



# Ti/Pd/Ag Contacts to *n*-Type GaAs for High Current Density Devices

PENGYUN HUO <sup>1,2</sup> and IGNACIO REY-STOLLE<sup>1,3</sup>

1.—Instituto de Energía Solar – Universidad Politécnica de Madrid, ETSI de Telecomunicación, Avda. Complutense 30, 28040 Madrid, Spain. 2.—e-mail: huo.pengyun@ies-def.upm.es. 3.—e-mail: ignacio.reystolle@upm.es

The metallization stack Ti/Pd/Ag on *n*-type Si has been readily used in solar cells due to its low metal/semiconductor specific contact resistance, very high sheet conductance, bondability, long-term durability, and cost-effectiveness. In this study, the use of Ti/Pd/Ag metallization on *n*-type GaAs is examined, targeting electronic devices that need to handle high current densities and with grid-like contacts with limited surface coverage (i.e., solar cells, lasers, or light emitting diodes). Ti/Pd/Ag (50 nm/50 nm/1000 nm) metal layers were deposited on *n*-type GaAs by electron beam evaporation and the contact quality was assessed for different doping levels (from  $1.3 \times 10^{18} \text{ cm}^{-3}$  to  $1.6 \times 10^{19} \text{ cm}^{-3}$ ) and annealing temperatures (from 300°C to 750°C). The metal/semiconductor specific contact resistance, metal resistivity, and the morphology of the contacts were studied. The results show that samples doped in the range of  $10^{18} \text{ cm}^{-3}$  had Schottky-like *I*-*V* characteristics and only samples doped  $1.6 \times 10^{19} \text{ cm}^{-3}$  exhibited ohmic behavior even before annealing. For the ohmic contacts, increasing annealing temperature causes a decrease in the specific contact resistance ( $\rho_{c,\text{Ti/Pd/Ag}} \sim 5 \times 10^{-4} \Omega \text{ cm}^2$ ). In regard to the metal resistivity, Ti/Pd/Ag metallization presents a very good metal conductivity for samples treated below 500°C ( $\rho_{M,\text{Ti/Pd/Ag}} \sim 2.3 \times 10^{-6} \Omega \text{ cm}$ ); however, for samples treated at 750°C, metal resistivity is strongly degraded due to morphological degradation and contamination in the silver overlayer. As compared to the classic AuGe/Ni/Au metal system, the Ti/Pd/Ag system shows higher metal/semiconductor specific contact resistance and one order of magnitude lower metal resistivity.

**Key words:** Ohmic contact, *n*-GaAs, high conductivity

## INTRODUCTION

The formation of high quality metal/semiconductor contacts has been an open topic in semiconductor technology research for several decades.<sup>1,2</sup> A broad variety of metallization systems on GaAs have been investigated and most of them are designed to improve the low metal–semiconductor specific contact resistance and enhance the contact bondability.<sup>3–6</sup> However, for some devices using GaAs contact layers, such as light emitting diodes (LEDs), lasers or solar cells, low metal resistivity is

also very important due to the inherent presence of large current densities in them. Moreover, in the case of LEDs and solar cells, this problem is specially demanding since the front contact has the form of a grid (i.e., does not fully cover the front side) and thus the problem of high current densities is aggravated by a contact with limited area.<sup>7–9</sup> These devices typically use gold in their metal contacts; for example, the AuGe/Ni/Au contact on *n*-GaAs is a classic metallization that has been the dominant scheme in many III–V devices on account of its low contact resistance and good adherence.<sup>10–12</sup> However, despite producing very low metal/semiconductor specific contact resistances ( $\sim 10^{-6} \Omega \text{ cm}^2$ ), this system is not optimal since: (1)

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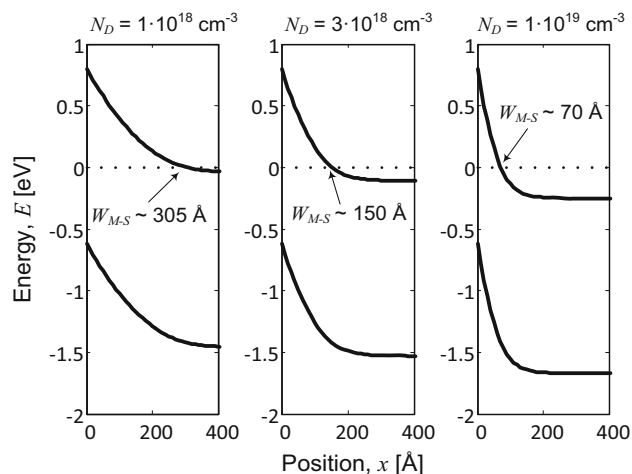


