





# High-aspect-ratio, ultrathick, negative-tone near-UV photoresist and its applications for MEMS

H. Lorenz a,\*, M. Despont b, N. Fahrni a, J. Brugger b, P. Vettiger b, P. Renaud a

<sup>a</sup> Swiss Federal Institute of Technology (EPFL), DMT-IMS, CH-1015 Lausanne, Switzerland <sup>b</sup> IBM Research Division, Zurich Research Laboratory, CH-8803 Rüschlikon, Zurich, Switzerland

#### Abstract

Detailed investigations of the limits of a new negative-tone near-UV resist (IBM SU-8) have been performed. SU-8 is an epoxy-based resist designed specifically for ultrathick, high-aspect-ratio MEMS-type applications. We have demonstrated that with single-layer coatings, thicknesses of more than 500  $\mu$ m can be achieved reproducibly. Thicker resist layers can be made by applying multiple coatings, and we have achieved exposures in 1200  $\mu$ m thick, double-coated SU-8 resist layers. We have found that the aspect ratio for near-UV (400 nm) exposed and developed structures can be greater than 18 and remains constant in the thickness range between 80 and 1200  $\mu$ m. Vertical sidewall profiles result in good dimensional control over the entire resist thickness. To our knowledge, this is the highest aspect ratio reported for near-UV exposures and the given range of resist thicknesses. These results will open up new possibilities for low-cost LIGA-type processes for MEMS applications. The application potential of SU-8 is demonstrated by several examples of devices and structures fabricated by electroplating and photoplastic techniques. The latter is especially interesting as SU-8 has attractive mechanical properties. © 1998 Elsevier Science S.A.

Keywords: High aspect ratio; Negative tone; Near-UV photoresists; LIGA-type applications; Electroplating; Photoplastic

#### 1. Introduction

The presence of high aspect ratios in very thick resists is not only interesting, it is often a requirement for fabricating micromechanical structures for MEMS or packaging applications. It allows vertical sidewalls of tall structures to be achieved with good dimensional control over the entire height. A well-known example is the Lithography, Galvanoforming, and Abformung process called LIGA [1], which makes use of X-ray lithography to pattern very thick PMMA (polymethylmethacrylate) layers used as templates for electroforming devices or shims for subsequent replication steps. X-ray lithography is an ideal technique for achieving highaspect-ratio structures with submicron resolution in very thick resists because it features reduced diffraction, low resist absorption and minimal proximity effects due to the absence of scattering. It has been demonstrated in many publications and by several groups that high-quality, X-ray-exposed PMMA structures can be used as templates and shims for large-scale reproduction with submicron resolution in very thick layers with very good dimensional control over the entire structure height [2-5]. However, the cost of X-ray LIGA-type fabrication is greatly influenced by the expensive X-ray source (synchrotron radiation) and the demanding mask technology. Of course, the cost factor is less severe if very large volumes are mass produced using low-cost replication techniques.

A substantial fraction of MEMS applications do not require submicron resolution, hence it would be very attractive if near-UV resists were available that have lower resolution (microns to tens of microns) and lower aspect ratios but otherwise have characteristics similar to PMMA/X-ray. Such an optical-lithography-based LIGA process technique would have great potential for low-cost MEMS fabrication. IBM [6,7] has recently announced a new resist (SU-8) that has the potential to fulfil the above profile. We have explored the limits of SU-8 in terms of its aspect ratio, resist thickness, and applicability to MEMS [8].

#### 2. SU-8 resist properties and process

SU-8 is a negative, epoxy-type, near-UV photoresist based on EPON SU-8 resin (from Shell Chemical). The resist has been specifically developed for applications requiring high aspect ratios in very thick layers [9]. The key property that

<sup>\*</sup> Corresponding author. Tel.: +41 21 693 58 51.

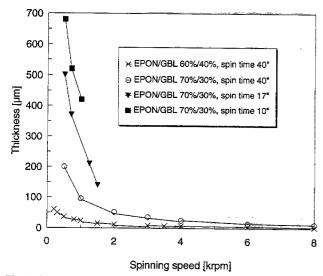


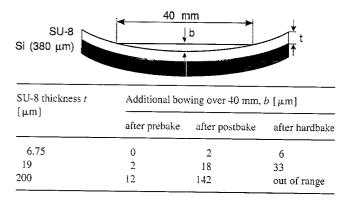
Fig. 1. SU-8 achievable thicknesses vs. spinning speed, dilution rate and spinning time. EPON/GBL dilution of 70%/30% covers thicknesses from 12 to 680  $\mu$ m by single-spin coating on a 3 inch silicon wafer. From [10], © 1997 IEEE.

makes the SU-8 so attractive for ultrathick resist applications is its very low optical absorption in the near-UV range. This leads to a relatively good exposure dose uniformly over the entire resist thickness, which gives rise to vertical sidewall profiles and hence good dimensional control over the entire structure height.

