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# Combined model-free data-interpretation methodologies for damage detection during continuous monitoring of structures

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## 2 Abstract

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4 Despite the recent advances in sensor technologies and data acquisition systems, interpreting 5 measurement data for structural monitoring remains as challenge. Furthermore, due to the 6 complexity of the structures, materials used and uncertain environments, behavioral models are 7 difficult to build accurately. This paper presents novel model-free data-interpretation methodologies 8 that combine MPCA with each of four regression-analysis methods – Robust Regression Analysis 9 (RRA), Multiple Linear Analysis (MLR), Support Vector Regression (SVR) and Random Forest (RF) – for 10 damage detection during continuous monitoring of structures. The principal goal is to exploit the advantages of both MPCA and regression-analysis methods. The applicability of these combined 11 12 methods is evaluated and compared with individual applications of MPCA, RRA, MLR, SVR and RF 13 through four case studies. Result showed that the combined methods outperformed non-combined methods in terms of damage detectability and time to detection. 14

Keywords: Model free, data interpretation, regression analysis, robust regression analysis, support
 vector regression, random forest, damage detectability, time to detection

## 17 **1** Introduction

18 The performance of civil engineering structures under operational and environmental actions may 19 decrease over time due to factors such as deterioration of structural materials, extreme and other 20 actions that were not adequately taken into account during design. In the USA, it has been estimated 21 that more than two trillion dollars are needed to bring America's infrastructure up to an acceptable 22 performance level. Current infrastructure budgets are only a fraction of this amount and future 23 deficit reduction plans will widen the gap (ASCE 2009). Structural Health Monitoring (SHM) has the 24 potential to save money through early detection and this may lead to cheaper repairs and 25 replacement avoidance. SHM is a process aimed at providing accurate and real-time information 26 concerning structural condition and performance (Glisic and Inaudi 2008). It consists of periodic or 27 continuous monitoring that measures quantities such as structural responses and environmental 28 variations for the evaluation of structural performance.

29 Recent advances in sensor technologies and data acquisition systems allow complex structures to be 30 equipped with hundreds of sensors that measure quantities such as structural responses 31 (acceleration, deformation rotation etc) and environmental variations (temperature, humidity, wind, 32 etc.). Despite the continuous evolution and development of measurement technologies, interpreting 33 a large amount of measurement data to obtain useful information on structural conditions remains a 34 challenge. This task falls into the field of Structural Identification (St-Id) which is an application of System Identification (Sys-Id) to civil structural systems. The Sys-Id concept (originated in electrical 35 36 engineering) was first studied in engineering mechanics by Hart and Yao (1977) and in structural 37 engineering by Liu and Yao (1978).

38 Classifying according to the presence or absence of physics-based behavioral models, there are generally two types of data interpretation methods: model-based and model-free methods. 39 Strengths and weaknesses of both types have been summarized in the ASCE State-of-the-art Report 40 on Structural Identification of Constructed Systems (ASCE 2011). Both types are complementary since 41 42 they are appropriate in different contexts. Model-based data interpretation methods are typically 43 performed through comparing predictions of behavior models with measured structural responses 44 (Okasha et al. 2012; Koh and Thanh 2010; Ren and Chen 2010; Reynders et al. 2010; Koh and Thanh 45 2009; Strauss et al. 2008). Behavior models are used to support decisions related to long-term 46 structural management such as estimation of reserve capacity and repair. However, behavior models 47 are expensive to build and identifying a unique model is difficult due to the intrinsic ambiguity of 48 inverse tasks as well as uncertainties. Furthermore many model predictions might approximately 49 match observations and due to compensating and systematic errors, the best matching model may 50 not be the correct model (Goulet et al. 2010; Robert-Nicoud et al. 2005; Saitta et al. 2005; Raphael 51 and Smith 1998).

52 Model-free data-interpretation methods involve analyzing measurement time series only; they do 53 not require geometrical and material information of a structure. These methods are well-suited for analyzing measurements during continuous monitoring of structures since they involve only tracking 54 55 changes in time-series signals. Omenzetter et al. (2004), Hou et al (2000), Moyo and Brownjohn 56 (2002) used wavelet-based methods for damage detection. Omenzetter and Brownjohn (2006) 57 proposed an autoregressive integrated moving average method (ARIMA) to detect damage from measurements. Lanata and Grosso (2006) applied a proper orthogonal decomposition method for 58 59 continuous static monitoring of structures. Yan et al. (2005a; 2005b) proposed a local PCA-based damage-detection method for vibration-based SHM. All these studies are limited to a single 60 methodology without comparison to other methods. Gul and Catbas (2011) employed Auto-61

Regressive models with eXogenous input (ARX) for different sensor clusters by using the freeresponse of a structure to assess damage.

