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¹ Simulating dispersion in the evening-transition boundary layer

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Abstract We investigate dispersion in the evening-transition boundary layer using large-eddy 6 simulation (LES). In the LES, a particle model traces pollutant paths using a combination of the resolved flow velocities and a random displacement model to represent subgrid-scale motions. The LES is forced with both a sudden switch-off of the surface heat flux and also a more gradual observed evolution. The LES shows 'lofting' of plumes from near-surface releases in the pre-10 transition convective boundary layer; it also shows the subsequent 'trapping' of releases in the 11 post-transition near-surface stable boundary layer and residual layer above. Given the paucity 12 of observations for pollution dispersion in evening transitions, the LES proves a useful reference. 13 We then use the LES to test and improve a one-dimensional Lagrangian Stochastic Model 14 (LSM) such as is often used in practical dispersion studies. The LSM used here includes both 15 time-varying and skewed turbulence statistics. It is forced with the vertical velocity variance, 16 skewness and dissipation from the LES for particle releases at various heights and times in the 17 evening transition. The LSM plume spreads are significantly larger than those from the LES in 18 the post-transition stable boundary-layer trapping regime. The forcing from the LES was thus 19 insufficient to constrain the plume evolution, and inclusion of the significant stratification effects 20 was required. In the so-called modified LSM, a correction to the vertical velocity variance was 21 included to represent the effect of stable stratification and the consequent presence of wave-like 22 motions. The modified LSM shows improved trapping of particles in the post-transition stable 23 boundary layer. 24

 $_{25}$ Keywords Dispersion \cdot Evening transition \cdot Lagrangian stochastic model \cdot Large-eddy $_{26}$ simulation

27 1 Introduction

The atmospheric boundary layer (ABL) over land typically experiences a strong diurnal cycle forced by solar radiation. Surface heating drives convective boundary-layer (CBL) turbulence in the daytime, and surface cooling leads to a stable boundary layer (SBL) at night. In the

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evening, the sensible heat flux diminishes in response to the sun's decreasing elevation, resulting in the dissipation exceeding the production of turbulent kinetic energy (TKE), and in the decay of large-scale convective eddies. The evening and morning transitions feature a period of rapid evolution in the state of the turbulence compared with other times in the diurnal cycle.

Dispersion models have a range of important applications, including: producing air-quality 35 forecasts, planning the placement of industry, deciding on the requirements for chimney-stack 36 heights, and tracking the paths of dangerous pollutants and issuing warnings in events such as 37 the Fukushima Daiichi nuclear accident, or the eruption of the Icelandic volcano Eyjafjallajökull. 38 For such models to be effective they must predict the path of the pollution accurately. However, 39 the effect of rapidly time-varying turbulence (such as in the boundary-layer evening transition) 40 is often highly idealized or overlooked. In this paper we use a large-eddy simulation (LES) and 41 a Lagrangian stochastic model (LSM) to study this problem. 42

43 1.1 Large-Eddy Simulation

LES models fluid flow in situations where the Reynolds number is large. Turbulent eddies larger than the grid scale are solved explicitly using the momentum, thermodynamic and continuity equations, while smaller scale motions are represented by a subgrid model. LES provides a 3D representation of the flow and includes many of the processes at work in the atmosphere, and hence provides the best substitute for experimental data, with the advantage of being adaptable to the conditions one wishes to simulate.

A dispersion model may be included in the LES by specifying initial particle positions, and advancing them by applying the local flow velocity at each timestep, along with a random perturbation to account for subgrid-scale motions. This method has previously been used to describe dispersion in the CBL by Mason (1992) and Weil et al. (2004), and in the SBL by Kemp and Thomson (1996).

55 1.2 Lagrangian Stochastic Model

LSMs are often used to simulate turbulent dispersion in the atmospheric boundary layer. The use of such models began with the work of Taylor (1921) who considered transport by homogeneous turbulence, and has continued with key advances such as:

Modelling dispersion in inhomogeneous turbulence in the atmospheric surface layer with
 comparisons to experimental data, for example, by Wilson et al. (1981).

Work by Thomson (1984), van Dop et al. (1985), Sawford (1986), Thomson (1987) and others
 on the conditions that should be satisfied in LSMs for turbulent diffusion. In particular, they
 established the well-mixed criterion, which states that, "If the particles of a tracer are initially

well-mixed (in position-velocity space) in a turbulent flow, they should remain so."

LSMs have also been applied to incorporate and describe the effects of important features of atmospheric boundary-layer turbulence on dispersion, such as the asymmetry of top-down and bottom-up diffusion (Weil, 1990). A short review of the use of LSMs to describe turbulent diffusion may be found in Chapter 2 of Rodean (1997) or in Wilson and Sawford (1996).

