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MODEL

1. Research directions

1. Development of an optimization procedure for the ramp down phase of the plasma and discharge to terminate plasmas in the fastest and safest way:

- Determination of the **optimal time evolution** of the plasma parameters, like plasma current I_p , plasma elongation κ , auxiliary power P_{aux} to terminate plasmas (decrease I_p) as fast as possible.

- For safe termination **physical constraints** have to be specified: constraint on normalized β_N and poloidal β_{pol} (not too high) to avoid MHD modes, constraint on plasma inductance L_i to avoid vertical instability,....

- Define **technical constraints** to match experimental limits, like **max ramp rate of plasma current I_p** , constraint on rate of change in vertical magnetic field B_v for radial position control,....

- Determination of optimal time of H- to L-mode transition.

2. Development of the RAPTOR transport model:

The **RAPTOR** code – Rapid Plasma Transport simulator [1,2]:

- 1D transport code without an equilibrium solver oriented to plasma real-time control.

- Time dependent geometry can be used.

- A new **gradient-based transport model** [3,4] for electron heat transport has been implemented.

- Successful validation via simulation of TCV and AUG full plasma discharges and comparison with the experimental measurements.

[1] F. Felici et al 2011 Nucl. Fusion 51 083502

[2] F. Felici, O. Sauter 2012 PFCF 54 25002

[3] O. Sauter et al 2014 Phys. of Plasmas 21 055906

[4] D. Kim et al 2016 PFCF 58 055002

2. Trajectory optimization [2]

To get a good trajectory optimization

- 1) **realistic predictive simulations** (\Rightarrow an appropriate transport model) and
- 2) **fast solver** (\Rightarrow RAPTOR) are needed.

- Plasma current I_p
- ECH power P_{ECH}
- NBI power P_{NBI}
- Plasma elongation κ
- Poloidal flux $\psi(\rho, t)$
- Electron temperature $T_e(\rho, t)$
- Electron density $n_e(\rho, t)$
- Ion temperature $T_i(\rho, t)$

actuator evolution (input trajectories) \rightarrow Tokamak profile simulation \rightarrow profile evolution (state trajectories)

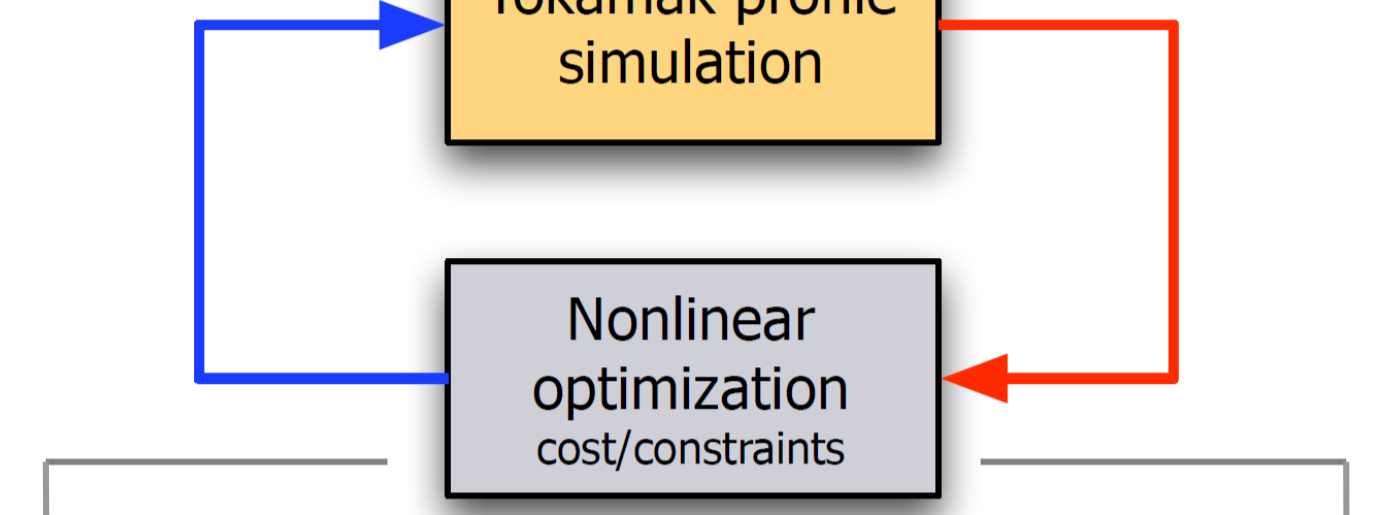


Fig. 1. Scheme of the nonlinear procedure for the actuator trajectories optimization [2].