Fig. 1. Energy band diagrams of Ti/*n*-GaAs contacts for various doping levels in the GaAs layer (left  $N_D = 1 \times 10^{18} \text{ cm}^{-3}$ ; center  $N_D = 3 \times 10^{18} \text{ cm}^{-3}$ ; right  $N_D = 1 \times 10^{19} \text{ cm}^{-3}$ ). The zero energy level is the Fermi energy level. All the diagrams have been calculated assuming the Ti/*n*-GaAs barrier layer to be  $\phi_{M-S} = 0.8 \text{ eV}$ . The resulting effective barrier thickness ( $W_{M-S}$ ) for each doping level are also included in the plots.

61 Au has intermetallic reactions with GaAs (i.e.,  
62 compromising the long term stability of the metal/  
63 semiconductor interface); (2) Au is very expensive;  
64 and (3) the conductivity of the gold overlayer -i.e.,  
65 the part of the metal stack intended to provide low  
66 metal resistivity- is significantly degraded by the in-  
67 diffusion of Ni and Ge from the contact layer and Ga  
68 and As from the semiconductor, since Ni does not  
69 work as a good barrier layer during the rapid  
70 thermal annealing (RTA) process. For these rea-  
71 sons, several other metallization systems have been  
72 studied to meet these requirements. For example,  
73 one method has targeted the minimization of the  
74 cross-diffusions in the AuGeNi system by opti-  
75 mizing the RTA temperature<sup>13</sup> or introducing a  
76 barrier layer to stop it.<sup>14</sup> Another strategy has been  
77 based on using totally different metal stacks. In this  
78 field, the study of metallizations based on Ti/Pt or  
79 Ti/Pd has been intense since both Ti and Pt or Pd  
80 work as efficient barrier layers and Ti also promotes  
81 the adhesion of the contact to the semiconduc-  
82 tor.<sup>15–17</sup> Some other metal systems receiving some  
83 attention over the last years include metallizations  
84 based on Pd/Ge, which exploit the inward diffusion  
85 of Ge and the formation of a highly doped semicon-  
86 ductor and/or barrier height lowering stemming  
87 from the formation of a Ge-GaAs heterojunction,  
88<sup>18–21</sup> and some other similar metallization  
89 systems such as Pd/Sn, Ge/Cu.<sup>22</sup> In summary, the  
90 search of a new metal system providing (1) low  
91 metal/semiconductor specific contact resistance  
92 ( $< 10^{-5} \Omega \text{ cm}^2$ ); (2) low metal sheet conductivity;  
93 (3) high long term stability; (4) good bondability and  
94 (5) low cost is still an open field of research.

95 In the field of silicon solar cells—in particular, in  
96 high efficiency or concentrator designs—this prob-  
97 lem was solved using the system Ti/Pd/Ag to define  
98 front grids on *n*-Si, with evidence of excellent metal/  
99 semiconductor specific contact resistance, good  
100 bondability, and demonstrated long-term stabil-  
101 ity.<sup>23,24</sup> These properties can be cursorily explained  
102 as follows: (1) Ti is a refractory metal that while  
103 having an firm adhesion to Si, does not show  
104 intermetallic reactions (at least for  $T < 500^\circ\text{C}$ ),  
105 providing excellent stability and total absence of  
106 spiking at the metal semiconductor interface; (2)  
107 high doping levels in Phosphorus-diffused solar cell  
108 emitters and Ti's ability to dissolve the native SiO<sub>2</sub>  
109 produce extremely thin Schottky barriers and very  
110 low specific contact resistances; (3) Ti/Pd works as a  
111 diffusion barrier layer, separating the Si and top Ag  
112 layer, and thus avoiding cross contamination; and  
113 (4) pure Ag has a large conductivity, ideal to  
114 produce contacts with low metal resistivity. In  
115 summary, the Ti/Pd/Ag metallization has been  
116 reported to work fine on *n*<sup>+</sup>Si.

