

# Back-Contacted Silicon Heterojunction Solar Cells: Optical-Loss Analysis and Mitigation

Bertrand Paviet-Salomon, Andrea Tomasi, Antoine Descoedres, Loris Barraud, Sylvain Nicolay, Matthieu Despeisse, Stefaan De Wolf, and Christophe Ballif

**Abstract**—We analyze the optical losses that occur in interdigitated back-contacted amorphous/crystalline silicon heterojunction solar cells. We show that in our devices, the main loss mechanisms are similar to those of two-side contacted heterojunction solar cells. These include reflection and escape-light losses, as well as parasitic absorption in the front passivation layers and rear contact stacks. We then provide practical guidelines to mitigate such reflection and parasitic absorption losses at the front side of our solar cells, aiming at increasing the short-circuit current density in actual devices. Applying these rules, we processed a back-contacted silicon heterojunction solar cell featuring a short-circuit current density of 40.9 mA/cm<sup>2</sup> and a conversion efficiency of 22.0%. Finally, we show that further progress will require addressing the optical losses occurring at the rear electrodes of the back-contacted devices.

**Index Terms**—Heterojunction, interdigitated back-contact, optical losses, parasitic absorption, silicon, solar cell.

## I. INTRODUCTION

**A**MORPHOUS/CRYSTALLINE silicon heterojunction (SHJ) solar cells are promising candidates to achieve high conversion efficiencies at competitive cost [1]. Owing to the outstanding passivation level of the crystalline silicon (c-Si) surface obtained by hydrogenated amorphous silicon (a-Si:H) layers, two-side contacted SHJ solar cells feature to date open-circuit voltages ( $V_{oc}$ ) as high as 750 mV and efficiencies up to 24.7%, as demonstrated by Panasonic, Japan [2].

However, two-side contacted SHJ architectures, with the hole collector (“emitter,” for n-type wafers) either located at the front (FE-SHJ) or at the rear (RE-SHJ) of the devices, are ultimately limited by front metal grid shadowing and parasitic absorption

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of light in the thin a-Si:H and transparent conductive oxide (TCO) deposited films [3], [4]. Meticulous efforts have been dedicated over the last few years toward the reduction of these parasitic losses, especially by thinning as much as possible the front a-Si:H layers [5] and reducing the metal-finger width using increasingly sophisticated metallization techniques [6]–[8]. To date, the best outcome for this approach is a short-circuit current density ( $J_{sc}$ ) value of 40.0 mA/cm<sup>2</sup>, obtained by Kaneka, Japan, for an SHJ solar cell with copper-electroplated contacts [6]. Other approaches include the use of window layers consisting of wider bandgap materials [9] or metal oxides [10].

Alternatively, parasitic losses can be drastically reduced by adoption of the back-contacted device architecture. In back-contacted SHJ solar cells, the hole and electron collectors, and their respective electrodes, are placed at the rear side of the device [11]. The front side is, hence, devoid of any front metal shadowing, increasing also the device “aesthetics.” In addition, since in this design, no carrier collection occurs in the front-side layers, any related material property constraint is absent. As a result, in back-contacted devices, front-side layers can be purposely tuned to harvest efficiently sunlight. Back-contacted SHJ solar cells are thus expected to yield higher  $J_{sc}$  values, while still featuring the high  $V_{oc}$  and implied fill-factor values characteristic for their two-side contacted counterparts. These expectations were convincingly fulfilled by Panasonic, Japan, reporting in early 2014 on a 25.6%-efficient back-contacted SHJ solar cell on a full 5-in wafer [12]. This remarkable result sets a new world-record efficiency for single-junction c-Si-based solar cells under 1-sun illumination.

Table I summarizes the current state of the art of back-contacted SHJ solar cells. We limit this overview to devices with efficiency higher than 19.0% and sorted them by decreasing  $J_{sc}$  values. Surprisingly, most of these devices feature  $J_{sc}$  values lower than Kaneka’s “standard” SHJ solar cell mentioned above [6]. The two notable exceptions are the results by Panasonic, Japan [12] and Sharp, Japan [13], who demonstrated  $J_{sc}$  values of 41.8 and 41.7 mA/cm<sup>2</sup>, respectively. Noteworthy, the details on the front stack they used to reach such impressive  $J_{sc}$  values remain not completely disclosed so far. From these results, we infer that proper optimization of sunlight absorption and carrier collection in back-contacted SHJ solar cells may not be so straightforward. Indeed, the front-side layers of such devices must provide simultaneously sufficiently high electrical passivation and optical transparency, while also featuring a suitable refractive index for antireflection coating (ARC) purposes.

Several reasons may be held accountable for the peculiar fact that most back-contacted SHJ devices have yet to achieve

TABLE I  
STATE-OF-THE-ART OF BACK-CONTACTED SHJ SOLAR CELLS WITH  
EFFICIENCY HIGHER THAN 19.0%, SORTED BY DECREASING  $J_{sc}$

| Affiliation and reference | Year | Area [cm <sup>2</sup> ] | $J_{sc}$ [mA/cm <sup>2</sup> ] | $V_{oc}$ [mV] | FF [%] | Eff. [%] |
|---------------------------|------|-------------------------|--------------------------------|---------------|--------|----------|
| Panasonic, Japan [12]     | 2014 | 143.7 (da)              | 41.8                           | 740           | 82.7   | 25.6     |
| Sharp, Japan [13]         | 2014 | 3.72 (ap)               | 41.7                           | 736           | 81.9   | 25.1     |
| CSEM-EPFL (this work)     | 2015 | 9.0 (da)                | 40.9                           | 726           | 74.0   | 22.0     |
| EPFL, Switzerland [14]    | 2014 | 9.0 (da)                | 39.9                           | 724           | 74.5   | 21.5     |
| HZB-ISFH, Germany [15]    | 2011 | 1 (da)                  | 39.7                           | 673           | 75.7   | 20.2     |
| CEA-INES, France [16]     | 2014 | 18.1 (da)               | 38.6                           | 689           | 74.9   | 19.9     |
| LG, Korea [17]            | 2014 | 221 (ta)                | 37.5                           | 716           | 76.4   | 20.5     |

ap: aperture area; da: designated area; ta: total area (see [18]). FF: fill-factor. Eff.: conversion efficiency.

top  $J_{sc}$  values. First and foremost, two front-side schemes are predominantly featured in such devices: either a-Si:H layers combined with dielectrics-based ARCs [14], [17], [19]–[22] or high-temperature diffused front-surface fields (FSF) combined with ARCs [15], [23]. These two options originate from stacks standardly used in two-side contacted solar cells, usually featured at the front side of both heterojunction [24] and homojunction [25] rear-emitter devices, respectively.

