



GRS Results for the Burnup Pin-cell Benchmark Propagation of Cross-Section, Fission Yields and Decay Data Uncertainties

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Outline

1. Introduction

- 1.1 the XSUSA Methodology
- **1.2** Extension to Fission Yields and Decay Data

2. Problem and Results

- 2.1 Description of the Burnup Pin-cell Benchmark
- 2.2 Impact on k-eff of Cross-Sections, Fission Yields and Decay Data Uncertainties
- 2.3 Impact on Isotopic Evolution
- 3. Conclusions and future work





1. Introduction: the XSUSA Methodology

- Influence of Engineering Parameters and Cross-Section Uncertainties
- Many calculations (typically >> 100) are run for the same problem with varied input data
- Variations are generated randomly from the probability distributions of the input parameters and correlations between them
- Output quantities are statistically analyzed, uncertainty ranges and sensitivities are determined
- Applications: Critical experiments. Transport calculations: multiplication factors, fission rate distributions

Full core calculations. MC and nodal diffusion: multiplication factors, power distributions Coupled nodal diffusion + thermo-hydraulics.

Fuel assembly depletion calculations. Multiplication factors, cross-sections, fission rates, nuclide inventories...

- XSUSA: Uncertainties through the generation of varied inputs and Cross-Sections (XS) and repeated simulation. Fission Yields (FY) and Decay Data (DD) uncertainties not propagated





Regarding depletion calculations, XSUSA has been dealing with cross-section uncertainties BUT missing the contribution coming from the temporal evolution of the nuclide inventory

- Accurate Burnup Simulation: Coupling between DEPLETION and TRANSPORT calculations





Which is the impact on nuclear calculations of uncertainties coming from decay data, fission yields and cross-sections when considered independently and altogheter ?





1. Introduction: Extension to Fission Yields and Decay Data

- XSUSA is updated to propagate uncertainties in Fission Yields and Decay Data
- XSUSA package includes two codes that generate pools of varied FY and DD libraries beforehand

- We vary the ORIGEN-S FY and DD libraries (ASCII files) respecting the information they contain (no additions, no replacements) according to the corresponding uncertainties found in ENDF/B-VII.1 through a gaussian sampling (MEDUSA) around the nominal values in ORIGEN-S libraries













2. Problem and Results: Description of the Burnup Pin-cell Benchmark

- The UAM-6 Burnup Pincell Benchmark (*)

Unit cell pitch (mm)	14.427
Fuel pellet diameter (mm)	9.391
Fuel pellet material	UO2
Fuel density (g/cm3)	10.283
Fuel enrichment (w/o)	4.85
Cladding outside diameter (mm)	10.928
Cladding thickness (mm)	0.673
Cladding material	Zircaloy-4
Cladding density (g/cm3)	6.55
Gap material	He
Moderator material	H2O
Fuel temperature (K)	900.0
Cladding Temperature (K)	600.0
Moderator (coolant) temperature (K)	562.0
Moderator (coolant) density (g/cm3)	0.7484
Reactor Power (MWt)	2772.0
Total number of fuel assemblies	177
Number of fuel rods per fuel assembly	208
Active core length (mm)	3571.20

Irradiation Characteristics

- simple pincell 4.85 % enrichment
- burnt at a constant power of 33.58 MW/MTU
- during **1825 days** to a burnup of **61.28 GWd/MTU**
- total decay time: 300 years

Data requested (at different time-steps)

- k-inf uncertainties Main nuclide reactions contributions + contribution of chi, nu-bar and others

- Reaction rates and uncertainties for major isotopes
 - capture for U235,238 and Pu239,240,241
 - fission for U235,238 and Pu239, 240,241
 - two-group macroscopic cross sections and uncertainties for thehomogenized pin-cell absorption, fission, nu-fission and diffusion

- Nuclide concentrations (15 Acts + 36 FPs)

* BENCHMARK FOR UNCERTAINTY ANALYSIS IN MODELING (UAM) FOR DESIGN, OPERATION AND SAFETY ANALYSIS OF LWRs, Addition to V.I: Specification and Support Data for the Neutronics Cases (Phase I) "PWR Burnup Pin-Cell Benchmark" O. Cabellos and K.Ivanov





Objectives

- Application of the extended XSUSA methodology to a simple test as a proof of principle
- Assessment of the impact on k-eff and the isotopic evolution of the independent and joint propagation of the different nuclear data uncertainties: XS, FY and DD