64 Posenato et al. (2010; 2008) proposed two methods, MPCA and RRA for damage detection during 65 continuous structural monitoring and performed a comparative study of these methods with several 66 other model-free data-interpretation methods (Wavelet packet transform, Discrete wavelet transform, ARIMA, Box-Jenkins, Instance based method, Short Term Fourier Transform and 67 68 correlation anomaly scores analysis) . Results demonstrated that the performances of MPCA and RRA 69 for damage detection were superior to other methods when dealing with civil-engineering challenges 70 such as significant noise, missing data and outliers. Both methods were observed to require low 71 computational resources to detect anomalies, even when there were large quantities of data.

72 Many studies have shown that structural responses due to temperature variation have a significant 73 effect on the overall system reliability. For example, the magnitude of thermal stresses was found to 74 be comparable to live and dead load stresses (Peng and Qiang 2007). Catbas and Aktan (2002) 75 observed that the magnitude of strains due to daily temperature variations far exceed those due to 76 traffic. Bell et al. (2008) found that temperature effects mask the load applied to Rollins Road Bridge 77 over the duration of load test. Brownjohn et al (2009) studied the thermal effects on performance on 78 the Tamar suspension bridge and showed that thermal effects dominate the bridge behavior. The 79 task of data interpretation is even more difficult in such situations. Laory et al. (2011) evaluated the 80 performance of MPCA and RRA under traffic and temperature variations. The study showed that 81 although MPCA is better than RRA in terms of damage detectability, RRA is better than MPCA in 82 terms of time to detection. Hence, both methods were considered to be complementary and it was 83 noted that synergies between both methods may result in a better overall methodology for damage 84 detection.

Building on these previous studies, this paper presents a new methodology that combines MPCA and
 regression-analysis methods - Robust Regression Analysis (RRA), Multiple Linear Analysis (MLR),

Support Vector Regression (SVR) and Random Forest (RF) - for damage detection during continuous monitoring of structures. Applications of SVR in the field Structural Health Monitoring have provided good results (Zhang et al. 2012; Ni et al. 2005; Loutas et al.). In addition, RF has been successfully employed for classification, prediction, studying variable importance, variable selection, and outlier detection (Rodriguez-Galiano et al. 2012; Verikas et al. 2011; Breiman 2001).

In this paper, the objective of combining MPCA with such regression analyses is to exploit the advantages of individual methods through appropriate combinations. The performance of the combined methods are evaluated and compared with single applications of MPCA, RRA, MLR, SVR and RF through four case studies. Comparison criteria are damage detectability, time to detection and performance in the presence of non-linear behavior. The next section includes description of several methodologies for damage detection. Four combined methods are also presented. This is followed by a section that evaluates effectiveness on four case studies.

## 99 2 Model-free data-interpretation methodologies for damage detection

## 100 2.1 Moving Principal Component Analysis (MPCA)

Moving Principal Component Analysis (MPCA) was first proposed for interpreting measurements from continuous monitoring for damage detection by Posenato et al. (2008). MPCA essentially applies Principal Component Analysis (PCA) (Hubert et al. 2005) to enhance the discrimination between features of undamaged and damaged state. In order to reduce computational time, PCA is applied to a sliding fixed-sized window of measurements instead of the whole dataset.

106 MPCA is carried out by first constructing a matrix that contains the history of all measured 107 parameters. The second step is to iteratively extract datasets corresponding to a sliding window. The 108 principal components are then computed by solving the eigenvalue problem of the covariance matrix 109 of the extracted datasets. The components are arranged in order of significance by sorting the 110 eigenvectors by eigenvalues in decreasing order. MPCA is conducted by analyzing only the eigenvectors that are related to the first few eigenvalues. When damage occurs, mean values and
components of the covariance matrix change and as consequence, so do values of eigenvalues and
eigenvectors.

A key issue is selecting the dimension of the moving window. It is necessary to select a value that is sufficiently large to minimize the influence of variations in measurements due to changes that are not related to damage (environmental effects, noise, etc.). If the time series has a periodic behavior, the choice of the window size should be at least as long as the longest period. This ensures the stationary behavior of the mean values over time and that eigenvalues of the covariance matrix do not have periodic behavior.

## 120 2.2 Robust Regression Analysis (RRA)

The application of RRA for damage detection in continuous monitoring is based on the distance of measurement points to computed regressions lines estimated during the undamaged state. The analysis is carried out by pairing sensors that are highly correlated and then focusing on these couples to detect anomalies. These sensor pairs are identified by computing correlation coefficients between measurement data and comparing them with a pre-defined correlation coefficient threshold. All sensor pairs having a correlation coefficient greater than the threshold are selected in order to formulate the robust regression model. The linear relation between  $y_i$  and  $y_j$  is written as

128 
$$y'_{j} = \beta_{0} + \beta_{1} y_{i}$$
 (1)

129 where  $\beta_0$  and  $\beta_1$  are the coefficients of the robust regression line estimated from measurements 130 using iteratively reweighted least squares.  $y'_j$  represents the value of  $y_j$  computed according to the 131 linear relation. The robust regression analysis is carried out by observing the regression residuals 132 (discrepancies between the measurements  $y_j$  and the prediction by linear regression-line  $y'_j$ ). 133 Damage is identified when the value exceeds a confidence interval that is defined using standard deviation of the difference in the undamaged state. The advantage of RRA is that it is insensitive to
outliers and missing data. It is thus suitable for civil engineering applications since all measurements
of civil-engineering structures contain outliers and most have missing data (Posenato et al. 2010).

