Parametrization of the average ionization and radiative cooling rates of carbon plasmas in a wide range of density and temperature

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ABSTRACT

In this work we present an analysis of the influence of the thermodynamic regime on the monochromatic emissivity, the radiative power loss and the radiative cooling rate for optically thin carbon plasmas over a wide range of electron temperature and density assuming steady state situations. Furthermore, we propose analytical expressions depending on the electron density and temperature for the average ionization and cooling rate based on polynomial fittings which are valid for the whole range of plasma conditions considered in this work.

1. Introduction

A detailed knowledge of the radiation distribution and in particular of the radiative power loss and cooling rate is necessary in order to understand the behavior of plasmas in which radiative heating and cooling processes are important. The radiative power loss is of great interest for thermonuclear fusion device as well as in both laboratory and astrophysical plasmas. For example, it plays an important role in the current decays after disruptions in magnetic nuclear fusion confinement devices in which disruptions are assumed to be caused by strongly radiating impurities and where hot tail runaway or supra-thermal electrons generation is caused by incomplete thermalization of the electron velocity distribution during the rapid plasma cooling [1]. It was recognized that radiation losses from the impurities

produced by plasma-wall interaction can hinder the plasma heating to thermonuclear temperatures and the concentration, being 'lethal' for fusion, have been estimated for different impurity species [2,3]. Moreover, while the heat conduction plays a stabilizing role on the thermal stability at the plasma edge, radiation losses from impurities can develop thermal instability [4,5]. On the other hand, the impurity radiation at the plasma edge of fusion device can also play a positive role by reducing the heat outflows to the certain wall elements, the anomalous heat and the particle losses from the plasma [6,7] or to mitigate disruption induced problems it has been proposed that 'killer' pellets could be injected into the plasma in order to safely terminate the discharge [8,9]. Besides, radiative power loss plays a very important role in the structure and behavior of radiative shock waves present in laboratory plasmas such as the velocity and the stability properties of radiative shock or the characteristics of the radiative precursor [10-13]. And, finally, in many astrophysical systems as radiative blast waves in the context of supernova remnants [14-16], radiative precursor shock waves with applications to the studies of stellar jets [17,18], pulsating stars [19] and accretion shock during star formation [20], radiatively collapsing jets relevant for protostellar outflows [21,22] or analysis of X-ray spectra of the cores of clusters of galaxies [23–25].

On the other hand, carbon is one of the most important elements under investigation in the research areas commented above. For example, in astrophysics, due to its abundance in the stars; in magnetic nuclear fusion confinement, because it is likely to be a major plasma-facing wall component in the international experimental reactor (ITER) and it is present as impurity in a lot of devices; and it plays a major role in inertial fusion scenarios, for example, in the direct-drive implosion cores where the deuterium target has a wall of plastic shells. Therefore, calculations of the radiative properties, and in particular the radiative power loss and cooling rate, of carbon plasmas over a wide range of plasma conditions are very useful. The calculations of these radiative properties for optically thin carbon plasma have been carried out by several authors at low densities and over a wide range of temperatures where the coronal equilibrium (CE) is achieved [26-28] and at moderate and high densities where the non-local and local thermodynamic equilibrium (NLTE and LTE) are achieved, respectively [29,30]. Furthermore, at low densities, there are some analytical formulas for the cooling rates obtained by means of fittings to a polynomial expressions of the temperature of databases assuming CE [26,31].

In a previous work [32], we presented a systematic calculation of average ionization, ionic and level populations of the optically thin carbon plasma in a wide range of plasma conditions. We showed that the comparison between the average ionization and ion and level populations calculated from collisional-radiative steady state (CRSS), corona and Saha-Boltzmann (SAHA) equations could provide information about the thermodynamic regime of the plasma, i.e. the plasma conditions where CE, LTE and NLTE regimes could be assumed. In the subsequent work [33] we presented a study of spectrally resolved, multigroup and mean opacities of carbon plasmas in a wide range of plasma conditions analyzing the effect of the thermodynamic regimes in these magnitudes. This work is a continuation of these previous ones, where we calculate the spectrally resolved emissivity, the radiative power loss and the radiative cooling rate of optically thin carbon plasmas assuming steady state situations and in a wide range of electron densities and temperatures which cover situations where CE, NLTE and LTE regimes are found. We perform an analysis of the influence of the thermodynamic regime in these quantities and we also present a parametrization of the cooling rate obtained by fitting bi-dimensional polynomial expressions (depending on the electron density and temperature) to our calculations which is valid in a wide range of electron temperatures (1-1000 eV) and electron densities (10¹⁰-10²¹ cm⁻³) covering CE, LTE and NLTE regimes. All the calculations presented in this work were made using ABAKO/RAPCAL computational package [34–36] which is briefly described in the next section. In Section 3 the analysis of the monochromatic emissivity, the radiative power loss and the cooling rate is made and the

parametrization of the average ionization and the cooling rate is also presented. Finally, Section 4 is devoted to main conclusions and general remarks.

2. Theoretical model

The calculations in this work were performed using the computational package ABAKO/RAPCAL [36] that consists of two codes, ABAKO [35] and RAPCAL [34]. In this section, a brief description of them is made.

2.1. ABAKO

In order to determine the plasma level populations, in ABAKO a collisional-radiative steady state (CRSS) model is implemented. Following the standard NLTE modeling approach, where an account of the existing atomic states is made and the microscopic (radiative and collisional) processes connecting these states are identified, a rate equation system describing the population density of the atomic states is built and solved, giving the population distribution. Therefore, to find the level population distribution the following system of rate equations is solved:

$$\sum_{\zeta'j} N_{\zeta'j} \mathbb{R}^+_{\zeta'j \to \zeta i} - \sum_{\zeta'j} N_{\zeta i} \mathbb{R}^-_{\zeta i \to \zeta'j} = 0, \tag{1}$$

where $N_{\zeta i}$ is the population density of the atomic level i of the ion with charge state ζ . The terms $\mathbb{R}^+_{\zeta j \to \zeta i}$ and $\mathbb{R}^-_{\zeta j \to \zeta i}$ take into account all the atomic processes which contribute to populate and depopulate the state ζi , respectively. In this paper no radiation-driven processes are explicitly considered. In ABAKO it is assumed that the system has had enough time to thermalize and, therefore, both the electrons and ions have a Maxwell–Boltzmann type energy distribution. Furthermore, in ABAKO it is also assumed that electron and ion temperatures are equal. Therefore, in the following, it will denote the plasma temperature by the electron temperature T_e .

The CRSS model implemented in ABAKO is applied for the calculation of the plasma level populations for arbitrary optical depths in both LTE and NLTE conditions using a CRSS model. The CRSS model is solved level by level (or configuration by configuration, depending on the atomic description) and it is applied to low-to-high Z ions under a wide range of plasma conditions: CE, NLTE or LTE, optically thin and thick plasmas. Special care was taken during the development of our CRSS model to achieve an optimal balance between accuracy and computational cost. Hence, analytical expressions have been employed for the rate coefficients of the atomic processes included in the CRSS model, which yield a substantial saving of computational requirements, but still providing satisfactory results in relation to those obtained from more sophisticated codes and experimental data as it has been shown in recent NLTE code comparison workshops [37–39]. The processes included in the CRSS model are the following: collisional ionization [40] and three-body recombination, spontaneous decay, collisional excitation [41] and deexcitation, radiative recombination [42], electron capture and autoionization. We have added between brackets the references wherefrom their approximated analytical

rate coefficients have been acquired. The rates of the inverse processes are obtained through the detailed balance principle. It is worth pointing out that the autoionizing states are included explicitly. It has been shown that these contributions are critical to the determination of the ionization balance. The cross section of the autoionization is evaluated using detailed balance principle from the electron capture cross section which is obtained from the collisional excitation cross section using the approximation given in Ref. [43].

Since the number of rate equations is large due to the number of atomic levels involved, ABAKO makes use of the technique of sparse matrices to storage the non-zero elements of the coefficient matrix of the system, which implies substantial savings in memory requirement. For the matrix inversion we use iterative procedures [36] because they entail much less memory than direct methods and they are faster as well.

The atomic data employed in this work were obtained from FAC code [44]. The calculations were carried out in the detailed level accounting (DLA) approach. The radiative transition rates in FAC are calculated in the single multipole approximation, and in this work they were obtained in the electric dipole approach. Furthermore, configuration interactions within the levels belonging to the same nonrelativistic configuration have been included since it has been shown that for carbon plasmas, for plasma conditions in which the less ionized ions are present, the effect of configuration interaction is noticeable [45]. In Table 1 the set of relativistic configurations and the numbers of resulting levels and line transitions included for each carbon ion in the calculation of the level populations and opacities is shown. In the table $(n)^{w}$ denotes all the possible relativistic configurations that arise from the shell n with w bound electrons. Finally, the continuum lowering due to the influence of the plasma surrounding is also considered. In this work, this one is calculated by means of the expression due to Stewart and Pyatt [46]. Because of the inclusion of the continuum lowering, the kinetics equations must be solved iteratively, since the atomic data depend on the ionization balance.

2.2. RAPCAL

RAPCAL code was developed to obtain several relevant plasma radiative properties such as the monochromatic absorption and emission coefficients, mean and multigroup opacities, source functions, radiative power losses, specific intensities and plasma transmission. A detailed description of the code can be found in [34]. For this work, the interest has been focused on the monochromatic emissivity, the radiative power loss and the radiative cooling rate. The monochromatic emissivity is denoted in this work as j(v) and includes the bound-bound, bound-free and free-free contributions

$$j(v) = j_{bb}(v) + j_{bf}(v) + j_{ff}(v)$$
 (2)

where v is the photon frequency. The bound-bound contribution to the emissivity is given by

$$j_{bb}(v) = \sum_{\mathcal{L}} \sum_{i,i} j_{\mathcal{L}_j \to \mathcal{L}_i}(v), \tag{3}$$

with

$$j_{\zeta j \to \zeta i}(\nu) = \frac{h\nu}{4\pi} N_{\zeta j} A_{\zeta j \to \zeta i} \phi_{ij}(\nu), \tag{4}$$

where $A_{ij \to \zeta i}$ is the Einstein coefficient for spontaneous deexcitation [47] between the bound states j, i of the ion ζ , h is Planck's constant, $N_{\zeta j}$ is the population density of the atomic level j of the ion with charge state ζ and $\phi_{ij}(v)$ represents the line profile. In its evaluation, natural, Doppler and electron-impact [48] broadenings were included. The line-shape function is applied with the Voigt profile that incorporates all these broadenings. The bound–free contribution to the emissivity is determined by means of

$$j_{bf}(v) = \sum_{\zeta,i} \sum_{\zeta,j} j_{\zeta+1j\to\zeta i}(v),\tag{5}$$

with

$$j_{\zeta+1j\to\zeta i}(v) = \frac{h}{2\pi c^2} \left(\frac{1}{2m_e}\right)^{3/2} N_{\zeta+1j} N_e f(\varepsilon) \frac{g_{\zeta i}}{g_{\zeta+1j}} \cdot \frac{(hv)^3}{\varepsilon^{1/2}} \sigma_{\zeta i\to\zeta+1j}^{pho}(v), \tag{6}$$

with ε being the energy of the free electron, m_e the electron mass, N_e the electron number density and $g_{\zeta i}$ and $g_{\zeta +1j}$ are the statistical weights of the i and j levels, respectively. In ABAKO a Maxwell-Boltzmann distribution, $f(\varepsilon)$, at temperature T_e for the free electrons is assumed. The photoionization cross section, $\sigma^{pho}_{\zeta i \to \zeta +1j}(v)$, has been evaluated using the semiclassical expression of Kramers [42].

