

Optimization of a Pressing Diagram in OSB Pressing

Optimizacija dijagrama prešanja pri prešanju OSB ploča

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ABSTRACT • This paper summarizes the results of a pressing diagram optimization based on changes in pressure, temperature and distance between frames of a continuous press during Oriented Strand Boards (OSB) pressing. Tests of selected mechanical properties were carried out on OSB/3 boards with a nominal thickness of 18 mm - a basic type with urea-formaldehyd (UF) glue in surface layers and isocyanate glue (PMDI) in the central layer and further an ECO type with PMDI glue in all layers produced by a prominent manufacturer of OSB boards in the Czech Republic. OSB/3 boards are intended for structural purposes for use in wet environments. Changes in the pressing diagram were carried out at the stage of “press opening”, which significantly affects mechanical and physical properties of OSB boards. In order to be able to compare the effects of changes in the pressing curve, the same setting of production parameters was used with all tested boards. The results of laboratory tests were compared with the values given in the ČSN EN 300 Standard. Optimization of the pressing process ranks among the most effective measures to increase the quality of particle boards at zero or minimum costs. The control of production processes is increasingly perfect thanks to the development of electronics, control and computer technology. At present, not only in our country but also worldwide, marked development of wooden constructions occurs thanks to the development of new types of wood-based composite materials and to the development of technologies in building industry. OSB boards are an important representative of wood-based composite materials for wooden constructions. As compared to natural material, OSB boards show a homogenous structure not including natural defects typical of solid wood. From the point of view of physical and mechanical properties, OSB boards are of orthotropic character.

Keywords: OSB, pressing, technical properties, isocyanate glue (PMDI), urea-formaldehyd glue (UF)

SAŽETAK • U radu se prikazuju rezultati optimizacije dijagrama prešanja utemeljeni na promjenama tlaka, temperature i udaljenosti između okvira kontinuirane preše pri prešanju ploča s usmjerenim iverjem – OSB ploča (Oriented Strand Boards). Mehanička svojstva mjerena su na pločama OSB/3, nominalne debljine 18 mm, na osnovnom tipu ploče s urea-formaldehidnim (UF) ljepilom u vanjskom sloju i izocijanatnim (PMDI) ljepilom u središnjem sloju te na ekološkom tipu ploče s PMDI ljepilom u svim slojevima, koje je proizveo priznati proizvođač OSB ploča u Republici Češkoj. OSB/3 ploče upotrebljavaju se za konstrukcijske svrhe u vlažnom okruženju. Promjene u dijagramu prešanja napravljene su u fazi “otvaranja preše”, koja bitno utječe na mehanička i fizikalna svojstva OSB ploča. Da bi se mogli uspoređivati učinci promjena u dijagramu prešanja, za sve su uzorke ploča upotrijebljeni jednaki parametri proizvodnje. Rezultati laboratorijskih mjerenja uspoređeni su s podacima iz norme ČSN EN 300. Optimizacija procesa prešanja pripada najučinkovitijim načinima povećanja kvalitete ploča iverica uz male troškove ili bez ikakvih izdataka. Kontrola procesa proizvodnje postala je bitno bolja zahvaljujući razvoju elektronike, kontrolne i računalne tehnologije. Trenutačno se u svijetu bilježi znatan porast upotrebe kon-

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strukcijskog drva zahvaljujući razvoju novih kompozitnih materijala od drva i novih tehnologija građenja. OSB ploče važan su predstavnik kompozitnih materijala za drvene konstrukcije. U usporedbi s prirodnim materijalima, prednost OSB ploča je to što imaju homogenu strukturu bez grešaka koje su tipične za masivno drvo. Sa stajališta fizikalnih i mehaničkih svojstava, OSB ploče su ortotropan materijal.

Ključne riječi: OSB ploče, tehnička svojstva, izocijanatno ljepilo (PMDI), urea-formaldehidno ljepilo (UF)

1 INTRODUCTION

1. UVOD

Hot pressing is considered to be the most important operation in the whole process of particleboard production. The aim of pressing is to compress particle mats to a required thickness and also to densify and fix the chips in this stage through glue hardening. The particle mat represents a complicated system of wood particles, water and chemical admixtures, which is fed into the wedged entrance of a hot continuous press where it is gradually thickened to a nominal thickness through the pressure of steel pressing belts and, at the same time, heated by the belts to the required reaction temperature (Kühne and Belimow, 1978). After passing all stages of the pressing process and after partial cooling and reducing the working pressure in the last part of the continuous press, the pressed material leaves the press (Hrázský and Král, 2007).

