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ANALYSIS OF DIFFERENT UNCERTAINTY ACTIVATION CROSS SECTION DATA LIBRARIES FOR LWR, ADS AND DEMO NEUTRON SPECTRA

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#### OUTLINE



Cross-section uncertainties under different neutron spectra







#### **INTRODUCTION.** The context of this work ...

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# Nuclear data requirements for the ADS conceptual design EFIT: Uncertainty and sensitivity study

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#### ABSTRACT

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Cross-section uncertainties Uncertainty propagation Sensitivity technique Monte Carlo simulation Target accuracies In this paper, we assess the impact of activation cross-section uncertainties on relevant fuel cycle parameters for a conceptual design of a modular European Facility for Industrial Transmutation (EFIT) with a "double strata" fuel cycle. Next, the nuclear data requirements are evaluated so that the parameters can meet the assigned design target accuracies. Different discharge burn-up levels are considered: a low burn-up, corresponding to the equilibrium cycle, and a high burn-up level, simulating the effects on the fuel of the multi-recycling scenario.

In order to perform this study, we propose a methodology in two steps. Firstly, we compute the uncertainties on the system parameters by using a Monte Carlo simulation, as it is considered the most reliable approach to address this problem. Secondly, the analysis of the results is performed by a sensitivity technique, in order to identify the relevant reaction channels and prioritize the data improvement needs. Cross-section uncertainties are taken from the EAF-2007/UN library since it includes data for all the actinides potentially present in the irradiated fuel.

Relevant uncertainties in some of the fuel cycle parameters have been obtained, and we conclude with recommendations for future nuclear data measurement programs, beyond the specific results obtained with the present nuclear data files and the limited available covariance information. A comparison with the uncertainty and accuracy analysis recently published by the WPEC-Subgroup26 of the OECD using BOLNA covariance matrices is performed. Despite the differences in the transmuter reactor used for the analysis, some conclusions obtained by Subgroup26 are qualitatively corroborated, and improvements for additional cross sections are suggested.

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- Within the frame of EUROTRANS-ADS project
- ADS conceptual design EFIT fuel cycle
- Uncertainty and Sensitivity study throughout fuel cycle
- Identifying critical XS in order to reduce uncertainties





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### **INTRODUCTION.** The context of this work ...



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#### UNCERTAINTY AND TARGET ACCURACY ASSESSMENT FOR INNOVATIVE SYSTEMS USING RECENT COVARIANCE DATA EVALUATIONS

A report by the Working Party on International Evaluation Co-operation of the NEA Nuclear Science Committee

#### CO-ORDINATOR

M. Salvatores Argonne National Laboratory/Commissariat à l'Énergie Atomique USA/France

#### MONITOR

*R. Jacqmin* Commissariat à l'Énergie Atomique France

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NUCLEAR ENERGY AGENCY ORGANISATION FOR ECONOMIC CO-OPERATION AND DEVELOPMENT



- Systematic approach to define data needs for advanced reactor systems
- Advanced reactor systems:
  - ABTR, SFR, EFR, VHTR
  - GFR, LFR, ADMAB
  - <u>PWR</u> (high burn-up)
- Identifying critical XS in order to reduce uncertainties



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# **ADS Uncertainty Requirements**



Table. Critical cross-section uncertainties collapsed in one-group and processed from EAF2007/UN ( $\Delta_{EAF}$ ) and their target accuracies ( $\Delta_{target}$ )

#### Target of required accuracies

Uncertainty in the concentration of all the nuclides of interest <5%</li>
Uncertainty in the response functions in the cooling times (decay heat, radiotoxicity, neutron emission, ...) <10%</li>

#### List of priorities

- Fission cross sections of <sup>242m</sup>Am, <sup>243</sup>Cm, <sup>250,251</sup>Cf
- (n, γ) of <sup>234</sup>U, <sup>237</sup>Np, <sup>241,242m</sup>Am, <sup>242,244,245,246,247,248</sup>Cm, <sup>249</sup>Bk, <sup>249,250,251</sup>Cf
- ➤ (n, γ-M) of <sup>234</sup>U, <sup>241</sup>Am