137 2.3 Multiple Linear Regression (MLR)

The aim of multiple linear regression is to evaluate the relationship between several independent (predictor) variables and a dependent (criterion) variable by fitting a linear equation to observed data. Given *n* observations, the multiple linear regression is formulated as

141 
$$y(x) = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \dots + \beta_p x_p$$
 for  $i = 1, 2, \dots n$  (2)

142 where  $\beta$  is a regression coefficient associated with the  $i^{th}$  input variable  $(x_i, i=1,...,n)$ . Using the 143 dataset of observations in measurement time series, the unknown coefficients are determined 144 using the least squares method. In the application for damage detection, similar to robust regression, 145 detection is based on the regression residual.

## 146 2.4 Support Vector Regression (SVR)

147 Support vector machines is a new class of learning algorithms that are derived from statistical 148 learning theory (Vapnik and Lerner 1963). These algorithms can be used for regression analysis and 149 thus known as Support Vector Regression (SVR). SVR builds a linear regression function in a high 150 dimensional new space (i.e. feature space in machine learning) where the input data in the original 151 space is mapped using a transformation function. A distinctive characteristic of SVR is that instead of 152 minimizing the observed training error such as MLR, SVR conducts the minimization of the generalization error bound in order to obtain generalized performance. The generalization error 153 154 bound is the combination of the training error and a regularization term that controls the complexity 155 of the prediction functions. The linear regression function in the new space is given by

156 
$$y(x) = w^T \varphi(x) + b$$
(3)

where input values  $x \in \mathbb{R}^n$  and output (or response) values  $y \in \mathbb{R}$ ; w is a weight vector; b is a constant and  $\varphi(x)$  is a transformation function that maps the input vector x into the high dimensional space. Given a training set  $\{x_i, y_i\}$  (i = 1, ..., N), a regression function is formulated by minimizing the following objective function (Suykens et al. 2002)

$$\min_{w,b,e} J(w,e) = \frac{1}{2} w^T w + \frac{1}{2} \gamma \sum_{i=1}^N e_i^2$$
subject to  $y_i = w^T \varphi(x_i) + b + e_i, \quad i = 1,...,N.$ 
(4)

161

where  $e_i$  is the error and  $\gamma$  is the regularization parameter that determine the trade-off between the training error minimization and the complexity of the function. The optimization task is solved by constructing the Lagrangian function

165 
$$L(w,b,e,\alpha) = J(w,e) - \sum_{i=1}^{N} \alpha_i \left\{ w^T \varphi(x_i) + b + e_i - y_i \right\}$$
 (5)

166 where  $\alpha_i$  are Lagrange multipliers.

A kernel function is employed to compute inner-products in the new space using only the original input data. The advantage of using kernels for inner products is that if a kernel function is known, it is not necessary to define the explicit form of the transformation function  $\varphi(x)$  as well as the new space. The selection of the kernel function generally depends on the application domain. It has been shown that Gaussian radial-basis function (RBF) is a reasonable first choice of kernel functions since it has only a single parameter (standard deviation,  $\sigma$ ) to be determined (Saitta et al. 2010). The Gaussian RBF is expressed as

174 
$$K(x_i, x_j) = e^{-\|x_i - x_j\|^2/2\sigma^2}$$
 (6)

175 When using the RBF kernel function, only two tuning parameters,  $\gamma$  and  $\sigma$ , need to be determined 176 to formulate a prediction function and their optimal values could be determined using grid search 177 method.

#### 178 2.5 Random Forest (RF)

179 Random forest is a nonparametric statistical regression method that offers an alternative to 180 parametric regression methods (Breiman 2001). The prediction is achieved by constructing an 181 ensemble of regression trees. Given a training dataset  $L = (x_{ij}, y_i)$  where i = 1, ..., N is the number 182 of observations and j = 1, ..., p is the number of input variables.

The first step is to generate *B* training sub-datasets by continuously copying observations randomly from the original training dataset *L* until each sub-dataset  $L_b$  (b = 1, ..., B) has the same number of observations as the original training dataset. Thus, some of the observations from the original dataset can be repeatedly copied into each sub-dataset, while others are not copied at all. The set of non-copied observations corresponding to each sub-dataset functions as a validation dataset.

The second step involves building *B* regression trees using the generated *B* training sub-datasets. A regression tree  $T_b$  is built by recursively splitting each sub-dataset into more and more homogeneous groups. From the decision-tree point of view, the entire training sub-dataset is represented by a *root* node and the splitting groups are represented by nodes, as shown in Figure 1.