Cost function

$$J = \sum_{i=1}^n v_i J_i; \min(J)$$

$$\text{Examples: } J_i = \|v_i(t_f) - v_{i,ref}\|_{W_i}^2$$

$$J_{ss} = \|\partial U_p / \partial \rho\|_{W_{ss}}^2$$

$$J_{I_p} = \int I_p dt$$

Constraints:

- Safety factor q (>1.0)
- Plasma inductance $L_i(3)$
- Edge loop voltage U_{pi}
- ... various physical and technical constraints (I_p max ramp rate)

3. The transport model

Diffusion equations: electron temperature and poloidal flux

$$\frac{3}{2} (V')^{-5/3} \left(\frac{\partial}{\partial t} - \frac{B_0}{2B_0} \frac{\partial}{\partial \rho} \right) \left[(V')^{5/3} n_e T_e \right] = \frac{\partial}{\partial \rho} \left(V' G_1 n_e \chi_e \frac{\partial T_e}{\partial \rho} + V' P_e \right)$$

$$\sigma \left(\frac{\partial \psi}{\partial t} - \frac{\rho B_0}{2B_0} \frac{\partial \psi}{\partial \rho} \right) = \frac{J^2 R_0}{\mu_0 \rho} \frac{\partial}{\partial \rho} \left(\frac{G_2}{J} \frac{\partial \psi}{\partial \rho} \right) - \frac{V'}{2\pi \rho} (j_{BS} + j_{CD})$$

Electron heat diffusivity: gradient-based model [3,4]

$$\chi_e = \frac{q_e}{V' (\rho)^2 n_e T_e} \left[\frac{\mu_{Te}}{T_e} f \left(\frac{\rho - \rho_{ped}}{\delta \rho_{ped}} \right) + \frac{\mu_{Te}}{\rho_{edge}} f \left(\frac{\rho - \rho_{ped}}{\delta \rho_{ped}} \right) \right]^{-1} \times f \left(\frac{\rho_{inv} - \rho}{\delta \rho_{inv}} \right) + \chi_{ST} f \left(\frac{\rho - \rho_{inv}}{\delta \rho_{inv}} \right)$$

$$\frac{R}{L_{Te}} = \frac{R_0}{a} \frac{d \ln T_e}{d \rho} = \begin{cases} 0 & \text{for } \rho_V < \rho_{Te,inv} \\ \frac{R_0}{a} \lambda_{Te} & \text{for } \rho_{Te,inv} < \rho_V < \rho_{Te,ped} \\ \frac{R_0}{a} \frac{\mu_{Te}}{T_e (\rho_V)} & \text{for } \rho_V > \rho_{Te,ped} \end{cases}$$