Immediately after putting the chip mat into the press, surface layers of the mat meet with hot pressing belts of the continuous press and thus intensive exchange occurs between the belts and the chip mat. This intensity depends on the temperature gradient whose size is continuously changed in the hot pressing process because the chip mat temperature changes during this procedure. The process of the heat transfer occurs in two directions, namely perpendicular to the board plane and in parallel with the board plane. The transfer of heat is realized through heat conductivity, convection and heat emission (radiation). The heat conductivity of a chip mat is calculated from the heat conductivity of wood particles, water, air and chemical admixtures. The heat transfer through the material originates from the flow of water vapour and diffusion of moisture contained in the chip mat. (Bolton *et al*, 1989). In consequence of the unevenly distributed moisture in the chip mat and moisture differences between the chip mat and surroundings, two moisture gradients occur, thereby generating moisture diffusion. The first moisture gradient becomes particularly evident perpendicular to the mat plane towards the central layer of the mat. After drying-up the upper chip layer, the direction of this gradient changes by 180°, simultaneously with the change of the pressure gradient direction. The second moisture gradient occurs in parallel with the mat plane toward the surroundings. The transfer of heat by the flow of water vapours and gases is particularly intensive. Their flow is caused by producing inner pressure. At the contact of hot pressing belts (about 220 °C) with the chip mat, intensive formation of vapours occurs first in the surface zone. At the same time, air contained in the surface layer is heated, which results in increasing the volume. Therefore, corre-

sponding overpressure is generated in the mat surface zone, which results in the development of two pressure gradients. One pressure gradient occurs in the direction perpendicular to the chip mat plane. At the beginning of pressing, its direction first takes place towards the inner layers of the mat. After heating the central layer to a temperature of about 100 °C, the inner pressure is generated in this area by vapours formed from the existing moisture, which will result in the change of the direction of pressure gradient by 180°. Through this pressure in the chip mat, the second pressure gradient is created, which functions in parallel with the mat plane towards the surroundings. The time effect of pressure and temperature gradients results in the process of material transfer in the hot pressing process. Heat, material and pressure processes determine to a great extent the quality of products and the production line productivity. The compressing process in the press is controlled from outside through temperature, pressure and the speed of the maximum working pressure start. The higher the temperature the higher the relative resistance to the compression of a chip mat not yet heated (Deppe and Ernst, 1991).

The pressing temperature will always play an important - crucial role. The pressing cycle principally consists of three stages: time t_1 – until reaching the nominal thickness of a pressed material, time t_2 – effects of the maximum working pressure and the course of an actual board-formation process, t_3 – ventilation, cooling, pressure reduction and leaving the continuous press. The course of the pressing process is programmed in practice. If pressure and time are selected as control values (p, t_1 – program), the speed of reaching the nominal thickness and maximum working pressure depends on the resistance of the pressed material to pressing (compression). If travel and pressure are the starting basis (s, p – program), then resistance to pressing (compression) is affected by time t_1 and in a program the distance from the entry point, time (s, t – program), is the third control element, i.e. pressure in pistons (hydraulic pressure). External control values, namely pressure (p), piston speed (v) and time (t) are measurable and adjustable; they can be set within certain limits. As the inner resistance to pressing (compression) is unknown and measurable with difficulties, only two external control values are always programmable. In the course of the development of particleboards, both pressing temperature and working pressure were increased (Štefka, 1999).

There were expectations that rapid achievement of maximum pressing pressure will be avoided by using low-quality surface area, but they were not always satisfactorily met.

Table 1 Adjusted manufacturing parameters for OSB/3, 18 mm nominal thickness

Tablica 1. Postavljeni proizvodni parametri za ploče OSB/3 nominalne debljine 18 mm

Nominal thickness <i>Nominalna debljina</i> mm	Press factor <i>Faktor prešanja</i> s/mm	Calculating density <i>Izračunana gustoća</i> kg/m ³	Amount of glue <i>Količina ljepila</i>		Chips moisture content before blending <i>Sadržaj vode u iverju prije miješanja</i>	
			UF (SL*) %	PMDI (ML*) %	SL %	ML %
18.0	7.54	575	3.1	3.5	5.1	3.9

*SL – surface layer / *vanjski sloj*; ML – middle layer / *središnji sloj*

Table 2 Adjusted manufacturing parameters for OSB/3 ECO, 18 mm nominal thickness

Tablica 2. Postavljeni proizvodni parametri za ekološke ploče OSB/3 ECO nominalne debljine 18 mm

Nominal thickness <i>Nominalna debljina</i> mm	Press factor <i>Faktor prešanja</i> s/mm	Calculating density <i>Izračunana gustoća</i> kg/m ³	Amount of glue <i>Količina ljepila</i>		Chips moisture content before blending <i>Sadržaj vode u iverju prije miješanja</i>	
			PMDI (SL*) %	PMDI (ML*) %	SL %	ML %
18.0	7.54	575	3.1	3.5	5.1	3.9

*SL – surface layer / *vanjski sloj*; ML – middle layer / *središnji sloj*

Štefka (2007) supposed that residual stress was caused by the pressure of vapours originating from moisture contained in the chip mat. This fact can cause not only larger or smaller springing of the board, but at excessive moisture, also ripping of the board. Therefore, the pressing process has to be carried out in such a way not only to achieve the optimum construction of particle boards from the aspect of the density profile but also the required strength of bonding the chips, which is, as a matter of fact, the basic condition of good properties of particleboards.