Table 1Set of configurations and the numbers of relativistic configurations, levels and line transitions considered in the calculations performed by ABAKO/RAPCAL code for carbon ions ($n \le 10$, $n' \le 6$).

	C-like	B-like	Be-like	Li-like	He-like	H-like
	(2)4	(2) ³	(2) ²	(2)1	1 <i>s</i> ²	1s ¹
	$(2)^{3}nl$	$(2)^{2}nl$	$(2)^{1}nl$	$1s^2nl$	$1s^1nl$	nl
	$(2)^2(3)^2$	$(2)^{1}(3)^{2}$	$(3)^2$	$1s^{1}(2)^{2}$	$(2)^2$	
	$(2)^2(3)^1 n'l$	$(2)^{1}(3)^{1}n'l$	$(3)^{1}n'l$	$1s^{1}(2)^{1}n'l$	$(2)^1 n'l$	
		$1s^{1}(2)^{4}$	$1s^{1}(2)^{3}$	$1s^{1}(3)^{2}$	$(3)^2$	
		$1s^{1}(2)^{3}n'l$	$1s^{1}(2)^{2}n'l$	$1s^{1}(3)^{1}n'l$	$(3)^{1}n'l$	
Configurations	1677	1299	644	519	352	100
Levels	16,616	8871	2789	2642	910	100
Transitions	864,448	250,073	45,671	54,433	9386	742

For the free-free contributions to the emissivity the Kramers semi-classical expression for the inverse brems-strahlung cross section has been used [49]

$$\sigma_{\zeta}^{ibr}(v) = \frac{16\pi^2 e^2 h^2 \alpha}{3\sqrt{3}(2\pi m_e)^{3/2}} \frac{\zeta^2 N_e}{T_e^{1/2} (hv)^3}.$$
 (7)

Assuming a Maxwell-Boltzmann distribution for the free electrons, it is obtained that

$$j_{ff}(v) = \frac{32\pi^2 e^4 a_0^2 \alpha^3}{\sqrt{3} (2\pi m_e)^{3/2} h} \left(\frac{m_e}{2\pi T_e}\right)^{1/2} \overline{Z^2} N_{ion} N_e e^{-hv/T_e}, \tag{8}$$

where N_{ion} is the ion number density. The radiative power loss is evaluated as following [50] in (eV/s/ion). For the bound-bound contribution

$$P_{bb}(N_e, T_e) = \sum_{\zeta} \sum_{ij} h v_{ij} A_{ij} N_{\zeta j}. \tag{9}$$

The bound-free contribution is given by

$$P_{bf}(N_e, T_e) = 4\pi \sum_{\zeta} \sum_{ij} N_{\zeta i} \left(\frac{N_{\zeta+1j} N_{\zeta}}{N_{\zeta i} N_{\zeta+1}} \right)^{LTE}$$

$$\times \int_{\nu_0}^{\infty} \sigma_{\zeta i \to \zeta+1j}^{pho}(\nu) \left(\frac{2h\nu^3}{c^2} \right) e^{-h\nu/T_e} d\nu,$$
(10)

where v_0 is the threshold energy and the LTE population ratio is obtained from the Saha equation. The contribution from the free–free transitions is given for a pure Coulomb

field as following [51]

$$P_{ff}(N_e, T_e) = 9.55 \times 10^{-14} N_e T_e^{1/2} \sum_{\zeta} Z_{\zeta}^2 N_{\zeta}, \tag{11}$$

where it has been assumed that the gaunt factor equals to unity. The total radiative power loss is then obtained as the sum of the three contributions, and the cooling rate is evaluated as

$$\Lambda(N_e, T_e) = \frac{(P_{bb} + P_{bf} + P_{ff})}{N_e N_{low}}.$$
 (12)

Finally, in this work we have performed a polynomial fitting in powers of the logarithm of the electron densities and temperatures of the average ionization and the cooling rates obtained from ABAKO/RAPCAL simulations for the whole range of electron temperatures and densities considered in this work. If *A* denotes the magnitude to fit, the analytical expression employed for the fitting is the following:

$$\log A(N_e, T_e) = \sum_{i=0}^{n} \sum_{j=0}^{m} C_{ij} (\log N_e)^{i} (\log T_e)^{j}.$$
 (13)

The maximum degrees of the polynomial fitting were fixed to 7 both for the electron density and electron temperature in order to avoid oscillating behaviors. For the fitting it was required relative errors lower than 1% for the average ionization and lower than 10% for the cooling rates. Obviously, as the error imposed becomes more

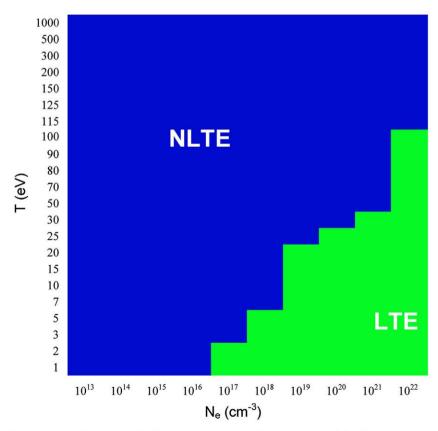


Fig. 1. Thermodynamic regimes for an optically thin carbon plasma in steady state in terms of the electron temperature and density.

restrictive the number of polynomial functions needed to make the fit of the whole range of plasma conditions increases. We have already used this kind of polynomial fit for Kr and Xe plasma for ranges of plasma conditions typically found in laboratory experiment of blast waves launched in cluster of gases [52].

3. Results

This section is divided into four parts. The first one is devoted to the analysis of the average ionization and the thermodynamic regimes as a function of the plasma conditions. This study will allow us to identify which are the most abundant ions that contribute to the monochromatic emissivity of the optically thin carbon plasmas and also when LTE or NLTE regimes can be assumed. In the second part a study of the influence of the thermodynamic regime into the monochromatic emissivity is carried out, by means of the comparison between the ones calculated using the CRSS and the SAHA equations implemented in ABAKO. In the third part, a similar analysis on the radiative power loss and the radiative cooling rate is performed. Finally, the last part is devoted to the parametrization of the average ionization and radiative cooling rates and the coefficients of the corresponding formulas are listed in Appendix A. The ranges of electron temperatures and densities considered in this work are $1-10^3$ eV and $10^{10}-10^{21}$ cm⁻³, respectively.

3.1. Average ionization and thermodynamic regimes

The wide range of plasma conditions considered in this work covers different thermodynamic regimes, i.e. LTE or NLTE. The knowledge of the plasma regime for a given density and temperature condition could entail a considerable saving in calculation time since the resolution of SAHA equations is considerably faster than CRSS ones and the complexity is also reduced. Therefore, it is very useful to have criteria that permit us to establish the thermodynamic regime of the plasma for the given electron temperature and density. We have employed a criterion that can state the regime of the whole plasma: when the ion populations, p_i , calculated from SAHA equations, p_i^{SAHA} , present a mean deviation Δp , with respect to those obtained from the CRSS model, p_i^{CRSS} , smaller than a certain value imposed Δp^* then it is considered that LTE regime has been achieved. Otherwise, the plasma is under NLTE conditions. The mean deviation is calculated as

$$\Delta p^{LTE} = \sqrt{\frac{\sum_{i} (p_i^{CRSS} - p_i^{SAHA})^2}{\sum_{i} (p_i^{SAHA})^2}} \le \Delta p^*, \tag{14}$$

where i runs over the whole set of ions included in the calculations. Fixing $\Delta p^* = 0.1 (= 10\%)$ we obtain the map of the thermodynamic regimes showed in Fig. 1. We have checked that, with this value, the criterion proposed to classify the thermodynamic regime of the whole plasma

 Table 2

 Average ionization calculated using ABAKO for the range of electron densities $10^{10} - 10^{15}$ g cm⁻³ and all the temperatures considered in this work.

T_e (eV)	N_e (cm ⁻³)						
	1010	1011	10 ¹²	10 ¹³	1014	10 ¹⁵	
1.0000	0.6700	0.6768	0.7056	0.7747	0.8501	0.8591	
1.2600	0.9409	0.9446	0.9587	0.9762	0.9857	0.9869	
1.5800	0.9834	0.9850	0.9910	0.9970	0.9993	1.0009	
2.0000	1.0049	1.0059	1.0096	1.0166	1.0337	1.0726	
2.5100	1.0990	1.1011	1.1130	1.1563	1.3014	1.5217	
3.1600	1.3998	1.4066	1.4457	1.5452	1.7456	1.8958	
3.9800	1.7481	1.7557	1.7937	1.8549	1.9360	1.9943	
5.0100	1.9549	1.9617	1.9923	2.0239	2.0526	2.2060	
6.3100	2.2851	2.3040	2.3657	2.4030	2.4472	2.7169	
7.9400	2.9939	3.0184	3.0543	3.0686	3.0988	3.2289	
10.0000	3.6843	3.6894	3.6926	3.6944	3.7009	3.7435	
12.5900	3.9246	3.9250	3.9252	3.9254	3.9267	3.9369	
15.8500	3.9794	3.9794	3.9794	3.9795	3.9799	3.9825	
19.9500	3.9931	3.9931	3.9932	3.9932	3.9933	3.9942	
25.1200	3.9973	3.9973	3.9973	3.9973	3.9974	3.9977	
31.6200	3.9994	3.9994	3.9994	3.9994	3.9995	3.9996	
39.8100	4.0101	4.0101	4.0101	4.0101	4.0102	4.0105	
50.1100	4.0993	4.0992	4.0992	4.0992	4.0998	4.1031	
63.1000	4.4416	4.4416	4.4416	4.4418	4.4436	4.4563	
79.4300	4.9202	4.9202	4.9202	4.9204	4.9220	4.9328	
100.000	5.3746	5.3746	5.3746	5.3747	5.3753	5.3795	
125.890	5.7125	5.7125	5.7125	5.7125	5.7127	5.7140	
158.490	5.8856	5.8856	5.8856	5.8856	5.8857	5.8861	
199.530	5.9505	5.9505	5.9505	5.9505	5.9506	5.9507	
251.190	5.9765	5.9765	5.9765	5.9765	5.9765	5.9766	
316.230	5.9877	5.9877	5.9877	5.9877	5.9877	5.9878	
398.110	5.9931	5.9931	5.9931	5.9931	5.9931	5.9931	
501.190	5.9958	5.9958	5.9958	5.9958	5.9958	5.9958	
630.960	5.9973	5.9973	5.9973	5.9973	5.9973	5.9973	
794.330	5.9982	5.9982	5.9982	5.9982	5.9982	5.9982	
1000.00	5.9988	5.9988	5.9988	5.9988	5.9988	5.9988	

Table 3

Average ionization calculated using ABAKO for the range of electron densities $10^{16} - 10^{21}$ g cm⁻³ and all the temperatures considered in this work.