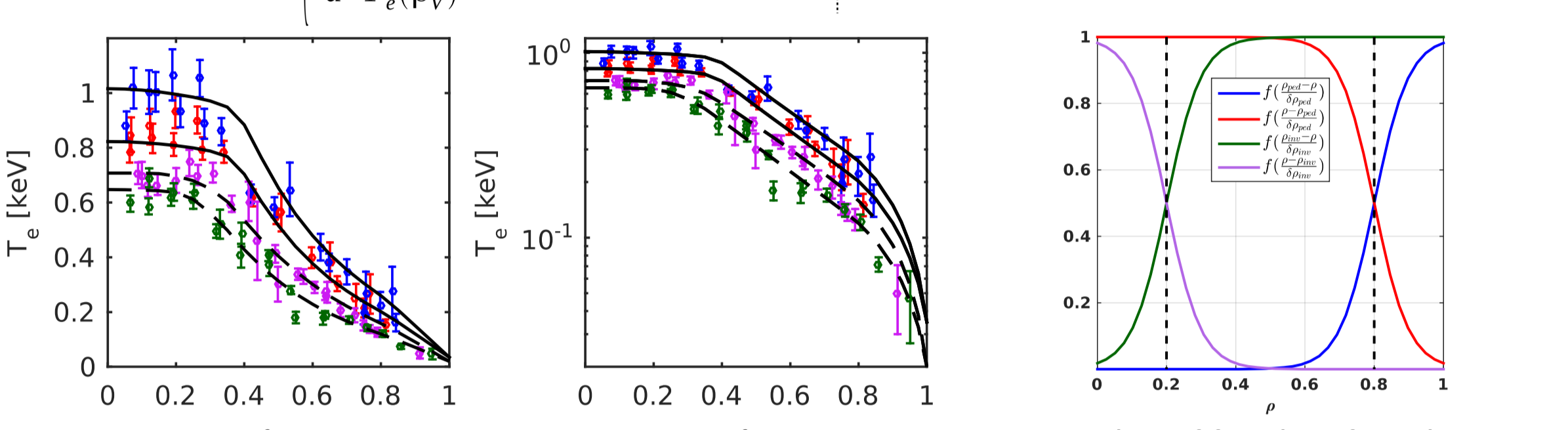
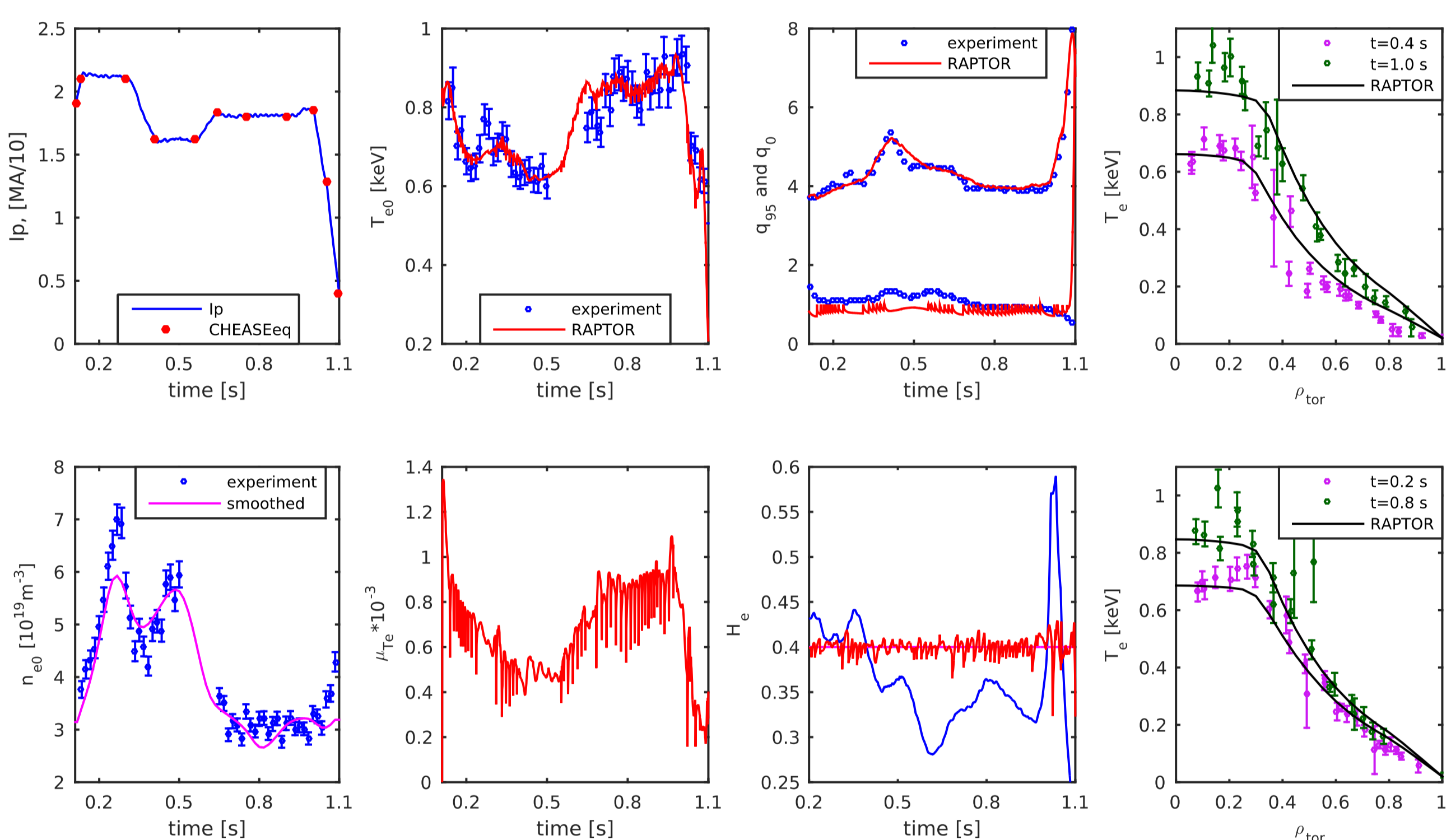


Fig. 2. RAPTOR simulated profiles (black solid) vs the experimental ones for the TCV plasma: \bullet – #50719 $I_p=195$ kA, \circ – #50719 $I_p=206$ kA, \diamond – #53851 $I_p=205$ kA, \square – #53851 $I_p=185$ kA.

