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Thermodynamic Properties of n-Propyl Alcohol

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Thermodynamic Properties of *n*-Propyl Alcohol

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VARIOUS USES of *n*-propyl alcohol as a solvent and chemical intermediate prompted a study of its derived thermodynamic properties. Sufficient volumetric, thermal, and vapor pressure data are available in the literature to evaluate these properties from 77° to 540° F. and pressures up to 700 p.s.i.a.

Extensive measurements of the volumetric behavior of *n*-propyl alcohol were made by Ramsey and Young (6) over the range from 30° to 263.6° C. and pressures from 800 to 53,480 mm. of mercury. Foz Gazulla, Morcillo, and Mendes (2) measured vapor densities in the low pressure range from 100 to 760 mm. of mercury and the temperature range from 75° to 130° C. Saturated vapor and liquid densities were reported by Young (11).

The vapor pressure-temperature data for *n*-propyl alcohol have been summarized by Stull (9).

The heat capacity data at zero pressure, calculated from spectroscopic measurements and reported by Kobe, Harrison, and Pennington (4), compare favorably with the calorimetric data of Sinke and De Vries (8).

Calorimetric measurements of the heat of vaporization of *n*-propyl alcohol were reported by Bennewitz and Rossner (1). The normal boiling point data and the heat of vaporization at the normal boiling point were summarized in International Critical Tables (3).

The critical constants $T_c = 537.3^\circ \text{K}$., $P_c = 50.2 \text{ atm}$., and $V_c = 220 \text{ cc./gram mole}$ are reported by Lyderson, Greenkorn, and Hougen (5) and these values were used in this work. The molecular weight of *n*-propyl alcohol used in all the calculation in this work was 60.09. The calculations were based on 1 pound of *n*-propyl alcohol, and the enthalpy and entropy were set equal to zero at 77° F. for the saturated liquid at its vapor pressure.

VAPOR PRESSURE AND HEATS OF VAPORIZATION

The vapor pressure data reported by Stull (9) were fitted to the following empirical equation:

$$\log P_v = (B/T - 43) + C + D(T - 43) + E(T - 43)^2 \quad (1)$$

To improve the fit, Equation 1 was applied over a low and a high temperature range. The constants obtained were:

| Constant | Temperature Range, ° K. | |
|----------|---------------------------|----------------------------|
| | 273-373 | 373-537 |
| <i>B</i> | -1645.194 | -2173.147 |
| <i>C</i> | 6.66707 | 11.16614 |
| <i>D</i> | 0.590031×10^{-2} | -0.620663×10^{-2} |
| <i>E</i> | -6.46252×10^{-6} | 3.58429×10^{-6} |

The latent heats of vaporization were calculated with the thermodynamically rigorous Clapeyron equation

$$\frac{dP_v}{dT} = \frac{\Delta H_v}{T(V_v - V_L)} \quad (2)$$

The necessary temperature derivatives of the vapor pressure were obtained from Equation 1. The saturated vapor (V_v) and liquid (V_L) volumes of Young allowed evaluation

of ΔH_v . The heats of vaporization used in preparing Table I are smoothed values calculated from Equation 2. At atmospheric pressure the value given in Table I is 295.0 B.t.u. per pound and compares favorably with 295.9 B.t.u. per pound reported in International Critical Tables (3), less favorably with 299.0 B.t.u. per pound reported by Bennewitz and Rossner (1).

VAPOR PHASE THERMODYNAMIC PROPERTIES

Residual volumes were calculated from the volumetric data of Ramsey and Young (6). Low pressure data on the high temperature isotherms were not reported. An extrapolating equation was developed for this low pressure vapor region based on dimerization of the *n*-propyl alcohol in the vapor phase. The data of Foz Gazulla, Morcillo, and Mendes (2) were used to confirm the extrapolated results. These two sources of volumetric data had so few common values that no direct comparison was possible.