⁶⁹ 1.3 Evening-transition boundary layer

The ABL is typically categorized into three states governed by surface heating: stable, neutral and convective. Boundary-layer transitions occur when the surface heating is added or removed,

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 $_{\rm 72}$ $\,$ which generally occurs at sunrise and sunset. This process has been modelled by Nieuwstadt and

⁷³ Brost (1986), Sorbjan (1997), Goulart et al. (2003), Pino et al. (2006) and Beare et al. (2006), ⁷⁴ among others. During boundary-layer transitions the turbulence properties are strongly time

⁷⁵ dependent, and the problem of dispersion in such time-dependent flows has not been addressed

⁷⁶ much in the literature. Here, we address this gap in the literature by performing both LES and

 π LSM simulations of dispersion for the evening transition. Given the paucity of observations of

⁷⁸ pollution dispersion in the evening transition, the LES is used as a reference against which the
 ⁷⁹ strengths and weaknesses of the LSM can be identified.

To date, there has been limited research into modelling dispersion during the boundary-80 laver evening transition. Carvalho et al. (2010) studied dispersion in decaying turbulence using 81 a LSM where the turbulence was represented by time-varying eddy diffusivities. Although an 82 approximation, this study provides a useful insight into the role of the residual layer and the 83 SBL in determining pollution concentrations. However, the LSM is only compared with itself. 84 There is thus significant scope for further investigation using LES as a reference: the first aim 85 is to determine the impact of the evening transition on dispersion using LES. The LSM is then 86 compared with the LES in order to identify improvements in its formulation. 87

88 2 Method

89 2.1 LES

The Met Office large-eddy model (Gray et al., 2004) is employed to simulate boundary layers over the duration of an evening transition using periodic lateral boundary conditions. Two cases of the evening transition are simulated using idealized and observed forcings respectively; we

⁹³ describe these cases below.

94 2.1.1 Idealized forcing



Fig. 1: Surface sensible heat flux plotted against time from the start of the simulation for the idealized forcing (red) of Nieuwstadt and Brost (1986) and the observed forcing (black) from the Cardington site for the evening of 23 September 2003.

The first case is the idealized decay of a CBL described by Nieuwstadt and Brost (1986). Here 95 the positive surface sensible heat flux is suddenly changed to zero. The Nieuwstadt and Brost 96 (1986) case will allow us to focus on the role of the decaying residual layer in dispersion. The 97 residual layer herein refers to the weakly stratified region with a depth similar to the preceding 98 CBL. This contrasts with the post-transition SBL that occurs for the observed forcing (see Sect. 99 2.1.2) which has a depth significantly smaller than the preceding CBL and is more strongly 100 stratified. The geostrophic wind vector is directed along the x-direction and is of magnitude 101 5 m s^{-1} . The roughness length is set at 0.01 m for momentum and heat. The initial potential 102 temperature is a constant 283 K from the surface to 800 m, with a capping inversion of 0.0025 K 103 m^{-1} from 800 m to the domain top. Figure 1 shows the time evolution of the surface sensible heat 104 flux for the idealized forcing. A constant surface heating of 100 W m⁻² is applied to generate 105 convective turbulence. The model is initially run for 10,800 s, by which time the turbulence has 106 become statistically stationary. At this time the surface sensible heat flux is set instantaneously 107 to zero to simulate the decay of convective turbulence. For the idealized forcing, a shallow SBL 108 does not form as the surface sensible heat flux does not go negative. Eventually the decay will 109 stop and form a neutral boundary layer with stratification above. The stratification effects will 110 thus be entirely due to the residual layer. A reference time coordinate (t_d) is introduced such 111 that $t_d = 0$ at the start of the transition (t = 10,800 s). A domain size of $5 \times 5 \times 4$ km³ is used 112 (the last number is the vertical extent), with 100×100 grid points in the horizontal, and 90 113 points of variable resolution in the vertical. The horizontal grid length is 50 m and the vertical 114 grid is refined near the surface and stretched above the CBL. 115

116 2.1.2 Observed forcing

In order to consider the role of the post-transition SBL, the second case uses the observed 117 forcing of Beare et al. (2006). The time evolution of the surface sensible heat flux is shown in 118 Fig. 1. Unlike the idealized forcing, there is now a negative nighttime sensible heat flux after the 119 transition leading to the development of a SBL. Such a developing SBL is more stratified than 120 the overlying residual layer, and strongly inhibits the vertical transport of pollution leading to 121 high concentrations in the SBL (trapping). In order to resolve the SBL, the LES is run with a 122 10-m horizontal resolution and variable vertical resolution (with a 10-m vertical grid length in 123 the SBL) over $256 \times 256 \times 90$ grid points and on a domain of $2.56 \times 2.56 \times 2$ km³. The model 124 is initialized with a uniform potential temperature up to 800 m with an overlying inversion of 125 strength 0.0025 K m⁻¹. The geostrophic wind vector is directed along the x-direction and is of 126 magnitude 7 m s⁻¹. 127

128 2.1.3 Trajectory calculation

Particle trajectories in the LES are calculated using a combination of the resolved flow velocity and a representation of the subgrid-scale motions at each timestep, following Kemp and Thomson (1996). The vector displacement of the particle ($\Delta \mathbf{x}$) is calculated with an Euler forward step method using the current LES timestep (Δt), the LES resolved velocity (\mathbf{u}) interpolated to the particle position, random vector displacements (\mathbf{R}_d) and a drift correction velocity (∇K) where K is the LES eddy diffusivity interpolated to the particle position,

$$\Delta \mathbf{x} = \mathbf{u} \Delta t + \mathbf{R}_d + \nabla K \Delta t. \tag{1}$$