#### 500GWd/tHM burn-up

Reaction		$\varDelta_{E\!AF}$	$\varDelta_{TARGET}$
U <sup>234</sup>	$(n, \gamma)$	38.9	7.1
	$(n, \gamma - M)$	38.9	7.1
U <sup>235</sup>	Fission	12.9	4.2
Np <sup>237</sup>	$(n, \gamma)$	14.3	2.8
Pu <sup>238</sup>	Fission	12.3	6.4
	$(n, \gamma)$	14.5	5.2
Pu <sup>239</sup>	Fission	9.6	3.4
Pu <sup>240</sup>	$(n, \gamma)$	9.3	4.8
Pu <sup>241</sup>	Fission	15.6	4.2
Pu <sup>242</sup>	$(n, \gamma)$	12.6	5.3
Am <sup>241</sup>	$(n, \gamma)$	15.8	2.8
	$(n, \gamma - M)$	15.9	2.9
Am <sup>242m</sup>	Fission	24.0	2.4
	$(n, \gamma)$	32.8	6.2
Am <sup>243</sup>	$(n, \gamma - M)$	15.3	4.1
Cm <sup>242</sup>	$(n, \gamma)$	30.0	3.4
Cm <sup>243</sup>	Fission	16.0	3.2
	$(n, \gamma)$	32.0	7.4
Cm <sup>244</sup>	$(n, \gamma)$	24.6	4.6
Cm <sup>245</sup>	Fission	9.7	4.1
	$(n, \gamma)$	32.7	5.5
Cm <sup>246</sup>	$(n, \gamma)$	28.2	4.3
Cm <sup>247</sup>	Fission	16.5	4.0
	$(n, \gamma)$	32.1	5.0
Cm <sup>248</sup>	$(n, \gamma)$	19.2	2.5
Bk <sup>249</sup>	$(n, \gamma)$	31.7	3.2
Cf <sup>249</sup>	$(n, \gamma)$	32.4	4.3
Cf <sup>250</sup>	Fission	33.0	6.9
	$(n, \gamma)$	29.3	2.6
Cf <sup>251</sup>	Fission	31.6	3.7
	$(n, \gamma)$	29.9	2.4







Table.One-group uncertainties in the critical cross-sections processed from<br/>EAF2007/UN (3-4 groups), EAF2010/UN(3-4 groups) and SCALE6.0-COVA (44<br/>groups). Calculations correspond to a burn-up of 500GWd/tHM.