The aim of this paper was to optimize the pressing diagram on the basis of measuring changes of pressure and temperature and distance between frames of a continuous press in the board in OSB pressing. Changes of the pressing curve were carried out at the stage of “press opening” because these changes substantially affected physical and mechanical properties of OSB boards.

2 MATERIAL AND METHODS

2. MATERIJAL I METODE

Pressing the OSB boards was carried out using the Dieffenbacher CPS 280-53/OSB continuous press, an OSB production line of a prominent Czech manufacturer of board composite materials in the Czech Republic. The pressing process proceeded between two steel belts running along a fixed pressing line. This line consists of 41 identical pressing frames. Furthermore, the press consists of an upper and lower heating plate. The lower plate is supported by 160 hydraulic cylinders, situated on lower beams. The lower heating plate moves up by means of hydraulics producing pressure on the chip mat through roller chains and steel belts. Warming the heating plates is performed by thermo oil. In the process of pressing in a continuous press, the following pressure and temperature phases are distinguished:

Pressing phase	Temperature, °C	Specific pressure, N/mm ²
1- Input	220 – 225	3.0
2-	215 - 230	1.6
3- Centre	215 – 225	1.7
4-	205 – 215	0.8
5- Output	200 – 180	0.05

Setting the production parameters of the OSB line:

The course of a pressing diagram particularly affects the bending strength (MOR), modulus of elasticity in bending (MOE) and most of all tensile strength perpendicular to the board plane. OSB boards sampled for tests of the OSB mechanical properties were glued in 1.1 – 1.3 variants by using UF glue in surface layers and by PMDI glue in the central layer (Tab. 1). In variants 2.1 – 2.3, the PMDI glue is used both for surface and central layers (Tab. 2). Requirements for boards of the OSB/3 technical class are determined by the ČSN EN 300 Standard. Test procedures to determine the bending strength in both axes are described in the ČSN EN 310 Standard and a test procedure to determine the tensile strength perpendicular to the board plane is described in the ČSN EN 319 Standard.

OSB/3 boards within thickness ranging between 18 and 25 mm have to fulfil the following requirements according to the ČSN EN 300 Standard – see Tab. 3.

In the manufacture of experimental OSB boards, for each variant of the pressing diagram three trial boards were sampled at the stage of “press opening” and necessary test specimens were cut from the boards according to the cutting plan (Fig. 1). At the end of pressing (all variants), the following tracks were selected: in variants 1.1 and 2.1 very fast “press opening” (i.e. larger distances in setting gaps between frames and larger differences in pressure between particular frames of the press – see Tabs. 4 and 7), in variants 1.2 and 2.2 gradual “press opening” (i.e. smaller differences between frame distances and smaller differences in pressure between particular frames) – see Tabs. 5 and 8 and in variants 1.3 and 2.3 very gradual “press opening” (i.e. small differences between distances of frames and small differences in pressure between particular frames of the press) – see Tabs. 6 and 9.

Test specimens were cut from sampled experimental OSB boards of particular variants, and tests were carried out of selected mechanical properties. Dimensions of test specimens are determined by the ČSN EN 325 Standard. To obtain test specimens, the manufacturer plan of cutting (sawing) was used (Fig. 1).

Table 3 Requirements related to OSB/3 according to ČSN EN 300

Tablica 3. Zahtjevi za OSB ploče prema ČSN EN 300

OSB/3	Standard Norma	Unit Jedinica	Requirements / Zahtjevi		
			Range of thickness, mm (nominal values) Raspon nominalnih debljina, mm		
			6 to 10	>10 to <18	18 to 25
Properties / Svojstvo					
MOR \parallel	ČSN EN 310	N/mm ²	22	20	18
MOR \perp	ČSN EN 310	N/mm ²	11	10	9
MOE \parallel	CSN EN 310	N/mm ²	3500	3500	3500
MOE \perp	ČSN EN 310	N/mm ²	1400	1400	1400
σ_{\perp}	ČSN EN 319	N/mm ²	0.34	0.32	0.30
Swelling / Bubrenje	ČSN EN 317	%	15	15	15

Legend / Legenda: MOR – Bending strength / savojna čvrstoća; MOE – Modulus of elasticity / modul elastičnosti; σ_{\perp} – Tensile strength perpendicular / vlačna čvrstoća okomito

Table 4 Variant 1.1 – Optimization of press diagram – „very fast press opening“

Tablica 4. Varijanta 1.1 – optimizacija dijagrama prešanja – „vrlo brzo otvaranje preše“