Some alternatives to these front stacks have also been investigated. The zinc sulfide/silicon carbide stack proposed by Shu *et al.* [22] yielded a  $J_{sc}$  of 31.2 mA/cm<sup>2</sup>: a value mainly limited due to a low passivation level. Similarly, the native oxide/silicon nitride scheme introduced by Chowdhury *et al.* [26] led to a maximum  $J_{sc}$  of 35.4 mA/cm<sup>2</sup> [27]. Doubtlessly, these values are also seriously limited, since for both results, mirror-polished wafers were used. Ziegler *et al.* [28] processed back-contacted SHJ devices with black silicon at the front, aiming at enhanced light absorption. However, this approach has yet to lead to higher  $J_{sc}$  values than those achieved with a standard pyramid-textured front side using a potassium hydroxide solution.

For *homojunction* back-contacted devices, Ohrdes *et al.* [29] recently showed that the diffused FSF is mainly required to maintain high passivation at low injection levels at the front side, rather than to provide additional lateral conductivity for majority carriers. Hence, the FSF can advantageously be replaced by a dielectric layer with a high fixed charges density, such as aluminum oxide [29]. Along these lines, using an aluminum oxide/silicon nitride stack to passivate the undiffused front side of homojunction back-contacted solar cells, Peibst *et al.* demonstrated a  $J_{sc}$  of 41.8 mA/cm<sup>2</sup> [30]. Using only silicon nitride,  $J_{sc}$  values > 41.0 mA/cm<sup>2</sup> have also been reached [31]. Although originally designed for homojunction back-contacted solar cells, such front-side schemes can equally well be applied to heterojunction back-contacted devices.

Other phenomena intrinsically linked to the back-contacted SHJ architecture can also hinder the achievement of high  $J_{sc}$  values. Minority carriers generated above the electron-collecting

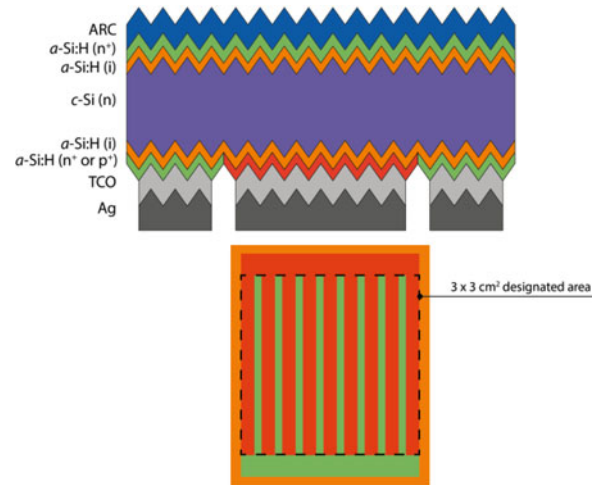


Fig. 1. Cross-sectional (top) and bottom view (bottom) of our IBC-SHJ solar cell (not to scale).

regions have indeed a reduced probability of being efficiently collected by the hole collector, due to the several 100- $\mu$ m-long spacing between the electron- and hole-collecting regions. This can result in  $J_{sc}$  losses. This effect is known as *electrical shading* and has been extensively investigated both for homojunction and heterojunction back-contacted devices [32]–[34]. Eventually, back-contacted SHJ devices require bulk materials with sufficiently long carrier diffusion lengths to perform at their best [35], [36].

To quantify the losses resulting from these different mechanisms, an in-depth investigation of the  $J_{sc}$  losses in back-contacted SHJ devices is needed. In this contribution, we therefore aim at 1) proposing a complete analysis of the  $J_{sc}$  losses in back-contacted SHJ devices and 2) providing practical guidelines to mitigate these losses, hence increasing the  $J_{sc}$  in actual devices. Regarding this latter point, we focus on the reduction of the reflection and parasitic absorption losses at the front side of back-contacted SHJ solar cells. As a result of our optimization, we obtained a  $J_{sc}$  gain of 1.0 mA/cm<sup>2</sup> compared with our previous best device, yielding a conversion efficiency of 22.0% with a  $J_{sc}$  of 40.9 mA/cm<sup>2</sup>.

## II. EXPERIMENTAL DETAILS

### A. Interdigitated Back-Contacted Silicon Heterojunction Solar Cells Processing

Interdigitated back-contacted silicon heterojunction solar cells (IBC-SHJ) were fabricated on n-type, 250- $\mu$ m-thick, 3- $\Omega$ -cm, 4-in float-zone wafers. The active cell area is 9.0 cm<sup>2</sup>, excluding the busbar area. A schematic of our standard device structure is depicted in Fig. 1. It features a pitch of 2.6 mm, with 1.6-mm-wide hole-collecting fingers and 1.0-mm-wide electron-collecting regions. No gap was left between the hole- and the electron-collecting regions. This does not lead to shunt losses due to the low conductivity of the a-Si:H layers. The respective metallization fingers for hole and electron collection are separated by a gap of 300  $\mu$ m.

TABLE II  
DESCRIPTION OF THE IBC-SHJ DEVICES PROCESSED IN THIS PAPER

| IBC-SHJ device | n-type a-Si:H layer thickness at front [nm] | ARC scheme                                       |
|----------------|---|--|
| #1             | 12  | single-layer a-SiN <sub>x</sub> :H               |
| #2             | 6   |  |
| #3             | 1   |  |
| #4             | 0   |  |
| #5             | 6   | a-SiN <sub>x</sub> :H/a-SiO <sub>x</sub> :H DARC |
| #6             | 0   |  |

Following saw-damage etching, alkaline texturing, and chemical cleaning, the wafers were shortly dipped into a 5% hydrofluoric acid solution for oxide etching and loaded into our plasma-enhanced chemical vapor deposition (PECVD) tool. We used an OctopusII system from INDEOtec SA. We deposited a stack consisting of an intrinsic a-Si:H layer capped with an n-type a-Si:H layer at the device front side, and a single intrinsic a-Si:H passivation layer was deposited at the back. These layers have typical thickness as used in two-side contacted SHJ devices (5–10 nm). Patterned p- and n-type a-Si:H fingers were afterwards plasma-deposited at the back, using *in-situ* shadow masking. The device front side was eventually completed by plasma-depositing a 75-nm-thick hydrogenated amorphous silicon nitride (a-SiN<sub>x</sub>:H) ARC layer. All a-Si:H and a-SiN<sub>x</sub>:H layers were deposited at 200 °C. To fabricate the rear electrodes, we deposited a TCO/Ag stack on the full rear side using physical vapor deposition. The patterning into electron- and hole-collecting electrodes was achieved by a combination of hot-melt inkjet printing and wet-chemical etching. Hot-melt inkjet printing was performed by the commercial system LP50 from Roth & Rau B. V. Finally, the solar cells were cured at 200 °C in a belt furnace to heal potentially present sputter-induced damage of the a-Si:H layers [37]. Further experimental details can be found in [14] and [38], especially regarding the low-cost patterning processes we developed.

