

Real-Time Kinetic Hard-Modelling for the Optimisation of Reaction Conditions and the Detection of Process Upset in Semi-Batch Reactors

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Motivation

- **Loss of productivity:** Fluctuations in reaction processes are partly due to variations in the concentration of initial reactants (sub-optimal operating conditions).

Another source of fluctuations comes from impurities present in the initial reactants causing unexpected side reactions.

- **Loss of time:** Initial concentrations are often determined by offline analysis (e.g. HPLC, spectroscopy) and can result in delaying the batch start.

Trends in favour of online Kinetic Hard-Modelling (KHM)

- **Improving knowledge:** Fine chemical industries try to improve manufacturing by elucidating the underlying kinetic model (rate law) of processes whose patents have expired.
- **Multivariate on-line sensors:** Recent progress in Process Analytical Technology (PAT) allows now the monitoring of processes in real time using multivariate probes.

KHM in Research phase

- Kinetic hard-modelling compares a measured signal with a modelled one obtained from a 1st principle hard model (rate law). The residuals are used as driving force for the least-square optimisation of the kinetic parameters.

Hard model = *function* (kinetic parameters, IC, CV, NCV)

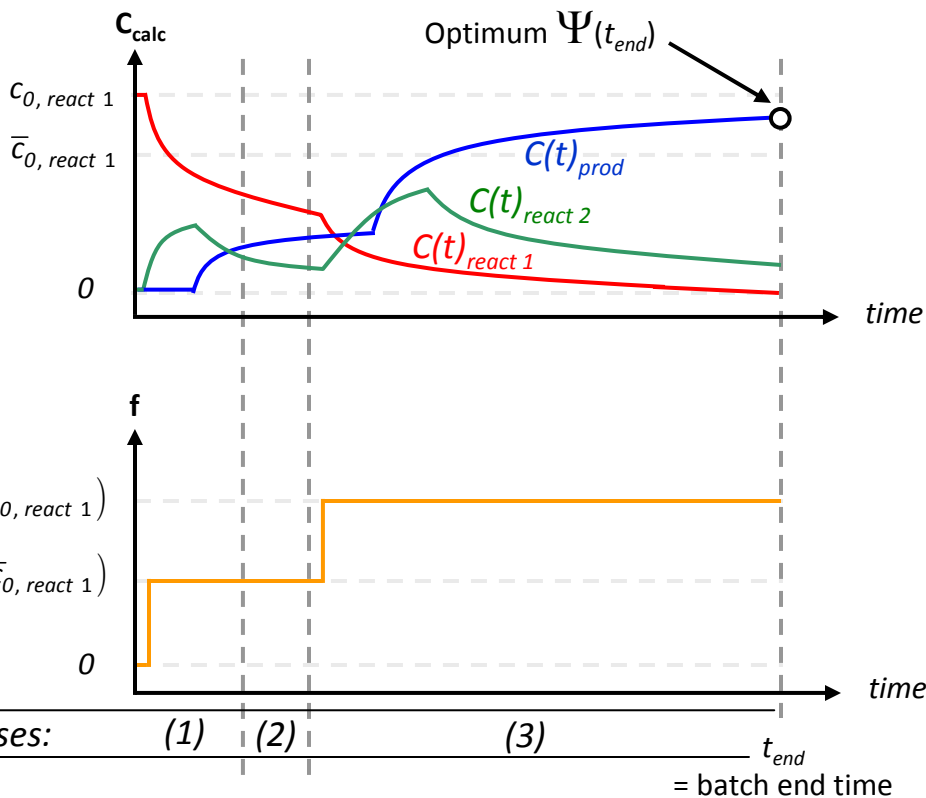
- | | | |
|-------|---|--|
| ■ IC | Initial C onditions | e.g. initial concentrations |
| ■ CV | Control V ariables | e.g. dosing rate, temperature |
| ■ NCV | Non- C ontrolled V ariables | e.g. concentration of the dosing agent |

- Our kinetic hard-modelling approach is a calibration free method in the sense that the calibration (the absorptivity spectra) is nested into the non-linear optimisation and linearly fitted at each iteration.