Isotope     EAF2007     EAF2010     SCALE6.0     TARGET     EAF2010     SCALE6.0     TARGET     EAF2010     SCALE6.0     TARGET       235U     16.5     16.5     30.0      38.9     26.0     6.9     7.1     38.9     26.0      7.1       235U     15.9     15.3     27.2     8.9     3.2     3.1			(n,fis	sion)		(n,γ)				(n,γ-M)			
234U   16.5   16.5   30.0   38.9   26.0   6.9   7.1   38.9   26.0   -   7.1     235U   12.9   5.5   0.4   4.2   11.3   3.2   21.8   -	Isotope	EAF2007	EAF2010	SCALE6.0	TARGET	EAF2007	EAF2010	SCALE6.0	TARGEŢ	EAF2007	EAF2010	SCALE6.0	TARGET
235U   12.9   5.5   0.4   4.2   11.3   3.2   21.8   -   -   -   -   -     236U   15.9   15.3   27.2   8.9   3.2   3.1   - </th <th>234U</th> <th>16.5</th> <th>16.5</th> <th>30.0</th> <th>1</th> <th>38.9</th> <th>26.0</th> <th>6.9</th> <th>7.1</th> <th>38.9</th> <th>26.0</th> <th>-</th> <th>7.1</th>	234U	16.5	16.5	30.0	1	38.9	26.0	6.9	7.1	38.9	26.0	-	7.1
236U   15.9   15.3   27.2   8.9   3.2   3.1   -   -   -   -     238U   16.6   16.6   0.5   6.7   3.2   1.4   -	235U	12.9	5.5	0.4	4.2	11.3	3.2	21.8	•	-	-	-	
238U   16.6   16.6   0.5   6.7   3.2   1.4   -   -   -   -     238Pu   16.7   16.4   6.6   14.3   9.1   3.3   2.8   - </th <th>236U</th> <th>15.9</th> <th>15.3</th> <th>27.2</th> <th>·</th> <th>8.9</th> <th>3.2</th> <th>3.1</th> <th></th> <th>-</th> <th>-</th> <th>-</th> <th></th>	236U	15.9	15.3	27.2	·	8.9	3.2	3.1		-	-	-	
237Np   16.7   16.4   6.6   14.3   9.1   3.3   2.8   -   -   -   -     238Pu   12.4   10.1   10.6   6.4   14.3   9.1   3.3   2.8   -	238U	16.6	16.6	0.5		6.7	3.2	1.4	,	-	-	-	
238Pu   12.4   10.1   10.6   6.4   14.5   3.7   6.6   5.2   -   -   -   -     239Pu   9.6   7.9   0.4   3.4   12.5   4.2   4.8   -   -   -   -   -     240Pu   15.8   14.7   0.6   9.3   3.6   1.2   4.8   -	237Np	16.7	16.4	6.6	,	14.3	9.1	3.3	2.8	-	-	-	
239Pu   9.6   7.9   0.4   3.4   12.5   4.2   4.8   -   -   -   -   -     240Pu   15.8   14.7   0.6   9.3   3.6   1.2   4.8   -<	238Pu	12.4	10.1	10.6	6.4	14.5	3.7	6.6	5.2	-	-	-	
240Pu   15.8   14.7   0.6   9.3   3.6   1.2   4.8   -   -   -   -   -     241Pu   15.6   5.6   1.2   4.2   15.4   5.2   4.0   -	239Pu	9.6	7.9	0.4	3.4	12.5	4.2	4.8		-	-	-	
241Pu   15.6   5.6   1.2   4.2   15.4   5.2   4.0   -	240Pu	15.8	14.7	0.6	$\sim$	9.3	3.6	1.2	4.8	> -	-	-	
242Pu   16.5   16.5   3.4   12.6   3.5   5.0   5.3   -   -   -   -     244Pu   16.5   16.5   19.0   30.4   7.4   24.9   -   -   -   -   -     241Am   16.6   16.6   2.2   15.8   16.7   4.7   2.8   15.8   16.7   -   -   -   -   -   -   -   -   2.9     242MAm   16.6   16.6   2.2   15.8   16.7   4.7   2.8   15.8   16.7   - <th>241Pu</th> <th>15.6</th> <th>5.6</th> <th>1.2</th> <th>4.2</th> <th>15.4</th> <th>5.2</th> <th>4.0</th> <th></th> <th>-</th> <th>-</th> <th>-</th> <th></th>	241Pu	15.6	5.6	1.2	4.2	15.4	5.2	4.0		-	-	-	
244Pu   16.5   16.5   19.0   30.4   7.4   24.9       24     241Am   16.6   16.6   2.2   15.8   16.7   4.7   2.8   15.8   16.7    2.9     242MAm   16.5   5.6   9.8   2.4   32.8   13.2   14.5   6.2        2.9     243Am   16.6   16.0   5.8   15.3   5.0   4.5   15.3   3.8    4.1     243Cm   16.5   16.5   31.9   30.0   12.9   10.8   3.4   <	242Pu	16.5	16.5	3.4	·	12.6	3.5	5.0	5.3	-	-	-	
241Am   16.6   16.6   2.2   15.8   16.7   4.7   2.8   15.8   16.7   -   2.9     242Mam   16.5   5.6   9.8   2.4   32.8   13.2   14.5   6.2   - </th <th>244Pu</th> <th>16.5</th> <th>16.5</th> <th>19.0</th> <th></th> <th>30.4</th> <th>7.4</th> <th>24.9</th> <th></th> <th>-</th> <th>-</th> <th>-</th> <th></th>	244Pu	16.5	16.5	19.0		30.4	7.4	24.9		-	-	-	