The curves of residual volume *vs.* pressure were prepared and used to calculate the fugacity coefficients. The relationship used was

$$\ln \left(\frac{f}{P} \right) = \frac{-1}{RT} \int_0^P \alpha dP \quad (3)$$

Equation 3 was evaluated graphically.

The enthalpies of the superheated vapor were calculated as differences between the enthalpy of the gas at pressure P and the value in the zero pressure or ideal state for each isotherm. The thermodynamic relationship used was

$$(H - H^\circ)_T = \int_0^P \left[T \left(\frac{\partial \alpha}{\partial T} \right)_P - \alpha \right] dP \quad (4)$$

To integrate Equation 4, a curve of α *vs.* temperature was prepared by cross-plotting the α -pressure diagram. The derivatives, $T \left(\frac{\partial \alpha}{\partial T} \right)_P$, were evaluated numerically using the Gregory-Newton backward and forward interpolation formulas (10) at the ends of the curves and Stirling's formula (7) in the central position. A plot of $T \left(\frac{\partial \alpha}{\partial T} \right)_P$ was prepared and Equation 4 evaluated graphically.

The entropies of the superheated vapor were calculated as differences between the entropy of the gas at pressure P and the ideal gas state at zero pressure by the expression

$$(S - S^\circ)_T = \int_0^P - \left(\frac{\partial V}{\partial T} \right)_P dP \quad (5)$$

When the residual volume is substituted in Equation 5, the integral becomes indeterminate at the lower limit. Equation 5 can be evaluated from $P = 0$ to $P = P^*$, an ideal gas state at unit fugacity. When this is subtracted from Equation 5, the lower limit $P = 0$ is eliminated and the result is

$$(S - S^*)_T = (S - S^\circ)_T = \int_{P^*}^P \left(\frac{\partial \alpha}{\partial T} \right)_P dP - \int_{P^*}^P \left(\frac{R}{P} \right) dP \quad (6)$$

Equation 6 was evaluated using the results of Equations

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Table I. Thermodynamic Properties of Saturated *n*-Propyl Alcohol

| Temp., ° F. | Pressure, P.S.I.A. | Volume, Cu. Ft./Lb. | | Enthalpy, B.t.u./Lb. | | | Entropy, B.t.u./Lb.-° R. | | | Fugacity Ratio, <i>f</i> / <i>P</i> |
|----------------|-----------------------|---------------------|--------|----------------------|-------------------|-------|--------------------------|-------------------|-------|--|
| | | Liquid | Vapor | Liquid | Vapori- zation | Vapor | Liquid | Vapori- zation | Vapor | |
| 77 | 0.39 | 0.0200 | 244.7 | 0.0 | 337.5 | 337.5 | 0.0 | 0.629 | 0.629 | 0.997 |
| 100 | 0.85 | 0.0203 | 116.4 | 12.60 | 333.0 | 345.6 | 0.103 | 0.595 | 0.698 | 0.994 |
| 140 | 2.83 | 0.0208 | 37.26 | 35.74 | 324.5 | 360.0 | 0.243 | 0.541 | 0.784 | 0.986 |
| 180 | 7.94 | 0.0214 | 13.98 | 60.24 | 315.6 | 375.9 | 0.358 | 0.493 | 0.851 | 0.973 |
| 280 | 14.696 | 0.0217 | 7.86 | 90.02 | 295.0 | 385.0 | 0.455 | 0.442 | 0.897 | 0.959 |
| 220 | 19.17 | 0.0219 | 6.21 | 99.81 | 291.8 | 390.0 | 0.486 | 0.429 | 0.915 | 0.952 |
| 260 | 40.18 | 0.0231 | 2.94 | 139.4 | 268.4 | 402.7 | 0.580 | 0.373 | 0.953 | 0.924 |
| 300 | 76.17 | 0.0237 | 1.55 | 165.4 | 249.6 | 415.0 | 0.659 | 0.328 | 0.987 | 0.886 |
| 340 | 132.9 | 0.0249 | 0.880 | 208.9 | 218.8 | 427.7 | 0.752 | 0.274 | 1.026 | 0.842 |
| 380 | 216.5 | 0.0265 | 0.530 | 243.6 | 194.1 | 437.7 | 0.823 | 0.231 | 1.054 | 0.788 |
| 420 | 333.1 | 0.0289 | 0.321 | 284.0 | 160.6 | 445.0 | 0.905 | 0.182 | 1.087 | 0.747 |
| 460 | 488.2 | 0.0320 | 0.186 | 329.7 | 116.1 | 445.8 | 0.977 | 0.126 | 1.103 | 0.687 |
| 500 | 688.5 | 0.0410 | 0.0995 | 380.6 | 58.1 | 440.0 | 1.053 | 0.060 | 1.113 | 0.652 |
| 507 | 737.9 | 0.0587 | 0.0587 | 414.5 | 0.0 | 414.5 | 1.115 | 0.0 | 1.115 | ... |

