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# Degradation of dye-containing textile effluents by enzymatic catalysis

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## Abstract

The use of biotechnological processes in textile dye effluents treatment has attracted considerable attention and achieved interesting results in recent years. These effluents are moderately toxic but conventional treatments are not able to accomplish new environmental regulations. Legislation about toxic and hazardous substances in industrial wastewaters is becoming increasingly strict; consequently a large number of researchers are addressing a variety of issues in this area. New technologies must be developed and adapted to achieve such low limits of effluent discharge toxicity. Enzymes of the oxidase type, particularly laccases are now used as an alternative to the conventional effluent treatments.

In this work the degradation potential of enzyme laccase against several reactive textile dyes, that are difficult to decolourize and often found in real textile wastewaters, was assessed. For this purpose, a pure laccase (DeniLite II Base) and a commercial formulation (DeniLite II S) containing the laccase, a mediator and a non-ionic surfactant were employed.

The dye degradation of six reactive dyes typically used in textile industry (reactive black 5, reactive blue 114, reactive yellow 15, reactive yellow 176, reactive red 239 and reactive red 180) was optimized using pure laccase. In this context five traditional laccase mediators, temperature, pH and mediator concentrations were tested to evaluate the decolourization by laccase mediator system.

The efficiency of the commercial laccase formulation in dyes degradation was also evaluated and optimized by the application of a three-level Box-Behnken factorial design with three factors (pH, temperature and enzyme concentration) combined with response surface methodology. Mathematical models were developed for each dye, showing the effect of each factor and their interactions on colour removal.

The results have shown that the efficiency of the laccase mediator system depends on the type of the dye. To better understand the mechanisms of reactive dyes oxidation with laccase and the correlation between the redox potential and dye degradation, cyclic voltammetry was carried out. A linear correlation between the percentage of decolourization and the respective anodic peak potential was verified. Sequential decolourization of dyes by laccase mediator system was also studied, showing that this method may be applied for the effective treatment of effluents from textile dyeing industries, since seven repetitive decolourization cycles were successfully performed.

The treatability of a mixture of three reactive textile dyes (reactive black 5, reactive yellow 15 and reactive red 239) and of a simulated real effluent with the three reactive dyes, salts and auxiliary chemicals by commercial laccase was evaluated. The decolourizations were efficient, demonstrating also the capability of producing an effluent with parameter values below the legal discharge limits if carried out with immobilized laccase.

Concerning the kinetics in batch reactor, several models based on Michaelis-Menten equation were developed to simulate the laccase (commercial formulation) catalyzed degradation of a single reactive dye or a mixture of dyes in aqueous solution and of a simulated textile effluent. The close correlation between the experimental data and the simulated values indicates that the proposed models are able to describe with remarkable accuracy the kinetic behaviour of the reactions and that they could be used for design and simulation applications.

The treatability of the reactive dyes by immobilized commercial laccase into coconut fiber (adsorption mechanism) was also studied. The effect of the immobilization conditions on the properties of laccase and the characterization of the immobilized enzyme were achieved, showing its suitability for continuous colour removal from textile industrial effluents.

Finally, a new possibility for the degradation of dyes in supercritical carbon dioxide media catalyzed by commercial laccase as a greener and clean technology was investigated and optimized by response surface methodology. However, and despite the advantages of using supercritical carbon dioxide, the results show that this is not the best technique for this process.

In summary, it was shown that the laccase mediator system was an efficient method for the decolourization of the more difficult to degrade dyes (reactive type dyes). Compared to the common and sometimes expensive physical and/or chemical ways for industrial textile effluent remediation, the biodegradation by the use of commercial laccase appears to be an attractive alternative for larger scale applications.

**Keywords:** Reactive textile dyes, laccase, mediators, decolourization, biocatalysis, optimization, kinetic modelling, textile effluent, enzyme immobilization.

## Resumo

Nos últimos anos, o uso de processos biotecnológicos tem atraído considerável atenção e tem conseguido resultados interessantes no tratamento de corantes de efluentes têxteis. Estes efluentes são moderadamente tóxicos e os tratamentos convencionais não são capazes de acompanhar as novas normas ambientais. A legislação relativa à presença de substâncias tóxicas e perigosas em águas residuais industriais tem-se tornado cada vez mais rigorosa e, conseqüentemente, um grande número de investigadores tem-se interessado mais sobre os vários problemas desta temática. Para atingir esses limites de toxicidades de descarga dos efluentes é necessário desenvolver ou adaptar novas tecnologias. As enzimas do tipo oxidase, particularmente as lacases, têm sido usadas como uma alternativa aos tratamentos convencionais dos efluentes.

Neste trabalho foi avaliado o potencial de degradação da enzima lacase em relação a vários corantes têxteis reactivos, difíceis de degradar e frequentemente presentes em efluentes têxteis reais. Para tal, usou-se a enzima lacase pura (*DeniLite II Base*) e uma formulação comercial contendo a lacase, um mediador e um tensoactivo não-iónico (*DeniLite II S*).

Numa primeira etapa, efectuou-se a optimização da degradação de seis corantes reactivos normalmente usados na indústria têxtil (*reactive black 5*, *reactive blue 114*, *reactive yellow 15*, *reactive yellow 176*, *reactive red 239* e *reactive red 180*) com a lacase pura. Para este efeito foram testados cinco mediadores tradicionais da lacase, a temperatura, o pH e a concentração do mediador, de forma a avaliar a descoloração pelo sistema lacase mediador.

Foi também avaliada e optimizada a eficiência da formulação comercial da lacase na degradação destes corantes mas agora com a aplicação de um modelo factorial *Box-Behnken* com três níveis e três factores (pH, temperatura e concentração de enzima), combinado com a metodologia de superfície de resposta. Foram desenvolvidos modelos matemáticos para cada um dos corantes, de forma a mostrar o efeito de cada factor e das suas interacções na remoção de cor.

Os resultados demonstraram que a eficiência do sistema lacase mediador depende do tipo de corante. Assim, utilizou-se a voltametria cíclica para melhor elucidar os mecanismos de oxidação dos corantes reactivos pela enzima lacase e a correlação existente entre o potencial redox e a degradação dos corantes. Foi verificada uma correlação linear entre a percentagem de descoloração dos corantes e o respectivo potencial do pico anódico. Investigou-se também a descoloração sequencial dos corantes pelo sistema lacase mediador, tendo-se verificado que este método pode ser aplicado para o tratamento eficaz dos efluentes das indústrias têxteis, uma vez que foram realizados com sucesso sete ciclos repetitivos de descoloração.

A degradação de uma mistura de três corantes têxteis reactivos (*reactive black 5*, *reactive yellow 15* e *reactive red 239*) pela formulação comercial da laccase e de um efluente real simulado com os mesmos três corantes reactivos, sais e substâncias auxiliares químicas

foi também avaliada. As degradações foram bastante eficientes, demonstrando também a capacidade de se produzir um efluente com parâmetros abaixo dos valores limite legais de descarga, caso se efectue o tratamento com a lacase imobilizada.

Quanto à cinética de reacções em reactor fechado, foram desenvolvidos vários modelos baseados na equação de *Michaelis-Menten* para simular a degradação dos corantes reactivos em estudo pela enzima lacase (formulação comercial) quando separados, numa mistura e num efluente têxtil simulado. A concordância verificada entre os dados experimentais e os valores simulados indica que os modelos propostos são capazes de descrever com elevado rigor o comportamento cinético das reacções e que poderiam ser utilizados em trabalhos de projecto e de simulação.

Foi também avaliado o tratamento dos corantes reactivos pela lacase comercial imobilizada por adsorção em fibra de coco. Estudou-se o efeito das condições de imobilização sobre as propriedades da lacase e realizou-se a caracterização da enzima imobilizada, demonstrando a sua aptidão para a remoção contínua da cor de efluentes industriais têxteis.

Finalmente, foi investigada e otimizada, através da metodologia de superfície de resposta, uma nova possibilidade para a degradação de corantes catalisada pela lacase comercial em dióxido de carbono supercrítico, como uma tecnologia limpa e ecológica. No entanto, apesar do uso de dióxido de carbono supercrítico apresentar muitas vantagens, os resultados indicam que esta não é a melhor técnica a usar para este processo.

Resumindo, todo este trabalho mostrou que o sistema lacase mediador é um método eficiente para a descoloração dos corantes mais difíceis de degradar (corantes do tipo reactivo). Em comparação com os métodos tradicionais e por vezes caros, físicos e químicos para a remediação de efluentes têxteis industriais, a biodegradação com o uso da enzima lacase comercial mostrou ser uma alternativa atraente para aplicações em maior escala.

**Palavras-Chave:** Corantes têxteis reactivos, lacase, mediadores, descoloração, biocatálise, optimização, modelação cinética, efluentes têxteis, imobilização de enzimas.



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## **Part I**

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### Thesis Outline



## I – Thesis Outline

Textile industries release during the process large quantities of intensely coloured and hazardous effluents, which cause serious environmental pollution. Rivers must preserve their natural colour and the clarity of water. Even minor releases of coloured effluents (1 mg/L) may cause irregular colouration of surface waters as well as the pollution of the water with toxic compounds. Dyes change the absorption and reflection of sunlight on the water giving rise to problems to photosynthetic aquatic plants and algae. Due to their large-scale production and extensive application, synthetic dyes can cause considerable nonaesthetic pollution and are serious health-risk factors. Furthermore, the effluents from textile industries contain a variety of other compounds, such as dispersing agents, salts, emulsifiers and organometallic compounds containing heavy metals.

Although the growing impact of environmental protection on industrial development promotes eco-friendly technologies, reduced consumption of water and lower output of wastewater, the discharge of effluents with synthetic dyes is very problematic. It is therefore important to study how to meet the effluent discharge limits in legislation. The impact and toxicity of dyes in the environment have been extensively studied. However, due to the large variety of dyes used in industry, not all their properties are known, namely its mutagenicity and carcinogenicity.

Due to their stability under sunlight and resistance to microbial attack, the majority of dyes are not degraded by conventional treatments. The research of powerful and practical treatments to decolourize and degrade dyeing wastewaters to decrease their environmental impact has attracted an increasing interest. Traditional physico-chemical treatments applied to the purification of dyeing wastewaters include adsorption with inorganic and organic supports, coagulation, filtration, ion exchange, among others. These procedures lead to effective decolourization, but their application is restricted due to some problems such as the formation of sludge to be disposed or the need to regularly regenerate the adsorbent materials. More powerful chemical methods such as ozonation and oxidation with hypochlorite ion, as well as advanced oxidation processes such as Fenton's reagent and photocatalytic systems involving  $\text{TiO}_2/\text{UV}$ ,  $\text{H}_2\text{O}_2/\text{UV}$  and  $\text{O}_3$ , also provide fast decolourization, along with degradation of dyes. However, these methods are quite expensive and have operational problems. The application of microorganisms to the biodegradation of synthetic dyes has been an attractive alternative. A series of aerobic and anaerobic biological methods, including activated sludge, mixed cultures, fungi, bacteria or algae have been studied for the dyes degradation. However, due to chemical stability and resistance to microbial attack of several dyes, many of these methods are not effective.

The decomposition of dyes by enzymes from various microorganisms has been also studied. The textile wastewater treatment with enzymes from fungi can be simpler and more efficient than the traditional treatments. The enzymes are highly selective and can effectively

treat the wastes. They are less likely to be inhibited by substances which may be toxic to living organisms and can operate at mild conditions of temperature, pressure and pH.

Enzymes of the oxidase type, particularly ligninolytic enzymes (laccase, lignin peroxidase and manganese peroxidase), have been used as an attractive technology for the development of new methodologies of dye degradation from textile industries. Laccase (EC 1.10.3.2, p-benzenediol:oxygen oxidoreductase) is able to catalyze the oxidation of various aromatic compounds (particularly phenols) with the concomitant reduction of oxygen to water. According to the literature, it has been the preferred lignin-degrading enzyme for dye decolourization most likely because the enzyme requires only oxygen as a co-substrate. The relatively high optimal temperatures of the enzyme makes it ideal for industrial applications and it should be more easily implemented into industrial processes. Thus, in this study, the enzyme laccase was chosen for the decolourization of dyes. Specific compounds usually denominated by mediators are under study to extend the number of dyes decolourized. In general, in order to increase the potential use of enzymes, their immobilization is necessary for biochemical stability and reuse. By using these immobilized forms, adequate characteristics including high resistance to thermal denaturation, significant improvement of the enzymatic activity and its preservation for long periods are obtained. An understanding of the mechanisms and kinetics of enzyme systems is also essential for the design of efficient reactor systems to carry out industrial processes.

Several review papers in the area of colour removal of textile effluents are available. However, specifically in the case of reactive dyes little research has been conducted, particularly in the field of mathematical modelling. Studying dye degradation kinetics by laccase can give more insight on how it is affected by the composition of dye effluents and help to predict the kinetic behaviour of the enzyme in industrial dye decolourization. The use of this treatment method in real effluents has also not been fully explored. Studies published continuously only evaluate the behaviour of synthetic wastewater under conditions different from those observed in real effluents. Therefore, the exploit of this potential is also an important goal of this research. Finally, in order to use this process on a continuous mode, in view of its scale-up and considering the costs involved, it is important to think about the use of the enzyme in the immobilized form.

Thus, this thesis aims to develop and optimize an enzymatic process to degrade reactive dyes from textile effluents with free and immobilized laccase to implement in textile industries. For this purpose, a systematic experimental and modelling working plan was carried out.

1. The decolourization efficiency of six different synthetic reactive dye effluents in batch reactions with laccase was evaluated;
2. The parameters that potentially affect the enzymatic batch reaction such as enzyme concentration, temperature, pH and the addition of mediators were optimized; for this

- pure laccase (DeniLite II Base) and in a commercial formulation (DeniLite II S) containing the laccase, a mediator and a non-ionic surfactant were employed;
3. A kinetic model of enzyme-catalyzed dye transformation to assist in understanding of the enzymatic process was developed;
  4. The sequential decolourization of reactive dyes by laccase mediator system was studied;
  5. Cyclic voltammetry was used in order to obtain a correlation between the redox potential and dye degradation;
  6. The degradation in the optimal conditions of a simulated wastewater containing a mixture of three dyes was evaluated. The kinetic modelling of this enzymatic reaction in a batch reactor was also carried out;
  7. The degradation of a synthetic dye house effluent, containing three reactive dyes, salts and auxiliary chemicals, simulating a textile wastewater by commercial laccase was examined in a batch reactor. Kinetic models to simulate the decolourization were developed;
  8. The water quality properties of the textile effluent, such as total organic carbon, chemical oxygen demand, biochemical oxygen demand and toxicity were examined;
  9. The reactive textile dyes degradation by immobilized laccase was optimized and the immobilized enzyme reuse was evaluated;
  10. The laccase catalyzed degradation of the reactive textile dyes in supercritical carbon dioxide media was also considered and optimized.

The thesis is organised in seven parts. The first part of the thesis (part II) presents the state of the art on textile industrial effluents, dyes, on current technologies for dye removal (physical, chemical and biological methods), on the application of enzymes in wastewater treatment and finally a more detailed review on laccase enzymes, their molecular and structural properties, their use with mediators, their applications and immobilization.

Part III focuses the optimization of the reactive dyes degradation by enzyme laccase in batch reactors. For that the factorial design methodology and the response surface methodology are applied to some of the systems to evaluate the effect of pH, temperature and enzyme concentration on the extent of the decolourization reaction equilibrium. The best work conditions for laccase catalysis are established and the voltammetric measurements of the dyes are used to predict the dye decolourization ability of commercial laccase.

Part IV investigates the kinetic features of the reactions. The kinetic modelling and simulation of the decolourization of the reactive textile dyes, of a mixture of them and of a simulated dye house effluent by commercial laccase are performed. The mathematical modelling work is complemented with experimental work for the different project stages. The environmental parameters of the simulated real effluent before and after enzyme treatment are also evaluated.

In part V the immobilization of laccase by adsorption into coconut fiber and its application to dye decolourization are investigated. Parameters such as the immobilization efficiency, activity retention, operational and thermal stability are studied. The results suggest that the immobilization technique is important for the control of the catalysis and for the economy of the process.

In part VI, a new possibility for the degradation of dyes in supercritical carbon dioxide media catalyzed by commercial laccase is investigated and optimized by response surface methodology. A comparison with the results in aqueous media is made.

Finally in part VII, the findings of the previous parts are organized in the general conclusions and suggestions for future work are given.



## **Part II**

---

### General Introduction



## II. 1 Textile industry

The Textile and Clothing Manufacturing is one of the industries with the largest representation in the Portuguese industrial structure and has always taken a prominent role in terms of employment and weight in the national economy (Vasconcelos, 2006). The Textile Industry (from preparation to finishing up the fiber) and the Clothing Industry (production) account for 11 % of total Portuguese exports, 22 % of employment in manufacturing, 8 % of its business volume and 7 % of its production (Associação Têxtil e Vestuário de Portugal (ATP, 2010)). Table II. 1 shows some of the values associated with the Portuguese textile industry over the years.

**Table II. 1** – Economic aspects of Portuguese textile industry (ATP, 2010).

	2003	2004	2005	2006	2007	2008	2009
Production (million €)	7840	7890	6756	6749	6733	6164*	5704
Business volume (million €)	8103	8145	6993	6931	6980	6349*	5357
Exports (million €)	4572	4319	4118	4113	4295	3985	3448
Imports (million €)	3048	2971	2993	3086	3329	3212	2889
Employment	222602	209768	201265	186837	180335	167712*	163415

\* ATP estimates

Portugal has about 7 thousand companies labouring in all sub-sectors of textile and clothing industries, some of which are vertical units, although they are mostly small and medium sized companies, well known for their flexibility and quick response, know-how and innovation. They are located mainly in Northern Portugal (Porto, Braga, Guimarães and Famalicão) but some, dedicated to wool products, can be found in Covilhã (Eastern Portugal) (ATP, 2010). This concentration is mainly due to historical reasons: preference for locations where the discharge of effluents was easier, existence of skilled workers and also abundant low hardness water. While the textile industry was growing it retained its attachment to the traditional sites.

## II. 2 Textile industry effluents

### II. 2.1 General characteristics

The textile industry includes a wide range of activities, from preparation of raw material to pre-treatment, dyeing and finishing of textile material. All these activities consume water and energy and are highly polluting. Textile industry processes are known to be intensive users of water. In Figure II. 1 a process diagram of a textile industry is shown, highlighting the steps where the water consumption and the generation of aqueous effluents occur (Braille and Cavalcanti, 1993).

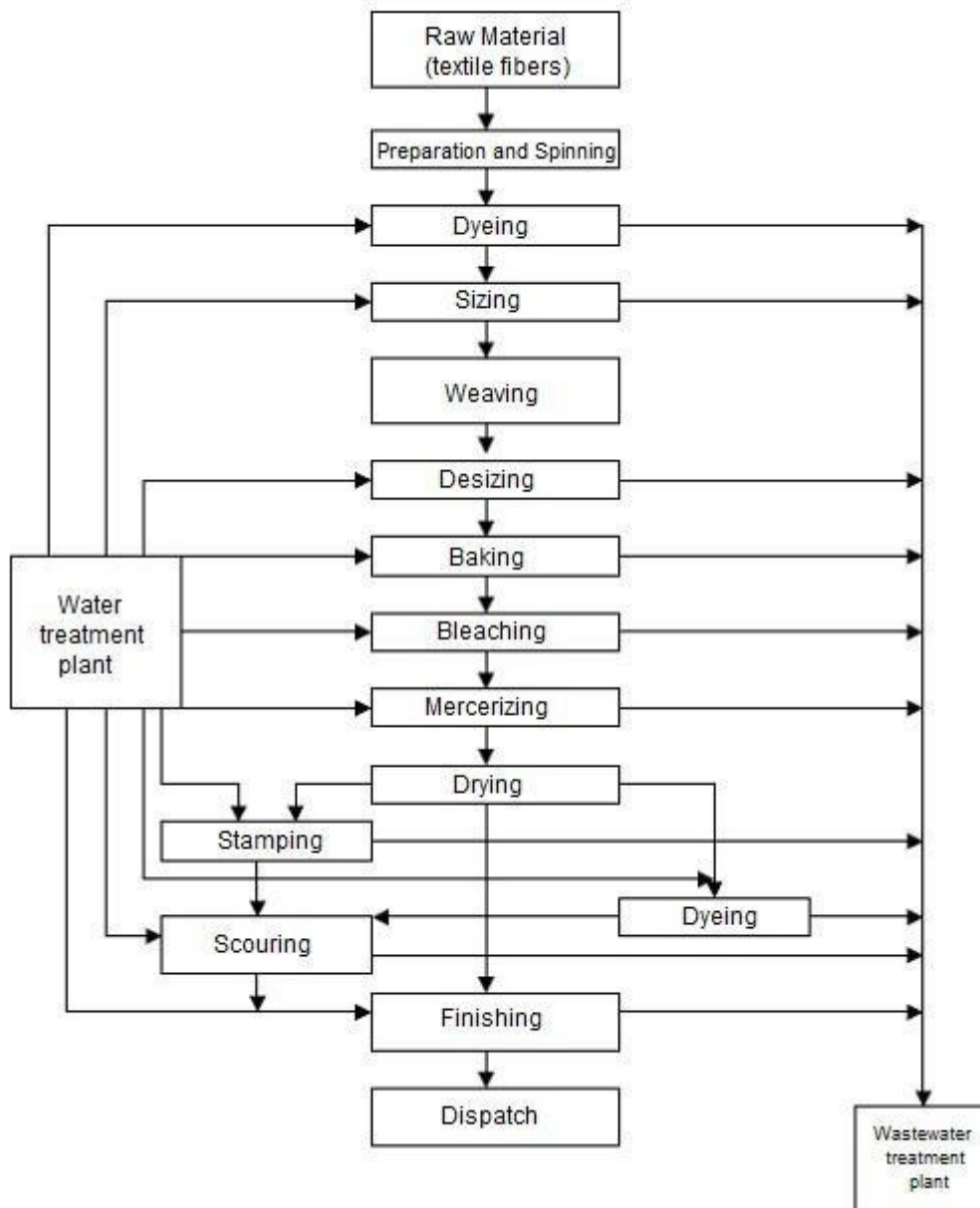


Figure II. 1 – Stages of a textile industry.

Due to the wide variety of fibers, dyes, process auxiliaries and final products, these processes generate waters of great diversity and chemical complexity. This complex composition is reflected in the colour, in a high ratio between chemical oxygen demand and biochemical oxygen demand (COD/BOD<sub>5</sub>), in the presence of suspended matter and, possibly, heavy metals, and in variable pH values, mostly in the alkaline range (Gonçalves et al., 1996). However, since the fashions are always varying, the textile effluents composition is never constant. Environmental problems related to the textile industry are numerous and well documented. Despite the high volume of waste and its high organic load, the main problem of textile industry effluents is related to the colour generated by unfixed dyes during textile processing and directly released to the effluent.

The major pollutant types identified in textile wastewater are summarised in Table II. 2 along with their main origin in the textile manufacturing processes.

**Table II. 2** – Major pollutant types in textile wastewater, chemical types and process of origin (Delée et al., 1998).

<b>Pollutants</b>	<b>Major chemical types</b>	<b>Main processes of origin</b>
Organic load	Starches, enzymes, fats, greases, waxes, surfactants, acetic acid	Desizing, Scouring, Washing, Dyeing
Colour	Dyes, scoured wool impurities	Dyeing, Scouring
Nutrients (N,P)	Ammonium salts, urea, phosphate-based buffers and sequestrants	Dyeing
Acids Alcalis and salts	NaOH, mineral/organic acids, sodium chloride, silicate, sulphate, carbonate	Scouring, Desizing, Bleaching, Mercerizing, Dyeing, Neutralization
Sulphur	Sulphate, sulphite and hydrosulphite salts, sulphuric acid	Dyeing
Toxic compounds	Heavy metals, reducing agents (sulphide), oxidising agents (chlorite, peroxide, dichromate, persulphate), biocides, quaternary ammonium salts	Desizing, Bleaching, Dyeing, Finishing
Refractory organics	Surfactants, dyes, resins, synthetic sizes (PVA), chlorinated organic compounds, carrier organic solvents	Scouring, Desizing, Bleaching, Dyeing, Washing, Finishing

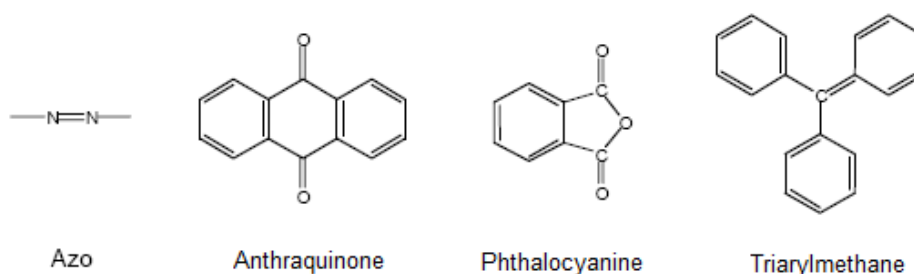
## II. 2.2 Dyes

Ever since the beginning of times, people have demonstrated the need to add colour to all that surrounds them. They use dyes from natural origins, such as soot, manganese oxide, hematite and ochre for painting their stories in caves, their skins and their clothes. The textile natural dyes were mainly obtained from plants, insects, fungi and lichens (Ingamells, 1993).

Mauveine, the first synthetic dye, was discovered in 1856 by William Henry Perkin. Since then, thousands of new synthetic dyes have been produced. Nowadays, the total annual world textile dye production is estimated at about  $7 \times 10^5$  tons, with more than 100,000 dyes available on the market (Santhi et al., 2010). The largest consumer of these dyes is the textile industry accounting for around two thirds of its market (Anjaneyulu et al., 2005).

To be coloured compounds, dyes have to absorb radiation in the visible range, i.e., 380 to 780 nm. This property is due to the possession of two different groups, the chromophore, which is typically an electron withdrawing group and is responsible for the colour of the compound, and the auxochrome, which is an electron donating substituent that can intensify the colour of the chromophore and provides solubility and adherence of the dye to the fiber (Christie, 2001).

Dyes can be divided in 20-30 different groups regarding their chromophores. The most important are azo (monoazo, diazo, triazo, polyazo), anthraquinone, phthalocyanine and triarylmethane dyes (Figure II. 2). Azo dyes represent about 70 % on weight basis of total annual world production (dos Santos et al., 2003). These dyes are followed, in terms of prevalence, by the anthraquinone dyes (dos Santos et al., 2005).



**Figure II. 2** – The most important chromophores.

Dyes can be classified according to their colour, structure or method of application in the Colour Index (C.I.). This system was developed by the “Society of Dyers and Colourists” and the “American Association of Textile Chemists and Colourists” in 1925 and consists in assigning a generic name for each dye, according to its colour and method of application, followed by a number that specifies the chronological order or its commercial introduction (CII, 2010). Table II. 3 shows the 15 Colour Index different application classes.

**Table II. 3** – Colour Index application classes (adapted from Christie (2001)).

Application class	Characteristics	Substrates	Common structures
Acid dyes	Highly water soluble; form ionic interactions between the $\text{-NH}_3^+$ groups of fibers and the negative charge of the dyes	Wool, polyamide, silk, nylon, leather	Azo, anthraquinone, triarylmethane
Reactive dyes	Form covalent bonds with $\text{-OH}$ , $\text{-NH}$ or $\text{-SH}$ groups	Cotton, wool, silk, nylon	Azo, metal complex azo, anthraquinone, phthalocyanine
Direct dyes	Their flat shape and length enables them to maximize van-der-Waals, dipole and hydrogen bonds	Cellulose fibers, cotton, viscose, paper, leather, nylon	Sulphonated azo dyes

Basic dyes	Strong ionic interaction between dye cationic groups and the negative charges in the copolymer	Synthetic fibers, paper, inks	Azo, diarylmethane, triarylmethane, anthraquinone
Mordant dyes	Metal salts that act as “fixing agent” to improve the colour fastness	Wool, leather, silk, modified cellulose fibers	Azo, oxazine, triarylmethane
Disperse dyes	Non-ionic structure, with polar functionality, that improves water solubility, van-der-Waals and dipole forces and the colour.	Polyester, polyamide, acetate, acrylic, plastics	Azo, nitro, anthraquinone, metal complex azo
Pigment dyes	Insoluble, non-ionic compounds or salts that retain their crystalline or particulate structure throughout their application	Paints, inks, plastics, textiles	Azo, metal complex phthalocyanine
Vat dyes	Insoluble coloured dyes which on reduction give soluble colourless forms /leuco form with affinity for the fiber; can be oxidized back, with H <sub>2</sub> O <sub>2</sub> , to insoluble form	Cellulose fibers, cotton, viscose, wool	Anthraquinone, indigoid
Ingrain dyes	Insoluble products of a reaction between a coupling component and a diazotized aromatic amine that occurs in the fiber	Cotton, viscose, cellulose acetate, polyester	Tetra-azaporphin
Sulphur dyes	Dyeing with sulphur dyes involves reduction and oxidation processes	Cellulose fibers, cotton, viscose	Complex polymeric aromatics
Solvent dyes	Non ionic dyes that dissolve the substrate to which they bind	Plastics, varnish, ink, waxes, fats	Diazo, triarylmethane, anthraquinone, phthalocyanine
Other dye classes	Food dyes: not used as textile dyes, non-toxic; Natural dyes: use in textile processing operations is very limited; Fluorescent brighteners: mask the yellowish tint of natural fibers; Metal complex dyes: strong complexes of one metal ion	Food, cotton, wool, silk, polyester, polyamide, soaps and detergents, paints, plastics	Azo

Colour is the first contaminant to be recognized in wastewater. The presence of very small amounts of dyes in water (less than 1 ppm for some dyes) is highly visible and affects not only the aesthetic aspect and water transparency, but also the absorption and reflection of sunlight, interfering with aquatic life in lakes, rivers and other waterbodies. In addition to their visual effect and their adverse impact in terms of chemical oxygen demand, many synthetic dyes are toxic, mutagenic and carcinogenic (Golka et al., 2004; Pointing, 2001).

All dyes used in the textile industry are synthesized to be chemically and photolytically stable, i. e., to resist to the light, water, various chemicals, including oxidizing agents, and microbial attack. Given that, during processing, a certain percentage of dyes used are taken with water from the process and since they are difficult to bleach because of complex structure, synthetic origin, and recalcitrant nature, their removal from industrial effluents before being discharged into water systems is compulsory (Suteu et al., 2005).

The dye fixation on the fibers during the dyeing process is not total, leading to the dye release. The degree of fixation depends on dye/fiber combinations and on the special characteristics of the dyeing process. Consequently, according to Easton (1995) the fixation rates of various dyes and their losses to the effluent can only be given as examples (Table II. 4).