242MAm   16.5   5.6   9.8   2.4   32.8   13.2   14.5   6.2   -   -   -   -     243Am   16.6   16.0   5.8   15.3   5.0   4.5   15.3   3.8   -   4.1     242Cm   16.5   16.5   31.9   30.0   12.9   10.8   3.4   - <t< th=""><th>241Am</th><th>16.6</th><th>16.6</th><th>2.2</th><th></th><th>15.8</th><th>16.7</th><th>4.7</th><th>2.8</th><th>15.8</th><th>16.7</th><th>-</th><th>2.9</th></t<>	241Am	16.6	16.6	2.2		15.8	16.7	4.7	2.8	15.8	16.7	-	2.9
243Am   16.6   16.0   5.8   15.3   5.0   4.5   15.3   3.8   -   4.1     242Cm   16.5   16.5   31.9   30.0   12.9   10.8   3.4   -	242MAm	16.5	5.6	9.8	2.4	32.8	13.2	14.5	6.2	-	-	-	,
242Cm   16.5   16.5   31.9   30.0   12.9   10.8   3.4   -   -   -   -     243Cm   16.0   5.9   19.7   3.2   32.0   5.2   14.2   7.4   -   -   -   -     244Cm   16.4   14.8   37.0   24.6   3.7   7.7   4.6   -   -   -   -     245Cm   9.8   11.3   20.2   4.1   32.8   4.1   9.8   5.5   -   -   -   -     246Cm   16.6   15.2   8.0   28.2   3.7   20.3   4.3   -   -   -   -     247Cm   16.5   16.5   11.3   4.0   32.1   7.7   20.6   5.0   -	243Am	16.6	16.0	5.8		15.3	5.0	4.5		15.3	3.8	-	4.1
243Cm   16.0   5.9   19.7   3.2   32.0   5.2   14.2   7.4   -   -   -   -     244Cm   16.4   14.8   37.0   24.6   3.7   7.7   4.6   -   -   -   -     245Cm   9.8   11.3   20.2   4.1   32.8   4.1   9.8   5.5   -   -   -   -     246Cm   16.6   15.2   8.0   28.2   3.7   20.3   4.3   -   -   -   -   -     247Cm   16.5   16.5   11.3   4.0   32.1   7.7   20.6   5.0   - <th>242Cm</th> <th>16.5</th> <th>16.5</th> <th>31.9</th> <th>,</th> <th>30.0</th> <th>12.9</th> <th>10.8</th> <th>3.4</th> <th>-</th> <th>-</th> <th>-</th> <th></th>	242Cm	16.5	16.5	31.9	,	30.0	12.9	10.8	3.4	-	-	-	
244Cm   16.4   14.8   37.0   24.6   3.7   7.7   4.6   -   -   -   -     245Cm   9.8   11.3   20.2   4.1   32.8   4.1   9.8   5.5   -	243Cm	16.0	5.9	19.7	3.2	32.0	5.2	14.2	7.4	-	-	-	
245Cm   9.8   11.3   20.2   4.1   32.8   4.1   9.8   5.5   - </th <th>244Cm</th> <th>16.4</th> <th>14.8</th> <th>37.0</th> <th></th> <th>24.6</th> <th>3.7</th> <th>7.7</th> <th>4.6</th> <th>-</th> <th>-</th> <th>-</th> <th></th>	244Cm	16.4	14.8	37.0		24.6	3.7	7.7	4.6	-	-	-	
246Cm   16.6   15.2   8.0   28.2   3.7   20.3   4.3   - <th>245Cm</th> <th>9.8</th> <th>11.3</th> <th>20.2</th> <th>4.1 &lt;</th> <th>32.8</th> <th>4.1</th> <th>9.8</th> <th>5.5</th> <th>&gt; -</th> <th>-</th> <th>-</th> <th></th>	245Cm	9.8	11.3	20.2	4.1 <	32.8	4.1	9.8	5.5	> -	-	-	
247Cm   16.5   16.5   11.3   4.0   32.1   7.7   20.6   5.0   -	246Cm	16.6	15.2	8.0		28.2	3.7	20.3	4.3	-	-	-	
248Cm   16.2   15.3   16.2   19.2   3.8   16.9   2.5   -   -   -   -   -     249Bk   16.6   16.6   22.5   31.7   8.8   23.7   3.2   -	247Cm	16.5	16.5	11.3	4.0	32.1	7.7	20.6	5.0	-	-	-	
249Bk   16.6   16.6   22.5   31.7   8.8   23.7   3.2   -   -   -   -   -     249Cf   16.3   5.8   19.3   .32.4   4.8   24.5   4.3   -	248Cm	16.2	15.3	16.2		19.2	3.8	16.9	2.5	-	-	-	
249Cf   16.3   5.8   19.3   32.4   4.8   24.5   4.3   - <th>249Bk</th> <th>16.6</th> <th>16.6</th> <th>22.5</th> <th></th> <th>31.7</th> <th>8.8</th> <th>23.7</th> <th>3.2</th> <th>-</th> <th>-</th> <th>-</th> <th></th>	249Bk	16.6	16.6	22.5		31.7	8.8	23.7	3.2	-	-	-	
250Cf   33.0   33.0   13.3   6.9   29.3   9.0   16.0   2.6   -   -   -   -     251Cf   31.6   12.9   21.9   3.7   30.0   3.9   16.6   2.4   -   -   -   -   -     252Cf   15.0   10.7   6.1   31.2   4.0   18.1   -   -   -   -	249Cf	16.3	5.8	19.3		32.4	4.8	24.5	4.3	-	-	-	
251Cf     31.6     12.9     21.9     3.7     30.0     3.9     16.6     2.4     - </th <th>250Cf</th> <th>33.0</th> <th>33.0</th> <th>13.3</th> <th>6.9</th> <th>29.3</th> <th>9.0</th> <th>16.0</th> <th>2.6</th> <th>-</th> <th>-</th> <th>-</th> <th></th>	250Cf	33.0	33.0	13.3	6.9	29.3	9.0	16.0	2.6	-	-	-	
<b>252Cf</b> 15.0 10.7 6.1 31.2 4.0 18.1	251Cf	31.6	12.9	21.9	3.7	30.0	3.9	16.6	2.4	-	-	-	
	252Cf	15.0	10.7	6.1		31.2	4.0	18.1		-	-	-	