Online KHM in Production phase

- In production phase, differences between batches result from different IC and/or NCV that can be optimised in a non-linear way, setting the kinetic parameters to the values found during the research phase.
- Subsequently, Control Variables (e.g. dosing flow rate) can be optimised and/or the process can be monitored for detection of possible faults.

Concept of online KHM



$\bar{C}_{0, react\ 1}$ = mean initial concentration,
 $f_{opt}(\bar{C}_{0, react\ 1})$ = optimum dosing rate for $\bar{C}_{0, react\ 1}$

Phase 1: OPTIMISATION OF THE IC/NCV AND PROCESS UPSET DETECTION

Optimisation of IC/NCV (e.g. $C_{0, react\ 1}$ and $C_{dos, react\ 2}$) with kinetic parameters fixed.

Possible Process Fault is detected.

Phase 2: OPTIMISATION OF THE CV

Extrapolation to a future time and optimisation of future **CV** under constraints to maximise Ψ (= Yield, Selectivity or Conversion).

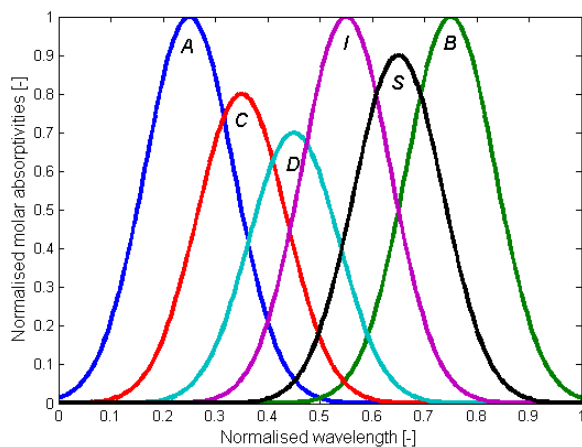
$$\begin{aligned} & \max_{f(t)} \Psi(t_{end}) \\ & \text{s.c. } V(t_{end}) \leq V_{max} \\ & \quad f_{min} \leq f(t) \leq f_{max} \end{aligned}$$

Phase 3: OBSERVATION PHASE

Process running under optimal **CV**.

Kinetic model

Absorptivity spectra



Heat released

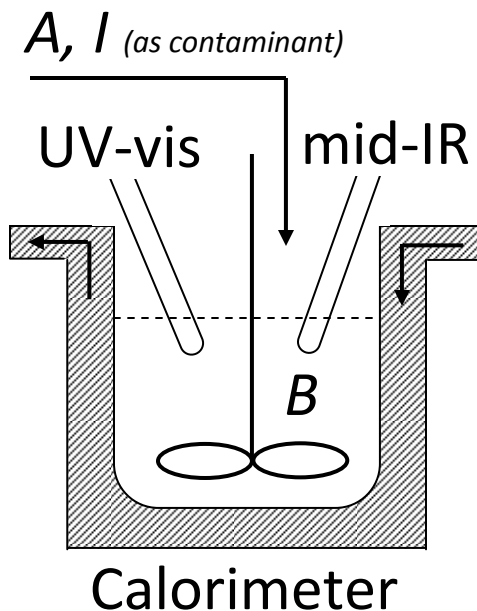
modelled:

$$\Delta H_{r1} = -10.0 \text{ kJmol}^{-1}$$

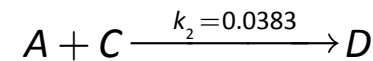
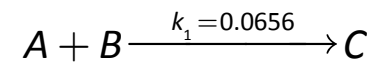
$$\Delta H_{r2} = -5.0 \text{ kJmol}^{-1}$$

unmodelled:

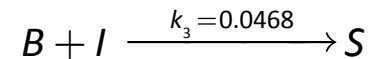
$$\Delta H_{r3} = -10.0 \text{ kJmol}^{-1}$$



modelled:



unmodelled:



A : dosed

C : wanted product

D : side product

I : contaminant in *A*

Base Case simulation

Mean IC / NCV

No process fault

$$\text{IC: } \bar{c}_0 = \begin{matrix} & A & B & C & D & I & S \\ \begin{bmatrix} 0 & 1 & 0 & 0 & 0 & 0 \end{bmatrix} \end{matrix}$$

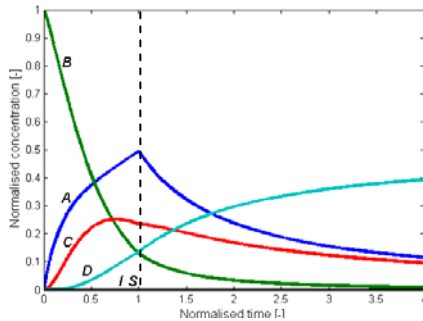
$$\text{NCV: } \bar{c}_{dos} = \begin{matrix} & A & B & C & D & I & S \\ \begin{bmatrix} 2 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \end{matrix}$$

$$f_{opt}(\bar{c}_0, \bar{c}_{dos}) = 0.025$$

Base case

$$\begin{array}{c}
 A \quad B \quad C \quad D \quad I \quad S \\
 IC: \bar{c}_0 = \begin{bmatrix} 0 & 1 & 0 & 0 & 0 & 0 \end{bmatrix} \\
 \\
 A \quad B \quad C \quad D \quad I \quad S \\
 NCV: \bar{c}_{dos} = \begin{bmatrix} 2 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}
 \end{array}$$

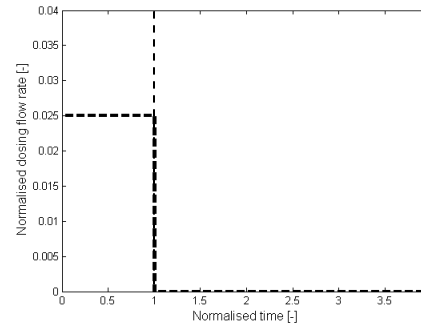
Concentration profiles



$$V_0 = 0.3, V_{end} = 0.6 \quad (V_{max} = 1)$$

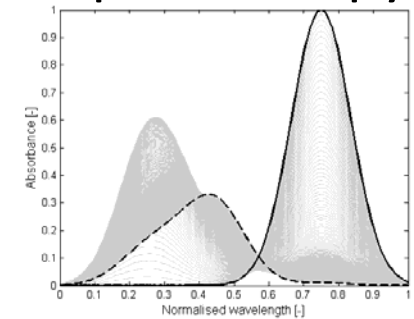
Time normalised to normal batch duration
(1: one normal batch duration)

Dosing rate (a CV)



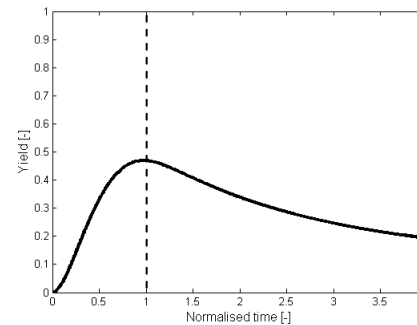
$$f_{opt}(\bar{c}_0, \bar{c}_{dos}) = 0.025 \quad (f_{max} = 1)$$