¹³⁵ The random perturbations follow a Gaussian distribution with standard deviation given by

$$\sigma_d = (2K\Delta t)^{1/2}.$$
(2)

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Gaussian random numbers are generated numerically using the Box-Müller transform (Box and Müller, 1958). The prescription of this random perturbation generates a mean drift towards regions of small K and this is corrected by adding the drift correction velocity. In areas of the flow where the size of the eddies is smaller than the grid length, the resolved TKE tends to zero. In these regions, such as near the surface, the representation of the subgrid energy via the random vector displacements becomes essential. Periodic lateral boundary conditions are applied to the particle model, as in the LES.

143 2.2 LSM

We first describe the standard form of the LSM for vertical dispersion in stationary, horizontallyhomogeneous flows with Gaussian velocity distributions and then the modified form that we are using for transitional boundary layers. The equations describing the evolution of particle vertical velocity w and vertical position z are

$$dw = a(z, w)dt + b(z, w)d\xi,$$
(3)

$$dz = wdt, \tag{4}$$

where $d\xi$ is a Gaussian random forcing with zero mean and variance dt and a and b are functions. In the standard LSM, the functions a and b are given by

$$a = -\frac{C_0 \epsilon w}{2\sigma_w^2} + \frac{1}{2} \left(1 + \frac{w^2}{\sigma_w^2} \right) \frac{\partial \sigma_w^2}{\partial z},\tag{5}$$

$$b = (C_0 \epsilon)^{1/2},\tag{6}$$

where C_0 , σ_w^2 and ϵ are a dispersion parameter (formally equal to the inertial subrange constant in 150 the Lagrangian velocity structure function, but often regarded as a tunable parameter to describe 151 the dispersion), the vertical velocity variance and the rate of dissipation of TKE per unit mass 152 respectively. The first term in Eq. 5 is deterministic and represents the fading memory of the 153 particle velocity from earlier times; the second term in Eq. 5 is the deterministic drift correction 154 term. The vertical gradient of σ_w^2 forces particles away from regions of small σ_w^2 ensuring they 155 become well-mixed in the domain over time and preventing their accumulation in regions of small 156 σ_w^2 that would otherwise occur. The function in Eq. 6 sets the amplitude of the random process. 157 For further details of vertical dispersion in stationary flows with Gaussian velocity distributions 158 see e.g. Rodean (1997). 159

In this study, we modify the standard LSM by allowing skewed velocity distributions following 160 Luhar and Britter (1989) and by introducing a time dependence to the functions a and b, thus 161 allowing the consideration of non-stationary, skewed turbulence such as occurs at the start of 162 the evening transition. The resulting function a is an extension of the form proposed by Hudson 163 and Thomson (1994). The derivation is complex so the details are summarized in the Appendix. 164 Herein, we refer to this model as 'the LSM'. We use a value of $C_0 = 2$ following Luhar and 165 Britter (1989), and, as is common in other LSMs, a reflection boundary condition is applied at 166 the CBL top. 167

Within the LSM the state of turbulence is defined by vertical profiles of the vertical velocity variance, the dissipation of TKE, and the skewness of vertical velocities $(\overline{w^3})$. Normally these profiles have been represented in two ways. The first is as functions continuous in the range $0 \le z \le h$ (where h is the height of the ABL) with amplitudes dependent on the friction velocity

 (u_*) , the convective velocity scale (w_*) and the length scales h and the Obukhov length (L). 172 These functions are derived by finding a best fit to observed profiles; the method is detailed in 173 Chapter 12 of Rodean (1997). The second approach, and the one adopted here, is to utilize a more 174 complex model such as LES to determine the turbulence profiles, and then use these directly in 175 the LSM, as done previously by Weil et al. (2004). Driving the LSM with LES turbulence profiles 176 and comparing dispersion concentrations between both models provides a test of whether the 177 formulation of the LSM and the boundary-layer specification in the LSM are sufficient. If there 178 is disagreement in the dispersion concentrations, then more detailed boundary-layer properties 179 may be required. 180

181 2.3 Modified LSM

The decay of turbulence caused by the instantaneous switch-off of surface heat flux leads to the 182 development of a positive potential temperature gradient over the depth of the residual layer. 183 Such a stably stratified layer may support both gravity waves and turbulence, with large-scale 184 vertical motions suppressed by the stability (Stull, 1988). The LSM has been previously modified 185 by Das and Durbin (2005) for stratified flows. Their method involved matching the LSM to the 186 corresponding second-order closure equations for stratified flows. We adopt a simpler approach 187 in terms of defining the key length scales and modifying the vertical velocity variance in the 188 LSM, with the aim of removing the contribution from waves. The natural length scale defining 189 the separation between gravity waves and turbulence is the Ozmidov scale (L_o) , 190

$$L_o = \epsilon^{\frac{1}{2}} N^{-\frac{3}{2}},\tag{7}$$

where N is the Brunt-Väisälä frequency. For length scales larger than L_o gravity waves tend to dominate, whilst for smaller scales turbulence prevails. We argue that gravity waves disperse much less efficiently than turbulence in the stratified boundary layer, and thus we need to modify the vertical velocity variance forcing the LSM to account for this effect. We represent dissipation as