The photoresist is prepared from commercially available components by dissolving an EPON resin SU-8 in an organic solvent GBL (gamma-butyrolacton). The quantity of the solvent determines the viscosity and hence the range of the possible resist thicknesses. Last, the photoinitiator, a triaryl sulfonium salt (10% of the EPON SU-8 weight), is mixed with the resin. Fig. 1 shows the dependence of the resist thickness on the spinning speed. The resist is spun at low speed for a very short time using a conventional spin coater. Resist thicknesses up to 700 µm have been achieved with very good reproducibility by a single spinning of a viscous SU-8 dilution (70% of EPON SU-8) at a speed of 500 rpm for 10 s. Much greater thicknesses can be achieved by multiple coatings; we have demonstrated SU-8 thicknesses of 1200 µm made by double coatings. An additional advantage of SU-8 is its capability to self-planarize during prebake and hence to eliminate the edge-bead effect, which results in good contact between mask and resist in contact lithography.

Substrate/wafer stress due to thick resist coatings is a key issue for many applications. After prebake, a small tensile stress is introduced by the difference between the thermal expansion coefficients (TECs) of the wafer and SU-8. The stress is small because during the cooling phase of the prebake, polymer chain rearrangements take place in the resists that are not crosslinked. The resulting slight bowing of the wafer is very advantageous for contact-printing lithography because good mask/wafer contact is ensured. As we are working with resist thicknesses comparable to the wafer thickness, this stress can be high and consequently the wafer

Table I Wafer bowing due to the stress induced by the SU-8 layer. The bowing was measured over a 40 mm distance of a fully exposed 3 inch, 380  $\mu$ m thick silicon wafer. From [10], © 1997 IEEE



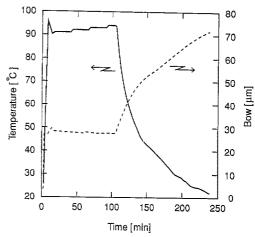


Fig. 2. Wafer bowing due to SU-8 stress as a function of postbake temperature and time: wafer thickness, 300  $\mu$ m; SU-8 thickness, 80  $\mu$ m; solid line, temperature; dashed line, wafer bow.

is bowed. Table 1 lists the measured bowing of a Si wafer coated with three different SU-8 thicknesses after pre-, post-and hardbaking.

The main stress is generated as the crosslinked SU-8 cools down. The greater bowing measured after hardbake (Table 1, see also Ref. [10]) is due to the higher baking temperature (200°C). However, it is important to note that for most applications, hardbaking is not required; hence the subsequent discussion will deal only with postbaking. In addition to the thermomechanical stress introduced by the difference of the TECs, stress due to resist polymerization is also present. Fig. 2 shows the evolution of wafer bowing during polymerization and cooling of a 3 inch, 300 µm thick Si wafer coated with a 80  $\mu m$  thick SU-8 layer. It clearly demonstrates that bowing (stress) is introduced mainly during the cooling phase (for details, see Ref. [11]). The influence of the illuminated (polymerized) area on wafer bowing is shown in Table 2. It shows that wafer bowing is strongly influenced by the illuminated (crosslinked) area. The illuminated area has been defined by exposed and developed areas of 1 cm  $\times$  1 cm, which are uniformly distributed over the wafer surface to

Table 2 Wafer bowing due to the stress induced by a 200  $\mu$ m thick SU-8 layer. The bowing was measured over a 40 mm distance on three 3 inch, 380  $\mu$ m thick silicon wafers

% of illuminated area	Additional bowing over 40 mm, b [μm]		
	after prebake	after postbake	
30	4.45	82.1	
60	5.2	115.5	
100	12	142	

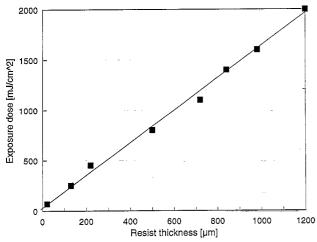


Fig. 3. Exposure dose vs. the SU-8 thickness. From [10], © 1997 IEEE.

achieve the 30 and 60% illuminated and polymerized area. The data in Table 2 are for a 3 inch, 380  $\mu$ m thick Si wafer coated with a 200  $\mu$ m thick SU-8 layer. Stress/bowing analysis for arbitrary shapes and areal coverage are currently being investigated, but in summary, the bowing (stress) of an SU-8-coated wafer can be lowered (i) by reducing the postbake temperature at the expense of baking time, (ii) by an appropriate mask design to reduce the illuminated area, and (iii) by choosing substrates that are a better thermal match for SU-8.