**Table II. 4** – Estimated degree of fixation for different dye/fiber combinations.

<b>Dye class</b>	<b>Fiber</b>	<b>Degree of fixation (%)</b>	<b>Loss to effluent (%)</b>
Acid	Polyamide	80-95	5-20
Basic	Acrylic	95-100	0-5
Direct	Cellulose	70-95	5-30
Disperse	Polyester	90-100	0-10
Metal-complex	Wool	90-98	2-10
<b>Reactive</b>	<b>Cellulose</b>	<b>50-90</b>	<b>10-50</b>
Sulphur	Cellulose	60-90	10-40
Vat	Cellulose	80-95	5-20

The treatment of textile effluents is particularly important in the case of intensely coloured wastewaters containing reactive dyes, since these dyes are those with a lower degree of fixation to the fiber, they are less receptive to conventional treatments of effluents, such as adsorption and aerobic biodegradation and, finally, belong to the most used class, as they are used for dyeing cotton which is also the substrate that requires more water in its processing (O'Neill et al., 1999). In this process, the dyeing occurs at alkaline pH (10-11) and high temperatures (50-70 °C), and the effluents are highly coloured, concentrated in salts and with a high COD/BOD<sub>5</sub> ratio (Allegre et al., 2006).

Concern about the environment has been led to an increasingly stringent legislation relating to the discharge of textile effluents and, therefore, to the search of more effective treatment methods for the removal of dyes from wastewaters in order to meet the established limits.

## **II. 2.3 Standards and legislation**

In the case of the Portuguese legislation, Law Decree No. 236/98 of August 1<sup>st</sup> defines the emission limit values (ELVs) in the discharge of wastewater. In the specific case of industrial textile units, excluding the sub-sector of wool, and regarding pH, BOD<sub>5</sub>, COD and colour, the constant values of Ordinance No. 423/97 of June 25<sup>th</sup> are applied. Those emission standards can be found in Table II. 5.



**Table II. 5** - Disposal of waste water standards for the textile sector, excluding the wool subsector (LD 236/98 and Ordinance 423/97).

Parameters	Units	ELV <sup>a</sup> / MPV <sup>b</sup>
pH*	Sorensen scale	5.5 – 9.0
Temperature	°C	Increase of 3°C <sup>c</sup>
BOD <sub>5</sub> , 20°C*	mg/L O <sub>2</sub>	100
COD*	mg/L O <sub>2</sub>	250
TSS	mg/L O <sub>2</sub>	60
Aluminium	mg/L Al	10
Total iron	mg/L Fe	2.0
Total manganese	mg/L Mn	2.0
Smell		Not detectable at 1:20 dilution
Colour*		Not visible at 1:40 dilution
Free available residual chlorine	mg/L Cl <sub>2</sub>	0.5
Total available residual chlorine	mg/L Cl <sub>2</sub>	1.0
Phenols	mg/L C <sub>6</sub> H <sub>5</sub> OH	0.5
Oils and fats	mg/L	15
Sulphides	mg/L S	1.0
Sulphites	mg/L SO <sub>3</sub>	1.0
Sulphates	mg/L SO <sub>4</sub>	2000
Total phosphorus	mg/L P	10: 3 <sup>f</sup> ; 0.5 <sup>g</sup>
Ammoniacal nitrogen	mg/L NH <sub>4</sub>	10
Total nitrogen	mg/L N	15
Nitrates	mg/L NO <sub>3</sub>	50
Aldehydes	mg/L	1.0
Total arsenic	mg/L As	1.0
Total lead	mg/L Pb	1.0
Total cadmium	mg/L Cd	0.2
Total chromium	mg/L Cr	2.0
Hexavalent chromium	mg/L Cr(VI)	0.1
Total copper	mg/L Cu	1.0
Total nickel	mg/L Ni	2.0
Total mercury	mg/L Hg	0.05
Total cyanide	mg/L CN	0.5
Mineral oils	mg/L	15
Detergents	mg/L LAS <sup>h</sup>	2.0 <sup>d e</sup>

(<sup>a</sup>) ELV – Emission limit value (LD 236/98), understood as a monthly average, defined as the arithmetic average of daily averages referring to the operation days of a month, which should not be exceeded. The daily amount determined based on a representative sample of waste water discharged during a period of twenty-four hours may not exceed twice the monthly average (the sample shall be composed in a period of twenty-four hours taking into account the scheme for the disposal of wastewater generated);

(<sup>b</sup>) MPV – Maximum permissible value (Ordinance 423/97);

(<sup>c</sup>) Temperature of the receiving media after discharge of the effluent, measured at 30m downstream of the discharge point;

(<sup>d</sup>) The daily average value shall not exceed the average monthly;

(<sup>e</sup>) Value relative to the plant discharge for the HCH production, lindane extraction or HCH production and lindane extraction, simultaneously;

(<sup>f</sup>) In waters that feed lakes or reservoirs;

(<sup>g</sup>) In lakes or reservoirs;

(<sup>h</sup>) Linear Alkylbenzene Sulphonate

\* Parameters whose ELVs are set by Ordinance No. 423/97, being specific to the textile sector (except the wool subsector).

## **II. 3 Dye removal techniques**

Currently there are several methods that can be used in the removal of dyes from textile industrial effluents. However, due to the variety of existent dyes and to the effluents complexity, not all methods have the same efficiency and the combination of various methods may be required, since each method has its limitations. Existing methods can be divided into three categories: physical, chemical and biological.

### **II. 3.1 Physical methods**

Within the physical methods, adsorption and ion exchange have been the most studied, being effective methods for dyes removal, producing a high quality water, depending on the dye in question (Choy et al., 1999). However, the most commonly used adsorbents such as activated carbon, involve high costs, turning adsorption a less attractive process. Thus, low-cost adsorbents have been developed and have demonstrated good efficiency in dyes removal (Crini, 2006; Gupta and Suhas, 2009). Nevertheless, as a result of this treatment method the pollutants are transferred to another phase, leading to the formation of solid waste that needs to be further treated by another process.

Coagulation/flocculation method is also widely used in colour removal from textile effluents. Since large amounts of inorganic coagulants, such as iron and aluminium salts, are required to obtain good removals, causing the formation of large amounts of toxic sludge, organic coagulants leading to relatively low production of sludge have been developed (Zouboulis et al., 2004). However, this method has always high costs associated due to the reagents involved.

The separation processes by membranes as nanofiltration and reverse osmosis have been shown to be quite efficient methods for the removal of dyes from effluents. The ultrafiltration and microfiltration are useful to separate the dyes from larger molecules present in the effluents, since membranes have larger pores. However these processes have the disadvantage of high costs of installation, maintenance and the replacement of membranes. The fact that the membranes can be attacked by compounds present in effluents and the need for further processing the concentrate retained also decrease the attractiveness of the process (Vandevivere et al., 1998).

### **II. 3.2 Chemical methods**

Partial or complete oxidation (mineralization) of dyes present in textile industry effluents can also be achieved through advanced oxidation processes (AOPs) involving compounds with a very strong oxidation potential, such as ozonation, Fenton's reagent, UV/H<sub>2</sub>O<sub>2</sub> and UV/TiO<sub>2</sub>. These reactions usually involve the production of OH radicals that can oxidize a wide range of

compounds, being effective in the decolourization of a wide range of dyes (Aplin and Waite, 2000). However, these processes also have some drawbacks: ozonation involves high costs associated with the ozone generation, Fenton oxidation leads to the formation of large amounts of sludge, UV/H<sub>2</sub>O<sub>2</sub> besides being an expensive process, sometimes is not very effective, finally UV/TiO<sub>2</sub>, despite being a cheaper and a more effective method, its efficiency depends on the penetration ability of UV radiation in the highly coloured effluents (Gogate and Pandit, 2004; Vandevivere et al., 1998).

Coloured effluents can also be chemically oxidized with chlorine or hypochlorite. However, since toxic molecules such as aromatic amines are released during the process, the usage of this method has been decreasing over time (Slokar and Le Marechal, 1998).

Electrolysis is also an effective method to dye decolourization and in the reduction of BOD, COD, total organic carbon (TOC) and total suspended solids (TSS) (Alinsafi et al., 2005). However it has some disadvantages associated with the high costs involved in the electrodes replacement and with the high energy consumption during the process (Cerón-Riviera et al., 2004).

### **II. 3.3 Biological methods**

The use of biological methods to remove colour from textile effluents is usually a cheaper alternative, since it presents no major processing costs. However this method presents some disadvantages, since several dyes are designed to resist to microbial attack. Biological methods involve the use of bacteria, fungi and algae.

Bacterial degradation has been mainly applied in the removal of azo dyes. However, this biological method has been found ineffective in removing colour from several dyes. The azo dyes generally resist to aerobic degradation. However its degradation was observed in anaerobic conditions, but aromatic amines are formed as final product, which despite having no colour, can be toxic, mutagenic or carcinogenic (Isik and Sponza, 2007).

Under these anaerobic conditions it is not possible to degrade the aromatic amines formed, which in turn are only degraded in aerobic environment. Thus, to achieve a complete degradation of azo dyes a method that combines anaerobic treatment of the dyes with the mineralization of aromatic amines under aerobic conditions should be applied (Carvalho et al., 2008; Lin et al., 2010).

Fungi can degrade textile dye effluents through its own action or by enzymes digestion produced by them. Ligninolytic fungi are the most common in the treatment processes for textile dyes, although some non-ligninolytic are also effective (Ambrósio and Campos-Takaki, 2004; Wafaa et al., 2003). The decolourization of dyes by white rot fungi *Phanerochaete chrysosporium* was first discovered by Glenn and Gold (1983). The more studied white rot fungi in the degradation process are *Phanerochaete chrysosporium*, *Trametes versicolor*, *Bjerkandera adusta* and *Pleurotus ostreatus* (Chander and Arora, 2007; Wesenberg et al.,

2003). The degradation achieved varies with each used species. Recently, new species for the degradation of dyes have been studied (Asgher et al., 2009; Mendonça et al., 2008).

Some algae are known to be used in effective decolourization of dyes from textile wastewaters (El-Sheekh et al., 2009; Omar, 2008). The azo bond reduction is the mechanism of degradation followed by algae. Aromatic amines thus formed can be then totally mineralized (Wang et al., 2007).

Table II. 6 summarizes the advantages and the disadvantages of the various treatment methodologies for colour removal of industrial effluents (Allegre et al., 2006; Anjaneyulu et al., 2005; Husain, 2006; Robinson et al., 2001).

**Table II. 6** – Advantages and disadvantages of various decolourization methods for industrial effluents.

<b>Treatment methodology</b>	<b>Advantages</b>	<b>Disadvantages</b>
Membrane filtration	Removes all dye types. Recovery and reuse of chemicals and water. Wider application for complex wastes.	Concentrated sludge production. Dissolved solids are not separated in this process. High running cost.
Coagulation/Flocculation	Good removal efficiencies. Elimination of insoluble dyes.	Cost of coagulants and chemicals for pH adjustment. Dewatering and sludge handling problems.
Adsorption on activated carbon	Good removal efficiency. Suspended solids and organic substances well reduced.	Regeneration process with high cost. Excessive solid waste generation.
Ion-exchange	Regeneration with low loss of resins.	Specific application. Not effective for all dyes. Cost effective.
Electrochemical oxidation	No additional chemicals required and end products are non-hazardous. Capacity of adaptation to different volumes and pollution loads.	Process with high cost. Iron hydroxide sludges.
Advanced oxidation processes	Complete mineralization ensured. Growing number of commercial applications. Effective pretreatment methodology in integrated systems and enhances biodegradability.	Expensive process.
Ozonation	Effective for azo dye removal. No alteration in volume.	Not suitable for dispersed dyes. Releases aromatic amines. Short half-life (20 min.).
Fenton's reagent	Capable of decolourizing wide variety of wastes. Effective for both soluble and insoluble colourants.	Problem with sludge disposal that makes the process relatively expensive.

Photocatalysis	Process carried out at ambient conditions. Inputs are atoxic and inexpensive. Complete mineralization with shorter retention times.	Effective for small amount of colourants. Expensive process.
NaOCl	Initiates and accelerates azo-bond cleavage. Low temperature requirement.	Process with high cost. Release of aromatic amines.
Aerobic biodegradation	Colour removal is facilitated along with COD removal.	Longer retention times. Less resistant to recalcitrant compounds.
Anaerobic biodegradation	Resistant to wide variety of complex colourants. Bio gas produced is used for electricity and steam generation.	Longer acclimatization phase.
Bacterial, fungal and algal biodegradation	Good removal efficiency for low volumes and concentrations. Very effective for specific colourant removal.	Culture maintenance is expensive. Cannot cope up with large volumes of coloured effluents.

## II. 4 Enzymes in wastewater treatment

Enzymes have a number of features that make them more viable in relation to conventional catalysts: they are biodegradable catalysts, allow the operation at low and high substrate concentrations, allow the operation over a wide range of pH, temperature and salinity, have no delays associated with the acclimatization of biomass, have a reduced sludge formation, are simple and easy to control (Nicell et al., 1993).

However, enzymes also have some disadvantages such as high costs associated and instability when taken from the natural wild. According to Karam and Nicell (1997), recent biotechnological advances have allowed the production of cheaper and more available enzymes through improved purification and isolation processes. All these advantages added to their high specificities and catalytic activities with the possibility of designing enzymes with the exactly desired properties through genetic engineering and computational design, suggest the potential application of this process in the treatment of effluents (Call and Mucke, 1997).

The ligninolytic enzymes, like lignin peroxidase, manganese peroxidase and laccase are produced by white-rot-fungi (secreted into the extracellular environment of the fungi), normally when levels of nutrients such as carbon, nitrogen or sulfur become limiting (Barr and Aust, 1994). They are able to oxidize a large number of different compounds, and therefore they have been intensively studied in textile wastewater treatment.

A numbering system was developed by the Enzyme Commission where the enzymes are classified according to their class and with the kind of reactions that they catalyze. The prefix E.C. is generally employed with the numerical scheme (Blanch and Clark, 1997).

#### **II. 4. 1 Lignin peroxidase (LiP, EC 1.11.1.14)**

LiP is a glycoprotein heme produced mainly by *Phanerochaete chrysosporium* fungus that catalyzes the oxidation of phenolic, non phenolic and polycyclic aromatic hydrocarbons compounds as well as a variety of recalcitrant aromatic compounds. This enzyme requires hydrogen peroxide as cofactor and the reaction occurs through a mechanism of an electron oxidation followed by a series of non-enzymatic reactions (Garg and Modi, 1999). LiP's have many forms, with a molecular weight between 38-47 kDa and an isoelectric point of 3.2-4.7 (Leonowicz et al., 2001).

Some studies show that LiP is capable to decolourize mainly azo dyes, nevertheless, the decolourization of other types of dyes was also verified (Ollikka et al., 1993; Verma and Madamwar, 2002).

#### **II. 4.2 Manganese peroxidase (MnP, EC 1.11.1.13)**

MnP is also principally produced by *Phanerochaete chrysosporium* fungus together with LiP. It is also a glycoprotein heme with a molecular weight between 40-46 kDa and an isoelectric point of 2.9-7.0 (Leonowicz et al., 2001).

This enzyme requires free manganese ion for its activity. Initially it catalyzes the oxidation of  $Mn^{2+}$  to  $Mn^{3+}$  oxidizing, subsequently, several phenolic compounds. As the MnP enzyme varies from species to species, the ability to dye decolourization also changes with the kind of MnP used and with the reaction conditions (Li et al., 2009).

#### **II. 4.3 Laccases (EC 1.10.3.2)**

Laccases are either mono or multimeric copper-containing oxidoreductases that do not require coenzymes to catalyse the one-electron oxidation of a vast amount of phenolic substrates, through a reaction mechanism catalyzed by radicals. The final electron acceptor is the oxygen that is reduced to water (Baldrian, 2006).

Laccase was discovered by Yoshida in 1883 in plants (*Rhus vernicifera*), and characterized by Bertrand in 1985 after its isolation and purification (Mayer and Staples, 2002). Fungal laccases were discovered during the XIX century (Call and Mucke, 1997). Laccase can be produced by many plants (Hoopes and Dean, 2004) and fungi (Couto and Toca-Herrera, 2007), as well as by bacteria (Sharma et al., 2007). Most laccases have been isolated from white-rot fungi (Fonseca et al., 2010; Zhao et al., 2008).

A typical laccase reaction is shown in Figure II. 3, where a diphenol undergoes a one electron oxidation to form an oxygen-centred free radical. This active species can be converted to a quinone in a second enzyme-catalysed step or by spontaneous disproportionation. Quinone as well as the free radical products undergo non-enzymatic coupling reaction leading to polymerization (Thurston, 1994).

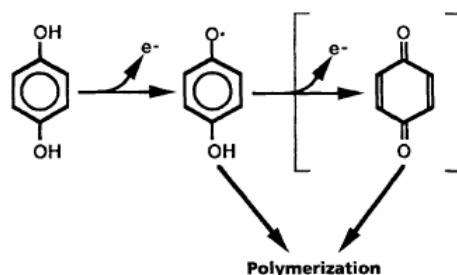
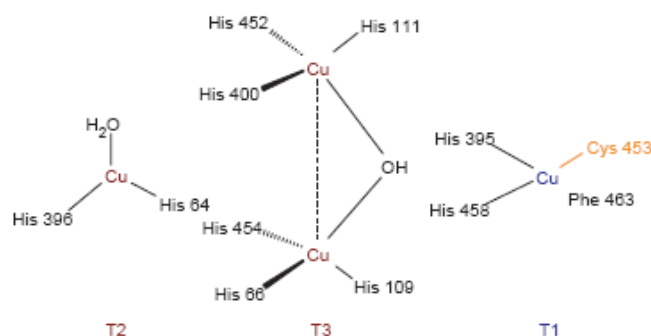


Figure II. 3 - A typical laccase reaction with a diphenol.

#### II. 4.3.1 Molecular and structural properties

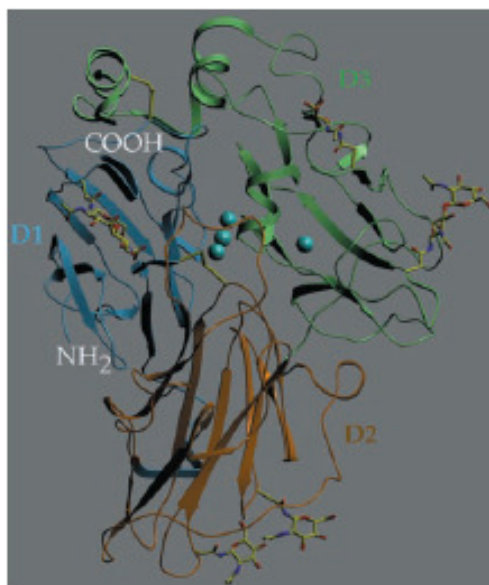
Laccase (benzenodiol:oxygen oxidoreductase) is a polyphenol oxidase, which belongs to the oxidoreductases enzymes class, also known by blue copper oxidase. In structural terms this glycoprotein normally contains four copper atoms per monomer, distributed in three different binding sites, copper  $T_1$ ,  $T_2$  and  $T_3$ , each one with an important role in the laccase catalytic mechanism. Copper  $T_1$  is involved in the capture and transfer of the electron to the trinuclear copper center  $T_2/T_3$ , which is involved in bonding with oxygen (Call and Mucke, 1997). Laccases usually comprise 520-550 amino acids, with a molecular weight ranging from 43 to 383 kDa depending on the fungal species (Baldrian, 2006). These enzymes are known to have a high stability due to the covalently linked carbohydrate moiety (10-45 %) (Claus, 2004).

The four copper atoms can be distinguished using UV/visible and electroparamagnetic resonance spectroscopy (EPR). One of the copper atoms belongs to the paramagnetic site  $T_1$ , is EPR detectable and presents a strong absorption at 610 nm, which gives rise to the typical blue colour of the copper oxidases. This is the place where substrate oxidation starts. Another atom belongs to the copper paramagnetic site  $T_2$ , does not confer colour but is EPR detectable. The other pair of copper atoms is strongly coupled by a hydroxyl bridge and belongs to the diamagnetic site  $T_3$ . This pair gives a weak absorbance in the near UV at 330 nm but is not detected by EPR. The  $T_1$  copper is usually coordinated to two nitrogens from two histidines and to a sulphur from cysteine. It is the bond of copper  $T_1$  to sulphur that is responsible for the characteristic blue colour of typical laccase enzymes. The reduction of molecular oxygen and the release of water occur in the trinuclear cluster formed by  $T_2$  and  $T_3$  coppers.  $T_2$  copper is coordinated by two histidines and  $T_3$  copper by six histidines (Figure II. 4) (Claus, 2004).



**Figure II. 4** – Model of the catalytic cluster of the laccase from *Trametes versicolor* made of four copper atoms (Riva, 2006).

Figure II. 5 shows the three-dimensional structure of laccase produced by *T. versicolor*.



**Figure II. 5** – Diagram of *Trametes versicolor* laccase. The arrangement of the structure of the three domains is depicted in different colours coding (D1–D3). Copper ions are drawn as blue spheres. Carbohydrates and disulfide bonds are included as stick models (Piontek et al., 2002).

The redox potential was determined for several laccases using different mediators, and ranges from 430 mV to 800 mV. It is important to remark that the redox potential of fungal laccases is independent of their origin species (Baldrian, 2006; Shleev et al., 2005).

Table II. 7 summarizes some important properties of fungal laccases.



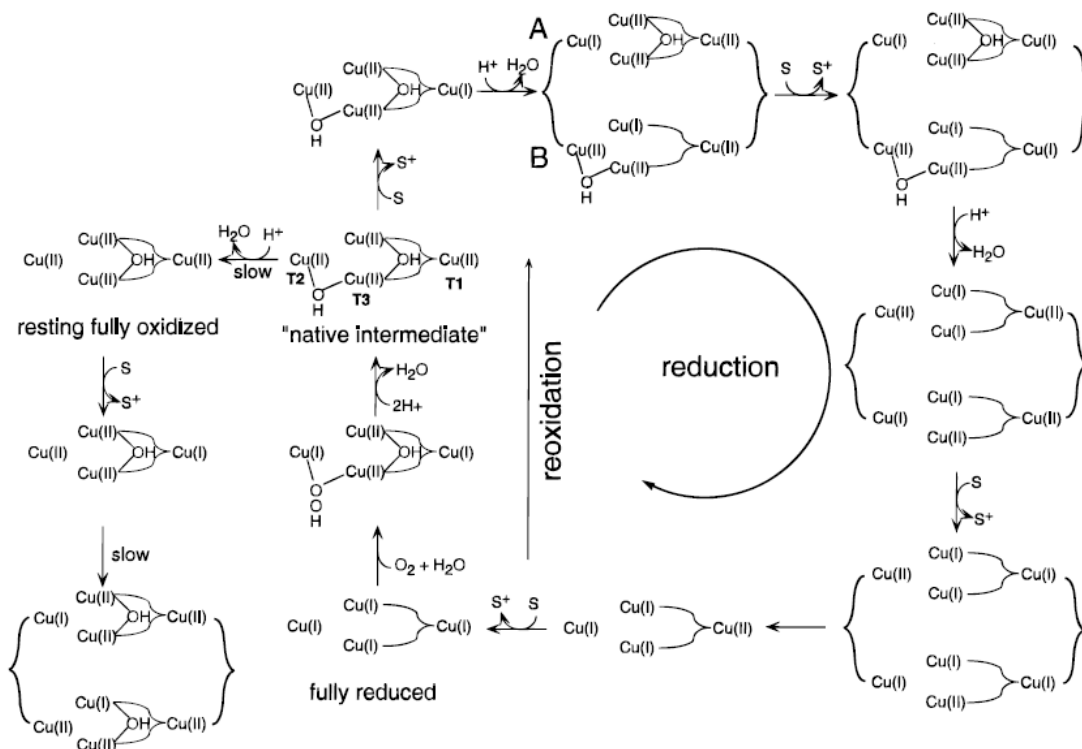
**Table II. 7** – Some properties of fungal laccases (Baldrian, 2006; Call and Mucke, 1997).

Property	Fungal Laccases
pH-Optimum	2.0 – 7.5
Temperature-Optimum (°C)	25 – 80
Molecular weight (kDa)	43 – 390
Copper content (atoms per molecule)	2 – 16
Redox potential (mV)	430 – 800
Isoelectric points	2.6 – 7.6

Beyond the interest in investigating laccase structure, catalytic mechanism and electrochemical properties, recently there has also been a great interest in developing new laccases through molecular evolution techniques (Giovanna et al., 2008; Rodgers et al., 2009).

#### II. 4.3.2 Catalytic cycle

Despite of not knowing the exact catalytic mechanism of laccase, several mechanisms have been proposed which are consistent with the available properties (Figure II. 6).



**Figure II. 6** – Proposed catalytic cycle of laccase showing the mechanism for reduction and oxidation of the copper sites (Solomon et al., 1996).

According to Durán et al. (2002) in the catalytic cycle of laccase, starting from the “native intermediate”, the substrate reduces the  $T_1$  site, which in turn transfers the electron to the trinuclear cluster, where molecular oxygen is reduced to water. Two possible mechanisms for the reduction of the trinuclear cluster are possible. The  $T_1$  and  $T_2$  sites together reduce the  $T_3$  pair (A in Figure II. 6) or each copper in the trinuclear cluster is sequentially reduced by electron transfer from  $T_1$  site (B in Figure II. 6), in which case the  $T_3$  no longer acts as a two-electron acceptor. Slow decay of the “native intermediate” leads to the resting fully oxidized form. In this form, the  $T_1$  site can still be reduced by substrate, but electron transfer to the trinuclear site is too slow to be catalytically relevant. The bridging to  $T_2$  center is linked to the stability of the intermediate peroxide, showing its importance to the reduction of oxygen (Cole et al., 1990).

### II. 4.3.3 Laccase applications

The practical applications of laccase have led to an increase in research of enzyme producing sources, particularly white-rot fungi. According to Mayer and Staples (2002) all laccase applications may be associated with its ability to produce free radicals from a suitable substrate.

During the last few years work on laccase applications has been extended. Reported applications include:

- Bioremediation, where toxic compounds and persistent environmental pollutants, in particular phenols, are removed from water and soil, contributing to its decontamination (Gianfreda et al., 2006);
- Design of fungicidal and bactericidal laccase preparations (Mougin et al., 2000);
- Green biodegradation of xenobiotics including pulp bleaching, providing milder and cleaner strategies for delignification (Widsten and Kandelbauer, 2008);
- Organic synthesis, such as polymerization (Ceylan et al., 2008), generation of colour from non-coloured substances (Pilz et al., 2003) or fuel ethanol improved production from renewable raw materials (Larsson et al., 2001);
- Enhancing or modification of beverage appearance, like wine (Minussi et al., 2007) or fruit juice stabilization (Alper and Acar, 2004) and improvement of beer storage life (Mathiasen, 1996) by polyphenols removal;
- Treatment of food, mainly as a baking aid (Selinheimo et al., 2006);
- Textile finishing, to improve the whiteness in conventional bleaching of cotton (Tzanov et al., 2003) or to bleach indigo dyes denim fabrics to lighter shades (Pazarlioglu et al., 2005);
- Development of biofuel cells (Barrière et al., 2006) and of biosensors, to detect various phenolic compounds, oxygen or azides (Haghighi et al., 2003) and to electrochemical measurements (Cordi et al., 2007) and also for electroimmunoassays (Kuznetsov et al., 2001);

- Medical applications, such as synthesis of complex therapeutic compounds (Nicotra et al., 2004), inhibition of HIV-1 reverse transcriptase (Wang and Ng, 2004), aceruloplasminemia fighting (Harris et al., 2004) and in distinction of morphine from codeine simultaneously in drug samples (Bauer et al., 1999);
- Desulfurization of harmful compounds emitted by fossil fuels (Villaseñor et al., 2004);
- Desinfection procedures with iodine formation through oxidation of iodide (Xu, 1996); painting and waving of hair, as less irritating processes (Jumino et al., 1994); cosmetic and dermatological preparations with proteins for skin lightening (Golz-Berner et al., 2004), in the leather area to improve dyeing efficiency and leather characteristics (Sorensen et al., 1993);

Moreover, interesting prospective directions for the application of the laccase in dye degradation have also been found.

Laccase enzymes are known to be able of successfully degrade various types of dyes such as azo, diazo and anthraquinone structures, among others, suggesting its application in the treatment of textile industrial effluents. However, due to the dye structures complexity and to the unawareness of enzymatic transformation mechanism, the capacity to describe laccase decolourization pathways still remains incomplete (Wesenberg et al., 2003).

Kirby et al. (2000) have demonstrated that laccase from *Phlebia tremellosa* was capable of decolourizing eight synthetic textile dyes (200 mg/L) more than 96 %. However, Nyanhongo et al. (2002) showed that dyes are not equally susceptible to enzymatic degradation. The decolourization rate depends both on the source of the enzyme preparation and on the structure of the dye. The optimum pH and temperature of decolourization vary with the dye to treat. Palmieri et al. (2005), have demonstrated that the extent of dye decolourization also depended on enzyme concentration.

Decolourization of Remazol Brilliant Blue Royal and Drimaren Blue CL-BR was investigated using laccase from three white rot fungi named as *Pleurotus ostreatus*, *Coriolus versicolor* and *Funalia troggi*. Maximum and minimum decolourizations were obtained by laccases from *Funalia troggi* and *Pleurotus ostreatus*, respectively (Erkurt et al., 2007).

Purified laccase from a white rot fungus strain SQ01 was capable of decolourizing a variety of synthetic dyes, including azo, triphenylmethane and anthraquinone dyes, but only few were completely removed, while others were not completely degraded even with increased decolourization time (Yang et al., 2009).

Kalme et al. (2009) reported that a laccase from *Pseudomonas desmolyticum* NCIM 2112 showed an optimum pH character that is substrate depending. Its decolourization of Direct Blue 6, Green HE4B and Red HE7B dyes also revealed a structural requirement of the dye to be degraded.

Some studies proposed several mechanisms for laccase catalyzed oxidation of azo dyes by generation of phenoxy radicals through one electron oxidations. These mechanisms avoid the formation of aromatic amines, leading to the detoxification of azo dyes (Figure II. 7).