$$\epsilon = D \frac{\sigma_w^3}{l},\tag{8}$$

where D is a constant and σ_w^2 and l are the variance and length scale of the turbulent part of the fluctuations. If we set $l = L_o$ we find that the maximum value for the turbulent variance is of order

$$\sigma_w^2 = E \frac{\epsilon}{N},\tag{9}$$

where E is a constant. Equation 9 thus defines the threshold between waves and turbulence. For $\sigma_w^2 > E\epsilon/N$ gravity waves predominate and turbulence dominates otherwise. Since the gravity waves are poor at dispersion, we define a modified, 'turbulence only', vertical velocity variance $(\sigma_{w_{mod}}^2)$ as

$$\sigma_{w_{mod}}^2 = \min\left(\sigma_w^2, \frac{E\epsilon}{N}\right). \tag{10}$$

We refer to the LSM using the modified vertical velocity variance $(\sigma_{w_{mod}}^2)$ as 'the modified LSM'. A value of E = 1 is used. The modified vertical velocity variance also conveniently takes the place of the reflection boundary condition used at the CBL top in the LSM; it naturally reduces spread above the CBL top.

207 2.4 Plume statistics

Plume behaviour is evaluated through statistical properties of a large ensemble of simulated particle trajectories. The plume centreline and spread are determined by finding the mean $(\overline{z_p})$ and standard deviation (σ_z) of the vertical position of all particles at any given timestep, using

$$\overline{z_p} = \left(\sum_{j=1}^{N_t} z_{p_j}\right) / N_t, \tag{11}$$

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$$\sigma_z = \sqrt{\frac{1}{N_t} \sum_{j=1}^{N_t} \left(z_{p_j} - \overline{z_p} \right)^2},\tag{12}$$

where the z_{p_i} are the particle heights, and N_t is the total number of particles being tracked.

In addition we consider vertical concentration profiles at various times. The vertical concentration profile is calculated by splitting the vertical axis into slices of depth Δz and counting the number of particles in each slice (N_z) . The concentration at each level is then given by $N_z/\Delta z$. This may be normalized by the total number of particles, N_t , divided by the CBL height at the start of the transition, z_i , such that the concentration equals 1 when the particles are well-mixed. z_i is defined as the height of the sensible heat flux minimum. The normalized concentration at a given height (C_z) is thus given by

$$C_z = \frac{N_z z_i}{N_t \Delta z}.$$
(13)

220 3 Results

Prior to investigating the effect of the transition on particle trajectories, the evolution of the state of turbulence in the boundary layer is examined through vertical profiles of potential temperature, vertical heat flux, vertical velocity variance, dissipation rate of TKE, and the third moment of vertical velocity (Figs. 2a, 2b, 3a, 3b, and 3c respectively) for the idealized forcing.

The decay of turbulence caused by the instantaneous switch-off of surface heat flux leads to 225 the development of a slightly positive potential temperature gradient with height over the extent 226 of the residual mixed layer (Fig. 2a). This effect has been shown to be a robust feature of the 227 decaying CBL in the LESs of Nieuwstadt and Brost (1986) and Pino et al. (2006), and in the 228 observations discussed in Grant (1997). This feature can be seen to develop rapidly (within 400 s 229 of the start of the switch-off of surface heat flux) and strengthen over the course of the transition 230 (shown by the profile at $t_d = 800$ s). The positive potential temperature gradient suppresses 231 vertical motions, which is expected to have an effect on particle dispersion. This is investigated 232 below. 233

The normalized profile of sensible heat flux (Fig. 2b) shows how the development of a positive potential temperature gradient occurs. Before the transition, a negative gradient of sensible heat flux over the majority of the boundary layer indicates that transport of heat from the surface is warming the boundary layer. Shortly after the start of the transition ($t_d = 400$ s), the sensible heat flux near the surface has a positive gradient indicating cooling, while the upper part of the boundary layer continues to warm. Nieuwstadt and Brost (1986) refer to this process as 'demixing'.

In Fig. 3, the solid lines represent daytime convective turbulence conditions at $t_d = 0$. Once the surface sensible heating is removed, all three profiles decay rapidly. By $t_d = 1200$ s, the peak vertical velocity variance has approximately halved, as shown in Fig. 3a. Also the peak has



Fig. 2: Profiles of (a) potential temperature and (b) sensible heat flux (normalized by the pretransition surface sensible heat flux) plotted against height (normalized by inversion depth) at various times for the idealized forcing case (see legends).

moved upwards, close to the mid-height of the boundary layer indicating a more symmetrical 244 eddy structure as observed by Nieuwstadt and Brost (1986). At later times, the vertical velocity 245 variance at the mid-point of the boundary layer continues to decay, while shear-driven turbulence 246 maintains velocity variance near the surface. Above the original CBL top, the variance does not 247 decay as it does over the rest of the layer. This shows that the free atmosphere is not rapidly 248 responding to the changes in surface forcing in the same way as the boundary layer, and suggests 249 that this velocity variance may be attributed to non-turbulent motions. The third moment of 250 vertical velocity rapidly decays to approximately zero throughout the boundary layer (Fig. 3c), 251 and the dissipation is sustained near the ground as a result of shear-driven turbulence (Fig. 3b). 252

253 3.1 Particle Dispersion in LES

To investigate the mean dispersive effect of the boundary-layer turbulence, particles are released in a uniform square grid spanning the horizontal domain of the model at a given height. The trajectories are calculated using the LES with the idealized forcing, with releases at times $t_d = 0$ and $t_d = 1200$ s, three release heights spanning the depth of the pre-transition CBL and 90,000 particles per release.