OSB/3 – surface layer: UF resin / vanjski sloj: UF ljepilo middle layer: PMDI resin / središnji sloj: PMDI ljepilo	Frame No. 36	Frame No. 37	Frame No. 38	Frame No. 39	Frame No. 40	Frame No. 41
Working pressure, N/mm ² / Radni tlak, N/mm ²	0.80	0.70	0.60	0.50	0.20	0.05
Pressing temperature, °C / Temperatura prešanja, °C	205	200	195	190	185	180
Distance between press frame, mm Udaljenost između okvira preše, mm	17.8	17.9	18.2	18.5	19.25	21.0

Table 5 Variant 1.2 – Optimization of press diagram – „gradual press opening“

Tablica 5. Varijanta 1.2 – optimizacija dijagrama prešanja – „postupno otvaranje preše“

OSB/3 – surface layer: UF resin / vanjski sloj: UF ljepilo middle layer: PMDI resin / središnji sloj: PMDI ljepilo	Frame No. 36	Frame No. 37	Frame No. 38	Frame No. 39	Frame No. 40	Frame No. 41
Working pressure, N/mm ² / Radni tlak, N/mm ²	0.80	0.75	0.70	0.65	0.30	0.05
Pressing temperature, °C / Temperatura prešanja, °C	205	200	195	190	185	180
Distance between press frame, mm Udaljenost između okvira preše, mm	17.8	17.9	18.0	18.25	18.75	19.5

Table 6 Variant 1.3 – Optimization of press diagram – „very gradual press opening“

Tablica 6. Varijanta 1.3 – optimizacija dijagrama prešanja – „vrlo postupno otvaranje preše“

OSB/3 – surface layer: UF resin / vanjski sloj: UF ljepilo middle layer: PMDI resin / središnji sloj: PMDI ljepilo	Frame No. 36	Frame No. 37	Frame No. 38	Frame No. 39	Frame No. 40	Frame No. 41
Working pressure, N/mm ² / Radni tlak, N/mm ²	0.75	0.72	0.68	0.65	0.45	0.05
Pressing temperature, °C / Temperatura prešanja, °C	205	200	195	190	185	180
Distance between press frame, mm Udaljenost između okvira preše, mm	18.0	18.1	18.2	18.3	18.4	18.5

Table 7 Variant 2.1 – Optimization of press diagram – „very fast press opening“

Tablica 7. Varijanta 2.1 – optimizacija dijagrama prešanja – „vrlo brzo otvaranje preše“

OSB/3 – surface layer: PMDI resin / vanjski sloj: PMDI ljepilo middle layer: PMDI resin / središnji sloj: PMDI ljepilo	Frame No. 36	Frame No. 37	Frame No. 38	Frame No. 39	Frame No. 40	Frame No. 41
Working pressure, N/mm ² / Radni tlak, N/mm ²	0.80	0.70	0.60	0.50	0.20	0.05
Pressing temperature, °C / Temperatura prešanja, °C	205	200	195	190	185	180
Distance between press frame, mm Udaljenost između okvira preše, mm	17.8	17.9	18.2	18.5	19.25	21.0

Table 8 Variant 2.2 – Optimization of press diagram – „gradual press opening“

Tablica 8. Varijanta 2.2 – optimizacija dijagrama prešanja – „postupno otvaranje preše“

OSB/3 – surface layer: PMDI resin / vanjski sloj: PMDI ljepilo middle layer: PMDI resin / središnji sloj: PMDI ljepilo	Frame No. 36	Frame No. 37	Frame No. 38	Frame No. 39	Frame No. 40	Frame No. 41
Working pressure, N/mm ² / Radni tlak, N/mm ²	0.80	0.75	0.70	0.65	0.30	0.05
Pressing temperature, °C / Temperatura prešanja, °C	205	200	195	190	185	180
Distance between press frame, mm Udaljenost između okvira preše, mm	17.8	17.9	18.0	18.25	18.75	19.5

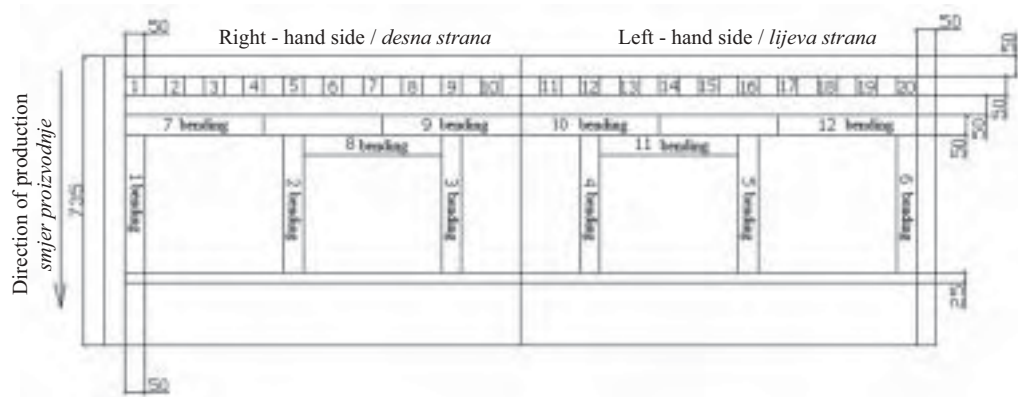


Figure 1 Cutting plan for sampling test specimens (1-20: tensile strength perpendicular to the board surface; 1-12 bending: MOR and MOE)