Simulations performed

- Generation of 1000 of varied Fission Yields libraries and 1000 of varied Decay Data libraries
- Nominal calculation based on the original unchanged libraries

Data Analyzed

- k-eff at EOB. Total Uncertainty and contribution from the different uncertainty sources
- Nuclide concentrations, uncertainties and contributions
- Comparison to the the results provided by other institutions





— Nominal k-eff ▼ k-eff [DD]



























K-eff uncertainty finds its major contributor in XS > FY > DD (negligible) all over the irradiation





Col.	Parm.	Var.	0 GWd/MTU	10 GWd/MTU	20 GWd/MTU	30 GWd/MTU	40 GWd/MTU	50 GWd/MTU	60 GWd/MTU	shutdown
UPM	Nom		1,4045	1,2461	1,1581	1,0837	1,0167	0,9560	0,9030	
. <u> </u>	Uncert	Xs.	0.49%	0.51%	0.57%	0.63%	0.68%	0.74%	0.79%	
GRS	Nom		1,4029	1,2474	1,1623	1,0913	1,0270	0,9688	0,9169	0,9102
	Uncert	Xs	0,48%	0,49%	0,55%	0,60%	0,65%	0,70%	0,75%	0,75%
		FY	0,0%	0,17%	0,21%	0,28%	0,32%	0,36%	0,37%	0,38%
		Tot.	0,48%	0,51%	0,58%	0,67%	0,73%	0,79%	0,84%	0,84%
NRG	Nom		1,41	1,25	1,16	1,08	1,02	0,955	0,901	
	Uncert	U-235	0,50%	0,44%	0,39%	0,35%	0,32%	0,28%	0,24%	
		U-238	0,46%	0,48%	0,45%	0,40%	0,35%	0,33%	0,36%	
		Pu-239	0,05%	0,15%	0,26%	0,33%	0,39%	0,44%	0,47%	
		L FPs	0,05%	0,37%	0,36%	0,32%	0,23%	0,29%	0,28%	
		FY	0,05%	0,18%	0,19%	0,21%	0,21%	0,19%	0,17%	
		Tot.	0,68%	0,79%	0,78%	0,76%	0,76%	0,76%	0,79%	





		0 GWd/MTU	10 GWd/MTU				30	0 GWd	/MTU		60 GWd/MTU			
		mean	mean	rel. std. dev.			mean	rel. std. dev.			mean rel. std. d			ev.
				ΔXS	ΔDD	ΔFYs		ΔXS	ΔDD	ΔFYs		ΔXS	ΔDD	ΔFYs
U-234	UPM	1.17E-05	1.03E-05	1.0	0.0	-	7.94E-06	1.9	0.0	-	5.04E-06	3.1	0.0	-
	NRG	1.17E-05	1.03E-05	0.1			7.92E-06	0.4			4.97E-06	0.9		
	GRS	1.13E-03	8.72E-04	0.8	0.0	0.02	4.98E-04	2.6	0.0	0.09	1.74E-04	5.7	0.0	0.30
U-235	UPM	1.13E-03	8.71E-04	0.2	0.0	-	4.97E-04	0.3	0.0	-	1.74E-04	0.6	0.0	-
	NRG	1.13E-03	8.75E-04	0.2			5.02E-04	0.7			1.75E-04	2.8		
	GRS	0.00E+00	4.87E-05	0.1	0.0	0.01	1.15E-04	0.5	0.0	0.06	1.58E-04	1.9	0.0	0.35
U-238	UPM	2.18E-02	2.17E-02	0.0	0.0	-	2.14E-02	0.1	0.0	-	2.08E-02	0.1	0.0	-
	NRG	2.18E-02	2.17E-02	0.0			2.14E-02	0.0			2.08E-02	0.0		
	GRS	0.00E+00	4.87E-05	0.01	0.0	0.0	1.15E-04	0.02	0.0	0.06	1.58E-04	0.04	0.0	0.35
Pu-238	UPM	0.00E+00	1.24E-07	2.3	0.0	-	2.08E-06	1.4	0.0	-	1.07E-05	0.9	0.0	-
	NRG	0.00E+00	1.22E-07	12.1			2.15E-06	5.0			1.14E-05	2.7		
	GRS	0.00E+00	8.07E-05	7.6	0.0	0.2	1.45E-04	4.4	0.0	0.24	1.57E-04	0.04	0.0	0.32
Pu-239	UPM	0.00E+00	8.08E-05	1.2	0.0	-	1.46E-04	1.1	0.0	-	1.60E-04	1.3	0.0	-
	NRG	0.00E+00	7.78E-05	1.8			1.40E-04	2.3			1.53E-04	3.2		
	GRS	0.00E+00	9.36E-06	1.2	0.0	0.1	4.00E-05	1.5	0.0	0.2	7.53E-05	2.0	0.0	0.46
Pu-240	UPM	0.00E+00	9.36E-06	3.1	0.0	-	4.01E-05	2.1	0.0	-	7.59E-05	1.9	0.0	-
	NRG	0.00E+00	9.09E-06	1.9			3.89E-05	2.0			7.39E-05	2.4		
	GRS	0.00E+00	3.55E-06	1.6	0.0	0.07	2.47E-05	1.9	0.0	0.11	4.67E-05	2.2	0.0	0.27
Pu-241	UPM	0.00E+00	3.55E-06	2.9	0.0	-	2.46E-05	1.7	0.0	-	4.68E-05	1.5	0.0	-
	NRG	0.00E+00	3.42E-06	2.0			2.42E-05	1.5			4.59E-05	2.2		
	GRS	0.00E+00	1.98E-07	1.6	0.0	0.16	4.96E-06	1.4	0.0	0.16	2.33E-05	1.8	0.0	0.32
Pu-242	UPM	0.00E+00	1.98E-07	3.7	0.0	-	4.95E-06	1.9	0.0	-	2.31E-05	1.4	0.0	-
	NRG	0.00E+00	1.92E-07	3.0			4.98E-06	1.9			2.40E-05	1.4		
	GRS	0.00E+00	1.98E-07	2.0	0.0	0.14	4.96E-06	2.3	0.0	0.10	2.33E-05	3.6	0.0	0.21