T_e (eV)	$N_{\rm e}~({\rm cm}^{-3})$						
	1016	10 ¹⁷	1018	10 ¹⁹	10 ²⁰	10 ²¹	
1.0000	0.7392	0.3178	0.0541	0.0082	0.0019	0.0012	
1.2600	0.9725	0.8519	0.4050	0.0832	0.0189	0.0084	
1.5800	1.0006	0.9747	0.7953	0.3253	0.1075	0.039	
2.0000	1.1267	1.0864	0.9365	0.5648	0.2864	0.131	
2.5100	1.6962	1.6505	1.2384	0.7513	0.4837	0.298	
3.1600	1.9653	1.9704	1.7908	1.1532	0.6921	0.501	
3.9800	2.1481	2.2967	2.1038	1.6703	1.0742	0.736	
5.0100	2.6786	2.8575	2.7154	2.1035	1.5616	1.054	
6.3100	3.0453	3.2680	3.2377	2.7284	2.0150	1.431	
7.9400	3.5223	3.7862	3.7834	3.3739	2.5025	1.853	
10.0000	3.8753	3.9561	3.9532	3.8015	3.0827	2.334	
12.5900	3.9694	3.9891	3.9864	3.9277	3.5745	2.855	
15.8500	3.9910	3.9965	3.9945	3.9648	3.7969	3.314	
19.9500	3.9968	3.9986	3.9972	3.9795	3.8636	3.569	
25.1200	3.9987	3.9994	3.9984	3.9870	3.9116	3.749	
31.6200	4.0001	4.0007	4.0004	3.9934	3.9433	3.849	
39.8100	4.0123	4.0177	4.0218	4.0261	3.9934	3.936	
50.1100	4.1232	4.1605	4.1862	4.2362	4.2807	4.309	
63.1000	4.5163	4.5824	4.6207	4.6955	4.7809	4.797	
79.4300	4.9717	5.0010	5.0257	5.1001	5.2338	5.256	
100.000	5.3914	5.4006	5.4240	5.5094	5.6499	5.659	
125.890	5.7171	5.7210	5.7365	5.7899	5.8617	5.847	
158.490	5.8871	5.8892	5.8967	5.9187	5.9451	5.927	
199.530	5.9512	5.9522	5.9556	5.9648	5.9744	5.958	
251.190	5.9768	5.9773	5.9789	5.9830	5.9866	5.968	
316.230	5.9879	5.9882	5.9890	5.9910	5.9922	5.978	
398.110	5.9931	5.9933	5.9938	5.9948	5.9952	5.981	
501.190	5.9959	5.9960	5.9962	5.9968	5.9969	5.987	
630.960	5.9974	5.9974	5.9976	5.9980	5.9979	5.990	
794.330	5.9983	5.9983	5.9984	5.9986	5.9986	5.993	
1000.00	5.9988	5.9988	5.9989	5.9990	5.9990	5.995	

suits Griem's criterion [53] for each ion of the plasma charge state distribution (CSD). In Tables 2 and 3 we have listed the average ionization calculated from ABAKO/ RAPCAL code by solving CRSS equations for several electron densities and temperatures in the ranges considered in this work. From the table it is detected that for temperatures greater than 30 eV the average ionization is density independent for electron densities less than or equal to 10^{15} cm⁻³. As it is known, when CE is achieved the plasma magnitudes are density independent, and, therefore we could assume CE in order to calculate the average ionization for those situations. The estimation of the degree of the ionization is needed for a variety of reasons, since, for example, the plasma thermodynamic properties depend upon ionization, and, furthermore, its knowledge permits a subsequent optimization in the computation of atomic level populations in plasma and radiative properties. A detailed analysis of the charge state distributions as a function of the plasma conditions may be consulted in the previous work [33].

3.2. Monochromatic emissivities

In Fig. 2 we plot the spectrally resolved emissivity for an isothermal sequence (10 eV) and several electron densities (10¹³, 10¹⁵, 10¹⁷ and 10¹⁹ cm⁻³) calculated by means of the resolution of the CRSS and SAHA equations implemented in ABAKO/RAPCAL. The average ionization

is practically the same for all the cases represented, between 3.69 and 3.80, and the ions involved in the emissivity spectra are He-, Li- and Be-like ones. We can see the influence of the theoretical model (CRSS or SAHA equations) used in the emissivity calculations, i.e. the influence of the thermodynamic regime considered in the calculations. As it is known, for a given temperature the LTE regimen is achieved when the electron densities arise and this behavior is observed in Fig. 2, obtaining that for the largest density represented we can assume that LTE regime has been achieved. This result agrees with the thermodynamic regimes map shown in Fig. 1. In Fig. 3 we show the spectrally resolved emissivity for an isodense sequence (10¹⁹ cm⁻³) and several electron temperatures (5, 10, 50 and 100 eV). In this case the average ionization changes noticeably (between 2.10 and 5.51) and, therefore, the ions involved and the spectrum in each situation are quite different. We can also observe that the lines are more broadened than for the situations of lower densities represented in Fig. 2 which is due to the electron collisional broadening including the line profile that depends on the electron density. As in Fig. 2, we have compared CRSS and SAHA calculations. As it is known, for a given electron density as the temperature increases the departure from the LTE regime is more noticeable and this is detected in Fig. 3. Thus, for the electron temperatures of 50 and 100 eV the plasma is in NLTE, and this result also agrees with the thermodynamic regimes map presented.

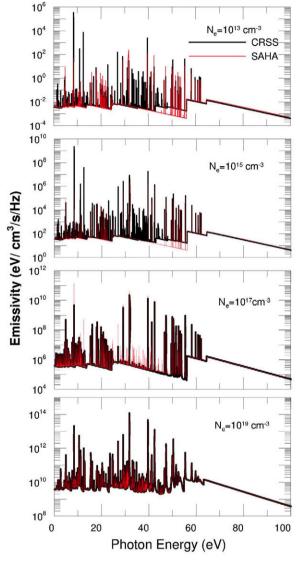


Fig. 2. Comparison between the CRSS and SAHA calculations of the monochromatic emissivities for several densities and an electron temperature of $10\,\text{eV}$.

3.3. Radiative power loss and cooling rate

Since one of the main goals of this work is to present analytical formulas for the radiative cooling rates based on polynomial fittings of the calculations of this magnitude made using ABAKO/RAPCAL, in Fig. 4 we present a comparison with results obtained using ATOMIC code [30] for the whole range of electron temperatures considered in this work and several electron densities. ATOMIC calculations are made both in configuration average (CA) and fine structure (FS) approximations, which includes intermediate-coupling and configuration-interaction effects and from the figure it is observed that at low densities and temperatures below 10 eV, the CA results differ considerably with respect to the FS ones. On the other hand, for temperatures higher than 10 eV both calculations give quite similar values of the cooling rates, and, therefore, for this

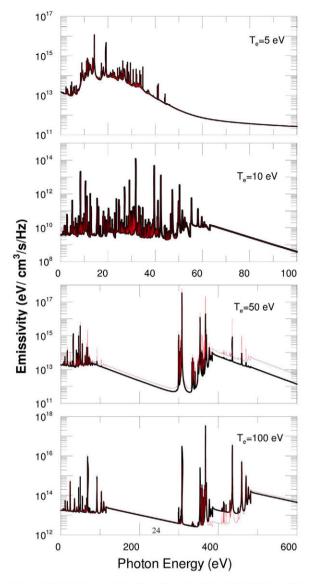


Fig. 3. Comparison between the CRSS and SAHA calculations of the monochromatic emissivities for several electron temperatures and for an electron density of $10^{19}\,\mathrm{cm}^{-3}$.

range of temperatures the authors only provide the CA calculations. For this reason, although our calculations were performed in the DLA approach, we compare our results with the FS ones for temperature lower than 10 eV and for the other temperatures with the DCA ones. In general, a good quantitative agreement is observed between them, although some discrepancies can be detected. Thus, for example, at lowest temperature (1 eV) and for the lowest two densities $(10^{13} \text{ and } 10^{15} \text{ cm}^{-3})$ we obtain differences close to a factor 2-3 between both calculations. This discrepancy could be due to the differences in the atomic data (for example in the coupling scheme considered) of the less ionized stages of carbon which are the most relevant at these plasma conditions as well as to the differences in the calculation of the rates of the processes included in both collisional-models.

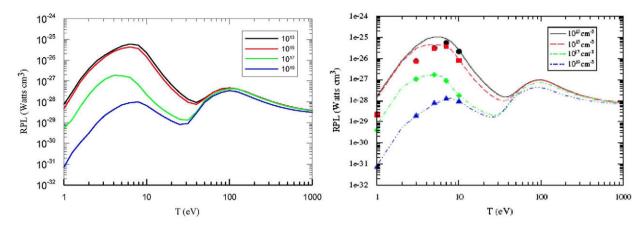


Fig. 4. Comparison between the radiative power losses normalized to obtained from ABAKO/RAPCAL (left) and ATOMIC (right) for several electron densities in cm⁻³.

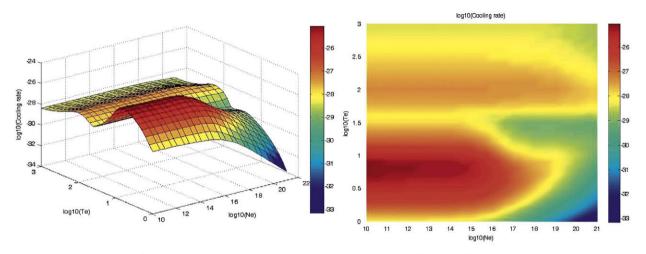


Fig. 5. Cooling rates as a function of the electron temperature and density (left) and its 2D projection (right).