Slika 1. Plan rezanja za izradu uzoraka (1-20 uzorci za mjerenje vlačne čvrstoće okomito na površinu ploče; 1-12 uzorci za savijanje i mjerenje veličina MOR i MOE)

Table 9 Variant 2.3 – Optimization of press diagram – „very gradual press opening“

Tablica 9. Varijanta 2.3 – optimizacija dijagrama prešanja – „vrlo postupno otvaranje preše“

OSB/3 – surface layer: PMDI resin / vanjski sloj: PMDI ljepilo middle layer: PMDI resin / središnji sloj: PMDI ljepilo	Frame No. 36	Frame No. 37	Frame No. 38	Frame No. 39	Frame No. 40	Frame No. 41
Working pressure, N/mm ² / Radni tlak, N/mm ²	0.75	0.72	0.68	0.65	0.45	0.05
Pressing temperature, °C / Temperatura prešanja, °C	205	200	195	190	185	180
Distance between press frame, mm Udaljenost između okvira preše, mm	18.0	18.1	18.2	18.3	18.4	18.5

3 RESULTS AND DISCUSSION

3. REZULTATI I RASPRAVA

Laboratory tests were carried out on OSB/3 and OSB/3 ECO of 18-mm nominal thickness. The actual average values of thickness of the OSB/3 variants 1.1–1.3 and OSB/3 ECO variants 2.1–2.3 are listed in Tabs. 10–11. The results of tests of mechanical properties are shown in Tabs. 12–17.

The actual average values of thickness of the OSB/3 1.1–1.3 and OSB/3 ECO variants 2.1–2.3 are listed in Tabs. 10–11. The values are lower than 18 mm. Technical properties of OSB boards were, therefore, considered in the thickness category ranging between 10 and 18 mm.

The measurement of density showed that at the set value of production density of 575 kg/m³, the highest increase of mean density occurred in variants OSB ECO 2.1 and 2.2 (580 kg/m³) and, on the contrary, the highest decline of mean density (below the set production value)

was determined in variant OSB 1.2 (574 kg/m³). The mean density of variant OSB 1.1 reached the set production density (575 kg/m³). Hence, from the aspect of the density evaluation, this variant appears to be the most suitable. Based on the comparison between the requirements of the ČSN EN 300 Standard and the measured values, the density of variants OSB and OSB ECO ranges within the set limits ± 15 % according to the general requirements for particular types of OSB boards.

As for tensile strength perpendicular to the board plane, our measurements demonstrated that the highest decline of its mean value occurred in variant OSB 1.1 (0.31 N/mm²). This value does not meet the requirements of the ČSN EN 300 Standard for OSB/3 (0.32 N/mm²). The highest increase in the mean value of tensile strength perpendicular to the board plane occurred in Variant OSB 1.2 (0.38 N/mm²) and the lowest increase in variants OSB ECO 2.1 and 2.2 (0.35 N/mm²). In other variants all determined values of tensile strength perpen-

Table 10 Average thickness of OSB/3 for variants 1.1–1.3

Tablica 10. Srednja vrijednost debljine OSB/3 za varijante 1.1–1.3.

Thickness, mm / Debljina, mm	Variant 1.1 / Varijanta 1.1.				Variant 1.2 / Varijanta 1.2.				Variant 1.3 / Varijanta 1.3.			
	1	2	3	\bar{x}	1	2	3	\bar{x}	1	2	3	\bar{x}
Average value \bar{x} Srednja vrijednost	17,75	17,44	17,36	17,52	17,45	17,53	17,62	17,53	17,55	17,54	17,43	17,51

Table 11 Average thickness of OSB/3 ECO for variants 2.1–2.3

Tablica 11. Srednja vrijednost debljine OSB/3 ECO za varijante 2.1–2.3.