117 Moving on to GaAs, Ti has been extensively  
118 studied to fabricate highly stable Schottky contacts  
119 on moderately doped *n*-GaAs<sup>25–27</sup> for its ability to  
120 produce inert and highly stable interfaces. Figure 1  
121 shows the energy band diagrams of Ti/*n*-GaAs

127 contacts for various doping levels in the GaAs layer  
128 (left  $N_D = 1 \times 10^{18} \text{ cm}^{-3}$ ; center  $N_D = 3 \times$   
129  $10^{18} \text{ cm}^{-3}$ ; right  $N_D = 1 \times 10^{19} \text{ cm}^{-3}$ ). All the dia-  
130 grams in this figure have been calculated using  
131 Snider's 1-D Poisson solver<sup>28</sup> assuming the Ti/*n*-  
132 GaAs barrier layer to be  $\phi_{M-S} = 0.8 \text{ eV}$ .<sup>26,27</sup> Obvi-  
133 ously, the resulting effective barrier thickness  
134 ( $W_{M-S}$ )—defined here as the depth at which the  
135 conduction band energy reaches the Fermi level  
136—is the parameter that controls the conduc-  
137 tion of charge carriers across this interface by  
138 governing their tunneling probability. For moder-  
139 ately doped *n*-GaAs layers (data not shown),  $W_{M-S}$   
140 can extend over a hundred nm but it also can reach  
141 values lower than 300 Å for dopings higher than  
142  $1.5 \times 10^{18} \text{ cm}^{-3}$ , indicating that (as occurs with  
143 *n*<sup>+</sup>Si) heavy doping in the contact layer is an  
144 effective way to control the transition from Schottky  
145 to ohmic behavior.

146 Therefore, the aforementioned working principles  
147 of the Ti/Pd/Ag metal system on *n*<sup>+</sup>Si also hold for  
148 *n*<sup>+</sup>GaAs, and therefore this metal system shows  
149 some potential for our target application. First, it  
150 should be noted that Ti also shows firm adhesion to  
151 GaAs and does not react with it at least for  
152  $T < 500^\circ\text{C}$ ,<sup>25</sup> providing excellent stability of the  
153 metal semiconductor interface. Second, Ti affinity  
154 for oxygen also provides an advantage over GaAs,  
155 since it can be used to get oxygen during the e-beam  
156 evaporation process and to dissolve the native GaAs  
157 oxides to produce clean sharp metal–semiconductor  
158 interfaces. Third, as shown in Fig. 1, high doping  
159 levels in the *n*-GaAs produce very thin Schottky  
160 barriers with potentially low specific contact resis-  
161 tance. In addition, Ti also works as a diffusion

barrier in GaAs,<sup>15–17,25</sup> separating the semiconductor and the top metal layer in charge of providing good sheet conductance; the endurance of this barrier is further enhanced by the presence of a layer of Pd.<sup>17</sup> Finally, pure Ag has a large conductivity, ideal to produce contacts with low metal resistivity.

In fact, pursuing some of these ideas, there are some works in the literature reporting the use of Ti/Pd/Au on p-GaAs,<sup>29</sup> and other Ti-based contacts on GaAs, such as Ti/Pt for p-GaAs<sup>30,31</sup> and Ti/Pt/Au for *n*-GaAs.<sup>15,16</sup> In these systems either gold (and not silver) is used as the conductive layer or Pt (and not Pd) is used as the diffusion barrier layer. Although Pt has been shown to have superior performance than Pd working as a diffusion barrier (because the Pd-Pd bond strength is about one fourth of that of the Pt-Pt bond), the fact is that Pd has demonstrated to be successful under moderate RTA temperatures (<500°C) and is more cost-effective.<sup>29,30</sup>

Despite its potential advantages, a thorough study of Ti/Pd/Ag metallization characteristics on *n*-GaAs is lacking, and would offer a more cost-effective alternative than systems using Pt and Au. Accordingly, in this paper we present an assessment of Ti/Pd/Ag contacts to *n*-GaAs as a function of the *n*-GaAs doping level and contact annealing treatment; analyzing the impact of these variables on the Schottky/Ohmic nature of the contact; its specific contact resistance, and the influence of contact formation on the metal resistivity and morphology (i.e., bondability) of the metallization.

