Verification & Validation: application to the TORPEX basic plasma physics experiment

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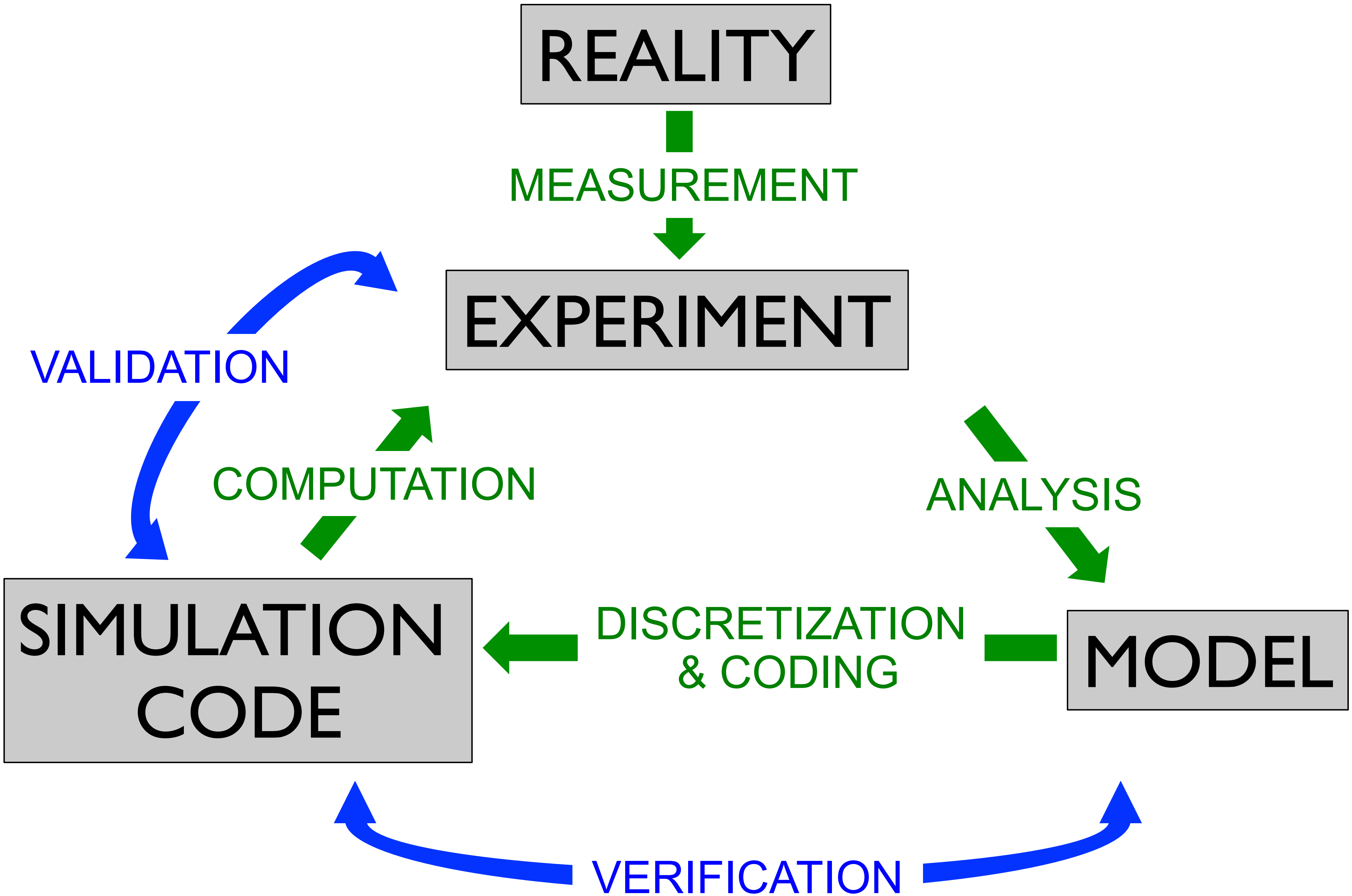
What does “Verification & Validation” mean?

What is TORPEX? And the simulation code we use?

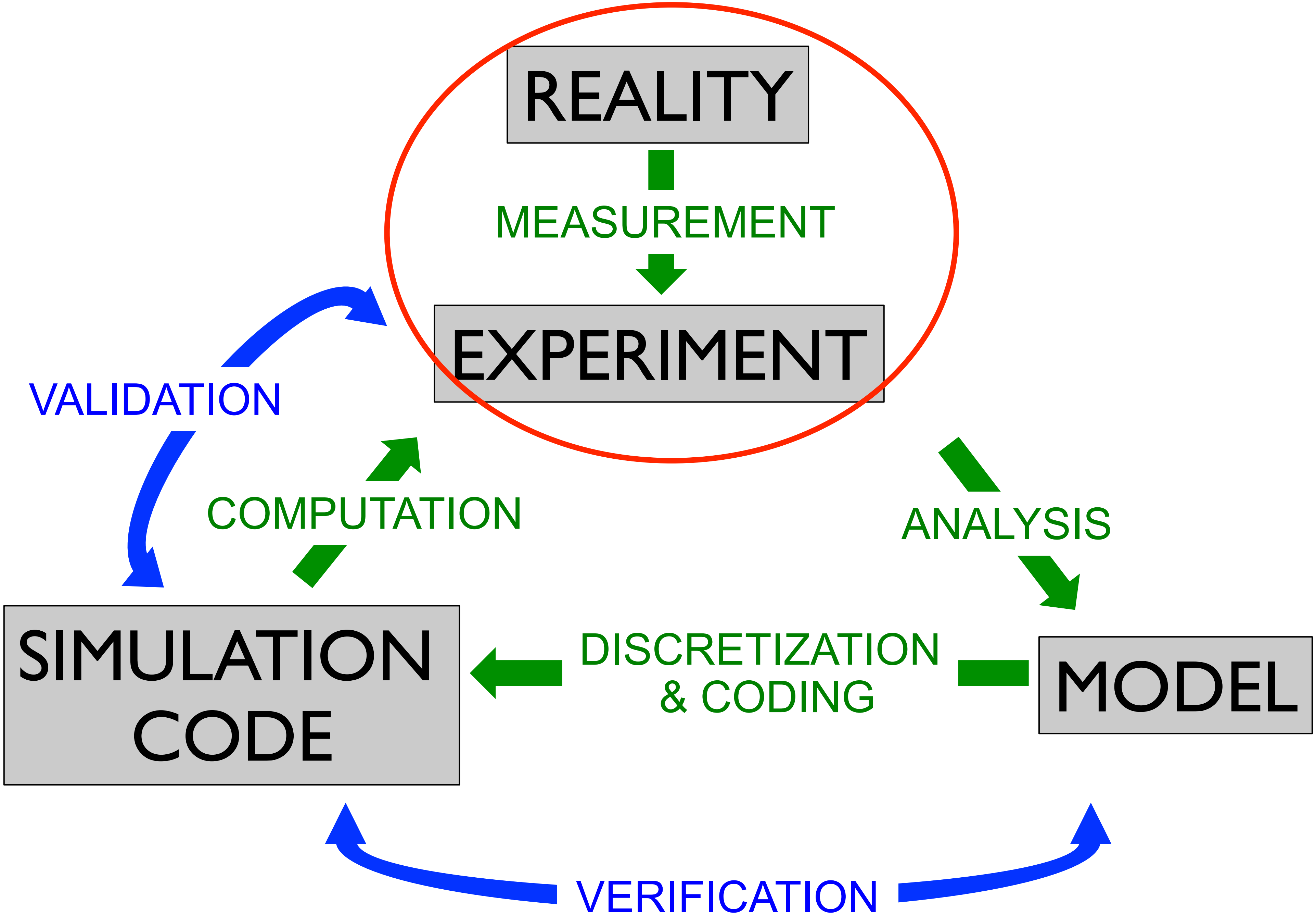
What verification methodology did we use? and validation methodology?

What have we learned?

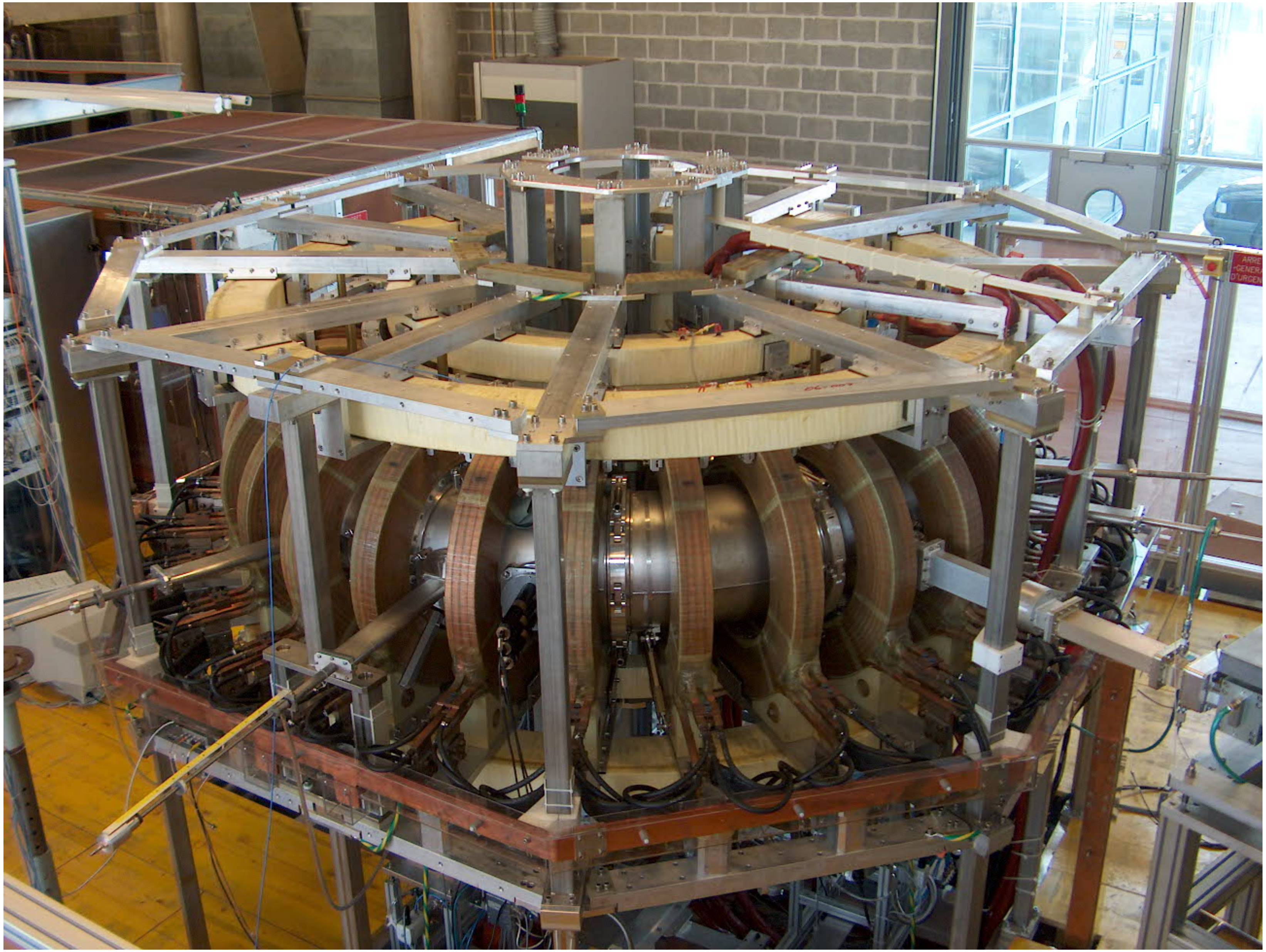
Verification & Validation



Verification & Validation



The TORPEX device



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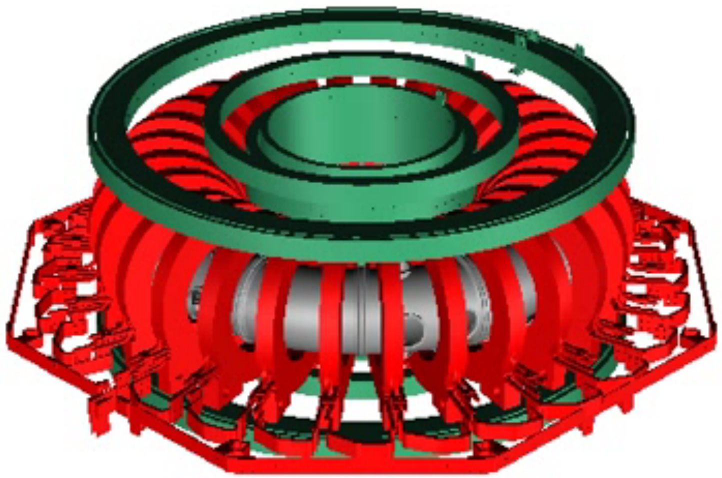

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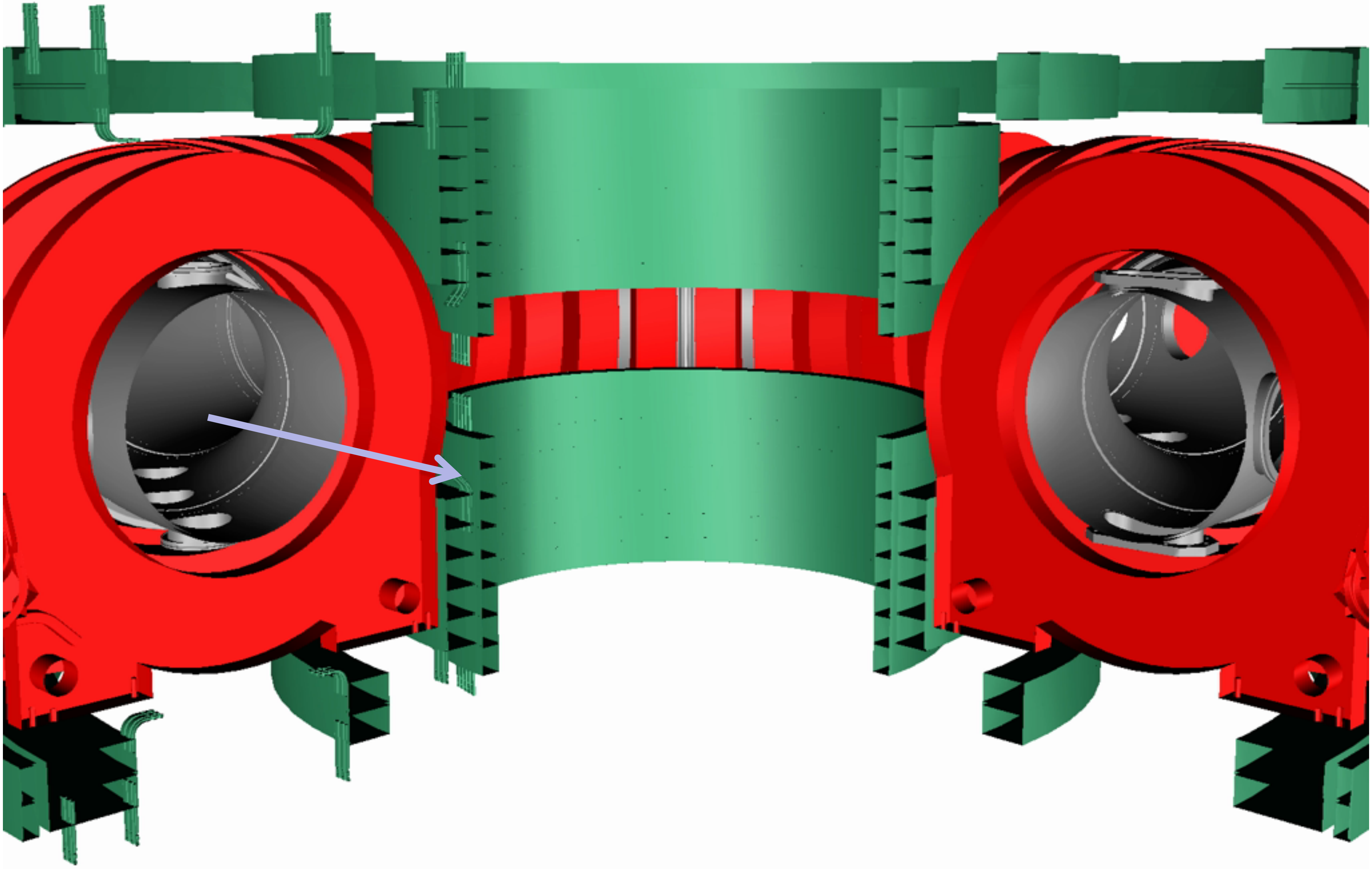