Thickness, mm / Debljina, mm	Variant 2.1 / Varijanta 1.1.				Variant 2.2 / Varijanta 1.2.				Variant 2.3 / Varijanta 1.3.			
	1	2	3	\bar{x}	1	2	3	\bar{x}	1	2	3	\bar{x}
Average value \bar{x} Srednja vrijednost	17,48	17,24	17,48	17,52	17,66	17,19	17,58	17,48	17,40	17,45	17,58	17,48

Table 12 Statistical evaluation for variant 1.1, OSB/3, 18 mm nominal thickness

Tablica 12. Statistička procjena rezultata za varijantu 1.1, OSB/3 nominalne debljine 18 mm

Variant 1.1 / Varijanta 1.1. High-speed press opening <i>Vrlo brzo otvaranje preše</i>	Density <i>Gustoća</i> kg/m ³	σ_L N/mm ²	MOR N/mm ²	MOE N/mm ²	MOR ⊥ N/mm ²	MOE ⊥ N/mm ²
<i>OSB No.1</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 1.</i>	571	0.31	22.04	4627	13.85	2328
Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	334.232	0.001	3.811	289611.868	1.694	7176.817
<i>OSB No.2</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 2.</i>	580	0.30	23.73	4864	14.21	2396
Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	535.787	0.003	39.873	1154673.544	4.495	22850.805
<i>OSB No.3</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 3.</i>	572	0.31	25.01	4971	12.14	1984
Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	806.876	0.001	13.886	499806.464	0.888	38764.905
Total average value $\bar{\bar{x}}$ / <i>Ukupna srednja vrijednost</i>	575	0.31	23.62	4821	13.40	2236
Variance of average values within the board s OSB 1–3 s_x^2 <i>Varijanca srednje vrijednosti za ploče OSB 1–3.</i>	27.539	0.00008	1.991	31015.143	1.220	48766.625
Average value of variance values within the boards OSB 1–3 s_w^2 <i>Srednja vrijednost varijanci za ploče OSB 1–3.</i>	558.965	0.002	19.190	648030.626	2.359	22930.842

Legend / *Legenda*: MOR – Bending strength / *savojna čvrstoća*; MOE – Modulus of elasticity / *modul elastičnosti*; σ_L – Tensile strength perpendicular / *vlačna čvrstoća okomito*

dicular to the board plane meet the requirements of the ČSN EN 300 Standard, viz. 0.32 N/mm².

The highest mean value of the bending strength in the main axis was determined in variant OSB 1.1 (23.62 N/mm²) and the lowest mean values were measured in variant ECO 2.1 (21.12 N/mm²). The ČSN EN 300 Standard requirement for this property is ≥ 20 N/mm². Hence, satisfactory values were achieved in all variants. The highest mean value of the bending strength in the secondary axis was determined in variant ECO 2.2 (14.70 N/mm²) and the lowest mean value

in variant OSB 1.2 (12.74 N/mm²). The ČSN EN 300 Standard requirement for this property is ≥ 10 N/mm². Hence, satisfactory values were achieved in all variants.

The highest determined mean value of the modulus of elasticity in the main axis was found with OSB 1.3 (4956 N/mm²) and the lowest mean value in variant ECO 2.2 (4754 N/mm²). The ČSN EN 300 Standard requirement for this property is ≥ 3500 N/mm². Consequently, satisfactory values were achieved in all variants.

Table 13 Statistical evaluation for variant 1.2, OSB/3, 18 mm nominal thickness

Tablica 13. Statistička procjena rezultata za varijantu 1.2, OSB/3 nominalne debljine 18 mm

Variant 1.2 / Varijanta 1.2. Gradual press opening <i>Postupno otvaranje preše</i>	Density <i>Gustoća</i> kg/m ³	σ_L N/mm ²	MOR N/mm ²	MOE N/mm ²	MOR ⊥ N/mm ²	MOE ⊥ N/mm ²
<i>OSB No.1</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 1.</i>	575	0.39	21.96	4 886	13.55	2 330
Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	588.467	0.008	3.567	51 934.749	4.515	30 658.713
<i>OSB No.2</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 2.</i>	574	0.39	24.02	4 825	12.36	2 018
Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	216.046	0.001	11*.032	282 853.177	1.119	29 063.316
<i>OSB No.3</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 3.</i>	572	0.36	23.92	5 048	12.30	2 140
Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	219.775	0.005	38.988	373 282.153	3.295	77 016.000
Total average value $\bar{\bar{x}}$ / <i>Ukupna srednja vrijednost</i>	574	0.38	23.30	4 920	12.74	2 163
Variance of average values within the board s OSB 1–3 s_x^2 / <i>Varijanca srednje vrijednosti za ploče OSB 1–3.</i>	3.634	0.00026	1.462	13 235.755	0.492	24 666.315
Average value of variance values within the boards OSB 1–3 s_w^2 <i>Srednja vrijednost varijanci za ploče OSB 1–3.</i>	341.429	0.005	17.862	236 023.359	2.976	45 579.343

Table 14 Statistical evaluation for variant 1.3, OSB/3, 18 mm nominal thickness

Tablica 14. Statistička procjena rezultata za varijantu 1.3, OSB/3 nominalne debljine 18 mm