The spin coating, exposure and development process for a single-layer resist of 500  $\mu$ m thickness is as follows:

- (i) low-speed, short-time spinning (500 rpm for 17 s) with conventional spinner,
- (ii) 3 h resist baking at 95°C on levelled hot plate,
- (iii) near-UV (400 nm) exposure with contact mask aligner (800 mJ cm $^{-2}$ ),
- (iv) 95°C postbake on level hot plate for 30 min,
- (v) development in PGMEA (propylene glycol methyl ether acetate) for 30 min,
- (vi) if necessary, hardbaking at 200°C for 30 min.

For multilayer coatings, steps 1 and 2 are repeated for each layer before exposure and development. The required exposure dose as a function of the SU-8 thickness is shown in Fig. 3. Stripping can be done either in hot 1-methyl-2-pyrrolidinone (NMP), some acid solutions, such as  $\rm H_2SO_4/H_2O_2$  or fuming HNO<sub>3</sub>, and/or by  $\rm O_2$  ashing.

### 3. Exposure results

All our exposure tests have been performed on SUSS M4A and MJB21 mask aligners in contact mode at 400 nm exposure wavelength. Figs. 4–6 demonstrate the SU-8 capabilities for resist thicknesses of 270, 500 and 1200 µm, respectively.

A small degree of non-verticality is noticeable. For instance, the structures shown in Fig. 6 have a top and bottom width of 65 and 45  $\mu m$ , respectively, in a 1200  $\mu m$  thick resist from a mask width of 60  $\mu m$ . This difference is due to the energy loss by absorption and spreading in the SU-8 layer. This can be minimized by increasing the dose and decreasing the mask width to compensate for overexposure effects. Nevertheless, the ability to structure such fine lines in such a thick layer demonstrates the very low absorption of SU-8. Fig. 7 shows a scanning electron microscopy (SEM) cross section through holes of different widths in a 730  $\mu m$  thick SU-8 structure. The smallest fully developed structure has a width of 43  $\mu m$ , resulting in an aspect ratio of 17. Our investigations of resist thicknesses between 80 and 1200  $\mu m$  revealed that aspect ratios up to 18 can be achieved reproducibly. Some-

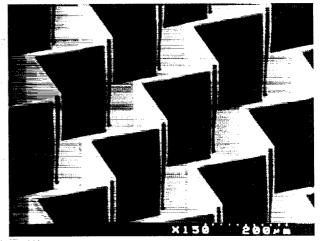


Fig. 4. SEM image of 270  $\mu$ m thick structures in SU-8 with a width of 16  $\mu$ m, resulting in an aspect ratio of 17 (single-spin coated). From [10], © 1997 IEEE.

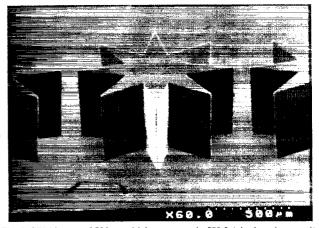


Fig. 5. SEM image of 500  $\mu$ m thick structures in SU-8 (single-spin coated). From [10], © 1997 IEEE.

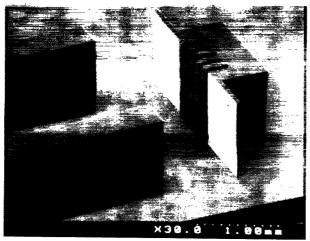


Fig. 6. SEM image of 1200  $\mu$ m thick structures in SU-8 with a line width of 65  $\mu$ m, resulting in an aspect ratio of 18 (double-spin coated). From [10], © 1997 IEEE.