VALIDATION

4. Full TCV plasma simulation: #53852, ohmic plasma, L-mode



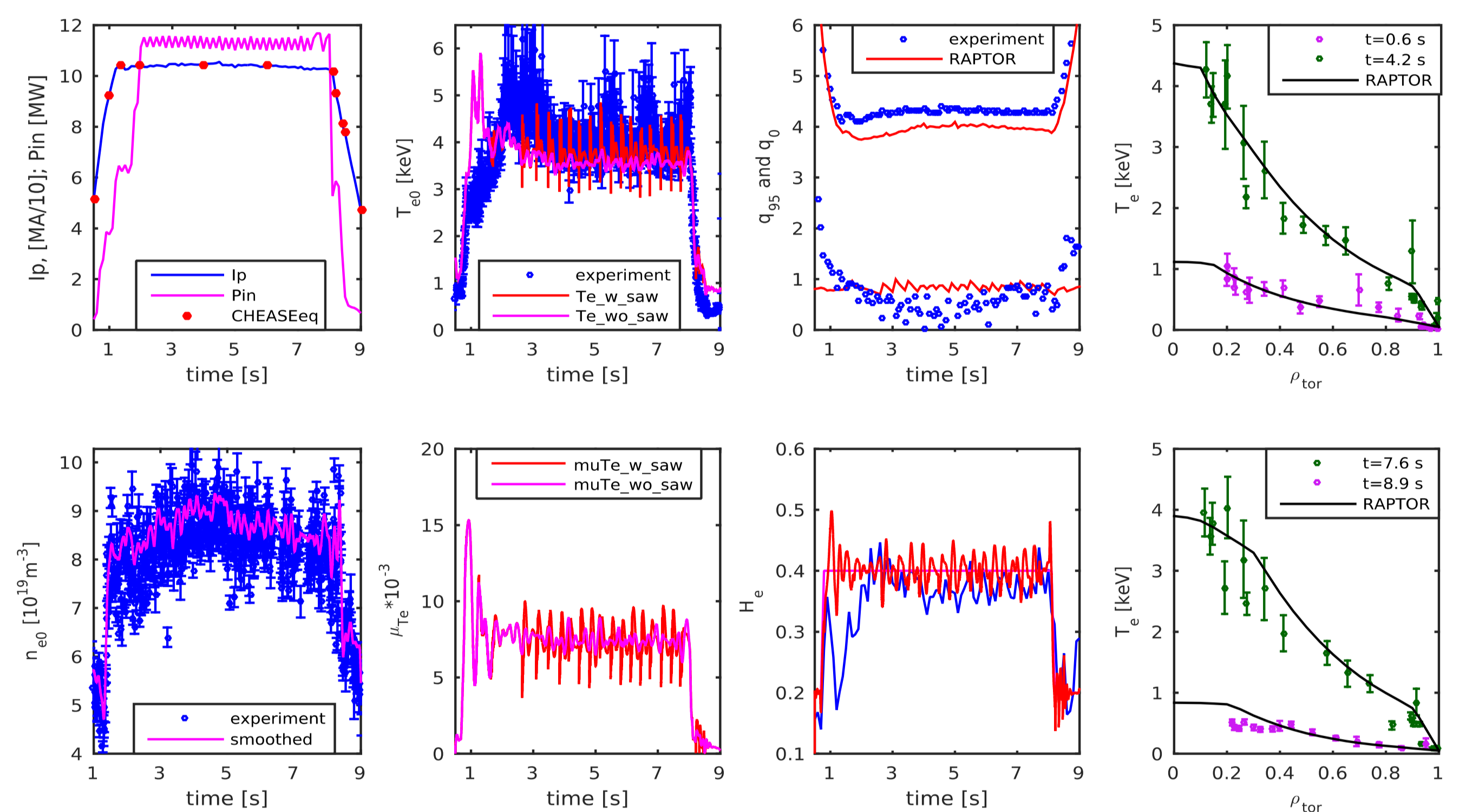
Prescribed parameters: total plasma current I_p over time, radial profiles of electron density n_e over time, H_e factor fixed at 0.4, $\lambda_e=3.2$ (λ_{e0} line averaged electron density n_{e0} if $n_e(\rho, t)$ not provided), scaling law H98(y,2) for total confinement time.

Predicted variables: electron temperature T_e , poloidal flux ψ , electron heat diffusivity χ_e , various physical quantities.

Equilibrium: 10 CHEASE equilibria (marked as \bullet on the I_p plot).

CPU time: less than 2 min for a time grid with 1 ms step (shot duration 1 s) on a standard PC.

5. Full AUG plasma simulation: #32546, NBH, ECRH, L-H-L modes



Prescribed parameters: same as for TCV case, total input NBI and EC power over time and their deposition, H_e factor fixed at 0.4 for H-mode and at 0.2 for L-mode, $\lambda_e=3.0/2.3$ for L/H-mode, Gaussian radial profiles for heating sources.