## EXPERIMENTAL PROCEDURES

A set of *n*-GaAs layers were grown by metalorganic vapor phase epitaxy (MOVPE) on semi-insulating (100) GaAs wafers with a miscut of 2° towards the nearest (111)A plane. The epilayer thickness was of 400 nm and three different doping concentrations of  $1.3 \times 10^{18} \text{ cm}^{-3}$ ,  $3.1 \times 10^{18} \text{ cm}^{-3}$ , and  $1.6 \times 10^{19} \text{ cm}^{-3}$  were fabricated to observe the doping level influence on the contact quality. Such doping levels were chosen to sweep typical contact layer doping levels used in MOVPE. After epitaxial growth, the doping level in the *n*-GaAs layers was confirmed by electrochemical capacitance-voltage profiling using a WEP Control CVP21 tool. Contact areas were defined by using conventional photolithographic techniques. Prior to contact deposition, the substrates were cleaned using  $\text{H}_2\text{SO}_4:\text{H}_2\text{O}_2:\text{H}_2\text{O}$  (2:1:50) and  $\text{HCl}:\text{H}_2\text{O}$  (1:1) to remove the native oxide layer, and a completely hydrophobic surface was obtained; deionized water rinsing and blown dry with nitrogen followed. Ti/Pd/Ag metal stacks of 50 nm/50 nm/1000 nm were deposited in a multi-pocket electron beam evaporator at a base vacuum of  $1 \times 10^{-6}$  mbar. Immediately after evaporation, the patterns suffered a lift-off process to take away the metal from unwanted areas. The samples were separately annealed by

RTA in forming gas ( $\text{H}_2:\text{N}_2$ , 1:9) at different temperatures (300–750°C) and times (20–180 s). In order to compare the quality of the metallization obtained, samples with the classic contact structure AuGe/Ni/Au (200 nm/60 nm/500 nm) were also fabricated on the highest doped layer ( $1.6 \times 10^{19} \text{ cm}^{-3}$ ) and RTA processing at 375°C for 180 s. For the electrical characterization, the transmission line model (TLM)<sup>32</sup> was used to measure specific contact resistance and the Van der Pauw method<sup>33</sup> was used to measure the metal layer sheet resistance, and the metal resistivity was calculated by sheet resistance times the measured thickness of the metal layer. To insulate both the TLM and Van der Pauw patterns, a mesa etching was done with  $\text{NH}_4\text{OH}:\text{H}_2\text{O}_2:\text{H}_2\text{O}$  (2:1:10). The electrical characterization was carried out using the 4-wires method by sweeping current and measuring voltage (in order to obtain better measurements in the low current range, the samples doped  $1.3 \times 10^{18} \text{ cm}^{-3}$  were measured by sweeping voltage and measuring current) using a Keithley 2062 programmable power supply. A profilometer KLA-Tencor Alpha-Step D-120 Stylus Profiler was used to measure the surface roughness.

## RESULTS AND DISCUSSION

In the first set of the experiments, Ti/Pd/Ag layers (50 nm/50 nm/1000 nm) were deposited on three *n*-GaAs layers with different doping levels ( $1.3 \times 10^{18} \text{ cm}^{-3}$ ,  $3.1 \times 10^{18} \text{ cm}^{-3}$ , and  $1.6 \times 10^{19} \text{ cm}^{-3}$ ) and subsequently annealed by RTA at 400°C for 100 s. Figure 2 shows, for each sample, representative *I*-*V* curves taken between two adjacent TLM contacts, which were 100 μm apart.

Figure 2 is evidence that, when the doping level is not high enough, Schottky contacts are obtained. Nevertheless, for the sample doped  $1.6 \times 10^{19} \text{ cm}^{-3}$ , the contact is ohmic and shows little influence of the RTA process (curves for annealed and non-annealed