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# **PWR Uncertainty Requirements**



Table.Critical cross-section uncertainties<br/>processed from BOLNA covariance<br/>matrices and their target accuracies

System studied:

Extended BU PWR

- U-235 enrichment: 8.5%
- Burnup 100 GW d/kg.

Table 22. PWR target accuracies  $(1\sigma)$ 

<b>k</b> <sub>eff</sub>	Doppler reactivity coefficient	Burn-up Δρ	Transmutation		
0.5%	10%	500 pcm	5%		

#### List of priorities

- ➢ Fission cross sections (n,f): <sup>239</sup>Pu, <sup>241</sup>Pu
- Capture cross sections (n, γ): <sup>235</sup>U, <sup>238</sup>U, <sup>239</sup>Pu, <sup>240</sup>Pu, <sup>241</sup>Pu, <sup>242</sup>Pu, <sup>16</sup>O

			Uncertainty (%)				
Isotope	Cross-section	Energy range	T	Required			
			Initial	λ=1	λ≠1 <sup>(a)</sup>		
		67.4 <b>-</b> 24.8 keV	32.9	19.9	18.5		
<sup>235</sup> U	σ <sub>capt</sub>	24.8-9.12 keV	34.0	17.8	16.2		
		9.12-2.03 keV	33.9	11.5	10.3		
		24.8-9.12 keV	9.4	4.6	4.0		
	$\sigma_{capt}$	9.12-2.03 keV	3.1	3.1	2.9		
238 <sub>T T</sub>		454-22.6 eV	1.7	1.4	1.3		
U		19.6-6.07 MeV	13.3	13.1	11.6		
	σ <sub>scatt</sub>	6.07-2.23 MeV	14.6	5.1	4.6		
		2.23-1.35 MeV	18.8	8.0	7.1		
<sup>239</sup> Du	σ <sub>capt</sub>	0.54-0.10 eV	1.4	1.0	0.9		
ru	σ <sub>fiss</sub>	0.54-0.10 eV	0.9	0.9	0.8		
<sup>240</sup> Pu		0.54-0.10 eV	3.2	3.1	3.2		
	Ocapt	0.10 eV-thermal	4.8	3.1	4.0		
		22.6-4.00 eV	8.4	7.3	8.4		
	Ocapt	0.54-0.10 eV	6.8	3.0	3.8		
		2.03-0.454 keV	12.7	11.2	12.7		
241 Du		454-22.6 eV	19.4	4.7	5.9		
ru		22.6-4.00 eV	4.2	3.3	4.2		
	Ofiss	4.00-0.54 eV	26.8	7.7	9.8		
		0.54-0.10 eV	2.9	1.7	2.2		
		0.10 eV-thermal	3.3	1.9	2.4		
<sup>242</sup> Pu	σ <sub>capt</sub>	4.00-0.54 eV	3.8	3.4	3.8		
	6	19.6-6.07 MeV	100.0	12.1	10.9		
	Ucapt	6.07 <b>-</b> 2.23 MeV	100.0	9.9	8.9		
0		19.6-6.07 MeV	84.6	15.6	13.9		
	σ <sub>scatt</sub>	6.07 <b>-</b> 2.23 MeV	54.9	12.6	11.3		
		2.23-1.35 MeV	12.2	8.3	7.5		