In Fig. 5 and Tables 4 and 5 we present qualitative and quantitative results of the database of radiative cooling rates generated using the CRSS implemented in ABAKO/ RAPCAL employed for the subsequent polynomial fitting. From the figure a region of plasma conditions is detected in which the cooling rates are considerably lower than in other regions. This region is associated to the range of highest densities $(10^{18}-10^{21})$ cm⁻³ and temperatures up to 50 eV, as it can be seen in Table 5. We can observe both from the figure and the tables that for temperatures greater than 200 eV the cooling rates show a weak dependence on electron density and this behavior is more noticeable as the temperature increases, For this range of temperatures the average ionization for all the densities under analysis is very similar, around 5.9, and the most relevant ions are the H-like and the fully stripped ones. This fact means that the free-free contribution to the cooling rates is very relevant, overall as the temperature increases, and, therefore, from Eqs. (11) and (12) it is clear, for these temperatures, their weak dependence on density. On the other hand, from the analysis of the tables of the average ionization we conclude that CE was a good approach for temperatures greater

than 30 eV and electron densities less than or equal to 10^{15} cm^{-3} . This result is confirmed analyzing the values of the cooling rates in Table 4, where we observe that for $\log T_e = 1.50$, i.e. around 30 eV, the cooling rates are very similar in the range of electron densities. Obviously, this similarity increases with the temperature. Finally, in Fig. 5 we also detect a region of plasma conditions in which the cooling rates are relatively greater than in other regions and it corresponds to a range of low electron densities $(10^{10}-10^{16} \text{ cm}^{-3})$ and temperatures (3-10 eV), in which the average ionization is in the interval 1.5-3.5 (see Tables 2 and 3) and B, Be and Li-like ions are the most abundant ones.

The influence of the thermodynamic regime on the calculation of the radiative power loss, and, therefore, in the radiative cooling rates, is analyzed in Fig. 6. In this figure we perform a comparison between the results obtained using the CRSS and the SAHA equations implemented in ABAKO/RAPCAL for three electron densities, (10¹⁵, 10¹⁷ and 10²¹ cm⁻³), and in the whole range of temperatures considered. For the two highest densities, LTE regime could be assumed for temperatures less than or equal to 3 and 30 eV, respectively, whereas for the lowest density represented this

Table 4 Logarithmic of the cooling rates (in W cm³) calculated using ABAKO/RAPCAL for the range of electron densities $10^{10}-10^{15}~{\rm g~cm^{-3}}$ and all the temperatures considered in this work.

$\log T_e$ (eV)	$\log N_e (\mathrm{cm}^{-3})$					
	10	11	12	13	14	15
0.00	-28.03	- 28.04	-28.05	-28.12	-28.21	-28.34
0.10	-27.52	-27.53	-27.51	-27.54	-27.58	-27.70
0.20	-26.91	-26.91	-26.92	-26.93	-26.96	-27.05
0.30	-26.41	-26.41	-26.41	-26.42	-26.44	-26.54
0.40	-26.00	-26.00	-26.01	-26.03	-26.06	-26.16
0.50	-25.67	-25.68	-25.70	-25.75	-25.76	-25.83
0.60	-25.41	-25.42	-25.47	-25.52	-25.49	-25.59
0.70	-25.19	-25.21	-25.27	-25.32	-25.29	-25.43
0.80	-25.07	-25.09	-25.17	-25.22	-25.21	-25.36
0.90	-25.17	-25.21	-25.26	-25.28	-25.28	-25.44
1.00	-25.62	-25.64	-25.65	-25.65	-25.67	-25.85
1.10	-26.19	-26.20	-26.20	-26.20	-26.22	-26.39
1.20	-26.73	-26.73	-26.73	-26.73	-26.75	-26.92
1.30	-27.18	-27.18	-27.18	-27.18	-27.20	-27.36
1.40	-27.56	-27.56	-27.56	-27.56	-27.58	-27.73
1.50	-27.88	-27.88	-27.88	-27.88	-27.90	-28.02
1.60	-28.04	-28.04	-28.04	-28.04	-28.05	-28.13
1.70	-27.83	-27.83	-27.83	-27.83	-27.84	-27.86
1.80	-27.55	-27.55	-27.55	-27.55	-27.56	-27.55
1.90	-27.38	-27.38	-27.38	-27.38	-27.38	-27.39
2.00	-27.33	-27.33	-27.33	-27.33	-27.33	-27.34
2.10	-27.39	-27.39	-27.39	-27.39	-27.39	-27.39
2.20	-27.52	-27.52	-27.52	-27.52	-27.52	-27.52
2.30	-27.68	-27.68	-27.68	-27.68	-27.68	-27.68
2.40	-27.83	-27.83	-27.83	-27.83	-27.83	-27.83
2.50	-27.97	-27.97	-27.97	-27.97	-27.97	-27.97
2.60	-28.09	-28.09	-28.09	-28.09	-28.09	-28.10
2.70	-28.20	-28.20	-28.20	-28.20	-28.20	-28.20
2.80	-28.29	-28.29	-28.29	-28.29	-28.29	-28.29
2.90	-28.37	-28.37	-28.37	-28.37	-28.37	-28.37
3.00	-28.42	-28.42	-28.42	-28.42	-28.42	-28.42

regime is not achieved at any temperature, and these results agree with the thermodynamic regimes map of Fig. 1. In previous works [32,33], we obtained that the relative deviation of both Planck and Rosseland mean radiative opacities between CRSS and SAHA calculations is less than or equal to 10% when the plasma can be assumed under LTE regime, i.e. when the criterion of Eq. (14) is fulfilled. This result is also obtained when we analyze the radiative cooling rates, as it is shown in Table 6. However, from the table is detected that for the electron density of $10^{21}\,\mathrm{cm^{-3}}$ for temperatures greater than 200 eV the relative deviation is, in general, less than 10% which should imply that the plasma can be considered in LTE, which disagrees with the thermodynamic regimes map. This similarity is due to the fact that for this range of temperatures the main contribution to the radiative power loss is the free-free one and that in ABAKO/RAPCAL a Maxwell-Boltzmann distribution for the free electrons is considered (as many available collisional-radiative codes) but the plasma is in NLTE.

3.4. Parametrization of the average ionization and radiative cooling rate

Hydrodynamic simulations of plasmas require the determination of the average ionization and radiative properties for a large set of plasma conditions. However,

Table 5 Logarithmic of the cooling rates (in $W\,cm^3$) calculated using ABAKO/RAPCAL for the range of electron densities $10^{16}-10^{21}~g~cm^{-3}$ and all the temperatures considered in this work.

$\log T_e (\mathrm{eV})$	$\log N_e$ (c	m ⁻³)				
	16	17	18	19	20	21
0.00	-28.10	-29.29	-30.16	-31.14	- 32.15	-33.16
0.10	-28.10	-28.86	-29.58	-30.45	-31.42	-32.43
0.20	-27.46	-28.24	-29.15	-29.97	-30.85	-31.83
0.30	-26.93	-27.67	-28.60	-29.52	-30.40	-31.33
0.40	-26.52	-27.23	-28.09	-29.02	-29.98	-30.90
0.50	-26.21	-26.91	-27.76	-28.64	-29.56	-30.53
0.60	-26.02	-26.74	-27.50	-28.38	-29.25	-30.20
0.70	-25.91	-26.75	-27.45	-28.15	-29.00	-29.91
0.80	-25.91	-26.83	-27.48	-28.04	-28.80	-29.65
0.90	-26.12	-27.18	-27.69	-28.01	-28.66	-29.41
1.00	-26.63	-27.66	-28.04	-28.18	-28.57	-29.22
1.10	-27.15	-28.07	-28.37	-28.45	-28.65	-29.11
1.20	-27.60	-28.39	-28.65	-28.71	-28.82	-29.11
1.30	-27.97	-28.64	-28.88	-28.93	-29.01	-29.18
1.40	-28.26	-28.85	-29.05	-29.09	-29.16	-29.28
1.50	-28.46	-28.89	-29.02	-29.04	-29.07	-29.18
1.60	-28.36	-28.50	-28.54	-28.55	-28.58	-28.53
1.70	-27.92	-27.96	-27.99	-28.02	-28.07	-28.08
1.80	-27.59	-27.64	-27.68	-27.72	-27.82	-27.90
1.90	-27.43	-27.46	-27.49	-27.55	-27.66	-27.76
2.00	-27.36	-27.37	-27.37	-27.46	-27.65	-27.79
2.10	-27.38	-27.38	-27.41	-27.53	-27.76	-27.92
2.20	-27.53	-27.54	-27.57	-27.69	-27.93	-28.09
2.30	-27.69	-27.70	-27.73	-27.85	-28.09	-28.25
2.40	-27.84	-27.85	-27.89	-27.99	-28.23	-28.38
2.50	-27.98	-27.99	-28.02	-28.13	-28.35	-28.49
2.60	-28.10	-28.11	-28.15	-28.24	-28.44	-28.57
2.70	-28.21	-28.22	-28.25	-28.34	-28.51	-28.62
2.80	-28.30	-28.31	-28.34	-28.41	-28.56	-28.66
2.90	-28.37	-28.38	-28.40	-28.47	-28.59	-28.67
3.00	-28.42	-28.43	-28.45	-28.50	-28.60	-28.66

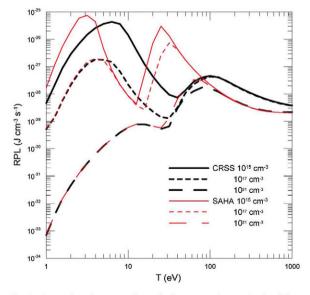


Fig. 6. Comparison between the radiative power losses obtained from ABAKO/RAPCAL using CRSS and SAHA equations for several electron densities.

their calculations involve high computational costs, and, for this reason, it is usual to make use of fitting to analytical

Table 6Relative deviations (in percentage) between CRSS and SAHA calculations of the radiative cooling rates for several electron densities and all the temperatures considered in this work.

$\log T_e$ (eV)	$\log N_e$ (cm ⁻³)				
	17	19	21		
0.00	1.18	0.02	0.01		
0.10	3.67	0.02	0.00		
0.20	6.45	0.00	0.03		
0.30	5.70	0.04	0.03		
0.40	3.66	0.08	0.02		
0.50	18.54	0.00	0.02		
0.60	9.19	0.12	0.01		
0.70	15.95	0.50	0.00		
0.80	62.83	2.73	0.06		
0.90	69.03	1.96	0.00		
1.00	61.43	0.47	0.00		
1.10	54.08	0.91	0.00		
1.20	36.18	0.64	0.00		
1.30	> 100	23.82	0.27		
1.40	> 100	> 100	9.26		
1.50	> 100	> 100	> 100		
1.60	> 100	> 100	> 100		
1.70	> 100	> 100	> 100		
1.80	> 100	> 100	> 100		
1.90	1.82	19.22	60.11		
2.00	54.11	41.04	13.44		
2.10	15.73	56.53	59.87		
2.20	71.53	59.94	3.91		
2.30	72.01	60.63	5.20		
2.40	71.19	59.85	5.53		
2.50	69.33	57.93	5.45		
2.60	66.33	54.75	5.04		
2.70	61.98	50.07	4.44		
2.80	56.35	44.72	3.73		
2.90	49.52	38.31	2.10		
3.00	41.94	31.59	2.36		

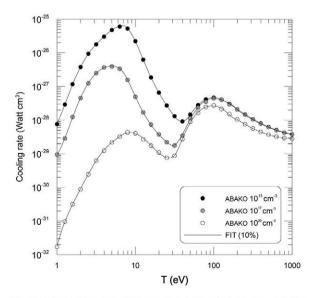


Fig. 7. Polynomial fitting of the cooling rates obtained for a relative deviation of 10%.

expressions of databases of those plasma quantities. In other papers [26–28] fittings of the cooling rates of carbon plasmas have been made but they are only valid for low

electron density since they were obtained assuming CE, and therefore, the fittings are density independent. However, CE regime is achieved at low electron density and high temperature and they are not accurate at larger densities or lower temperatures. In this work we present analytical expressions in powers of densities and temperatures for the calculation of the average ionization and radiative cooling rate which are valid for low to high electron densities and temperatures. The databases were generated using the CRSS model implemented in ABAKO/RAPCAL in the DLA approach.