Variant 1.3 / Varijanta 1.3. Highly gradual press opening <i>Vrlo postupno otvaranje preše</i>	Density <i>Gustoća</i> kg/m ³	σ_{\perp} N/mm ²	MOR N/mm ²	MOE N/mm ²	MOR \perp N/mm ²	MOE \perp N/mm ²
<i>OSB No.1</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 1.</i>	579	0.41	22.52	4 938	12.76	2 336
Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	668.390	0.004	10.526	213 257.723	1.424	15 029.237
<i>OSB No.2</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 2.</i>	578	0.34	23.90	4 973	14.01	2 313
Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	444.462	0.004	10.254	267 188.534	0.538	28 779.073
<i>OSB No.3</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 3.</i>	571	0.37	21.85	4 958	12.89	2 244
Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	78.012	0.004	18.062	713 755.949	3.154	54 230.130
Total average value $\bar{\bar{x}}$ / <i>Ukupna srednja vrijednost</i>	576	0.37	22.76	4 956	13.22	2 298
Variance of average values within the board s OSB 1–3 $s_{\bar{x}}^2$ / <i>Varijanca srednje vrijednosti za ploče OSB 1–3.</i>	18.830	0.001	0.230	306.753	0.468	2 304.553
Average value of variance values within the boards OSB 1–3 \bar{s}_w^2 / <i>Srednja vrijednost varijanci za ploče OSB 1–3.</i>	396.955	0.004	12.947	398 067.402	1.705	32 679.480

The highest mean value of the modulus of elasticity in the secondary axis was found in variant ECO 2.2 (2378 N/mm²) and the lowest mean value on average in variant OSB 1.2 (2163 N/mm²). The ČSN EN 300 Standard requirement for this property is ≥ 1400 N/mm². Hence, satisfactory values were achieved in all variants.

We believe that the possible reasons for the lower values of tensile strength perpendicular to board plane in variant 1.1 and higher number of cracks are caused by compressing of chip mats resulting in inner elastic forces. The size of these forces depend strongly on the morphological size of the characteristic parameters of chips, fractions, tree species, moisture, temperature,

specific compression pressure and possibly of compression speed. The coherence of boards for venting and discharge of the press is based on the cohesion of gluing bridges that are formed by pressing. The mat always finds places that are more compressed. In the finished boards this causes stress, which may result in springing. If this feedback springing is too big, its symptom is poor adhesion of chips. This can lead to the formation of thin zones. These loose zones indicate using of the wrong glue and may result in the rapid opening of the press caused by lower tensile strength perpendicular to board plane. The lower coherence of the pressed board is then reflected in a faster opening of the press.

Table 15 Statistical evaluation for variant 2.1, OSB/3 ECO, 18 mm nominal thickness

Tablica 15. Statistička procjena rezultata za varijantu 2.1, OSB/3 ECO nominalne debljine 18 mm

Variant 2.1 / Varijanta 2.1. High-speed press opening <i>Vrlo brzo otvaranje preše</i>	Density <i>Gustoća</i> kg/m ³	σ_{\perp} N/mm ²	MOR N/mm ²	MOE N/mm ²	MOR \perp N/mm ²	MOE \perp N/mm ²
<i>OSB No.1</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 1.</i>	579	0.35	18.92	4 535	12.52	2 159
Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	257.277	0.003	7.194	292 168.325	5.543	67 091.186
<i>OSB No.2</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 2.</i>	579	0.36	22.55	4 749	13.18	2 238
Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	253.923	0.003	21.075	916 820.112	4.474	66 075,029
<i>OSB No.3</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 3.</i>	581	0.35	21.90	5 042	15.55	2 365
Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	163.981	0.004	32.861	609 745.742	1.765	9 763.937
Total average value $\bar{\bar{x}}$ / <i>Ukupna srednja vrijednost</i>	580	0.35	21.12	4 775	13.75	2 254
Variance of average values within the board s OSB 1–3 $s_{\bar{x}}^2$ / <i>Varijanca srednje vrijednosti za ploče OSB 1–3.</i>	1.237	0.00001	3.836	64 750.495	2.529	10 819.885
Average value of variance values within the boards OSB 1–3 \bar{s}_w^2 / <i>Srednja vrijednost varijanci za ploče OSB 1–3.</i>	225.06	0.003	20.377	606 244.726	3.928	47 643.384

Table 16 Statistical evaluation for variant 2.2, OSB/3 ECO 18 mm nominal thickness

Tablica 16. Statistička procjena rezultata za varijantu 2.2, OSB/3 ECO, nominalne debljine 18 mm

Variant 2.2 / Varijanta 1.2. Gradual press opening <i>Postupno otvaranje preše</i>	Density <i>Gustoća</i> kg/m ³	σ_{\perp} N/mm ²	MOR N/mm ²	MOE N/mm ²	MOR \perp N/mm ²	MOE \perp N/mm ²
<i>OSB No.1</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 1.</i> Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	577	0.35	23.38	4 555	15.94	2 686
<i>OSB No.2</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 2.</i> Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	588	0.32	22.31	4 937	14.39	2 240
<i>OSB No.3</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 3.</i> Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	574	0.38	22.62	4 769	13.77	2 208
Total average value $\bar{\bar{x}}$ / <i>Ukupna srednja vrijednost</i>	580	0.35	22.77	4 754	14.70	2 378
Variance of average values within the board s OSB 1–3 s_x^2 / <i>Varijanca srednje vrijednosti za ploče OSB 1–3.</i>	48.728	0.0009	0.219	36 648.388	1.252	71 144.966
Average value of variance values within the boards OSB 1–3 \bar{s}_w^2 <i>Srednja vrijednost varijanci za ploče OSB 1–3.</i>	261.688	0.004	30.297	780 193.953	5.100	374 257.503