# PWR Uncertainty Requirements: EAF2007-EAF2010

Using BOLNA covariance matrices											
					Uncertainty		ΕΛΕ - 20	07	EVE - 30,	10	
Isotpe	•	<b>Cross-section</b>	Energy range	Initial	Requ	uired	EAF - 20	07	EAF - 20.	10	
				mua	λ=1	λ≠1	Energy Range	Uncertainty	Energy Range	Uncertainty	
			67.4 - 24.8 keV	32.9	19.9	18.5					
	235	(n,γ)	24.8 - 9.12 keV	43	17.8	16.2	2.25 keV - 20 MeV	16.67	0.10 eV - 0.10 MeV	3.33	
			9.12 - 2.03 keV	33.9	11.5	10.3					
U			24.8 - 9.12 keV	9.4	4.6	4	10 keV - 20 MeV	16.67			
	238	(n,γ)	9.12 - 2.03 keV	3.1	3.1	2.9	1.0 oV 10 koV	2 22	0.5 eV - 0.10 MeV	3.33	
			454 - 2.6 eV	1.7	1.4	1.3	1.0 eV - 10 keV	3.33			
23	220	(n,γ)	0.54 - 0.10 eV	1.4	1	0.9	Thermal - 0.10 eV	3.70	0.10 eV - 0.10 MeV	4.27	
	239	(n,fission)	0.54 - 0.10 eV	0.9	0.9	0.8	Thermal - 30 keV	3.33	Thermal - 0.50 eV	3.33	
	240	(n,γ)	0.54 - 0.10 eV	3.2	3.1	3.2	0.10 eV - 4.0 keV	3.57	0.10 eV - 0.10 MeV	3.33	
	240		0.10 eV - thermal	4.8	3.1	4	Thermal - 0.10 eV	3.43	Thermal - 0.10 eV	3.33	
		(n.)	22.6 - 4.00 eV	8.4	7.3	8.4	0.10 eV - 0.30 keV	6.27		2 2 2 2	
		(1),9)	0.54 - 0.10 eV	6.8	3	3.8			0.10 ev - 0.10 iviev	5.55	
Pu			2.03 - 0.454 keV	12.7	11.2	12.7					
	2/1		454 - 22.6 eV	19.4	4.7	5.9		2.22			
	241	(n fission)	22.6 - 4.00 eV	4.2	3.3	4.2	Thormal - 20 koV		Thermal - 0.10	2.22	
		(11,11351011)	4.00 - 0.54 eV	26.8	7.7	9.8		5.55	MeV	5.55	
			0.54 - 0.10 eV	2.9	1.7	2.2					
			0.10 eV - thermal	3.3	1.9	2.4					
	242	(n,γ)	4.00 - 0.54 eV	3.8	3.4	3.8	0.05 eV - 1.29 keV	9.10	0.50 eV - 0.10 MeV	3.33	
0		(n))	19.6 - 6.07 MeV	100	12.1	10.9		22.22		22.22	
0		(1,y)	6.07 - 2.23 MeV	100	9.9	8.9	1.0 Mev - 20 Mev	33.33	1.0 Mev - 20 Mev	33.33	





ISOTOPE     EAF-2007     EAF-2010     SCALE 6.0     EAF-2007     EAF-2010     SCALE 6.0     EAF-2010     SCALE 6.0     EAF-2010     SCALE 6.0     EAF-2010     SCALE 6.0     EAF-2007     EAF-2010     SCALE 6.0     EAF-2010     SCALE 6.0     EAF-2010     SCALE 6.0     EAF-2007     EAF-2010     SCALE 6.0     EAF-2010     SCALE 6.0     SCALE 6.0     EAF-2010     SCALE 6.0     SCA	(n,γ-M) <u>EAF-2010</u> <u>SCALE 6.0</u> 26.03 
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	<u>EAF-2010</u> <u>SCALE 6.0</u> 26.03
23415.8615.8424.8238.8726.035.7338.872352.392.390.332.642.351.351.3523611.6712.1619.53.853.12.992.9923816.6516.650.523.153.171.382.64Np23716.516.61773.153.171.382.642387.234.866.013.733.071.792.682393.323.20.788.213.551.171.0124014.9414.272.73.33.091.23	26.03
235   2.39   2.39   0.33   2.64   2.35   1.35      236   11.67   12.16   19.5   3.85   3.1   2.99      238   16.65   16.65   0.52   3.15   3.17   1.38      Np   237   16.5   16.41   7   5.72   7.58   2.68       238   7.23   4.86   6.01   3.73   3.07   1.79       239   3.32   3.2   0.78   8.21   3.55   1.17      240   14.94   14.27   2.7   3.3   3.09   1.23	
236   11.67   12.16   19.5   3.85   3.1   2.99      238   16.65   16.65   0.52   3.15   3.17   1.38      Np   237   16.5   16.41   7   5.72   7.58   2.68      238   7.23   4.86   6.01   3.73   3.07   1.79      239   3.32   3.2   0.78   8.21   3.55   1.17      240   14.94   14.27   2.7   3.3   3.09   1.23	
238   16.65   16.65   0.52   3.15   3.17   1.38   Image: state s	
Np     237     16.5     16.41     7     5.72     7.58     2.68        238     7.23     4.86     6.01     3.73     3.07     1.79        239     3.32     3.2     0.78     8.21     3.55     1.17        240     14.94     14.27     2.7     3.3     3.09     1.23	
238   7.23   4.86   6.01   3.73   3.07   1.79     239   3.32   3.2   0.78   8.21   3.55   1.17      240   14.94   14.27   2.7   3.3   3.09   1.23	
239     3.32     3.2     0.78     8.21     3.55     1.17       240     14.94     14.27     2.7     3.3     3.09     1.23	
<b>240</b> 14.94 14.27 2.7 3.3 3.09 1.23	
Du la	
<b>241</b> 3.3 3.32 0.87 3.9 2.39 0.94	
<b>242</b> 15.81 15.77 4.53 8.51 3.31 9.76	
<b>244</b> 16.56 16.56 21.32 23.48 4.87 35.39	
<b>241</b> 21.34 12.44 1.66 6.38 3.89 2.5 8.08	9.21
Am     241M     3.31     3.33     3.05     22.36     10.19     23.2	
<b>243</b> 15 14.62 5.12 3.72 4.44 2.41 8	3.04
<b>242</b> 16.6 10.79 32.83 19.29 9.42 12.05	
<b>243</b> 3.94 2.56 2.71 5.94 2.35 5.58	
<b>244</b> 13.36 12.22 25.8 6.93 3.01 9.99	
Cm     245     3.65     5.03     2.45     14.68     2.67     4.28	
<b>246</b> 14.6 13.67 8.37 7.99 3.15 5.63	
<b>247</b> 4.96 5.25 13.04 16.51 7.63 6.33	
<b>248</b> 12.91 13.36 16.33 10.48 3.57 5.5	
Bk 249 28.84 14.56 6.47 9.52 7.74 4.96	
<b>249</b> 7.3 2.6 1.76 3.94 2.51 4.39	
Cf 250 13.81 41.36 0.6 4.85 5.93 5.91	
<b>251</b> 8.74 5.7 4.37 5.95 2.88 4.73	
<b>252</b> 11.69 4.84 11.5 12.14 2.65 5.13	