The actual optimization of the  $J_{sc}$  of our devices starts from the baseline process flow described above. Several steps were then independently varied. First, we tested four different thicknesses for the front-side n-type a-Si:H layer, namely 12, 6, 1, and 0 nm (i.e., no front n-layer at all). Second, we investigated the use of a double-layer ARC (DARC) instead of the baseline single-layer a-SiN<sub>x</sub>:H ARC. This DARC consists of a 62-nm-thick layer of a-SiN<sub>x</sub>:H, capped with an 88-nm-thick hydrogenated amorphous silicon oxide (a-SiO<sub>x</sub>:H) layer. The refractive index of these layers is 1.87 and 1.46 at a wavelength of 630 nm, respectively. Finally, a device featuring only an intrinsic a-Si:H layer at the front (no n-type a-Si:H layer) and a DARC was processed, aiming at reaching high  $J_{sc}$ . Table II summarizes the characteristics of the aforementioned IBC-SHJ devices.

For reference, the performance of our IBC-SHJ devices was compared with that of a two-side contacted FE-SHJ solar cell processed in our laboratory, already reported in [24]. At the front side, this FE-SHJ device features a thin intrinsic/p-type a-Si:H layer, a highly-transparent IO:H/ITO stack, and a screen-printed

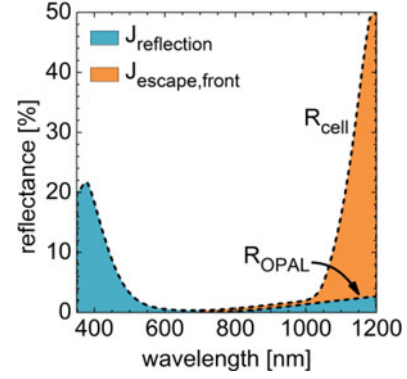


Fig. 2. Reflection spectrum experimentally measured ( $R_{cell}$ ) on an actual IBC-SHJ solar cell and OPAL-simulated ( $R_{OPAL}$ ) reflection spectrum accounting only for the front side of the same device. The two curves usually start to differ from 850 nm on. The area to be integrated over the AM1.5G spectrum to calculate the reflection losses ( $J_{reflection}$ ) and the amount of light escaping at the front ( $J_{escape,front}$ ) is also shown.

metal grid with 4% metallized area fraction. On the rear side, a full-area TCO/metal electrode is used.

### B. Solar Cells Characterization and Simulation

The current–voltage ( $I$ – $V$ ) characteristics of our solar cells were measured in-house on a Wacom WXS-90S-L2 system using standard test conditions at 25 °C under 1-sun AM1.5G equivalent illumination. We defined a 3 cm × 3 cm designated area using a shadow mask, excluding the busbar area (see Fig. 1). The shadow mask area is defined with an accuracy better than 0.05 cm<sup>2</sup>. We used an aluminum-anodized black chuck specifically designed to provide an alignment accuracy of ±50 μm between the device under test and the shadow mask. We measured the pseudo fill-factor ( $pFF$ ) values of our devices using a Suns- $V_{oc}$  tool from Sinton Instruments [39].

The external quantum efficiency (EQE) curves of the devices were measured using the IQE-SCAN system from PV-tools. The spot area is 2 cm × 2 cm. Solar cells were measured under a 0.5-sun light bias, at a chopping frequency of 230 Hz. These settings ensure that there is <2% relative difference between the  $J_{sc}$  measured on the  $I$ – $V$  setup and the one calculated from the EQE curve.

The solar cells reflectance ( $R_{cell}$ ) and transmission ( $T_{cell}$ ) spectra were measured using a Lambda950 spectrometer from PerkinElmer. The solar cell total absorbance ( $A_{cell}$ ) is then calculated as  $A_{cell} = 1 - (R_{cell} + T_{cell})$ .

We used the OPAL software [40] to calculate the theoretical reflectance ( $R_{OPAL}$ ) and absorbance ( $A_{OPAL}$ ) spectra for the front a-Si:H and ARC layers used in our SHJ devices. The refractive index and absorption-coefficient spectra of our layers required for these simulations were acquired using a Horiba UVISEL ellipsometer. As OPAL assumes semi-infinite substrates, the simulated  $R_{OPAL}$  spectrum does not account for long wavelength light internally reflected at the rear side of the wafer. The comparison of the OPAL-simulated reflection spectrum with the one measured on the actual device (see Fig. 2) thus allows us to separate the reflection losses due merely to the front



stack from those due to the long-wavelength light internally reflected at the back. In the case of the IBC-SHJ devices processed in our laboratory, the  $R_{OPAL}$  and  $R_{cell}$  spectra usually start to differ from 850 nm on.

### C. Calculation of Short-Circuit Current Losses

We calculated the  $J_{sc}$  losses in our SHJ solar cells by integrating the area between the EQE and the absorbance ( $A_{cell}$ ; see Section II-B) curves over the AM1.5G solar spectrum. The general expression for the calculation of the  $J_{sc}$  losses ( $J_{loss}$ ) has the following form:

$$J_{loss} = \frac{q}{hc} \int_{\lambda_1}^{\lambda_2} \lambda \cdot \Phi(\lambda) \cdot [A_{cell}(\lambda) - EQE(\lambda)] \cdot d\lambda \quad (1)$$

where  $q$  is the elementary charge,  $h$  is Planck's constant,  $c$  is the speed of the light,  $\lambda$  is the photon wavelength, and  $\Phi(\lambda)$  is the AM1.5G solar spectrum.  $\lambda_1$  and  $\lambda_2$  are the outer bounds of the range for which the  $J_{loss}$  calculation is performed. The values of  $\lambda_1$  and  $\lambda_2$  are reported in the Appendix.

To facilitate the discussion, current losses are grouped into external and internal losses, as also proposed in [3], [4], and [41]. External losses are optical losses which result from light that is not absorbed in the device (e.g., due to reflection or transmission losses) and, thus, does not generate any carrier. In contrast, internal losses result from light that is absorbed in the device, but is then either lost due to internal parasitic absorption (e.g., in the a-Si:H or the TCO layers), or whose generated carriers are lost due to imperfect collection.

Regarding *external* losses, we distinguish three different mechanisms. At the device front, part of the light is lost due to external reflection. These reflection losses ( $J_{reflection}$ ) are calculated by integrating the OPAL-simulated reflection spectrum of the front side of the IBC-SHJ device under test ( $R_{OPAL}$ ; cf., Section II-B), as shown in Fig. 2. At the back side of the device, part of the long wavelength light is lost by transmission through the gaps between the rear electrodes (300- $\mu$ m-wide; see Section II-A), whereas another part is internally reflected toward the front side, where part of it further escapes. The former is called escape light at the back ( $J_{escape,back}$ ), and the latter escape light at the front ( $J_{escape,front}$ ).  $J_{escape,back}$  is calculated by integrating the transmission curve of the cell.  $J_{escape,front}$  is calculated by integrating the area between the  $R_{cell}$  (the measured solar cell reflectance) and the  $R_{OPAL}$  curves at wavelengths  $>850$  nm, as illustrated in Fig. 2.