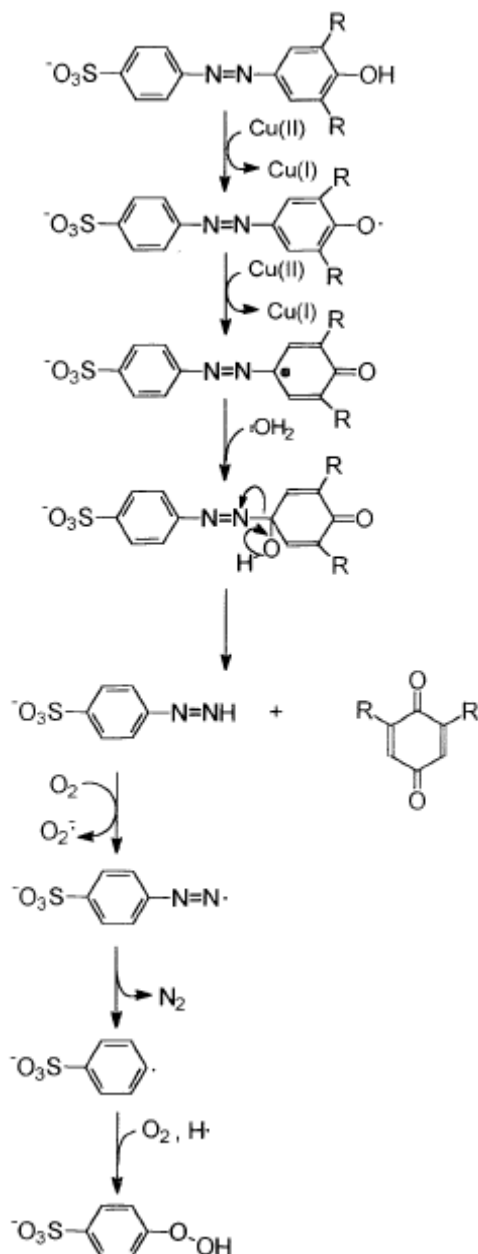


Figure II. 7 – Oxidation of phenolic-azo dyes by laccases (Chivukula and Renganathan, 1995) .

#### II. 4.3.4 Laccase mediators

Due to the lower redox potential, laccase can only oxidize phenolic compounds. However, the laccase application in the presence of small natural compounds of low molecular weight with high redox potential ( $> 900$  mV), called mediators, makes possible the oxidation of non-phenolic compounds or other compounds with redox potentials higher than those of laccase (Bourbonnais and Paice, 1990).

Laccases from different sources have different redox potentials. The difference between the enzyme and substrate redox potentials defines the need of a redox mediator (Soares et al., 2001). The mediator is a compound with low molecular weight which acts as an electron carrier. Once it is oxidized by the enzyme, it diffuses away from the catalytic system and in turn oxidizes any substrate that, because of its high redox potential could not be directly oxidized by the enzyme or that is not able to enter in the enzyme active site due to its larger size (Figure II. 8).

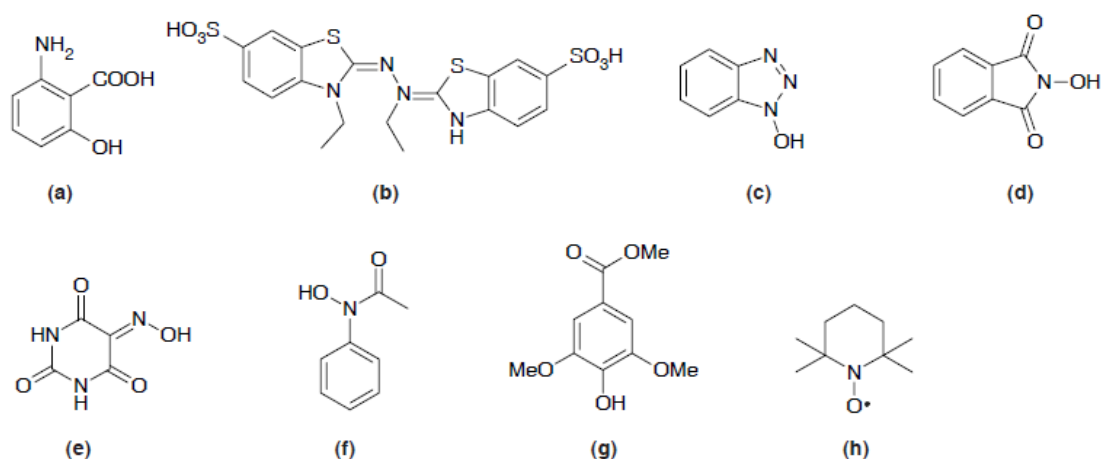


**Figure II. 8** - Catalytic cycle of a laccase-mediator oxidation system (Riva, 2006).

The activity of a laccase-mediator system depends on enzyme redox potential and on the stability and reactivity of the oxidized mediator. According to Bourbonnais et al. (1997) laccases from different organisms react variably with different mediators and different substrates. An ideal redox mediator must be a good laccase substrate; its oxidized and reduced forms must be stable but should not inhibit the enzymatic reaction (Johannes and Majcherczyk, 2000).

The first mediator to be used in laccase-mediator system was the azine 2,2'-azino-bis-(3-ethylbenzothiazoline-6-sulfonic acid) (ABTS), which was reported by Bourbonnais and Paice (1990). More than one hundred other compounds such as triazole 1-hydroxybenzotriazole (HBT), violuric acid (VA) and 2,2,6,6-tetramethylpiperidine-1-yloxy (TEMPO) have been tested since then for their laccase mediator ability. Various phenolic compounds (Murugesan et al., 2009) or anthraquinones dyes (Wong and Yu, 1999) were also evaluated with the aim of identifying cheaper, more efficient and ecofriendly mediators for the decolourization of recalcitrant dyes and for other industrial and environmental applications.

Figure II. 9 shows some possible laccase mediators.



**Figure II. 9** – Examples of laccase mediators: (a) 3-Hydroxyanthranilic acid (HAA); (b) 2,2'-azino-bis-(3-ethylbenzothiazoline-6-sulphonic acid) (ABTS); (c) N-hydroxybenzotriazole (HBT); (d) N-hydroxyphthalimide (HPI); (e) violuric acid (VLA); (f) N-hydroxyacetanilide (NHA); (g) methyl ester of 4-hydroxy-3,5-dimethoxybenzoic acid (syringic acid); (h) 2,2,6,6-tetramethylpiperidine-1-yloxy (TEMPO) (Riva, 2006).

The substrate oxidation mechanism by the mediator depends on the chemical structure of the mediator. In the case of ABTS several studies suggest a mechanism of electron transfer to the substrate. For mediators such as HBT and violuric acid (VA), if weak C-H bonds are present in the substrate, a mechanism of transfer of hydrogen atom is suggested (Cantarella et al., 2003; Galli and Gentili, 2004). The mediator TEMPO follows a different mechanism, the ionic oxidation (d'Acunzo et al., 2002).

The action mechanism of laccase-mediator system in dyes degradation has been extensively studied and it has been observed that the dye decolourization capability of a laccase depends on its species and strain and on the structure of the dye. Although Peralta-Zamora et al. (2003) reported that *T. versicolor* laccase (strain CCT-4521) decolourized Reactive blue 19 only in presence of HBT, laccase from *T. versicolor* (ATCC 20869) decolourized the anthraquinone dye without a redox mediator (Champagne and Ramsay, 2005). An anthraquinone dye SN4R was effectively decolourized by a crude laccase from *Pleurotus ostreatus* strain 32. However, the decolourization rate was increased by 90% with ABTS addition as a mediator of laccase and the decolourization time was shortened to about twice as fast as that without mediator (Hou et al., 2004).

Laccase from *Funalia troggi* was evaluated in the decolourization of several dyes from different classes (azo, anthraquinone, Cr-complexed class) commonly used in textile applications. The more recalcitrant dyes degradation was only achieved through the combined action of the laccase and the mediator. Correlations among the decolourization degree of the various dyes and their electronic and structural diversities were rationalized and discussed (Ciullini et al., 2008). The decolourization and detoxification of a textile industry effluent by laccase from *Trametes troggi* in the presence and the absence of laccase mediators was

investigated. The effluent was not degraded at any enzyme concentration. The degradation only occurred in the presence of a mediator, with HBT being the most effective (Khlifi et al., 2010).

Zille et al. (2004) observed a linear relationship between the redox potential of the azo-dyes and the decolourization efficiency of enzyme, enzyme/mediator. The less positive the anodic peak of the dye, the more easily it was degraded oxidatively with laccase. Although there are already many studies on the decolourization of dyes by the enzyme laccase, due to the huge number of dyes available, many studies are still needed in this field.

#### II. 4.3.5 Enzyme kinetics fundamentals

Enzyme kinetics studies the rate of reactions catalyzed by enzymes. The intrinsic kinetics of enzymatic reactions can be obtained by measuring the reaction rate while certain reaction conditions vary.

The effect of typical substrate concentration on the rate of an enzymatic reaction can be seen in Figure II. 10. For very low substrate concentrations, the initial reaction rate,  $v_0$ , is proportional to the substrate concentration, being a first order reaction. With the increase of substrate concentration, the reaction rate begins to decrease, being no longer linearly proportional to the substrate concentration. From a certain substrate concentration value, the reaction rate becomes almost independent of the substrate concentration, approaching asymptotically a constant value ( $v_{max}$ ). In these substrate concentration values the reaction may be considered of zero order and the enzyme is saturated with the substrate.

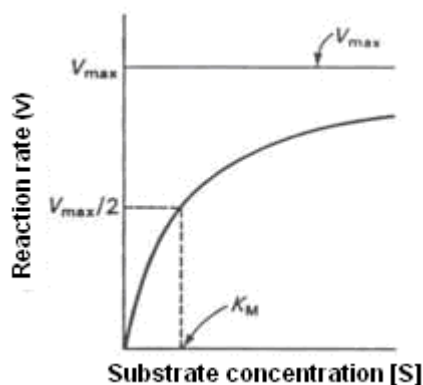


Figure II. 10 – Enzymatic kinetics.

By analyzing the enzymatic reactions behaviour, Michaelis and Menten proposed in 1913 that the enzyme ( $E$ ) first binds rapidly and reversibly to the substrate ( $S$ ) giving rise to an enzyme-substrate complex ( $ES$ ), where the substrate is held to the enzyme by physical forces. This complex then undergoes a chemical change, resulting in the formation of product ( $P$ ) and in the release of product from the enzyme, with a first order dependence on the concentration of the enzyme-substrate complex. This reaction can be expressed as follows:



where  $K_S$  is the dissociation constant of the enzyme-substrate complex and  $k_2$  is the first order rate constant for release of product from the complex.

From the proposed model, Michaelis and Menten developed an equation that allows to demonstrate how the reaction rate ( $v$ ) varies with substrate concentration  $[S]$ :

$$v = \frac{v_{max} [S]}{K_M + [S]} \quad (\text{II. 1})$$

where  $v_{max}$  is the maximum reaction rate and  $K_M$  is the Michaelis-Menten constant. For the simple reaction mechanism shown above,  $K_M$  is equal to  $K_S$ , the dissociation constant of  $ES$ , and corresponds to the substrate concentration for which the reaction rate is half the maximum rate, being a measure of the affinity of the enzyme for a particular substrate. The lesser the value of  $K_M$  the larger is the affinity of the enzyme to the substrate, i.e., an enzyme that has a low value of  $K_M$  for a substrate, reaches its maximum catalytic efficiency at a low concentration of substrate (Blanch and Clark, 1997).

Laccase oxidizes a very wide range of substrates. However, the catalytic constants have been reported mostly for a small group of substrates: ABTS and the phenolic compounds 2,6-dimethoxyphenol (DMP), guaiacol and syringaldazine (Table II. 8 ). These constants have been measured for a large number of laccases, and significant variations can be observed among them.

**Table II. 8** – Kinetic parameters of laccase for some substrates (Baldrian, 2006).

Catalytic constant	n*	Median	Min	Max
$K_M$ ( $\mu\text{M}$ )				
ABTS	36	39	4	770
2,6-Dimethoxyphenol	30	405	26	14720
Guaiacol	23	420	4	30000
Syringaldazine	21	36	3	4307
$k_{cat}$ ( $\text{s}^{-1}$ )				
ABTS	12	24050	198	350000
2,6-Dimethoxyphenol	12	3680	100	360000
Guaiacol	10	295	90	10800
Syringaldazine	4	21500	16800	28000

\*n: number of observations

Despite the large variation observed for different substrates, usually each enzyme has a characteristic catalytic performance  $k_{cat}$  ( $v_{max}/[E_0]$ , where  $[E_0]$  is the total amount of enzyme in the system). In general, laccases present high affinity for ABTS and syringaldazine with high



catalytic constant, whereas the oxidation of guaiacol and DMP is considerably slower and the respective  $K_M$  constants higher (Baldrian, 2006).

In 1994, Yaropolov et al. discussed the kinetic data of laccases from different sources. The values of  $K_M$ , Michaelis-Menten constant, are similar in case of co-substrate be the oxygen (about  $10^{-5}$ ), but the  $v_{max}$  value varies with the laccase source ( $50\text{-}300\text{ M}\cdot\text{s}^{-1}$ ) and with substrate. The kinetic constants differ in their pH dependence.  $K_M$  is pH independent for both substrate and co-substrate, while the  $k_{cat}$  is pH dependent (Call and Mucke, 1997).

### II. 4.3.5 Immobilization

Enzymes exhibit a number of features that make their use advantageous as compared to conventional catalysts. However, they have also a number of drawbacks when used as an efficient treatment method of wastewaters, such as their high cost of isolation and purification, their instability towards thermal and pH denaturation, their non-reusability and inactivation by inhibitors. The use of immobilized enzymes can increase their operational stability and durability and can provide easy separation of the product from reaction media and easy recovery of the enzyme. Furthermore, enzyme immobilization would allow the reuse of the enzyme and thus decrease the cost of industrial applications and allow the control of the process (Cao, 2005; Duran et al., 2002). As result of structural changes induced by immobilization and of the new environment, the immobilized enzyme typically has a lower activity and a higher Michaelis-Menten constant.

Several techniques may be applied to immobilize enzymes on solid supports. They are mainly based on chemical and physical mechanisms (Duran et al., 2002). Therefore, it is hardly surprising that there is no general universally applicable method of enzyme immobilization. The main task is to select a suitable carrier, conditions (pH, temperature and nature of medium) and enzyme itself (source, nature and purity) to design an immobilized biocatalyst. The selected method should meet both the catalytic needs (expressed in productivity, space-time, yield, stability and selectivity) and the non-catalytic needs (e.g. separation, control, down-streaming process) that are required by a given application (Bornscheuer, 2003; Dyal et al., 2003).

According to Duran et al. (2002) both chemical and physical methods offer advantages and disadvantages that depend on several factors. In general, chemical immobilization methods tend to reduce the activity of the enzyme, since the covalent bonds, formed as a result of immobilization, may perturb the enzyme native structure. By contrast, such covalent linkages provide strong and stable enzyme attachment and may, in some cases, reduce enzyme deactivation rates and usefully alter enzyme specificity. However, entrapment and adsorption immobilization methods typically perturb the enzyme less and consequently offer retention of the enzyme properties resembling those in solution. A proper choice between chemical and physical methods depends on several factors. Usually, a long-time applicable immobilized enzyme with a lower initial activity is preferable to that with a high level of initial activity but with

a short-time activity retention. Table II. 9 makes a comparison between the main methods of enzymes immobilization.

**Table II. 9 - Comparison of enzyme immobilization methods.**

<b>Characteristics</b>	<b>Adsorption</b>	<b>Covalent binding</b>	<b>Entrapment</b>	<b>Membrane confinement</b>
<b>Preparation</b>	simple	difficult	difficult	simple
<b>Cost</b>	low	high	moderate	high
<b>Binding force</b>	variable	strong	weak	strong
<b>Enzyme leakage</b>	yes	no	yes	no
<b>Applicability</b>	wide	selective	wide	very wide
<b>Running Problems</b>	high	low	high	high
<b>Matrix effects</b>	yes	yes	yes	no
<b>Large diffusional barriers</b>	no	no	yes	yes

The support also plays an important role on enzyme immobilization, influencing immobilization efficiency and enzyme stability. It is necessary to take into account their geometric properties, its stability, its chemical and physical nature, and finally, their costs.

In order to achieve an economically viable application at industrial level, effective but cheap supports and immobilization techniques are needed. Some cheaper supports from agro-industrial residues, like functionalized rice husk for invertase immobilization (D'Souza and Godbole, 2002), rice straw for lipase immobilization (Castro et al., 2001) and spent grains from breweries for trypsin immobilization (Rocha et al., 2005) were already reported.

Laccase immobilization was extensively studied with a wide range of different methods, supports and substrates. Table II. 10 reports some immobilized laccases on various supports applied in dye decolourization. The laccase source, the immobilization method, the dyes and the decolourization efficiency are specified.

Table II. 10 – Applications of immobilized laccases in dye decolourization.

Laccase source	Immobilization method	Dyes	Decolourization efficiency	References
<i>Coriolopsis galica</i>	Covalent on activated agarose	Reactive blue 198 – Dye effluent	70 %	(Reyes et al., 1999)
<i>Trametes versicolor</i>	Covalent on silica	Reactive blue 19 (anthraquinone), Remazol black B (azo), Reactive orange 122 (azo), Reactive red 251	45 % (0.5 h), 9 %, 55 % (0.5 h), 25 % (0.5 h)	(Peralta-Zamora et al., 2003)
<i>Trametes modesta</i>	Covalent on Al <sub>2</sub> O <sub>3</sub>	Lanaset Blue R (anthraquinone), Acid blue 74 (indigoid), Crystal violet (triphenyl-methane dye), Phenyl azo dye	100 % (10-12h) 99 % 98 % 99 %	(Kandelbauer et al., 2004)
<i>Pleurotus ostreatus</i>	Eupergit C (epoxy activated acrylic carrier)	Reactive blue 19	56 %	(Russo et al., 2008)
<i>Rhus vernicifera</i>	Poly (GMA/EDGMA)	Reactive red 120	91 % (10h)	(Arica et al., 2009)

## II. 5 References

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## **Part III**

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### Optimization of Decolourization Equilibrium and Cyclic Voltammetry



*This part focuses the optimization of the reactive dyes degradation equilibrium by pure laccase (DeniLite II Base) and by a commercial laccase formulation (DeniLite II S) in batch reactors. The best working conditions are established and voltammetric studies are performed in order to help predict the ability of the laccase to degrade the reactive dyes.*

*In part III. 1 the decolourization of six reactive textile dyes (reactive blue 114, reactive black 5, reactive yellow 15, reactive yellow 176, reactive red 180 and reactive red 239) by pure laccase (DeniLite II Base) is optimized, studying the effect of adding five typical laccase mediators and of the variation of its concentration, temperature and pH.*

*In parts III. 2 and III. 3 the degradation of the same reactive dyes by a commercial laccase formulation, including the enzyme, a buffer and an enzyme mediator is optimized using a three-level Box-Behnken full factorial design with three factors (pH, temperature and enzyme concentration) combined with response surface methodology.*

*Finally, in part III. 4 cyclic voltammetry is applied to better understand the degradations previously achieved and to try to predict the decolourization capacity of laccase by enzymes and reactive dyes redox potentials. The ability of laccase for sequential decolourization of the different dyes is also evaluated, in order to establish a reactor system that allows decolourization over an extended period without addition of new enzyme.*



## **Part III. 1** Optimization of reactive textile dyes degradation by laccase-mediator system\*

III. 1.1 Abstract

III. 1.2 Introduction

III. 1.3 Materials and Methods

III. 1.4 Results and Discussion

III. 1.5 Conclusions

III. 1.6 References

*\*based on: Tavares, A.P.M., Cristóvão, R.O., Loureiro, J.M., Boaventura, R.A.R., Macedo, E.A., 2008. Optimisation of reactive textile dyes degradation by laccase-mediator system. Journal of Chemical Technology and Biotechnology, 83, 1609-1615.*



## **III. 1 Optimization of reactive textile dyes degradation by laccase-mediator system**

### **III. 1.1 Abstract**

In the textile industry, large quantities of intensely coloured and toxic effluents are released, causing serious environmental pollution. Several biotechnological approaches have been suggested to eliminate this pollution source in an eco-efficient manner. Laccase can be used to decolourize dyes and its substrate range can be extended by inclusion of a mediator.

A screening using several laccase mediators (2,2-azinobis(3 ethylbenzothiazoline-6-sulfonate) (ABTS), 1-hydroxybenzotriazole (HBT), *N* hydroxyacetanilide (NHA), polioxometalates, violuric acid (VA) and (2,2,6,6-tetramethylpiperidin-1-yloxy) (TEMPO)) was performed on the degradation of six reactive textile dyes. ABTS was the most effective mediator leading to higher decolourization. The efficiency of ABTS depends on the type of dye, pH, temperature and dye concentration. The optimum temperature and pH values were 35 °C and 5.0, respectively, for maximum decolourization (above 70 %) of reactive black 5, reactive blue 114 and reactive yellow 15. For reactive red 239 the optimum conditions were found to be a temperature of 40 °C and pH of 4.5 (above 56 % decolourization). ABTS has no effect at low concentrations, except for reactive blue 114, where it resulted in the best decolourization (93 %). A comparison of decolourization based on the percentage absorbance reduction at the maximum absorbance wavelength of each dye and throughout the visible spectrum was made.

These results suggest that the laccase mediator system could be used to treat textile dyeing wastewaters.

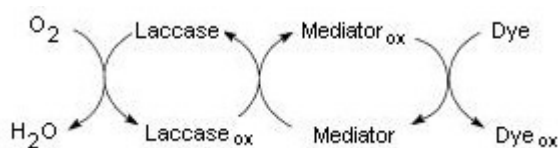
### **III. 1.2 Introduction**

In textile industry, colour is applied to finished products through dyeing, resulting in the generation of different wastewaters. During the process textile industries release large quantities (about 10 % of the global wastewater) of intensely coloured and toxic effluents (O'Neill et al., 1999), which cause serious environmental pollution. The rivers water quality depends on the colour and transparency of water. The dyes change the absorption and reflection of sunlight on the water, negatively affecting the photosynthesis. Additionally, there are other quality indicators such as the presence of colourless contaminants and biological oxygen demand (BOD) that are also important to evaluate the water quality. A number of biotechnological approaches have been suggested with potential interest to eliminate this pollution source in an eco-efficient manner (Wesenberg et al., 2003). It is known that white-rot fungus or lignolytic enzymes (e.g. Mn peroxidase, Lignin peroxidase and Laccase) could be used to decolourize dyes (Amaral et al., 2004; Lan et al., 2006; Mielgo et al., 2003; Osma et al.,

2007) as well as in pulp and paper industry (Arias et al., 2003; Font et al, 2003). Laccase is principally produced by white-rot fungus including *T. versicolor* (Tavares et al., 2005).

Laccase (*p*-diphenol oxidase, EC 1.10.3.2) is a multi-copper oxidase, belonging to a family of enzymes, called the large blue copper proteins. The range of substrates which laccase can attack are any phenolic substrates such as *p*-diphenol (Thurston, 1994). Laccase alone has a limited effect on textile dye degradation due to its specificity for phenolic compounds, however the range of laccase substrates can be extended to nonphenolic compounds by inclusion of a specific compound, called mediator, such as 2,2-azinobis(3-ethylbenzothiazoline-6-sulfonate) (ABTS) (Wong and Yu, 1999), 1-hydroxybenzotriazole (HBT) (Murugesan et al., 2007), and *N*-hydroxyacetanilide (NHA) (Chakar and Ragauskas, 2004), polioxometalates (Gamelas et al., 2005; Tavares et al., 2004), violuric acid (VA) (Soares et al., 2002) and (2,2,6,6-tetramethylpiperidin-1-yloxy) (TEMPO) (Fabbrini et al., 2002). Within the past several years, laccase-mediator system (LMS) has received must interest from the textile industry (Soares et al., 2001) and from the pulp and paper industries (Gutierrez et al., 2006) for application in environmentally friendly bleaching processes.

The role of mediators in enzymatic catalytic oxidation by laccase is described by redox cycles as shown in Figure III. 1.1.



**Figure III. 1.1** – Representation of dye degradation by laccase mediator system.

The mediator is a compound with low molecular weight, which acts as an electron carrier. Once it is oxidised by the enzyme, it diffuses away from the catalytic system and in turn oxidises any substrate that, due to its size, could not be directly oxidised by the enzyme (Call and Mucke, 1997).

The aim of this work is to optimize the dye degradation of six reactive dyes typically used in Portuguese textile industries, namely C.I. Reactive Black 5 (RB5), C.I. Reactive Blue 114 (RB114), C.I. Reactive Yellow 15 (RY15), C.I. Reactive Yellow 176 (RY176), C.I. Reactive Red 180 (RR180) and C.I. Reactive Red 239 (RR239). For this purpose five traditional laccase mediators, temperature, pH and mediator concentrations were tested in order to evaluate the decolourization by LMS.



### III. 1. 3 Materials and Methods

#### III. 1.3.1 Chemicals and enzyme

Textile Dyes: reactive black 5 (Remazol Black B), reactive yellow 176 (Remazol Yellow 3RS), reactive yellow 15 (Remazol Yellow GR), reactive red 239 (Remazol Brilliant Red 3BS), reactive red 180 (Remazol Brilliant Red F3B) and reactive blue 114 (Levafix Brilliant Blue E-BRA) were kindly provided by DyStar (Portugal). Information on dyes is given in Table III. 1.1. The chemical structures of reactive yellow 176 and reactive blue 114 are not provided by DyStar and are not found in the literature.

Enzyme: Commercial laccase (Denilite II Base; 800 U/g) from genetically modified *Aspergillus* was kindly provided by Novozymes (Denmark).

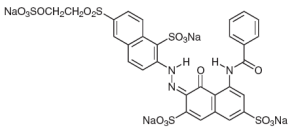
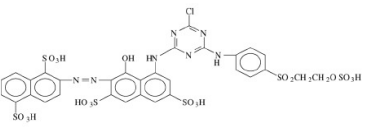
Enzyme Mediators: 2,2-azinobis(3-ethylbenzothiazoline-6-sulfonic acid) (ABTS); violuric acid (VA); *N*-hydroxyacetanilide (NHA); 1-hydroxybenzotriazole (HBT) and 2,2,6,6-tetramethylpiperidin-1-yloxy (TEMPO) were supplied by Sigma-Aldrich (Spain).

**Table III. 1.1a** – Dyes employed in the study.

<b>Dyes</b>			
<b>Colour index</b>	Reactive Black 5	Reactive Yellow 15	Reactive Yellow 176
<b>Abbreviation</b>	RB5	RY15	RY176
<b>Trade name</b>	Remazol Black B	Remazol Yellow GR	Remazol Yellow 3RS
<b>Chemical structure</b>			na
<b><math>\lambda_{max}</math> (nm)</b>	579	416	421
<b>Purity (%)</b>	70-80	na*	na
<b>Reference</b>	(Peralta-Zamora et al., 2003) <sup>†</sup>	(Voncina and Le-Marechal, 2003)	-

\*na: not available; <sup>†</sup>Reference only for dye structures

Table III. 1.1b – Dyes employed in the study (continued).

Dyes			
<b>Colour index</b>	Reactive Red 180	Reactive Red 239	Reactive Blue 114
<b>Abbreviation</b>	RR180	RR239	RB114
<b>Trade name</b>	Remazol Brilliant Red F3B	Remazol Brilliant Red 3BS	Levafix Brilliant Blue E-BRA
<b>Chemical structure</b>			na
<b><math>\lambda_{max}</math> (nm)</b>	540	542	593
<b>Purity (%)</b>	na*	na	65-75
<b>Reference</b>	(Hamlin et al., 1999) †	(Liu and Chiou, 2005)	-

\*na: not available; †Reference only for dye structures

### III. 1.3.2 Dye decolourization experiments

#### III. 1.3.2.1 Mediator screening

The reaction mixture for mediator screening consisted of an aqueous solution of each dye (50 mg/L), laccase (0.2 U/mL), redox mediator ABTS; HBT; TEMPO; NHA and VA (0.1 mM) and 50 mM phosphate buffer (pH 5.0) in a final volume of 25 mL, as shown in Figure III. 1.2. The reactions were incubated at 25 °C with stirring during one day (necessary time to attain the equilibrium). Control without mediator and control without laccase were carried out in parallel. 1.25 mL of dye from stock solution (1 g/L) was added to a specific volume of mediator (stock solution 1 mM) and buffer in order to obtain the desired concentration to a final reaction volume of 25 mL.



Figure III. 1.2 – Initial solutions of each dye (RY176, RY15, RR239, RR180, RB114 and RB5).

### III. 1.3.2.2 Effect of temperature and pH

To study the effect of temperature and pH on decolourization of the six textile dyes, 50 mg/L of each dye, 0.1 mM of ABTS as mediator and 0.2 U/mL of commercial laccase were incubated in 25 mL Erlenmeyer flasks under stirring for 24 h. The effect of temperature was studied in phosphate buffer (50 mM) pH 5.0. The dye solution was incubated at 20, 30, 35, 40 and 50 °C under orbital stirring at 320 rpm. An IKA stirrer (KS 130 basic) was used in all experiments. The dye concentration was chosen according to the values supplied by DyStar (Portugal), which is a typical dye concentration found in textile industry wastewater.

The effect of pH was studied at 40 °C by the incubation of dye solution in the following buffers: 50 mM of citrate/phosphate for pH 3.0, 4.0 and 4.5; 50 mM of phosphate for pH 5.0, 5.5, 6.0 and 7.0. Assays were done twice.

### III. 1.3.2.3 Effect of initial mediator concentration

To determine the effect of ABTS concentration on the decolourization of the six textile dyes, concentrations from 0.001 to 0.5 mM were tested. The reaction mixture consisted of 50 mg/l of each dye and 0.2 U/mL of commercial laccase. It was incubated in 25 mL Erlenmeyer flasks at 40°C with phosphate buffer (50 mM/pH 5.0) with orbital stirring at 320 rpm for 24 h. Assays were done in triplicate.

### III. 1.3.2.4 Determination of dye degradation

Dye decolourization by LMS was determined by monitoring the decrease in the absorbance peak at the maximum wavelength for each dye: reactive black 5 (579 nm), reactive yellow 176 (421 nm), reactive yellow 15 (416 nm), reactive red 239 (542 nm), reactive red 180 (540 nm) and reactive blue 114 (593 nm) or calculating (by integration of absorbance between 350 to 750 nm) the total area under the plot. UV-visible spectrophotometer (Thermo, model UV1) was used in all experiments. Decolourization is reported as: % decolourization =  $(A_i - A_f)/A_i \times 100$ , where  $A_i$  is the initial absorbance or total area from the initial spectrum and  $A_f$  is the final absorbance of the dye or total area from the final spectrum.

## III. 1.4 Results and Discussion

### III. 1.4.1 Mediator screening

LMS has been already described in several works (Riva, 2006) for delignification processes, but few research studies on its use for reactive textile dyes degradation are available. In order to evaluate the best mediator for the decolourization of six reactive textile dyes, 5 compounds (HBT, ABTS, NHA, VA and TEMPO) were screened as redox mediators of

laccase. In these assays, a decrease in the intensity of absorption at the maximum wavelength ( $\lambda_{\text{max}}$ ) of each dye was shown.