3 and 4. Dividing Equation 4 by *T* and subtracting from this, *R* times Equation 3 gives the first integral in Equation 6. Thus:

$$(S - S^{\circ})_T = \left(\frac{H - H^{\circ}}{T} \right) - R \ln \left(\frac{f}{P} \right) - R \ln \left(\frac{P}{P^*} \right) \quad (7)$$

Equation 7 was used to evaluate the superheated vapor entropy values.

The ideal gas, or zero pressure enthalpies were calculated from the heat capacity data of Kobe, Harrison, and Pennington (4) with the expression

$$dH = C_p dT \quad (8)$$

The ideal gas entropy values were obtained from the expression

$$dS = C_p / T dT \quad (9)$$

Saturated enthalpy values were obtained by plotting a temperature-enthalpy diagram and extrapolating the isobars to the saturated temperature. The saturated entropy values were obtained in a similar manner on a temperature-entropy diagram.

Enthalpy and entropy data for the saturated liquid were obtained by subtracting the enthalpy and entropy of vaporization from their saturated vapor values. The data were smoothed by plotting on enthalpy-entropy, tempera-

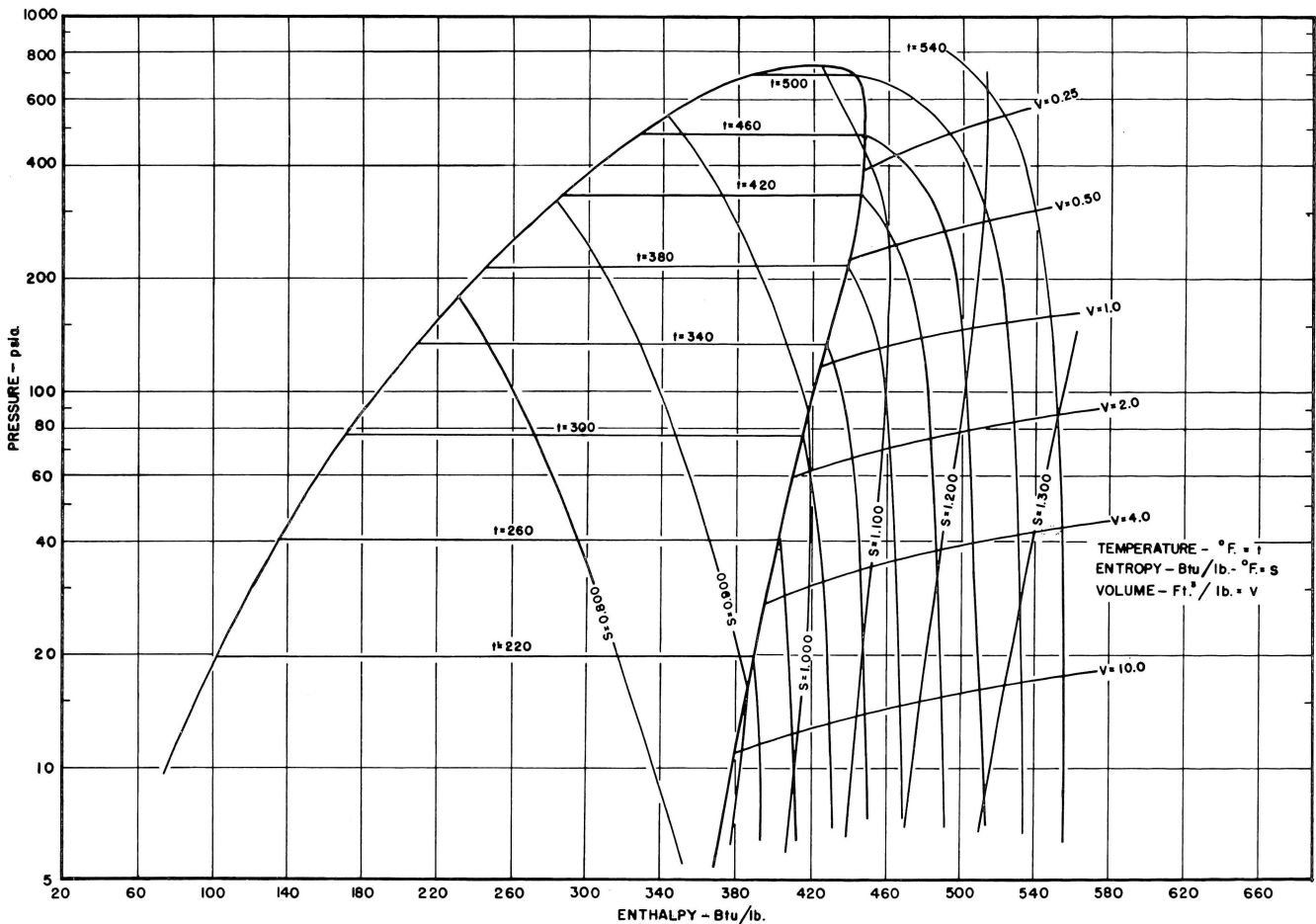


Figure 1. Pressure-enthalpy diagram for *n*-propyl alcohol
Reference state: *H* = 0, *S* = 0 at 77° F., saturated liquid