Note that in the case of two-side contacted SHJ devices, a fourth external loss mechanism exists, namely the effective shadowing losses ( $J_{shadowing}$ ) due to the front metal grid. When required, we calculated  $J_{shadowing}$  as the difference between the 1-sun  $J_{sc}$  measured on the actual device and the  $J_{sc}$  calculated by integrating the EQE curve measured on a front electrode-free device, purposely fabricated for spectral response measurement. On this device, the EQE is measured by placing the probes directly on the front TCO. The lateral conductivity of this layer is sufficient to carry out an EQE measurement.

*Internal* losses can be broken down according to the spectral region in which they occur. In our analysis (similarly to

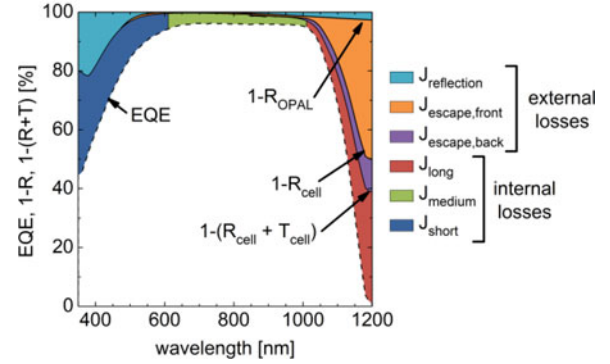


Fig. 3. Illustrative example of  $J_{sc}$  loss sources in our IBC-SHJ solar cell.

[3] and [4]), we discerned between short-wavelength current losses, corresponding to the wavelength integration range between 350 and 600 nm ( $J_{short}$ ), medium wavelength losses in the range 600–1000 nm ( $J_{medium}$ ), and long-wavelength losses in the range 1000–1200 nm ( $J_{long}$ ).  $J_{short}$  hence accounts for the losses occurring in the ultraviolet and the blue part of the spectrum,  $J_{medium}$  in the visible range, and  $J_{long}$  in the infrared region. For the sake of clarity, all these loss sources are exemplarily depicted in Fig. 3, and the corresponding formulas are detailed in Table V in the Appendix.

The actual  $J_{sc}$  of the device can finally be retrieved by subtracting the sum of all  $J_{sc}$  losses to the available photocurrent ( $J_{ph}$ ), where  $J_{ph}$  is given by the integration of the AM1.5G spectrum over 350–1200 nm, which equals 45.9 mA/cm<sup>2</sup>, assuming that each photon in this spectral region generates one electron–hole pair and each generated charge carrier is successfully separated and collected. This assumption does not take into account impact ionization effects occurring at short wavelengths, which can lead to quantum efficiencies exceeding unity [42], [43]. Thus, assuming  $J_{ph} = 45.9$  mA/cm<sup>2</sup> might actually result in a slight underestimation of the actual maximum  $J_{sc}$  for an infinitely thick Si solar cell. Quantum efficiency values higher than one have been recently observed in homojunction back-contacted devices [30].

Importantly, our  $J_{sc}$  losses are thus calculated with respect to this available photocurrent  $J_{ph} = 45.9$  mA/cm<sup>2</sup>. This value does not account for the finite thickness of the actual device and thus should not be considered as a maximum value for the achievable  $J_{sc}$  of practical devices. Detailed analysis of the theoretical limits of  $J_{sc}$  in solar cells can be found elsewhere [44], [45].

## III. RESULTS AND DISCUSSION

### A. Breakdown of Short-Circuit Current Losses: Two-Side Contacted Versus Interdigitated Back-Contacted Silicon Heterojunction Solar Cells

Table III gives the electrical parameters of two reference FE-SHJ and IBC-SHJ solar cells processed in our laboratory and reported in [24] and [14], respectively. Their EQE,  $R_{cell}$ ,  $T_{cell}$ , and  $A_{cell}$  curves are displayed in Fig. 4. Notice that the transmission curve of the FE-SHJ solar cell is zero, as it features a

TABLE III  
ONE-SUN  $I$ - $V$  PARAMETERS OF THE REFERENCE FE-SHJ AND IBC-SHJ SOLAR CELLS PROCESSED IN OUR LABORATORY AND OBJECTS OF THE  $J_{sc}$  LOSSES ANALYSIS PRESENTED IN THIS PAPER

| Device       | $J_{sc}$ [mA/cm <sup>2</sup> ] | $V_{oc}$ [mV] | FF [%] | Eff. [%] |
|--------------|--------------------------------|---------------|--------|----------|
| FE-SHJ [24]  | 38.9                           | 727           | 78.4   | 22.1*    |
| IBC-SHJ [14] | 39.9                           | 724           | 74.5   | 21.5**   |

\*certified by Fraunhofer ISE CaLab; \*\*in-house measurement.

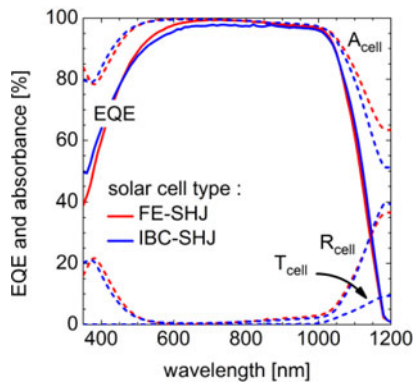


Fig. 4. EQE, reflection, transmission, and absorbance curves of the reference FE-SHJ and IBC-SHJ solar cells processed in our laboratory. Notice that the EQE curve for the FE-SHJ device does not account for the shadowing losses, as it is measured on a front electrode-free device, as explained in Section II-C.

fully metallized rear side (see Section II-A) so that no light is transmitted. In addition, the EQE curve of the FE-SHJ device does not account for the shadowing losses, as it is measured on a front electrode-free device, as explained in Section II-C.

As seen from Fig. 4, the EQE curves of the two solar cells are quite similar. Conversely, their absorbance curves mainly differ in the long-wavelength region: At 1200 nm, the IBC-SHJ device features 15%<sub>abs</sub> less absorbance than its FE-SHJ counterpart. This is related to long-wavelength light transmitted through the IBC-SHJ device.

Using the method outlined in Section II-C, we now calculate and compare the  $J_{sc}$  losses of both solar cells; the results are presented in Fig. 5. The total  $J_{sc}$  loss for the FE-SHJ solar cell amounts to 6.9 mA/cm<sup>2</sup>, compared with 5.9 mA/cm<sup>2</sup> for the IBC-SHJ solar cell, thus giving a 1.0-mA/cm<sup>2</sup> loss difference between the two structures. This is consistent with the  $J_{sc}$  difference experimentally measured on the two devices (see  $I$ - $V$  measurements; Table III).