According to the results in Table III. 1.2, the experiments with laccase and without mediator did not decolourize any dye during the incubation time, demonstrating that these reactive dyes were not primary substrates of laccase. However when redox mediator was introduced, the catalytic mechanism of decolourization started, the extent depending on the dye and on the mediator. In addition, experiments without laccase and with mediator did not decolourize the dyes. These results indicated that oxidation of reactive dyes occurs only when laccase and mediator are both present and the different results for the same mediator show that the decolourization probably depends on the structure of the dye (Almansa et al., 2004). RR180, RY176 and RR239 presented much more resistance to decolourization leading to only a small degradation i.e., a decolourization lower than 5 % for all mediators employed. Significant dye degradation was observed for RY15, RB5 and RB114 when ABTS was used, producing decolourization of 21, 42 and 70 % respectively.

**Table III. 1.2** – Mediator screening for reactive dye degradation by laccase.

Reactive Dye	Dye degradation (%)					
	No mediator	HBT	ABTS	TEMPO	NHA	VA
RB114	ND <sup>a</sup>	0.3	<b>70</b>	ND	1.5	5.0
RR180	ND	0.6	ND	1.7	ND	2.3
RR239	ND	0.3	<b>4.7</b>	1.8	0.3	4.0
RB5	ND	0.2	<b>42</b>	1.5	ND	2.5
RY15	ND	2.7	<b>21</b>	2.0	0.8	0.2
RY176	ND	1.8	ND	1.6	ND	ND

<sup>a</sup>ND, not detected.

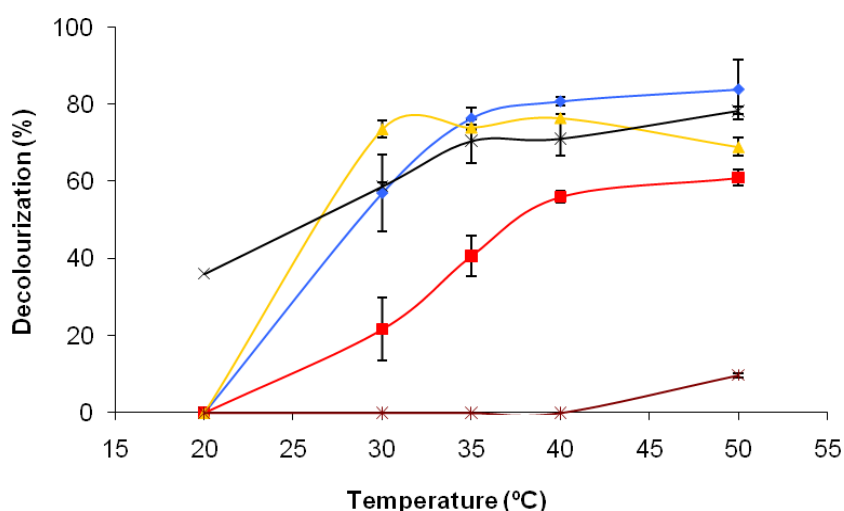
Laccase cannot decolourize these reactive dyes directly; a mediator is necessary. Reasons may be that the redox potential of the six reactive dyes is higher than that of laccase or the dyes cannot access the active site of the enzyme because of their steric structure. Thus a mediator is necessary to transfer electrons from the dye to the enzyme, as explained below.

The redox mediators used in this work were previously established as appropriate mediators of laccase (Camarero et al., 2005; Couto et al., 2005). However, in this study the results show that ABTS was a more effective mediator than the others for the oxidative degradation of the reactive textile dyes. The mechanism of dye oxidation by LMS is shown in Figure III. 1.1. First laccase oxidises ABTS to a cationic radical,  $\text{ABTS}^{\cdot+}$  then to the dication  $\text{ABTS}^{2+}$  (Bourbonnais and Paice, 1990). The oxidised ABTS degrades the substrate. The reduced laccase returns to the original status by transferring the electrons to oxygen and producing water. Bourbonnais et al. (1998) showed that the dication ( $\text{ABTS}^{2+}$ ) is responsible for the oxidation of the non phenolic substrates. In this catalytic system the small molecules of the

mediator act as electron carriers between the laccase and the dye. Thus, ABTS was selected as a redox mediator to optimize the conditions of textile dyes degradation by laccase.

### III. 1.4.2 Effect of temperature on textile dye degradation

To determine the optimum temperature for dye decolourization a temperature range of 25–50 °C was examined for a LMS with ABTS as redox mediator. In these experiments pH and ABTS concentration were fixed at 5.0 and 0.1 mM, respectively. In these conditions no degradation was observed for RY176. As seen in Figure III. 1.3 the optimum temperature for RB5, RY15 and RB115 decolourization was 35 °C attaining a maximum decolourization of 70, 74 and 76 %, respectively. However, the optimum temperature for RR239 was 40 °C with 56 % of maximum decolourization. Within the optimal values of temperature, the lowest temperature was selected as the optimum temperature since this leads to lower energy costs. No improvement in dye degradation was observed at temperatures above 40 °C, except for RR180 where a low degradation of 9.7 % was detected at 50 °C. At lower temperature (20 °C) no decolourization was observed, except for RB5 (36 %).

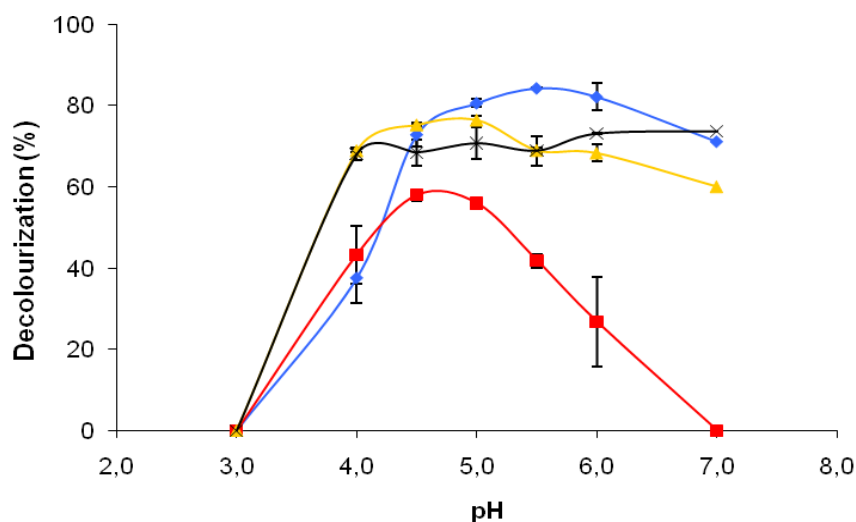


**Figure III. 1.3** – Effect of temperature on the decolourization of the reactive dyes: Blue 114 (♦), Black 5 (x), Red 239 (■), Red 180 (\*), Yellow 15 (▲) by laccase mediator system.

The results show that the decolourization of reactive dyes by LMS is very sensitive to the temperature depending on the kind of dye. According to technical literature from DeniLite, the best temperature for the decolourization of indigo in denim process of bleaching is 60-70 °C. Zhang et al. (2006) show that the optimum temperature for decolourization of Acid Green 27, Acid Violet 7 and Indigo Carmine with laccase and ABTS was 70 °C. In all the assays carried out in this study the optimum temperature was 35-40 °C. Temperatures above 50 °C were not studied since results shown that the increase from 40 °C to 50 °C promoted a marginal increase in dye decolourization and also due the high energetic costs to textile industry. All further decolourization studies were carried out at the optimum temperature of 40 °C.

### III. 1.4.3 Effect of pH on textile dye degradation

The effect of pH was studied at pH values 3.0, 4.0, 5.0, 6.0 and 7.0. The temperature was fixed at 40 °C and the ABTS concentration was fixed in 0.1 mM. Figure III. 1.4 shows the variations in textile decolourization at different pH values. RR180 and RY176 were not decolourized under these conditions. The results indicate that a pH increase from 3.0 to 5.0 enhanced the decolourization of RB5, RB114 and RY15. As can be observed, the decolourization attained a maximum at pH 5.0 for RB5 (71 %), RB114 (84 %) and RY15 (77 %). Dye decolourization was almost constant over the pH range 5.5 to 7.0. Optimum pH for RR239 was shown to be 4.5 (colour reduction 58 %) with a rapid decrease in decolourization for pH above 5.0.



**Figure III. 1.4** – Effect of pH on the decolourization of the reactive dyes: Blue 114 (♦), Black 5 (×), Red 239 (■), Yellow 15 (▲) by laccase mediator system.

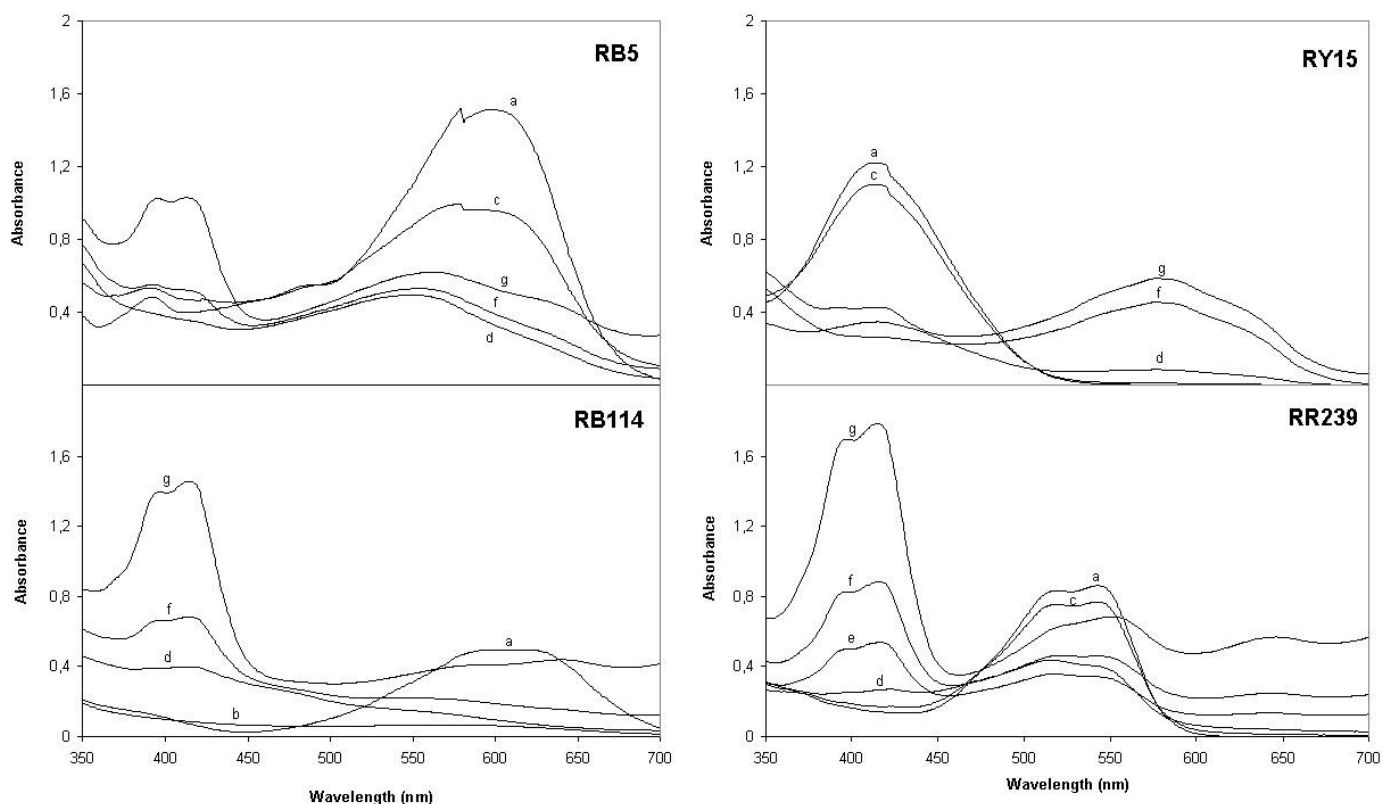
At pH 3.0 (2 pH units below the optimum) no decolourization was observed. At 2 units above the optimum pH (pH 7.0), RR239 dye showed no decolourization, dyes RY15 and RB114 showed a slight reduction in the decolourization and RB5 dye did not show any reduction in decolourization. These results suggest that acidic pH values may influence the stability of the enzyme causing denaturation. According to Tavares et al. (2006) laccase lost stability at pH of 3.0, while for pH 5.0 no loss of enzyme activity was observed.

Based on these results, pH 4.5 and 5.0 were used for subsequent decolourization assays for RR239 and for RB5, RB114 and RY15, respectively.

### III. 1.4.4 Effect of mediator concentration on textile dye degradation

The influence of mediator concentrations (0.001-0.5 mM) on the decolourization of RB5, RR239, RB114 and RY15 was monitored over the visible spectrum (350-700 nm). For RR180

and RY176 no degradation was observed. The absorption spectra in Figure III. 1.5 clearly show that the decolourization of all dyes was very dependent on ABTS concentration.



**Figure III. 1.5** – Visible absorption spectrum of RB5, RY15, RB114 and RR239 decolourization by laccase mediator system at different ABTS concentrations: (a) initial dye solution; (b) 0.001 mM; (c) 0.01 mM; (d) 0.075 mM; (e) 0.15 mM; (f) 0.2mM; (g) 0.3 mM.

The decrease in the peak of maximum absorbance corresponds to degradation of the respective dye. It was observed that all spectra (except for RY15) show a new peak that emerged near 420 nm when high ABTS concentrations were employed (above 0.2 mM). This peak corresponds to the stable dark green cationic radical formed by the oxidation of the ABTS by laccase,  $ABTS^{+\cdot}$ . In these situations a lower or loss of dye degradation was observed, while for the other ABTS concentrations, the dark green colour of solution disappears during the reaction, as it is possible to observe from Figure III. 1.6 which presents as example the reactive blue 114 degradation.



**Figure III. 1.6** – Reactive blue 114 solutions after treatment with increasing ABTS concentrations (from left to the right).

The best absorbance spectrum was obtained for RB114 in the presence of ABTS 0.001 mM where a very low absorbance was detected (Figure III. 1.5 (RB114 - b)) throughout the spectrum, which means a decolourization of 87 % relative to peak weight or 73 % relative to area, while for the other dyes this concentration did not promote any decolourization (Table III. 1.3). For RY15 a change in the spectrum was observed. An increase in the intensity of the peak at 570 nm appears at the end of reaction. This peak corresponds to light grey colour formed during the reaction, probably due to coupling between the reaction products or polymerization (Zille et al., 2005).

Most research studies related to dye degradation present results as the percentage of absorbance reduction at the maximum wavelength of the dye. In this work, a comparison between dye decolourization by absorbance reduction at the maximum absorbance wavelength and total colour removal based on the overall spectrum is presented. The results are shown in Table III. 1.3. The decolourization based on the whole spectrum range (area under the curve) was less efficient when compared with the decolourization calculated as the absorbance reduction at the maximum wavelength (peak). Efficiency results from the application of the first method (peak) are between 9 and 14% higher than those obtained by the second method (area). These results are expected since the decolourization of RB5, RB114 and RY15 was never completed and solutions of pale purple (RB5, RB114) and light grey (RY15) were obtained.

At high ABTS concentration (0.5 mM) decolourization did not occur for all dyes tested (Table III. 1.3), except for RB5 (assuming dye degradation at their maximum wavelength). These results indicate that this concentration probably inhibits enzyme activity.

The optimum ABTS concentration for reactive dye decolourization by LMS was 0.1 mM (Table III. 1.3) with colour reductions of 73, 59 and 76 % for RB5, RR239 and RY15, respectively. A very interesting result was obtained for RB114: no residual pale purple colour was observed with 0.001 mM ABTS (Figure III. 1.7) and decolourization was much faster; the decolourization was completed in approximately 30 min..



**Figure III. 1.7** – Initial and treated solutions of reactive blue 114 with 0.001 mM ABTS.



**Table III. 1.3** - Comparison between dye decolourization (%) based on the absorbance peak at maximum wavelength and on the area integration over all dye spectrum range.

ABTS (mM)	RB5		RR239		RY15		RB114	
	Peak	Area	Peak	Area	Peak	Area	Peak	Area
0.001	ND <sup>a</sup>	ND	ND	ND	ND	ND	87 ± 1.5 <sup>b</sup>	<b>73 ± 3.7</b>
0.01	32 ± 2.9	22 ± 8.5	14 ± 6.2	8.0 ± 1.9	7.0 ± 2.2	8.2 ± 3.1	<b>93 ± 1.2</b>	66 ± 1.9
0.05	72 ± 6.5	56 ± 11.9	53 ± 1.2	47 ± 0.2	51 ± 0.8	52 ± 1.4	88 ± 2.0	46 ± 3.6
0.1	<b>73 ± 2.8</b>	<b>63 ± 5.7</b>	<b>59 ± 1.8</b>	<b>50 ± 2.1</b>	76 ± 1.3	<b>65 ± 2.1</b>	80 ± 1.8	45 ± 0.2
0.15	72 ± 2.1	61 ± 4.0	59 ± 0.7	42 ± 2.0	<b>78 ± 0.8</b>	56 ± 1.5	70 ± 2.2	38 ± 2.4
0.2	67 ± 3.5	54 ± 5.3	46 ± 6.6	17 ± 10.6	75 ± 0.2	42 ± 1.3	62 ± 4.7	30 ± 4.7
0.3	61 ± 3.9	40 ± 7.4	20 ± 8.6	ND	60 ± 4.4	22 ± 7.6	5.2 ± 4.1	ND
0.5	35 ± 4.1	ND	ND	ND	ND	ND	ND	ND

<sup>a</sup>ND, not detected.<sup>b</sup>Standard deviation

These results are very promising and reveal the potential of LMS for reactive dye decolourization since it has been reported that reactive dyes are only 10 % (on average) removed by conventional treatments, such as adsorption, and also are not easily biodegradable (Pierce, 1994).

### III. 1.5 Conclusions

Among the different mediators tested, ABTS was the most effective, especially in the decolourization of reactive black 5, reactive red 239, reactive blue 114 and reactive yellow 15. The optimization of temperature, pH and mediator concentration show the great potential of commercial laccase (DeniLite II Base) in mediator treatment under the conditions used. These results suggest that LMS could be used for treating textile dyeing wastewaters, particularly as a polishing process for water recycling.

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## **Part III. 2** Application of statistical experimental methodology to optimize reactive dye decolourization by commercial laccase\*

III. 2.1 Abstract

III. 2.2 Introduction

III. 2.3 Materials and Methods

III. 2.4 Results and Discussion

III. 2.5 Conclusions

III. 2.6 References

*\*based on: Tavares, A.P.M., Cristovao, R.O., Loureiro, J.M., Boaventura, R.A.R., Macedo, E.A., 2009. Application of statistical experimental methodology to optimize reactive dye decolourization by commercial laccase. Journal of Hazardous Materials, 162, 1255-1260.*



## **III. 2 Application of statistical experimental methodology to optimize reactive dye decolourization by commercial laccase**

### **III. 2.1 Abstract**

Three-level Box–Behnken factorial design with three factors (pH, temperature and enzyme concentration) combined with response surface methodology (RSM) was applied to optimize the dye degradation of reactive red 239 (RR239), reactive yellow 15 (RY15), reactive blue 114 (RB114) and reactive black 5 (RB5) dyes by commercial laccase. Mathematical models were developed for each dye showing the effect of each factor and their interactions on colour removal. The model predicted for RY15 that a decolourization above 90 % (after 24 hours) could be obtained when the enzyme concentration, temperature and pH were set at 109.8 U/L, 39.2 °C and 6.6, respectively; whilst for RB114, RR239 and RB5 the temperature and enzyme concentration did not affect the decolourization (>90 %) in the considered range and optimum pH value was found at 5.5-7.0, 7.0-7.5 and 7.0-7.5, respectively. These predicted values were also experimentally validated. Average final values of responses were in good agreement with calculated values, thus confirming the reliability of the models of RY15, RB114, RR239 and RB5 decolourization.

### **III. 2.2 Introduction**

Reactive dyes are extensively used in textile industries to colour the cellulosic fibres. These compounds are chemically classified as azo, anthraquinone, formazan, phthalocyanine, oxazine and basic (Husain, 2006; Wesenberg et al., 2003). The dyes are first adsorbed on cellulose and then react with the fibres. However, 10-50 % (corresponding to a degree of fixation between 50-90 %) of the initial dye load will be present in the dye bath effluent giving a highly coloured effluent causing serious types of problems in the environment (Al-Degs et al., 2000).

A number of references related to the applicability of chemical and physical methods such as precipitation, adsorption, filtration, oxidative process, etc. (Slokar and Le Marechal, 1998; Vandevivere et al., 1998) for removing reactive dyes is available. Recent studies have shown that fungi or their enzymes are able to decolourize and detoxify industrial dyes (Amaral et al., 2004; Cristóvão et al., 2008; Romero et al., 2006). However, enzymatic treatments are not still commonly used in the textile industries.

Enzyme methods applied in dye degradation have low energy costs, are easy to control and have low impact on ecosystems. Laccase has been studied in the oxidation of textile dyes. Laccase (benzendiol:oxygen oxidoreductase, EC 1.10.3.2) belongs to the group of oxidative enzymes that catalyse the oxidation of phenolic compounds, polyphenols, and aromatic amines

(Thurston, 1994). Studies have shown that the range of substrate specificity of laccases can be extended to non-phenolic substrates by addition of redox mediators (Tavares et al., 2008) such as 2,2-azino-bis(3-ethylbenzothiazoline-6-sulfonate) (ABTS) (Wong and Yu, 1999), 1-hydroxybenzotriazole (HBT) (Murugesan et al., 2007), polioxometalates (Gamelas et al., 2005; Tavares et al., 2004) and violuric acid (Soares et al., 2002).

The application of experimental design and response surface methodology (RSM) in textile effluent treatment process can result in improved decolourization, reduced process variability, time and overall costs. Additionally the factors that influence the experiments are identified, optimized and possible synergic or antagonistic interactions that may exist between factors can be evaluated (Box et al., 1978). However, only a few recent studies aiming the optimization of textile dye decolourization by enzymatic catalysis are available (Murugesan et al., 2007). The accuracy of the models generated is evaluated by the coefficient of determination  $R^2$ . Response surface methodology is a multivariate technique that mathematically fits the experimental domain studied in the theoretical design through a response function. RSM has been extensively studied on biotechnology namely optimization of medium composition (Tavares et al., 2005; Weuster-Botz, 2000), fermentations (Medeiros et al., 2000; Tavares et al., 2006) and food process (Yann et al., 2005), etc. However, a few reports are presented for dye degradation optimization by enzymatic catalysis with RSM. The most common and efficient design used in response surface modelling is Box–Behnken design. It has three levels per factor, but avoids the corners of the space, and fills in the combinations of centre and extreme levels in which the optimal conditions for an experiment are found (Box and Behnken, 1960; Hanrahan and Lu, 2006).

In this study a three-level Box–Behnken full factorial design was employed with RSM to maximize the decolourization of four reactive textile dyes, reactive blue 114 (B114), reactive yellow 15 (RY15), reactive red 239 (RR239) and reactive black 5 (RB5) by enzymatic catalysis with a commercial laccase.

## III. 2.3 Materials and Methods

### III. 2.3.1 Chemicals and enzyme

Textile Dyes: Reactive yellow 15 (Remazol Yellow GR), reactive red 239 (Remazol Brilliant Red 3BS), reactive blue 114 (Levafix Brilliant Blue E-BRA) and reactive black 5 (Remazol Black B) were kindly provided by DyStar (Porto, Portugal).

Enzyme: Commercial laccase formulation (DeniLite II S; 120 U/g and DeniLite II Base; 800 U/g) from genetically modified *Aspergillus* was kindly provided by Novozymes. These formulations are used for indigo dye decolourization in denim finishing operations and include a buffer (both) and an enzyme mediator (DeniLite II S).



### III. 2.3.2 Factorial design

A 3<sup>3</sup> Box–Behnken full factorial design, including three replicates at central point, was carried out in order to study the factors (pH, temperature, enzyme concentration) that influence the decolourization by commercial laccase (Tables III. 2.1 and III. 2.2). The temperature and pH factors were chosen because it is well known that they are the factors affecting more the reaction. The enzyme concentration factor was chosen because the reactions of dyes degradation are unknown and because of the unknown composition of the commercial laccase formulation (DeniLite II S) that, besides the enzyme, includes a buffer, an enzyme mediator and surfactants.

This design permits to establish both linear and quadratic models, determining their accuracies by comparing lacks of fit of model predictions to experimental points with experimental error estimated from replicates at the central point. The accuracy and general ability of the polynomial model was evaluated by the coefficient of determination  $R^2$ . Tables III. 2.1 and III. 2.2 give the factors, their values, and the experimental design, respectively. The experimental Box–Behnken design, analysis of variance (ANOVA) and 3D response surface were carried out using the software Statistical v.5.1 (Statsoft Inc.). Equation (III. 2.1) describes the regression model of the present system, which includes the interaction terms:

$$\begin{aligned} \hat{Y} = & \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_3 + \beta_{12} x_1 x_2 + \beta_{13} x_1 x_3 + \beta_{23} x_2 x_3 \\ & + \beta_{11} x_1^2 + \beta_{22} x_2^2 + \beta_{33} x_3^2 \end{aligned} \quad (\text{III. 2.1})$$

where  $\hat{Y}$  is the predicted response, *i.e.* the colour removal;  $x_1$ ,  $x_2$  and  $x_3$  are the coded levels of the independent factors temperature, pH and enzyme concentration. The regression coefficients are:  $\beta_0$  the intercept term;  $\beta_1$ ,  $\beta_2$  and  $\beta_3$  the coefficients for linear effects;  $\beta_{12}$ ,  $\beta_{13}$ ,  $\beta_{23}$  the coefficients for interaction effects and  $\beta_{11}$ ,  $\beta_{22}$ ,  $\beta_{33}$  the coefficients for quadratic effects. The model evaluates the effect of each independent factor on the response.

### III. 2.3.3 Dye decolourization experiments

To study the decolourization of the four textile dyes, solutions with concentration of 50 mg/L of each dye were incubated in 25 mL Erlenmeyer flasks under stirring during one day. Dye degradation conditions are presented in Table III. 2.1 according to the experimental design (Table III. 2.2): laccase concentrations (192, 96 and 48 U/L), temperature (25, 35 and 45 °C) and pH (3.0, 5.0 and 7.0). The pH values of dye solutions were established by preparation of the buffers: 50 mM of citrate/di-sodium hydrogen phosphate for pH 3.0; 50 mM of di-sodium hydrogen phosphate for pH 5.0 and pH 7.0.

**Table III. 2.1** – Factor levels for a 3<sup>3</sup> Box–Behnken factorial design

Coded factor	Factor	Coded level		
		+1	0	-1
x <sub>1</sub>	Temperature (°C)	45	35	25
x <sub>2</sub>	pH	7.0	5.0	3.0
x <sub>3</sub>	Enzyme (U/L)	192	96	48

### III. 2.3.4 Determination of dye degradation

Dye decolourization by laccase was determined by monitoring the decrease in the absorbance peak at the maximum wavelength (peak) for each dye: reactive yellow 15 (416 nm), reactive red 239 (542 nm), reactive black 5 (579 nm) and reactive blue 114 (593 nm) or calculating (by integration of absorbance between 350 to 750 nm) the total area (area) under the plot. The first approach considers that absorbance reduction at maximum wavelength is totally due to dye oxidation, not taking into account the dye fraction eventually converted to other compounds. The second one takes into account the conversion of the dye molecules to other compounds absorbing at different wavelengths and then the ratio of the area under the visible spectrum is always equal or lower than the ratio of the absorbances at the peak. UV-visible spectrophotometer (Thermo, model UV1) was used in all experiments. Decolourization is reported as: % decolourization =  $(A_i - A_f)/A_i \times 100$ , where  $A_i$  is the initial absorbance or total area from the initial spectrum and  $A_f$  is the final absorbance or total area from the final spectrum.

## III. 2.4 Results and discussion

In this study a commercial laccase formulation containing a specific mediator (DeniLite II S) and pure laccase (DeniLite II Base) was used for degradation of RB114, RB5, RR239 and RY15. Preliminary results had shown that pure laccase did not decolourize the four reactive dyes studied (data not shown), indicating that the presence of mediator is required. Similarly to this study, reports from literature show that laccase alone does not decolourize some types of textile dyes (Kandelbauer et al., 2004; Rodríguez et al., 1999). Thus the further experiments for the experimental design were carried out with DeniLite II S.

### III. 2.4.1 Experimental design

In order to optimize the dye degradation, Box–Behnken full factorial design with three factors (enzyme concentration, pH and temperature) was chosen. The levels of the factors and the results from the 29 experiments for each dye are presented in Tables III. 2.1 and III. 2.2, respectively.

Using the experimental data, the second order polynomial model was fitted to decolourization results (peak) of RR239, RY15, RB114 and RB5 and obtained in terms of coded factors:

$$\hat{Y}\hat{y} \text{ (RY15)} = 58.66 + 4.53x_1 + 40.98x_2 - 0.491x_3 + 1.59x_1^2 + 12.932x_2^2 + 2.59x_3^2 - 1.48x_1x_2 + 1.509x_1x_3 - 2.29x_2x_3 \quad \text{(III. 2.2)}$$

$$\hat{Y}\hat{y} \text{ (RB114)} = 58.76 + 1.02x_1 + 45.82x_2 - 2.62x_3 - 0.312x_1^2 + 19.35x_2^2 - 0.131x_3^2 + 0.381x_1x_2 + 0.402x_1x_3 - 1.71x_2x_3 \quad \text{(III. 2.3)}$$

$$\hat{Y}\hat{y} \text{ (RR239)} = 31.7 - 0.218x_1 + 47.35x_2 - 0.442x_3 - 0.095x_1^2 - 23.45x_2^2 - 0.048x_3^2 - 0.317x_1x_2 + 0.308x_1x_3 - 0.300x_2x_3 \quad \text{(III. 2.4)}$$

$$\hat{Y}\hat{y} \text{ (RB5)} = 74.62 + 3.24x_1 + 13.96x_2 + 0.232x_3 + 1.161x_1^2 + 0.119x_2^2 + 1.75x_3^2 - 5.49x_1x_2 - 4.21x_1x_3 - 4.18x_2x_3 \quad \text{(III. 2.5)}$$

The dye decolourization results predicted by the models presented above, at each experimental point, are presented in Table III. 2.2.

**Table III. 2.2** – Comparison between experimental data and predicted values for RB114, RY15, RR239 and RB5 decolourization by commercial laccase.