Table II. Thermodynamic Properties of Superheated *n*-Propyl Alcohol

| Temp., ° F. | Volume, Cu. Ft./Lb. | Enthalpy, B.t.u./Lb. | Entropy, B.t.u. per Lb.° R. | Fugacity, Ratio, <i>f</i> / <i>P</i> | Temp., ° F. | Volume, Cu. Ft./Lb. | Enthalpy, B.t.u./Lb. | Entropy, B.t.u. per Lb.° R. | Fugacity Ratio, <i>f</i> / <i>p</i> |
|---------------------------|------------------------|-------------------------|-----------------------------------|--|------------------------|------------------------|-------------------------|-----------------------------------|---|
| 0 P.S.I.A. | | | | | 100 P.S.I.A. (319° F.) | | | | |
| 77 | Undefined | 337.7 | 0.509 | 1.000 | 340 | 1.243 | 436.3 | 1.042 | 0.8804 |
| 100 | | 346.0 | 0.604 | 1.000 | 380 | 1.349 | 458.8 | 1.101 | 0.9008 |
| 140 | | 361.3 | 0.732 | 1.000 | 420 | 1.439 | 481.5 | 1.155 | 0.9155 |
| 180 | | 377.4 | 0.833 | 1.000 | 460 | 1.526 | 504.2 | 1.210 | 0.9274 |
| 220 | | 394.4 | 0.918 | 1.000 | 500 | 1.610 | 527.5 | 1.252 | 0.9368 |
| 260 | | 412.1 | 0.993 | 1.000 | 540 | 1.690 | 550.9 | 1.296 | 0.9440 |
| 300 | | 430.6 | 1.058 | 1.000 | 150 P.S.I.A. (345° F.) | | | | |
| 340 | | 450.5 | 1.119 | 1.000 | 360 | 0.803 | 438.4 | 1.051 | 0.8423 |
| 380 | | 469.9 | 1.174 | 1.000 | 380 | 0.848 | 452.2 | 1.082 | 0.8561 |
| 420 | | 490.6 | 1.226 | 1.000 | 420 | 0.928 | 476.3 | 1.138 | 0.8772 |
| 460 | | 512.0 | 1.275 | 1.000 | 460 | 0.984 | 499.8 | 1.189 | 0.8957 |
| 500 | | 534.1 | 1.321 | 1.000 | 500 | 1.044 | 524.0 | 1.236 | 0.9098 |
| 540 | | 556.5 | 1.362 | 1.000 | 540 | 1.104 | 548.0 | 1.281 | 0.9199 |
| 10 P.S.I.A. (190° F.) | | | | | 200 P.S.I.A. (374° F.) | | | | |
| 220 | 11.414 | 392.5 | 0.915 | 0.9708 | 380 | 0.584 | 442.5 | 1.062 | 0.8124 |
| 260 | 11.803 | 410.6 | 0.990 | 0.9795 | 420 | 0.656 | 471.3 | 1.123 | 0.8431 |
| 300 | 13.349 | 429.4 | 1.056 | 0.9838 | 460 | 0.711 | 496.0 | 1.176 | 0.8662 |
| 340 | 14.094 | 449.2 | 1.117 | 0.9870 | 500 | 0.761 | 520.6 | 1.224 | 0.8843 |