### **FUSION** application: **DEMO**

**Cross-section uncertainties collapsed in one-group using DEMO neutron spectrum** 



(n,γ)



### **FUSION** application: **DEMO**



**Cross-section uncertainties collapsed in one-group using DEMO neutron spectrum** 



# **FUSION** application: **DEMO**



**Cross-section uncertainties collapsed in one-group using DEMO neutron spectrum** 

(n,p) EAF-07/EAF-10



#### **Neutron spectrum effect**

ETSII | UPM







# Neutron spectrum effect: (n,gamma)



To compare values				alues	Best	legular N	Vorst			
(n	,γ)		EAF-2007			EAF-2010		SCALE 6.0		
ISOT	OPE	<u>PWR</u>	<u>ADS</u>	<u>DEMO</u>	<u>PWR</u>	<u>ADS</u>	<u>DEMO</u>	<u>PWR</u>	<u>ADS</u>	<u>DEMO</u>
	234	38.87	38.87	38.87	26.03	26.03	26.03	5.73	6.93	4.95
	235	2.64	11.28	4.75	2.35	3.23	3.2	1.35	21.8	7.32
0	236	3.85	8.9	4.11	3.1	3.2	3.24	2.99	3.11	2.07
	238	3.15	6.67	3.27	3.17	3.17	3.27	1.38	1.44	1.49
Np	237	5.72	14.33	7.63	7.58	9.13	9.79	2.68	3.3	2.21
	238	3.73	14.46	9.99	3.07	3.69	3.27	1.79	6.63	3.84
	239	8.21	12.48	8.64	3.55	4.21	4.18	1.17	4.86	1.59
Du	240	3.3	9.26	3.52	3.09	3.62	3.28	1.23	1.2	0.96
Pu	241	3.9	15.37	7.99	2.39	5.22	3.27	0.94	4	1.9
	242	8.51	12.62	8.01	3.31	3.51	3.27	9.76	5	6.36
	244	23.48	30.44	23.86	4.87	7.36	5.64	35.39	24.88	35.87
	241	6.38	15.81	9.72	3.89	16.65	16.55	2.5	4.67	4.08
Am	241M	22.36	32.77	27.78	10.19	13.18	10.48	23.2	14.66	12.4
	243	3.72	15.34	7.28	4.44	4.98	4.71	2.41	4.48	2.71
	242	19.29	30.01	24.25	9.42	12.86	13.65	12.05	10.8	6.25
	243	5.94	31.97	20.18	2.35	5.21	3.56	5.58	14.24	10.39
	244	6.93	24.56	8.47	3.01	3.72	3.27	9.99	7.72	7.18
Cm	245	14.68	32.75	25.83	2.67	4.13	3.35	4.28	9.83	8.35
	246	7.99	28.21	13.82	3.15	3.7	3.29	5.63	20.32	8.11
	247	16.51	32.12	23.03	7.63	7.67	8.17	6.33	20.59	7.13
	248	10.48	19.19	10.57	3.57	3.79	3.68	5.5	16.85	5.79
Bk	249	9.52	31.73	20.56	7.74	8.82	8.86	4.96	23.99	9.49
	249	3.94	32.39	23.13	2.51	4.8	3.73	4.39	24.59	13.35
Cf	250	4.85	29.33	8.72	5.93	8.97	9.72	5.91	16.06	4.65
CI	251	5.95	29.95	12.72	2.88	3.85	3.22	4.73	16.89	3.99
	252	12.14	31.22	23.64	2.65	4.03	3.8	5.13	18.11	8.01
<b>_</b>										(STINITO)