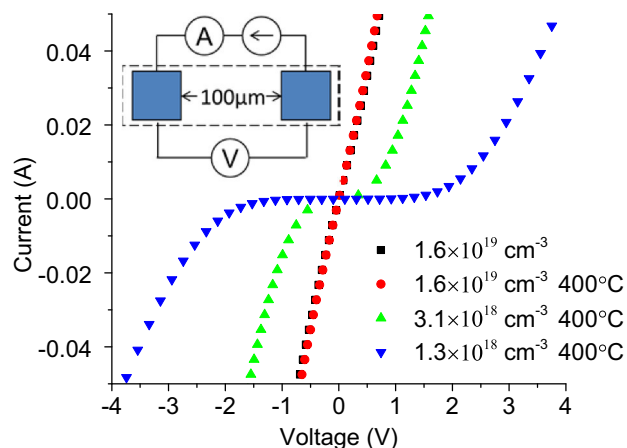


Fig. 2. *I*-*V* curve of Ti/Pd/Ag contact resistance as a function of *n*-GaAs doping. Pad separation is 100 μm.



samples virtually overlap in Fig. 2). The specific contact resistance and metal resistivity of these samples are included in Table I. As anticipated by Fig. 2, the specific contact resistance  $\rho_c$  experiences only small changes before and after RTA, going from  $\rho_c = 1.9 \times 10^{-3} \Omega \text{ cm}^2$  to  $\rho_c = 1.5 \times 10^{-3} \Omega \text{ cm}^2$ . However, despite being ohmic, these values of  $\rho_c$  are still quite high, as compared to the reference AuGe/Ni/Au contact (last row in Table I). On the contrary, the values of metal resistivity  $\rho_M$  are significantly better and quite homogeneous for all samples in Fig. 2. All values of  $\rho_M$  are around  $2.4 \times 10^{-6} \Omega \text{ cm}$ , which is about one magnitude lower than the metal resistivity of the AuGe/Ni/Au reference contact. Notably, this metal resistivity range is reasonably close to its tabulated value for pure bulk material ( $1.6 \times 10^{-6} \Omega \text{ cm}$ ). Given the fact that even small impurity concentrations tend to affect the conductivity of thin films, it seems plausible that the Ag layer is not contaminated by GaAs, supporting the idea that TiPd works fine as a barrier layer, hindering the diffusion of Ga and As atoms into the Ag layer. Of course this result is not an unequivocal proof for lack of significant diffusion, though it is certainly in line with the results with Ti/Pd/Au reported by Chor et al.<sup>29</sup> and Jones et al.,<sup>30</sup> where no significant contamination of the Au layer could be measured for RTA processing temperatures of 500°C or less. On the contrary, the metal resistivity of the AuGe/Ni/Au system is one order of magnitude lower than that of pure bulk gold. This seems to be an indirect evidence of Ni not being as an effective diffusion barrier and thus gold overlayer conductivity being degraded by Ga and As, Ge, and Ni contamination.

To assess the impact of annealing conditions on the Ti/Pd/Ag contact quality, different RTA processes have been carried out. Figure 3a shows the results for the contacts made on GaAs doped  $1.3 \times 10^{18} \text{ cm}^{-3}$ . In all cases, Schottky-like behavior is observed. For increasing temperatures a slight decrease in the turn-on voltage (i.e., on the barrier height) is observed. At this point, it seemed plausible that further increasing the annealing temperature would eventually make the contact ohmic.

Therefore, the experiment was repeated and higher temperatures were explored for the RTA. In order to further facilitate the formation of ohmic contacts (i.e., in order to increase tunneling probability), highly doped samples ( $N_D = 3.1 \times 10^{18} \text{ cm}^{-3}$ ) were used in this new set of experiments. The result of this experiment can be seen in Fig. 3b. As shown in this figure, when the annealing temperature is raised to 750°C, which is the optimum temperature for a Ti contact on degenerated doped *n*-GaAs as reported by Zhou et al.<sup>15</sup> the contact becomes ohmic and  $\rho_c = 9.2 \times 10^{-4} \Omega \text{ cm}^2$ . However, for lower temperatures (400°C and 500°C), Schottky contacts are obtained as displayed in Fig. 3b.