4 CONCLUSION

4. ZAKLJUČCI

The aim of this paper was to optimize a pressing diagram on the basis of measuring changes of pressure and temperature in the board in the course of pressing. Changes of the pressing diagram were carried out at the stage of “press opening” because these changes substantially affected physical and mechanical properties of OSB boards. For each change of “press opening” three boards were sampled and used to cut test samples. With these specimens, the following parameters were determined: density, tensile strength perpendicular to the board plane, bending strength and the modulus of elasticity in bending in the main and secondary axes of production.

dulus of elasticity in bending in the main and secondary axes of production.

In variant 1.1 (very fast “press opening”), the unsatisfactory mean value of tensile strength perpendicular to the board plane was detected, exactly 0.31 N/mm². In this variant, increased formation of vapour “blisters” and cracking of the boards occurred due to very fast cooling and outflow of water vapours after shortening the process to the required time, namely about 5% of OSB production. So, this variant is unusable in production since it is impossible to achieve the required values of tensile strength perpendicular to the board plane as well as due to the large number of wasters. According to the measured laboratory results, the

Table 17 Statistical evaluation for variant 2.3, OSB/3 ECO, 18 mm nominal thickness

Tablica 17. Statistička procjena rezultata za varijantu 2.3, OSB/3 ECO nominalne debljine 18 mm

Variant 2.3 / Varijanta 1.3. High gradual press opening <i>Vrlo postupno otvaranje preše</i>	Density <i>Gustoća</i> kg/m ³	σ_{\perp} N/mm ²	MOR N/mm ²	MOE N/mm ²	MOR \perp N/mm ²	MOE \perp N/mm ²
<i>OSB No.1</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 1.</i> Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	576	0.36	21.04	5 020	14.26	2 304
<i>OSB No.2</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 2.</i> Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	581	0.38	23.45	4 535	13.02	2 138
<i>OSB No.3</i> Average value within the board \bar{x}_j <i>Srednja vrijednost za ploču 3.</i> Variance within the board s_{wj}^2 / <i>Varijanca unutar ploče</i>	574	0.33	23.34	5 100	13.26	2 134
Total average value $\bar{\bar{x}}$ / <i>Ukupna srednja vrijednost</i>	577	0.36	22.61	4 885	13.51	2 192
Variance of average values within the board s OSB 1–3 s_x^2 / <i>Varijanca srednje vrijednosti za ploče OSB 1–3.</i>	11.971	0.0004	1.942	93 612.425	0.431	9 387.606
Average value of variance values within the boards OSB 1–3 \bar{s}_w^2 / <i>Srednja vrijednost varijanci za ploče OSB 1–3.</i>	215.897	0.005	17.622	813 305.725	1.325	22 871.406

variant OSB/3 ECO, 2.2 gradual “press opening”, was evaluated as optimal.

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5 REFERENCES

5. LITERATURA

1. Bolton, A.; Humphrey, P.; Kavvmouras, P., 1989: The hot pressing of the dry formed wood-based composites. Part IV. Predicted variation of mattress moisture content with time. *Holzforschung* 43 (5): 345-349. doi:10.1515/hfsg.1989.43.5.345
2. Deppe, H. J.; Ernst, K., 1991: Taschenbuch der Spanplattentechnik. 3. überarbeitete und erweiterte Auflage. DRW Verlag Leinfelden. 468 p.
3. Hrázský, J.; Král, P., 2007: Wood-based composites. Part I.: Chips and fibrematerials. MZLU Brno. 253 p.
4. Kühne, G.; Belimow, F., 1978: Ein Beitrag zur Analyse des Heisspressvorgangs dreischichtiger Möbelplatten II. *Holzindustrie* (2): 50-52.
5. Štefka, V., 2007: Wood-based composites. Part II: Agglomerated materials technology. TU Zvolen. 204 p.

6. Štefka, V., 1999: Particleboard pressing process and transfer phenoma. TU Zvolen. 61 p.
7. ***CSN EN 300. OSB-panels of oriented flat chips. Definition, classification and requirements. Czech standard institution, 1998:20.
8. ***CSN EN 310. Wood-based panels. Bending strength and modulus of elasticity determination. Czech standard institution, 1995:8.
9. ***CSN EN 319. Chips- and fibreboards. Tensile strength perpendicular to the board surface determination. Czech standard institution, 1994:12.
10. ***CSN EN 323. Wood-based panels. Density determination. Czech standard institution, 1994:8.

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