Predicted variables: as for TCV case

Equilibrium: 11 CHEASE equilibria (marked as \bullet on the I_p plot).

CPU time: less than 10 min for a time grid with 1 ms step (shot duration 8.5 s) on a standard PC.

OPTIMIZATION

6. Generic ramp down optimization

Ramp down optimization of plasma current and elongation at $t=0.5$ s for AUG-like plasma: cost function $J_p = \int I_p dt$

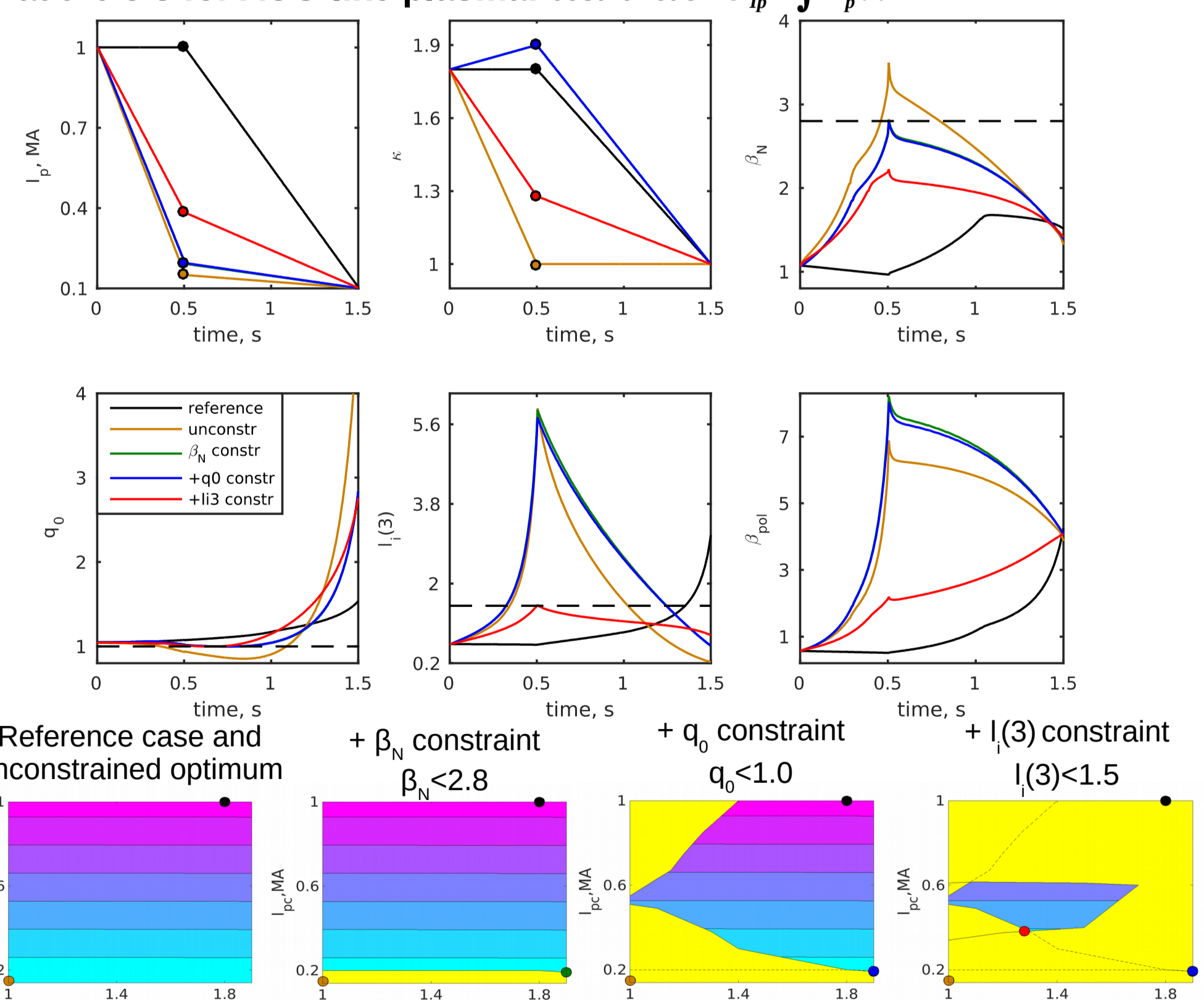
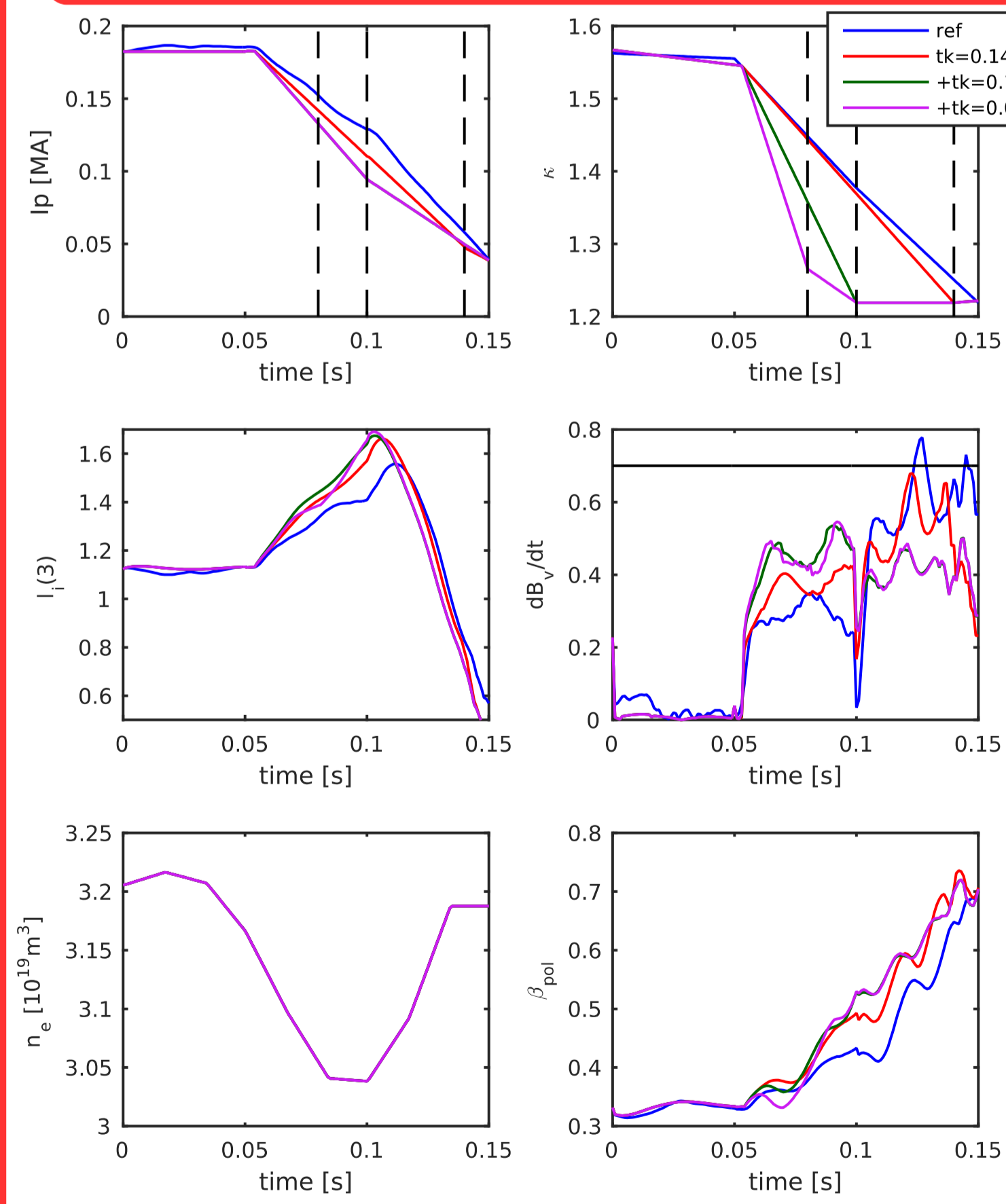