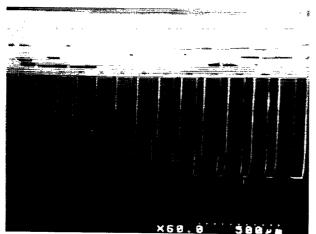


Fig. 7. SEM image of 730  $\mu m$  thick structures in SU-8 showing the actual trench width limit. The smallest completely developed structure has a width of 43  $\mu m$ , resulting in an aspect ratio of 17 (double-spin coated). From [10], © 1997 IEEE.

times a slight bending at the bottom of small trenches (as in Fig. 7) or pillows have been noticed. Such bendings can be eliminated by increasing the exposure dose and by postbaking first at  $50^{\circ}$ C before the final postbaking at  $95^{\circ}$ C.

All results reported here are based on standard dipping techniques for developing the exposed SU-8. We found a limitation to developing narrow openings (smaller than 4  $\mu m$ ), which is due to the difficulty of refreshing the developer in these small and deep holes. For that purpose other techniques such as spray developing or megasonic bath agitation may be necessary. The exposed material is highly crosslinked, resulting in a very low dilution rate in the developer. This is crucial because the developing step takes about 1 h for a 1200  $\mu m$  thick resist. It is also important to note that the developed structures are free of residues.

These results demonstrate the best capabilities known for near-UV exposed resists in terms of thickness and aspect ratio.

# 4. MEMS applications of SU-8

Given the capabilities of SU-8, the application scenery is very similar to X-ray-based LIGA but of course with reduced resolution and aspect ratio. On the other hand, all applications not requiring ultrahigh resolution can be done well at very low cost. Currently, we believe that the interest in MEMS-type applications within the capabilities of SU-8 is high.

In the following, we shall present a few application examples of SU-8 for MEMS fabrication in the areas of electroplating, injection moulding and photoplastic devices [12].

#### 4.1. Electroplating

The SU-8 fulfils the requirements placed on a mould for electroplating various devices such as gears and coils [7,8]. Fig. 8 shows an example of an electroplated Cu coil, which can generate very localized and high magnetic fields. This example by no means reflects the limits of SU-8 in terms of thickness and aspect ratio but demonstrates its capabilities as an electroplating mould.

The potential of fabricating metallic mechanical structures with SU-8 electroplating masks is demonstrated by the flexible gear shown in Fig. 9. The flexible gear shape has been exposed and developed in a 200  $\mu m$  thick SU-8 layer, which was spin-coated onto a Si wafer with an Al sacrificial (200 nm) and a Au (30 nm) seed layer on top. Afterwards, the flexible gear was electroplated in a Ni bath and lifted off by diluted KOH, the Au seed layer being removed simultaneously. The springs connecting the outer ring with the inner axle ring are 50  $\mu m$  wide.

# 4.2. Photoplastic and plastic injection moulding

In addition, we have explored EPON SU-8 material not only for masking and pattern-transfer applications but also as a photoplastic material to fabricate micromechanical components. Photoplastic material means that the components are

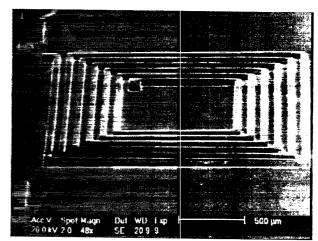


Fig. 8. SEM image of copper coil electroplated using an SU-8 mask. The coil pitch is 50  $\mu$ m, the copper wires are 40  $\mu$ m high and 25  $\mu$ m wide. From [10], © 1997 IEEE.



Fig. 9. Electroplated, flexible Ni gear (diameter = 5 mm, thickness =  $200 \mu m$ ).

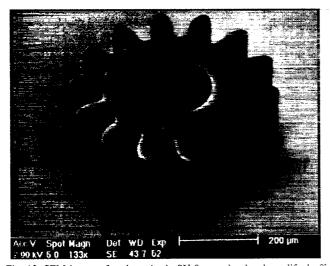


Fig. 10. SEM image of a photoplastic SU-8 gear that has been lifted off (diameter =  $530 \mu m$ , thickness =  $200 \mu m$ ).

made of EPON SU-8 in only one or two process steps [12]. Preliminary investigations have shown that EPON SU-8 has interesting mechanical properties that make it attractive for applications as a photoplastic material.

Fig. 10 demonstrates the capabilities of SU-8 as a photoplastic material to fabricate gears. Sacrificial-layertechniques have been used to release the photoplastic components from the wafer after exposure and development. For this purpose the wafer was coated with a 200 nm thick layer of Al prior to spin coating the SU-8. After exposure and development, the Al sacrificial layer is removed in an Al etchant (KOH 40 wt.%) in order to release the structures. Sacrificial-layer etching takes place at a high rate, allowing large structures to be lifted off within a short time and without corroding the EPON SU-8. The gear shown in Fig. 10 has a diameter of 530  $\mu m$  and a thickness of 200  $\mu m$ .

