

UNIVERSITÀ DI PISA

Scuola di Dottorato in Ingegneria “Leonardo da Vinci”



Corso di Dottorato di Ricerca in
INGEGNERIA DELL'INFORMAZIONE

Tesi di Dottorato di Ricerca

A GSM-based method for the electromagnetic analysis and design of truncated periodic structures

Autore:

Alice Pellegrini _____

Relatori:

Prof. Giuliano Manara _____

Prof. Agostino Monorchio _____

Anno 2006

TABLE OF CONTENTS

Table of Contents.....	I
Abstract	III
Sommario	IV
List of Acronyms.....	V
List of Figures	VI
List of Tables.....	IX
Acknowledgements	IX
Introduction	1
1 The Hybrid Method: Mode Matching - Finite Element	3
<i>1.1 GSM-based Method</i>	<i>3</i>
<i>1.1.1 The Mode Matching Method as GSM-based approach.....</i>	<i>3</i>
<i>1.1.2 Circuit representation of a discontinuity.....</i>	<i>6</i>
<i>1.1.3 Step Junction.....</i>	<i>11</i>
<i>1.2 Finite Element Method.....</i>	<i>18</i>
<i>1.2.1 FEM formulation.....</i>	<i>19</i>
<i>1.3 The hybridization of Mode Matching - Finite Element Method.....</i>	<i>22</i>
2 Analysis and optimization of thick Frequency Selective Surfaces	27
<i>2.1 Formulation: the periodic problem.....</i>	<i>28</i>
<i>2.1.1 The genetic optimization.....</i>	<i>31</i>
<i>2.2 Numerical results.....</i>	<i>34</i>
<i>2.3 AMC with genetic optimization.....</i>	<i>36</i>
3 Analysis of radiating apertures	41
<i>3.1 Formulation</i>	<i>42</i>
<i>3.1.1 Infinite array</i>	<i>43</i>
<i>3.1.2 Finite array: the Spectral Decomposition method.....</i>	<i>44</i>
<i>3.2 Depolarization technique.....</i>	<i>47</i>
<i>3.3 Horn antennas array</i>	<i>48</i>
<i>3.4 Radiation pattern</i>	<i>49</i>
<i>3.5 Numerical results.....</i>	<i>50</i>
4 Analysis of finite FSSs	59
<i>4.1 Formulation</i>	<i>59</i>
<i>4.2 Spectral decomposition approach</i>	<i>65</i>
<i>4.3 Preliminary results.....</i>	<i>66</i>

5	Analysys of composite devices	71
5.1	<i>Methodology</i>.....	71
5.2	<i>Preliminary numerical Results</i>.....	77
5.2.1	<i>Analysis of infinite composite structures</i>	78
5.2.2	<i>Analysis of finite composite structures</i>.....	81
	Conclusions	87
	References	89

ABSTRACT

The research activity, illustrated in this work, has been developed in the area of applied electromagnetics and it concerns the development and the improvement of a hybrid numerical method combining the Mode Matching (MM) and the Finite Element (FE) specifically derived for the study of complex microwave devices. Firstly, the optimization problem of unconventional Frequency Selective Surfaces (FSSs), obtained by using NURBS curves, is analyzed. A genetic algorithm is used in order to address the optimization of a multiparametric structure such as the FSS. The hybrid method MM-FE is used to evaluate the frequency behaviour of this kind of structures. The hybrid technique is therefore applied to the study of large finite arrays of open-ended or iris-loaded waveguide apertures or horn antennas. The finite dimensions are taken into account by using a Spectral Decomposition (SD) approach that allows us to reduce the finite problem to a summation of infinite periodic ones. A similar procedure, now based on the Method of Moments (MoM) and the spectral decomposition approach, is applied to the analysis of finite thin frequency selective surfaces. Finally the hybrid methodology MM-FEM-SD, combined with an MoM, is used to study finite arrays of rectangular waveguide cascaded with a finite thin FSS. In order to prove the effectiveness of this methodology, several numerical results are compared with that obtained through a commercial software or available in literature.