Runs	Factors			Dye degradation (%)							
	$x_1$ (°C)	$x_2$	$x_3$ (U/L)	RB114		RY15		RR239		RB5	
				Actual Value	Predicted Value	Actual Value	Predicted Value	Actual Value	Predicted Value	Actual Value	Predicted Value
1	25	3.0	48	ND*	1.0	3.7	ND	ND	0.4	11.5	41.3
2	25	3.0	96	ND	ND	5.8	5.2	ND	ND	66.1	50.5
3	25	3.0	192	0.4	ND	ND	0.4	ND	ND	63.1	58.5
4	25	5.0	48	87.3	86.9	63.7	70.4	2.0	1.5	78.6	65.2
5	25	5.0	96	85.8	84.6	76.0	74.2	ND	0.9	74.9	71.6
6	25	5.0	192	75.8	80.8	62.3	66.4	ND	ND	69.4	74.0
7	25	7.0	48	94.4	95.3	88.7	89.3	95.8	96.4	90.6	88.6
8	25	7.0	96	92.4	91.9	94.3	91.6	97.3	95.6	89.1	92.2
9	25	7.0	192	88.4	85.8	83.6	80.7	93.5	94.3	87.8	89.1
10	35	3.0	48	ND	0.6	5.2	8.0	ND	ND	65.3	56.6
11	35	3.0	96	ND	ND	10.7	14.4	ND	ND	65.1	63.0
12	35	3.0	192	0.8	ND	15.9	11.6	ND	ND	64.3	65.4
13	35	5.0	48	89.5	86.9	79.3	77.2	1.8	0.8	81.0	74.9
14	35	5.0	96	84.7	84.9	83.5	82.0	ND	0.4	76.0	78.6
15	35	5.0	192	79.0	81.6	71.9	76.2	ND	ND	70.2	75.4
16	35	7.0	48	95.2	95.7	95.1	94.6	94.7	95.3	91.0	92.8
17	35	7.0	96	91.7	92.5	94.0	97.9	95.1	94.7	89.6	93.7
18	35	7.0	192	87.9	87.0	88.5	89.0	93.7	93.9	86.0	84.9
19	45	3.0	48	ND	1.5	ND	8.8	ND	ND	69.8	67.2
20	45	3.0	96	ND	0.9	12.2	16.2	ND	ND	69.3	70.8
21	45	3.0	192	ND	0.5	16.3	15.4	ND	0.3	66.4	67.6
22	45	5.0	48	90.5	88.1	78.7	76.5	1.2	0.4	81.8	80.1
23	45	5.0	96	88.4	86.4	83.3	82.3	ND	0.3	74.8	80.9
24	45	5.0	192	83.9	83.7	78.2	78.5	ND	0.2	69.3	72.1
25	45	7.0	48	96.3	97.3	92.6	92.4	94.0	94.7	89.6	92.5
26	45	7.0	96	93.2	94.4	94.0	96.7	94.4	94.3	90.2	90.5
27	45	7.0	192	89.9	89.5	91.2	89.8	94.4	93.8	86.7	76.2
28	35	5.0	96	81.3	84.9	85.1	82.0	ND	0.4	76.7	78.6
29	35	5.0	96	87.4	84.9	85.5	82.0	ND	0.4	77.3	78.6

\*ND, not detected

The statistical significance of the polynomial model for the experimental responses (Table III. 2.2) was evaluated by analysis of variance (ANOVA). According to the ANOVA results (Table III. 2.3a and Table III. 2.3b), the models present high correlation coefficients ( $R^2$ ): 0.99363, 0.99983 and 0.99804 for the degradation of RY15, RR239 and RB114, respectively, and a lower value for the RB5 dye: 0.73924. These results indicate that the accuracy of the polynomial models was good.

The significance of the estimated effects was evaluated by  $F$  and  $p$  values. The  $F$  value is the ratio between the variance of the group means and the mean of the within group variances. If the null hypothesis is true, the  $F$  value is close to 1.0 most of the time. A large  $F$  ratio means that the variation among group means is more than expected and the null hypothesis is wrong (the data are not sampled from populations with the same mean). The  $p$  value is the estimated probability of rejecting the null hypothesis of a study question when that hypothesis is true. If the  $p$  value is less than the chosen significance level then the null hypothesis is rejected. Then, the regression coefficients and the interaction between each independent factor can be considered statistically significant for  $p$ -values below 0.05, with 95 % of confidence interval. For RY15, the regression coefficients of all the linear and quadratic terms were significant, except for  $x_3$  and for the interactions  $x_1x_2$  and  $x_1x_3$ . RB114 presented linear and quadratic coefficients of pH, linear coefficient of enzyme and the interaction  $x_2x_3$  as significant coefficients. For RR239 the significant coefficients were only linear and quadratic terms of pH and linear term of enzyme. For RB5 only the linear term of pH was significant.

**Table III. 2.3a** – Analysis of variance (ANOVA) for the fitted quadratic polynomial models of RB114, RY15, RR239 and RRB5 decolourization.

Source	Sum of squares (SS)				$df^a$	Mean Square (MS)			
	RY15	RB114	RR239	RB5		RY15	RB114	RR239	RB5
(1) $x_1$ (L <sup>b</sup> )	363	18.5	0.84	185	1	363	18.5	0.84	185
$x_1$ (Q <sup>c</sup> )	91.9	2.58	0.24	35.8	1	91.9	2.58	0.24	35.8
(2) $x_2$ (L)	29706	37141	39651	3447	1	29706	37141	39650	3447
$x_2$ (Q)	4447	9965	14630	0.37	1	4447	9965	14630	0.37
(3) $x_3$ (L)	4.35	123	3.51	0.97	1	4.35	123	3.51	0.97
$x_3$ (Q)	171	0.44	0.06	77.9	1	171	0.44	0.06	77.9
$x_1$ L by $x_2$ L	26.5	1.74	1.20	361	1	26.5	1.74	1.20	361
$x_1$ L by $x_3$ L	28.3	2.02	1.18	221	1	28.3	2.02	1.18	221
$x_2$ L by $x_3$ L	65.1	36.5	1.12	217	1	65.1	36.5	1.12	217
Error	233	95.3	9.21	1738	19	12.3	5.02	0.48	91.5
Total SS	36589	48632	55467	6663	28				

$df^a$ : degrees of freedom; L<sup>b</sup>: linear; Q<sup>c</sup>: quadratic

RY15:  $R^2 = 0.99363$ ; adj  $R^2 = 0.99061$ .

RB114:  $R^2 = 0.99804$ ; adj  $R^2 = 0.99711$ .

RR239:  $R^2 = 0.99983$ ; adj  $R^2 = 0.99976$ .

RB5:  $R^2 = 0.73924$ ; adj  $R^2 = 0.61572$

**Table III. 2.3b** – Analysis of variance (ANOVA) for the fitted quadratic polynomial models of RB114, RY15, RR239 and RRB5 decolourization (continued).

Source	<i>F-value</i>				<i>p-value</i>			
	RY15	RB114	RR239	RB5	RY15	RB114	RR239	RB5
(1) $x_1$ (L <sup>b</sup> )	29.6	3.69	1.73	2.03	0.0000	0.0697	0.2037	0.1708
$x_1$ (Q <sup>c</sup> )	7.49	0.51	0.50	0.39	0.0131	0.4818	0.4886	0.5387
(2) $x_2$ (L)	2421	7405	81842	37.7	0.0000	0.0000	0.0000	0.0000
$x_2$ (Q)	362	1986	30197	0.00	0.0000	0.0000	0.0000	0.9496
(3) $x_3$ (L)	0.35	24.6	7.25	0.01	0.5588	0.0001	0.0144	0.9191
$x_3$ (Q)	13.9	0.09	0.12	0.85	0.0014	0.7707	0.7307	0.3675
$x_1$ L by $x_2$ L	2.16	0.35	2.48	3.95	0.1584	0.5628	0.1316	0.0614
$x_1$ L by $x_3$ L	2.31	0.40	2.44	2.41	0.1452	0.5337	0.1347	0.1370
$x_2$ L by $x_3$ L	5.31	7.27	2.31	2.38	0.0327	0.0143	0.1446	0.1396
Error								
Total SS								

### III. 2.4.1.1 Response Surface Methodology

Using RSM, the effects of the independent factors (pH, temperature and enzyme concentration) and their interaction on the dyes decolourization are represented, the response can be predicted and the optimum values of decolourization can be determined. The response surface plots (Figures III. 2.1 – III. 2.4) show the decolourization of RY15, RR239, RB114 and RB5 as function of two factors, whilst the third was kept at a constant level.

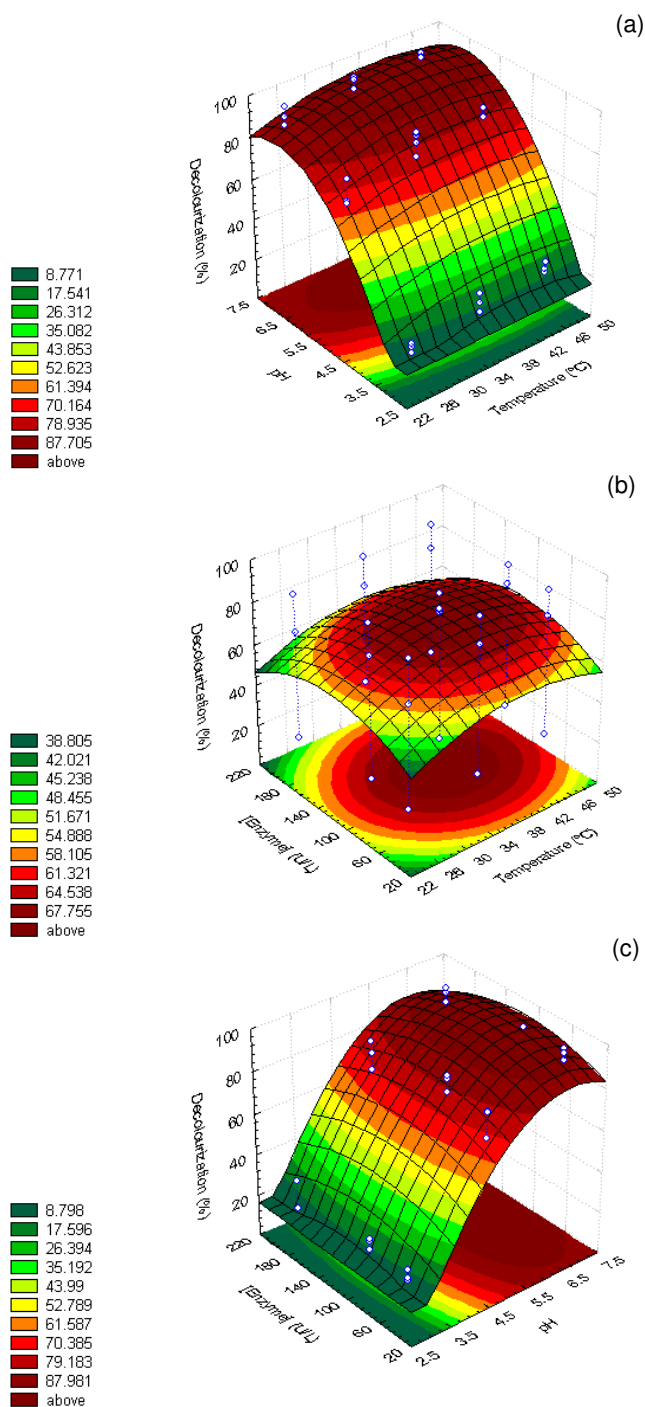
Figure III. 2.1 represents the response surface for RY15 decolourization. Surface plots show the increase on dye degradation with increasing on pH values. Plots III. 2.1a and III. 2.1c clearly show that the decolourization by commercial laccase was sensitive even to small alterations of the pH. As it can be seen from plots III. 2.1a and III. 2.1c, the temperature slightly influenced the decolourization. On the other hand the enzyme concentration did not affect the decolourization in the treated range.

The response surface plots of RB114, RR239 and RB5 degradation are presented in Figures III. 2.2 - III. 2.4, respectively. From the results it can be observed that pH was the only influential factor.

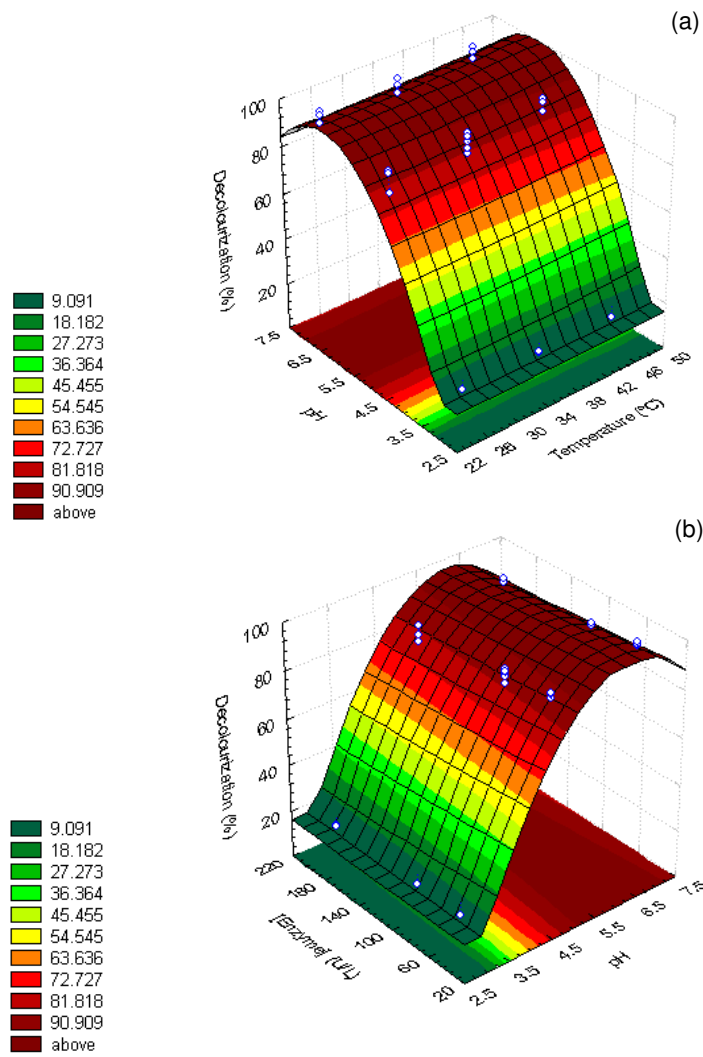
The results presented above showed that pH was the more relevant factor for the decolourization of the four dyes. At acidic conditions (pH<4.0) a little or no decolourization was observed for all dyes. Similar results were observed in other studies (Eggert et al., 1996; Nyanhongo et al., 2002) with dyes or similar substrates. These results suggest that acidic pH values may influence the stability of the enzyme causing denaturation. According to Tavares et al. (2006) laccase loses stability at pH of 3.0 whilst for pH of 5.0 no loss of enzyme activity is observed.

Literature studies show that laccase-catalyzed dye oxidation is affected by the temperature (Kim and Nicell, 2006; Nyanhongo et al., 2002). From the results presented in Figures III. 2.1 - III. 2.4 it can be concluded that the temperature did not seem to play an

important role on decolourization of RY15, RR239, RB114 and RB5 in the range 25-45 °C. Temperatures above 45 °C were not studied since previous results (data not presented) have shown that the increase from 40 °C to 50 °C did not promote an increase on dye decolourization. As temperature, the laccase concentration did not influence the dye degradation for the four dyes.

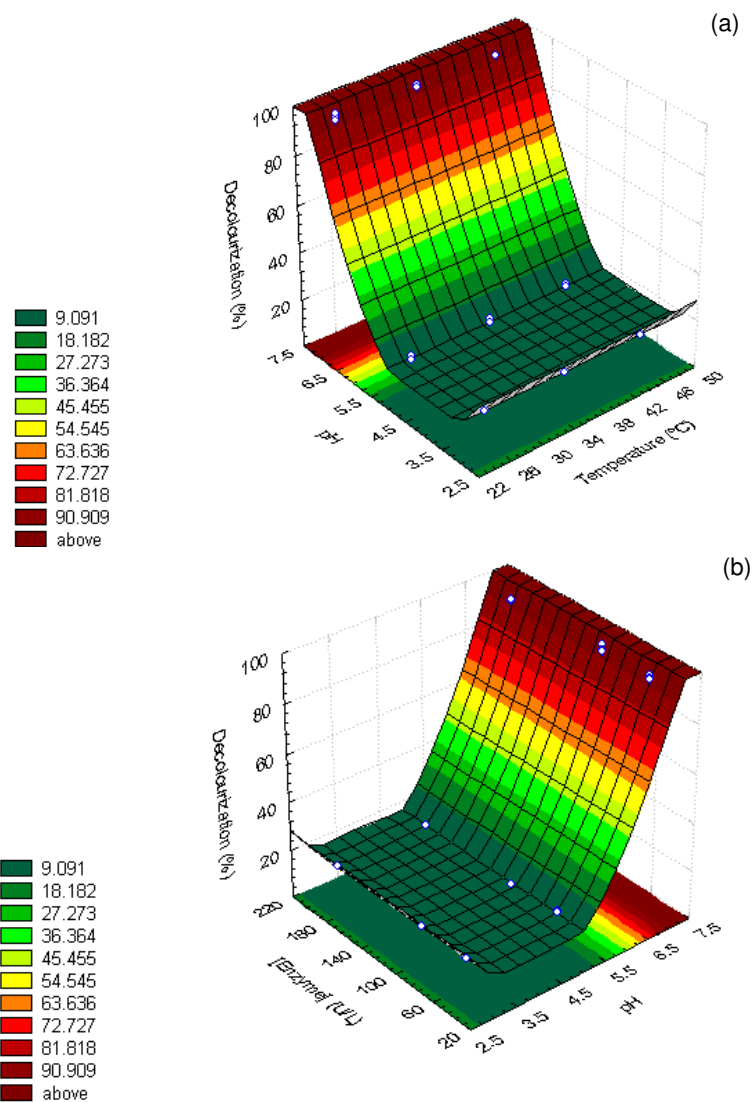


**Figure III. 2.1** – Response surface plots for decolourization of RY15 as a function of: **(a)** pH and temperature at 96 U/L; **(b)** enzyme concentration and temperature at pH 5.0; **(c)** pH and enzyme concentration at 35 °C.

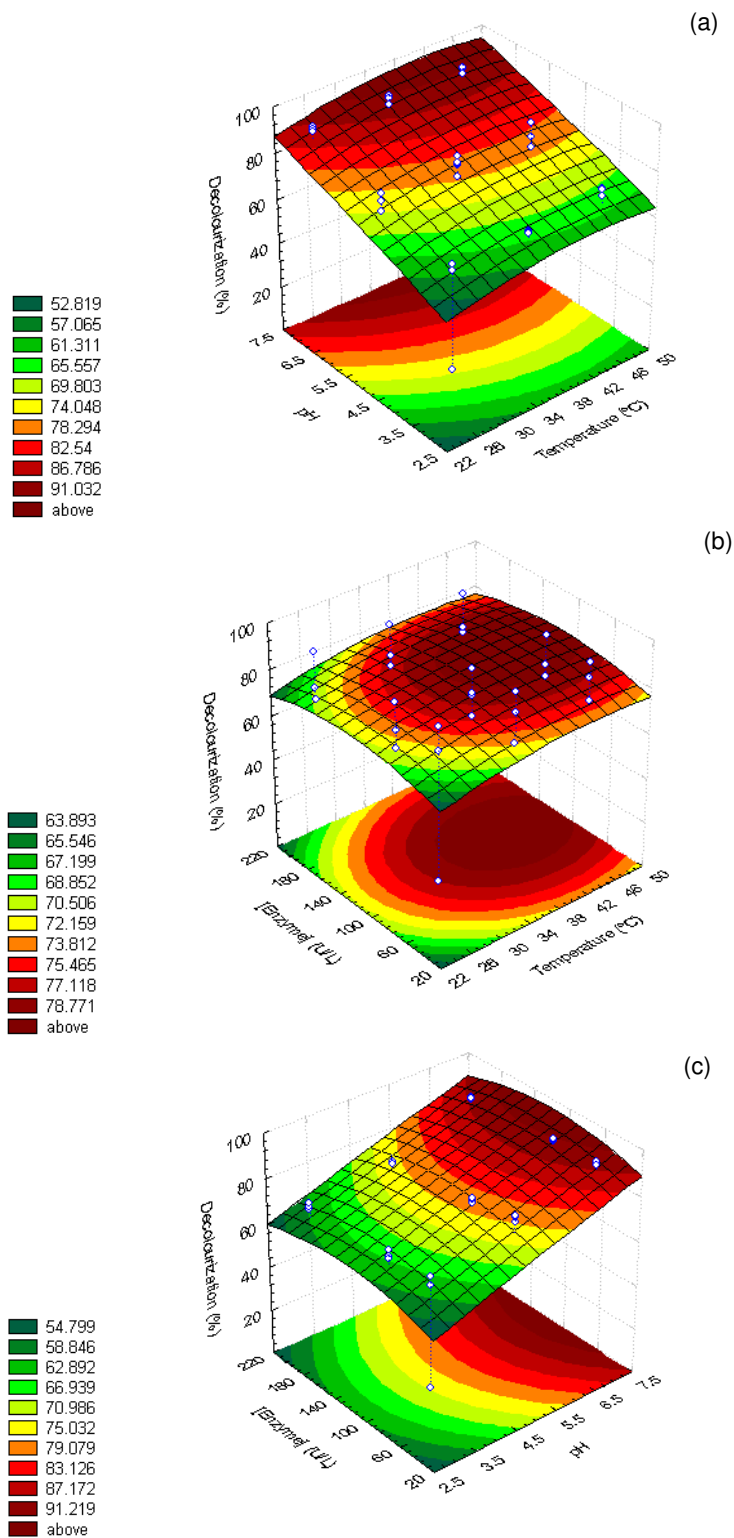


**Figure III. 2.2** – Response surface plots for decolourization of RB14 as function of: **(a)** pH and temperature at 96 U/L; **(b)** pH and enzyme concentration at 35 °C.





**Figure III. 2.3** – Response surface plots for decolourization of RR239 as function of: **(a)** pH and temperature at 96 U/L enzyme concentration; **(b)** pH and enzyme concentration at 35 °C.



**Figure III. 2.4** – Response surface plots for decolourization of RB5 as a function of: **(a)** pH and temperature at 96 U/L; **(b)** enzyme concentration and temperature at pH 5.0; **(c)** pH and enzyme concentration at 35 °C.

### III. 2.4.2 Model validation

The adequacy of the proposed model (Equation III. 2.1) for dye decolourization by commercial laccase was evaluated using the optimum conditions for each dye. For this purpose new experiments were conducted in triplicate to verify the optimum conditions. According to the models the optimum conditions for the RY15 dye degradation were: temperature 39.2 °C, enzyme concentration 109.8 U/L and pH 6.6, predicting above 90 % decolourization. For RR239, RB114 and RB5 it was not possible to calculate the optimum of temperature and enzyme concentration as these factors did not affect the response (Figures III. 2.2 - III. 2.4). In these cases, according to the response surface, it is possible to determine an optimal region for dye decolourization: pH of 5.5-7.0 for RB114 and pH of 7.0-7.5 for RR239 and RB5. At these conditions, the highest RB114, RR239 and RB5 decolourization ( $\geq 90$  %) was obtained. Under the optimal conditions, a decolourization of 96 %, 90 %, 93 % and 90 % was experimentally achieved for RR239, RB114, RY15 and RB5, respectively, which is in good agreement with the decolourization predicted by the model. For the entire range of the tested factors, the experimental results are very close to the predicted values obtained from the models.

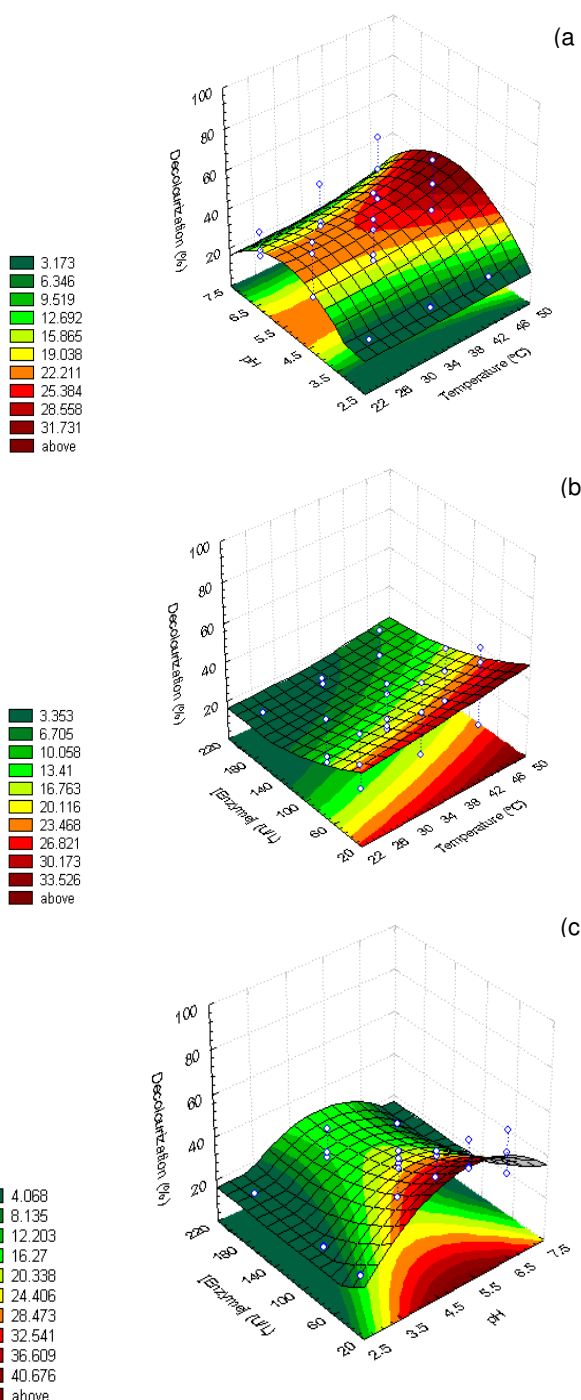
### III. 2.4.3 Decolourization at the optimum conditions

For a better performance in dye wastewater treatment, no absorbance in the visible spectrum must be detected after decolourization. Thus, the decolourization at the optimum conditions was followed by measuring the absorbance reduction over all the visible spectrum. The results presented in Table III. 2.4 show a lower decolourization based on the entire visible spectrum when compared with the absorbance reduction at the maximum wavelength, particularly for RB114 which presents a difference of 65 % in the decolourization. This result can be explained by the new peak of absorbance that emerged between 400 and 420 nm during the degradation of RB114, corresponding to a light orange colour formed probably due to the coloured intermediates. Sugano et al. (2006) showed the generation of light red-brown reaction products during the decolourization of Reactive black 5 by versatile peroxidase, which was also observed in this study. RR239 and RY15 did not show any colour change and no additional peaks of absorbance were observed in the entire visible spectrum (data not shown).

**Table III. 2.4** – Comparison between dye decolourization (%) based on the absorbance reduction at maximum wavelength and on the area under all dye spectrum range.

Dye	Decolourization (%)	
	Peak	Area
RR239	96	70
RB114	90	25
RY15	93	84
RB5	90	76

The application of RSM to RB114 degradation results based on the area under all dye spectrum range are presented in Figure III. 2.5. Although the area based decolourization is lower when compared to the peak absorbance reduction, which is the classical method to calculate decolourization, pH continues to be the factor that affects more and presents practically the same optimal region (pH 5.0-6.5). However, in this case the temperature and enzyme concentration also present a small influence in RB114 decolourization.



**Figure III. 2.5** – Response surface plots for decolourization of RB114 based on the area under all dye spectrum range as function of: (a) pH and temperature at 96 U/L enzyme concentration; (b) enzyme concentration and temperature at pH 5.0; (c) pH and enzyme concentration at 35 °C.

### III. 2.5 Conclusions

Box–Behnken statistical experimental design and response surface methodology are important tools to optimize the conditions for textile dye wastewater treatment as well as to reduce the number of experiments and provide useful information about the effect of the factors and the possible interactions. The decolourization of RY15, RR239, RB114 and RB5 by enzymatic catalysis using commercial laccase was optimized leading to dye degradation above 90 %. pH proved to be the principal factor that affects the decolourization of the four reactive dyes whilst temperature and enzyme concentration presented a low or none effect on dye degradation. The decolourization based on all the visible spectrum showed to be lower when compared with the degradation at the maximum wavelength for all dyes studied. In the case of RB114 this difference is high (65 %) due to the formation of another peak, corresponding to a formed light orange colour during the degradation.

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## **Part III. 3** Optimization of reactive dye degradation by laccase using box-behnken design\*

III. 3.1 Abstract

III. 3.2 Introduction

III. 3.3 Materials and Methods

III. 3.4 Results and Discussion

III. 3.5 Conclusions

III. 3.6 References

*\*based on: Cristóvão, R.O., Tavares, A.P.M., Loureiro, J.M., Boaventura, R.A.R., Macedo, E.A., 2008. Optimisation of Reactive Dye Degradation by Laccase Using Box-Behnken Design. Environmental Technology, 29, 1357-1364*





### **III. 3 Optimization of reactive dye degradation by laccase using box-behnken design**

#### **III. 3.1 Abstract**

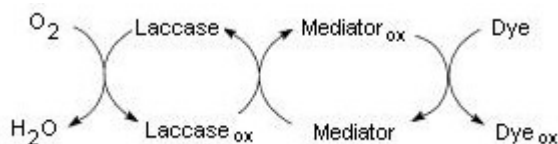
A three-level Box–Behnken factorial design with three factors and the response surface methodology were used to optimize the colour removal of the reactive textile dye, Colour Index (C.I.) reactive red 180, by commercial laccase. A mathematical model was developed to study the effect of temperature, pH, enzyme concentration and their interactions on the decolourization. Enzyme concentration and pH as well as their interaction were the principal factors that affected the decolourization. The dye degradation was independent of temperature. The model estimated that the highest decolourization (> 92 %) was obtained for 27 °C, pH 7.5 and 85 U/L. This predicted value was experimentally validated, obtaining dye colour removal (540 nm) of  $93 \pm 1.5$  %.

#### **III. 3.2 Introduction**

Reactive dyes are the principal class of dyes employed in textile industries because they are used to dye cotton; half of the world's fibre consumption comprises cotton and dyeing 1 kg of cotton requires approximately 40 g reactive dye (Allègre et al., 2006). However, around 30 % of the applied reactive dyes are discarded and the conventional wastewater treatments are not efficient to completely remove the residual colour (Correia et al., 1994). Reactive dyes present in effluents from dyeing processes can be detected in water by the human eye down to concentrations of 0.005 mg/L (Vandevivere et al., 1998). Many conventional treatments including adsorption, chemical precipitation, ozonation and flocculation have been reported for decolourization of effluents; however, in many cases they are inefficient and have a high cost. Conversely, biological processes such as biodegradation are an efficient alternative (Amaral et al., 2004; Casas et al., 2007; Kapdan et al., 2002). However, few studies involving enzymatic degradation of reactive dyes with commercial laccase are available (Soares et al., 2002a). The reactive dye RR180 is widely used for textile dyeing processes and it is resistant to biodegradation (Reyes et al., 1999; Rodríguez et al., 1999) and conventional treatments of degradation.