When *B* regression trees are built from *B* sub-datasets, an ensemble of these trees is called a random forest. For each individual tree, the prediction of the response for a new observation x is determined by following the path from the root node down the appropriate terminal node and the prediction value is the average response in that terminal node. Finally, the overall prediction of the forest for a new observation is the average of prediction values from individual trees.

# 197 **3 Combined methodologies**

198 The methodologies presented in the previous section have advantages and limitations for data 199 interpretation in the field of Structural Health Monitoring (SHM). The objectives of combining 200 methodologies are to exploit the advantages of such methodologies and overcome limitations 201 associated to each of them through an appropriate combination. For example, MPCA and RRA are 202 found to be complementary methods for damage detection of continuously monitored structures 203 under environmental variations since they are most appropriate in different situations. While MPCA 204 is better than RRA in terms of damage detectability, RRA detects damage faster than MPCA. Hence, 205 the combination of these methods is able to improve the detection performance in terms of damage 206 detectability and time to detection.

207 This study proposes methodologies that combine MPCA with the previously presented four 208 regression analysis methods: RRA, MLR, SVR and RF, for damage detection during continuous 209 monitoring. Figure 2 shows the layout of the combined methodologies that is composed of two main 210 steps. The first step is to transform measurement data into main eigenvector time series (main 211 principal components) using MPCA. As mentioned in Section 2.1, MPCA is carried out by using a 212 fixed-size window that moves along the measurement time series to extract specified datasets. The 213 data within the window are used to compute a covariance matrix and then solve the eigenvalue 214 problem of the covariance matrix to obtain the eigenvector time series.

The second step involves analyzing the correlations between eigenvector time series to detect damage in structures. The idea behind this step is built on an assumption that when damage occurs in structures, the correlations between the principal components will be changed. Thus, damage can be detected by tracking changes in these correlations over time. This step explores the correlations between PCs by developing regression functions using RRA, MLR, SVR and RF. For long-term monitoring of structures, the regression functions are then used to predict an eigenvector corresponding to a measurement location based on the known eigenvectors of other locations. If the

222 difference between the predicted eigenvector obtained from regression functions and the known values (regression residual) exceeds a defined threshold bound, then damage is detected. The 223 224 distinctive feature of these combined methods from the application of each individual regression 225 analysis method for damage detection is that instead of tracking directly the correlations between 226 measurement time series, the combined methods analyze the correlations between eigenvector time 227 series. Therefore, it is capable of taking full advantages of high damage detectability from MPCA and 228 small time to detection from regression analysis methods. The performance of such methods is 229 demonstrated in the following case studies.

230 **4** Case studies

### 231 4.1 Numerical studies

#### 232 4.1.1 A railway truss bridge

233 A railway truss bridge in Zangenberg, Germany has been selected for a case study. The bridge is composed of two parallel trusses each having 77 members. A numerical model inspired by this bridge 234 235 is used to provide responses (strain) under traffic loading and temperature variations. These 236 responses are taken as measurement data from continuous monitoring. Only one truss of the bridge is modeled (Figure 3). Truss members are made of steel having an elastic modulus of 200 GPa and a 237 density of 7870 kg/m<sup>3</sup>. Their properties are summarized in Table 1. Supports of the truss are 238 239 restrained in vertical and horizontal directions. Although this is not the boundary conditions that 240 were designed for this bridge, these supports represent an upper-bound worst case when the 241 supports have deteriorated with age. Traffic loading is simulated by applying a randomly generated 242 vertical load (0-19 tonnes) at each node in the bottom chords. A load of 19 tonnes is equivalent to an 243 axle load of a railway locomotive. Daily and seasonal temperature variations are simulated as 244 thermal loads. Temperature differences between top and bottom chords due to solar radiation are 245 also taken into account in the simulations. In this example, damage is represented by a loss of 246 member axial stiffness. Damage scenarios are used to evaluate the damage detectability and time to 247 detection for all methods. In this study, damage detectability is represented by the minimum 248 detectable damage level that is the smallest percentage loss of axial stiffness in a member that can249 be detected.

250 Data-interpretation methods ,includes single applications and combined method are employed for 251 damage detection. Four years of undamaged data is simulated and treated as training period. A 252 window size of a year is chosen for MPCA. Figure 4 shows the minimum detectable damage-level 253 using 9 model-free data-interpretation methods, including the applications of single individual 254 method as well as combined methods. The figure demonstrates that combined methods are better in 255 terms of damage detectability than individual methods. As expected, MPCA is better than RRA in 256 terms of damage detectability. MPCA also shows a superior performance in comparison to other 257 individual methods. Generally, while RRA performs the least, combined MPCA-RRA shows the best 258 performance and it is able to detect a damage of 3% stiffness loss. Such small damage can be caused 259 by many sources such as cracks and localized corrosion.