SOMMARIO

Obiettivo dell'attività di ricerca scientifica, svolta nel settore dell'elettromagnetismo applicato, consiste nell'impiego e nell'estensione di un metodo numerico Mode Matching - Finite Element Method (MM-FEM) per l'analisi di dispositivi a microonde. In una prima fase, è stato affrontato il problema dell'ottimizzazione di superfici selettive in frequenza (Frequency Selective Surfaces - FSSs) non convenzionali ottenute mediante curve NURBS (Non Uniformal Rational B-Spline). Data la natura multiparametrica delle strutture in esame, il problema dell'ottimizzazione è stato affrontato mediante l'impiego di una tecnica evolutivistica, di natura stocastica, nota come algoritmo genetico. Per l'analisi delle prestazioni e del comportamento in frequenza di tali strutture, è stato impiegato il metodo ibrido Mode Matching- Finite Elements Method. Tale metodo è stato inoltre utilizzato per l'analisi di array finiti di guide d'onda open-ended o iris-loaded e antenne horn. Le dimensioni finite delle strutture in esame sono state considerate mediante il metodo Spectral Decomposition (SD). Tale tecnica consente di ricondurre l'analisi del problema finito, a quella di una combinazione di problemi equivalenti di tipo infinito, più semplicemente analizzabili.

Una procedura basata sulla decomposizione spettrale e su un metodo dei momenti (Method of Moments - MoM) per strutture periodiche sottili è stata applicata allo studio di superfici sottili selettive in frequenza di dimensioni finite. Infine, la metodologia impiegata nelle attività sopra descritte è stata utilizzata per lo studio di sistemi compositi, costituiti dalla cascata di un array di guide d'onda o antenne horn e una o più FSS entrambi di dimensioni finite e diversa periodicità.

La correttezza della metodologia impiegata nelle attività descritte è stata verificata mediante esempi presenti in letteratura o mediante software commerciali.

LIST OF ACRONYMS

AMC: Artificial Magnetic Conductor;

DFT: Discrete Fourier Transform;

EFIE: Electric Field Integral Equation;

EBG: Electromagnetic Band Gap;

FEM: Finite Element Method;

FFT: Fast Fourier Transform;

FSS: Frequency Selective Surface;

GA: Genetic Algorithm;

GAM: Generalized Admittance Matrix;

GIM: Generalized Impedance Matrix;

GSM: Generalized Scattering Matrix;

MM: Mode Matching;

MoM: Method of Moments;

NURBS: Non Uniform Rational B-Spline;

PEC: Perfect Electric Conductor;

PMC: Perfect Magnetic Conductor;

SD: Spectral Decomposition;

TE: Transverse Electric;

TEM: Transverse ElectroMagnetic;

T(FW)²: Truncated Floquet Wave Full-Wave;

TM: Transverse Magnetic;

LIST OF FIGURES

Fig. 1.1 - Geometry of a waveguide problem	4
Fig. 1.2 - Geometry for representing a waveguide discontinuity.....	7
Fig. 1.3- Multi-port equivalent circuit to the discontinuity depicted in Fig. 1.2.....	7
Fig. 1.4 - Multi-port circuit representation of a waveguide discontinuity for deriving the standard admittance matrix.	8
Fig. 1.5 - Boundary enlargement problem	11
Fig. 1.6 - Identification of the scattering parameters of the step discontinuity as entries of the GSM.	15
Fig. 1.7 - Geometry for the analysis of a double step discontinuity.	15
Fig. 1.8 - Reference systems at a step discontinuity analyzed through the transmission matrix.	17
Fig. 1.9 - Step discontinuity between two different heights rectangular waveguides.....	18
Fig. 1.10 – Unconventional shaped cross-section waveguide.....	19
Fig. 1.11 – Vector basis function (a); amplitude of the Whitney function over a triangular element(b).....	21
Fig. 1.12 – Boundary reduction: a rectangular waveguide (Ω_1) ends with a smaller unconventional waveguide (Ω_2).....	22
Fig. 2.1 - Geometry of a thick inductive Frequency Selective Surface.....	28
Fig. 2.2 – The elementary periodicity cell of the thick metallic screen: longitudinal section	30
Fig. 2.3 - Chromosome structure: each gene represent a structure parameter.	32
Fig. 2.4 – Set of possible aperture shapes	32
Fig. 2.5 – NURBS defined by 16 control points.....	33
Fig. 2.6 – Optimization of thickness, skewness angle and periodicity of a FSS with a given shaped aperture	34
Fig. 2.7 – Transmission (a) and reflection (b) coefficient for the FSS in Fig. 2.6	34
Fig. 2.8 – FSS screen with optimized shaped aperture selected from database	35
Fig. 2.9 – Transmission (a) and reflection (b) parameters for the geometry in Fig. 2.8	35
Fig. 2.10 – FSS screen with optimized skewness angle, thickness and shape aperture (a), a particular of the unit cell (b).....	35
Fig. 2.11 – Transmission and reflection coefficient for the screen in Fig. 2.10.....	36
Fig. 2.12 - Comparison of the normalized fitness function of three examples	36
Fig. 2.13 – Image Theorem: the longitudinal component of the electric field nulls on a PEC, the orthogonal one on a PMC.....	37
Fig. 2.14 - PMC surface as dual of a PEC surface after 180° phase shift.....	38
Fig. 2.15 - A FSS terminated with a PEC surface, a PMC surface is obtained at a distance of $\lambda_g/4$ in the waveguide.	38
Fig. 2.16 - An optimized FSS that realize a PMC condition (a), a particular of the unit cell (b).....	39
Fig. 2.17 - Reflection coefficient phase of the PMC realized by using the GA.....	39
Fig. 3.1 – Geometry and characteristic dimensions of the finite array of waveguide fed apertures.....	42
Fig. 3.2 - Cross section (a) and longitudinal (b) view of the unit cell under analysis.....	44
Fig. 3.3 - Windowing function applied to the excitation. The parameter δ defines the taper of the spatial gate	45
Fig. 3.4 - Fourier transform and discretization of the spatial gate	46