| 380 | 14.837 | 468.6 | 1.172 | 0.9892 | 540 | 0.807 | 544.9 | 1.269 | 0.8979 |
| 420 | 15.565 | 489.5 | 1.225 | 0.9908 | 250 P.S.I.A. (393° F.) | | | | |
| 460 | 16.294 | 511.2 | 1.274 | 0.9920 | 400 | 0.452 | 446.7 | 1.076 | 0.7895 |
| 500 | 17.011 | 533.4 | 1.321 | 0.9927 | 420 | 0.493 | 463.8 | 1.109 | 0.8239 |
| 540 | 17.743 | 556.0 | 1.361 | 0.9934 | 460 | 0.546 | 496.5 | 1.164 | 0.8376 |
| 14.696 P.S.I.A. (208° F.) | | | | | 500 | 0.590 | 517.1 | 1.214 | 0.8602 |
| 220 | 7.932 | 392.5 | 0.913 | 0.9526 | 540 | 0.632 | 542.0 | 1.260 | 0.8773 |
| 260 | 8.201 | 409.7 | 0.988 | 0.9709 | 300 P.S.I.A. (410° F.) | | | | |
| 300 | 9.016 | 429.1 | 1.054 | 0.9770 | 420 | 0.373 | 453.4 | 1.093 | 0.7725 |
| 340 | 9.532 | 448.7 | 1.116 | 0.9812 | 460 | 0.433 | 486.1 | 1.154 | 0.8094 |
| 380 | 10.041 | 468.4 | 1.171 | 0.9843 | 500 | 0.475 | 513.5 | 1.205 | 0.8363 |
| 420 | 10.546 | 489.2 | 1.224 | 0.9867 | 540 | 0.510 | 539.2 | 1.252 | 0.8564 |
| 460 | 11.047 | 510.8 | 1.273 | 0.9883 | 400 P.S.I.A. (439° F.) | | | | |
| 500 | 11.545 | 533.0 | 1.319 | 0.9899 | 460 | 0.284 | 471.3 | 1.131 | 0.7283 |
| 540 | 12.043 | 555.7 | 1.359 | 0.9913 | 480 | 0.308 | 489.4 | 1.161 | 0.7524 |
| 25 P.S.I.A. (233° F.) | | | | | 500 | 0.329 | 504.8 | 1.188 | 0.7898 |
| 240 | 4.712 | 395.6 | 0.934 | 0.9451 | 540 | 0.363 | 533.0 | 1.238 | 0.8170 |
| 260 | 4.883 | 407.5 | 0.971 | 0.9512 | 500 P.S.I.A. (459° F.) | | | | |
| 300 | 5.373 | 428.4 | 1.037 | 0.9610 | 480 | 0.213 | 471.4 | 1.142 | 0.7211 |
| 340 | 5.530 | 447.5 | 1.098 | 0.9681 | 500 | 0.236 | 492.8 | 1.171 | 0.7441 |
| 380 | 5.837 | 467.2 | 1.155 | 0.9734 | 520 | 0.254 | 509.1 | 1.198 | 0.7633 |
| 420 | 6.141 | 488.3 | 1.217 | 0.9774 | 540 | 0.266 | 525.7 | 1.224 | 0.7785 |
| 460 | 6.442 | 510.0 | 1.256 | 0.9804 | 600 P.S.I.A. (479° F.) | | | | |
| 500 | 6.739 | 532.4 | 1.302 | 0.9828 | 500 | 0.167 | 472.9 | 1.152 | 0.6966 |
| 540 | 7.032 | 554.9 | 1.346 | 0.9849 | 520 | 0.190 | 497.3 | 1.182 | 0.7211 |