Having a closer look at the  $J_{sc}$  loss breakdown in Fig. 5, it can be noticed that while most of the losses are common to the two structures (FE- and IBC-SHJ solar cells), some are architecture-specific. First of all, obviously, there is no front-electrode shadowing loss for the IBC-SHJ solar cell. This alone represents a potential gain of about 1.3 mA/cm<sup>2</sup> (equal to the amount of effective shadowing losses in the FE-SHJ device) for back-contacted devices, provided that these extra-generated carriers are efficiently collected. However, after the module encapsulation of two-side contacted solar cells, the effective shadowing losses are reduced by 50%, owing to the light recycling between

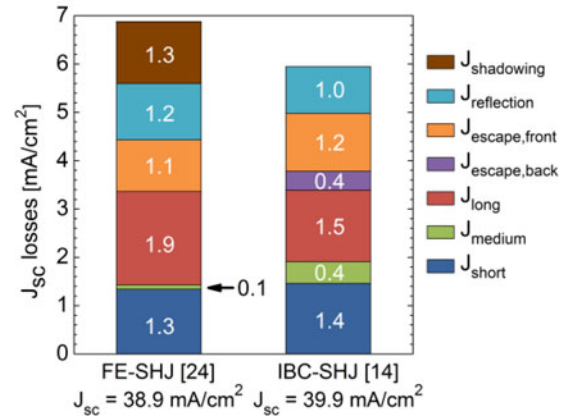


Fig. 5. Comparison of short-circuit current losses in the reference FE-SHJ and IBC-SHJ solar cells processed in our laboratory, calculated with respect to the available photocurrent  $J_{ph} = 45.9$  mA/cm<sup>2</sup>.

the metal grid and the front glass [46]. Moreover, several strategies have been proven to efficiently reduce the shadowing losses at solar cell level already, such as copper plating [6]–[8] or the SmartWire technology [47], to name a few. The final gain for back-contacted devices resulting from the suppression of the front shadowing losses is thus difficult to ascertain at module level.

In contrast with shadowing losses, light escaping at the back is a peculiar feature of the IBC-SHJ device. As seen in Fig. 4, this loss is caused by light escaping at the back of the IBC-SHJ solar cell through the gap between the fingers of the back electrodes. In contrast, this phenomenon is not present in the FE-SHJ solar cell featured in this paper. Indeed, as mentioned in Section II-A, its rear side is fully metallized, and thus, no light escapes at the back.<sup>1</sup> However, this does not mean that the FE-SHJ solar cell makes better use of this part of light: Indeed, an important amount of it is lost within the TCO/metal rear stack due to plasmonic absorption and, thus, contributes to long-wavelength parasitic absorption [3], [4], as further discussed below in this section. In the IBC-SHJ device presented here,  $J_{escape,back}$  amounts to 0.4 mA/cm<sup>2</sup> and represents 1% of the total  $J_{sc}$  of the solar cell. This value is consistent with what has been observed on other back-contacted structures, such as SunPower's A-300 solar cells [48].

Besides  $J_{shadowing}$  and  $J_{escape,back}$ , all the remaining  $J_{sc}$  loss terms are present in both device architectures. Front-side reflection losses are found to be rather similar in both device architectures. This is expected, as the two solar cells are both based on a single-layer ARC with comparable refractive indices, even though this ARC is a-SiN<sub>x</sub>:H in the case of the IBC-SHJ device, whereas it is an IO:H/ITO stack in the FE-SHJ device [49]. This is further supported by the very resembling reflection curves of the two solar cells in the short-wavelength region (see Fig. 4).

Short-wavelength losses are virtually identical for both solar cells, totaling about 1.4 mA/cm<sup>2</sup>. This is consistent, as both

<sup>1</sup>This situation would nevertheless be different in the case of bifacial SHJ solar cells [2]: Indeed, such devices would also feature light escaping at the rear side.

devices feature a-Si:H layers with similar thicknesses at the front. However, whereas the front a-Si:H layers of our champion FE-SHJ device presented here have already been purposely optimized to reach high  $J_{sc}$ , the front side of our IBC-SHJ solar cell under investigation had yet to be subject to any  $J_{sc}$  optimization. Importantly, this result underlines that our IBC-SHJ device could benefit from careful further optimization of its front side. This topic is developed in more detail in Section III-B.

Optical losses occurring in the medium part of the spectrum are rather small in both cases. They appear to be higher for the IBC-SHJ solar cell than for the FE-SHJ device: 0.4 versus 0.1 mA/cm<sup>2</sup>, respectively. This difference may be attributed to electrical shading losses, usually occurring above the electron-collecting regions in back-contacted devices [32]–[34]. It is well known that the narrower the electron-collecting stripes, the lower the electrical shading [50]. In this regard, redesigning the back side of our IBC-SHJ devices, with narrower electron-collecting regions, might help to mitigate such losses. However, achievable designs are ultimately limited by the practically feasible patterning techniques for the a-Si:H layers and the rear electrodes. In our case, it seems reasonable to consider 0.5-mm-wide electron-collecting stripes as a practical limit for our process flow. Alternatively, as the electrical shading is also dependent on the surface-passivation level of the electron-collecting regions [33], it can be reduced by enhancing the passivation quality in our IBC-SHJ devices. To which quantitative extent these two levers will allow mitigating  $J_{medium}$  still needs to be investigated.

Long-wavelength losses are found to be higher for the FE-SHJ solar cell than for the IBC-SHJ device, with 1.9 versus 1.5 mA/cm<sup>2</sup>, respectively. As detailed in [51] and [52], these long-wavelength losses mainly owe to the parasitic absorption in the rear TCO/metal electrode. The EQE of the two solar cells being virtually identical, the smaller  $J_{long}$  value of the IBC-SHJ solar cell mainly stems from its reduced absorbance at long wavelength.<sup>2</sup> As already discussed above, the reduced absorbance of the IBC-SHJ solar cell at long wavelength is due to the light being partly transmitted through the rear electrodes. In other words, it means that for the IBC-SHJ device,  $J_{long}$  is smaller because part of the long wavelength light is already anyhow lost due to transmission losses, these latter being accounted for in  $J_{escape,back}$ . Interestingly, the sum of  $J_{long}$  and  $J_{escape,back}$  for the IBC-SHJ device (1.5 and 0.4 mA/cm<sup>2</sup>, respectively; see Fig. 5) equates to  $J_{long}$  for the FE-SHJ solar cell, namely 1.9 mA/cm<sup>2</sup>. This highlights that the reduced  $J_{long}$  for the former device is compensated by an equivalent increase of  $J_{escape,back}$ . Noteworthy, part of this escape light could be recycled at module level, e.g., by using a white back sheet or paint [48].