If A denotes the magnitude to fit, the analytical expression employed for the fitting is the bi-dimensional polynomial function given by Eq. (13). Taking into account that the range of electron densities and temperatures is too wide it is impossible to find only one polynomial function to make the fit of the whole range of plasma conditions, and this one must be divided into subsets to obtain a polynomial fitting in each subset. Obviously, as the error imposed becomes more restrictive the number of subsets and, therefore, of polynomial functions needed to make the fit of the whole range of plasma conditions increases. In this work we have imposed relative errors of 1% and 10% for the fittings of the average ionization and the radiative cooling rates, respectively, which gave to 28 polynomial functions to fit the average ionization and 13 for the radiative cooling rates. In order to optimize the search of the subsets of plasmas conditions and the corresponding polynomial functions a quad-tree algorithm was used. Furthermore, the maximum degrees of the polynomial was fixed to 7, both in electron temperature and density, in order to avoid oscillating behaviors. The corresponding tables including the coefficients of the fittings are listed in Tables 7 and 8 in Appendix A, where the degrees of the polynomial with respect to the temperature and electron density are m and n respectively (see Eq. (13)). Finally, in Fig. 7 we compare the radiative cooling rates for the whole range of electron temperatures and for two electron densities (10¹³ and 10¹⁹ cm⁻³) calculated from ABAKO/RAPCAL code and their polynomial fittings obtained assuming relative deviations of 10%.

4. Conclusions

In this work we performed an analysis of the influence of the thermodynamic regime in the simulation of some relevant plasma properties such as the monochromatic emissivity, the radiative power loss and the radiative cooling rates in a wide range of electron densities and temperatures. For the analysis, we first presented a map obtained using a criterion to establish the thermodynamic regime of the plasma as a whole as a function of the electron density and temperature. The results obtained with this criterion agree with those obtained using Griem's criteria for the ions and level populations. Tables of the average ionization are also presented that provide valuable information about the ions involved in each plasma condition. The influence of the thermodynamic regime on the monochromatic emissivity, the radiative power loss and the radiative cooling rates has been also analyzed. The conclusions from this analysis agree with those obtained from the

Table 7Parameters of the polynomial fitting for the average ionization of carbon. The degrees of the polynomial respect to the temperature and electron density are m (column) and n (row) respectively.

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					
	m = 7, n = 4	$T_e \in [31.62, 10^3] \text{ eV}$	$N_e \in [10^{10}, 4 \times 10^{15}] \mathrm{cm}^{-3}$		
- 1.488913300	7.6658032e1	-5.1868967e1	4.4305694e0	-3.4271528e-1	6.6729519e-3
2.146733902					
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					
-5.0629348e0 - 8.0571766c - 4 9.717988e - 3 -3.7401048e - 4 1.7517184e - m - 5.0808961e - 1 8.0571766c - 4 9.7171988e - 3 -3.7401048e - 4 1.7517184e - m - 5.0808961e - 1 8.0571766c - 4 9.7171988e - 3 -3.7401048e - 4 1.7517184e - m - 5.0808961e - 1 8.0571766c - 4 9.717198e - 3 -3.7401048e - 4 1.7517184e - m - 5.08087965e0 3 3.2245301e2 - 1.084708e1 - 3.2245301e2 - 1.084708e1 - 3.2245301e2 - 1.084708e1 - 3.2245301e2 - 4.506143e0 - 3.2245301e2 - 4.506143e0 - 3.9229540e0 - 1.4991982e - 1 - 3.301312e1 - 3.0219245e2 - 7.6182706e1 - 2.9757958e0 - 3.0219245e2 - 7.6182706e1 - 2.9757958e0 - 3.0219245e2 - 7.6182706e1 - 2.975758e0 - 3.0368425e2 - 7.5482478e1 - 2.9677799e0 - 1.4214057e2 - 3.4662412e1 - 3.072008e0 - 2.4191653e - 1 - 4.214057e2 - 3.4662412e1 - 3.072008e0 - 2.4191653e - 1 - 5.093389e2 - 4.4353304e3 - 4.486316e2 - 1.071807e1 - 7.2794203e - 1.593344e - 1 - 5.003389e2 - 7.6648310e0 - 1.593344e - 1 - 5.003183e3 - 3.4864316e2 - 1.071807e1 - 7.2794203e - 1.99391878e2 - 7.0783053e1 - 2.4473393e1 - 9.1406000e - 1 - 7.2794203e - 1 - 7.9794203e - 7.0795202e1 - 7.7995202e1					
$\begin{array}{llllllllllllllllllllllllllllllllllll$					
$\begin{array}{llllllllllllllllllllllllllllllllllll$					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5.0808961e – 1	8.0571766e-4	9.7171988e – 3	-3.7401048e-4	1.7517184e-5
-1.8827361e2 - 1.0849709e1 - 2.2959974e2 - 1.0018726e1 - 1.3350472e2 - 4.5061430e0 - 2.3427887e1 - 7.9350563e - 1	m=5, n=1	$T_e \in [6.31, 31.62] \text{ eV}$	$N_e[10^{10}, 10^{13}] \text{ cm}^{-3}$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.3852211e1	-1.1365407e0			
$-2.9759974c2 - 4.5061430e0 \\ -2.3427787e1 $	- 1.6823761e2	5.6807965e0			
$-2.9759974c2 - 4.5061430e0 \\ -2.3427787e1 $	3.2246301e2	- 1.0849709e1			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					
$-2.342787e1 \qquad 7.9359563e-1 \\ m=5, n=2 \qquad T_e \in [6.31,31.62] eV \qquad N_e \in [10^{13}.4 \times 10^{15}] cm^{-3} \\ -6.1314495e0 \qquad 3.9229540e0 \qquad -1.4991982e-1 \\ 1.1835573e2 \qquad -3.3303132e1 \qquad 1.2900979e0 \\ -3.0364625e2 \qquad 7.5483478e1 \qquad 2.9974558e0 \\ 3.0864625e2 \qquad 7.5483478e1 \qquad 2.9974558e0 \\ 3.0864625e2 \qquad 3.4862412e1 \qquad -1.3720080e0 \\ 2.463045e1 \qquad -6.0709050e0 \qquad 2.4191653e-1 \\ m=5, n=3 \qquad T_e \in [6.31,31.62] eV \qquad N_e \in [4 \times 10^{15}.4 \times 10^{18}] cm^{-3} \\ 1.3971538e3 \qquad -1.69003388e2 \qquad 5.8808028e0 \qquad -4.7402138e-2 \\ -4.4333304e3 \qquad 4.3709556e2 \qquad -7.6648310e0 \qquad -1.5093440e-1 \\ 5.5605183e3 \qquad -3.4884316e2 \qquad -1.0718007e1 \qquad 7.2794203e-1 \\ -3.0429580e3 \qquad 2.9553908e1 \qquad 2.4473393e1 \qquad -9.1406600e-1 \\ 7.3931878e2 \qquad 7.0738053e1 \qquad -1.4993972e1 \qquad 4.7244757e-1 \\ 7.2988243e1 \qquad -2.1628547e1 \qquad 3.0338103e0 \qquad -8.8335067e-2 \\ m=5, n=1 \qquad T_e \in [31.62.19953] eV \qquad N_e \in [4 \times 10^{15}.4 \times 10^{18}] cm^{-3} \\ -5.0029001e2 \qquad 2.7384342e1 \qquad 1.3562415e3 \qquad 7.39562e1 \qquad 7.7975262e1 \qquad 7.79975262e1 \qquad 7.99975269951e3 \qquad 2.23415827e-4 \qquad 8.69979999999999999999999999999999999999$					
$\begin{array}{llllllllllllllllllllllllllllllllllll$					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	m=5, n=2	$T_e \in [6.31, 31.62] \text{ eV}$	$N_e \in [10^{13}, 4 \times 10^{15}] \text{ cm}^{-3}$		
$-3.019245c2 - 7.6182705c1 - 2.9745558c0 \\ 3.086465c2 - 7.5481378c1 - 2.9677799c0 \\ -1.4214067c2 - 3.4662412c1 - 1.3720080c0 \\ -6.0709050c0 - 2.4191635c - 1 \\ m=5, n=3 $	- 6.1314495e0	3.9229540e0	- 1.4991982e - 1		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.1835573e2	-3.3303132e1	1.2900979e0		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	- 3.0219245e2	7.6182705e1	- 2.9745558e0		
$-1.4214067e2 \\ 2.4630450e1 \\ -6.0709050e0 \\ 2.4191653e-1 \\ m=5, n=3 $ $ T_e \in [6.31,31.62] eV $					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					
$\begin{array}{llllllllllllllllllllllllllllllllllll$					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					
$-4.4533304e3 \\ -3.4684316e2 \\ -3.0429580e3 \\ -3.0429580e3 \\ -3.953908e1 \\ -2.473393e1 \\ -1.4993972e1 \\ -7.2988243e1 \\ -2.1628547e1 \\ -2.1362615e3 \\ -2.34342e1 \\ -2.16285415e3 \\ -2.34615263 \\ -2.194570e1 \\ -2.1180134e0 \\ -2.118013$	m=5, n=3	$T_e \in [6.31, 31.62] \text{ eV}$	$N_e \in [4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.3971538e3	-1.6903388e2	5.8808028e0	-4.7402138e-2	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-4.4353304e3	4.3709556e2	- 7.6648310e0	-1.5093440e-1	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5.3605183e3	-3.4684316e2	- 1.0718007e1	7.2794203e – 1	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					
$\begin{array}{llllllllllllllllllllllllllllllllllll$					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$				0.05550076 2	
$\begin{array}{llllllllllllllllllllllllllllllllllll$	m=5, n=1	$I_e \in [31.62, 199.53] \text{ eV}$	$N_e \in [4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-5.0029001e2	2.7384342e1			
$\begin{array}{lllll} 7.7492448e2 & -4.1113780e1 \\ -2.0442463e2 & 1.0757788e1 \\ 2.1394570e1 & -1.1180134e0 \\ \hline $m=1,n=1$ & $T_e \in [199.53,10^3] {\rm eV}$ & $N_e \in [4\times10^{15},4\times10^{18}] {\rm cm}^{-3}$ \\ \hline \hline $7.5555866e-1$ & 6.7214463e-4 \\ 7.8659691e-3 & -2.3415827e-4 \\ \hline $m=6,n=4$ & $T_e \in [6.31,31.62] {\rm eV}$ & $N_e \in [4\times10^{18},10^{21}] {\rm cm}^{-3}$ \\ \hline \hline $2.4684202e3$ & -4.0062702e2 & 5.3911627e0 & 1.4557860e0 & -5.1630889e-4015964e3 & 1.0971103e3 & -3.9020701e1 & -3.3384080e0 & 1.5509133e-3.6290531e3 & -2.2320719e2 & 3.5497819e1 & 2.6274177e0 & -1.7049981e-6.2544232e3 & -8.9947237e2 & 1.0191246e1 & -5.2258042e-1 & 7.5654945e-3.2550159e3 & 3.7908662e2 & -2.6691415e1 & 2.0399592e-1 & -1.2633442e-5.9144069e3 & 1.7653350e2 & 1.5372105e1 & -5.8056290e-1 & 6.1083635e-1.7181771e3 & -8.3962723e1 & -3.8169967e0 & 2.4612281e-1 & -3.1103028e-2.22341086e2 & -3.4428634e1 & 9.7926963e-1 & -3.2640066e2 & -3.4428634e1 & 9.7926963e-1 & -2.2006441e0 & 6.16755342e & -6.5961682e1 & 1.8721124e0 & -2.2934403e2 & 2.4625928e1 & -6.9674832e-1 \\ \hline $0.0000000000000000000000000000000000$	1.3562415e3	7.3360787e1			
$\begin{array}{lllll} 7.7492448e2 & -4.1113780e1 \\ -2.0442463e2 & 1.0757788e1 \\ 2.1394570e1 & -1.1180134e0 \\ \hline $m=1,n=1$ & $T_e \in [199.53,10^3] {\rm eV}$ & $N_e \in [4\times10^{15},4\times10^{18}] {\rm cm}^{-3}$ \\ \hline \hline $7.5555866e-1$ & 6.7214463e-4 \\ 7.8659691e-3 & -2.3415827e-4 \\ \hline $m=6,n=4$ & $T_e \in [6.31,31.62] {\rm eV}$ & $N_e \in [4\times10^{18},10^{21}] {\rm cm}^{-3}$ \\ \hline \hline $2.4684202e3$ & -4.0062702e2 & 5.3911627e0 & 1.4557860e0 & -5.1630889e-4015964e3 & 1.0971103e3 & -3.9020701e1 & -3.3384080e0 & 1.5509133e-3.6290531e3 & -2.2320719e2 & 3.5497819e1 & 2.6274177e0 & -1.7049981e-6.2544232e3 & -8.9947237e2 & 1.0191246e1 & -5.2258042e-1 & 7.5654945e-3.2550159e3 & 3.7908662e2 & -2.6691415e1 & 2.0399592e-1 & -1.2633442e-5.9144069e3 & 1.7653350e2 & 1.5372105e1 & -5.8056290e-1 & 6.1083635e-1.7181771e3 & -8.3962723e1 & -3.8169967e0 & 2.4612281e-1 & -3.1103028e-2.22341086e2 & -3.4428634e1 & 9.7926963e-1 & -3.2640066e2 & -3.4428634e1 & 9.7926963e-1 & -2.2006441e0 & 6.16755342e & -6.5961682e1 & 1.8721124e0 & -2.2934403e2 & 2.4625928e1 & -6.9674832e-1 \\ \hline $0.0000000000000000000000000000000000$	- 1.4561792e3	7.7975262e1			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					
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$\begin{array}{llllllllllllllllllllllllllllllllllll$					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					
$\begin{array}{llllllllllllllllllllllllllllllllllll$	m=1, n=1	$T_e \in [199.53, 10^3] \text{ eV}$	$N_e \in [4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	7.8659691e-3	−2.3415827e−4			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	m = 6, n = 4	$T_e \in [6.31, 31.62] \text{eV}$	$N_e \in [4 \times 10^{18}, 10^{21}] \text{ cm}^{-3}$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2.4684202e3	-4.0062702e2	5.3911627e0	1.4557860e0	-5.1630889e-2
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					
3.2640066e2				2.4612281e – 1	-3.11030286-3
-7.3421683e2 7.8103891e1 -2.2206441e0 6.1675534e2 -6.5961682e1 1.8721124e0 -2.2934403e2 2.4625928e1 -6.9674832e-1	m=4, n=2	$T_e \in [31.62, 199.53] \text{ eV}$	$N_e \in [4 \times 10^{18}, 10^{21}] \text{ cm}^{-3}$		
6.1675534e2 -6.5961682e1 1.8721124e0 -2.2934403e2 2.4625928e1 -6.9674832e-1	3.2640066e2	-3.4428634e1	9.7926963e – 1		
6.1675534e2 -6.5961682e1 1.8721124e0 -2.2934403e2 2.4625928e1 -6.9674832e-1					
-2.2934403e2 $2.4625928e1$ $-6.9674832e-1$					
5.10554E4C1 = 5.420055EC0 5.0054173C= 2					
	J.10JJ724C1	- 3.420033260	3.033 4 173C-2		