Finally, Fig. 3c summarizes the same set of experiments for the sample doped  $1.6 \times 10^{19} \text{ cm}^{-3}$ . As shown in Fig. 3c and Table I, an increase in annealing temperature mildly decreases  $\rho_c$ . After annealing at 750°C, a minimum  $\rho_c$  value is reached of  $1.3 \times 10^{-4} \Omega \text{ cm}^2$ , which is similar to the results obtained with Ti/Pt/Au on *n*-GaAs ( $\sim 1.0 \times 10^{-4} \Omega \text{ cm}^2$ );<sup>15,16</sup> still far from the values of the reference AuGe/Ni/Au contact ( $\rho_c = 2.9 \times 10^{-6} \Omega \text{ cm}^2$ ) and metallization systems based on Pd/Ge on *n*-GaAs ( $\sim 3.0 \times 10^{-7}$ ).<sup>19,21,34</sup> Obviously, the

**Table I. Comparison of contact properties of Ti/Pd/Ag on *n*-type GaAs with different doping and annealing conditions**

System	Doping concentration $N_D$ ( $\text{cm}^{-3}$ )	RTA	Specific contact resistance $\rho_c$ ( $\Omega \text{ cm}^2$ )	Metal resistivity $\rho_M$ ( $\Omega \text{ cm}$ )
Ti/Pd/Ag (50 nm/50 nm/1000 nm)	$1.3 \times 10^{18}$	375°C 180 s	–	$2.36 \times 10^{-6}$
		400°C 100 s	–	$2.38 \times 10^{-6}$
		430°C 100 s	–	$2.47 \times 10^{-6}$
		460°C 100 s	–	$2.49 \times 10^{-6}$
Ti/Pd/Ag (50 nm/50 nm/1000 nm)	$3.1 \times 10^{18}$	–	–	$2.02 \times 10^{-6}$
		400°C 100 s	–	$2.48 \times 10^{-6}$
		500°C 100 s	–	$2.14 \times 10^{-6}$
		750°C 30 s	$9.2 \times 10^{-4}$	$7.19 \times 10^{-5}$
Ti/Pd/Ag (50 nm/50 nm/1000 nm)	$1.6 \times 10^{19}$	–	$1.9 \times 10^{-3}$	$1.98 \times 10^{-6}$
		400°C 100 s	$1.5 \times 10^{-3}$	$2.23 \times 10^{-6}$
		500°C 100 s	$4.9 \times 10^{-4}$	$2.23 \times 10^{-6}$
		750°C 30 s	$1.3 \times 10^{-4}$	$9.31 \times 10^{-5}$
		375°C 180 s	$2.9 \times 10^{-6}$	$2.22 \times 10^{-5}$
AuGe/Ni/Au (200 nm/60 nm/500 nm)	$1.6 \times 10^{19}$	375°C 180 s	$2.9 \times 10^{-6}$	$2.22 \times 10^{-5}$

The time included in the third column is the so-called *soaking time* for the RTA process (i.e., the time for which the temperature remains constant, not including ramp-up and ramp-down times). The results of the classic AuGe/Ni/Au metallization have been included for reference in the last row.