Spectroscopy



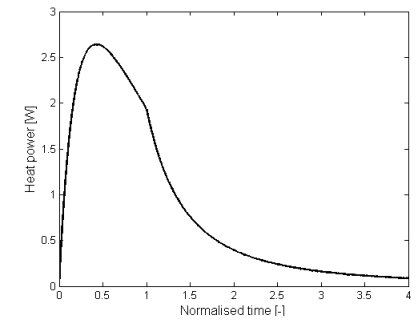
Added noise: 10^{-4}

$\Psi = \text{Yield}$



$$\Psi(t_{end}) = \text{Yield}_{C/A, opt}(\bar{c}_0, \bar{c}_{dos}) = 46.98\%$$

Calorimetry



Added noise: 10^{-3}

Optimisation of the Initial **IC** and Non-Controlled **Variables (NCV)**

and subsequent optimisation of the
Control Variables (CV)

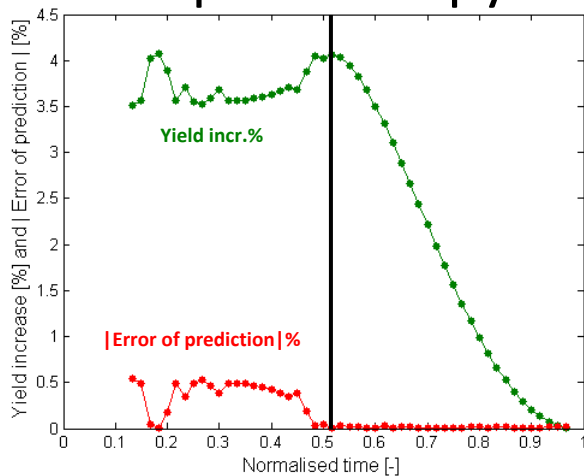
$$\text{IC: } \bar{c}_0 - 15\% = \begin{matrix} & A & B & C & D & I & S \\ \begin{bmatrix} 0 & 0.85 & 0 & 0 & 0 & 0 \end{bmatrix} \end{matrix}$$

$$\text{NCV: } \bar{c}_{dos} + 15\% = \begin{matrix} & A & B & C & D & I & S \\ \begin{bmatrix} 2.30 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \end{matrix}$$

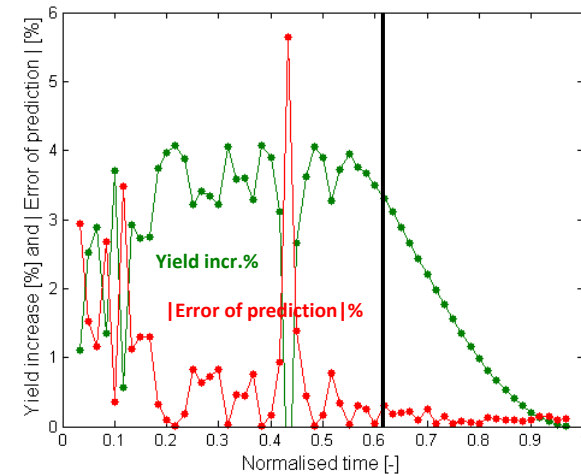
$$f_{opt}(\bar{c}_0 - 15\%, \bar{c}_{dos} + 15\%) = ?$$

Optimisation of the Control Variables (CV)

Spectroscopy



Calorimetry



	UV-vis	Calorimetry
Time of calculation	0.516	0.616
σ_p/p	$\leq 0.20\%$	$\leq 1.70\%$
Calculated dosing rate	0	0
Yield increase	+4.05%	+3.30%
Maximum Yield increase	+4.08%	+4.08%

Extrapolation time = 0.0167

CV optimisation and comparison with offline analysis

<i>IC</i>	<i>NCV</i>	Signal	Yield increase	Error of prediction	Time criterion for online KHM to be more efficient than offline analysis
0% (base case)	0% (base case)	Spectroscopy	0.09%	+0.00%	always
		Calorimetry	0.09%	+0.00%	always
		Offline	0.09%	-	-
-15%	+15%	Spectroscopy	4.05%	+0.02%	0.02%
		Calorimetry	3.30%	+0.30%	0.75%
		Offline	4.08%	-	-
-30%	+30%	Spectroscopy	11.06%	+0.15%	3.30%
		Calorimetry	8.47%	+0.45%	5.76%
		Offline	14.72%	-	-

Optimisation of the CV

- For this particular mechanism and these pure component spectra, spectroscopy can be used to optimise online the CV.
- Due to its univariate nature, **calorimetry** produces a low improvement in yield when used in online KHM.
- For **extreme variations in the IC/NCV**, online KHM is only better than offline analysis if the time required for the offline analysis largely delays the batch start.
- For this particular mechanism, the concentration of the dosing agent has the most impact on the yield.