For the sake of completeness, we also emphasize that quantitatively, the  $J_{sc}$  loss analysis done in this section is mainly representative for the specific case of our SHJ devices. Indeed, high- $J_{sc}$  two-side contacted SHJ devices such as the ones pro-

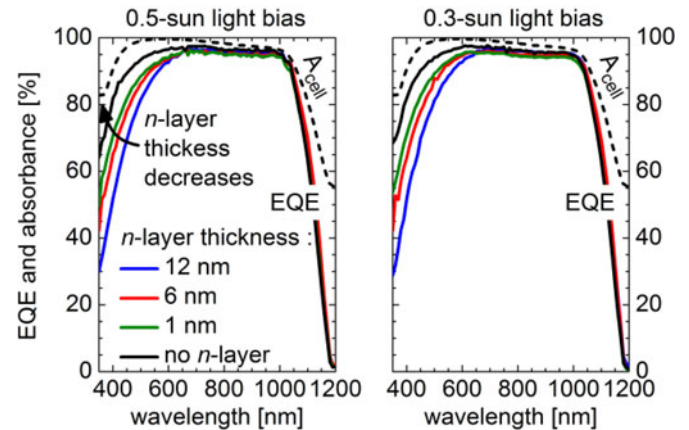


Fig. 6. EQE curves of IBC-SHJ devices with various thicknesses of n-type a-Si:H layer at the front (0, 1, 6, and 12 nm; see devices #1 to #4 in Table II), under a light bias of 0.5 sun (left) and 0.3 sun (right). We also reported the measured absorbance curve (identical for all the solar cells within this batch).

duced by Panasonic [2] or Kaneka [6] would surely feature a different  $J_{sc}$  loss breakdown. However, qualitatively, our methodology holds for every possible device and, thus, serves as a fair term of comparison to identify and mitigate the  $J_{sc}$  losses in our IBC-SHJ solar cells.

Overall, our  $J_{sc}$  loss analysis reveals that with the exception of escape light at the back (and to a lesser extent  $J_{medium}$  losses), our IBC-SHJ solar cells suffer from similar loss mechanisms as our two-side contacted FE-SHJ devices. As a consequence, most of the solutions already proposed to mitigate the  $J_{sc}$  losses on two-side contacted FE-SHJ solar cells also hold for back-contacted SHJ devices. An additional salient asset of the back-contacted architecture is that no carriers are collected at the front; this reduces significantly the constraints when optimizing the front side, as already discussed in Section I.

### B. Mitigation of Short-Circuit Current Losses at the Front of Interdigitated Back-Contacted Silicon Heterojunction Devices

Following the analysis presented in Section III-A, we started the mitigation of the  $J_{sc}$  losses in our IBC-SHJ devices tackling the parasitic absorption occurring at the front side. The left side of Fig. 6 shows the EQE curves of IBC-SHJ devices #1 to #4, with various n-type a-Si:H layer thicknesses at the front (see Table II), under a light bias of 0.5 sun. The thinner the n-type a-Si:H layer at the front, the higher the EQE at short wavelengths. This clearly results from reduced parasitic absorption in the thinner a-Si:H stack at the front.

It is well known that EQE data for both homojunction and heterojunction back-contacted devices can feature strong illumination dependences [11], [53], [54]. This is the case when the surface recombination velocity at the front side is highly sensitive to the (excess) carrier density. In our case, we did not notice any change on the EQE of our IBC-SHJ devices #1 to #4 down to a light bias of 0.3 sun, as illustrated on the right side of Fig. 6. Remarkably, the trend observed at a light bias of 0.5 sun is also conserved at lower light bias: the thinner the n-layer, the higher the EQE at short wavelength. This suggests that our

<sup>2</sup>Indeed,  $J_{long}$  is proportional to the area between the EQE and the absorbance curves (see its formula in Table V in the Appendix). Hence, in case of identical EQE curves, the lower the absorbance, the smaller  $J_{long}$ .



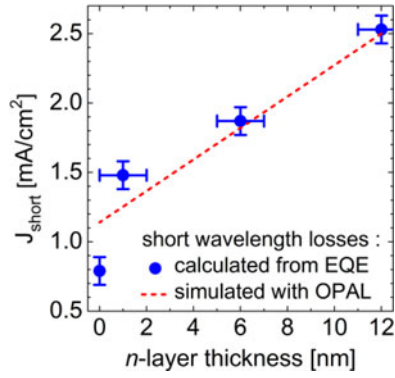


Fig. 7. Short-wavelength losses as a function of the front n-type a-Si:H layer thickness. As a comparison, we reported the values obtained with OPAL simulations.

TABLE IV  
OPTICAL LOSSES OF TWO IBC-SHJ SOLAR CELLS WITH DIFFERENT ARC SCHEMES ON THE FRONT SIDE

| IBC-SHJ device | ARC scheme                                       | $J_{\text{reflection}}$ [mA/cm <sup>2</sup> ] | $J_{\text{escape,front}}$ [mA/cm <sup>2</sup> ] |
|----------------|--|---|---|
| #2             | single-layer a-SiN <sub>x</sub> :H               | 1.0   | 1.2   |
| #5             | a-SiN <sub>x</sub> :H/a-SiO <sub>x</sub> :H DARC | 0.6   | 1.4   |

front-side passivation is relatively insensitive to the generated carrier density.

From the EQE curves on the left side of Fig. 6, we calculated the resulting  $J_{\text{short}}$  losses, as already detailed in Section II-C. The results are reported in Fig. 7.  $J_{\text{short}}$  is dramatically reduced when decreasing the front n-type a-Si:H layer thickness. For instance, replacing the 6-nm-thick n-type a-Si:H layer (featured at the front of the IBC-SHJ device on which we reported in [14]) with no n-layer at all, represents a current gain of  $\sim 1.0$  mA/cm<sup>2</sup>. These  $J_{\text{short}}$  values are consistent with those obtained using OPAL, especially for n-layers thicker than 6 nm. It thus suggests that for these thicknesses,  $J_{\text{short}}$  is completely dominated by parasitic absorption losses, and that recombination at the device front side plays a minor role. In contrast, we think that the discrepancies between the experimental and the simulated values of  $J_{\text{short}}$  for the smallest n-layer thicknesses are mainly due to the uncertainty in accurately measuring the optical properties and the thickness of a-Si:H layers thinner than  $\sim 2$  nm.

We now address the reflection losses at the front of our IBC-SHJ devices. Table IV gives the values of  $J_{\text{reflection}}$  and  $J_{\text{escape,front}}$  calculated for the IBC-SHJ solar cells #2 and #5, featuring either the standard single-layer a-SiN<sub>x</sub>:H ARC or the a-SiN<sub>x</sub>:H/a-SiO<sub>x</sub>:H DARC scheme.