Figure 4a shows the mean plume height for particles released from three different levels at $t_d = 0$. The plumes released from low and mid levels tend to a mean height of approximately $z_i/2$ after 3000 s ($z_i = 1374$ m). The particles have thus become well-mixed throughout the layer, and so their horizontally integrated concentration will be unaffected by further decay of the CBL. The plumes released near the boundary-layer top deviate less from their starting point. This is due to the decay of TKE near the boundary-layer top.

The plume structure is shown further by the standard deviation (σ_z) for the same three simulations (Fig. 4b). Particles from both the low-level and mid-level releases spread out rapidly, with σ_z reaching 400 m. With a sharp boundary-layer capping inversion we would expect a uniform concentration profile up to some specified height; in this context we note that $\sigma_z = 400$ m corresponds to a uniform distribution of depth 1386 m, using the theoretical result σ_z



Fig. 3: Vertical profiles from the LES using the idealized forcing. Shown are (a) vertical velocity variance (resolved plus subgrid), (b) dissipation of TKE and (c) the third moment of vertical velocity at various times (t_d) after the switch-off of surface heat flux.

depth/ $\sqrt{12}$, and this is close to the actual boundary-layer depth of 1374 m. In the high release case, however, the particles disperse less rapidly and tend to a smaller spread at large times. This also indicates a reduction of TKE near the boundary-layer top early in the transition.

Figure 4c shows the mean plume height for particles released from the same heights as in Fig. 273 4a but at $t_d = 1200$ s. In this case, the mean height deviates little from the release height over 274 time. The reduced dispersion is also indicated by the standard deviation of these plumes, with 275 slower initial rates of spread and with σ_z tending to a smaller value of only 200 m in the case of 276 the high and low releases. The mid-level release has a larger standard deviation indicating more 277 motion near the middle of the boundary layer. This is supported by the profile of vertical velocity 278 variance in Fig. 3a. Before the transition, large-scale turbulent eddies, driven by surface heating, 279 transport and mix material over the entire depth of the boundary layer. After the transition the 280 large eddies decay, and mixing and vertical velocities are greatly reduced. 281

We now compare the LES particle simulations for a steady-state CBL with the experimental water-tank data of Willis and Deardorff (1976) and Willis and Deardorff (1978). Figure 5 shows



Fig. 4: Plume mean heights and standard deviations for releases from a range of heights at $t_d = 0$ ((a) and (b)) and at $t_d = 1200$ s ((c) and (d)) for the idealized forcing. Release heights are at 100 m (solid), 687 m (dashed) and 1260 m (dot-dashed). Inversion depth at $t_d = 0$ is 1374 m.

close agreement between the LES and the water-tank data. This validates our method for the CBL
 regime and gives us additional confidence in the dispersion results for the decaying-turbulence
 regime.

The trapping of particles close to their release height in the rapid transition leads to higher 287 concentrations than occur when the particles are strongly mixed. This is demonstrated by Figs. 288 6a and 6b where the height distribution of particle concentrations for releases before and after 289 the transition is given for a release height of 100 m. For the pre-transition release $(t_d = -1200 \text{ s})$, 290 particles mix over a deep layer and hence have a low concentration. However, for the post-291 transition release $(t_d = 1200 \text{ s})$, particles do not disperse away from their release height so 292 easily and remain in a shallow band at high concentrations. In order to understand this result 293 further, it is instructive to consider the characteristic physical scales after the transition, namely 294 the buoyancy scale z_b defined by $z_b = \sigma_w/N$. For this case $z_b \sim 150$ m and is the same order 295 of magnitude as σ_z (Fig. 4d) indicating that particle dispersion is strongly influenced by the 296 stratification. 297



Fig. 5: Plume height normalized by z_i plotted against time for a steady-state CBL. Results for the LES (solid) and one standard deviation either side (dashed) are shown for release heights of: (a) $z/z_i = 0.067$ and (b) $z/z_i = 0.24$. Plotted as circles are the experimental water-tank data of plume height from Willis and Deardorff (1976) and Willis and Deardorff (1978).



Fig. 6: Particle concentration (C_z) from a near-surface release occurring at (a) $t_d = -1200$ s and (b) $t_d = 1200$ s where t_d is the time after the switch-off of surface heat flux. Particles are released at height z = 100 m for the idealized forcing. Note that the time of the release shown in frame (a) is earlier than the time $t_d = 0$ used in the other figures.