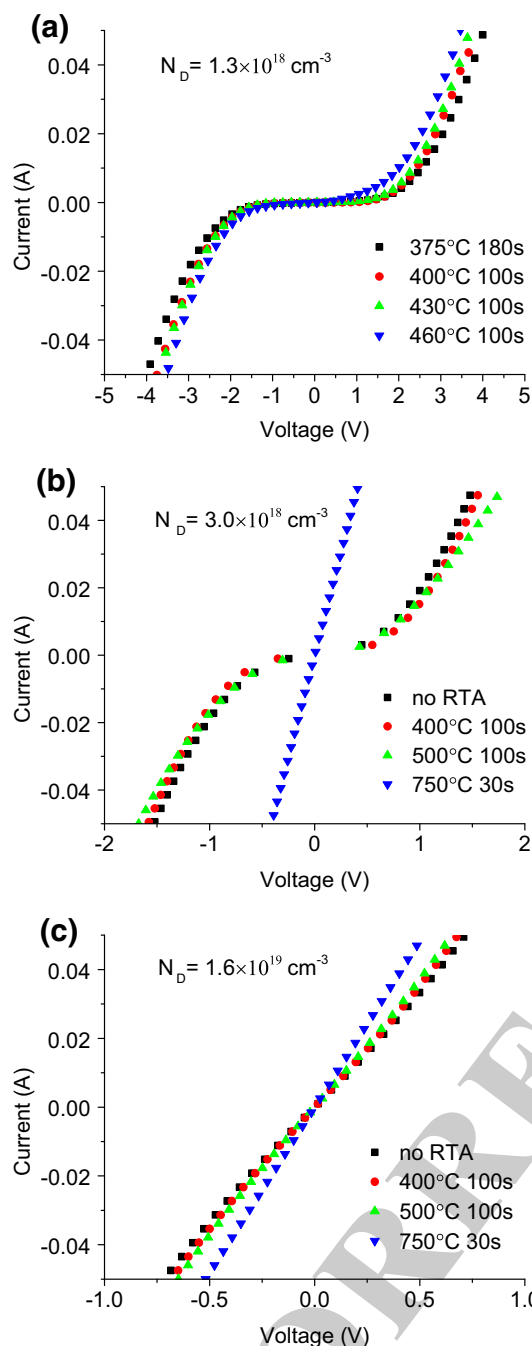


Fig. 3. *I*-*V* curves of Ti/Pd/Ag contact resistance as a function of annealing temperature and doping level. The *n*-GaAs layer doping concentration is: (a)  $N_D = 1.3 \times 10^{18} \text{ cm}^{-3}$ ; (b)  $N_D = 3.1 \times 10^{18} \text{ cm}^{-3}$ ; (c) and  $N_D = 1.6 \times 10^{19} \text{ cm}^{-3}$ . Pad separation is  $100 \mu\text{m}$  in all cases. Please note the different voltage scale in the three figures.

336 high  $\rho_c$  limitation places restrictions on the use of this  
 337 metallization system; however, it could be accept-  
 338 able in some cases. For example, according to the  
 339 calculation reported by Cotal et al.<sup>16</sup> it could be used  
 340 with low or medium concentrator photovoltaic (CPV)  
 341 solar cells operating below 500 suns. Nevertheless,

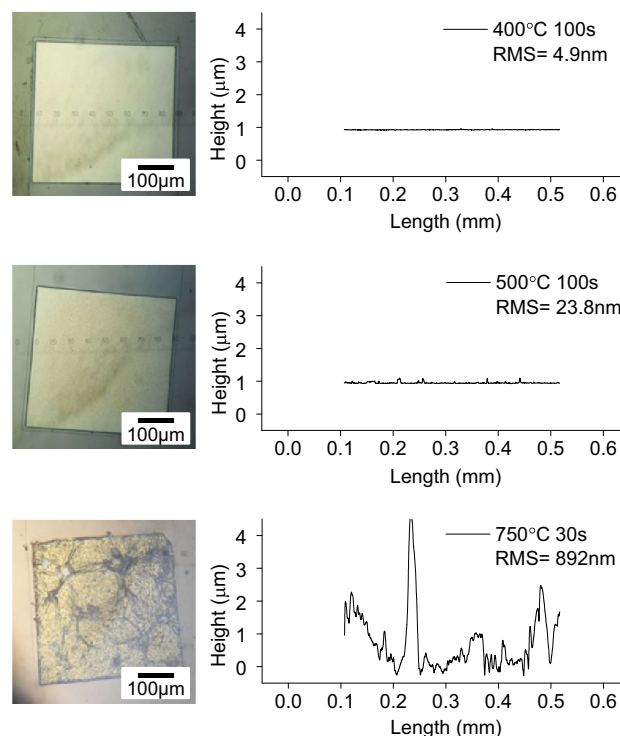


Fig. 4. Surface roughness of Ti/Pd/Ag contacts deposited on  $3.1 \times 10^{18} \text{ cm}^{-3}$  doped *n*-type GaAs with different annealing conditions.

given the fact that many CPV manufacturers are  
 moving their designs to ultra-high concentration  
 levels (above 1000 suns),  $\rho_c$  needs to be improved to  
 values below  $1 \times 10^{-5} \Omega \text{ cm}^2$ .

Table I also summarizes the results of metal  
 resistivity of the experiments in Fig. 3a-c. A first  
 fact observable in this table is that annealing  
 temperatures lower than  $500^\circ\text{C}$  seem not to affect  
 significantly the metal resistivity of the layer. The  
 metal resistivity barely increases after annealing  
 below  $500^\circ\text{C}$ . Furthermore, the average metal resis-  
 tivity of all these experiments from  $375^\circ\text{C}$  to  $500^\circ\text{C}$   
 is  $2.4 \times 10^{-6} \Omega \text{ cm}$  with a standard deviation of  
 around 6%, which is in agreement with the uncer-  
 tainty expected in the deposited thickness in our  
 e-gun evaporator. In other words, if there is a change  
 in metal resistivity associated with annealing the  
 samples for temperatures from  $375^\circ\text{C}$  to  $500^\circ\text{C}$ , it is  
 not observable due to the uncertainty in the  
 deposited thickness. However, this situation  
 changes for the samples processed at  $750^\circ\text{C}$ . In  
 such a case, the metal resistivity is highly degraded,  
 increasing by more than a factor of 30.