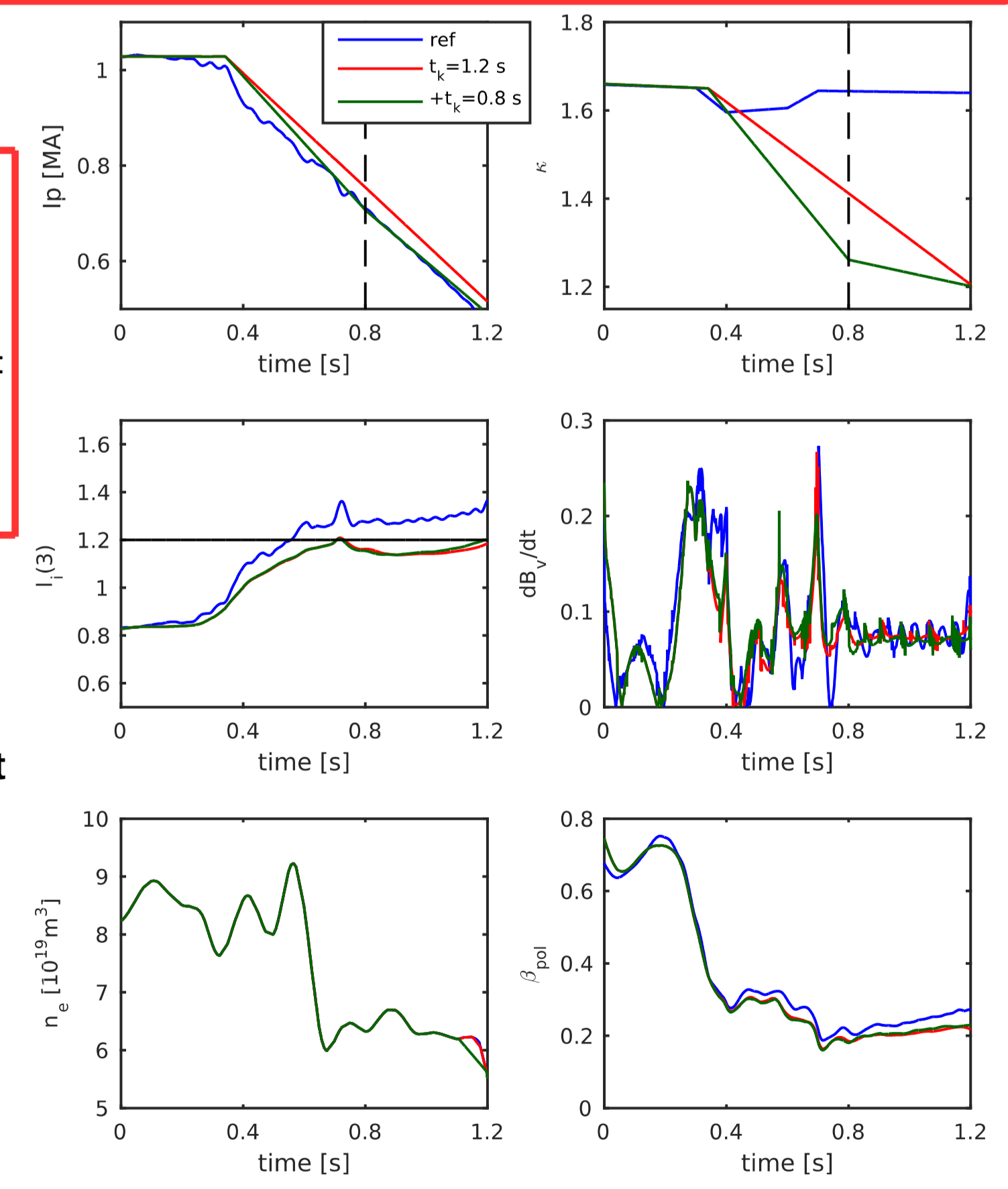
Fig. 4. The contours for J_p are shown with the coloured circles which correspond to values of I_p and κ at $t=0.5$ s. An area where the constrained parameter violates the constraint is yellow-marked.