$J_{\text{reflection}}$  is reduced by 0.4 mA/cm<sup>2</sup> when using the DARC scheme, owing to its overall reduced reflectance over the spectral range of interest. In contrast,  $J_{\text{escape,front}}$  results 0.2 mA/cm<sup>2</sup> higher than with the single-layer ARC. This again is due to the lower reflectance of the DARC scheme, especially in the long-wavelength spectral region. Indeed, as more light is coupled into the wafer, more light is reflected at the wafer rear side, and eventually,  $J_{\text{escape,front}}$  increases. In the end, the resulting net

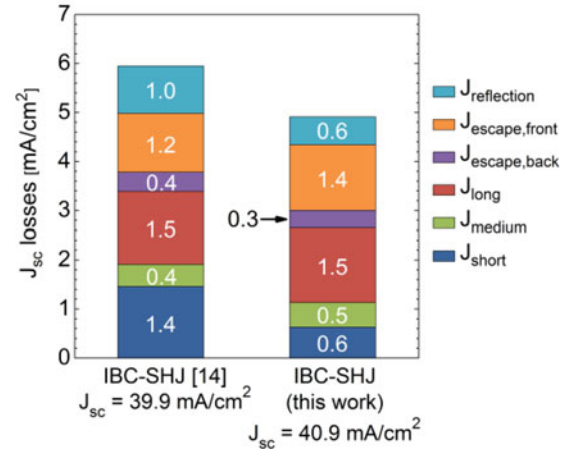


Fig. 8.  $J_{\text{sc}}$  loss breakdown for our previous best IBC-SHJ device (with  $J_{\text{sc}} = 39.9$  mA/cm<sup>2</sup>; see [14]) and our new  $J_{\text{sc}}$ -optimized device, featuring a  $J_{\text{sc}}$  of 40.9 mA/cm<sup>2</sup> (this publication).

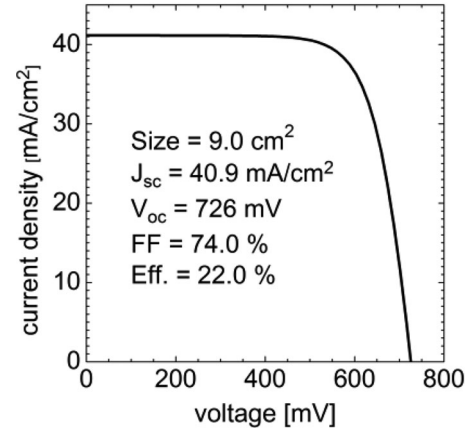


Fig. 9.  $I$ - $V$  characteristic of our new best IBC-SHJ solar cell (in-house measurement).

$J_{\text{sc}}$  gain when using the DARC scheme will, therefore, be close to 0.2 mA/cm<sup>2</sup>.

### C. High- $J_{\text{sc}}$ Interdigitated Back-Contacted Silicon Heterojunction Device

Taking benefit from the points discussed in Section III-B, we processed an IBC-SHJ device featuring a DARC but no n-type a-Si:H layer at the front (device #6; see Table II). Its  $J_{\text{sc}}$  loss breakdown is reported in Fig. 8 and is compared with our previous best IBC-SHJ device (already reported in Fig. 5).

As a result of the removal of the n-type a-Si:H layer at the front and the use of the DARC scheme,  $J_{\text{short}}$  and  $J_{\text{reflection}}$  are reduced by 0.8 and 0.4 mA/cm<sup>2</sup>, respectively. In contrast,  $J_{\text{escape,front}}$  losses are 0.2 mA/cm<sup>2</sup> higher in the high- $J_{\text{sc}}$  device. These values are in good agreement with the outcomes of Section III-B (see especially Fig. 7 and Table IV). All other losses remain virtually identical. Overall, the  $J_{\text{sc}}$  losses are, hence, reduced by 1.0 mA/cm<sup>2</sup> in this new device.

Fig. 9 plots the  $I$ - $V$  curve of our  $J_{\text{sc}}$ -optimized IBC-SHJ device #6. It features a  $J_{\text{sc}}$  of 40.9 mA/cm<sup>2</sup>, which is 1.0 mA/cm<sup>2</sup> higher than for our previous best device. This is in good

agreement with the values obtained from the  $J_{sc}$  loss analysis presented in Fig. 8. As can be seen, the  $J_{sc}$  gain was not obtained at the expenses of the other parameters, as this cell features an efficiency of 22.0%, with a  $V_{oc}$  of 726 mV and an FF of 74.0%. As already emphasized in [14], the transport losses at the two heterocontacts remain the major FF limitation in our IBC-SHJ devices.

These results indicate that the FSF passivation induced by the front n-type a-Si:H layer is not imperatively required for efficient IBC-SHJ devices. Indeed, we did not notice losses neither in FF nor in  $V_{oc}$  in our new best IBC-SHJ device without front n-type a-Si:H layer, compared with our previous best IBC-SHJ device with a front n-type a-Si:H layer (see [14]). The  $pFF$  stays  $\geq 81.0\%$  for all devices, but no particular trend is seen as a function of the n-layer thickness (data not shown). This latter result suggests that the recombination at the front side plays a minor role in the overall recombination losses in our IBC-SHJ devices [29].

Eventually, our findings are not in direct contradiction with earlier published results in which the presence of an FSF was indicated as a requirement 1) for efficient lateral transport of the photogenerated carriers and 2) for low surface recombination velocities [53], [55]. Both mentioned effects indeed depend on the passivation quality provided in absence of the front n-type a-Si:H layer, through the substrate injection level in case 1 and directly in case 2. In our case, the concomitant achievement of good  $J_{sc}$ ,  $V_{oc}$ , and FF values without front n-type a-Si:H layer owes to the fact that our intrinsic a-Si:H layer alone provides extremely high passivation over a wide injection range. However, as the n-type a-Si:H layer gets thinner, the a-SiN<sub>x</sub>:H layer deposited at the front side will also provide a field-effect passivation, induced by its positive fixed charges [56], [57]. To which extent this effect is competing with the decreasing field-effect passivation of the thinner n-type a-Si:H layer requires further investigation.