Table 7 (continued)

m=1, n=1	$T_e \in [199.53, 10^3] \text{eV}$	$N_e \in [4 \times 10^{18}, 10^{21}] \mathrm{cm}^{-3}$	
7.7975801e – 1 5.7246665e – 4	− 5.1106715e − 4 1.1844395e − 4		
m = 4, n = 1	$T_e \in [1,2.51] \text{ eV}$	$N_e \in [10^{10}, 4 \times 10^{11}] \text{ cm}^{-3}$	
-2.5208768e-1	7.6728730e – 3		
3.4172960e+0	-7.0796618e-2		
-1.8914900e+1	3.0549477e – 1		
4.6108302e+1 -3.9682778e+1	– 7.1020792e – 1 7.4008970e – 1		
m=4, n=1	$T_e \in [2.51, 6.31] \text{ eV}$	$N_e \in [10^{10}, 4 \times 10^{11}] \text{ cm}^{-3}$	
4.7350131 0		ng c[10 ,1 × 10] cm	
4.7258131e+0 -3.4433472e+1	– 7.0155136e – 2 2.9247642e – 1		
8.9904568e+1	-1.7431467e-1		
-9.8820766e+1	-4.4788783e-1		
3.9485964e+1	4.4750371e – 1		
m = 4, n = 1	$T_e \in [1.00, 2.51] \text{eV}$	$N_e \in [4 \times 10^{11}, 10^{13}] \text{ cm}^{-3}$	
-5.8479081e-1	3.6300712e-2		
8.6072701e+0	-5.1537017e-1		
-5.1912823e+1	3.1265719e+0		
1.4215554e + 2	-8.9157397e+0		
$-1.4710993e\!+\!2$	9.9165913e + 0		
m = 4, n = 1	$T_e \in [2.51, 6.31] \text{ eV}$	$N_e \in [4 \times 10^{11}, 10^{13}] \text{cm}^{-3}$	
2.3714753e+1	- 1.6930999e+0		
-1.6229918e+2	1.1213763e+1		
4.0065262e+2	-2.6696438e+1		
-4.2623892e+2	2.7475615e+1		
1.6653660e + 2	$-1.0379133e\!+\!1$		
m = 3, n = 2	$T_e \in [1.00, 2.51] \text{eV}$	$N_e \in [10^{13}, 4 \times 10^{14}] \text{ cm}^{-3}$	
-3.7119210e+0	4.9773417e – 1	- 1.6976163e - 2	
4.8873938e+1	-6.6217125e+0	2.2972558e-1	
-2.0686276e+2	2.8692680e+1	-1.0279175e+0	
$3.0089768e\!+\!2$	-4.3329138e+1	1.6209812e + 0	
m = 4, n = 2	$T_e \in [2.51, 6.31] \text{eV}$	$N_e \in [10^{13}, 4 \times 10^{14}] \text{ cm}^{-3}$	
1.5820777e+2	- 1.9838154e+1	5.9889801e – 1	
-9.3026793e+2	1.1201690e+2	-3.2023979e+0	
1.9749279e + 3	-2.2641856e+2	6.0288436e+0	
$-1.8118240e{+}3$	1.9574624e + 2	-4.7240104e+0	
6.1685036e + 2	-6.2205886e+1	1.3135224e+0	
m = 3, n = 2	$T_e \in [1.00, 2.51] \text{eV}$	$N_e \in [4 \times 10^{14}, 4 \times 10^{15}] \text{ cm}^{-3}$	
-6.6623075e+0	8.9816751e – 1	-3.0562268e-2	
7.3207830e + 1	-9.8517460e+0	3.3680362e - 1	
$-2.0161075e\!+\!2$	$2.7178316e\!+\!1$	$-9.4880738e\!-\!1$	
$1.0716386e\!+\!2$	-1.5184511e+1	6.0205247e – 1	
m = 4, n = 2	$T_e \in [2.51, 6.31] \text{eV}$	$N_e \in [4 \times 10^{14}, 4 \times 10^{15}] \text{ cm}^{-3}$	
-9.2929868e+2	1.2689916e+2	-4.3510893e+0	
6.8943613e + 3	-9.4471936e+2	3.2478450e + 1	
$-1.8958501e\!+\!4$	2.6041925e + 3	$-8.9668118e\!+\!1$	
2.2818283e+4	-3.1391073e+3	1.0817131e+2	
-1.0101306e+4	1.3907512e+3	-4.7933682e+1	
m = 4, n = 3	$T_e \in [1.00, 2.51] \mathrm{eV}$	$N_e \in [4 \times 10^{15}, 10^{17}] \text{ cm}^{-3}$	
1.9338287e+2	-3.8410498e+1	2.5434390e+0	-5.6168541e-2
1.6539254e + 3	-2.7066895e+2	1.4294551e + 1	-2.3934230e-1
-3.6994050e+4	6.6747450e + 3	$-3.9972255e\!+\!2$	7.9377091e+0
1.5744964e+5	-2.8812491e+4	1.7531770e+3 -2.1970047e+3	-3.5456222e+1 4.4722109e+1
-1.9513713e+5	3.5898127e+4		