Fig. 3.5 - N-sided planar polygon; $\hat{\alpha}_n$ is the tangential vector and $\hat{\gamma}_n$ describes the position of the nth corner.....	47
Fig. 3.6 - Longitudinal profile discretized as a series of steps whose length is $\lambda/32$	49
Fig. 3.7 – Magnitude (a) and phase (b) of the active reflection coefficient and E-plane radiation pattern for the 20×20 array of open-ended waveguides: comparison with [73].....	51
Fig. 3.8 - Amplitude of active reflection coefficient for the 21×21 array of open-ended waveguides scanned at 20° in E-plane as compared with [74].....	52
Fig. 3.9 - Shape and dimensions of the iris for the 20×20 array of waveguides, ensuring a better matching.....	52
Fig. 3.10 - Active reflection coefficient, along the central horizontal row (continuous line) and along the central vertical row (dashed line), for the 20×20 array of irises-loaded waveguides.....	53
Fig. 3.11 - Active reflection coefficient, along the central horizontal row (a) and along the central vertical row (b), for the 6×6 array of open-ended waveguides: comparison of our technique with Ansoft HFSS.....	53
Fig. 3.12 - Normalized radiation pattern of the 6×6 open ended rectangular waveguide array compared with Ansoft HFSS: a) H-plane pattern, b) E-plane pattern.....	54
Fig. 3.13 - Geometry of the hexagonal array of rectangular open-ended waveguides: a) original problem with characteristic dimensions ($a=17.142$ mm, $b=11.428$ mm, $dx=28.57$ mm, $dy=17.142$ mm and $\alpha=50.194^\circ$), b) equivalent problem: infinite array with hexagonal illumination.....	54
Fig. 3.14 - Magnitude of the reflection coefficient evaluated on each aperture for an hexagonal array of open-ended waveguides. The upper values are obtained with the present method, the lower values are obtained with Ansoft HFSSv10.1.....	55
Fig. 3.15 - Phase (in degrees) of the reflection coefficient evaluated at each aperture for an hexagonal array of open-ended waveguides. The upper values are obtained with the present method, the lower values are obtained with Ansoft HFSSv10.1.....	55
Fig. 3.16 - Geometry of the array and dimension of elementary radiating element.....	56
Fig. 3.17 - Comparison with Ansoft HFSS: active reflection coefficient along the central column for the 6×6 array of pyramidal horn antennas.....	56
Fig. 3.18 - Normalized radiation pattern of the 6×6 pyramidal horn array compared with Ansoft HFSS: a) H-plane pattern, b) E-plane pattern.....	57
Fig. 3.19 - Geometry of the hexagonal array and magnitude of the active reflection coefficients belonging to the first quadrant.....	57
Fig. 3.20 - The radiation pattern on the two principal planes (a)-(b) and the co-polar and cross-polar component on a plane at $\phi = 45^\circ$ (c).....	58
Fig. 4.1 – Mondimensional patch FSS.....	59
Fig. 4.2 - x-directed and y-directed rooftop basis functions.....	60
Fig. 4.3 – Doubly periodic infinite thin FSS screen.....	62
Fig. 4.4 - Subdomain rooftop basis function.....	64
Fig. 4.5 – Truncated spatial rectangular (a) and kaiser (b) gate that impinges on the infinite FSS.....	65
Fig. 4.6 – FSS with ring elements arranged in a 5×5 rectangular grid.....	66
Fig. 4.7 – Radiation pattern for a FSS with 5×5 elements; E_ϕ component (a) and E_θ component (b) compared with HFSS for an incident plane wave along the orthogonal direction. E_θ component (c) and E_ϕ component (d) compared with HFSS for a plane wave with incident angle $\theta = 30^\circ$	67