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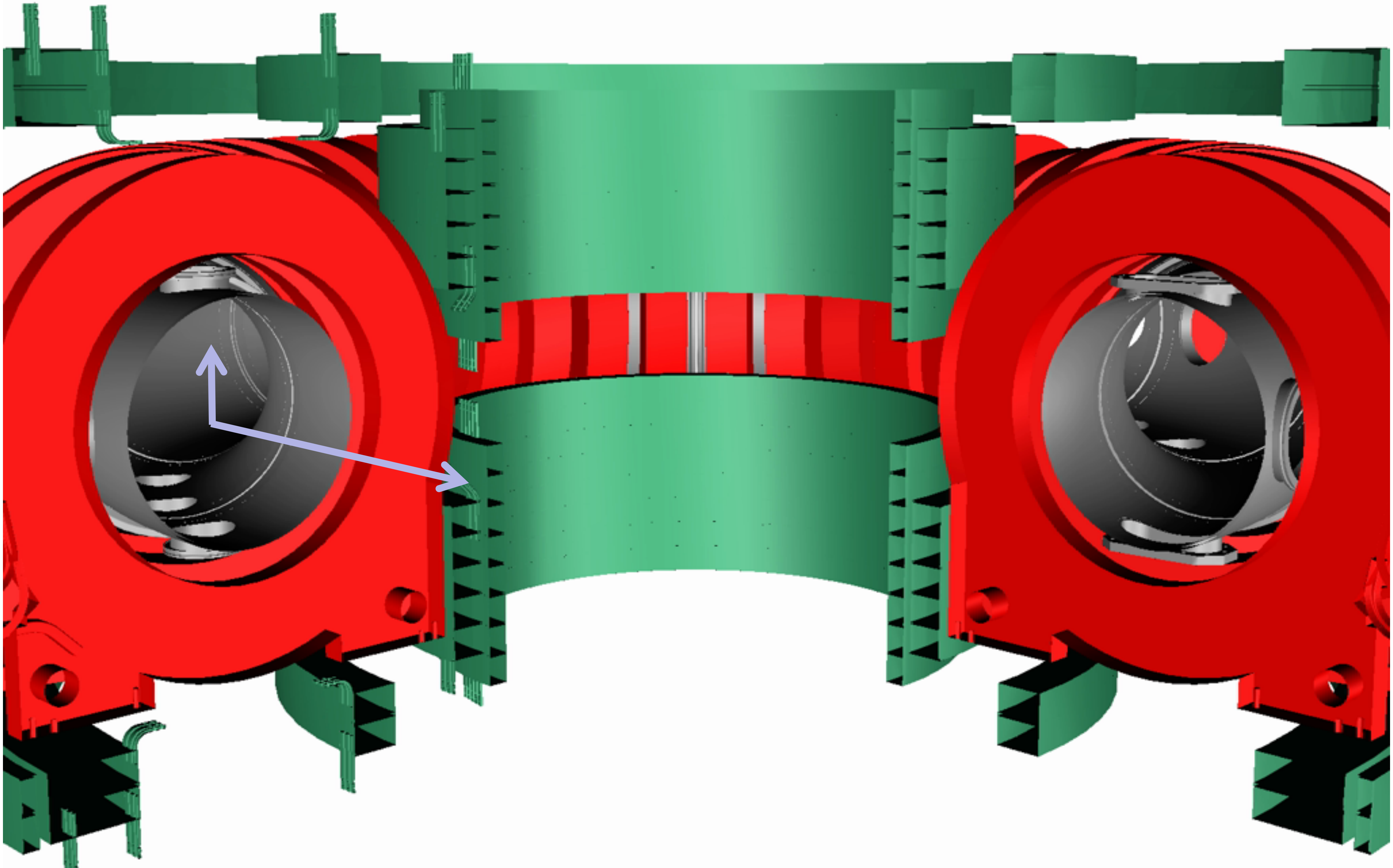

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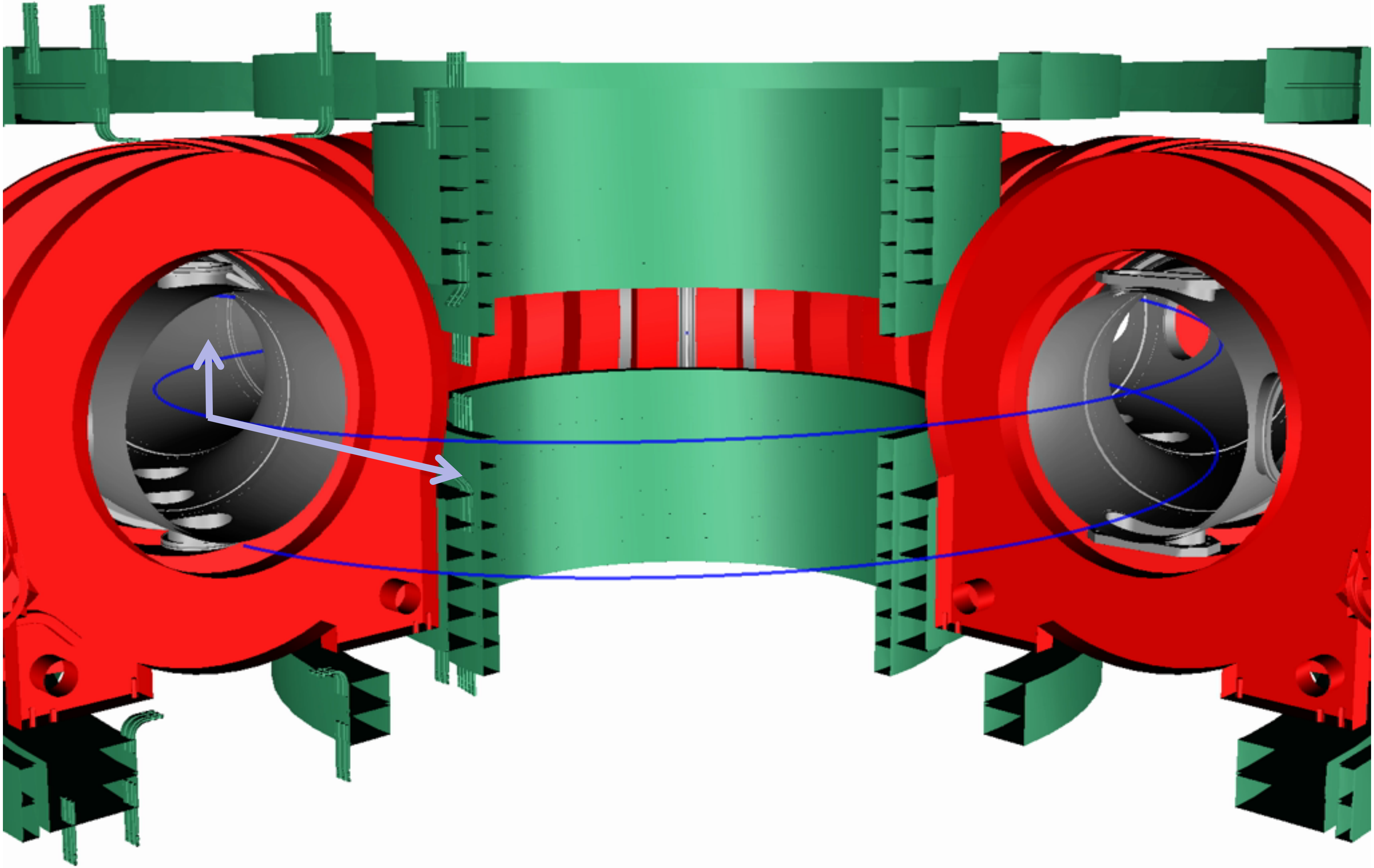
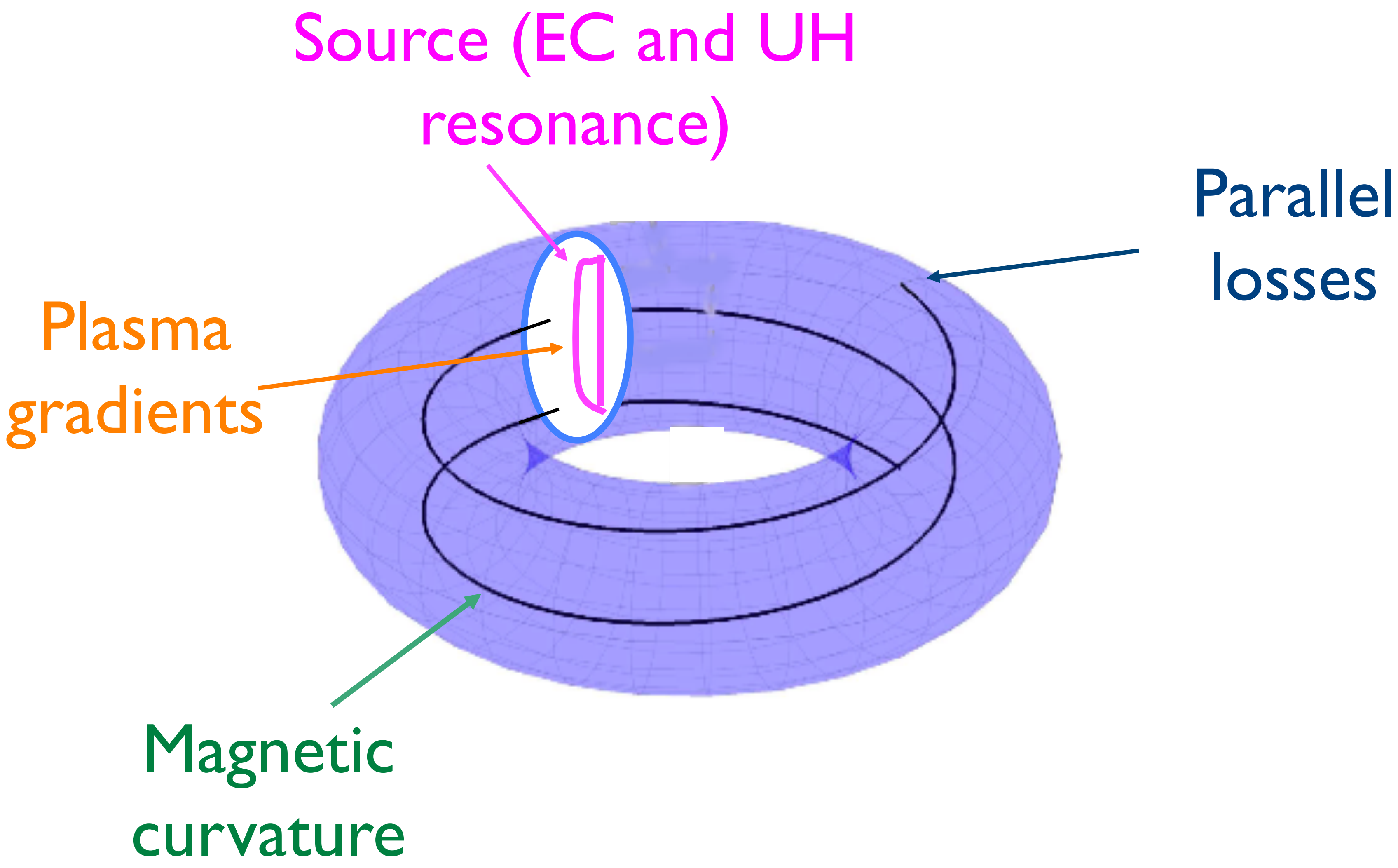
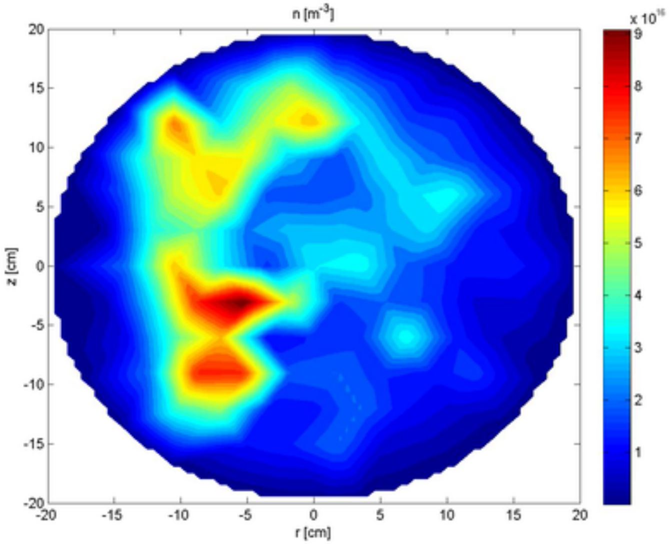