# Neutron spectrum effect: (n,fission)



To compare values					Best	Regular	Worst				
(n,fis	sion)		EAF-2007			EAF-20	10		SCALE 6.0		
ISOT	OPE	<u>PWR</u>	<u>ADS</u>	<u>DEMO</u>	PWR	ADS	DEMO	<u>PWR</u>	ADS	<u>DEMO</u>	
	234	15.86	16.47	16.43	15.84	16.47	16.43	24.82	29.99	15.37	
	235	2.39	12.86	6.99	2.39	5.5	4.7	0.33	0.41	0.3	
0	236	11.67	15.88	15.68	12.16	15.31	15.63	19.5	27.16	11.42	
	238	16.65	16.61	16.66	16.65	16.61	16.66	0.52	0.54	0.55	
Np	237	16.5	16.66	16.64	16.41	16.39	16.55	7	6.55	3.81	
	238	7.23	12.35	12.5	4.86	10.09	11.21	6.01	10.55	10.75	
	239	3.32	9.59	6.02	3.2	7.87	6.48	0.78	0.4	0.58	
Du	240	14.94	15.84	16.16	14.27	14.68	15.87	2.7	0.57	0.59	
Fu	241	3.3	15.58	8.79	3.32	5.64	4.3	0.87	1.23	0.75	
	242	15.81	16.46	16.52	15.77	16.46	16.52	4.53	3.43	3.61	
	244	16.56	16.48	16.6	16.56	16.47	16.59	21.32	18.96	17.29	
	241	21.34	16.62	16.4	12.44	16.62	16.4	1.66	2.19	2.71	
Am	241M	3.31	16.48	15.1	3.33	5.59	4.28	3.05	9.88	7.28	
	243	15	16.61	16.48	14.62	15.95	16.29	5.12	5.76	9.67	
	242	16.6	16.52	16.17	10.79	16.51	15.66	32.83	31.85	24.37	
	243	3.94	16	10.64	2.56	5.91	4.68	2.71	19.72	9.03	
	244	13.36	16.42	15.93	12.22	14.82	15.39	25.8	37.01	21.33	
Cm	245	3.65	9.75	7.3	5.03	11.33	12.56	2.45	20.18	9.45	
	246	14.6	16.59	16.41	13.67	15.24	15.99	8.37	8.01	8.58	
	247	4.96	16.46	14.43	5.25	16.46	14.44	13.04	11.3	11.42	
	248	12.91	16.19	15.41	13.36	15.28	15.33	16.33	16.17	16.11	
Bk	249	28.84	16.61	16.44	14.56	16.61	16.44	6.47	22.5	20.02	
	249	7.3	16.28	12.85	2.6	5.83	4.79	1.76	19.35	7.31	
Cf	250	13.81	32.97	29.36	41.36	32.98	30.73	0.6	13.32	12.85	
	251	8.74	31.57	17.82	5.7	12.92	9.5	4.37	22.02	9.23	
	252	11.69	14.95	14.72	4.84	10.68	9.74	11.5	6.11	12.54	
-										(States)	





# **SUMMARY & CONCLUSIONS**

#### - ADS

- EAF2010 shows a real improvement
  - $\rightarrow$ To be used as a "reference" activation uncertainty library
- SCALE6.0 should be used as a "reference" uncertainty library

#### $\rightarrow$ Fulfil most accuracy requirements

#### - PWR

- EAF2010 shows an improvement, but does not fulfil all target accuracies
- SCALE6.0 lacks in giving uncertainties for all isotopes
  - → Obtains the lowest uncertainties for U, Np, Pu, Am, Cm, Bk, Cf on (n,f)
  - $\rightarrow$  Obtains the lowest uncertainties for U, Np, Pu on (n,g)

#### - DEMO

- The bulk of cross-section uncertainties is between 3% and 40% for most isotopes
- EAF2010 reduces most of uncertainties, but not for (n,p)
- SCALE6.0 uncertainties **do not reach lower errors than EAF-2010**, but **have some lowest values** for some isotopes

#### - Neutron spectrum effect:

- ADS spectrum has the worst effect on one-group uncertainties
- PWR spectrum reaches the lowest uncertainties
- DEMO spectrum produces cross-section uncertainties between ADS and PWR because it is a mix of fast and thermal energies





# THANK YOU FOR YOUR ATTENTION!!

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