As SU-8 is a negative-tone resist, it opens up interesting possibilities for the fabrication of three-dimensional struc-

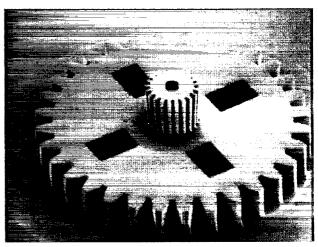


Fig. 11. Two-level photoplastic gear.

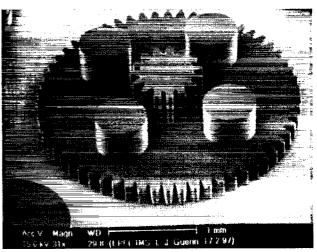


Fig. 12. Two-level photoplastic SU-8 structure as basis for micromould fabrication.

tures by multiple spin coatings and exposures [13]. This feature is more difficult to achieve with positive-type X-ray LIGA. Fig. 11 shows an example of a two-level SU-8 structure. The first level defines a big wheel, whereas the well-aligned second level forms the pinion.

These photoplastic structures are also the basis for fabricating metallic moulds for plastic injection moulding. We made metallic moulds by starting with a photoplastic multilayer structure as shown in Fig. 12. While the structure is still on the wafer, it is completely covered with an evaporated thin metal layer (Cr/Au). The subsequent Ni electroplating forms the negative metallic structure of the photoplastic. The final injection mould is made by double-sided mechanical polishing and photoplastic stripping. Fig. 13 shows the magnified section of the pinion structure in the Ni mould. The pinion diameter is 853  $\mu$ m, and the Ni mould is 450  $\mu$ m thick. This Ni mould is now used to fabricate low-cost plastic watch microparts by injection moluding. This mould-fabrication technique is an interesting alternative to today's wire electric-discharge techniques for fabricating micromoulds.

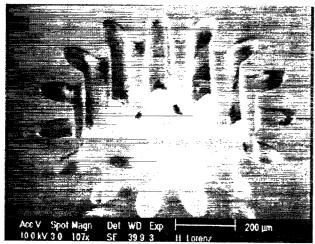


Fig. 13. Magnified view of the pinion area of the Ni micromould. (diameter = 853  $\mu m$ , thickness = 450  $\mu m$ ).

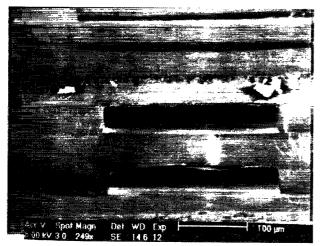


Fig. 14. Cross section of an SU-8 two-level fluidics microchannel.

### 4.3. Other applications

The high thermal stability ( $T_{\rm g} > 200^{\circ}{\rm C}$  for the crosslinked material) of SU-8 allows it to be used as a stable mask for deep silicon reactive ion etching (DRIE) [7]. Another interesting application of SU-8 multiple structures is the fabrication of embedded microchannels for microfluidic devices. The use of SU-8 as a photoplastic allows the fabrication of monolithic auto-assembled channels for microfluidid applications. Various techniques have been developed to obtain single or multi-level microchannels. Details about the microchannel application of SU-8 are described in Ref. [14]. Fig. 14 shows a cross section of a two-level fluidics device made of SU-8.

# 5. Summary and conclusions

We have explored the limits and applications of the EPON SU-8 near-UV photoresist for high-aspect-ratio, MEMS-type component fabrication. To our knowledge, this is the first

demonstration of near-UV exposed and developed photoresist structures up to 1200 µm thick and having an aspect ratio of greater than 18. We believe that we have not yet reached the limit of thickness, whereas the aspect ratio seems to remain constant for the thickness range we have investigated (80-1200 μm). This has been found for dipping development; other development techniques such as spraying may increase the aspect ratio. The outstanding performance concerning SU-8's aspect ratio and thickness is predominately determined by the very low optical absorption in the near-UV range. As a result of this, the structures also show very vertical sidewall profiles, which are essential for good dimensional control in all three dimensions. Pattern-transfer investigations by electroplating and injection moulding confirmed the potential of SU-8 for LIGA-type device fabrication. We consider SU-8 a very attractive material for fabricating photoplastic micromechanical components because of its interesting mechanical properties and its low fabrication process costs. In conclusion, SU-8 has demonstrated outstanding performance for applications as a masking layer for pattern transfer by etching and plating, as well as being a new material for photoplastic device fabrication. Moreover, the use of standard UV photolithography provides the basis for very lowcost mass production of MEMS-type components and systems.