7. Ramp-down optimization: TCV #53852



\Rightarrow Faster I_p and κ ramp down can be used.

8. Ramp-down optimization: AUG #32546



\Rightarrow Reducing κ during ramp down would allow to better control I_p .

PLANS

9. Further research directions

1. Need better control on μ_{Te} (less oscillations):

now μ_{Te} = feed-forward + feed-back control.

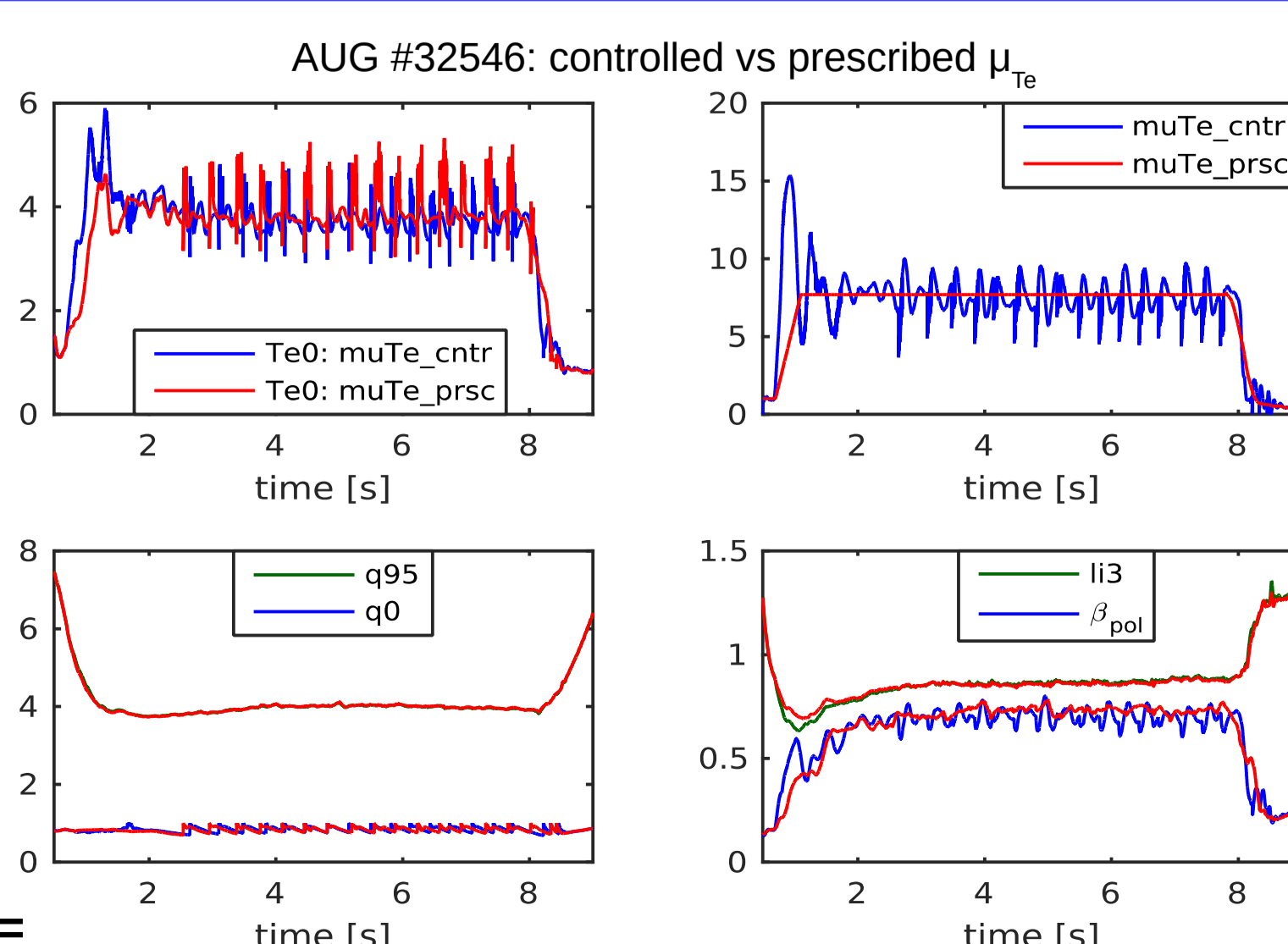
$$\mu_{Te} = \frac{\mu_{Te}^{ff}}{\text{feed-forward}} + \frac{\mu_{Te}^{fb}}{\text{feed-back}}$$

$$\text{where } \text{err}(t) = H_e^{ref} - H_e^{calc} = H_e^{ref} - \tau_{e0} / \tau_{scf}$$

Feed-forward law for μ_{Te} via relation with $T_e(\rho_{ped})$:

$$\mu_{Te}^{ff} = - \frac{dT_e}{d\rho} = - \frac{T_e(\rho_{ped}) - T_e^{BC}}{\rho_{ped} - 1.0}$$

Present oscillations do not disturb physics result \Leftarrow



now $T_e(\rho_{ped})$ for μ_{Te}^{ff} is estimated: $T_e(\rho_{ped}) = T_{e0} \exp(-\lambda_{Te}(\rho_{ped} - \rho_{inv}))$

T_{e0} scaling law for TCV: $T_{e0} = 7.5 \cdot 10^3 \cdot (I_p [MA])^{0.93} \cdot (P_{tot} [MW])^{0.3} \cdot (n_e [10^{19} m^{-3}])^{-0.6}$

T_{e0} scaling law for AUG: $T_{e0} = 3.3 \cdot 10^3 \cdot (I_p [MA])^{0.93} \cdot (P_{tot} [MW])^{0.3} \cdot (n_e [10^{19} m^{-3}])^{-0.6}$

2. Need a scaling law for pedestal pressure for L-/H-mode (to determine μ_{Te} directly).

3. Include diffusion equation for electron density to the transport model:

now prescribed n_e is used;

now to keep density within Greenwald density limit during optimization: $n_e(0, t) = \min(n_{ref}(0, t), n_{GR}) = \min(n_{ref}(0, t), 0.9 \frac{I_p(t)}{\pi a^2})$

4. Continue ramp-down optimization with an extended set of parameters:

- time of H- to L-mode transition as an optimization parameter (already implemented, need tests);
- constraints related to radiated power and impurities;
- technical constraints on rate of change of electron density, plasma shape;
- technical constraint on vertical position control (constraint on dI/dt).

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