260 To evaluate performance in terms of time to detection, a damage scenario of 50% loss of axial 261 stiffness in a member is chosen. Figure 5 shows the time to detection for all methods. In comparison 262 to other methods, MPCA requires the longest time to detect damage. Another expected observation, 263 RRA shows a better performance than MPCA, that is RRA can detect damage earlier than MPCA. 264 However, it is seen that other regression analysis methods such as MLR, SVR and RF, are able to 265 detect damage instantly. For the combined methods, the combination of MPCA with regression 266 analysis methods performs better than the use of MPCA alone. Figure 5 also shows that although 267 both RRA and MLR are based on linear regression analysis, MPCA-RRA can detect damage earlier 268 than MPCA-MLR. Indeed, MPCA-RRA detects damage instantly while MPCA-MLR takes about 20 269 days. A plausible reason is that while RRA only performs analysis on high correlated measurement 270 pairs, MLR analyzes all measurements regardless of the correlations within measurement data.

These results show that not all combinations lead to better performance in damage detection. For this case study, the combination of MPCA and RRA outperforms other methods in terms of damage

detectability and it is as good as the individual application of MLR, SVR and RF in terms of time todetection.

#### 275 4.1.2 A concrete frame

276 This case study takes structural responses from a numerical model of a concrete frame (Figure 6) as 277 measurement data. This case study revisits numerical simulation data that was performed by 278 Cavadas (2011). The model was used for evaluation of damage detection approach using influence 279 lines of moving loads. It is a simply supported concrete frame with Young's modulus of 15 GPa. Four 280 responses – vertical displacement at mid-span, horizontal displacement at roller support, rotation 281 over the left support bearing and rotation over the right support bearing – are measured for damage 282 detection. Taking into account sensor accuracy of available sensors with + 0.01 mm for displacements and  $\pm$  1°x10<sup>-3</sup> for rotations, a uniform distributed noise is added to measurement data. 283 284 Damage is introduced as stiffness reduction along 30 cm of the beam element (Figure 6).

For this case study, 500 influence lines are used as a training period and the window size for MPCA is defined as 200 influence lines. Figure 7 shows the minimum detectable damage-level of individual and combined methods. Indeed, the combined methods are able to detect lower damage level than the minimum detectable damage-level when using single methods. Thus, it is concluded that the combination of MPCA with regression analysis methods results in a better methodology in terms of damage detectability. As shown in Figure 8, the best performance is achieved when MPCA is combined with SVR.

For time to detection, a damage scenario of 35% stiffness reduction is used. Times to detections of all methods are shown in Figure 8. For this scenario, all combined methods are able to detect damage instantly. Therefore, it is concluded that for this case study, combining MPCA with regression analysis improves the performance in terms of time to detection.

296 While the previous case study shows that combination of MPCA and RRA (MPCA-RRA) performs best 297 in terms of damage detectability, this case study demonstrates that MPCA-SVR outperforms other

298 methods. These results indicate that the selection of regression analysis to be combined with MPCA 299 is case-dependent. A reason for this is that since combined methods conduct damage detection 300 based on the correlation of eigenvector time histories, detection is dependent on the characteristics 301 of these time series.

302 Figure 9 shows the plots of the relationship of two eigenvector time series for both case studies 303 above. For the first case study (Figure 9 left), the relationship between eigenvector components of 304 sensor 13 and 14 is shown to be linear and thus linear regression is well-suited to analyze such 305 relationship. On the other hand, for the second case study (Figure 9 right), the relationship between 306 eigenvector components of sensors 1 and 3 is shown to be non-linear. Therefore the combination of 307 MPCA with non-linear regression is more appropriate for the second case study. Results from both 308 case studies of damage detectability demonstrate that the most appropriate regression-analysis 309 methods to be combined with MPCA are those that are compatible with eigenvector-correlation 310 characteristics.

# 311 4.2 A full-scale test on the Ricciolo viaduct

312 The applicability of the combined methods for damage detection under environmental variations is 313 also assessed in this paper using measurements from a full-scale test on the Ricciolo viaduct that was 314 conducted by Posenato et al. (2010). The Ricciolo viaduct was built in 2004 - 2005 at the Lugano 315 North exit of Swiss motorway A2. This bridge was continuously monitored at a rate of one 316 measurement session per hour. The monitoring system includes parallel and crossed sensor 317 topologies and inclinometers in order to monitor axial strain, horizontal and vertical curvature 318 changes, torsion, average shear strain and rotations in both vertical plans. The configuration of the 319 measurement system is given in Figure 10 and Figure 11.

320 During the first four and a half months of the monitoring period, the bridge was under construction.

321 Several important stages in the construction process are listed in Table 2.

During the monitoring period, the bridge is in a good condition and there are no damage events that could generate anomalous behavior. Therefore, the time scale of the monitoring data is inverted so that events during the construction period appear as anomalous events. Previously, Posenato et al. (2010) demonstrated the successful application of MPCA and RRA in detecting construction stages. Following this study, this section compares the performance of MPCA and RRA with the combined methods in terms of detectability and time to detection.