Key elements of the TORPEX device

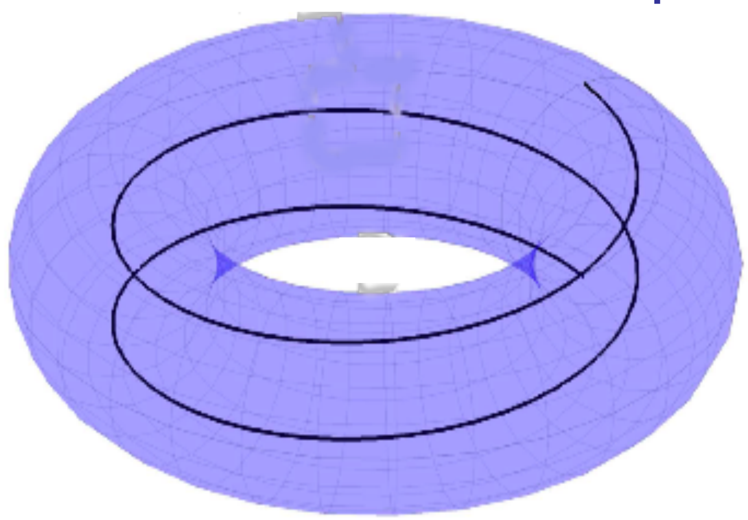


TORPEX: an ideal verification & validation testbed



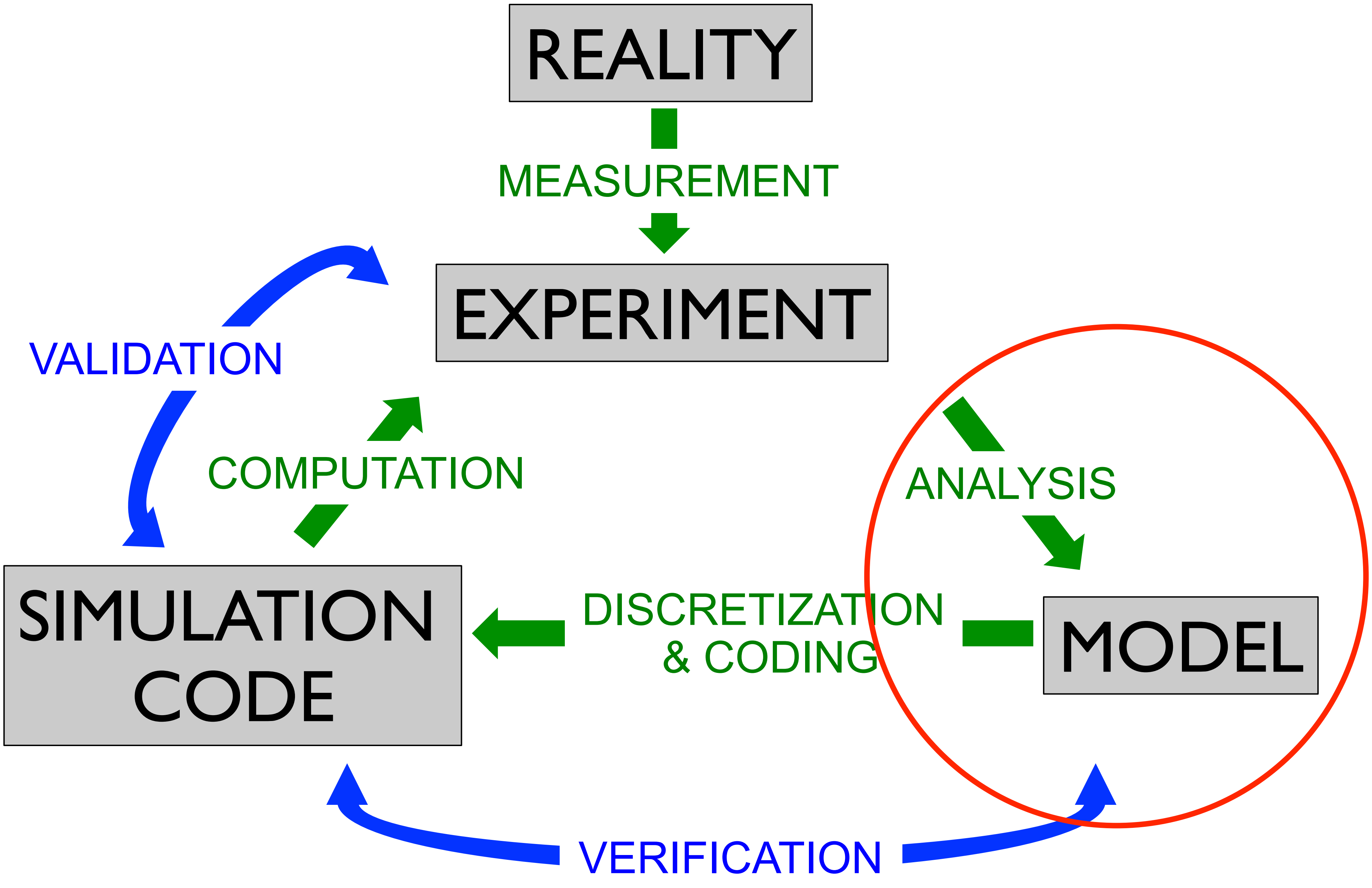
- Complete set of diagnostics, full plasma imaging possible

Example: N=2



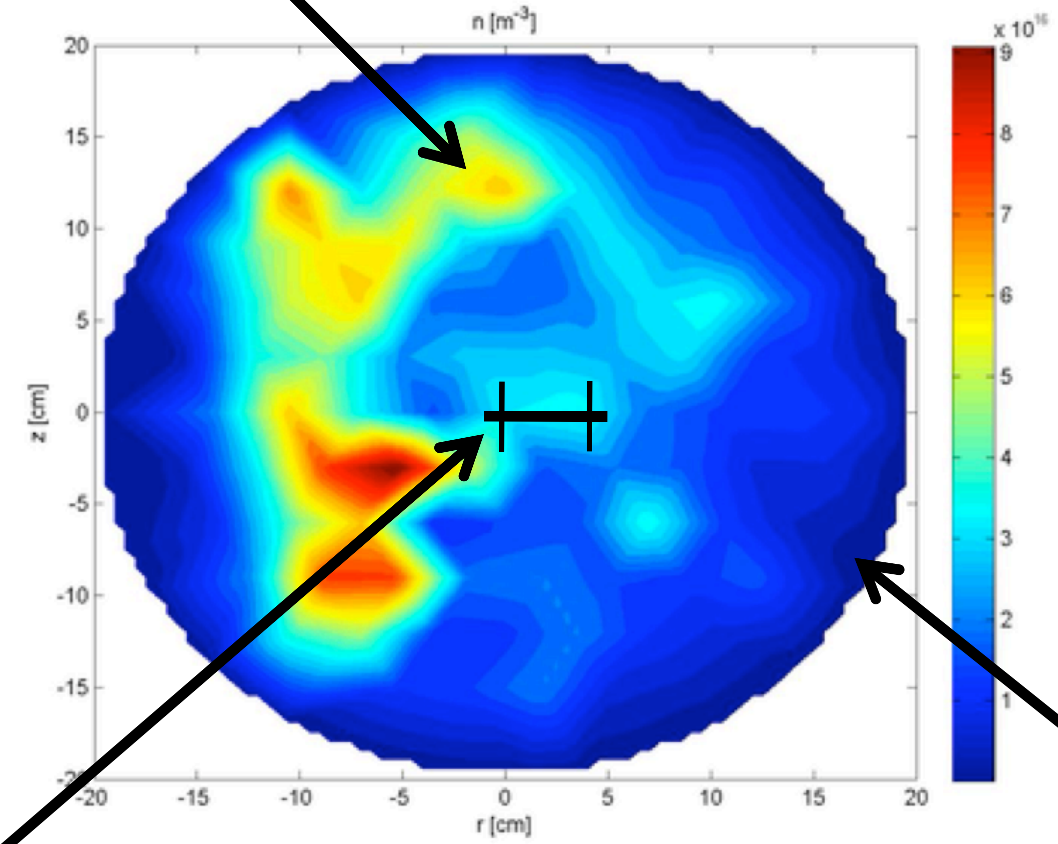
- Parameter scan, N – number of field line turns

Verification & Validation



Properties of TORPEX turbulence

$n_{fluc} \sim n_{eq}$



Collisional

$L_{eq} \sim L_{fluc}$

$L >> \rho_i$

The model

Collisional Plasma → **Braginskii model** → ($\rho_i << L$, $\omega << \Omega_{ci}$, $\beta << 1$) → **Electrostatic Drift-reduced Braginskii equations**

Convection | Magnetic curvature | Parallel dynamics | Source

$$\frac{\partial n}{\partial t} + [\phi, n] = \hat{C}(nT_e) - n\hat{C}(\phi) - \nabla_{\|}(nV_{\|e}) + S$$

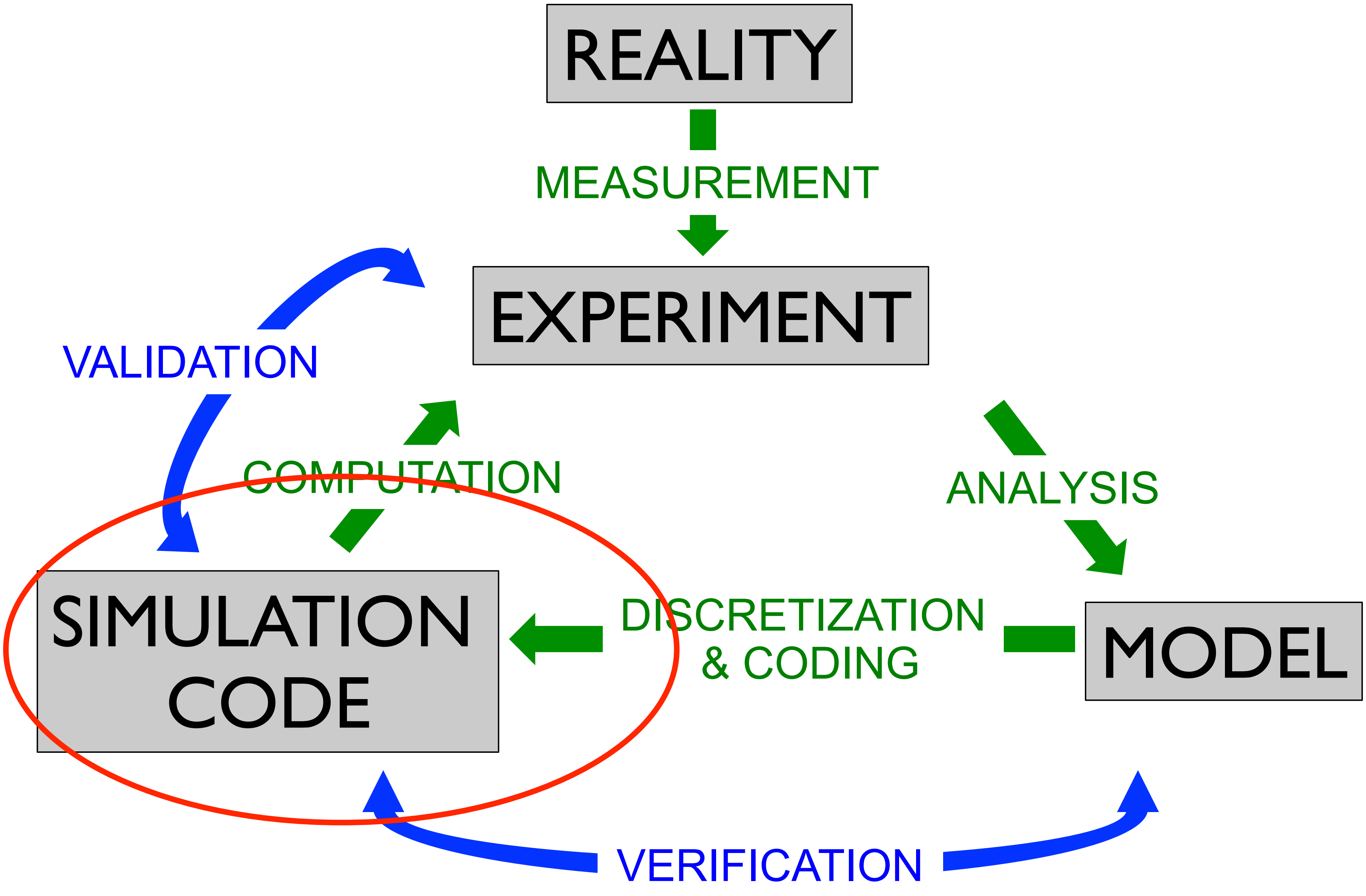
T_e, Ω (vorticity) → similar equations

$V_{\|e}$, $V_{\|i}$ → parallel momentum balance

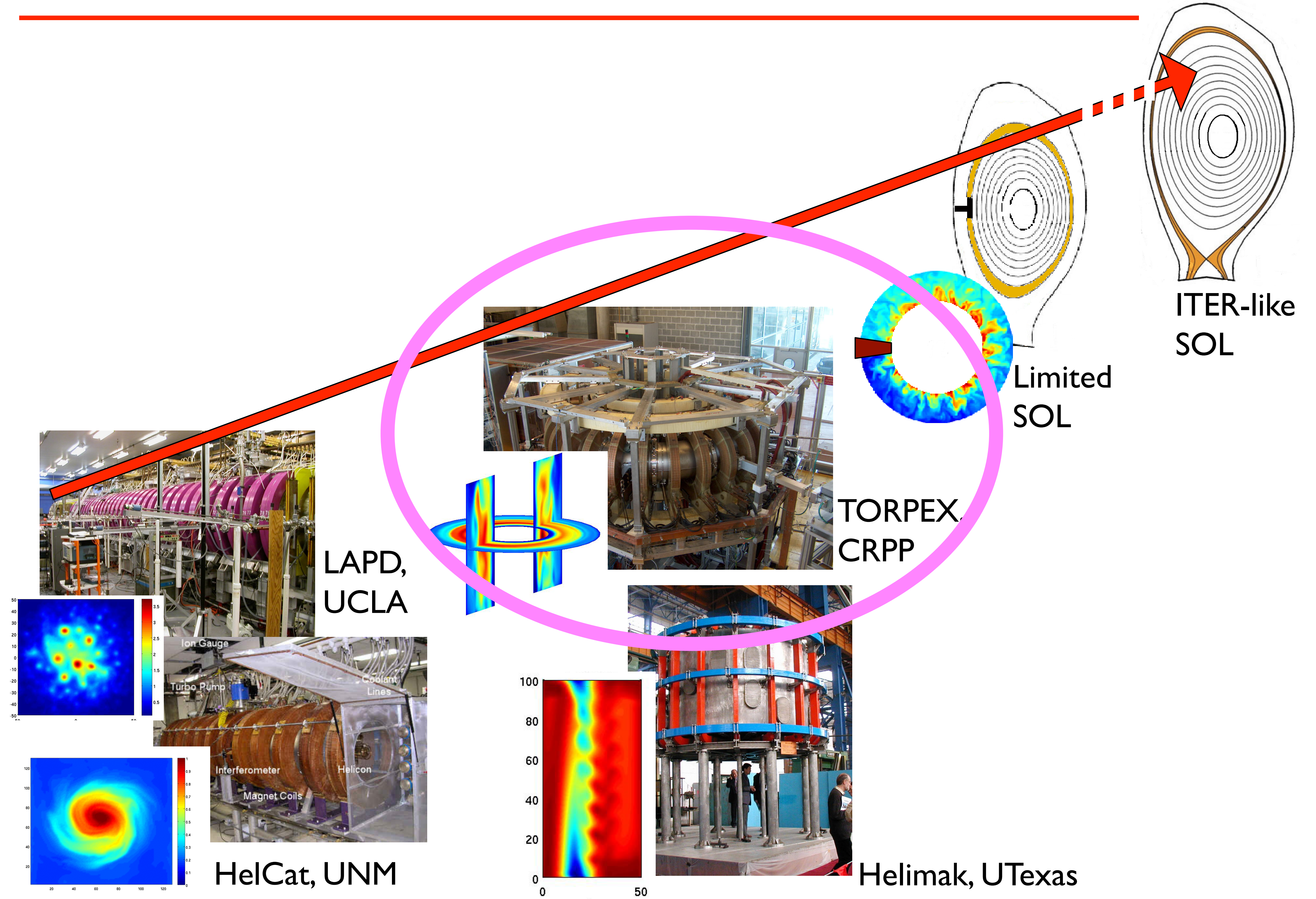
$\nabla_{\perp}^2 \phi = \Omega$

Quasi steady state – balance between:
plasma source, perpendicular transport, and parallel losses