		0 GWd/MTU	10 GWd/MTU				30) GWd	/MTU		60 GWd/MTU				
		mean	mean	rel. std. dev.			mean	rel. std. dev.			mean rel. std.		. std. de	ev.	
				ΔXS	ΔDD	ΔFYs		ΔXS	ΔDD	ΔFYs		ΔXS	ΔDD	ΔFYs	
Gd-155	UPM	0.00E+00	5.06E-10	12.4	0.2	5.1	2.23E-09	15.2	0.2	2.4	5.80E-09	15.4	0.2	1.1	
	NRG	0.00E+00	5.06E-10	27.0			2.30E-09	22.4			6.02E-09	22.8			
	GRS	0.00E+00	1.56E-07	4.9	0.27	15	1.34E-06	6.0	0.24	9.8	7.63E-06	5.3	0.20	8.8	
Nd-143	UPM	0.00E+00	1.23E-05	0.6	0.0	2.6	3.23E-05	0.5	0.0	1.4	4.79E-05	0.5	0.0	1.1	
	NRG	0.00E+00	1.21E-05	4.4			3.20E-05	4.9			4.72E-05	6.6			
	GRS	0.00E+00	9.11E-06	0.3	0.05	3.9	2.46E-05	0.9	0.03	4.5	4.20E-05	2.1	0.03	5.9	
Nd-145	UPM	0.00E+00	9.10E-06	0.7	0.0	2.8	2.46E-05	0.5	0.0	1.6	4.18E-05	0.5	0.0	1.1	
	NRG	0.00E+00	9.05E-06	4.9			2.48E-05	6.7			4.28E-05	10.9			
	GRS	0.00E+00	7.53E-06	0.3	0.0	4.6	2.35E-05	1.0	0.0	5.2	5.05E-05	2.0	0.0	6.7	
Nd-148	UPM	0.00E+00	4.20E-06	0.7	0.0	2.1	1.24E-05	0.5	0.0	1.3	2.45E-05	0.4	0.0	0.9	
	NRG	-	-				-				-				
	GRS	0.00E+00	1.76E-06	0.3	0.0	16.5	5.58E-06	0.3	0.0	14.5	1.18E-05	0.4	0.0	13	