Process Fault Detection (PFD) or Process Upset Detection

$$\text{IC: } \bar{c}_0 = \begin{matrix} & A & B & C & D & I & S \\ \begin{bmatrix} 0 & 1 & 0 & 0 & 0 & 0 \end{bmatrix} \end{matrix}$$

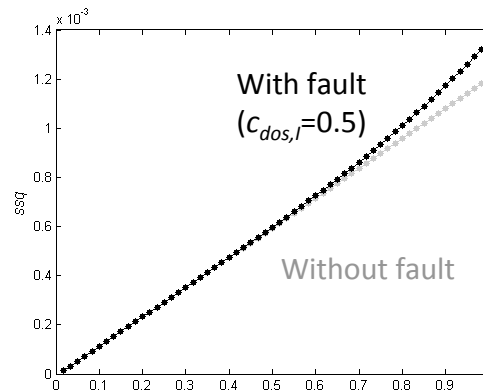
$$\text{NCV: } \bar{c}_{dos} + I = \begin{matrix} & A & B & C & D & I & S \\ \begin{bmatrix} 2 & 0 & 0 & 0 & c_{dos,I} & 0 \end{bmatrix} \end{matrix}$$

$$f_{opt}(\bar{c}_0, \bar{c}_{dos}) = 0.025$$

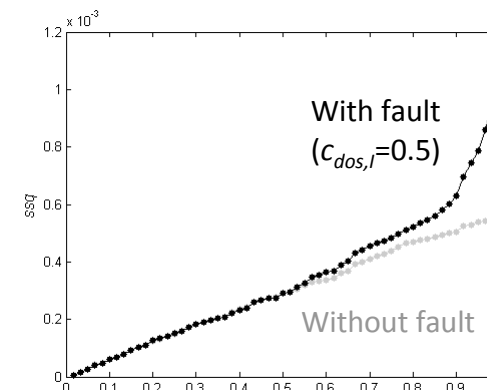
SSQ and Standard deviation of the residuals as Process Fault indicators

ssq

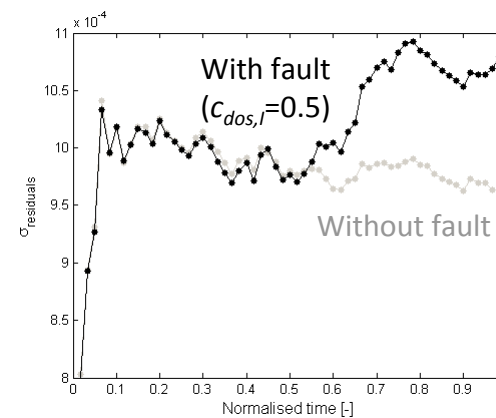
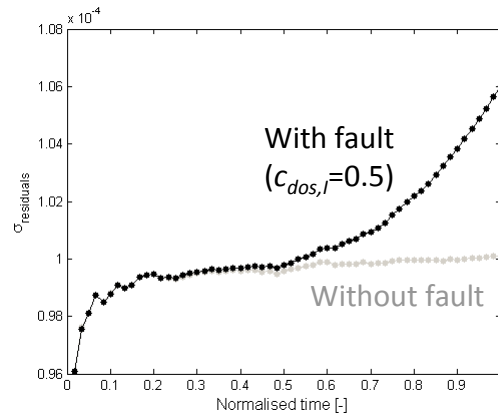
Spectroscopy