As mentioned in Section 2.1, MPCA is carried out by observing the eigenvector time histories. For this method, a window size of four months is used for data analysis. Figure 12 presents the resulting eigenvector time histories and shows that detection is visible. One notable observation from this figure is that the eigenvector time histories are highly correlated before event 6 occurs and this correlation is suddenly changed when the anomalous event occurs. This is a good example that verifies the data interpretation methods proposed in this study where detection is based on the correlation of the eigenvectors (main principal components).

Figure 13 presents an eigenvector time history through-out the monitoring period. Confidence interval  $(\pm 6\sigma)$  is used as detection criteria and an anomalous event is detected when the eigenvector falls out of the confidence interval. It is seen that the event is successfully detected using MPCA. However, it requires a period of 11 days to detect this event.

Figure 14 presents the comparison of RRA and MPCA-RRA. Both methods detect damage based on the linear correlation. However, the difference is that RRA analyzes the correlations between measurement data while MPCA-RRA analyzes the correlations between the eigenvectors (main principal component) time histories. Figure 14 shows that these two methods are better than MPCA in terms of time to detection. They are able to detect anomalous event almost instantaneously.

In addition, there is a remarkable observation in Figure 14. Although the magnitude of the changes in the regression residuals due to Event 6 is almost the same, there is a significant difference in the amount of scatter. The threshold size within the reference period for MPCA-RRA is thus much smaller than that of RRA. Unlike abrupt structural changes due to construction stages, in most cases, structural degradation occurs gradually starting from small damage. Thus, the figure implies that it will be more difficult for RRA to detect a change that is smaller than the change of Event 6 due to the size of the threshold. Obviously, this is not the case for MPCA-RRA since the size of the threshold is so small that detection is possible for relatively small changes. This shows that MPCA-RRA has the potential for higher damage detectability than RRA alone.

353 Similar to MPCA-RRA, the combination of MPCA with other regression analysis are able to detect 354 Event 6 instantaneously. Thus, it can be concluded that combined methodologies are better than 355 each individual method in terms of damage detectability and time to detection.

356 **5** Conclusions

357 Results of four case studies lead to the following conclusions:

The combination of Moving Principal Component Analysis (MPCA) and regression-analysis
 methods, including Robust Regression Analysis (RRA), Multiple Linear Analysis (MLR), Support
 Vector Regression (SVR) and Random Forest (RF) performs better than each individual method
 in terms of damage detectability and time to detection.

For the combined data-interpretation methods, the most appropriate regression analyses are
 those that are compatible with eigenvector-correlation characteristics. For example, RRA and
 MLR are appropriate when eigenvector correlations are linear while SVR and RF are appropriate
 when eigenvector correlations are non-linear.

Correlation-based methods are useful tools for damage detection of civil engineering structures.
 These methods are notably suitable for continuous monitoring of structures where there are
 large quantities of measurement data that are influenced by traffic load and environmental
 parameters such as temperature.

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## 374 **References**

- ASCE. (2009). "Report card for America's infrastructure." American Society of Civil Engineers.
- ASCE. (2011). "Structural Identification (St-Id) of Constructed Facilities : Approaches, Methods and
   Technologies for Effective Practice of St-Id." A State-of-the-Art Report by ASCE SEI
   Committee on Structural Identification of Constructed Systems.
- Bell, E. S., Sipple, J., and Yost, J. (2008). "Long-Term Thermal Performance of a CFRP-Reinforced
   Bridge Deck." Vancouver, BC, Canada, 242-242.
- 381 Breiman, L. (2001). "Random Forests." *Machine Learning*, 45(1), 5-32.
- Brownjohn, J. M. (2009). "Thermal effects on performance on Tamar Bridge." *4th International Conference on Structural Health Monitoring of Intelligent Infrastructure (SHMII-4)*, Zurich,
   Swirzerland.
- Catbas, F. N., and Aktan, A. E. (2002). "Condition and Damage Assessment: Issues and Some Promising Indices." *Journal of Structural Engineering*, 128(8), 1026-1036.
- Cavadas, F. (2011). "Structural Health Monitoring Applied to the Life-Cycle Management of Bridges Approaches for Damage Identification," Research Thesis Project, Universidade do Porto.
- Glisic, B., and Inaudi, D. (2008). *Fibre Optic Methods for Structural Health Monitoring*, John Wiles &
  Sons.
- Goulet, J.-A., Kripakaran, P., and Smith, I. F. C. (2010). "Multimodel Structural Performance
   Monitoring." *Journal of Structural Engineering*, 136(10), 1309-1318.
- Gul, M., and Catbas, F. N. (2011). "Structural health monitoring and damage assessment using a
   novel time series analysis methodology with sensor clustering." *Journal of Sound and Vibration*, 330(6), 1196-1210.
- Hart, G. C., and Yao, J. T. P. (1977). "System Identification in structural dynamics." *Journal of Engineering Mechanics, Division ASCE*, 103(EM6), 1089-1104.
- Hou, Z., Noori, M., and Amand, R. S. (2000). "Wavelet-based approach for structural damage detection." *Journal of Engineering Mechanics*, 126(7), 677-683.
- Hubert, M., Rousseeuw, P. J., and Branden, K. V. (2005). "ROBPCA: A new approach to robust
   principal component analysis." *Technometrics*, 47, 64-79.
- Koh, C. G., and Thanh, T. N. (2009). "Challenges and Strategies in Using Genetic Algorithms for
   Structural Identification." Soft Computing in Civil and Structural Engineering, B. H. V. Topping
   and Y. Tsompanakis, eds., Saxe-Coburg Publications, Stirlingshire, UK, 203-226.
- Koh, C. G., and Thanh, T. N. (2010). "Output-only Substructural Identification for Local Damage
   Detection." *The Fifth International Conference on Bridge Maintenance, Safety and Management*, Philadelphia, Pennsylvania, USA.