UPM: ΔN due to ΔXS , ΔFYs and ΔDD

GRS: ΔN due to $\Delta XS,$ ΔFYs and ΔDD

NRG: ΔN due to $\Delta XS+FYs$





		0 GWd/MTU	10 GWd/MTU				30) GWd/	'MTU		60 GWd/MTU				
		mean	mean rel. std. dev.			mean	re	. std. d	ev.	mean	rel. std. dev.				
				ΔXS	ΔDD	ΔFYs		ΔXS	ΔDD	ΔFYs		ΔXS	ΔDD	ΔFYs	
Sm-149	UPM	0.00E+00	1.17E-07	14.0	0.0	6.4	1.21E-07	14.3	0.0	5.7	1.05E-07	15.5	0.0	5.1	
	NRG	0.00E+00	1.09E-07	11.4	0.0		1.15E-07	10.8	0.3		9.97E-08	11.3	0.3		
	GRS	0.00E+00	2.76E-06	1.7		10.1	9.28E-06	2.0		9.5	1.91E-05	2.5		10.6	
Sm-152	UPM	0.00E+00	1.30E-06	1.0	0.0	1.9	3.47E-06	1.2	0.0	1.3	5.26E-06	1.6	0.0	0.9	
	NRG	0.00E+00	1.25E-06	16.2			3.47E-06	13.3			5.37E-06	11.7			
	GRS	0.00E+00	2.51E-07	0.8	0.0	15.2	9.61E-07	1.8	0.1	11.3	2.41E-06	2.9	0.1	8.8	
Cs-133	UPM	0.00E+00	1.55E-05	0.7	0.0	2.0	4.36E-05	0.5	0.0	1.1	7.63E-05	0.4	0.0	0.9	
	NRG	0.00E+00	1.50E-05	3.5			4.25E-05	3.7			7.48E-05	5.4			
	GRS	0.00E+00	4.79E-07	0.2	0.0	3.2	3.72E-06	0.5	0.0	1.7	1.15E-05	1.2	0.0	1.7	
Cs-137	UPM	0.00E+00	1.51E-05	0.7	0.1	2.6	4.43E-05	0.5	0.0	1.6	8.59E-05	0.4	0.0	1.2	
	NRG	0.00E+00	1.49E-05	2.2			4.42E-05	2.0			8.62E-05	2.1			
	GRS	0.00E+00	1.54E-05	0.0	0.2	1.9	4.47E-05	0.0	0.2	1.7	8.59E-05	0.0	0.2	1.7	
Mo-95	UPM	0.00E+00	8.36E-06	1.0	0.0	9.7	3.55E-05	0.7	0.0	6.8	6.90E-05	0.5	0.0	4.8	
	NRG	0.00E+00	8.28E-06	4.9			3.56E-05	5.8			6.97E-05	7.6			
	GRS	0.00E+00	1.48E-05	0.1	0.1	5.2	4.15E-05	0.2	0.1	6	7.41E-05	0.4	0.1	7.9	
Tc-99	UPM	0.00E+00	1.47E-05	0.7	0.0	2.6	4.15E-05	0.5	0.0	1.6	7.44E-05	0.4	0.0	1.3	
	NRG	0.00E+00	1.42E-05	10.4			4.08E-05	9.4			7.39E-05	9.1			
	GRS	0.00E+00	1.29E-05	0.1	0.0	11.2	3.84E-05	0.2	0.01	9.9	7.47E-05	0.4	0.1	9.5	

UPM: ΔN due to ΔXS , ΔFYs and ΔDD GRS: ΔN due to ΔXS , ΔFYs and ΔDD NRG: ΔN due to $\Delta XS+FYs$





IN SHORT

- The **GRS / XSUSA** methodology accounts for **cross-sections and engineering** uncertainties. Now, in addition, it takes into account **fission yields and decay data** uncertainties from ENDF-6 libs.
- Tools to generate pools of varied libraries for **ORIGEN-S** have been developed (**YiSaB** and **DeSaB**) and their outputs are used following the **XSUSA** method of repeated calculations
- The **XSUSA** extended capabilities have been applied to the UAM-6 burnup pincell benchmark.

<u>On k-eff</u>: low impact from decay data uncertainties, Xs main contributors to its uncertainty <u>On inventory</u>: depending on the nuclide, fission yields and cross-section uncertainties

FUTURE WORK

- Integration of **YiSaB** and **DeSaB** within the **XSUSA** flow chart so they generate libraries on the fly
- Application of the methodology to complex problems
- **Inclusion of correlations** to be taken into account in the **MEDUSA** sampling of the fission yields (GRS ORNL collaboration)





Thank you very much for your attention

Questions?