²⁹⁸ 3.2 LSM and modified LSM predictions

²⁹⁹ Trajectories are also calculated using the LSM for release times of $t_d = 0$ and $t_d = 1200$ s and

³⁰⁰ for release heights near the surface, at a mid-level and at a high-level. As in the LES, 90,000

³⁰¹ particles are used per release. Figure 7 shows the mean plume heights and standard deviations

for releases at the start of the transition $(t_d = 0)$. At the start of the transition the boundary

layer is still significantly convective. For the near-surface releases (Fig. 7a), both the LSM and the LES mean plume heights are significantly greater than the release height. The LSM mean plume height deviates by about 100 m (12% difference) from the LES at the maximum point, but overall the LSM is in good agreement with the LES. The standard deviations in Fig. 7a indicate a closer agreement for the spread of the LSM and LES plumes. For the mid-level releases there is close agreement between the LES and LSM (Fig. 7b). For the high-level releases, whilst the mean plume heights differ by about 200 m, the plume spreads are much closer (Fig. 7c).

In contrast, Fig. 8 shows the mean plume heights and standard deviations for releases at 310 $t_d = 1200$ s. For the near-surface releases at a height of 100 m (Fig. 8a), the LSM significantly 311 over-predicts both the mean plume height (by 400 m after 10,000 s) and the spread. For the mid-312 level releases (Fig. 8b), the LSM produces a mean height that remains close to the release height, 313 in agreement with the LES; however, it over-predicts the spread. For the high-level releases (Fig. 314 8c), the LSM again over-predicts the spread of the plume relative to the LES. The over-dispersion 315 of particles by the LSM at times after the switch-off of surface sensible heat flux suggests that 316 the turbulence parameters supplied to the LSM are not fully describing the state of the boundary 317 layer during this period. The effect of stratification is not fully represented in the LSM. 318

The modified LSM adjusts the vertical velocity variance to account for the partitioning be-319 tween waves and turbulence in the stratified regions. Mean plume heights and spreads simulated 320 using the modified LSM are shown in Fig. 8. For the low-level releases (Fig. 8a), the LES shows 321 the mean plume height ascending slightly but remaining close to the height of release, indicating 322 low levels of turbulent mixing. This behaviour is captured well by the modified LSM, with the 323 mean plume height remaining within 50 m of the LES after 10,000 s, compared to 400 m in the 324 case of the LSM. The spread of the modified LSM is also much closer to the LES than the LSM 325 spread is. For the mid-level releases (Fig. 8b), all three models are in agreement for the mean 326 height which deviates little from the middle of the boundary layer, while the spread given by the 327 modified LSM agrees more closely with the LES than the LSM does. For the high-level releases 328 (Fig. 8c), the modified LSM is in close agreement with the LES for both the mean height and 329 spread. 330

331 3.3 Observed forcing

For the LES driven by the observed forcing, area-averaged boundary-layer properties at selected times are presented in Fig. 9. The area-averaged potential-temperature profile during the period of positive surface sensible heat flux (Fig. 9a) is that typical of a clear-sky CBL. As the heat flux decreases and becomes negative, a shallow SBL develops, deepening over time. In the residual layer above the developing SBL, the potential temperature has a slight positive gradient as discussed by Grant (1997) and Pino et al. (2006). As the sensible heat flux becomes negative in the lowest part of the boundary layer, the sensible heat flux in the residual layer tends to zero.

To calculate plume statistics for the observed forcing case, the trajectories of 90,000 particles 339 were simulated using the LES, the LSM and the modified LSM. Two particle release heights of 340 50 m and 500 m were used, with the 50 m release lying within the strongly positive temperature 341 gradient of the SBL shortly after it began to develop and with the 500 m release lying near 342 the middle of the residual mixed layer. The release time was decided upon by considering the 343 surface heat flux, the volume-averaged vertical velocity variance, and the potential-temperature 344 profile, to ensure particles were released during the period of rapid decay of the vertical velocity 345 variance. 346

Figure 10 shows the plume mean heights and standard deviations for the low and mid-level releases after the SBL has formed. For the low-level release (Fig. 10a), the LSM greatly over-

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Fig. 7: Time evolution of mean plume heights (solid lines) and \pm one standard deviation (dashed) for releases at the start of the transition ($t_d = 0$) and at: (a) 100 m, (b) 687 m and (c) 1260 m for the idealized forcing. Compared are the LES (black) and LSM (blue).



(a) Release height 100 m, after transition.





Fig. 8: Time evolution of mean plume heights (solid lines) and \pm one standard deviation (dashed) for releases after the transition ($t_d = 1200$ s) and at: (a) 100 m, (b) 687 m and (c) 1260 m for the idealized forcing. Compared are the LES (black), LSM (blue) and modified LSM (magenta).



Fig. 9: Vertical profiles of (a) potential temperature and (b) sensible heat flux (normalized by $\rho_0 c_p$, where ρ_0 is the surface density and c_p the specific heat capacity at constant pressure) at various times after the start of the simulation for the observed forcing. Times shown in legend.

predicts the vertical spread of the plume, which is likely to be due to the lack of representation of the stable stratification. This is a similar bias to that found for the idealized forcing. The modified

³⁵¹ LSM again predicts significantly reduced height and spread relative to the LSM, and predicts

³⁵² plume statistics much closer to the LES. For the mid-level release, Fig. 10b shows the LSM again

³⁵³ over-predicting the spread of the plume, whilst the modified LSM slightly under-predicts it.

