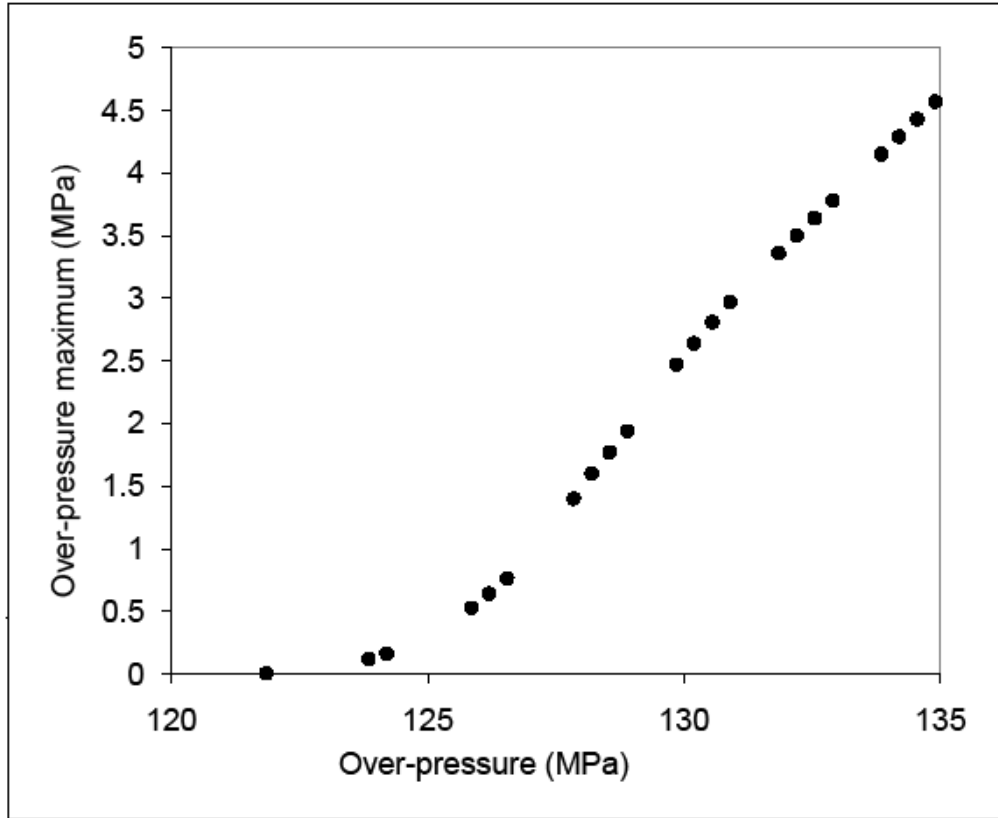
801 Figure 7:



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804 Figure 8a:

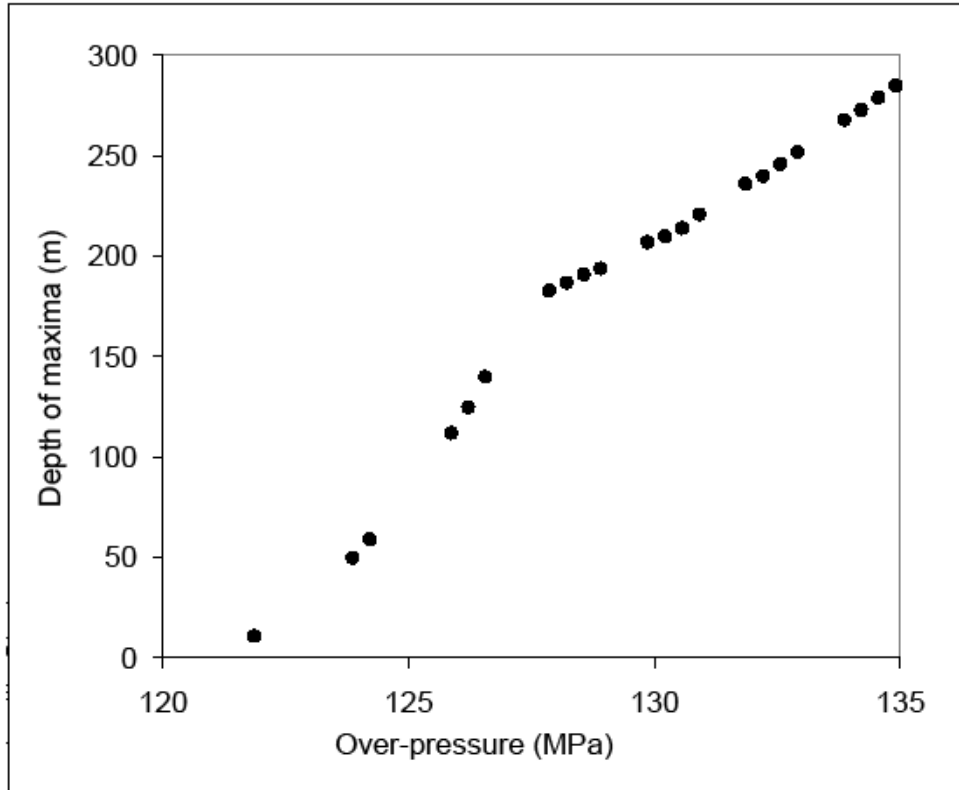


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808 Figure 8b:



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