- Lanata, F., and Grosso, A. D. (2006). "Damage detection and localization for continuous static
   monitoring of structures using a proper orthogonal decomposition of signals." *Smart Materials and Structures*, 15(6), 1811-1829.
- Laory, I., Trinh, T. N., and Smith, I. F. C. (2011). "Evaluating two model-free data interpretation
  methods for measurements that are influenced by temperature." *Advanced Engineering Informatics*, 25(3), 495-506.
- Liu, S. C., and Yao, J. T. P. (1978). "Structural identification concept." *Journal Structural Division,ASCE*, 104(12), 1845-1858.
- Loutas, T. H., Panopoulou, A., Roulias, D., and Kostopoulos, V. "Intelligent health monitoring of
  aerospace composite structures based on dynamic strain measurements." *Expert Systems*with Applications(0).
- Moyo, P., and Brownjohn, J. M. W. (2002). "Detection of Anomalous Structural Behaviour Using
   Wavelet Analysis." *Mechanical Systems and Signal Processing*, 16(2-3), 429-445.
- Ni, Y. Q., Hua, X. G., Fan, K. Q., and Ko, J. M. (2005). "Correlating modal properties with temperature
   using long-term monitoring data and support vector machine technique." *Engineering Structures*, 27(12), 1762-1773.
- 424 Okasha, N. M., Frangopol, D. M., and Orcesi, A. D. (2012). "Automated finite element updating using
  425 strain data for the lifetime reliability assessment of bridges." *Reliability Engineering & amp;*426 *System Safety*, 99(0), 139-150.
- Omenzetter, P., Brownjohn, J. M. W., and Moyo, P. (2004). "Identification of unusual events in multi channel bridge monitoring data." *Mechanical Systems and Signal Processing*, 18(2), 409-430.
- Omenzetter, P., and Brownjohn, J. M. W. (2006). "Application of time series analysis for bridge
   monitoring." *Smart Materials and Structures*, 15(1), 129-138.
- Peng, Y., and Qiang, S. (2007). "Analytical Solution to Temperature Variations in Highway Concrete
  Bridges Due to Solar Radiation." Chengdu, China, 252-252.
- Posenato, D., Lanata, F., Inaudi, D., and Smith, I. F. C. (2008). "Model-free data interpretation for
  continuous monitoring of complex structures." *Advanced Engineering Informatics*, 22(1),
  135-144.
- Posenato, D., Kripakaran, P., Inaudi, D., and Smith, I. F. C. (2010). "Methodologies for model-free data
  interpretation of civil engineering structures." *Computers & Structures*, 88(7-8), 467-482.
- Raphael, B., and Smith, I. (1998). "Finding the right model for bridge diagnosis." Artificial
  Intelligence in Structural Engineering in Computer Science, Springer, Heidelberg, 308-319.
- Ren, W.-X., and Chen, H.-B. (2010). "Finite element model updating in structural dynamics by using
   the response surface method." *Engineering Structures*, 32(8), 2455-2465.
- Reynders, E., Teughels, A., and De Roeck, G. (2010). "Finite element model updating and structural
  damage identification using OMAX data." *Mechanical Systems and Signal Processing*, 24(5),
  1306-1323.
- Robert-Nicoud, Y., Raphael, B., Burdet, O., and Smith, I. F. C. (2005). "Model Identification of Bridges
  Using Measurement Data." *Computer-Aided Civil and Infrastructure Engineering*, 20(2), 118131.
- Rodriguez-Galiano, V. F., Ghimire, B., Rogan, J., Chica-Olmo, M., and Rigol-Sanchez, J. P. (2012). "An
  assessment of the effectiveness of a random forest classifier for land-cover classification." *ISPRS Journal of Photogrammetry and Remote Sensing*, 67(0), 93-104.