Calorimetry

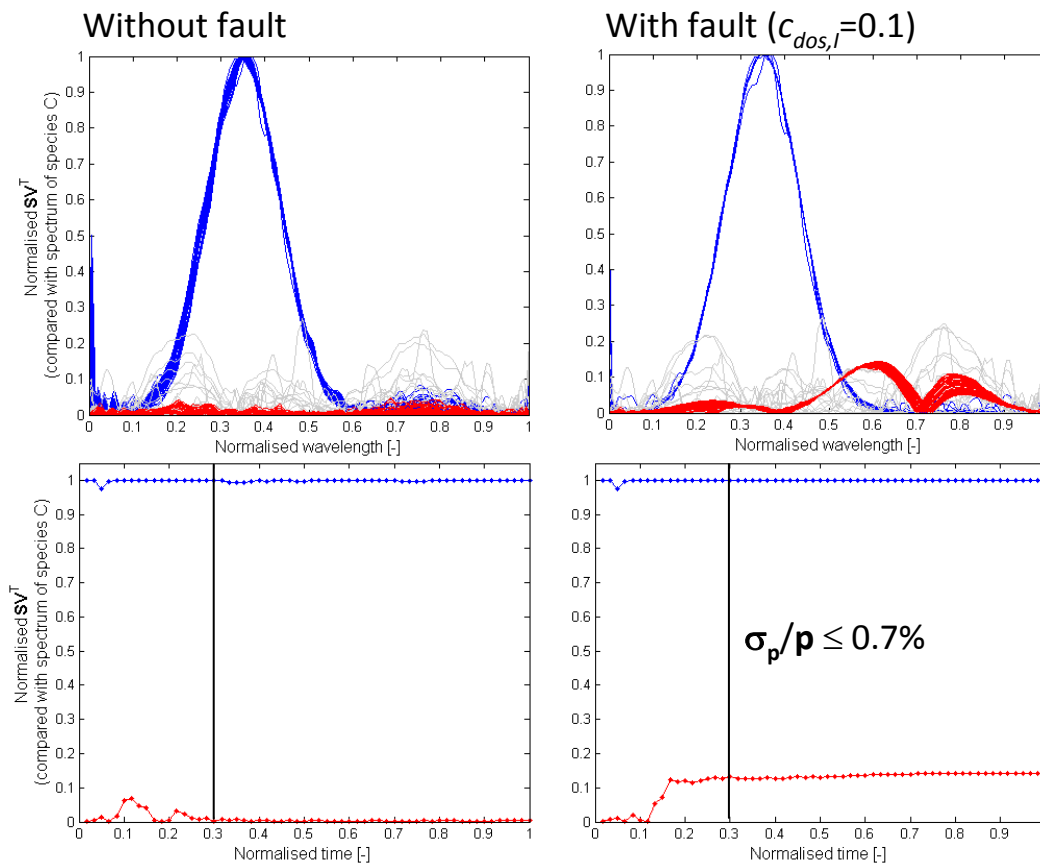


$\sigma_{residuals}$

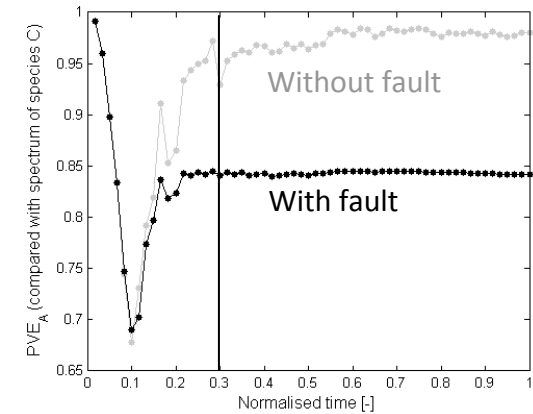


Known absorptivity spectra (in eigen-space) as Process Fault indicators

\mathbf{SV}^T (benchmark: spectrum of C)