Laccase is a copper-containing oxidoreductase (EC 1.10.3.2, *p*-diphenol:dioxygen oxidoreductase), which catalyzes the oxidation of phenolic compounds with reduction of oxygen to water (Thurston, 1994). However, the substrate range can be extended to non-phenolic compounds by the addition of a mediator (Bourbonnais and Paice, 1990; Gamelas et al., 2005; Tavares et al., 2004). Catalytic degradation of dyes with the laccase-mediator system (LMS) is

an environmentally friendly technology which constitutes a promising alternative to conventional decolourization. The mechanism of catalysis by LMS is presented in a simplified view in Figure III. 3.1. The mediator is a diffusible electron carrier between the dye and the enzyme (Bourbonnais et al., 1998).



**Figure III. 3.1** - Representation of dye degradation by laccase mediator system.

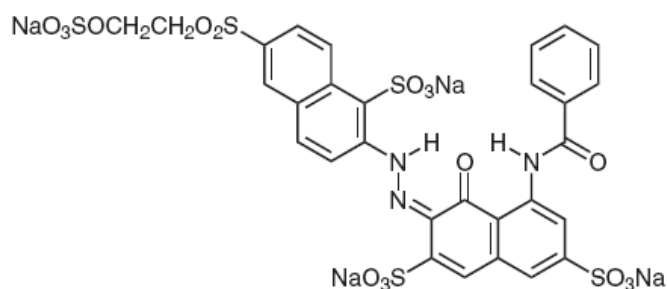
The experimental design and Response Surface Methodology (RSM) are useful statistical techniques that can be used in decolourization processes to identify and optimize the relevant factors that influence colour removal, and also and it can be used to evaluate the relative significance of several of these factors and their interactions. It is an experimental strategy to obtain the optimum conditions for a multivariable system. Although this methodology has been widely applied in other sciences, e.g. in enzyme production, and in culture medium optimization, a few reports are available on the optimization of reactive dyes (Hanrahan and Lu, 2006; Myers and Montgomery, 2002). A class of three level complete factorial designs for the estimation of the parameters in a second-order model was developed by Box and Behnken (Box and Behnken, 1960).

In this study the RSM using the full Box-Behnken design of experiments was applied to optimize the decolourization conditions of C.I. reactive red 180 (RR180) by commercial laccase. A synthetic effluent containing the reactive dye was used to obtain a constant composition in order to understand more easily the effects of the treatment.

### III. 3.3 Materials and Methods

#### III. 3.3.1 Chemicals and Enzyme

Textile dyes: C.I. Reactive red 180 (Remazol Brilliant Red F3B), a monoazo dye, was kindly provided by DyStar (Porto, Portugal) and was used for degradation experiments without any further purification. The chemical structure is presented in Figure III. 3.2. A wide variety of dyes, namely acid, reactive, disperse, vat, metal complex, mordant, direct, basic and sulphur are available. Among these, the most used in the textile industry are the reactive dyes. In this work, a reactive red dye, which is widely used on cotton and wool dyeing was chosen, as this type of dye is less degradable when compared with other dyes.



**Figure III. 3.2** - Chemical structure of C.I. reactive red 180.

**Enzyme:** A commercial laccase formulation (DeniLite II S; 120 U/g) from genetically modified *Aspergillus* was kindly provided by Novozymes. This formulation is used for indigo dye decolourization in denim finishing operations and includes a buffer and an enzyme mediator. Due to the wide application of laccase in the treatment of textile effluents and the degradation of phenolic compounds, this enzyme was used for the oxidation of the reactive red 180.

### III. 3.3.2 Box–Behnken Design of Experiments

A 3<sup>3</sup> Box–Behnken full factorial design was used to identify the factors having significant effects on RR180 decolourization by laccase. The normal practice is to test within the feasible range, so that the variation in the process does not mask the factor effect. Factors were selected and the ranges were further assigned based on our previous experience with enzymatic catalysis (Cristóvão et al., 2008; Tavares et al., 2008). Three factors, i.e., temperature, enzyme concentration and pH were chosen. The low level (–1), high level (+1) and the middle point (0) of each factor are listed in Table III. 3.1. The experimental Box–Behnken design, analysis of variance (ANOVA) and 3D response surface were carried out using the software Statistica v.5.1 (Statsoft Inc.). Equation (III. 3.1) describes the regression model of the present system, which includes the interaction terms:

$$Y = \beta_0 + \beta_1 X_1 + \beta_2 X_2 + \beta_3 X_3 + \beta_{12} X_1 X_2 + \beta_{13} X_1 X_3 + \beta_{23} X_2 X_3 + \beta_{11} X_1^2 + \beta_{22} X_2^2 + \beta_{33} X_3^2 \quad (\text{III. 3.1})$$

where  $Y$  is the predicted response, i.e. the colour removal;  $x_1$ ,  $x_2$  and  $x_3$  are the coded levels of the independent factors temperature, pH and enzyme concentration. The regression coefficients are:  $\beta_0$  - the intercept term;  $\beta_1$ ,  $\beta_2$  and  $\beta_3$  - the linear coefficients;  $\beta_{12}$ ,  $\beta_{13}$ ,  $\beta_{23}$  - the interaction coefficients and  $\beta_{11}$ ,  $\beta_{22}$ ,  $\beta_{33}$  - the quadratic coefficients. The model evaluates the effect of each independent factor on the response.

**Table III. 3.1** - Variables and experimental Box-Behnken design levels.

Factors	Parameters	Coded level		
		+1	0	-1
$x_1$	Temperature (°C)	45	35	25
$x_2$	pH	8.0	7.0	6.0
$x_3$	Enzyme concentration (U/L)	96	48	24

### III. 3.3.3 Dye Decolourization Experiments

To study the decolourization of the reactive textile dye, 50 mg/L of C.I. RR180 was incubated in a 25 mL Erlenmeyer flask under stirring for one day. Dye degradation conditions are presented in Table III. 3.1 according to the experimental design (Table III. 3.2): laccase concentrations of 24, 48 and 96 U/L, temperature of 25, 35 and 45 °C and pH of 6.0, 7.0 and 8.0. The pH values of the dye solutions were adjusted with 50 mM phosphate buffer.

### III. 3.3.4 Determination of Dye Degradation

Dye decolourization was determined by monitoring the decrease in the absorbance peak at the maximum absorbance wavelength for the C.I. reactive red 180 at 540 nm (peak) or by calculating the total area under the plot (integration of absorbance between 350 to 700 nm) (area). A UV-visible spectrophotometer (Thermo, model UV1) was used in all experiments. The percentage decolourization is calculated by  $(A_i - A_f)/A_i \times 100$ , where  $A_i$  is the initial absorbance or total area under the initial spectrum and  $A_f$  is the final absorbance or total area under the final spectrum.

## III. 3.4 Results and Discussion

The most important factors which affect the efficiency of enzymatic dye degradation, are temperature and pH of the solution and enzyme concentration. In order to study the combined effect of these factors, experiments were performed for different combinations using factorial design methodology. The effect of temperature, enzyme concentration and pH on the decolourization of RR180 by commercial laccase is shown in Table III. 3.1. From the present results, the quadratic model, including linear interactions, fitted adequately to the experimental data giving a coefficient of determination,  $F^2$ , of 0.9306. Equation (III. 3.2), which indicates the effect of factors on RR180 decolourization, is shown below, in terms of coded factors:

$$Y = 68.702 + 0.650x_1 + 10.563x_2 + 16.133x_3 + 0.527x_1^2 + 9.680x_2^2 + 6.709x_3^2 - 3.357x_1x_2 - 0.787x_1x_3 + 9.033x_2x_3 \quad (\text{III. 3.2})$$

The predicted decolourization of RR180 from the model at each experimental point is presented in Table III. 3.2 together with the experimental observed values. Additionally, a

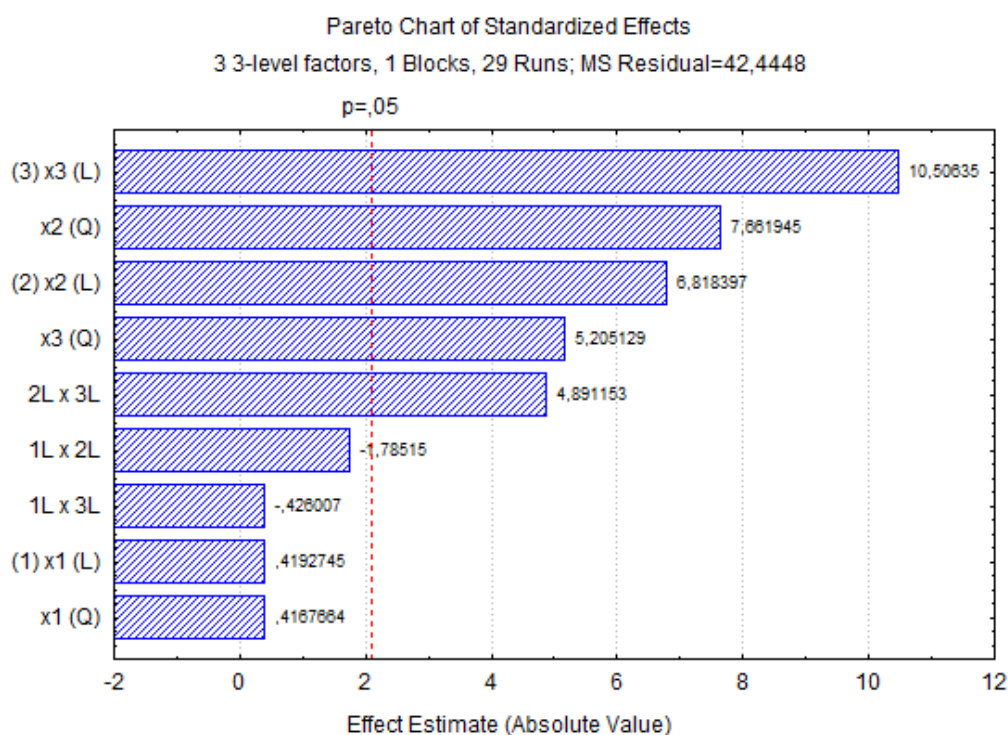
comparison between dye decolourization by absorbance reduction at the maximum wavelength and the total decolourization based on the overall spectrum is also presented.

**Table III. 3.2** - Box–Behnken design matrix and the responses of the dependent factors and predicted values.

Run	Factors			Dye degradation (%)			
	$x_1$ (°C)	$x_2$	$x_3$ (U/L)	Peak	Peak Predicted Value	Area	Area Predicted Value
1	25	6.0	24	47.4	35.0	36.4	27.6
2	25	6.0	48	44.5	53.6	34.0	40.2
3	25	6.0	96	48.7	50.7	26.1	28.1
4	25	7.0	24	48.4	59.2	39.9	46.9
5	25	7.0	48	88.9	83.9	68.4	66.0
6	25	7.0	96	94.2	93.0	71.5	66.6
7	25	8.0	24	40.9	44.7	31.2	34.7
8	25	8.0	48	85.7	75.5	65.1	60.2
9	25	8.0	96	93.7	96.7	71.2	73.5
10	35	6.0	24	42.7	40.8	34.2	32.2
11	35	6.0	48	53.0	59.0	41.0	45.3
12	35	6.0	96	60.3	55.0	33.7	34.1
13	35	7.0	24	57.9	61.7	45.6	48.4
14	35	7.0	48	86.7	85.9	67.7	67.9
15	35	7.0	96	94.3	94.0	70.8	69.5
16	35	8.0	24	44.9	43.9	37.8	33.1
17	35	8.0	48	70.8	74.1	56.8	59.0
18	35	8.0	96	93.4	94.2	71.3	73.3
19	45	6.0	24	43.4	44.6	32.4	32.1
20	45	6.0	48	59.0	62.2	43.1	45.7
21	45	6.0	96	59.0	57.2	39.9	35.5
22	45	7.0	24	70.6	62.1	47.1	45.3
23	45	7.0	48	81.7	85.7	64.0	65.3
24	45	7.0	96	91.1	92.8	64.6	67.8
25	45	8.0	24	36.7	40.9	22.7	26.9
26	45	8.0	48	75.7	70.6	58.8	53.3
27	45	8.0	96	88.5	89.7	67.8	68.5
28	35	7.0	48	83.7	85.9	66.7	67.9
29	35	7.0	48	92.5	85.9	73.3	67.9

A decrease in RR180 total decolourization (area) was observed when compared with decolourization at maximum wavelength (peak). The decolourization of RR180 causes a reduction in absorbance at the peak but the dye is not fully decolourization when considering the entire visible spectrum.

The model was found to be adequate for prediction within the range of factors chosen. The optimum operating conditions for RR180 decolourization can be predicted from the second order polynomial function. The Pareto chart displays the statistically relevant effect of each factor on the response and it is a practical mode to view the results. These are sorted from the largest to the smallest, and the effects to the right of the divisor line are significant. From Figure III. 3.3, the enzyme concentration ( $x_3$ ) and pH ( $x_2$ ) and their interaction  $x_3 \times x_2$  are shown to have an effect on RR180 decolourization whilst the temperature ( $x_1$ ) did not affect the decolourization.



**Figure III. 3.3** - Pareto chart of standardized effects for  $3^3$  Box–Behnken factorial design. (1) Temperature; (2) pH; (3) enzyme concentration.

This significant interaction between the factors allowed an optimum point (max.) for RR180 decolourization to be found on the Response Surface (Figure III. 3.4b), due to the curvature obtained. Figure III. 3.4 shows a decrease in dye degradation with the decrease in pH. This result can be explained by the conformational changes in the enzyme's three-dimensional structure promoted by low pH values, affecting the active site, and, then, the biocatalytic reactions mechanism (Figure III. 3.1). A study on laccase activity and stability showed that a loss of 50 % of the activity was observed for pH = 3.0 during the first day of incubation, attaining 80 % after 3 days, whereas for pH = 4.5 a loss of only 11 % was observed after 3 days (Tavares et al., 2006).

The significance of the estimated effects was tested by analysis of variance (ANOVA), by determination of  $F$  and  $p$  values. The  $F$  value is the ratio between the variance of the group means and the mean of the within group variances. If the null hypothesis is true, the  $F$  value is

close to 1.0 most of the time. A large  $F$  ratio means that the variation among group means is more than expected and the null hypothesis is wrong (the data are not sampled from populations with the same mean). The  $p$  value is the estimated probability of rejecting the null hypothesis of a study question when that hypothesis is true. If the  $p$  value is less than the chosen significance level then the null hypothesis is rejected.

The ANOVA (Table III. 3.3) test indicates that the model adequately describes the decolourization of RR180 by commercial laccase. The significance of each coefficient was determined through the  $p$  value test considering 95 % confidence, in which low  $p$  values ( $p < 0.05$ ) indicate a high significance of the corresponding coefficient. The effect of pH and enzyme concentration and their interaction on RR180 decolourization is significant whilst the temperature did not influence the decolourization.

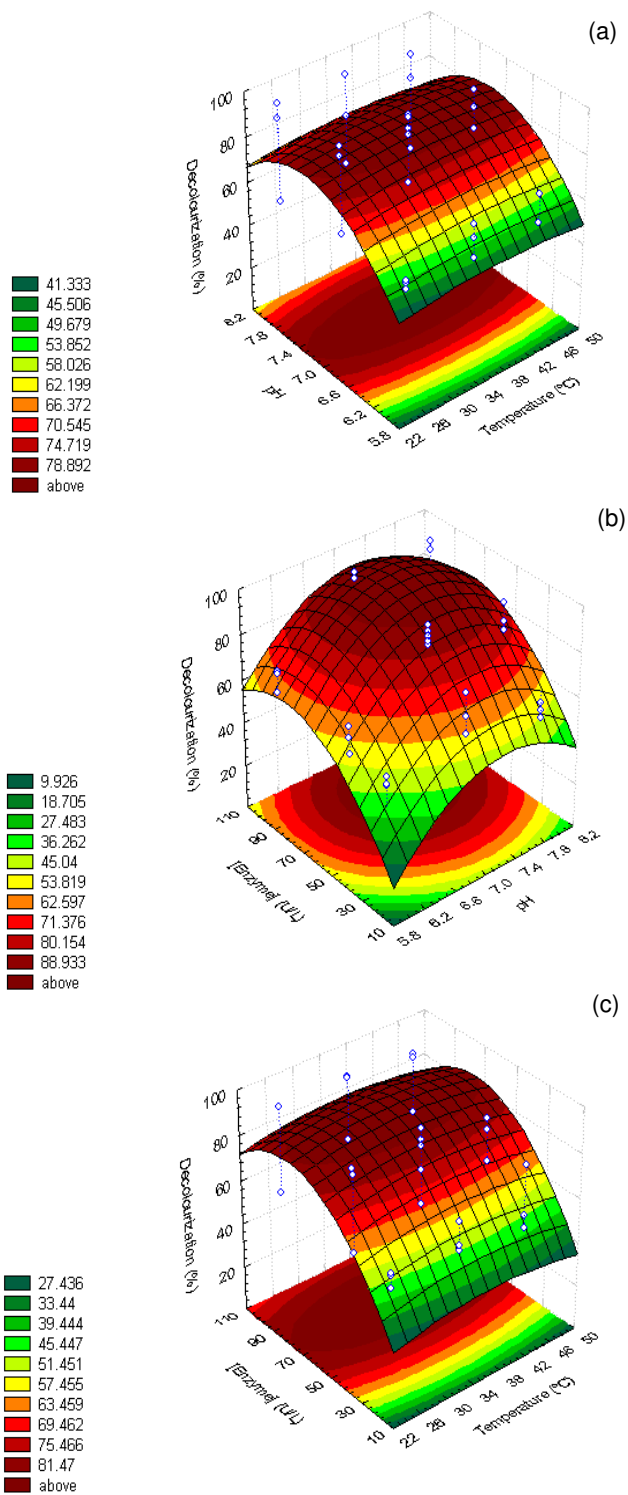
**Table III. 3.3** - Analysis of variance (ANOVA) for the fitted quadratic polynomial model for optimization of C.I. reactive red 180 decolourization by commercial laccase.

Source	Sum of squares (SS)	df <sup>a</sup>	Mean square (MS)	F-value	p-value
(1) $x_1$ (L <sup>b</sup> )	7.5	1	7.5	0.18	0.6797
$x_1$ (Q <sup>c</sup> )	7.4	1	7.4	0.17	0.6815
(2) $x_2$ (L)	1973.3	1	1973.3	46.5	0.0000
$x_2$ (Q)	2491.8	1	2491.8	58.7	0.0000
(3) $x_3$ (L)	4685.2	1	4685.2	110.4	0.0000
$x_3$ (Q)	1149.0	1	1149.0	27.1	0.0001
1L by 2L	135.3	1	135.3	3.2	0.0902
1L by 3L	7.7	1	7.7	0.2	0.6749
2L by 3L	1015.4	1	1015.4	24.0	0.0001
Error	806.5	19	42.4		
<b>Total SS</b>	<b>11618.0</b>	<b>28</b>			

df<sup>a</sup>: degree of freedom; L<sup>b</sup>: linear; Q<sup>c</sup>: quadratic  
 $R^2 = 0.9306$ ; adj  $R^2 = 0.8977$

The response surface plots, generated from the Box–Behnken design, are shown in Figure III. 3.4 a-c. The plots represent the decolourization of RR180 with changes in two independent factors (temperature, pH or enzyme concentration) while a third factor was kept constant. Figure III. 3.4a shows the response surface of interactions between pH and temperature at 55 U/L. Decolourization increases with pH up to 7.5, and then decreases. The decolourization was practically independent of temperature changes as observed in Figures III. 3.4a and III. 3.4c. Figure III. 3.4b represents the effect of changes in enzyme concentration and pH at 35 °C. It clearly shows that the optimum conditions for obtaining the maximum decolourization are within the experimental ranges tested. The decolourization increased with

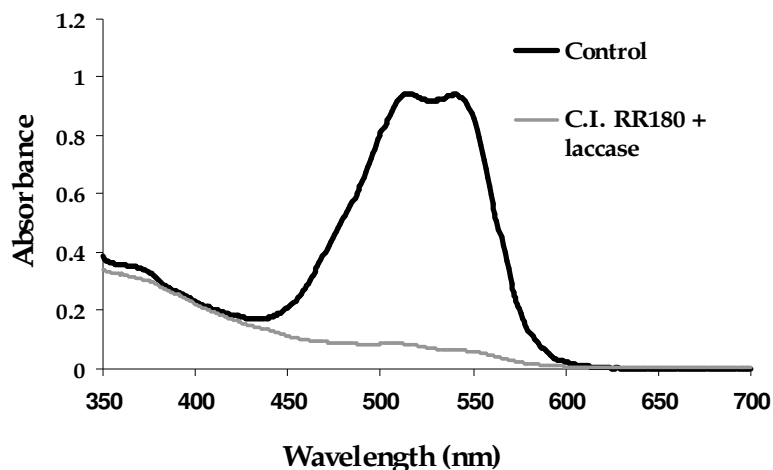
increasing pH and enzyme concentration up to approximately 7.5 and 85 U/L, respectively. Then the decolourization decreased slowly. Maximum decolourization was observed at those conditions and dye degradation above 92 % was predicted by the response surface.



**Figure III. 3.4** - Response surface plots of the C.I. reactive red 180 decolourization by commercial laccase: (a) effect of temperature ( $x_1$ ) vs. pH ( $x_2$ ) at 55.4 U/L; (b) effect of enzyme concentration ( $x_3$ ) vs. pH ( $x_2$ ) at 35 °C; (c) effect of temperature ( $x_1$ ) vs. enzyme concentration ( $x_3$ ) at pH 7.0.



The adequacy of the regression model for RR180 decolourization by laccase was checked by using the calculated optimum conditions: 27.4 °C, 85.4 U/L and pH 7.5 in triplicate experiments. Under these conditions,  $93 \pm 1.5$  % of RR180 decolourization was obtained which is in good agreement with the predicted value (above 92 %). The absorbance spectrum of RR180 before and after decolourization by commercial laccase at the optimum conditions determined by the experimental design is shown in Figure III. 3.5. The decrease in the absorbance values indicates that the decolourization of RR180 was almost complete.



**Figure III. 3.5** - Absorption spectra of RR180 before and after decolourization by commercial laccase. Optimum decolourization conditions obtained by RSM.

DeniLite II S is a commercial laccase with great potential to decolourize textile dyes; however, only a few studies regarding the use of this commercial laccase on the treatment of effluents containing dyes and especially with reactive dyes (RR180) are available. It is a formulation containing laccase, a mediator and a non-ionic surfactant used in the finishing process for indigo stained clothes (Soares et al., 2002b). In this study DeniLite II S was used for decolourization of RR180 and the obtained results prove that pH and enzyme concentration play an important role in decolourization. Recent reports have shown that a mediator is necessary for the decolourization of dyes by laccase (Camarero et al., 2005; Murugesan et al., 2007). In order to confirm these finds, some experiments were carried out with pure commercial laccase (DeniLite II Base) and no degradation of RR180 was detected (data not shown), which is in agreement with the results of other researchers reporting on RR180 decolourization by laccase and others dyes (Rodríguez et al., 1999). A mediator is necessary for dye degradation by laccase in order to complete the mechanism of electron transfer from the substrate to the enzyme (Figure III. 3.1). The mediator acts as an electron carrier, an intermediate substrate for the laccase (Riva, 2006). The overall catalytic cycle is the reduction of the oxygen molecule to a water molecule with the concomitant oxidation of the substrate. The higher capacity of laccase for oxidising the substrate in the presence of a mediator could be related to the redox potentials. For example, the mechanism of oxidation of lignin by laccase and a mediator was investigated,

and the results showed that the potential redox of laccase alone is not high enough to oxidise non-phenolic compounds (Bourbonnais et al., 1997; 1998).

### III. 3.5 Conclusions

Commercial laccase (DeniLite II S) was tested for decolourization of RR180. A 3<sup>3</sup> Box–Behnken full factorial design was found to be an efficient tool for optimization of RR180 decolourization. Enzyme concentration and pH were the factors that influenced the decolourization whilst the temperature changes did not affect the dye degradation. Validation experiments were carried out in order to check the suitability of the model. The results showed that the predicted decolourization is in agreement with the experimental value. It is clear that dye degradation by commercial laccase proved to be an alternative treatment for decolourization of RR180 (> 92 %).

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## **Part III. 4** Sequential decolourization of reactive textile dyes by laccase mediator system\*

III. 4.1 Abstract

III. 4.2 Introduction

III. 4.3 Materials and Methods

III. 4.4 Results and Discussion

III. 4.5 Conclusions

III. 4.6 References

*\*based on: Tavares, A.P.M., Cristovao, R.O., Gamelas, J.A.F., Loureiro, J.M., Boaventura, R.A.R., Macedo, E.A., 2009. Sequential decolourization of reactive textile dyes by laccase mediator system. Journal of Chemical Technology and Biotechnology, 84, 442-446.*



### **III. 4 Sequential decolourization of reactive textile dyes by laccase mediator system**

#### **III. 4.1 Abstract**

The use of enzymes has attracted much interest for the decolourization of dyes from wastewater as an alternative to conventional treatments, which have limitations. Laccase can be used to decolourize dyes and its substrate range can be extended by inclusion of mediators.

Sequential decolourization of reactive dyes was carried out by laccase mediator system using as mediators violuric acid and 1-hydroxybenzotriazole. Violuric acid resulted in a high level of decolourization on the first and second cycles for reactive blue 114 ( $\geq 95\%$ ), reactive yellow 15 and reactive red 239 ( $\geq 80\%$ ), while for reactive black 5 a slightly lower value was observed (70 %) on the second cycle. The degree of reactive blue decolourization remained at 90% after the third cycle and at about 60 % after seven cycles; with the other dyes decolourization decreased to 50-70 % on the third cycle and further up to the final cycle (lower than 20 %). When using 1-hydroxybenzotriazole as mediator a slight decrease in decolourization efficiency was obtained. Correlation between dye oxidation peak potential and dye degradation after 10 min. reaction was obtained for both mediators.

These results show that sequencing batch decolourization by laccase mediator system is a useful methodology for treating textile dyeing wastewaters with a high potential for application at industrial level.

#### **III. 4.2 Introduction**

Synthetic dyes are widely used in such industries as textile, leather, cosmetics, food and paper printing (Forgacs et al., 2004). Reactive dyes are coloured molecules used to dye cellulose fibres. Normally, from 10 to 50 % of the initial dye load will be present in the dyebath effluent, giving rise to a highly coloured effluent. Colour removal from these wastewaters has been a major environmental concern, not only for aesthetic reasons but also and mainly because of the toxicity of many reactive dyes to aquatic life and mutagenicity to humans (Houk, 1992). Regulations have become stricter, requiring the dyes industry to reduce environmental problems related to the effluent.

A wide range of physicochemical methods have been developed for the degradation of dye-containing wastewaters (Vandevivere et al., 1998). These methods include coagulation and flocculation, adsorption, ozonation and oxidation. However, due to the chemical nature, molecular size and structure of the reactive dyes these classical processes can cause a problem in the environment and better treatments can be obtained using bioprocesses.

Recently, enzymatic treatments have attracted much interest in the decolourization/degradation of textile dyes in wastewater (Amaral et al., 2004; Cristóvão et al., 2008; Tavares et al., 2009) as an alternative strategy to conventional chemical and physical treatments, which present serious limitations. Enzymatic treatments are very useful due to the action of enzymes on pollutants even when they are present in very dilute concentrations and are recalcitrant to the various microbes participating in the degradation of dyes (Husain, 2006). The potential of the enzymes (peroxidases, manganese peroxidase, lignin peroxidase, laccases, microperoxidase, horseradish peroxidase, and turnip peroxidase) has been exploited in the decolourization and degradation of dyes (Husain and Husain, 2008). Some recalcitrant dyes were not degraded/decolourized in the presence of such enzymes. The addition of certain redox mediators enhanced the range of substrates and efficiency of degradation of those compounds. Several redox mediators have been reported in the literature (Camarero et al., 2005; Gamelas et al., 2005; Tavares et al., 2008), but very few of them are frequently used (e.g., 1-hydroxybenzotriazole, veratryl alcohol, violuric acid, 2-methoxyphenothiazone and 2,2-azinobis(3-ethylbenzothiazoline-6-sulfonic acid)).

Sequencing batch degradation is an interesting and efficient strategy for the treatment of effluents containing textile dyes. Few studies have investigated the degradation of dyes in a sequencing mode by enzymatic catalysis. Most studies of sequential decolourization of dyes are restricted to degradation with white-rot fungi (Borchert and Libra, 2001; Libra et al., 2003), bacteria and also by chemical oxidation (Horwitz et al., 1998; Krull et al., 1998).

Many studies of enzymatic catalysis with laccase have been published and assumptions regarding these mechanisms were proposed. However, few studies have been carried out on the use of cyclic voltammetry (Fernández-Sánchez et al., 2002; Zille et al., 2004) in order to better understand the correlation between the redox potential and dye degradation.

This study reports on the ability of commercial laccase for the decolourization of different reactive dyes (reactive black 5, reactive yellow 15, reactive red 239 and reactive blue 114). Sequential batch cycles of degradation were adopted in order to establish a reactor system that allows decolourization of reactive dyes over an extended period without addition of new enzyme. Effects of different enzyme mediators such as violuric acid and 1-hydroxybenzotriazole on the decolourization were studied. To better understand the mechanisms of reactive dyes oxidation with laccase and also to verify if redox potential is a good tool to predict the decolourization capacity, cyclic voltammetry was carried out.



### III. 4.3 Materials and Methods

#### III. 4.3.1 Chemicals, enzyme and mediators

Textile dyes: reactive black 5 (Remazol Black B), reactive yellow 15 (Remazol Yellow GR), reactive red 239 (Remazol Brilliant Red 3BS) and reactive blue 114 (Levafix Brilliant Blue E-BRA) were kindly provided by DyStar (Porto, Portugal).

Enzymes: Denilite II Base laccase from genetically modified *Aspergillus* and laccase from *Trametes villosa* were kindly provided by NovoNordisk (Denmark).

Enzyme mediators: Violuric acid (VA) and 1-hydroxybenzotriazole (HBT) were supplied by Sigma-Aldrich (Spain).

#### III. 4.3.2 Sequential dye decolourization

Sequential batch decolourization was carried out to evaluate the longevity of the laccase mediator systems (LMS). For this purpose, seven sequential cycles of decolourization were evaluated. No more cycles were carried out due to the lower decolourization at the end of the last cycle. The first cycle was run in an aqueous solution (25.0 mL) of dye simulating textile effluent (50 mg/L), laccase (0.2 U/mL), redox mediator VA or HBT (0.2 mmol/L) and 40 mmol/L phosphate buffer (pH 5.0). At the end of each cycle (intervals of 40 min.) an additional aliquot of concentrated dye solution (2 g/L) was added in order to obtain 50 mg/L of dye again. The reactions were incubated at 40 °C under orbital stirring. Control without mediator and control without laccase were carried out in parallel. The absorbance of the dye solution was monitored at intervals of 10 min..