- 451 Saitta, S., Raphael, B., and Smith, I. F. C. (2005). "Data mining techniques for improving the reliability 452 of system identification." *Advanced Engineering Informatics*, 19(4), 289-298.
- Saitta, S., Kripakaran, P., Raphael, B., and Smith, I. F. C. (2010). "Feature Selection using Stochastic
  Search: An Application to System Identification." *Journal of Computing in Civil Engineering*,
  24(1), 3-10.
- Strauss, A., Frangopol, D. M., and Kim, S. (2008). "Use of monitoring extreme data for the
  performance prediction of structures: Bayesian updating." *Engineering Structures*, 30(12),
  3654-3666.
- Suykens, J. A. K., Gestel, T. V., Brabanter, J. D., Moor, B. D., and Vandewalle, J. (2002). *Least Squares Support Vector Machines*, World Scientific, Singapore.
- 461 Vapnik, V., and Lerner, A. (1963). "Pattern Recognition using Generalized Portrait Method."
  462 Automation and Remote Control, 24, 774-780.
- Verikas, A., Gelzinis, A., and Bacauskiene, M. (2011). "Mining data with random forests: A survey and
   results of new tests." *Pattern Recognition*, 44(2), 330-349.
- Yan, A. M., Kerschen, G., De Boe, P., and Golinval, J. C. (2005a). "Structural damage diagnosis under
   varying environmental conditions--Part I: A linear analysis." *Mechanical Systems and Signal Processing*, 19(4), 847-864.
- Yan, A. M., Kerschen, G., De Boe, P., and Golinval, J. C. (2005b). "Structural damage diagnosis under
  varying environmental conditions--part II: local PCA for non-linear cases." *Mechanical Systems and Signal Processing*, 19(4), 865-880.
- Zhang, X., Liang, D., Zeng, J., and Asundi, A. (2012). "Genetic algorithm-support vector regression for
  high reliability SHM system based on FBG sensor network." *Optics and Lasers in Engineering*,
  50(2), 148-153.



Figure 1 An example of a regression tree with 12 splits and 13 terminal nodes. A node represents a group of data.



Figure 2 Flowchart of the combined model-free data-interpretation methodologies



Figure 3 . An 80-m railway steel truss bridge with sensor locations marked as black bars and the damage location marked as a black dot.



Figure 4 Minimum detectable damage-level for a truss bridge using 9 model-free data interpretation methods.



Figure 5 Time to damage detection for a truss bridge using 9 model-free data interpretation methods for 50% damage level



Figure 6 A concrete frame model with four measured responses including vertical displacement at midspan, horizontal displacement at roller support, rotation over the left support bearing and rotation over the right support bearing.



Figure 7 Minimum detectable damage level for a concrete frame using 9 model-free data interpretation methods



Figure 8 Time to detection for a concrete frame using 9 model-free data interpretation methods for 35% damage level



Figure 9 High correlated principal component pairs for the truss model (left) and the frame model (right).



Figure 10 Measurement configuration for the Ricciolo viaduct: a cross-section view (Posenato et. al., 2010)



Figure 11 Measurement configuration for the Ricciolo viaduct: a plane-view (Posenato et. al., 2010)



Figure 12 Plot of the first eigenvector during the monitoring period recalculated from Posenato et al. (2010). Detection of construction stages as events that simulate anomalous structural behavior (time scale is inverted)



Figure 13 Time to detection for event number 6, recalculated from Posenato et al. (2010)



Figure 14 Results of correlation-based methods for damage detection using RRA (left) and MPCA-RRA (right)

**Table 1. Properties of truss members of a railway bridge in Zangenberg, Germany** 

| Member type    | Area (m²)               | I <sub>x</sub> (m <sup>4</sup> ) | I <sub>y</sub> (m⁴)      |
|----------------|-------------------------|----------------------------------|--------------------------|
| Top chord      | 5.15 x 10 <sup>-2</sup> | 2.267 x 10 <sup>-3</sup>         | 2.586 x 10 <sup>-3</sup> |
| Bottom chord   | 3.03 x 10 <sup>-1</sup> | 1.467 x 10 <sup>-3</sup>         | 1.458 x 10 <sup>-3</sup> |
| Vertical       | 2.19 x 10 <sup>-2</sup> | 1.215 x 10 <sup>-3</sup>         | 4.245 x 10 <sup>-5</sup> |
| Diagonal       | 3.69 x 10 <sup>-2</sup> | 9.704 x 10 <sup>-4</sup>         | 4.164 x 10 <sup>-3</sup> |
| Small diagonal | 2.19 x 10 <sup>-2</sup> | 1.215 x 10 <sup>-3</sup>         | 4.245 x 10 <sup>-5</sup> |

# **Table 2 List of events**

| Event number | Period                | Description                              |
|--------------|-----------------------|--|
| 1            | January 12-14         | Post-tensioning from 30 to 70%           |
| 2            | January 17            | Partial lowering formworks               |
| 3            | January 17 - April 22 | Construction of lateral protection walls |
| 4            | April 25-26           | Post-tensioning from 70 to 100%          |
| 5            | April 25-27           | Cast of left side wing                   |
| 6            | April 25-27           | Removal of external formworks            |