#### D. Further Short-Circuit Current Improvements

Our experimental results evidenced that short-wavelength losses at the front of back-contacted SHJ devices can be dramatically reduced by removing the front n-type a-Si:H layer without encountering  $V_{oc}$  losses, provided that state-of-the-art intrinsic a-Si:H passivating layers are used. An additional gain could thus be expected by further thinning the front intrinsic a-Si:H layer as well. However, it is known to be a tough challenge to maintain efficient passivation when the intrinsic a-Si:H layer thickness drops below  $\sim 4$  nm [5]. Such a thin layer would anyway still feature  $\sim 0.4$  mA/cm<sup>2</sup> of parasitic absorption. To further decrease the short-wavelength losses, it is thus required to seek for alternatives to the standard a-Si:H layer. Possible approaches include wide-bandgap materials such as a-SiO<sub>x</sub>:H [9], [58], indirect bandgap materials such as  $\mu$ c-Si:H [59] and perhaps the use of black silicon surfaces passivated by atomic-layer deposited aluminum oxide [60], [61]. Recently, Wan *et al.* [62] also demonstrated PECVD a-SiN<sub>x</sub>:H layers featuring parasitic absorption less than 0.1 mA/cm<sup>2</sup> and excellent surface passivation. This kind of layers could be a promising candidate

for the front side of back-contacted SHJ devices, as it also offers interesting ARC properties in addition to its low absorption and excellent surface passivation. Its compatibility to our IBC-SHJ devices process flow remains, however, to be investigated, e.g., regarding the deposition temperature. Importantly, as already discussed in Section I, the use of aluminum oxide or silicon nitride as front dielectric passivation layers and ARCs could also allow reaching high FF without the use of a diffused FSF [29].

Regarding reflection losses, we shown in Section III-B that replacing the single-layer ARC by a DARC reduces  $J_{reflection}$  by 0.4 mA/cm<sup>2</sup>. To further reduce  $J_{reflection}$ , multilayer coatings can be implemented [63]. However, it must be taken into account that each extra layer yields an incrementally smaller gain [64] and notably increases the process complexity. Moreover, after the encapsulation of the solar cell,  $J_{reflection}$  is already efficiently reduced without the need of a DARC, as the polymer foil and the front glass used in the module will play the role of the intermediate refractive index medium. Consequently, the use of multilayer ARCs might be reserved to devices measured under air (i.e., not encapsulated) and aiming at demonstrating high  $J_{sc}$  values, while the actual mitigation of  $J_{reflection}$  should rather take place at the module level.

Besides losses occurring at the front side of back-contacted SHJ devices, the road toward  $J_{sc}$  values  $> 41.0$  mA/cm<sup>2</sup> will require tackling the remaining  $J_{sc}$  loss sources. First on the list would thus be the long-wavelength losses. Indeed, in our 40.9 mA/cm<sup>2</sup> device, they now represent the major  $J_{sc}$  loss mechanism and account for 31% of the total losses, versus 25% in the case of our 39.9 mA/cm<sup>2</sup> solar cell. In this frame, it remains to be investigated if the mitigation solutions known for FE- and RE-SHJ devices, such as advanced rear reflectors [3], [51], [65] would also prove to be useful for back-contacted SHJ solar cells. The mitigation of long-wavelength losses will indeed involve the rear TCO that in our IBC-SHJ devices serves as contact for both heterocontacts. Therefore, specific constraints could differentiate the case of back-contacted SHJ devices from two-side contacted SHJ devices.

#### IV. CONCLUSION

In this paper, the optical losses of the IBC-SHJ devices fabricated in our laboratory were thoroughly examined and discussed. We found that our IBC-SHJ devices are in overall affected by  $J_{sc}$  loss mechanisms similar to those of two-side contacted SHJ solar cells, such as short-wavelength parasitic absorption in the front passivation layers, reflection losses, and long-wavelength losses in the rear electrodes.

We then provided practical guidelines to mitigate the reflection and parasitic absorption losses occurring at the front side of IBC-SHJ devices. We first demonstrated that removing the front n-type a-Si:H layer yields a dramatic  $J_{sc}$  gain without compromising the  $V_{oc}$  nor the FF of the device. Second, we showed that replacing the single-layer ARC by a DARC provides an additional  $J_{sc}$  gain.

As a result, we processed an IBC-SHJ device featuring a  $J_{sc}$  of 40.9 mA/cm<sup>2</sup>. This represents an improvement of 1.0 mA/cm<sup>2</sup> compared with our previous best  $J_{sc}$  result. Importantly, the



achievement of this high  $J_{sc}$  was not done detrimentally to the other device parameters, as this new best solar cell features a  $V_{oc}$  of 726 mV and an FF of 74.0%, yielding a final efficiency of 22.0%.

Finally, we discussed further possible  $J_{sc}$  improvements. We proposed that further reducing the short-wavelength losses requires to consider alternatives to the standard a-Si:H layers to passivate the front side of back-contacted SHJ devices. Here, we suggested that wide-bandgap materials appear as promising candidates. Further,  $J_{sc}$  optimization in back-contacted SHJ solar cells will have to address long-wavelength losses, as they represent by far the major loss mechanism once the short-wavelength losses are mitigated.

## APPENDIX

TABLE V

FORMULAS USED IN SECTION II-C TO CALCULATE THE SHORT-CIRCUIT CURRENT LOSSES OF IBC-SHJ DEVICES USING THEIR EQE, REFLECTANCE, TRANSMITTANCE, AND ABSORBANCE CURVES

| $J_{sc}$ loss sources formulas   |
|--|
| $J_{\text{reflection}} = \frac{q}{hc} \int_{350\text{nm}}^{1200\text{nm}} \lambda \cdot \Phi(\lambda) \cdot R_{\text{OPAL}}(\lambda) \cdot d\lambda$   |
| $J_{\text{escape, front}} = \frac{q}{hc} \int_{850\text{nm}}^{1200\text{nm}} \lambda \cdot \Phi(\lambda) \cdot [R_{\text{cell}}(\lambda) - R_{\text{OPAL}}(\lambda)] \cdot d\lambda$             |
| $J_{\text{escape, back}} = \frac{q}{hc} \int_{850\text{nm}}^{1200\text{nm}} \lambda \cdot \Phi(\lambda) \cdot T_{\text{cell}}(\lambda) \cdot d\lambda$   |
| $J_{\text{short}} = \frac{q}{hc} \int_{350\text{nm}}^{600\text{nm}} \lambda \cdot \Phi(\lambda) \cdot [1 - R_{\text{cell}}(\lambda) - T_{\text{cell}}(\lambda) - EQE(\lambda)] \cdot d\lambda$   |
| $J_{\text{medium}} = \frac{q}{hc} \int_{600\text{nm}}^{1000\text{nm}} \lambda \cdot \Phi(\lambda) \cdot [1 - R_{\text{cell}}(\lambda) - T_{\text{cell}}(\lambda) - EQE(\lambda)] \cdot d\lambda$ |
| $J_{\text{long}} = \frac{q}{hc} \int_{1000\text{nm}}^{1200\text{nm}} \lambda \cdot \Phi(\lambda) \cdot [1 - R_{\text{cell}}(\lambda) - T_{\text{cell}}(\lambda) - EQE(\lambda)] \cdot d\lambda$  |

$q$  is the elementary charge,  $h$  is Planck's constant,  $c$  is the speed of the light, and  $\Phi(\lambda)$  is the AM1.5G solar spectrum (all other symbols are defined in the text).

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