#### III. 4.3.3 Determination of dye degradation

Dye decolourization by LMS was determined by monitoring the decrease in the absorbance at the wavelength of maximum absorption for each dye: reactive black 5 ( $\lambda_{\max} = 579$  nm), reactive yellow 15 ( $\lambda_{\max} = 416$  nm), reactive red 239 ( $\lambda_{\max} = 542$  nm), and reactive blue 114 ( $\lambda_{\max} = 593$  nm). A UV-visible spectrophotometer (Thermo, model UV1) was used in all experiments. Decolourization is reported as:  $\text{decolourization} = (A_i - A_f) / A_i \times 100$ , where  $A_i$  is the initial absorbance and  $A_f$  is the final absorbance of the dye solution.

#### III. 4.3.4 Cyclic voltammetry

Voltammetric measurements of the reactive dyes were carried out using a BAS 100BW (Indiana, USA) electrochemical analyzer ( $v = 50$  mV/s). A conventional three-electrode cell was supplied by BAS Inc. The working electrode was a glassy carbon disc electrode (BAS). The reference and auxiliary electrodes were saturated Ag/AgCl and Pt wire, respectively. The measurements were made at room temperature (25 °C). Solutions were purged with nitrogen for 5 min. before the measurements and blanketed with nitrogen gas during the voltammetric

scans. The experiments were performed in 0.2 mol/L acetate buffer at pH 4.5 with a dye concentration of 1 g/L. The redox potentials recorded versus Ag/AgCl were corrected by +197 mV to normal hydrogen electrode (NHE).

### III. 4.4 Results and Discussion

#### III. 4.4.1 Sequencing batch decolourization by commercial laccase

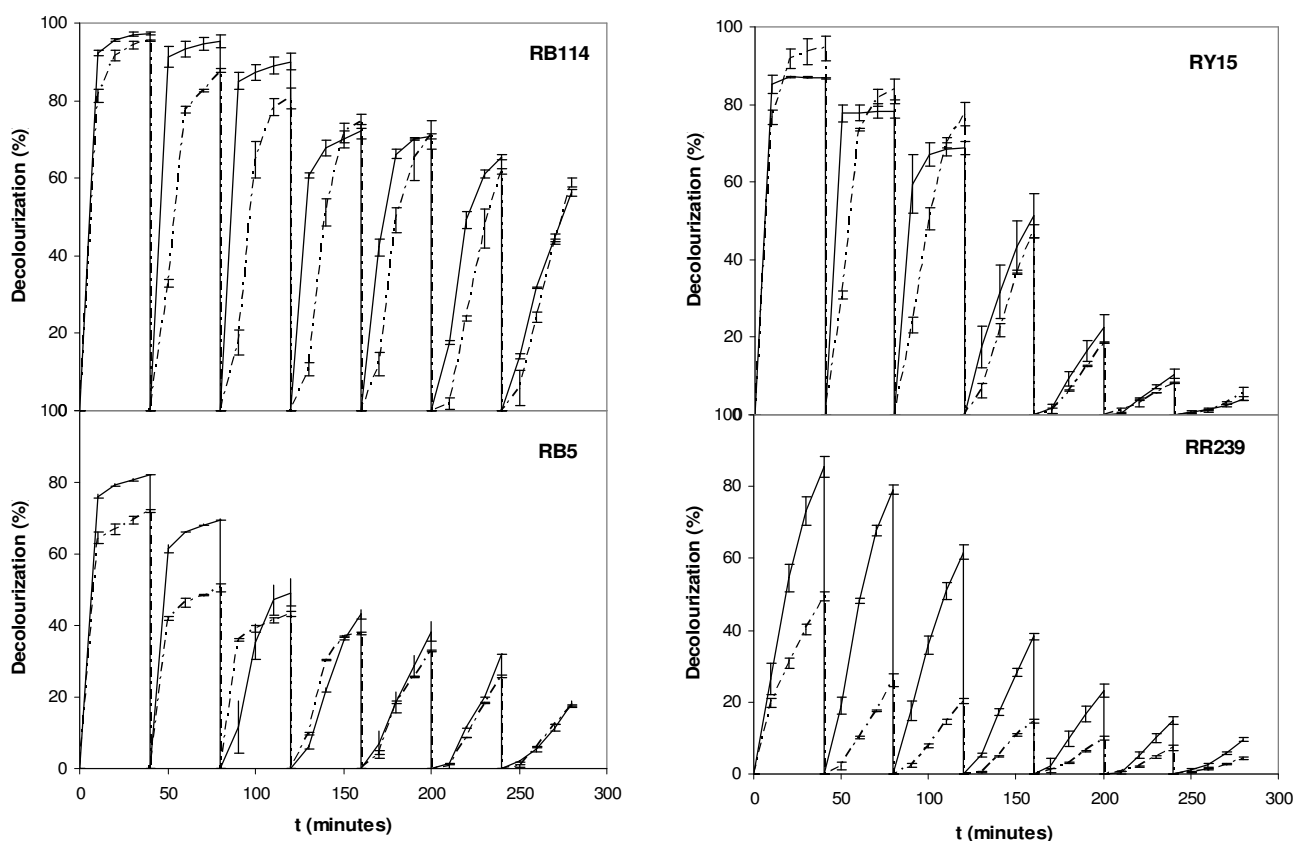
Dyes decolourization by two commercial laccases from different fungus was first evaluated. No decolourization was obtained when laccase from *Aspergillus* (DeniLite II Base) was employed. For laccase from *T. villosa* strong degradation was observed. The different behaviour of laccases can be due to the redox potential values of each enzyme. Some studies comparing the potential of fungal laccases have found that the difference in their redox potential is dependent on the source of laccase (Xu et al., 1996). Laccase from *Aspergillus oryzae* presents a low redox potential (550 mV vs. NHE) (Schneider et al., 1999) when compared with the *T. villosa* laccase which presents a potential of 790 mV versus NHE (Li et al., 1999). So, the higher redox potential is probably correlated with the observed higher enzyme activity.

Figure III. 4.1 shows the degradation of the reactive dyes in the presence of VA and HBT as mediators. Commercial laccase from *T. villosa* was capable of decolourizing the reactive dyes in repeated sequences over an extended period of 280 min. (7 cycles) for both mediators, VA and HBT. Additional aliquots of concentrated dye, to obtain a final concentration of 50 mg/L, were added to the LMS at intervals of 40 min..

The first and second cycles were accompanied by a high decolourization degree when VA was used as mediator (Figure III. 4.1) for RB114 ( $\geq 95\%$ ), RY15 and RR239 ( $\geq 80\%$ ), and for RB5 a slightly lower value was observed (70 %) at the second cycle. However, decolourization efficiency decreased to 50–70 % in the third cycle (except for RB114) and declined further in the next three cycles, to 10–30 % and then in the last cycle it was below 20%. For RB114, very high decolourization was observed at the third cycle (90 %), and in the following three cycles a slight decrease of decolourization was obtained, attaining near 60 % decolourization in the last cycle. Comparing the decolourization of the four dyes it was noted that for RB114 and RY15, rapid decolourization was obtained up to the third cycle, while for RB5 this behaviour was observed up to the second cycle and for RR239 the time required for decolourization was always higher (Figure III. 4.1). Thus, excluding RR239, in the first cycles most of the degradation took place within 10 min.. This is also evident considering the dyes decolourization rate values at 10 min. of reaction, for the first cycle of degradation (Table III. 4.1), which show, as pointed out above, faster degradation of the RB114, RY15 and RB5 dyes in comparison with RR239. The reaction rate is an intensive quantity, defined at each point of the enzymatic reaction. Therefore the rate varies if the concentration changes from point to

point. Probably due to the strong affinity of the substrate to the enzyme, the degradation was rapid in the first minutes of reaction.

A slight decrease in decolourization efficiency was obtained for sequential decolourization with HBT as mediator (Figure III. 4.1 and Table III. 4.1). This was more evident in the case of RR239 degradation, in which the decolourization degree obtained after each cycle using HBT was typically 2–3 lower than that obtained using AV.



**Figure III. 4.1** - Sequencing batch decolourization of 50 mg/L solutions of RB114, RY15, RB5 and RR239 by laccase (0.2 U/mL) from *Trametes villosa* in the presence of mediators (0.2 mM): violuric acid (—) and 1-hydroxybenzotriazole (---) at pH 5.0 and T=40 °C.

**Table III. 4.1** – Decolourization of reactive dyes by laccase mediator system in a single batch, and anodic peak potential (vs. NHE) of reactive dyes<sup>a</sup>.

Dye	Decolourization (%) <sup>b</sup>						Anodic peak (mV)	
	1 day		10 min.		Rate (mg/L.min) <sup>c</sup>			
	Laccase <sup>d</sup>	lac + VA	lac + HBT	lac + VA	lac + HBT	lac + VA		lac + HBT
RB114	99.8±0.1	99.2±0.3	99.6±0.2	92.3±0.7	81.1±1.6	4.6	4.1	889
RY15	ND <sup>e</sup>	90.2±1.1	94.5±1.2	85.2±2.3	76.7±1.8	4.3	3.8	1242
RB5	ND <sup>e</sup>	90.6±1.7	82.5±2.1	76.1±0.6	64.4 ±1.7	3.8	3.2	1272
RR239	ND <sup>e</sup>	98.1±0.5	83.2±1.9	26.5±4.3	19.7±1.4	1.3	1.0	1400

<sup>a</sup> Experimental conditions: dye (50 mg/L); mediator (0.2 mM); laccase (0.2 U/mL); pH = 5.0 and T = 40°C.

<sup>b</sup> Decolourization calculated as  $(A_i - A_f)/A_i \times 100$ , where  $A_i$  is the initial absorbance and  $A_f$  is the final absorbance of the dye solution.

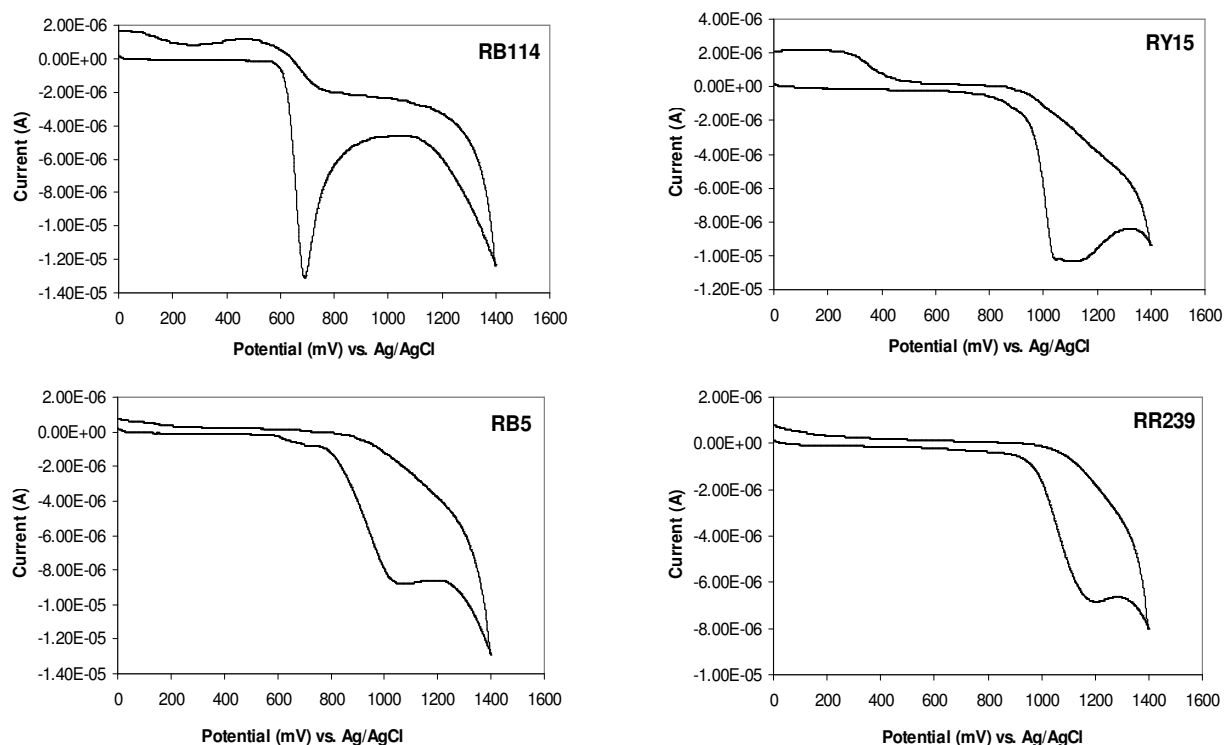
<sup>c</sup> Defined as the initial slope (up to 10 min.) of the dye decolourization (mg/L) vs. time (min.).

<sup>d</sup> No mediator was added

<sup>e</sup> No products of dye degradation were detected.

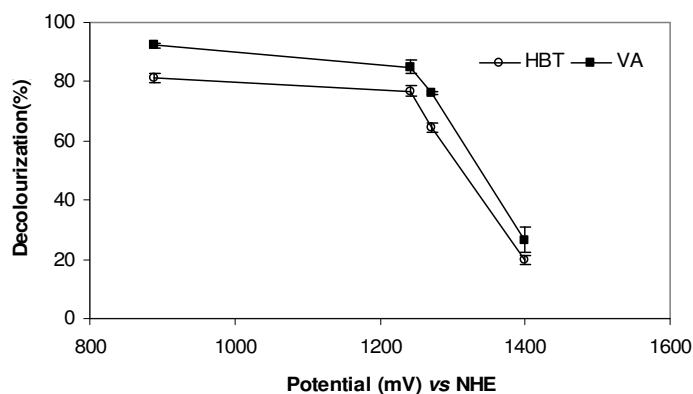
### III. 4.4.2 Cyclic voltammetry of reactive dyes

In order to establish a correlation between the dyes redox behaviour and sequential decolourization by LMS, cyclic voltammetry of the reactive dyes was employed. Figure III. 4.2 shows the cyclic voltammograms of the reactive dyes in the positive range (0–1400 mV) at a scan rate of 50 mV/s. The oxidation peak potential ( $E_{pa}$ ) resulted in the following order: RB114 ( $E_{pa} = 889$  mV versus NHE) < RY15 ( $E_{pa} = 1242$  mV versus NHE) < RB5 ( $E_{pa} = 1272$  mV versus NHE) < RR239 ( $E_{pa} = 1400$  mV versus NHE). In general, no noticeable reduction peaks were observed, showing that for the dyes studied oxidation reactions were electrochemically irreversible. For RB5 and RR239 the oxidation peak in each case was less well-defined probably due to the adsorption of the dye at the electrode surface.



**Figure III. 4.2** - Cyclic voltammograms ( $\nu = 50$  mV/s) of the reactive dyes (1 g/L) in a 0.2 M acetate buffer solution at pH = 4.5.

The decolourization after 10 min. of reaction versus the redox potential is displayed in Figure III. 4.3. The oxidation efficiency remained very high for the dyes with redox potentials below 1250 mV versus NHE and decreased proportionally for redox potentials exceeding this value. Previous work with azo dyes has shown that a linear correlation between the percentage decolourization and the respective anodic peak potential is found (Zille et al., 2004). However, this linearity was maintained for a specific period, just during the initial period of decolourization, and then the linearity disappeared (Zille et al., 2004). Thus, the results presented here show that the efficiency of decolourization by laccase increases with decreasing dye oxidation potential.



**Figure III. 4.3** - Correlation between the oxidation peak potential and decolourization (%) of reactive dyes (50 mg/L) after 10 minutes of reaction with laccase (0.2 U/mL) from *Trametes villosa*.

To help understand the suggested mechanism, new investigations of decolourization by LMS were carried out under the same conditions. The decolourization of the reactive dyes was tested in a single batch for 1 day of incubation with and without mediator to attain the maximum dye removal. The results presented in Table III. 4.1 show that RB114 was the only dye decolourized by laccase without mediator due to the lower redox potential (889 mV versus NHE) presenting high decolourization. The oxidation rate of the dyes decreased to zero after significantly exceeding the redox potential of the laccase. However, in some cases laccase is able to oxidize certain compounds with  $E_0$  values higher than its own (500–800 mV versus NHE) (Husain and Husain, 2008). Then, the presence of a mediator was required for decolourization of the other dyes RY15, RB5 and RR239, whose potentials are very high (>1200 mV versus NHE), once the use of redox mediators provide high redox potentials (>900 mV) to attack the recalcitrant structure and those are able to migrate into the aromatic structure of the dyes (Husain and Husain, 2008). Figure III. 4.4 shows the decolourizations achieved for each dye.



**Figure III. 4.4** – Initial and treated solutions of RY15, RR239, RB114 and RB5, showing the decolourizations achieved.

Comparing the two mediators, VA seems to be a more effective mediator for decolourization (Figure III. 4.3 and Table III. 4.1) of the reactive dyes studied. VA is a more favourable mediator than HBT, probably due to the longer lifetime of the VA under the conditions studied.  $E_{1,2} = 900$  mV (versus NHE) for VA and  $E_{pa} = 1100$  mV for HBT have been reported at pH 5.0 (Feng et al., 2000). In addition, the cyclic voltammetry of HBT exhibited irreversible oxidation once only a very small cathodic peak was detected. The better stability, electrochemical reversibility and lower potential of VA can explain the better performance of VA when compared with HBT. The oxidation of HBT generates an unstable intermediate radical that decays into inactive catalytic products (Feng et al., 2000).

The choice of an adequate mediator plays a key role for the general applicability and effectiveness of LMS. Many possible mediator compounds have already been described in the literature for the degradation of various compounds. In this work, two mediators were tested as

described above. The colour removal from the reactive dyes was dependent on their redox potentials and could also depend on the mediator (VA and HBT) potential. The oxidation of polycyclic aromatic hydrocarbons by laccase and mediators with different redox potential demonstrated that the oxidation efficiency increased proportionally with the redox potentials of the phenolic mediators up to a maximum value of 900 mV and decreased thereafter with redox potentials exceeding this value. This was attributed to the fact that the reaction does not end for mediators with potentials much higher than laccase (Johannes and Majcherczyk, 2000).

### III. 4.5 Conclusions

The results presented here demonstrate that laccase from *T. villosa* can be used over a long period (>250 min.) of sequential dye degradations. Seven repetitive decolourization cycles performed using LMS demonstrated the feasibility of biological catalysts and their reuse in reactive dyes degradation. Thus, LMS may possibly be applied for the effective treatment of effluents from the textile industry.

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## **Part IV**

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# Kinetic Modelling and Simulation



*Part IV deals with the kinetic modelling and simulation of the decolourization reactions.*

*Part IV. 1 is dedicated to the development of mathematical models to simulate the decolourization kinetics of each of the reactive dyes studied in the previous part by commercial laccase (DeniLite II S).*

*In part IV. 2 the degradation of a mixture of three reactive textile dyes (Reactive Black 5, Reactive Yellow 15 and Reactive Red 239), simulating a real textile effluent, by commercial laccase, is investigated in a batch reactor and mathematical models are developed to simulate the kinetics of the reaction.*

*Part IV. 3 presents the treatment of a synthetic dye house effluent, simulating a textile wastewater containing various reactive dyestuffs (Reactive Yellow 15, Reactive Red 239 and Reactive Black 5), salts and auxiliary chemicals by commercial laccase and the mathematical models developed concerning the kinetics of the reaction. The water quality parameters of the simulated effluent are also evaluated.*



## **Part IV. 1** Kinetic modelling and simulation of laccase catalyzed degradation of reactive textile dyes\*

IV. 1.1 Abstract

IV. 1.2 Introduction

IV. 1.3 Materials and Methods

IV. 1.4 Kinetic Modelling: Optimization and Simulation

IV. 1.5 Results and Discussion

IV. 1.6 Conclusions

IV. 1.7 References

*\*based on: Cristóvão, R.O., Tavares, A.P.M., Ribeiro, A.S., Loureiro, J.M., Boaventura, R.A.R., Macedo, E.A., 2008. Kinetic modelling and simulation of laccase catalyzed degradation of reactive textile dyes. Bioresource Technology, 99, 4768-4774.*



## **IV. 1 Kinetic modelling and simulation of laccase catalyzed degradation of reactive textile dyes**

### **IV. 1.1 Abstract**

A kinetic model based on Michaelis–Menten equation was developed to simulate the dye decolourization of Reactive Black 5 (RB5), Reactive Blue 114 (RB114), Reactive Yellow 15 (RY15), Reactive Red 239 (RR239) and Reactive Red 180 (RR180) dyes by commercial laccase. The unusual kinetic behaviour of some of these reactions suggests that the kinetic model must consider the activation of the laccase-mediator system. Several reactions at different concentrations of each dye were performed in batch reactors and time courses were obtained. A LSODE code to solve the differential equation obtained from the batch reactor was combined with an optimization Fortran program to obtain the theoretical time courses. The time courses obtained from the developed program were compared with the experimentally obtained ones to estimate the kinetic constants that minimized the difference between them. The close correlation between the predicted and the experimental results seems to support the reliability of the established models.

### **IV. 1.2 Introduction**

Considering both volumes discharged and effluent composition, the wastewater generated by the textile industry is rated as the most polluting among all industrial sectors (Vandevivere et al., 1998). The presence of very low concentrations of dyes in effluent is highly visible and undesirable (Nigam et al., 2000). There are more than 100,000 commercially available dyes with over  $7 \times 10^5$  ton of dyestuff produced annually (Robinson et al., 2001). The dyes do not bind completely to the fabric and depending on the class of the dye its loss in wastewaters could vary from 2 % for basic dyes to as high as 50 % for reactive dyes (Pandey et al., 2007), causing serious environmental problems. The presence of colour in water will affect the transmission of light and photosynthesis and reduce aquatic diversity.

Many dyes are difficult to decolourize due to their complex structure and synthetic origin. A variety of physical, chemical and biological methods are presently available for the treatment of textile wastewater (Anjaneyulu et al., 2005; Forgacs et al., 2004; Slokar and Marechal, 1998). There is a growing recognition that enzymes can be used in many remediation processes to target specific pollutants for treatment (Durán and Esposito, 2000). Different studies show that extracellular ligninolytic enzymes of white-rot fungi can degrade a wide variety of recalcitrant compounds, such as dyes (Chivukula and Renganathan, 1995; Harazono et al., 2003; Lan et al., 2006; Nyanhongo et al., 2002). Laccase (p-diphenol oxidase, EC 1.10.3.2) catalyzes the oxidation of phenolic compounds and aromatic amines and accepts a broad range

of substrates (Claus, 2004; Thurston, 1994). The number of substrates can be extended by addition of a redox mediator (Bourbonnais and Paice, 1990; Soares et al., 2001). The mediator is a compound with low molecular weight which acts as a kind of electron carrier. Once it is oxidised by the enzyme, it diffuses away from the catalytic system and in turn oxidizes any substrate that, due to its size, could not be directly oxidized by the enzyme (Call and Mucke, 1997).

The kinetics of a reaction system can be studied by a mathematical modelling technique. The most important matter is to find an accurate model equation that has the capability to estimate the value of the reaction rate close to the experimentally observed one. The model of a certain reaction system should consider all the important parameters. Once formulated, it can be solved and the predicted behaviour can be compared with experimental data. Any significant differences between the system performance and the behaviour predicted by the model imply that there may be some other important effects not considered. The kinetic constants are estimated by fitting the model equation to the experimental data. The model can then be used for such purposes as predicting the system performance under different operating conditions, reactor design, scale-up, optimization and control of the system (Bas et al., 2007; Houg and Liao, 2006).

Studies on dye degradation by laccase have been published (Abadulla et al., 2000; Campos et al., 2001; Kandelbauer et al., 2004; Wong and Yu, 1999). However, not so many papers have actually dealt with the kinetics of the reaction. Some works reported the values of kinetic constants of enzymatic dye degradation obtained from initial reaction rates (Almansa et al., 2004; Moldes and Sanroman, 2006), but to our knowledge there has been no study that determined the kinetic constants of enzymatic dye decolourization from the entire time course data.

The aim of this work is to establish a mathematical model and to determine the kinetic constants that can adequately describe the kinetic behaviour of five reactive textile dyes (Reactive Black 5 (RB5), Reactive Blue 114 (RB114), Reactive Yellow 15 (RY15), Reactive Red 239 (RR239) and Reactive Red 180 (RR180)) decolourization by a commercial laccase. Success of the model was determined by comparing the time courses obtained experimentally with those obtained from the model.

## **IV. 1.3 Materials and Methods**

### **IV. 1.3.1 Chemicals and enzyme**

Textile dyes: Reactive Black 5 (Remazol Black B), Reactive Blue 114 (Levafix Brilliant Blue E-BRA), Reactive Yellow 15 (Remazol Yellow GR), Reactive Red 239 (Remazol Brilliant



Red 3BS) and Reactive Red 180 (Remazol Brilliant Red F3B) were kindly provided by DyStar (Portugal) and were used for degradation experiments without any further purification.

Enzyme: Commercial laccase formulation (DeniLite II S; 120 U/g) from genetically modified *Aspergillus* was kindly provided by Novozymes. This formulation is used for indigo dye decolourization in denim finishing operations and includes a buffer and an enzyme mediator.

#### IV. 1.3.2 Dye decolourization kinetics

Preliminary studies of optimization of laccase-catalyzed decolourization of reactive dyes by response surface methodology enabled us to establish the optimal conditions of pH, temperature and enzyme mass used in reactor for each degradation. However, the commercial laccase formulation is a heterogeneous mixture. Reactions with the optimal enzyme mass showed that it was not possible to get reproducible results with this amount of enzyme. The amount of enzyme used was not representative of the composition of the mixture. Assays were carried out where the enzyme mass was increased five times, obtaining, by this way, reproducible results. However, unexpectedly, the reactions with more enzyme loads exhibited an apparent lesser degradation. In order to understand this phenomenon, a batch without dye, i.e., with only the enzyme and a buffer was carried out under stirring. It was observed that, after a short period of time, some turbidity appeared that increased with time (Figure IV. 1.1). This fact was not observed when a small amount of enzyme was used. Thus, this turbidity (apparent colour) masks the effective degradation and contributes for the observed lesser degradation. To cope with this problem, the enzyme and buffer solution absorbances were measured along time at the maximum absorbance wavelength of each dye and their values were subtracted from the corresponding absorbance value of the dye degradation reaction.



**Figure IV. 1.1** - Colour formed by the enzyme solution over time.

So, to study the kinetic behaviour of the five reactive textile dyes, five different concentrations of each dye (from 25 mg/L to 125 mg/L) and 432 U/L of commercial laccase were incubated in 50 mL Erlenmeyer flasks at 35 °C with phosphate buffer (50 mM/ pH 7.0) under stirring. For each assay duplicate runs were made.

After taking a zero sample, decolourization was started by the addition of laccase. Samples were withdrawn at certain time intervals that increased as the reaction proceeded. The samples were subsequently analyzed by UV–vis spectrophotometry.

### IV. 1.3.3 Determination of dye concentration

Dye concentration was determined through a calibration curve by reading the absorbance of the samples at the maximum absorbance wavelength for each dye: Reactive Black 5 (579 nm), Reactive Blue 114 (593 nm), Reactive Yellow 15 (416 nm), Reactive Red 239 (542 nm) and Reactive Red 180 (540 nm). UV–vis spectrophotometer (Thermo, model UV1) was used in all experiments. By measuring the amount of the substrate remaining overtime it is possible to obtain the concentration versus time plot which is known as progress curve of the enzymatic reaction or time course.

## IV. 1.4 Kinetic modelling: optimization and simulation

### IV. 1.4.1 Kinetics of enzymatic reactions

In 1913, Michaelis and Menten proposed a reaction mechanism for enzymatic reactions. As a starting point, it is assumed that the enzyme and substrate combine to form a complex, which then dissociates into product and free enzyme as follows:



where  $E$ ,  $S$ ,  $ES$  and  $P$  are enzyme, substrate, enzyme-substrate complex and product, respectively.  $K_{MS}$  and  $k_2$  represent Michaelis-Menten constant and catalytic rate constant, respectively. The dependence of the reaction rate ( $v$ ) on the substrate concentration is represented by the Michaelis-Menten equation and can be derived as:

$$v = k_2 [ES] = \frac{v_{max} [S]}{K_{MS} + [S]} \quad (\text{IV. 1.1})$$

where  $v_{max}$  is the maximum reaction rate and  $[ES]$  and  $[S]$  are concentrations of the enzyme-substrate complex and the substrate, respectively.

Preliminary studies showed that the degradation of some reactive dyes by commercial laccase is not complete. So, to describe the kinetics of these enzymatic decolourizations the irreversible (Equation (IV. 1.1)) and the reversible (Equation (IV. 1.2)) forms of Michaelis-Menten equation were employed (Murzin and Salmi, 2005).

$$v = \frac{v_{max} \left( [S] - \frac{[P]}{K_{eq}} \right)}{K_{MS} \left( 1 + \frac{[P]}{K_{MP}} \right) + [S]} \quad (\text{IV. 1.2})$$

where  $K_{eq}$  is the equilibrium constant and  $K_{MP}$  is the Michaelis-Menten constant for product.  $[P]$  is the product concentration.

#### IV. 1.4.2 Batch reactor balance

The differential equation obtained from the mass balance to a batch reactor is given by Equation (IV. 1.3).

$$-\frac{d[S]}{dt} = v \cdot W_E \cdot \frac{1}{V_L} \quad (\text{IV. 1.3})$$

where  $W_E$  is the enzyme mass,  $V_L$  is the volume of the reactor and  $t$  is the time.

#### IV. 1.4.3 Activation of the laccase-mediator system

In general enzymatic reactions, the reaction rate increases with the increase of substrate concentration. When the substrate concentration increases up to a certain high value, the reaction rate reaches a plateau and keeps constant even if more substrate is used. On preliminary studies of dye degradation reactions it was possible to observe for some reactive dyes an unusual kinetic behaviour: there is a short period of time in the beginning of the reaction that does not follow the Michaelis-Menten equation. At this point an increase in the concentration of substrate causes only a very small increase in the rate – the slope is less than predicted. Preliminary results have also shown that pure laccase did not decolourize the five reactive textile dyes under study, indicating that the presence of a mediator to oxidise the dyes was required. The oxidation was not carried out by the enzyme directly, but rather by the oxidised form of the mediator. So, the time period described seems to correspond to an induction time where an activation effect of the laccase-mediator system occurs. This situation is similar to a perfectly agitated solution where the enzyme and the mediator are present, but initially they cannot oxidise the substrate. They need a period of time to be activated, that is represented by an exponential term. So, in order to predict this period for some of the dyes a new term, taking into account this induction time, was added to the equations previously presented.

$$v = \frac{v_{max}[S]}{K_{MS} + [S]}(1 - e^{-kt}) \quad (\text{IV. 1.4})$$

$$v = \frac{v_{max} \left( [S] - \frac{[P]}{K_{eq}} \right)}{K_{MS} \left( 1 + \frac{[P]}{K_{MP}} \right) + [S]}(1 - e^{-kt}) \quad (\text{IV. 1.5})$$

where  $k$  is the rate constant of the activation period of the laccase-mediator system.