Table 7 (continued)

m = 4, n = 2	$T_e \in [2.51, 6.31] \mathrm{eV}$	$N_e \in [4 \times 10^{15}, 10^{17}] \text{ cm}^{-3}$		
3.3142164e+1	-7.9635756e+0	3.3866306e-1		
-9.5954900e+2	1.4496224e+2	-5.0965232e+0		
4.2613868e+3	-5.9160446e+2	1.9767218e+1		
-6.7513522e+3	9.0330152e+2	-2.9440387e+1		
3.5699239e+3	-4.6786691e+2	1.5026675e+1		
m = 4, n = 3	$T_e \in [1.00, 2.51] \text{ eV}$	$N_e \in [10^{17}, 4 \times 10^{18}] \text{ cm}^{-3}$		
2.505050			C. 0.F.F.F.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.	
-3.5687652e+2	6.0630436e+1	-3.3967885e+0	6.2555082e – 2	
-3.2360812e+2	-1.9541882e+1	5.2176523e + 0	- 1.7184112e - 1	
4.3549521e+4	-6.8094350e+3	3.5120842e + 2	-5.9707062e+0	
-1.7169150e+5	2.7604993e+4	-1.4695042e+3	2.5891373e + 1	
1.7121824e+5	-2.7721107e+4	1.4865616e + 3	-2.6391564e+1	
m = 4, n = 2	$T_e \in [2.51, 6.31] \text{eV}$	$N_e \in [10^{17}, 4 \times 10^{18}] \text{ cm}^{-3}$		
2.6423475e+3	-2.9725915e+2	8.3281841e+0		
-1.8694149e+4	2.1070571e+3	-5.9151918e+1		
4.8210534e+4	-5.4408240e+3	1.5295047e+2		
-5.4071419e+4	6.1087034e + 3	-1.7191170e+2		
2.2298440e+4	-2.5214409e+3	7.1023790e+1		
m = 4, n = 3	$T_e \in [1.00, 2.51] \text{ eV}$	$N_e \in [4 \times 10^{18}, 10^{20}] \mathrm{cm}^{-3}$		
4.000000	0.0450505	4.555000	4 0000000	
1.8627965e+1	2.3456527e – 1	- 1.5756623e - 1	4.6232736e – 3	
1.1782167e+3	-1.7580842e+2	8.9017429e + 0	-1.5160371e-1	
1.0361140e + 3	-3.6473930e+2	2.8245373e+1	-6.2888068e - 1	
-3.8959107e+5	6.1633191e+4	- 3.2455455e+3	5.6881367e + 1	
8.0400670e+5	-1.2643731e+5	6.6230111e+3	-1.1554280e $+2$	
m = 4, n = 2	$T_e \in [1.00, 2.51] \text{ eV}$	$N_e \in [10^{20}, 10^{21}] \mathrm{cm}^{-3}$		
1.4049173e+2	-1.3790245e+1	3.3147983e – 1		
-1.7328432e+2	1.8828869e + 1	-4.8337427e-1		
-2.8766051e+3	2.9275998e+2	-7.4261889e+0		
9.9556665e+3	-1.0510777e+3	2.7431279e+1		
-9.8236386e+3	1.0619775e+3	-2.8236424e+1		
m = 4, n = 2	$T_e \in [2.51, 6.31] \text{ eV}$	$N_e \in [10^{20}, 10^{21}] \mathrm{cm}^{-3}$		
	4.040400	4045000		
1.9595252e+3	-1.8421095e+2	4.3153320e+0		
-1.5354865e+4	1.4535359e+3	-3.4324414e+1		
4.3311854e+4	-4.1199047e+3	9.7804495e+1		
-5.2038774e+4	4.9684679e+3	-1.1841092e+2		
2.2592869e+4	-2.1633083e+3	5.1710921e + 1		
m=2, n=2	$T_e \in [2.51, 3.98] \mathrm{eV}$	$N_e \in [4 \times 10^{18}, 4 \times 10^{19}] \ \mathrm{cm^{-3}}$		
- 1.6894190e+1	6.0768905e – 1	1.1706292e-2		
-1.8847053e+2	2.6362847e + 1	-8.5711302e-1		
2.4859649e+2	-3.3225834e+1	1.0565682e+0		
m=2, n=2	$T_e \in [3.98, 6.31] \text{eV}$	$N_e \in [4 \times 10^{18}, 4 \times 10^{19}] \mathrm{cm}^{-3}$		
1 2724420 2	1 24676244 . 2	2 EE27E90a · O		
-1.2724429e+3	1.3467624e+2 -3.6773660e+2	-3.5637689e+0		
3.4802958e+3 -2.3782109e+3	-3.6773660e+2 2.5117676e+2	9.7143659e+0 -6.6302500e+0		
m=2, n=1	$T_e \in [2.51, 3.98] \mathrm{eV}$	$N_e \in [4 \times 10^{19}, 10^{20}] \mathrm{cm}^{-3}$		
4.6468494e+0	-2.6176070e - 1			
$-5.1628975e\!+\!1$	2.5806884e+0			
7.8720007e + 1	-3.8486646e+0			
m = 2, n = 1	$T_e \in [3.98, 6.31] \mathrm{eV}$	$N_e \in [4 \times 10^{19}, 10^{20}] \mathrm{cm}^{-3}$		
7.0007991e+0	-4.5184854e-1			
-1.7629094e+1	-4.5184854e-1 1.1317847e+0			
- 1.7629094e+1 1.5501194e+1	-9.0512669e-1			
1.550115 4 0+1	- 5.05120036 - 1			

Table 8Parameters of the polynomial fitting for cooling rate of carbon. The degrees of the polynomial respect to the temperature and electron density are m (column) and n (row) respectively.