Verification & Validation

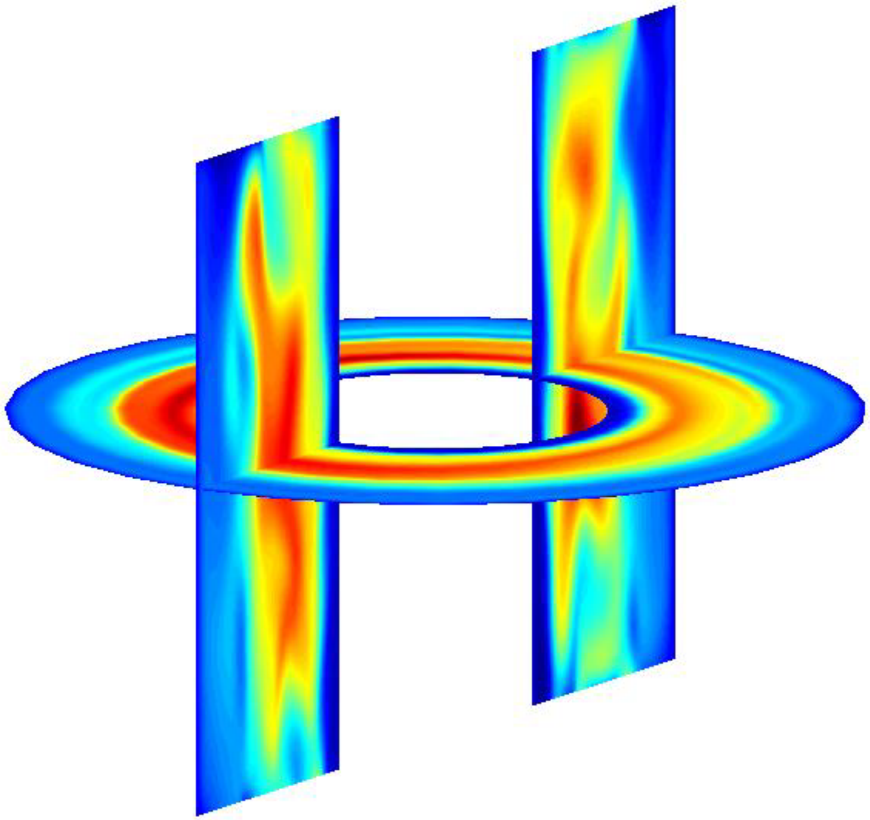


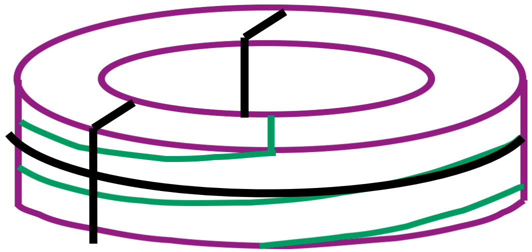
GBS: simulation of plasma turbulence in edge conditions



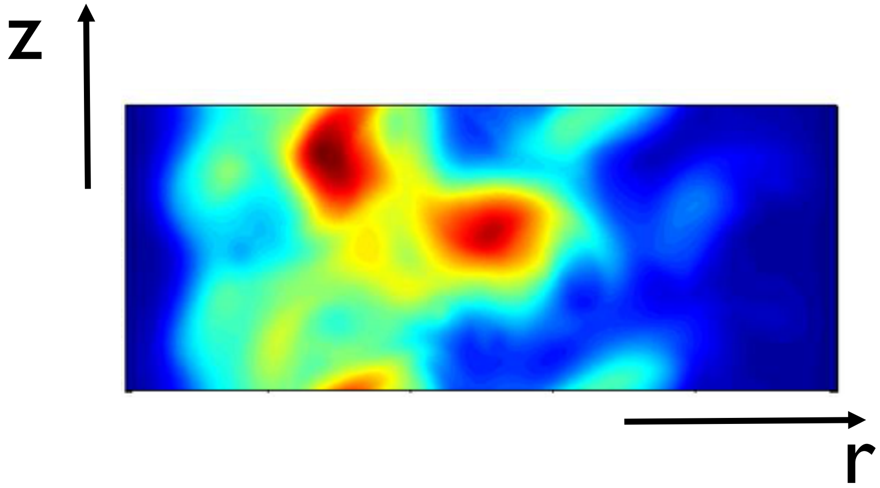
3D and 2D GBS simulations

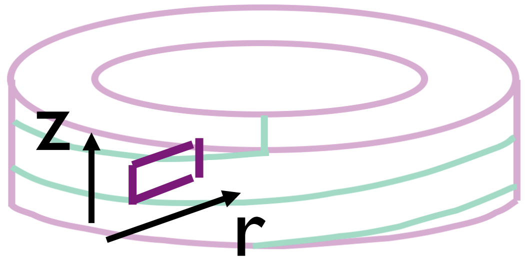
Fully 3D version



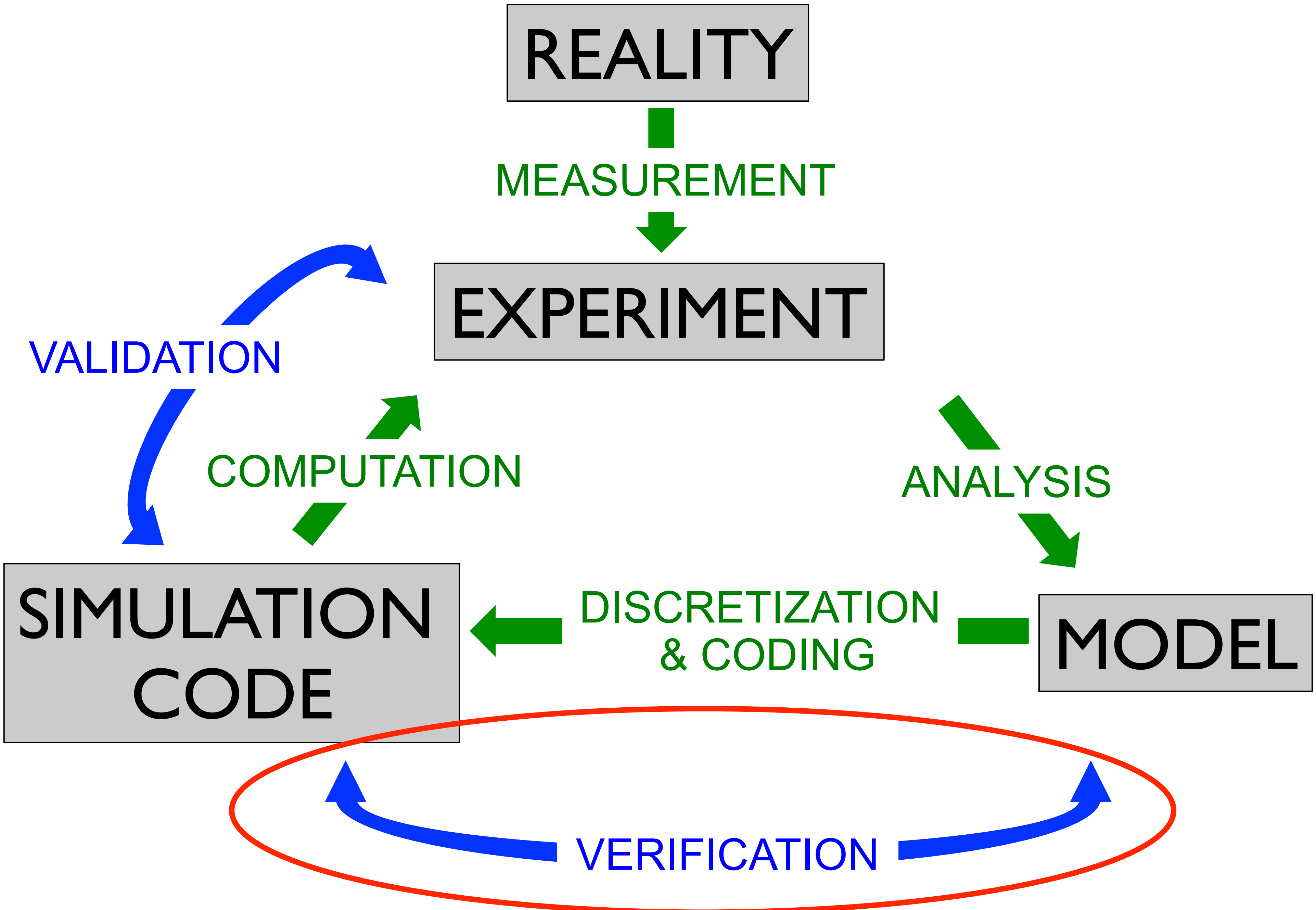


2D version ($k_{||}$=0 hypothesis)





Verification & Validation



Code verification, the techniques

1) Simple tests
2) Code-to-code comparisons (benchmarking)
3) Discretization error quantification
4) Convergence tests
5) Order-of-accuracy tests

NOT RIGOROUS

RIGOROUS, requires analytical solution

Only verification ensuring convergence and correct numerical implementation

Order-of-accuracy tests, method of manufactured solution

Our model: $A(f) = 0\,,\quad f$ unknown

We solve $A_n(f_n) = 0\,,$ but $\epsilon_n = f_n - f = ?$

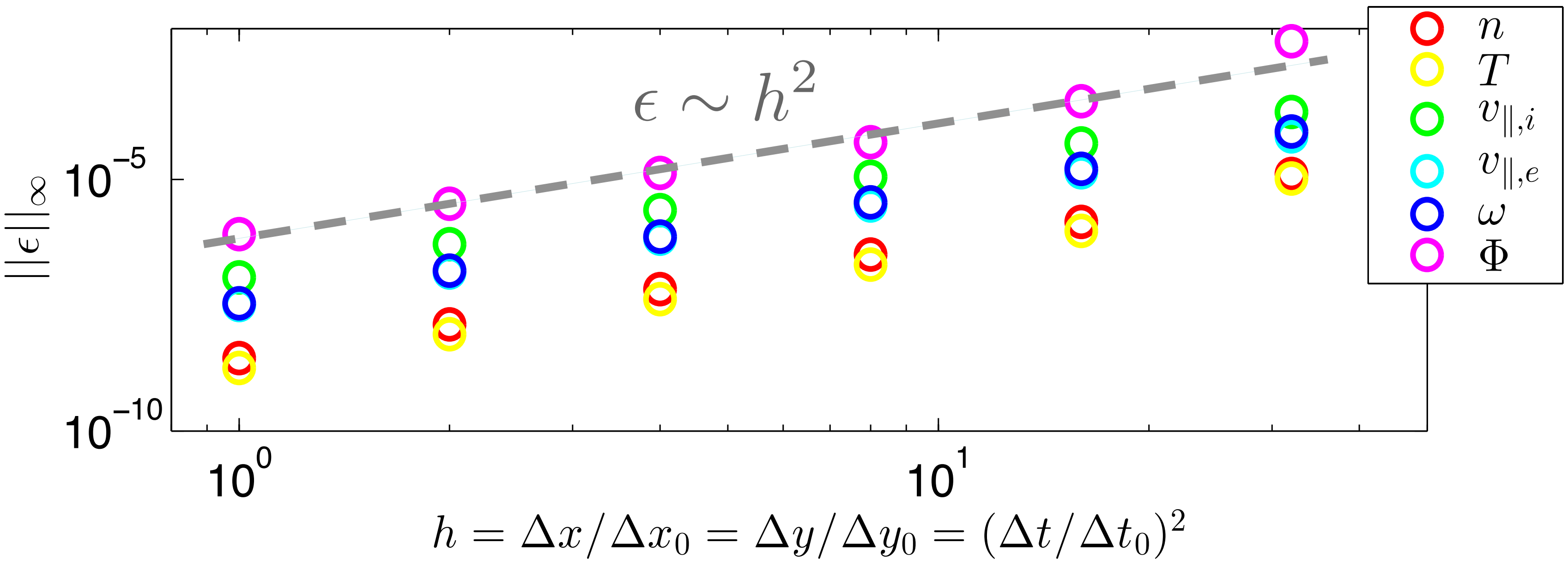
Method of manufactured solution:

1) we choose g, then $S = A(g)$

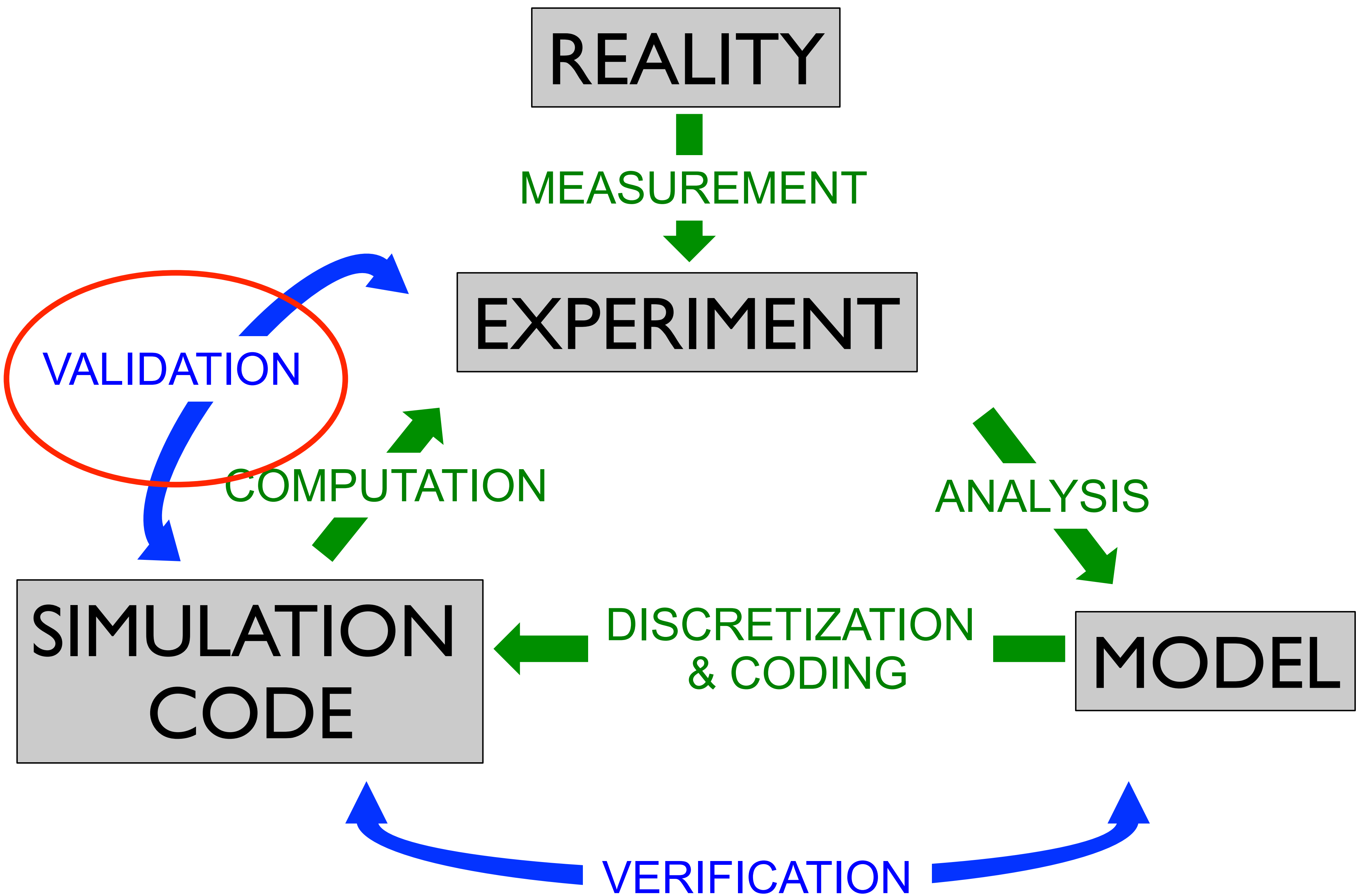
2) we solve: $A_n(g_n) - S = 0$

$\epsilon_n = g_n - g$

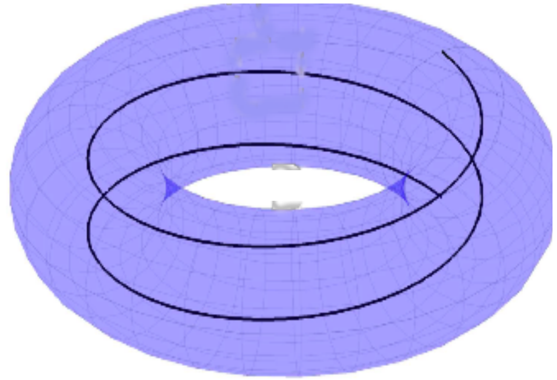
For GBS:



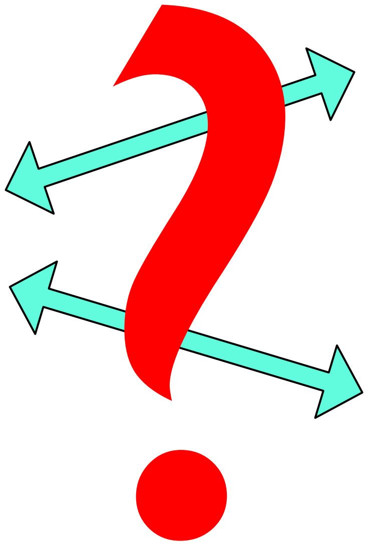
Verification & Validation



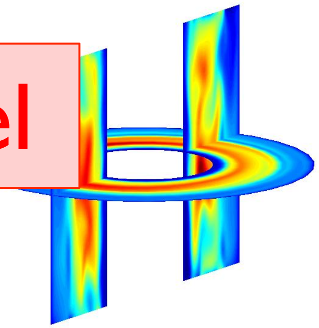
Our project, paradigm of turbulence code validation



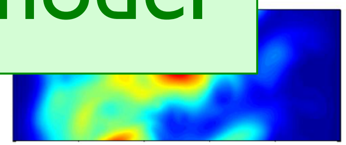
TORPEX



3D GBS model



2D reduced model



What is the agreement of experiment and simulations as a function of *N*? Is 3D necessary?