354 4 Conclusions

In this paper we studied the dispersion of passive tracers during the evening-transition boundary 355 layer using both LES and LSM techniques. Whilst dispersion in steady-state boundary layers 356 has been much simulated, only a few studies that simulate dispersion in transitional boundary 357 layers exist. The LES, coupled to a particle model, exhibited the familiar effects of lofting of 358 particles released near the surface in the pre-transition CBL and trapping of particles in the 359 post-transition SBL. The LES, when forced by a sudden switch-off of the surface sensible heat 360 flux, showed that the vertical spread of particles away from the source height was significantly 361 reduced in the residual layer. This had the effect of increasing particle concentrations near the 362 source height. For the LES forced by observations, the development of a SBL of depth 100 m 363 resulted in very little vertical dispersion and even higher concentrations near the ground. These 364 LES results thus provide more information on the problem of trapping by the post-transition 365 SBL. 366

The LES results were then used to test two types of LSM. The first of these was a method 367 to simulate dispersion in non-stationary skewed turbulence. The second, the modified LSM, also 368 took into account the effect of stratification. The modified LSM is a simpler way of includ-369 ing stratification than that of Das and Durbin (2005). Both the LSM and the modified LSM 370 were driven by flow statistics from the LES. For particle releases occurring early in the evening 371 transition while the boundary layer is still convective, the LSM produced a fairly accurate repre-372 sentation of the plume statistics as simulated using the LES. For releases later in the transition, 373 however, the LSM significantly over-predicted plume heights for near-surface releases. In con-374



(a) Release height of 50 m, after transition (t = 20000 s).



(b) Release height of 500 m, after transition (t = 20000 s).

Fig. 10: Mean plume heights (solid lines) and \pm one standard deviation (dashed) for particle releases at t = 20,000 s from the start of the observed-forcing simulation (when a SBL is established). Compared are LES (black), LSM (blue) and modified LSM (magenta).

trast, the modified LSM corrected this bias and produced much closer agreement with the plume
 statistics generated by the LES.

We showed that, in modelling the stratified turbulence in residual layers and SBLs with LSMs, it is important to take account of the stratification, at least when the LSM is driven by vertical velocity variance, skewness and dissipation values from LES or measurements, which include contributions from waves and turbulence. The usual formulations of LSMs do not fully account for stratification. Our simulations also highlighted the important role of residual-layer turbulence in dispersing material above the SBL and of SBL stratification in inhibiting vertical dispersion during the evening transition. We also note that our results could apply to spatial transitions, ³⁸⁴ for example for a plume moving from land to cooler water (although the analogy is not exact

as space and time do not have a one-to-one relationship due to wind varying with height and

to along-wind turbulence). Our results suggest that operational dispersion models would benefit from development in the treatment both of residual-layer turbulence and of stratification in

³⁸⁸ evening-transition boundary layers.

³⁸⁹ Appendix - LSM including skewness and time dependence

³⁹⁰ Here we outline the formulation of the LSM used in this study. The LSM differs from the normal ³⁹¹ formulation (Eqs. 3-6) by the inclusion of skewness and time dependence. We modify a(z, w) and ³⁹² b(z, w) in Eq. 3 to now be functions of time, i.e. a = a(z, w, t) and b = b(z, w, t). Equations 3 and ³⁹³ 4 have a corresponding Fokker-Planck equation, and we require this to have a solution equal to ³⁹⁴ the probability density function of the positions and velocities of all air parcels (P(w, z, t)), i.e. ³⁹⁵ we require the 'well-mixed condition' (Thomson, 1987) to be satisfied.

With the assumption that b is given by Eq. 6, manipulation of the Fokker-Planck equation will allow the determination of a(z, w, t) for a given form of P(w, z, t). The Fokker-Planck equation can be written in terms of the probability flux in the w direction, ϕ , as

$$\frac{\partial \phi}{\partial w} = -\frac{\partial P}{\partial t} - \frac{\partial}{\partial z}(wP),\tag{14}$$

399 where

$$\phi = aP - \frac{\partial}{\partial w} \left(\frac{C_0 \epsilon}{2} P\right),\tag{15}$$

⁴⁰⁰ and the boundary condition of no flux at infinity is

$$\phi \to 0 \text{ as } |w| \to \infty. \tag{16}$$

⁴⁰¹ The procedure for deriving the LSM is to first prescribe a form for P, whether skewed, time-⁴⁰² dependent or both, and then determine ϕ using Eqs. 14 and 16. Once ϕ is determined, a(z, w, t)⁴⁰³ can be found from Eq. 15.