In order to gain insight into these changes of the  
 metal resistivity, the surface roughness of samples  
 annealed at different temperatures was measured  
 using a profilometer, as shown in Fig. 4. This  
 figure shows that sample roughness increases with  
 annealing temperature and surface roughness  
 (RMS) increases from 4.9 nm to 892 nm, reaching

a deleterious morphology for samples annealed at 750°C. In addition, the color of the metallization changed from silver to bronze-green after annealing at 750°C, evidencing some chemical (intermetallic) reactions between the components of the metal system possibly as a result of the blurring of the Ti/Pd barrier layer.<sup>35,36</sup> In summary, morphology degradation together with the degradation of Ag conductivity as a result of contamination could explain the degradation measured and calculated in the metal resistivity.

## SUMMARY AND CONCLUSIONS

Ti/Pd/Ag metallizations on *n*-GaAs have been studied in the quest for a metal system that can provide (1) low metal/semiconductor specific contact resistance; (2) low metal conductivity; (3) high long-term stability; (4) good bondability; and (5) low cost as compared to traditional gold-based systems.

In terms of contact resistance, we found that samples doped in the range of  $10^{18} \text{ cm}^{-3}$  had Schottky-like *I*-*V* characteristics, and only samples doped in the range of  $10^{19} \text{ cm}^{-3}$ , exhibited ohmic behavior even before RTA. For the Schottky contacts, we observed a decrease in the Schottky barrier with increasing RTA temperature. For the ohmic contacts, non-annealed samples had a metal/semiconductor specific contact resistance of  $\rho_c \sim 2 \times 10^{-3} \Omega \text{ cm}^2$ , whilst in annealed samples  $\rho_c$  decreased with RTA temperatures down to  $\rho_c \sim 5 \times 10^{-4} \Omega \text{ cm}^2$  for samples treated at 500°C. In samples annealed at 750°C,  $\rho_c$  went further down to  $\rho_c \sim 1 \times 10^{-4} \Omega \text{ cm}^2$  at the expense of a total degradation of the morphology and evidence of intermetallic reactions in the silver overlayer.

Regarding metal resistivity, we found that Ti/Pd/Ag contacts on *n*-type GaAs present a very good metal resistivity as far as RTA temperatures are kept below 500°C. In fact, our measurements show that the conductivity of the silver overlayer virtually equals that of pure bulk Ag. This fact would be in agreement with Ag being free of contamination and the Ti/Pd bilayer acting as an efficient diffusion barrier for Ga and As for temperatures below 500°C as observed in other works. Above this temperature, morphological degradation and contamination in the silver overlayer strongly degrade metal resistivity. These results have been compared to the classic AuGe/Ni/Au metal system for which metal/semiconductor specific contact resistance is two orders of magnitude lower ( $\rho_{c,\text{AuGe/Ni/Au}} \sim 3 \times 10^{-6} \Omega \text{ cm}^2$  and  $\rho_{c,\text{Ti/Pd/Ag}} \sim 5 \times 10^{-4} \Omega \text{ cm}^2$ ) while the metal resistivity is a factor of 10 larger ( $\rho_{\text{M,AuGe/Ni/Au}} \sim 2.4 \times 10^{-5} \Omega \text{ cm}$ , as compared  $\rho_{\text{M,Ti/Pd/Ag}} \sim 2.3 \times 10^{-6} \Omega \text{ cm}$ ).

In conclusion, the good metal resistivity of the Ti/Pd/Ag system shows promise to develop ohmic contacts to electronic devices that handle large current densities. The lowest values reached for the metal/semiconductor specific contact resistance

are still far from the records reported in the literature, though would be enough to be used in low or medium concentration solar cells (<500 suns). Future work will be dedicated to enhance the metal–semiconductor specific contact resistance, which could be accomplished by introducing other metal layers between Ti and GaAs.

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