What can we learn on TORPEX physics from the validation?

The validation methodology

[Based on ideas of Terry *et al.*, PoP 2008; Greenwald, PoP 2010]

What quantities can we use for validation? The more, the better…

- Definition & evaluation of the validation observables

What are the uncertainties affecting measured and simulation data?

- Uncertainty analysis

For one observable, within its uncertainties, what is the level of agreement?

- Level of agreement for an individual observable

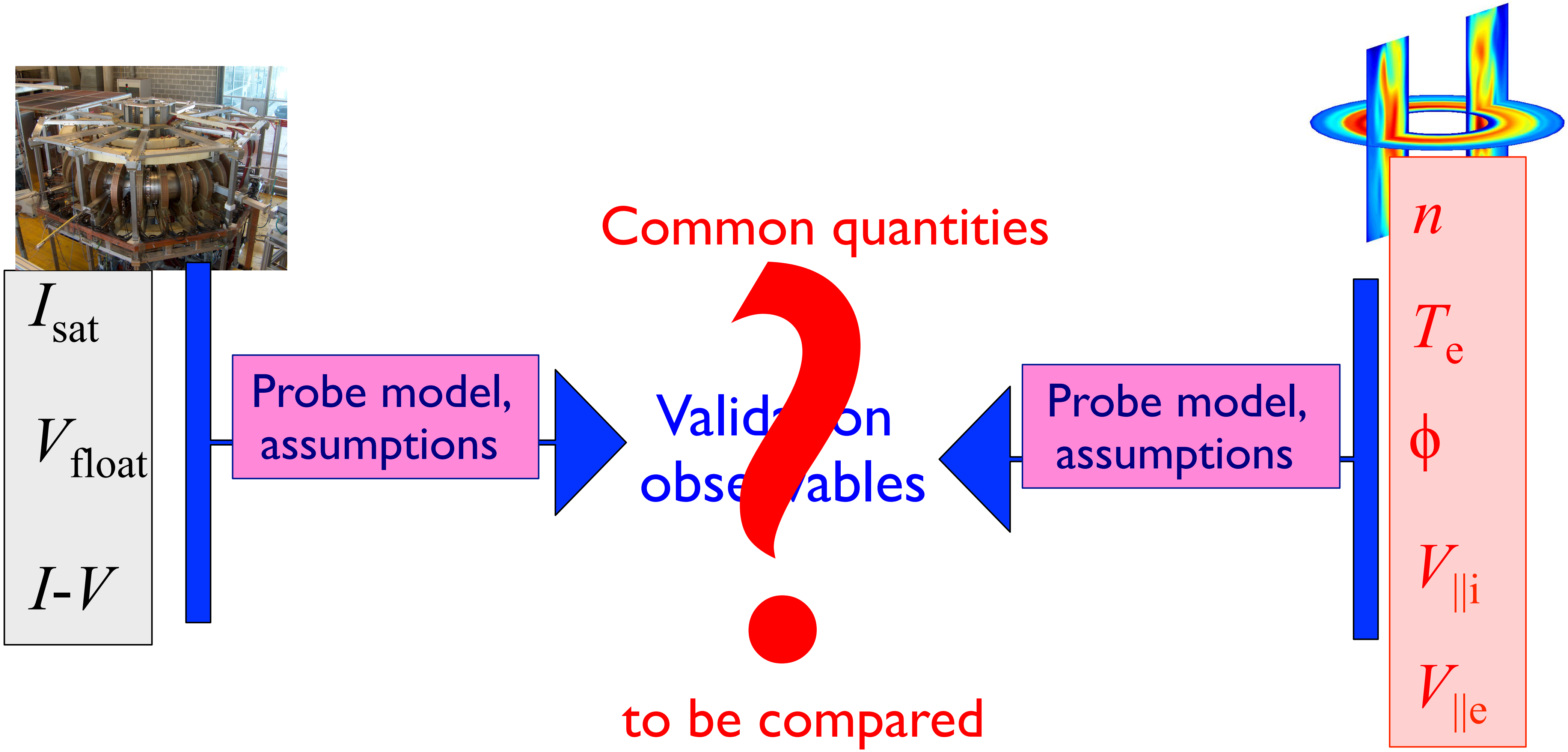
How directly can an observable be extracted from simulation and experimental data? How worthy is it, i.e. what should be its weight in a composite metric?

- The observable hierarchy

How to evaluate the global agreement and how to interpret it

- Composite metric

Definition of the validation observables



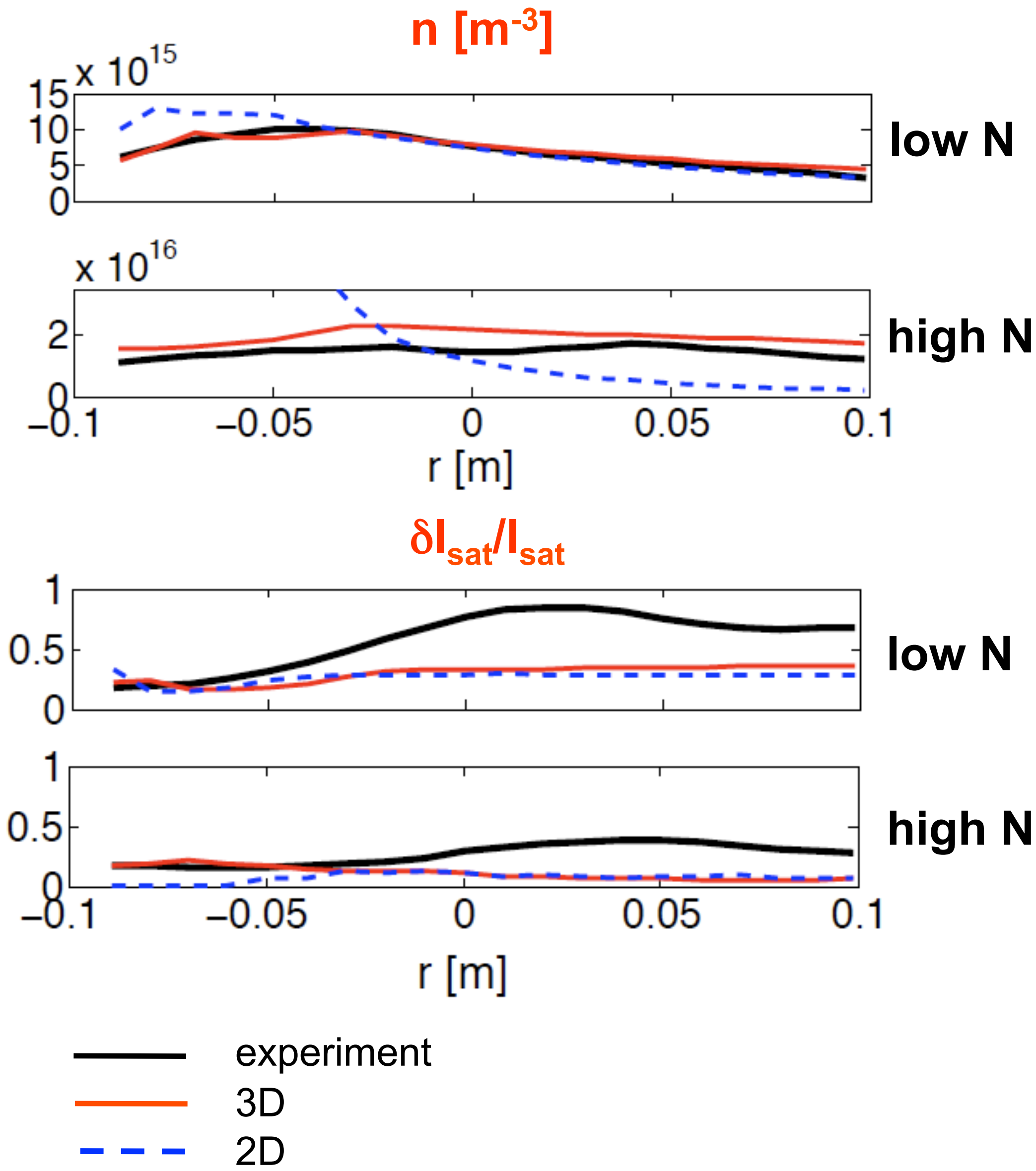
- Examples: $\langle I_{\mathrm{sat}} \rangle_t$, $\langle n \rangle_t$, Γ, ...
- A validation observable should not be a function of the others
- Quantities to predict should be included among the observables

Evaluation of the validation observables

We evaluate 11 observables:

- $\langle n(r) \rangle_t$
- $\langle T_e(r) \rangle_t$
- $\langle I_{\text{sat}}(r) \rangle_t$
- $\delta I_{\text{sat}} / I_{\text{sat}}$
- k_v
- $\text{PDF}(I_{\text{sat}})$
- ...

Examples



Uncertainty analysis

Experiment

$$\Delta x^2 = \Delta x^2_{\mathrm{fit}} + \Delta x^2_{\mathrm{prb}} + \Delta x^2_{\mathrm{rep}} + \Delta x^2_{\mathrm{fin}}$$

- $\Delta x^2_{\mathrm{fit}}$: I-V Fitting
- $\Delta x^2_{\mathrm{prb}}$: Probe properties, measurement uncertainties
- $\Delta x^2_{\mathrm{rep}}$: Plasma reproducibility
- $\Delta x^2_{\mathrm{fin}}$: Finite statistics

Simulation

$$\Delta y^2 = \Delta y^2_{\mathrm{num}} + \Delta y^2_{\mathrm{inp}} + \Delta y^2_{\mathrm{fin}}$$

- $\Delta y^2_{\mathrm{num}}$: Numerics
- $\Delta y^2_{\mathrm{inp}}$: Input parameters - scan in resistivity and boundary conditions
- $\Delta y^2_{\mathrm{fin}}$: Finite statistics

Agreement with respect to an individual observable

Distance:

Experimental measurements

Simulation results

$$d = \sqrt{\frac{1}{G}\sum_{i=1}^{G}\frac{(x_i - y_i)^2}{\Delta x_i^2 + \Delta y_i^2}}$$

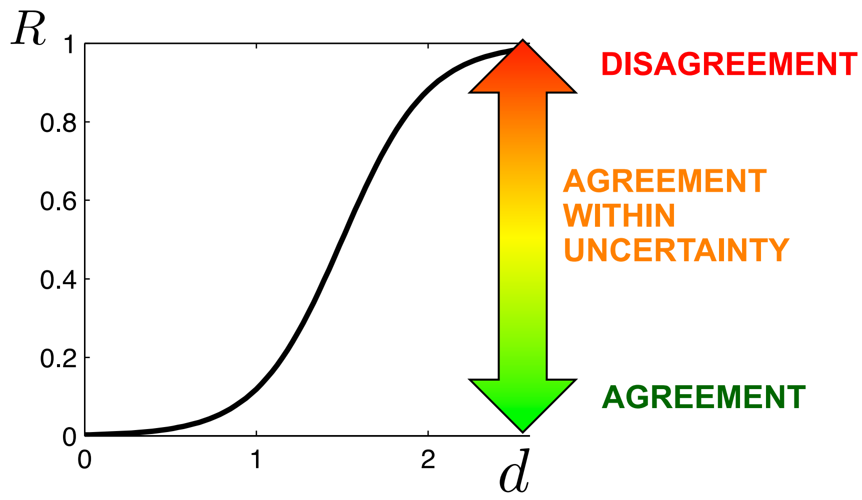
Average over all points

Normalization to uncertainties

Level of agreement:

$$R = \frac{\tanh[(d - d_0)/\lambda] + 1}{2}$$

$$d_0 = 1.5$$
$$\lambda = 0.5$$



Observable hierarchy

Not all the observables are equally worthy…

The hierarchy assesses the assumptions used for their deduction

h^{exp} : # of assumptions to get the observable from experimental data

h^{sim} : same for simulation results

$$h = h^{exp} + h^{sim}$$

Examples: - $\langle n \rangle_t$: $h^{\mathrm{exp}} = 1,\ h^{\mathrm{sim}} = 0,\ h = 1$

- $\Gamma_{I_{\mathrm{sat}}}$: $h^{\mathrm{exp}} = 2,\ h^{\mathrm{sim}} = 1,\ h = 3$

Composite metric

Level of agreement

$$R_j = \frac{\tanh[(d_j - d_0)/\lambda] + 1}{2}$$

Hierarchy level

$$H_j = 1/(h_j + 1)$$

Sensitivity

$$S_j = \exp\left(- \frac{\Sigma_i \Delta x_{j,i} + \Sigma_i \Delta y_{j,i}}{\Sigma_i |x_{j,i}| + \Sigma_i |y_{j,i}|} \right)$$