404 Including skewness

In order to include skewness, P is specified, following Baerentsen and Berkowicz (1984), as the weighted sum of two Gaussian distributions

$$P = F_1 P_1 + F_2 P_2, (17)$$

407 where

$$P_{1,2} = \frac{1}{\sqrt{2\pi\sigma_{1,2}}} \exp\left[-\frac{1}{2}\left(\frac{w - w_{1,2}}{\sigma_{1,2}}\right)^2\right],\tag{18}$$

and F_1 and F_2 are the weights. At this stage P is assumed time independent. We then follow Luhar and Britter (1989) and substitute Eqs. 17 and 18 into Eq. 14 and integrate with respect to w. The expression for ϕ for the time independent case (ϕ_s) is then found to be

$$\phi_{s} = -\frac{1}{2} \left(1 + \operatorname{erf} \frac{v_{1}}{\sqrt{2}} \right) \frac{\partial}{\partial z} \left(F_{1}w_{1} \right) - \frac{1}{2} \left(1 + \operatorname{erf} \frac{v_{2}}{\sqrt{2}} \right) \frac{\partial}{\partial z} \left(F_{2}w_{2} \right) + P_{1}\sigma_{1} \left\{ \left(\frac{\partial}{\partial z} \left(F_{1}\sigma_{1} \right) + \frac{F_{1}w_{1}}{\sigma_{1}} \frac{\partial w_{1}}{\partial z} \right) + \left(F_{1} \frac{\partial w_{1}}{\partial z} + \frac{F_{1}w_{1}}{\sigma_{1}} \frac{\partial \sigma_{1}}{\partial z} \right) v_{1} + F_{1} \frac{\partial \sigma_{1}}{\partial z} v_{1}^{2} \right\} + P_{2}\sigma_{2} \left\{ \left(\frac{\partial}{\partial z} \left(F_{2}\sigma_{2} \right) + \frac{F_{2}w_{2}}{\sigma_{2}} \frac{\partial w_{2}}{\partial z} \right) + \left(F_{2} \frac{\partial w_{2}}{\partial z} + \frac{F_{2}w_{2}}{\sigma_{2}} \frac{\partial \sigma_{2}}{\partial z} \right) v_{2} + F_{2} \frac{\partial \sigma_{2}}{\partial z} v_{2}^{2} \right\}$$
(19)

411 where

412 and

$$v_1 = \frac{w - w_1}{\sigma_1} \tag{20}$$

$$v_2 = \frac{w - w_2}{\sigma_2}.\tag{21}$$

Following Hudson and Thomson (1994), the values of F_1 , F_2 , w_1 , w_2 , σ_1 and σ_2 are set by ensuring that the variance (σ_w^2) and skewness $(S = \overline{w^3}/\sigma_w^3)$ of P match the values from the LES, by imposing the constraints that the integral of P is one and the mean of w is zero, and by making the choice $w_1/\sigma_1 = -w_2/\sigma_2 = S^{1/3}$. This yields

$$w_1 = \alpha \sigma_1, \tag{22}$$

$$w_2 = -\alpha \sigma_2, \tag{23}$$

$$F_1 = \sigma_2 / (\sigma_1 + \sigma_2), \tag{24}$$

$$F_2 = \sigma_1 / (\sigma_1 + \sigma_2),$$
 (25)

$$\sigma_1 = \sigma_2 + \gamma/\beta,\tag{26}$$

421 and

$$\sigma_2 = \frac{1}{2} \{ \sqrt{\gamma^2 / \beta^2 + 4\beta} - \gamma / \beta \}$$
(27)

where $\alpha = S^{1/3}$, $\beta = \sigma_w^2/(1 + \alpha^2)$ and $\gamma = \overline{w^3}/(3\alpha + \alpha^3)$. The choice $w_1/\sigma_1 = -w_2/\sigma_2 = S^{1/3}$ ensures P is Gaussian for S = 0.

424 Including time dependence

The above derivation can now be repeated, but without assuming that P is time independent. The integral of P with respect to w can be written as

$$\int_{-\infty}^{w} P(w', z, t) \, dw' = T_1 + T_2, \tag{28}$$

where T_1 and T_2 are the contributions from the Gaussian distributions P_1 and P_2 and w' is a dummy variable. Using Eq. 14, the expression for ϕ including both skewness and time-dependence is

$$\phi = -\frac{\partial}{\partial t} \left(T_1 + T_2 \right) + \phi_s \tag{29}$$

430 where the tendencies of T_1 and T_2 are given by

$$\frac{\partial}{\partial t}T_1 = \frac{1}{2}\left(\operatorname{erf}\frac{v_1}{\sqrt{2}} + 1\right)\frac{\partial F_1}{\partial t} - P_1\sigma_1\left[\frac{F_1}{\sigma_1}\frac{\partial w_1}{\partial t} + \frac{F_1}{\sigma_1}\frac{\partial \sigma_1}{\partial t}v_1\right],\tag{30}$$

$$\frac{\partial}{\partial t}T_2 = \frac{1}{2}\left(\operatorname{erf}\frac{v_2}{\sqrt{2}} + 1\right)\frac{\partial F_2}{\partial t} - P_2\sigma_2\left[\frac{F_2}{\sigma_2}\frac{\partial w_2}{\partial t} + \frac{F_2}{\sigma_2}\frac{\partial \sigma_2}{\partial t}v_2\right].$$
(31)

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