m=6, n=4	$T_e \in [31.62, 10^3] \text{eV}$	$N_e \in [10^{10}, 4 \times 10^{15}] \mathrm{cm}^{-3}$		
1.4466239e3	– 2.5414737e3	1.2913350e3	- 1.5388914e2	1.4614787e1
-3.2101834e1	7.2845683e0	-2.1407393e2	2.2519807e2	1.3522864e2
-2.1790989e2	6.6961659e1	2.4106377e – 1	- 1.7572750e0	2.7911923e1
-4.6098777e1	1.6741775e1	1.3767907e0	1.3947540e0	- 1.8184345e0
3.4549368e – 1	-5.2603896e-1	5.5610489e – 1	6.0917672e – 1	- 6.8252506e - 1
6.2561554e – 2	7.9712727e – 2	-1.7361701e-2	– 2.7294179e – 2	7.6874905e – 2
-9.7763436e-2	5.8566893e – 2	– 1.4793720e – 2	6.4619241e – 4	1.8784064e – 4
m=5, n=1	$T_e \in (1,6.31] \text{ eV}$	$N_e \in [10^{10}, 10^{13}] \mathrm{cm}^{-3}$		
-2.7742073e1	1.0524315e0			
3.0191184e1	- 9.0804482e1			
1.1777138e2	- 5.6929288e1			
-2.7593407e-2	2.8875203e-1			
-1.2553607e0	2.6920674e0			
-3.5406569e0	1.8775137e0			
m = 4, n = 1	$T_e \in [6.31, 31.62] \text{ eV}$	$N_e \in (10^{10}, 10^{13}] \text{ cm}^{-3}$		
0.6142201-1	2.2020505-2			
-8.6143381e1	2.2920595e2			
-3.0501289e2	1.7198764e2			
– 3.5500956e1	5.7014204e – 1			
- 3.3040701e0	5.5746904e0			
-3.7358932e0	8.7929428e – 1			
m = 4, n = 4	$T_e \in (1,6.31] \text{ eV}$	$N_e \in (10^{13}, 10^{15}] \text{ g cm}^{-3}$		
-1.7613062e3	– 7.5346300e2	1.1700720e5	- 3.4833132e5	2.6359789e5
4.9085148e2	2.4961104e2	-3.3075808e4	9.8251547e4	-7.4292810e4
-5.2068070e1	- 3.0589087e1	3.5035704e3	- 1.0382186e4	7.8434857e3
2.4522888e0	1.6541372e0	-1.6481317e2	4.8709469e2	-3.6762369e2
-4.3278205e-2	- 3.3257253e - 2	2.9050104e0	– 8.5608535e0	6.4540996e0
m=4, n=3	$T_e \in (6.31, 31.62] \text{ eV}$	$N_e \in (10^{13}, 4 \times 10^{15}] \mathrm{cm}^{-3}$		
-2.9662951e2	- 6.1324434e2	3.2708764e3	-3.0520189e3	
8.3493768e2	3.0575479e1	2.2931265e2	- 8.3147979e2	
7.2868093e2	- 1.9448195e2	-1.0706141e0	- 2.0371374e1	
6.4950475e1	- 5.5367541e1	1.4607084e1	-2.0474880e-4	
5.7693990e – 1	- 1.6745481e0	1.3947606e0	- 3.6426466e - 1	
m = 5, n = 3	$T_e \in (1,6.31] \text{ eV}$	$N_e \in (4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$		
-7.6168421e1	2.1178980e3	-3.0822349e4	1.1373063e5	
- 1.6013417e5	7.7223562e4	7.7630858e0	- 3.4718752e2	
5.2897480e3	- 1.9751432e4	2.7979304e4	- 1.3537140e4	
– 3.8337119e – 1	1.8822385e1	-3.0095562e2	1.1379461e3	
–1.6223203e3	7.8762274e2	5.2289405e – 3	− 3.3621429e − 1	
5.6763718e0	- 2.1750641e1	3.1216388e1	– 3.3621429e – 1 – 1.5209275e1	
5.6763718e0	-2.1750641e1	3.1216388e1		– 2.2081750e4
5.6763718e0 m=5, n=4	$-2.1750641e1$ $T_e \in (6.31,31.62] \text{ eV}$	3.1216388e1 $N_{e} \in (4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$	– 1.5209275e1	– 2.2081750e4 – 2.4525423e2
5.6763718e0 <i>m</i> =5, <i>n</i> =4 4.4121716e3 8.6657175e3	$-2.1750641e1$ $T_e \in (6.31,31.62] \text{ eV}$ $-3.7104556e4$ $-4.1414976e1$	3.1216388e1 $N_e \in (4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$ 3.8715131e4 5.4773887e3	- 1.5209275e1 2.5848877e3 - 6.1841073e3	-2.4525423e2
5.6763718e0 m=5, n=4 4.4121716e3 8.6657175e3 3.6414318e3	$-2.1750641e1$ $T_e \in (6.31,31.62] \text{ eV}$ $-3.7104556e4$ $-4.1414976e1$ $-1.5194306e3$	3.1216388e1 $N_e \in (4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$ 3.8715131e4 5.4773887e3 -1.0965143e2	- 1.5209275e1 2.5848877e3 - 6.1841073e3 - 9.8843249e1	-2.4525423e2 1.3905446e2
5.6763718e0 m=5, n=4 4.4121716e3 8.6657175e3 3.6414318e3 1.0202499e2	$-2.1750641e1$ $T_e \in (6.31,31.62] \text{ eV}$ $-3.7104556e4$ $-4.1414976e1$ $-1.5194306e3$ $-2.2660526e2$	$N_e \in (4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$ $3.8715131e4$ $5.4773887e3$ $-1.0965143e2$ $9.4599867e1$	- 1.5209275e1 2.5848877e3 - 6.1841073e3 - 9.8843249e1 9.5825195e0	2.4525423e2 1.3905446e2 1.4498456e1
5.6763718e0 m=5, n=4 4.4121716e3 8.6657175e3 3.6414318e3 1.0202499e2 1.5572265e1	$-2.1750641e1$ $T_e \in (6.31,31.62] \text{ eV}$ $-3.7104556e4$ $-4.1414976e1$ $-1.5194306e3$ $-2.2660526e2$ $-1.1083295e1$	$N_e \in (4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$ $3.8715131e4$ $5.4773887e3$ $-1.0965143e2$ $9.4599867e1$ $6.7043316e0$	- 1.5209275e1 2.5848877e3 - 6.1841073e3 - 9.8843249e1 9.5825195e0 - 2.4016389e0	-2.4525423e2 1.3905446e2 -1.4498456e1 -2.3041839e-1
5.6763718e0 m=5, n=4 4.4121716e3 8.6657175e3 3.6414318e3 1.0202499e2 1.5572265e1 5.3071499e-1	$-2.1750641e1$ $T_e \in (6.31,31.62] \text{ eV}$ $-3.7104556e4$ $-4.1414976e1$ $-1.5194306e3$ $-2.2660526e2$ $-1.1083295e1$ $-6.1331763e-1$	$N_e \in (4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$ $3.8715131e4$ $5.4773887e3$ $-1.0965143e2$ $9.4599867e1$ $6.7043316e0$ $3.2762342e-1$	- 1.5209275e1 2.5848877e3 - 6.1841073e3 - 9.8843249e1 9.5825195e0	– 2.4525423e2 1.3905446e2 – 1.4498456e1
5.6763718e0 m=5, n=4 4.4121716e3 8.6657175e3 3.6414318e3 1.0202499e2 1.5572265e1	$-2.1750641e1$ $T_e \in (6.31,31.62] \text{ eV}$ $-3.7104556e4$ $-4.1414976e1$ $-1.5194306e3$ $-2.2660526e2$ $-1.1083295e1$	$N_e \in (4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$ $3.8715131e4$ $5.4773887e3$ $-1.0965143e2$ $9.4599867e1$ $6.7043316e0$	- 1.5209275e1 2.5848877e3 - 6.1841073e3 - 9.8843249e1 9.5825195e0 - 2.4016389e0	-2.4525423e2 1.3905446e2 -1.4498456e1 -2.3041839e-1
5.6763718e0 m=5, n=4 4.4121716e3 8.6657175e3 3.6414318e3 1.0202499e2 1.5572265e1 5.3071499e – 1 m=5, n=2 1.0131510e4	$-2.1750641e1$ $T_e \in (6.31,31.62] \text{ eV}$ $-3.7104556e4$ $-4.1414976e1$ $-1.5194306e3$ $-2.2660526e2$ $-1.1083295e1$ $-6.1331763e-1$	$N_e \in (4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$ $3.8715131e4$ $5.4773887e3$ $-1.0965143e2$ $9.4599867e1$ $6.7043316e0$ $3.2762342e-1$	- 1.5209275e1 2.5848877e3 - 6.1841073e3 - 9.8843249e1 9.5825195e0 - 2.4016389e0	- 2.4525423e2 1.3905446e2 - 1.4498456e1 - 2.3041839e - 1
5.6763718e0 m=5, n=4 4.4121716e3 8.6657175e3 3.6414318e3 1.0202499e2 1.5572265e1 5.3071499e-1 m=5, n=2	$-2.1750641e1$ $T_e \in (6.31,31.62] \text{ eV}$ $-3.7104556e4$ $-4.1414976e1$ $-1.5194306e3$ $-2.2660526e2$ $-1.1083295e1$ $-6.1331763e - 1$ $T_e \in (31.62,199.53] \text{ eV}$	$N_e \in (4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$ $3.8715131e4$ $5.4773887e3$ $-1.0965143e2$ $9.4599867e1$ $6.7043316e0$ $3.2762342e-1$ $N_e \in (4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$	- 1.5209275e1 2.5848877e3 - 6.1841073e3 - 9.8843249e1 9.5825195e0 - 2.4016389e0	- 2.4525423e2 1.3905446e2 - 1.4498456e1 - 2.3041839e - 1
5.6763718e0 m=5, n=4 4.4121716e3 8.6657175e3 3.6414318e3 1.0202499e2 1.5572265e1 5.3071499e-1 m=5, n=2 1.0131510e4	$-2.1750641e1$ $T_e \in (6.31,31.62] \text{ eV}$ $-3.7104556e4$ $-4.1414976e1$ $-1.5194306e3$ $-2.2660526e2$ $-1.1083295e1$ $-6.1331763e - 1$ $T_e \in (31.62,199.53] \text{ eV}$ $-1.8546408e4$	$N_e \in (4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$ $3.8715131e4$ $5.4773887e3$ $-1.0965143e2$ $9.4599867e1$ $6.7043316e0$ $3.2762342e-1$ $N_e \in (4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$ $1.1403640e4$	- 1.5209275e1 2.5848877e3 - 6.1841073e3 - 9.8843249e1 9.5825195e0 - 2.4016389e0	- 2.4525423e2 1.3905446e2 - 1.4498456e1 - 2.3041839e - 1
5.6763718e0 m=5, n=4 4.4121716e3 8.6657175e3 3.6414318e3 1.0202499e2 1.5572265e1 5.3071499e - 1 m=5, n=2 1.0131510e4 -2.0077429e3 -5.9238179e2	$-2.1750641e1$ $T_e \in (6.31,31.62] \text{ eV}$ $-3.7104556e4$ $-4.1414976e1$ $-1.5194306e3$ $-2.2660526e2$ $-1.1083295e1$ $-6.1331763e-1$ $T_e \in (31.62,199.53] \text{ eV}$ $-1.8546408e4$ $-4.4456628e2$ $6.2854075e2$	$3.1216388e1$ $N_e \in (4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$ $3.8715131e4$ $5.4773887e3$ $-1.0965143e2$ $9.4599867e1$ $6.7043316e0$ $3.2762342e - 1$ $N_e \in (4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$ $1.1403640e4$ $1.4041741e2$ $2.5151772e2$	- 1.5209275e1 2.5848877e3 - 6.1841073e3 - 9.8843249e1 9.5825195e0 - 2.4016389e0	- 2.4525423e2 1.3905446e2 - 1.4498456e1 - 2.3041839e - 1
5.6763718e0 m=5, n=4 4.4121716e3 8.6657175e3 3.6414318e3 1.0202499e2 1.5572265e1 5.3071499e-1 m=5, n=2 1.0131510e4 -2.0077429e3	$-2.1750641e1$ $T_e \in (6.31,31.62] \text{ eV}$ $-3.7104556e4$ $-4.1414976e1$ $-1.5194306e3$ $-2.2660526e2$ $-1.1083295e1$ $-6.1331763e - 1$ $T_e \in (31.62,199.53] \text{ eV}$ $-1.8546408e4$ $-4.4456628e2$	3.1216388e1 $N_e \in (4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$ 3.8715131e4 5.4773887e3 -1.0965143e2 9.4599867e1 6.7043316e0 3.2762342e - 1 $N_e \in (4 \times 10^{15}, 4 \times 10^{18}] \text{ cm}^{-3}$ 1.1403640e4 1.4041741e2	- 1.5209275e1 2.5848877e3 - 6.1841073e3 - 9.8843249e1 9.5825195e0 - 2.4016389e0	- 2.4525423e2 1.3905446e2 - 1.4498456e1 - 2.3041839e - 1

Table 8 (continued)

m=2, n=1	$T_e \in (199.53, 10^3] \text{ eV}$	$N_e \in (4 \times 10^{15}, 4 \times 10^{18}] \mathrm{cm}^{-3}$		
- 2.1820168e1 3.2287070e - 1 - 1.4783947e - 1	−3.0802436e0 1.4351770e − 1 3.1490439e − 2			
m=5, n=2	$T_e \in (1,6.31] \mathrm{eV}$	$N_e \in (4 \times 10^{18}, 10^{21}] \text{ cm}^{-3}$		
- 1.1552539e + 1	-2.7600554e+2	1.7554959e+3		
-3.8894898e+3	3.4851539e + 3	-1.0947698e+3		
-1.0557006e+0	2.8971070e+1	-1.8681069e+2		
4.2879761e + 2	-4.0422186e $+2$	1.3588710e + 2		
1.2668114e-3	– 7.3570790e – 1	4.8994054e+0		
-1.1596016e + 1	1.1358117e + 1	-3.9978006e+0		
m = 4, n = 2	$T_e \in (6.31, 31.62] \text{eV}$	$N_e \in (4 \times 10^{18}, 10^{21}] \text{ cm}^{-3}$		
-4.7343766e2	3.1713026e3	-6.2768870e3		
4.7308890e36	-1.2186030e3	2.4338246e1		
- 2.4029942e2	5.2642298e2	-4.1648129e2		
1.1034747e2	-8.8387306e-2	3.9860953e0		
-1.0440149e1	8.8559168e0	-2.4344869e0		
m = 6, n = 3	$T_e \in (31.62, 199.53] \text{ eV}$	$N_e \in (4 \times 10^{18}, 10^{21}] \mathrm{cm}^{-3}$		
-6.7094598e+3	1.1441974e+4	-4.1065464e+3	-1.9322320e+3	
9.5477713e+2	1.8269760e+2	-8.9011114e+1	5.3413978e + 2	
-1.0902049e+3	6.4215382e + 2	-1.2687602e+2	1.0024735e+2	
-7.9312370e+1	1.6653356e + 1	1.9834573e+1	-4.2687196e+1	
4.3883969e+1	-2.0726996e+1	-6.1511503e-1	3.5249222e+0	
-7.6747666e-1	-6.7496255e - 1	8.0843216e-1	1.9866930e – 1	
$-8.6490957e\!-\!1$	6.3386969e - 1	$-2.0540649e\!-\!1$	2.5736330e – 2	
m=2, n=1	$T_e \in (199.53, 10^3] \text{ eV}$	$N_e \in (4 \times 10^{18}, 10^{21}] \mathrm{cm}^{-3}$		
- 2.3720987e1	3.1804483e0			
- 1.4257110e0	2.4400976e – 1			
-4.8469274e-1	1.2570407e – 1			

observation of the thermodynamic regimes map. Furthermore, when the criterion presented to establish the LTE regime is fulfilled the relative deviations between CRSS and SAHA calculations of the radiative cooling rates are always less than or equal to 10%, as it also happened with the radiative mean opacities. Finally, parametrizations of the average ionization and the radiative cooling rates based on polynomial functions of the electron density have been also presented. These parametrizations are valid for a wide range of electron densities and temperatures.

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Appendix A

In this section we present the tables of the coefficients corresponding to the parametrization of the average ionization and the radiative cooling rates, Tables 7 and 8, respectively.

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