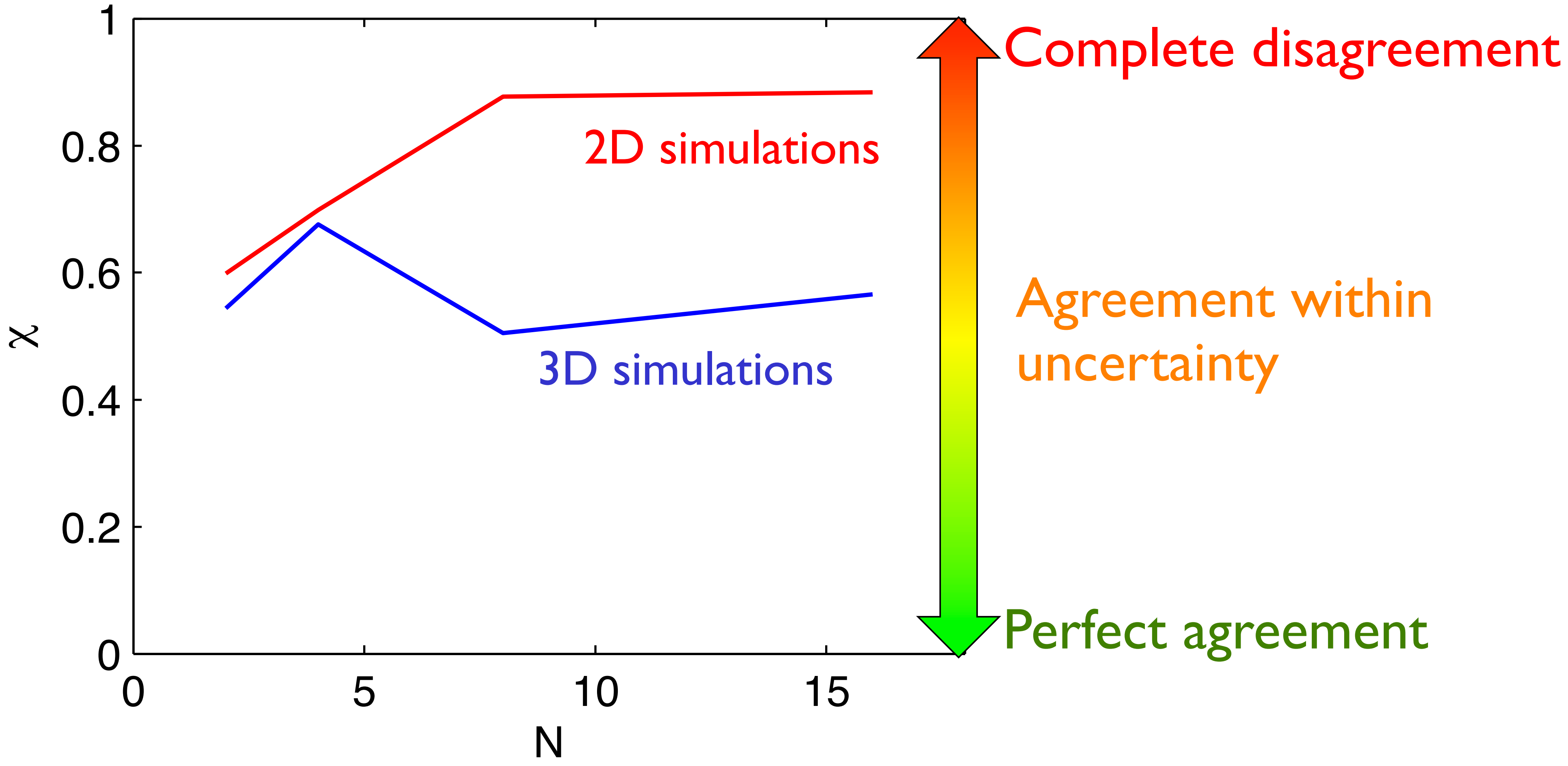
Sum over all the observables

$$\chi = \frac{\Sigma_j R_j H_j S_j}{\Sigma_j H_j S_j}$$

Normalization:

- $\chi = 0$: perfect agreement
- $\chi = 0.5$: agreement within uncertainty
- $\chi = 1$: total disagreement

The validation results



Why 2D and 3D work equally well at low N and 2D fails at high N?
What can we learn on the TORPEX physics?

Flute instabilities - ideal interchange mode

$k_{\parallel} = 0$ ➡

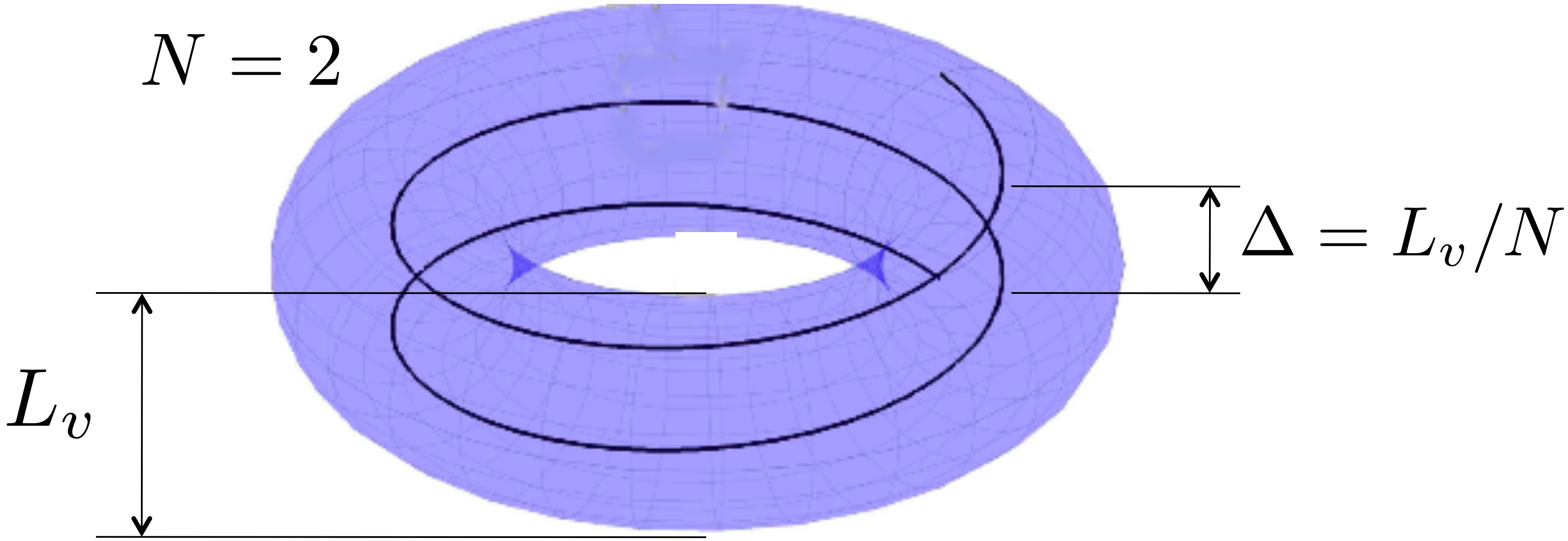
n + T_e eqs. ⟶ $$\frac{\partial p_e}{\partial t} = \frac{c}{B}[\phi, p_e]$$

Vorticity eq. ⟶ $$\frac{\partial \nabla_{\perp}^2 \phi}{\partial t} = \frac{2B}{cm_i R n}\frac{\partial p_e}{\partial y}$$

➡ $\gamma = \gamma_I$ $\qquad \gamma_I = c_s\sqrt{\frac{2}{L_p R}}$

Compressibility stabilizes the mode at $k_v \rho_s > 0.3\gamma_I R/c_s$

Anatomy of a $k_{\parallel} = 0$ perturbation



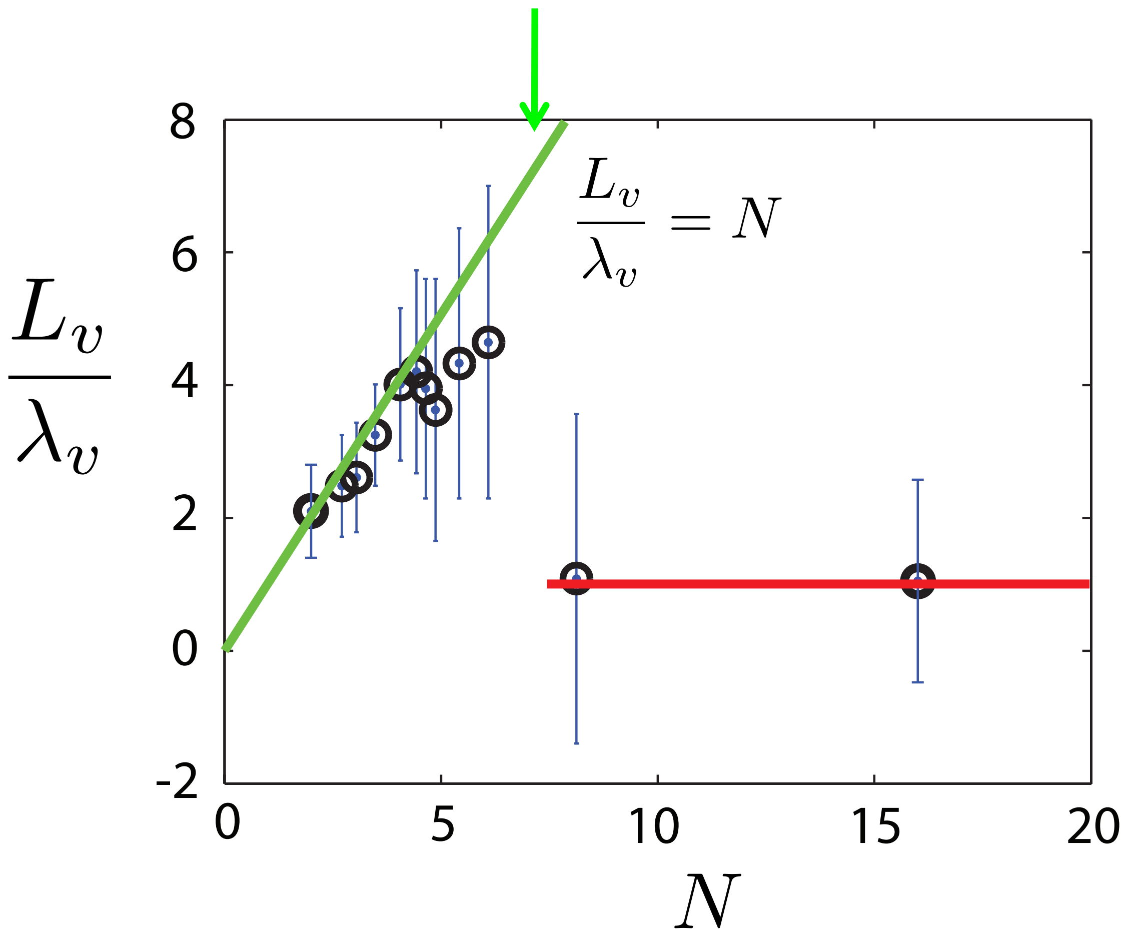
λ_v : longest possible vertical wavelength of a perturbation

If $k_{\parallel} = 0$ then $\lambda_v = \Delta = \dfrac{L_v}{N}$

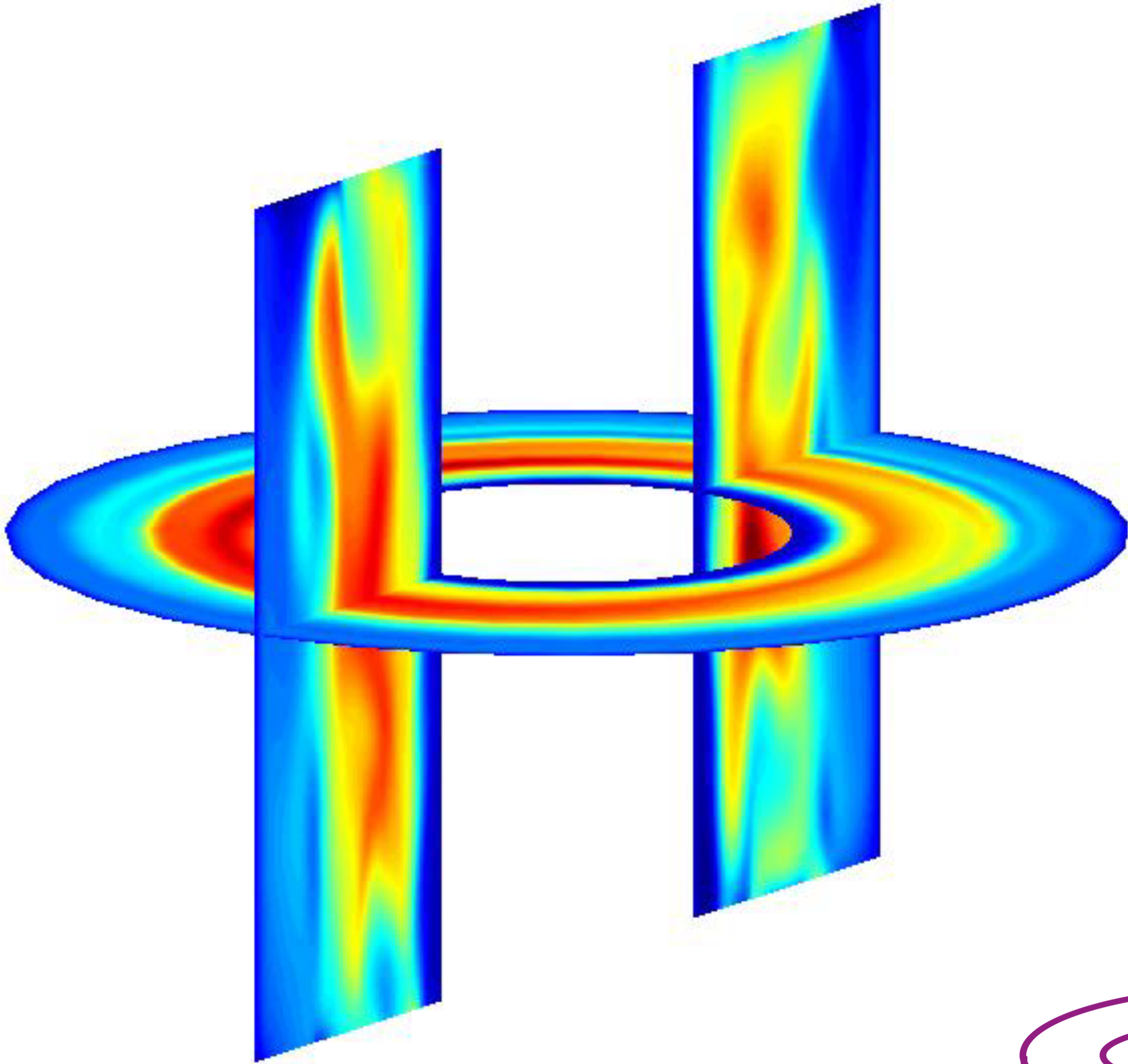
TORPEX shows $k_{\parallel} = 0$ turbulence at low N