#### Acknowledgements

We thank N. LaBianca, J.D. Gelorme and J. Shaw of the IBM T.J. Watson Research Center, Yorktown Heights, for introducing us to the SU-8 technique as well as for much useful advice and many discussions. We are also pleased to acknowledge the contributions of and discussions with our colleagues C. Andreoli, H. Biebuyck, U. Drechsler, A. Gasser, L. Guérin, F. Marinelli, H. Richard and H. Rothuizen.

#### References

- [1] E.W. Becker, W. Ehrfeld, P. Hagmann, A. Maner and D. Münchmeyer, Fabrication of microstructures with high aspect ratios and great structural heights by synchrotron radiation lithography, galvanoforming, and plastic moulding (LIGA process), Microelectron. Eng., 4 (1986) 35.
- [2] W. Menz, W. Bacher, M. Harmening and A. Michel, The LIGA technique — a novel concept for microstructures and the combination with Si-technologies by injection molding, Proc. IEEE Micro Electro Mechanical Systems, Nara, Japan, 1991, pp. 69–73.
- [3] H. Guckel, K.J. Skrobis, T.R. Christenson, J. Klein, S. Han, B. Choi and E.G. Lovell. Fabrication of assembled micromechanical components via deep x-ray lithography, Proc. IEEE Micro Electro Mechanical Systems, Nara, Japan, 1991, pp. 74–79.
- [4] M. Harmening, W. Bacher, P. Bley, A. Kholi, H. Kalb, B. Kowanz, A. Michel and J. Mohr, Molding of three-dimensional microstructures by the LIGA process. Proc. IEEE Micro Electro Mechanical Systems '92, Travemunde, Germany, Feb. 1992, pp. 202–207.
- [5] M.W. Börner, M. Kohl, F.L. Pantenburg, W. Bacher, H. Hein and W.K. Schomburg, Sub-micron LIGA process for movable microstructures, Microelectron. Eng., 30 (1996) 505–508.

- [6] IBM Corp., US Patent No. 4 882 245 (1989).
- [7] K.Y. Lee et al., Micromachining applications of a high resolution ultrathick photoresist, J. Vac. Sci. Technol. B, 13 (1995) 3012–3016.
- [8] H. Lorenz, M. Despont, N. Fahrni, N. LaBianca, P. Renaud and P. Vettiger, SU-8: a low-cost negative resist for MEMS, J. Micromech. Microeng., 7 (1997) 121-124.
- [9] N. LaBianca and J.D. Gelorme, Epoxies: lithographic resists for thick film applications, Proc. SPIE, Vol. 2438, Ellenville Conf., Nov. 1994, pp. 846–849.
- [10] M. Despont, H. Lorenz, N. Fahrni, J. Brugger, P. Renaud and P. Vettiger, High-aspect-ratio, ultrathick, negative-tone near-UV photoresist for MEMS applications, Proc. 10th IEEE Int. Workshop Micro Electro Mechanical Systems (MEMS '97), Nagoya, Japan, Jan. 1997, pp. 518–522.
- [11] P. Sarbach, L. Guérin, A. Weber, M. Dutoir and P. Clot, Stress analysis and reliability of chip on board technology, Proc. 15th IEEE Int. Manufacturing Technol. Symp., Denver, CO, USA, Oct. 1993, pp. 82– 86.
- [12] H. Lorenz, N. Fahrni, P. Renaud and P. Vettiger, Photoplastic micromechanical components fabricated using optical lithography and sacrificial-layer-lift-off technique, Proc. High Aspect Ratio Micro Structure Technology (HARMST) Forum, Madison, WI, USA, June 1997, pp. 27–28.
- [13] Swiss Federal Institute of Technology, Lausanne, Patent pending, No. FR 96 16130 (1996).
- [14] L.J. Guérin, M. Bossel, M. Demierre, S. Calmes and Ph. Renaud, Simple and low cost fabrication of embedded micro-channels by using a new thick-film photoplastic, Proc. Transducers '97, Chicago, IL, USA, June 1997, Elsevier Science, 1997, pp. 1419–1422.