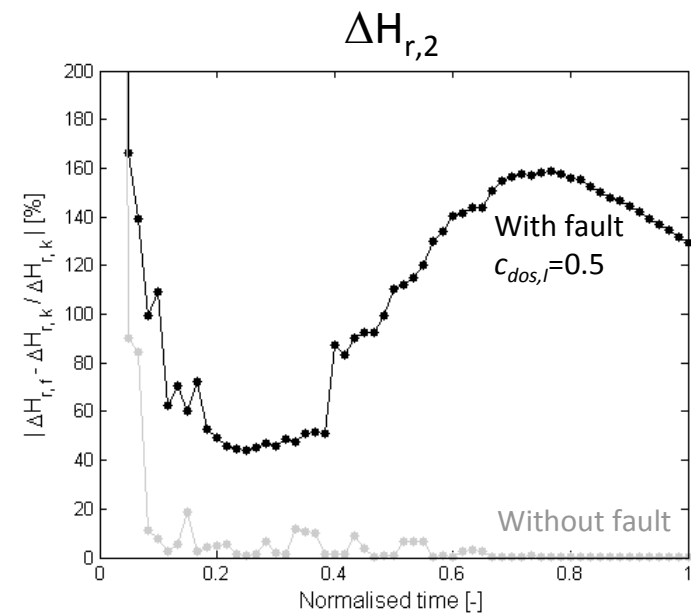
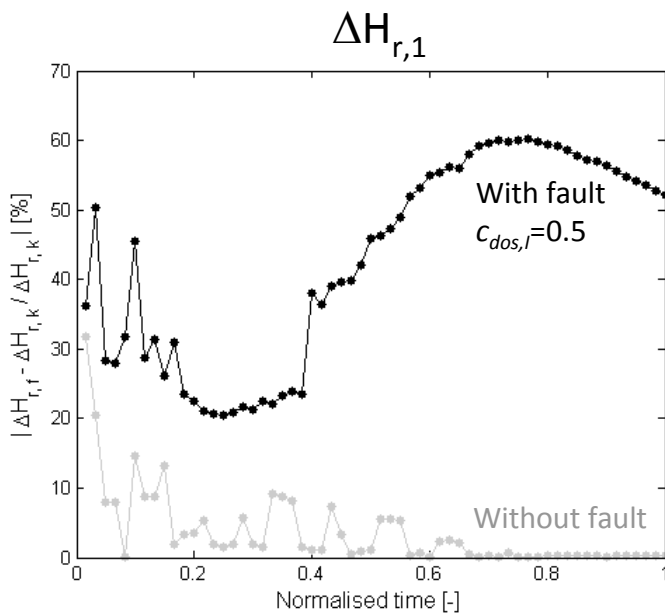


PVE_A



Spectrum selected for PFD	PVE_A at t_{end}	
	With fault	Without fault
Spectrum of A	85.51%	98.68%
Spectrum of B	98.50%	99.47%
Spectrum of C	78.33%	97.57%
Spectrum of D	69.82%	96.62%

Known reaction enthalpies as Process Fault indicator



Process Fault Detection

- Spectroscopy and calorimetry can be used to detect Process Faults
- The best process fault indicators are generally the ones based on a priori information, i.e. the absorptivity spectra and the reaction enthalpies

Conclusion

- The capabilities of online KHM have been demonstrated by:
 - Optimisation of the Initial Conditions (IC) and Non-Controlled Variables (NCV)
 - Subsequent optimisation of the Control Variables (CV)
 - And constant Detection of possible Process Faults (PFD)
- Next, online KHM will be applied on experimental data for a simple chemical system.

A blue-tinted banner image at the top of the slide showing a large, domed building, likely a part of the ETH Zurich campus, with mountains in the background.

**Thank you for
your attention**