$$k_{\parallel} = 0 \quad (\lambda_v = L_v / N)$$

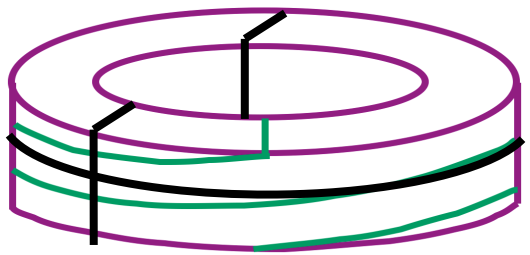
Ideal interchange regime



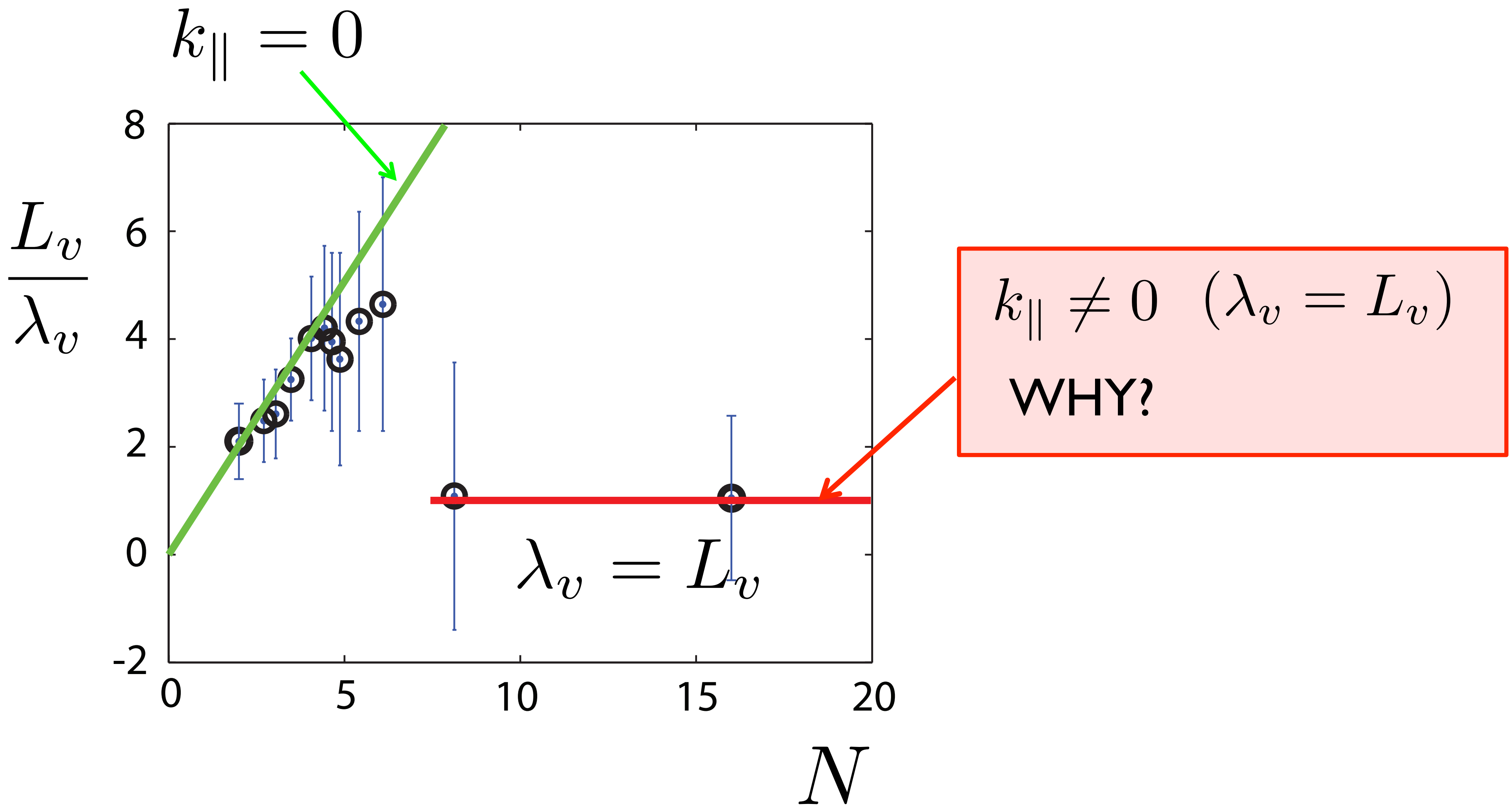
For N~1-6, ideal $k_{\|} = 0$ interchange modes dominant



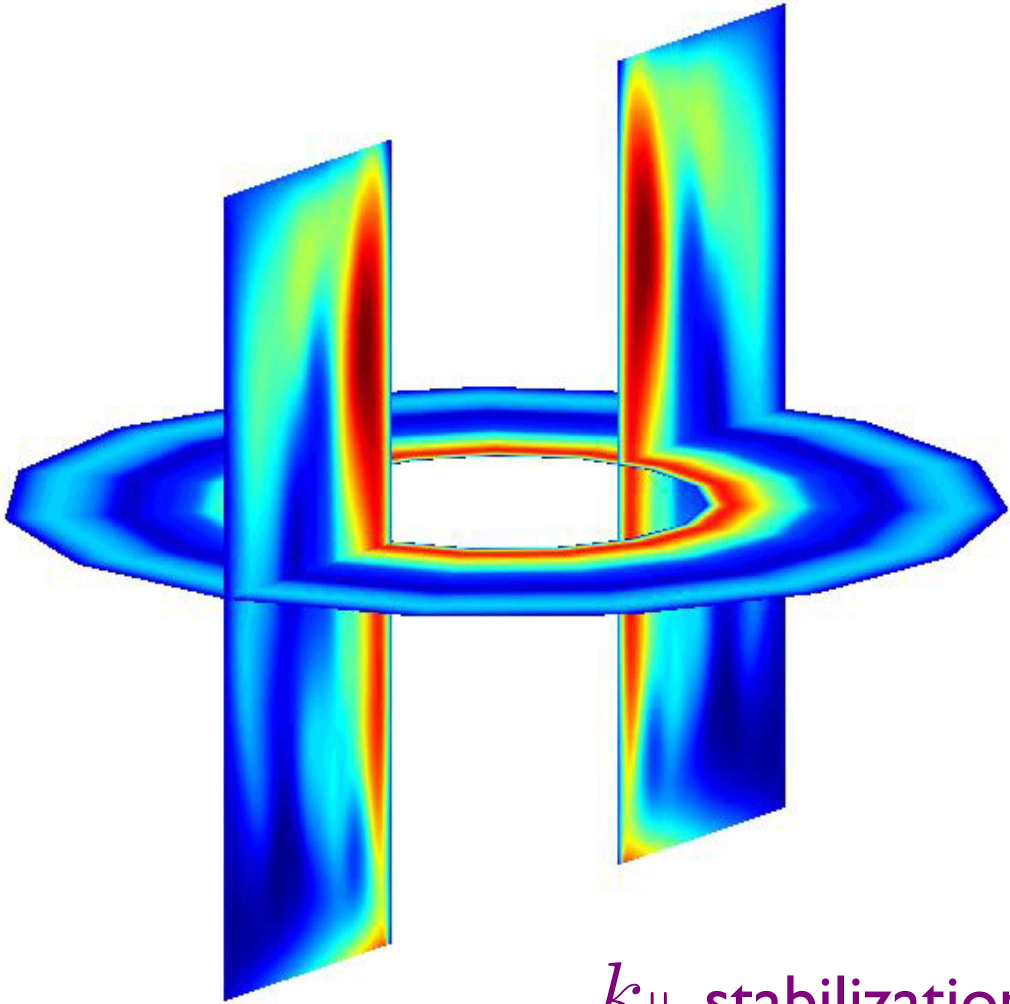
N=2



Turbulence changes character at N>7



At high N>7, Resistive Interchange Mode turbulence



Toroidally symmetric

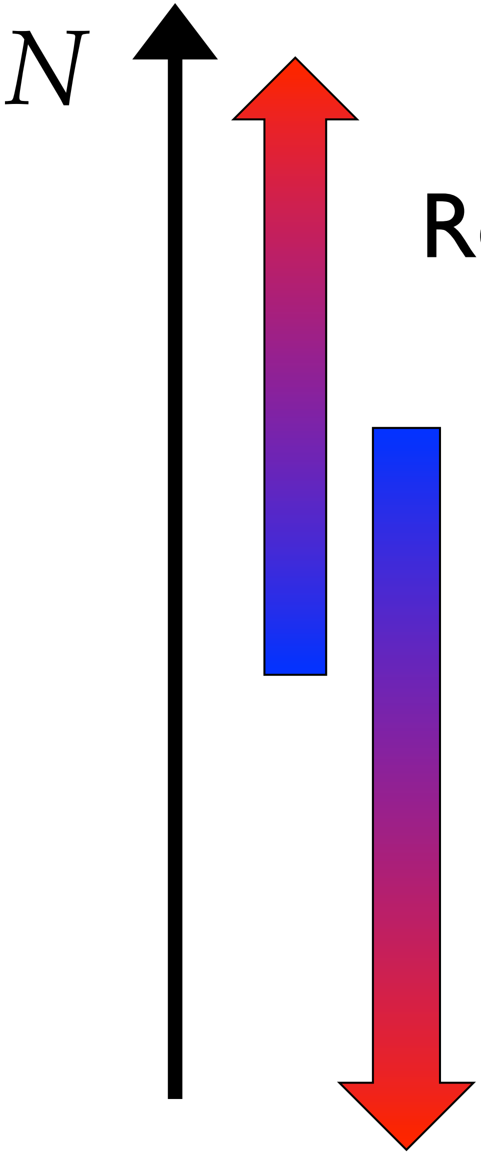
$\lambda_v \sim L_v$

$k_{||}$ stabilization, requires high N and $\eta_{||} \neq 0$

Introducing $k_{||} \neq 0$ modes

$$\gamma^2 = \gamma_I^2 - \gamma \frac{4\pi V_A^2 k_{||}^2}{\eta_{||} c^2 k_y^2}, \quad \gamma_I = c_s \sqrt{\frac{2}{R L_p}}$$

Why does TORPEX transition from ideal to resistive interchange for large N?



Resistive interchange requires high N

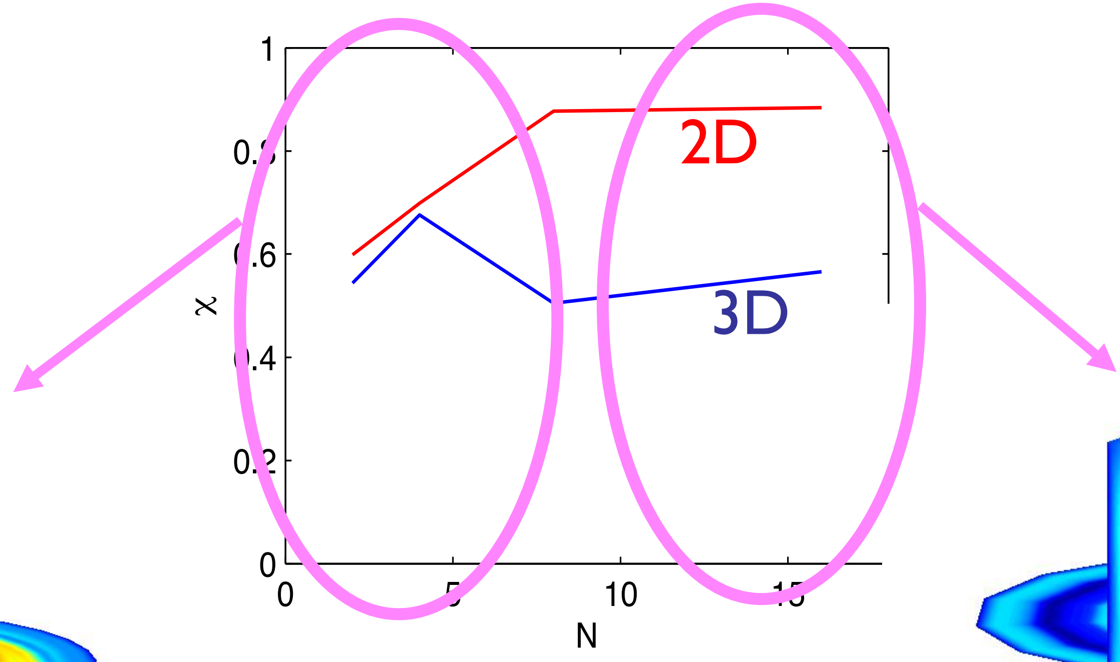
Ideal interchange requires low N:

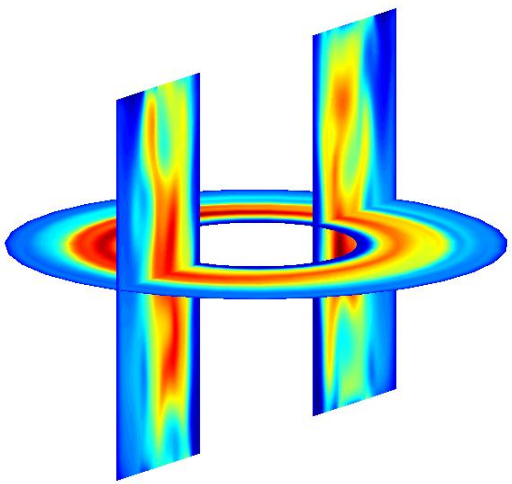
$$\lambda_v = \frac{L_v}{N} \quad \text{thus} \quad k_v = \frac{2\pi N}{L_v}$$

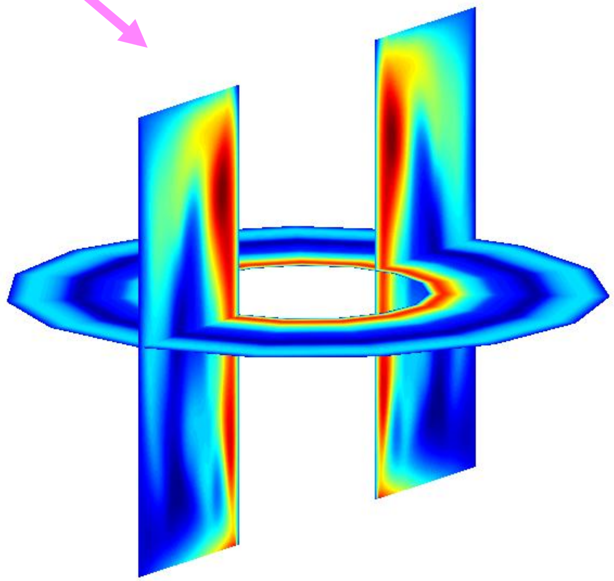
stable: $k_v \rho_s > 0.3 R \gamma_I / c_s$

Threshold: N~10 in TORPEX

Interpretation of the validation results







$k_{\|} = 0$

- Ideal interchange turbulence
- 2D model appropriate

$k_{\|} \neq 0$

- Resistive interchange turbulence
- 2D model not appropriate

Where can a verification & validation exercise help?

1. Make sure that the code works correctly

   Correct GBS implementation, rigorously, discretization error estimate

2. Compare codes

   2D and 3D simulations agree with experimental measurements similarly at low N.

   Global 3D simulations are needed to describe the plasma dynamics at high N.

3. Let the physics emerge

   Two turbulent regimes: ideal interchange mode at low N and non-flute modes at high N.