Fig. 4.8 - Radiation pattern for a FSS with 10×10 elements, E_phi component (a) and E_theta component (b) compared with HFSS for orthogonal incidence.....	67
Fig. 4.9 - FSS with cross elements arranged in a 9×9 rectangular grid	68
Fig. 4.10 - Radiation pattern for a FSS with 9×9 cross elements, E_phi component along the principal plane compared with HFSS for a plane wave with incident angle theta = 30	68
Fig. 4.11 - FSS with asymmetrical elements arranged in a 9×9 rectangular grid	68
Fig. 4.12 – Radiation pattern along the principal planes, E_theta component (a) and E_phi component (b) compared with HFSS for orthogonal incidence.	69
Fig. 5.1 – Composite structure of a finite array of rectangular waveguides with above one or more FSS; each subsystem has its own periodicity.....	72
Fig. 5.2 – Equivalent infinite problem: the plane wave is replaced with a truncated spatial gate g(x,y).	73
Fig. 5.3 – Mapping between the local harmonic numeration for the FSS and the global one of the array	75
Fig. 5.4 – Mapping of the local shifted harmonics for the FSS into the global numeration of the array	76
Fig. 5.5 – Geometry of a cascade system of an infinite array of rectangular waveguides with above an infinite FSS (a); the unit cell of the composite structure (b)	78
Fig. 5.6 – S-parameters of each separated subsystem: (a) S-parameters for the infinite array of rectangular waveguides, (b) S-parameters of the infinite FSS.....	78
Fig. 5.7 – S-parameters of the composite structure; the transmission of TM mode in free space region (a) and the reflection of the TE10 in the waveguide (Fig. 5.5).	79
Fig. 5.8 – Unit cell of the composite structure.....	79
Fig. 5.9 – S-parameters of the infinite FSS (Fig. 5.8).....	80
Fig. 5.10 - S-parameters of the composite structure; the transmission of TM mode in free space region (a) and the reflection of the TE10 in the waveguide (Fig. 5.8).	80
Fig. 5.11 – Unit cell of the composite structure; the FSS dimensions are twice the dimensions of the array	80
Fig. 5.12 – S-parameters of the infinite FSS (Fig. 5.11).....	81
Fig. 5.13 - S-parameters of the composite structure; the transmission of TM mode in free space region (a) and the reflection of the TE10 in the waveguide (b).....	81
Fig. 5.14 - Geometry of a cascade system of a finite array of rectangular waveguides with above a finite FSS (a); the unit cell of the composite structure (b).	82
Fig. 5.15 – S-parameters of the equivalent FSS Fig. 5.14(b) as a function of the frequency (a) and of the incident angle (b) (Freq = 14.5GHz).....	82
Fig. 5.16 – Radiation patterns for the composite structure along the two principal planes phi = 0° (a) and phi = 90° (b).	83
Fig. 5.17 – S-parameters of the FSS as frequency function (a) and as incident angle function (b).....	83
Fig. 5.18 – Radiation patterns for the composite structure compared with the radiation pattern of the single array system on the two principle planes.....	84
Fig. 5.19 – Unit cell of the FSS obtained by using a genetic optimization algorithm.	84
Fig. 5.20 – S-parameters as function of the incident angle.....	85
Fig. 5.21 – Radiation pattern on the two principal planes evaluated for the cascade system and compared with single array patterns.....	85

LIST OF TABLES

Table 3.1 - Comparison between computational time and memory usage for the proposed MM/FE/SD and Ansoft HFSS v10.1.....	58
Table 5.1 – Mapping from SGI to SSI for the FSS, the upper rows represent the local numeration of Floquet’s harmonics and the lower rows represents the global numeration of the global Foquet’s expansion	75
Table 5.2 - Mapping from SGI to SSI for the FSS, the upper rows represent the local numeration of Floquet’s harmonics and the lower rows represents the global numeration of the global Foquet’s expansion ($m_k = 1; n_k = 0$)	76
Table 5.3 – Dimensions of each subsystem of the composite structure (Fig. 5.5).....	78
Table 5.4 – Dimensions of each subsystem of the composite structure (Fig. 5.8).....	79
Table 5.5 – Dimensions of each subsystem of the composite structure (Fig. 5.11).....	81
Table 5.6 – Dimensions of each subsystem of the 6×6 array Fig. 5.14.	82
Table 5.7 – Dimensions of each subsystem of the 6×6 array Fig. 5.14.	83
Table 5.8 – Dimensions of each subsystem of the 6×6 array.....	84

ACKNOWLEDGEMENTS

The author wishes to thank Prof. Raj Mittra for the possibility to develop the last part of this activity at the Electromagnetic Communication Laboratory of the Penn State University (PA).