| 50 P.S.I.A. (273° F.) | | | | | 540 | 0.205 | 515.9 | 1.209 | 0.7402 |
| 280 | 2.377 | 410.0 | 0.973 | 0.9167 | 700 P.S.I.A. (501° F.) | | | | |
| 300 | 2.441 | 422.1 | 1.009 | 0.9244 | 520 | 0.136 | 480.5 | 1.161 | 0.6774 |
| 340 | 2.677 | 444.2 | 1.072 | 0.9375 | 540 | 0.152 | 505.3 | 1.196 | 0.7025 |
| 380 | 2.842 | 464.5 | 1.129 | 0.9476 | | | | | |
| 420 | 3.005 | 486.2 | 1.181 | 0.9555 | | | | | |
| 460 | 3.160 | 505.7 | 1.231 | 0.9618 | | | | | |
| 460 | 3.160 | 505.7 | 1.231 | 0.9618 | | | | | |
| 500 | 3.315 | 530.8 | 1.277 | 0.9667 | | | | | |
| 540 | 3.464 | 553.8 | 1.322 | 0.9706 | | | | | |

^aSaturated temperature.

ture-enthalpy, and temperature-entropy diagrams. Tabulated data are given in Tables I and II, and the data are plotted on a pressure-enthalpy diagram (Figure 1).

The calculated data were checked for internal consistency with the combined first and second law of thermodynamics

$$dH = TdS + VdP \quad (10)$$

Equation 10 was integrated graphically at both constant pressure and constant entropy and compared with the enthalpy from the calculated data. These checks showed that the data presented are internally consistent.

The accuracy of the data cannot be checked by direct comparison, because the necessary data are lacking. The vapor phase enthalpy values are probably accurate to

±1.00 B.t.u. per pound and the entropy values to ±0.001 B.t.u. per pound ° R.

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NOMENCLATURE

B, C, D, E = constants in Equation 15
C_p = constant pressure heat capacity
f = pure component fugacity

H = enthalpy
 P = pressure
 R = universal gas constant, 1.9872 B.t.u./lb.-mole ° R.
 S = entropy
 T = temperature
 V = volume
 α = residual volume

Superscripts

° = zero pressure, ideal gas state
* = unit fugacity, ideal gas state

Subscripts

c = critical constants
 L = liquid phase
 v = vapor phase

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