   Parameter scans have a crucial role

4. Assess the predictive capabilities of a code

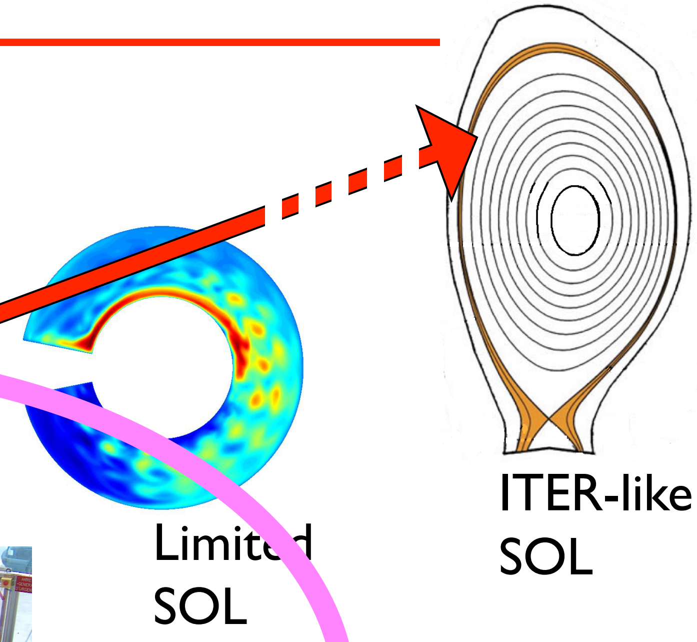
   3D simulations predict (within uncertainty) profiles of n but not of I_{sat}

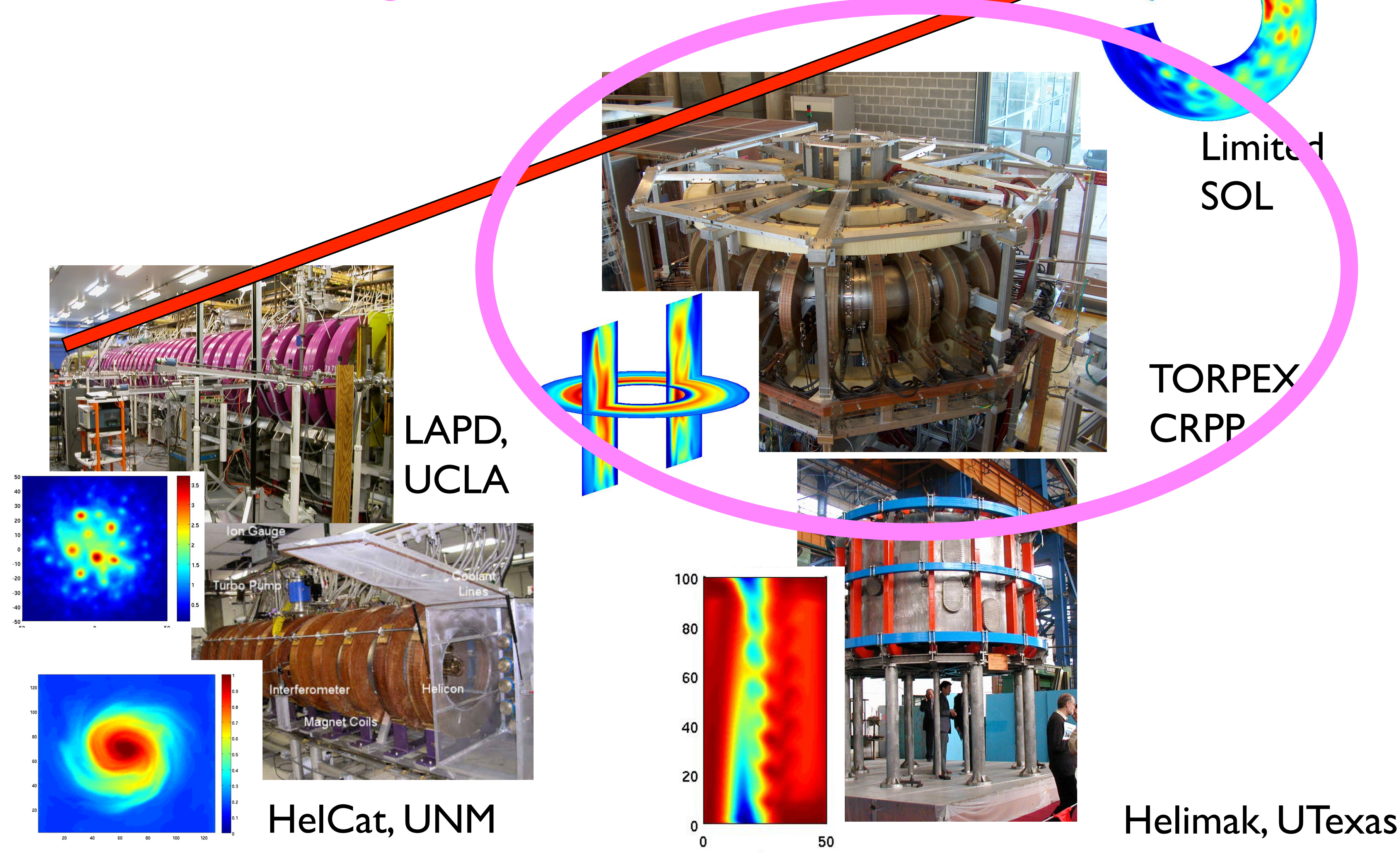
EPFL

CRPP

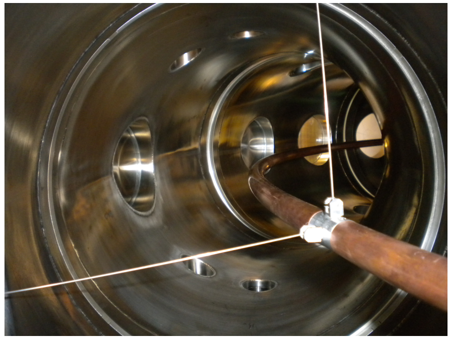
What comes next?

- Validation at each code refinement
- Considering more observables
- Involving more codes

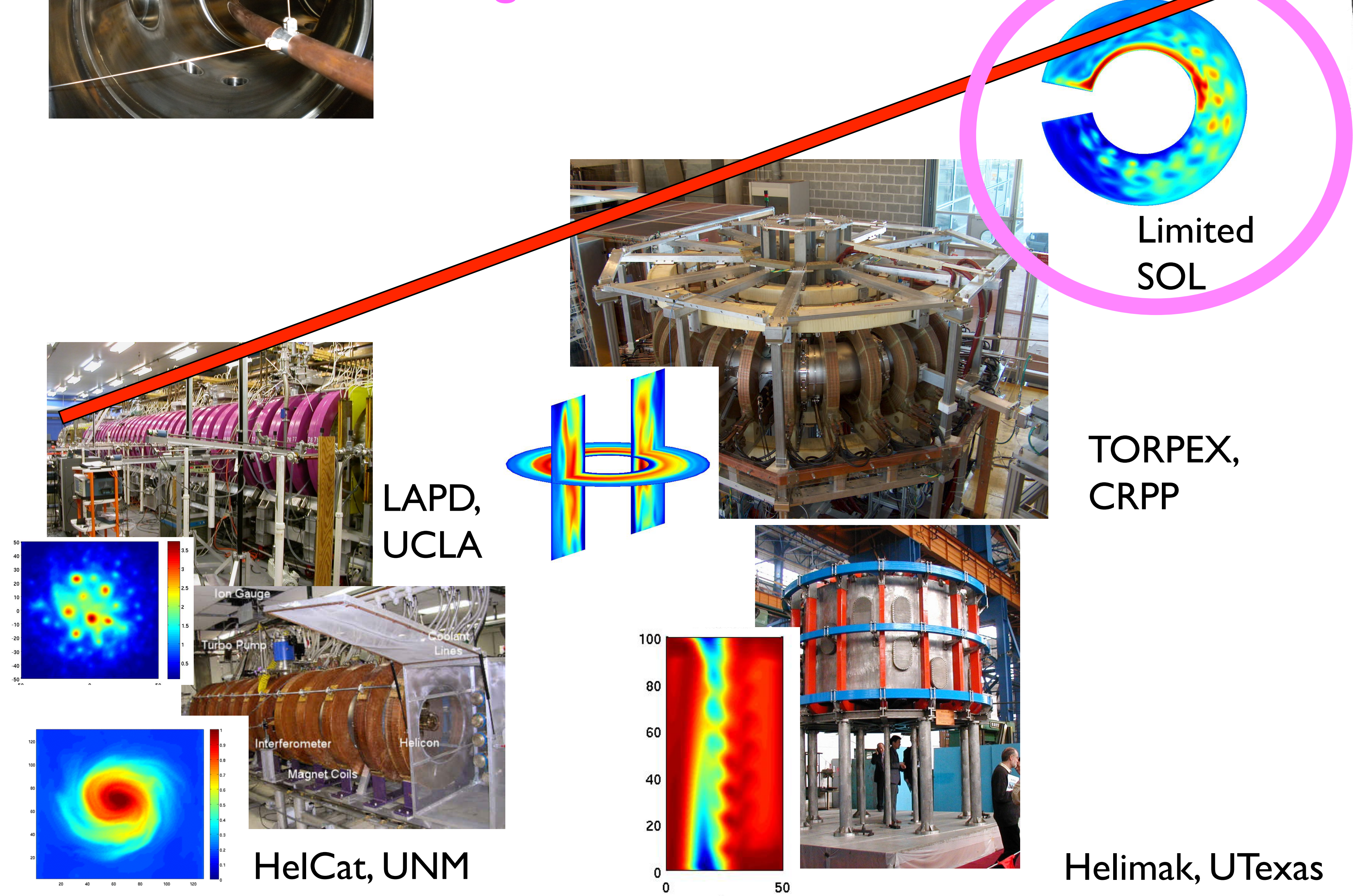


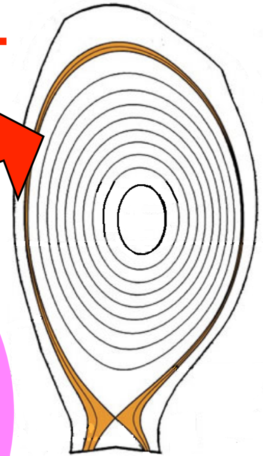


What comes next?



Validation on a recently achieved SOL-like configuration in TORPEX





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   Rigorously, with discretization error estimate

2. Compare codes

   2D and 3D simulations agree with experimental measurements similarly at low N.

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3. Let the physics emerge

   Two turbulent regimes: ideal interchange mode at low N and non-flute modes at high N.

   Parameter scans have a crucial role

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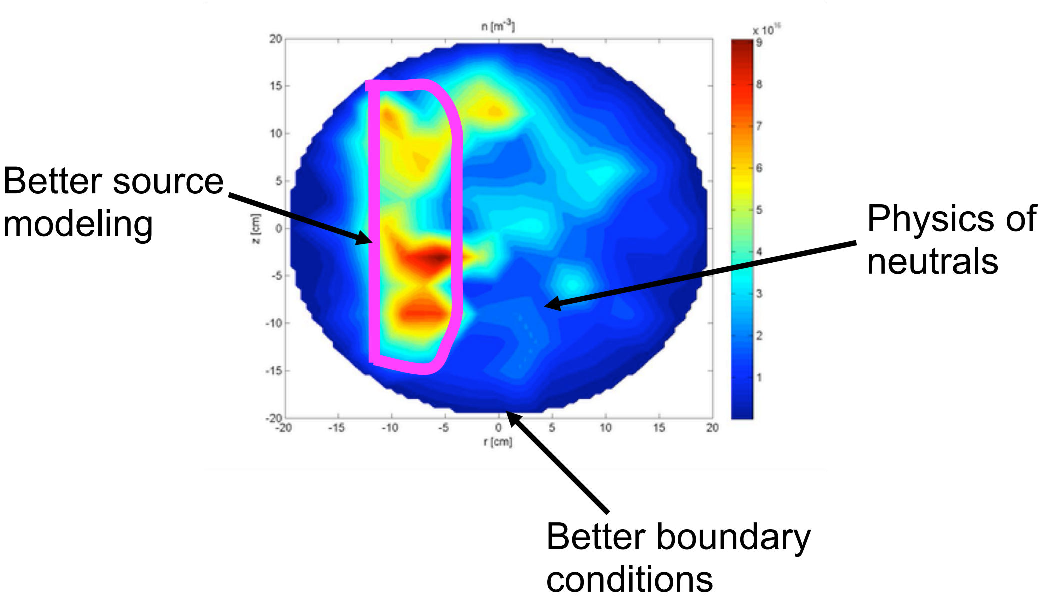
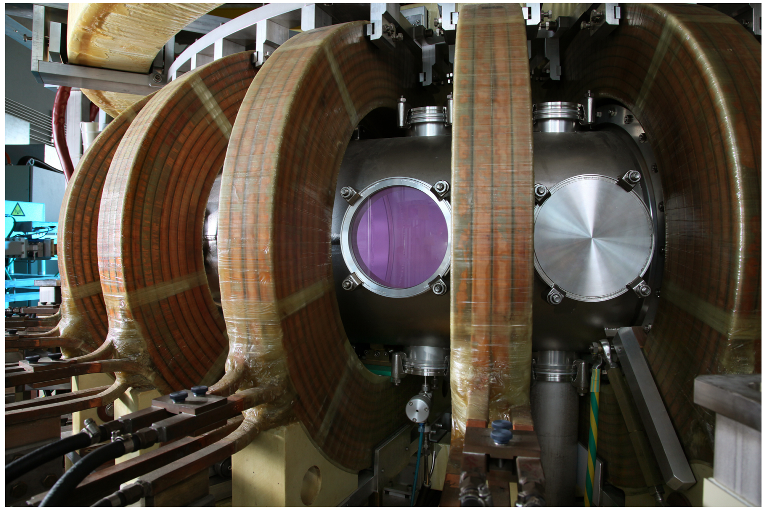
Future work

Missing ingredients for a complete description of plasma dynamics in TORPEX:



Use of more diagnostics: Mach probes, Triple probes or Bdot probes to compare other interesting observables.



V&V

A validation project requires a four step procedure:

(i) Model qualification

(ii) Code verification

(iii) Definition and classification of observables

(iv) Quantification of agreement

$$\frac{\partial n}{\partial t} = R[\phi, n] + 2\left(n\frac{\partial T_e}{\partial y} + T_e\frac{\partial n}{\partial y} - n\frac{\partial \phi}{\partial y}\right) + D_n\nabla_\perp^2 n - n\frac{\partial V_{\|e}}{\partial z} - V_{\|e}\frac{\partial n}{\partial z} + S_n, \quad (1)$$

$$\frac{\partial \nabla_\perp^2 \phi}{\partial t} = R[\phi, \nabla_\perp^2 \phi] - V_{\|i}\frac{\partial \nabla_\perp^2 \phi}{\partial z} + 2\left(\frac{T_e}{n}\frac{\partial n}{\partial y} + \frac{\partial T_e}{\partial y}\right) + \frac{1}{n}\frac{\partial j_\|}{\partial z} - \frac{\eta_{0i}}{n}\left(2\frac{\partial^2 V_{\|i}}{\partial y\,\partial z} + \frac{\partial^2 \phi}{\partial y^2}\right) + D_\phi \nabla_\perp^4 \phi, \quad (2)$$

$$\frac{\partial T_e}{\partial t} = R[\phi, T_e] - V_{\|e}\frac{\partial T_e}{\partial z} + \frac{4}{3}\left(\frac{7}{2}T_e\frac{\partial T_e}{\partial y} + \frac{T_e^2}{n}\frac{\partial n}{\partial y} - T_e\frac{\partial \phi}{\partial y}\right) + D_T\nabla_\perp^2 T_e + \frac{2}{3}\frac{T_e}{n}0.71\frac{\partial j_\|}{\partial z} - \frac{2}{3}T_e\frac{\partial V_{\|e}}{\partial z} + S_T, \quad (3)$$

$$\frac{m_e}{m_i}n\frac{\partial V_{\|e}}{\partial t} = \frac{m_e}{m_i}nR[\phi, V_{\|e}] - \frac{m_e}{m_i}nV_{\|e}\frac{\partial V_{\|e}}{\partial z} - T_e\frac{\partial n}{\partial z} + n\frac{\partial \phi}{\partial z} - 1.71n\frac{\partial T_e}{\partial z} + n\nu j_\| + \frac{4}{3}\eta_{0e}\frac{\partial^2 V_{\|e}}{\partial z^2} + \frac{2}{3}\eta_{0e}\frac{\partial^2 \phi}{\partial y\,\partial z} - \frac{2}{3}\frac{\eta_{0e}}{n}\frac{\partial^2 p_e}{\partial z\,\partial y} + D_{V_e}\nabla_\perp^2 V_{\|e}, \quad (4)$$

$$n\frac{\partial V_{\|i}}{\partial t} = nR[\phi, V_{\|i}] - nV_{\|i}\frac{\partial V_{\|i}}{\partial z} - T_e\frac{\partial n}{\partial z} - n\frac{\partial T_e}{\partial z} + \frac{4}{3}\eta_{0,i}\frac{\partial^2 V_{\|i}}{\partial z^2} + \frac{2}{3}\eta_{0,i}\frac{\partial^2 \phi}{\partial y\,\partial z} + D_{V_i}\nabla_\perp^2 V_{\|i}, \quad (5)$$