#### IV. 1.4.4 Estimation of the reaction kinetics and kinetic constants

To predict dye concentrations versus time profile in the batch reactor, the system of equations obtained from the batch reactor balance (Equation (IV. 1.3)) and from the proposed kinetics for the enzymatic reactions (Equation (IV. 1.1), (IV. 1.2), (IV. 1.4) or (IV. 1.5)) was solved using a Fortran program with integration by LSODE solver (Livermore Solver for Ordinary Differential Equations) based on Adams Backward Differentiation Formula methods. The initial concentrations of dye and variables were fed to the program. This program was combined with an optimization algorithm to estimate the kinetic constants of the proposed model by minimizing the difference between the predicted time courses and the ones obtained experimentally. The function to minimize between both time courses was the sum of squared relative residuals and was calculated as in Equation (IV. 1.6).

$$F = \sum_1^n \left| \frac{C_{calc} - C_{exp}}{C_{exp}} \right|^2 \quad (\text{IV. 1.6})$$

where  $C_{calc}$  is the concentration calculated using the model equation,  $C_{exp}$  is the experimental concentration and  $n$  is the total number of experimental or calculated points. The function was minimized through an optimization loop based on an adaptive random search algorithm that varies the values of the kinetic constants until a global minimum within the optimization criteria is achieved (Salcedo et al., 1990; Salcedo, 1992). This procedure was repeated for each dye studied.

### IV. 1.5 Results and discussion

#### IV. 1.5.1 Kinetic modelling and estimation of kinetic constants

A kinetic model to simulate the decolourization of each of the five reactive textile dyes in a batch reactor by a commercial laccase formulation containing a specific mediator was

proposed. Some studies related to dye degradation present kinetic constants values based on initial reaction rates (Kandelbauer et al., 2004; Soares et al., 2002). In this work, the kinetic constants of the proposed models were estimated by comparing the experimental time courses with the predicted ones for each dye.

Experimental time courses were obtained in duplicate at five different initial dye concentrations for each dye. For RB5, RB114 and RY15, it was observed that initially the dye concentration almost do not decrease, probably corresponding to the activation time of the laccase-mediator system. So, the kinetic model for these dyes must present an exponential term to predict this induction time. For RB5 and RB114 the dye concentration decreases with the increase of time until reaching a plateau where no more dye is degraded, while the experiments with RY15, RR239 and RR180 presented complete degradation.

A program using the LSODE code to solve the differential equation obtained from the batch reactor balance (Equation (IV. 1.3)) considering the proposed kinetics for the enzymatic reaction (Equation (IV. 1.1) for RR239 and RR180, Equation (IV. 1.4) for RY15 and Equation (IV. 1.5) for RB5 and RB114) was combined with an optimization program (Salcedo et al., 1990; Salcedo, 1992) to obtain the theoretical time courses. The algorithm developed adjusts automatically the kinetic constants so that the output response (predicted by the model) and the input values (experimental data) were as close as possible according to the objective function (Equation (IV. 1.6)). Estimation was made and the results were compared with the corresponding experimental value. This process was repeated while the relative errors between the estimated and the experimental values decreased.

The obtained kinetic constants for each dye considering the selected kinetic model are shown in Table IV. 1.1, which were used to draw the continuous lines in Figures IV. 1.2 – IV. 1.6.

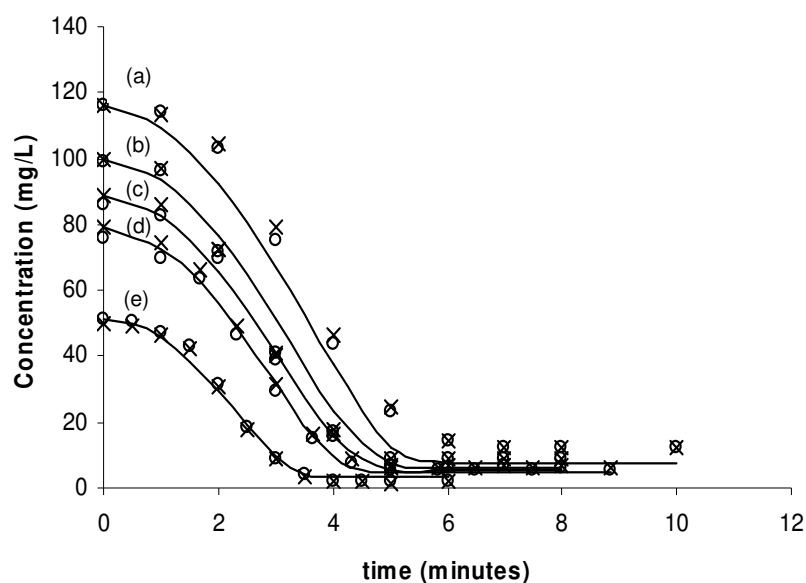
**Table IV. 1.1** – Proposed model, kinetic data and average sum of squared relative residuals (*SSRR*) for RB5, RB114, RY15, RR239 and RR180 degradation by commercial laccase.

	<b>RB5</b>	<b>RB114</b>	<b>RY15</b>	<b>RR239</b>	<b>RR180</b>
<b><i>Kinetic equation</i></b>	(IV. 1.5)	(IV. 1.5)	(IV. 1.4)	(IV. 1.1)	(IV. 1.1)
<b><math>v_{max}</math> (mg/g.min)</b>	20.000	18.677	37.500	1.190	3.460
<b><math>K_{MS}</math> (mg/L)</b>	3.1384	21.283	99.000	165.000	650.000
<b><math>K_{MP}</math> (mg/L)</b>	300.0	450.0	---	---	---
<b><math>K_{eq}</math></b>	15.000	2.278	---	---	---
<b><math>k</math> (min<sup>-1</sup>)</b>	0.192	0.067	0.081	---	---
<b><i>SSRR/n</i></b>	$8.836 \times 10^{-2}$	$4.948 \times 10^{-3}$	918.548	6.233	6.823

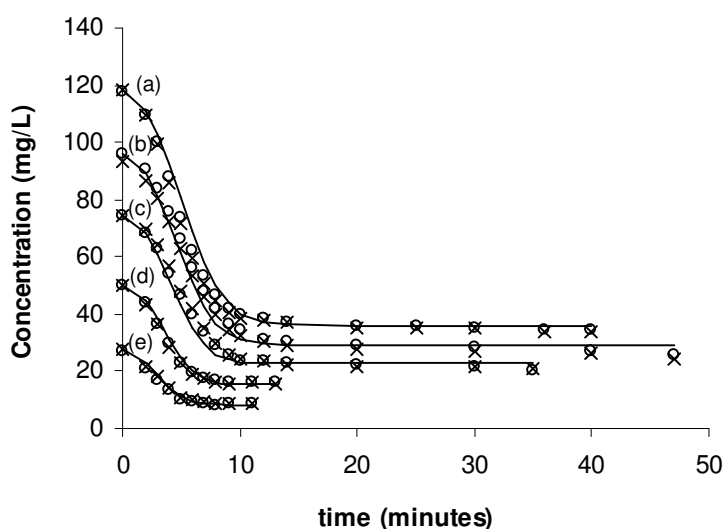
In a system without a mediator, the Michaelis–Menten constant  $K_{MS}$  is the equilibrium constant of the enzyme–substrate complex decomposition, so, by analogy, in a system with a mediator the  $K_{MS}$  constant is probably the equilibrium constant of the enzyme-mediator/substrate complex decomposition. So, it is a measure of the enzyme-mediator system affinity to the substrate. The lesser the value of  $K_{MS}$ , the larger is the affinity of the enzyme-mediator system to the substrate. Comparing the  $K_{MS}$  values of each dye, the laccase-mediator system affinities for the dyes decrease according to the following order: RB5 > RB114 > RY15 > RR239 > RR180. This result is easy to confirm in Figures IV. 1.2 – IV. 1.6 by the time that each dye takes to reach the equilibrium. A larger dyes degradation time corresponds to a more difficult decolourization (less affinity of laccase-mediator system for the dye), probably due to the structure of the dye or to the difference of redox potential between the dye and the laccase-mediator system (Almansa et al., 2004; Kandelbauer et al., 2004; Zille et al., 2004). The velocity of dyes degradation can also be evaluated by the value of  $v_{max}$  – the theoretical maximal velocity, which is proportional to the kinetic constant  $k_2$ . According to the values of  $v_{max}$  presented in Table IV. 1.1 for each dye studied, the degradation of dyes RB5, RB114 and RY15 by commercial laccase is faster than the degradation of RR239 and RR180, that present lower values of  $v_{max}$ .

The activation of the laccase-mediator system is another important aspect to be considered. The present study enables one to evaluate the activation rate of the laccase mediator system on RB5, RB114 and RY15 dyes degradation by inspection of the  $k$  values obtained in the kinetic model (Table IV. 1.1). According to the results, the activation of the laccase-mediator system is faster in the degradation of RB5 and decreases in the following order: RB5 > RY15 > RB114. To our knowledge, this is the first report on the activation of the laccase-mediator system on dyes degradation by enzyme laccase.

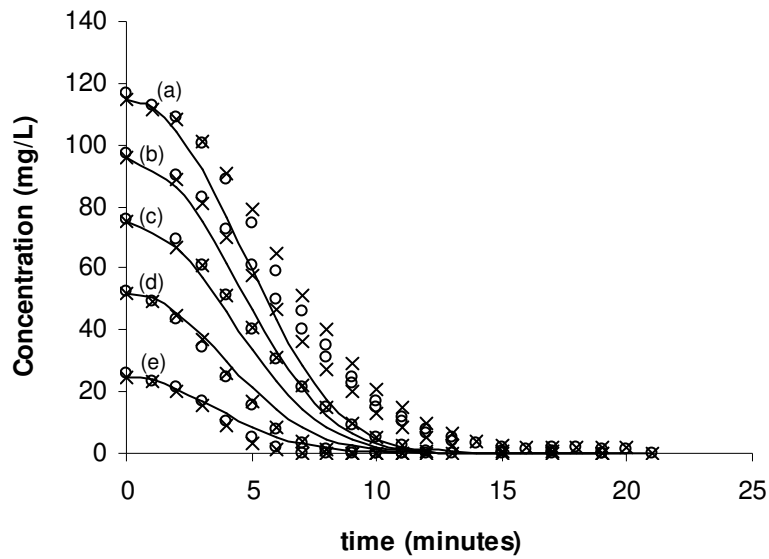
In order to evaluate the adequacy of the proposed model for the kinetics of dye decolourization by commercial laccase, the time courses calculated by the kinetic models were compared with the experimental ones. These comparisons for RB5, RB114, RY15, RR239 and RR180 degradation are presented in Figures IV. 1.2 – IV. 1.6, respectively. For RR239 and RR180 only three different concentrations are presented to avoid overloading the graphs.



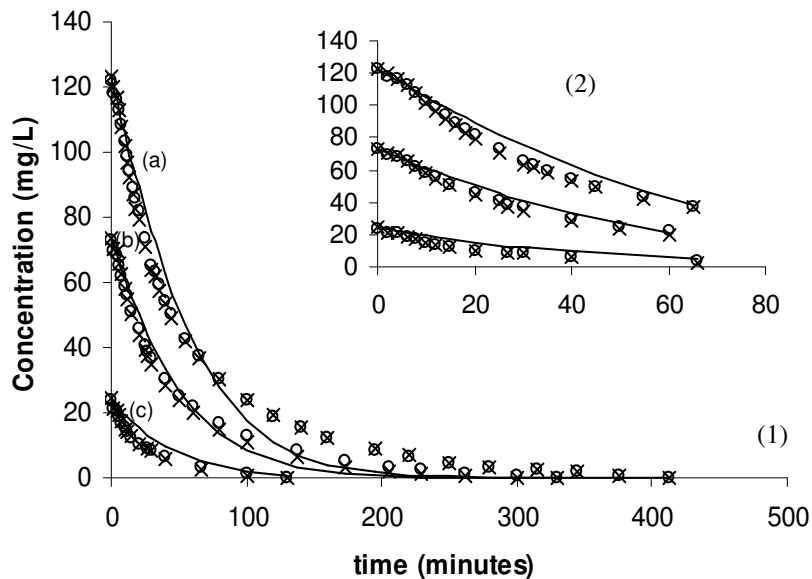
**Figure IV. 1.2** - Comparison of experimental ( $\times$  run 1;  $o$  run 2) and simulated (continuous line) time courses of RB5 degradation by commercial laccase under different dye initial concentrations: (a) 116.0 mg/L and 115.8 mg/L; (b) 99.5 mg/L and 99.3 mg/L; (c) 88.5 mg/L and 85.8 mg/L; (d) 78.9 mg/L and 76.0 mg/L; (e) 49.9 mg/L and 51.5 mg/L.



**Figure IV. 1.3** – Comparison of experimental ( $\times$  run 1;  $o$  run 2) and simulated (continuous line) time courses of RB114 degradation by commercial laccase under different dye initial concentrations: (a) 118.4 mg/L and 117.8 mg/L; (b) 93.2 mg/L and 96.2 mg/L; (c) 74.6 mg/L and 74.1 mg/L; (d) 50.3 mg/L and 50.4 mg/L; (e) 27.6 mg/L and 27.3 mg/L.

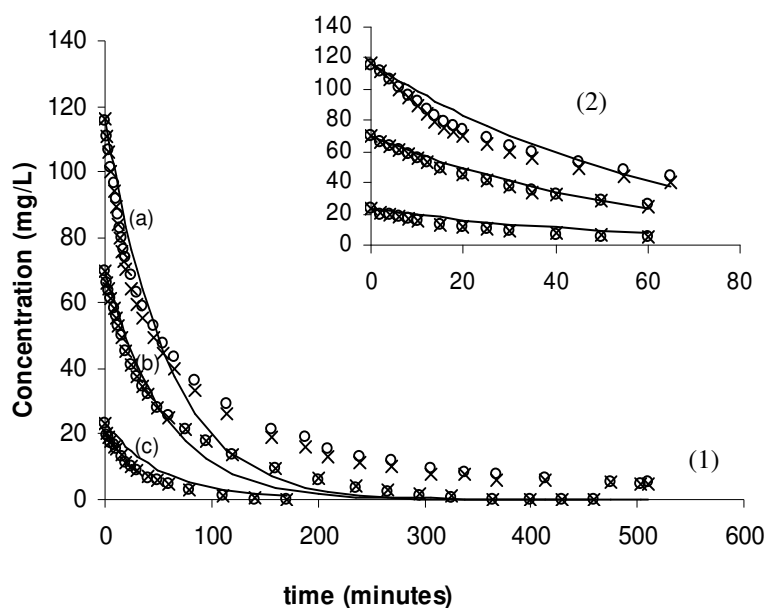


**Figure IV. 1.4**– Comparison of experimental (× run 1; o run 2) and simulated (continuous line) time courses of RY15 degradation by commercial laccase under different dye initial concentrations: (a) 116.8 mg/L and 116.9 mg/L; (b) 95.9 mg/L and 97.4 mg/L; (c) 75.3 mg/L and 76.1 mg/L; (d) 47.7 mg/L and 49.1 mg/L; (e) 25.3 mg/L and 25.6 mg/L.



**Figure IV. 1.5** – (1) Comparison of experimental (× run 1; o run 2) and simulated (continuous line) time courses of RR239 degradation by commercial laccase under different dye initial concentrations: (a) 123.0 mg/L and 122.2 mg/L; (b) 73.7 mg/L and 72.8 mg/L; (c) 24.3 mg/L and 24.0 mg/L. (2) Scale amplification of (1).





**Figure IV. 1.6** – (1) Comparison of experimental ( $\times$  run 1;  $o$  run 2) and simulated (continuous line) time courses of RR180 degradation by commercial laccase under different dye initial concentrations: (a) 116.3 mg/L and 115.8 mg/L; (b) 69.9 mg/L and 69.8 mg/L; (c) 23.4 mg/L and 23.0 mg/L. (2) Scale amplification of (1).

The comparisons show that the model proposed, including an induction period and reversible reaction (Equation (IV. 1.5)), describes with remarkable accuracy the RB114 degradation (Figure IV. 1.3) and less well the RB5 degradation (Figure IV. 1.2). The degradation of the remaining dyes seems to be irreversible since the experimentally measured concentrations, after subtracting the turbidity communicated by the enzyme support, tends to zero. In these cases, whether with (RY15, Figure IV. 1.4) or without (RR239, Figure IV. 1.5 and RR180, Figure IV. 1.6) an induction period, the proposed models, although exhibiting a correct qualitative behaviour, present some systematic quantitative deviations, more evident for the yellow dye RY15. The results in Table IV. 1.1 show that Equation (IV. 1.4) seems not to be applicable to RY15; this is probably due to the fact that both this dye and the enzyme plus buffer solution show their maximum absorbances at close wavelength values. Note that the absorbance of the enzyme plus buffer solution was subtracted during the treatment of the results, probably masking the dye absorbance results for this case. It should be noted that if the turbidity (apparent colour) due to the enzyme support were not subtracted, the last models would do a better job. Since this apparent colour is not very reproducible, some work has to be done yet in order to try to understand what is really happening. Nonetheless, the proposed mathematical models with the parameters values displayed in Table IV. 1.1, can be considered to represent within reasonable accuracy the observed dyes degradations and the overall behaviour of these systems. In principle, the models can be used whenever the commercial laccase is used in the degradation of reactive dyes. But the fact that the behaviour of the

commercial laccase changes with the colour of the dye indicates that they should be used with care.

#### IV. 1.6 Conclusions

Mathematical models based on Michaelis–Menten equation were proposed for reactive dyes degradation by commercial laccase in a batch reactor.

In this study, kinetic constants were determined by minimizing the difference between the time courses predicted by the model and experimental ones. The similarity between the experimental data and the predicted values for all dyes studied indicates that the proposed models could simulate successfully the kinetic behaviour of reactive dyes degradation by commercial laccase.

The models allow to examine the effects of the considered process parameters on decolourization of reactive dyes by commercial laccase and can be used to predict the time courses of the substrate consumption and the product formation under different substrate concentrations. The knowledge of the kinetic models of these reactions also provides an emergent tool that can be applied to the simulation and design of enzymatic bioreactors.

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## **Part IV. 2** Modelling the decolourization of a mixture of reactive textile dyes by commercial laccase\*

IV. 2.1 Abstract

IV. 2.2 Introduction

IV. 2.3 Materials and Methods

IV. 2.4 Kinetic Modelling: Optimization and Simulation

IV. 2.5 Results and Discussion

IV. 2.6 Conclusions

IV. 2.7 References

*\*based on: Cristóvão, R.O., Tavares, A.P.M., Ferreira, L.A., Loureiro, J.M., Boaventura, R.A.R., Macedo, E.A., 2009. Modeling the discoloration of a mixture of reactive textile dyes by commercial laccase. Bioresource Technology, 100, 1094-1099.*



## **IV. 2 Modelling the decolourization of a mixture of reactive textile dyes by commercial laccase**

### **IV. 2.1 Abstract**

Degradation of a mixture of three reactive textile dyes (Reactive Black 5, Reactive Yellow 15 and Reactive Red 239), simulating a real textile effluent, by commercial laccase, was investigated in a batch reactor. The decolourization was appraised as a percentage of the absorbance reduction at the wavelength of maximum absorbance for each dye and as total colour removal based in all visible spectrum. A significantly high decolourization was achieved in both cases, indicating the applicability of this method for textile wastewater treatment. Mathematical models were developed to simulate the kinetics of laccase catalyzed degradation of reactive dyes in mixtures. Like in single dye degradation, some of the reactions present an unusual kinetic behaviour, corresponding to the activation of the laccase-mediator system. The kinetic constants of the models were estimated by minimizing the difference between the predicted and the experimental time courses. Although not perfect, the ability of the models in representing the experimental results suggests that they could be used in design and simulation applications.

### **IV. 2.2 Introduction**

Textile dyeing plants, particularly those involving finishing processes are among the major sources of water pollution. These industries consume large volumes of water and chemicals. There are more than 100,000 commercially available dyes with over  $7 \times 10^5$  tons of dyestuff produced annually worldwide and used extensively in textile, dyeing and printing industries (Robinson et al., 2001; Spadaro et al., 1994; Zollinger, 1987). Wastewater streams from the textile dyeing operations contain unused dyes (about 8–20 % of the total pollution load due to incomplete exhaustion of the dye) and auxiliary chemicals (Mukherjee et al., 1999). Often, dyes are recalcitrant organic molecules that impart strong colour to the wastewater, also contributing to the organic load and toxicity of the wastewater. Apart from the aesthetic problem, the greatest environmental concern with dyes is the absorption and reflection of sunlight entering the water, which interferes with the growth of algae, limiting it to levels insufficient to biologically degrade impurities in the water. It is evident, therefore, that removal of such coloured agents from aqueous effluents is of significant environmental, technical and commercial importance (Forgacs et al., 2004; Pearce et al., 2003; Pinheiro et al., 2004; Vandevivere et al., 1998).

The treatment of such dye-containing effluents is mostly based on physical and chemical procedures, e.g. adsorption, flotation, fenton oxidation, reduction ( $\text{Na}_2\text{S}_2\text{O}_4$ ), ion

exchange, chlorination/ozonation and incineration. These methods are rather costly and sometimes produce hazardous byproducts (Shaul et al., 1991). The idea of using oxidoreductive enzymes for wastewater treatment was developed in the early 1980s, since enzyme-based methods have minimal impact on ecosystems and low energy requirements. Moreover, enzymes can operate in a wide pH range, at moderate temperature or ionic strength and, to some extent, they are active in the presence of organic solvents (Torres et al., 2003).

Laccases (EC 1.10.3.2) are blue multi-copper-containing enzymes that catalyze the oxidation of a variety of organic substances coupled to the reduction of molecular oxygen (Alcalde et al., 2006; Reinhammar, 1984; Solomon et al., 1996). Because of their broad specificity for the reducing substrates, laccases from white-rot fungi are receiving increasing attention as potential industrial enzymes in various applications, such as pulp delignification, wood fiber modification, dye or stain bleaching, chemical or medicinal synthesis and contaminated water or soil remediation (Couto and Herrera, 2006). Further, the presence of small molecular weight redox mediators enhances the range and the rates of compounds to be oxidized (including recalcitrant dyes) by the so-called laccase-mediator systems (LMS) (Reyes et al., 1999).

An understanding of the kinetics of enzyme systems is essential for the design of efficient reactors to carry out industrial processes, as well as for optimization and control purposes. The most important objective of a kinetic study is to find a model equation that has the capability to estimate the experimental reaction rate as closely as possible to the experimental reaction rate. Thus, in a kinetic study, the first step is to find suitable model(s) to simulate the experimental data properly. One or more model equations are selected and kinetic parameters are estimated by fitting the model equation(s) to the experimental data (Bas et al., 2007).

Various studies on dye degradation by laccase have been published. Most of these works were single-solute studies which used commercially available dyes as model pollutants (Abadulla et al., 2000; Campos et al., 2001; Kandelbauer et al., 2004; Tavares et al., 2008; Wong and Yu, 1999). However, most often, industrial situations involve the discharge of effluents that contain mixtures of several dyes. Limited data are available on laccase mixed dye degradation but it is important to evaluate the feasibility of this method to treat real textile effluents. Investigations using simulated dye wastewaters are helpful to understand the colour removal process in the actual textile wastewater treatments. In a preliminary work, we studied the effects of several operating parameters, namely pH, temperature and enzyme mass on the single dye degradation process (Tavares et al., 2009). This enabled us to establish the optimal conditions to be used in reactors for degradation of a commercial dye, used as a model pollutant, by commercial laccase. We also studied the kinetics of the degradation reactions, which has been the subject of very few research works, so far. Some works reported the values of kinetic constants of enzymatic dye degradation obtained from initial reaction rates (Almansa et al., 2004; Moldes and Sanromán, 2006) and, apart from our previous work (Cristóvão et al.,



2008), as far as we are aware, there was no other study that determined the kinetic constants of enzymatic dye decolourization from the entire time course data.

In this paper, we extend our work to study the applicability of the laccase degradation method for the treatment of mixed dyes, simulating an effluent, and to study the kinetics of this reaction. This constitutes a strategic approach for environmental protection, in the framework of pollution abatement in textile industries by enzymatic wastewater treatment.

So, this work aims to establish a mathematical model and to determine the kinetic constants that can adequately describe the kinetic behaviour of the decolourization of a mixture of reactive textile dyes (Reactive Black 5 (RB5), Reactive Yellow 15 (RY15) and Reactive Red 239 (RR239)) by a commercial laccase. The success of the model was appraised by comparing the time courses obtained experimentally with those predicted by the model.

## **IV. 2.3 Materials and Methods**

### **IV. 2.3.1 Chemicals and enzyme**

Textile dyes: Reactive Black 5 (Remazol Black B), Reactive Yellow 15 (Remazol Yellow GR) and Reactive Red 239 (Remazol Brilliant Red 3BS) were kindly provided by DyStar (Portugal) and were used for degradation experiments without any further purification.

Enzyme: Commercial laccase formulation (DeniLite II S; 120 U/g) from genetically modified *Aspergillus* was kindly provided by Novozymes (Denmark). This formulation is used for indigo dye decolourization in denim finishing operations and includes a buffer and an enzyme-mediator.

### **IV. 2.3.2 Dye decolourization kinetics**

Real effluents often include more than one component. Once laccase catalyzed degradation has been tested on solutions of single reactive textile dyes, an attempt was made to determine the efficiency of decolourization of a mixture of dyes and to study the kinetics of this reaction. All the three dyes were mixed together in equal proportions to simulate a textile effluent. The conditions used in this work were exactly the same used to study the degradation kinetics of single dyes by commercial laccase (Cristóvão et al., 2008). To compare the kinetic constants of the single dye degradation reactions with the ones of the dye mixture degradation and to compare the dyes behaviours in both situations, the decolourization kinetics of the dye mixture reactions were studied under the maximum absorbance wavelength of each dye present in the mixture.

So, to study the kinetic behaviour of the dye mixture (with approximately equal amounts of each dye), five different concentrations of the mixture (from 50 mg/L to 125 mg/L) and 432 U/L of commercial laccase were incubated in 50 mL Erlenmeyer flasks at 35 °C with phosphate

buffer (50 mM/pH 7.0) under stirring. For each assay duplicate runs were made. After taking a zero sample, decolourization was started by the addition of laccase. Samples were withdrawn at certain time intervals and subsequently analyzed by UV–visible spectrophotometry.

### IV 2.3.3 Determination of dye degradation

Usually, the degradation of a single dye is presented as the percentage of absorbance reduction at the maximum absorbance wavelength. When studying a mixture of three different dyes, the spectrum of the solution presents three peaks. So, it seems appropriate to study also the total colour removal based on the overall visible spectrum.

Thus, the dye mixture decolourization by commercial laccase was determined by monitoring the decrease in the absorbance peak at the maximum absorbance wavelength of each dye, Reactive Black 5 (598 nm), Reactive Yellow 15 (416 nm) and Reactive Red 239 (542 nm), as well as by calculating the total area under the plot, by integration of the absorbance between 350 and 800 nm (Thermo model UV1, UV–visible spectrophotometer). Percent decolourization was calculated as  $(A_i - A_f)/A_i \times 100$ , where  $A_i$  is the initial absorbance at a given wavelength or the total area under the initial spectrum and  $A_f$  is the final absorbance of the dye or the total area under the final spectrum.

### IV. 2.3.4 Determination of dyes concentrations

Dyes concentrations were calculated from calibration curves by reading the absorbance of the samples at the maximum absorbance wavelength for each dye present in the mixture: Reactive Yellow 15 (416 nm), Reactive Red 239 (542 nm) and Reactive Black 5 (598 nm). A UV–visible spectrophotometer (Thermo model UV1) was used in all the experiments. By measuring the amount of the substrate remaining overtime it is possible to obtain the concentration vs. time plot which is known as progress curve of the enzymatic reaction or time course.

## IV 2.4 Kinetic modelling: optimization and simulation

### IV. 2.4.1 Kinetic models

To date, most kinetic studies of laccase catalyzed reactions involved the application of the Michaelis-Menten kinetic model (Gianfreda et al., 1998; Hofer and Schlosser, 1999; Ryan et al., 2003; Xu, 2001). This widely used model was developed based on assumed steps in which the free enzyme combines with the substrate to form an enzyme-substrate complex, which further dissociates into product and free enzyme as follows:



where  $E$ ,  $S$ ,  $ES$  and  $P$  are enzyme, substrate, enzyme-substrate complex and product, respectively.  $K_{MS}$  and  $k_2$  represent the Michaelis-Menten and the catalytic rate constants.

This approach has been successfully used to model the initial rates of several enzymatic reactions. However, the Michaelis-Menten approach to modelling the kinetics over an extended period seems to be rather limited. According to Cristóvão et al. (2008), the kinetics of the laccase catalyzed degradation of the single reactive dyes can be described by one of the following equations:

$$v = \frac{v_{max} [S]}{K_{MS} + [S]} \quad (\text{IV. 2.1})$$

$$v = \frac{v_{max} \left( [S] - \frac{[P]}{K_{eq}} \right)}{K_{MS} \left( 1 + \frac{[P]}{K_{MP}} \right) + [S]} \quad (\text{IV. 2.2})$$

$$v = \frac{v_{max} [S]}{K_{MS} + [S]} (1 - e^{-kt}) \quad (\text{IV. 2.3})$$

$$v = \frac{v_{max} \left( [S] - \frac{[P]}{K_{eq}} \right)}{K_{MS} \left( 1 + \frac{[P]}{K_{MP}} \right) + [S]} (1 - e^{-kt}) \quad (\text{IV. 2.4})$$

where  $v$  is the reaction rate,  $v_{max}$  is the maximum reaction rate,  $K_{eq}$  is the equilibrium constant of the catalytic reaction,  $K_{MP}$  is the Michaelis-Menten constant for the product,  $[S]$  and  $[P]$  are concentrations of the substrate and the product, respectively,  $k$  is the rate constant of the activation period of the laccase-mediator system and  $t$  is time.

Since these models are valid for the degradation of the single dyes RY15 (Equation (IV. 2.3)), RR239 (Equation (IV. 2.1)) and RB5 (Equation (IV. 2.4)) (Cristóvão et al., 2008), we tried to use the same models to describe the kinetics of the degradation of the dyes now mixed, simulating a real effluent.

#### IV. 2.4.2 Batch reactor balance

The differential equation obtained from the mass balance to the batch reactor is given by Equation (IV. 2.5).

$$-\frac{d[S]}{dt} = v \cdot W_E \cdot \frac{1}{V_L} \quad (\text{IV. 2.5})$$

where  $W_E$  is the enzyme mass and  $V_L$  is the volume of the reactor.

#### IV. 2.4.3 Estimation of the reaction kinetics and kinetic constants

As in a previous work (Cristóvão et al., 2008), the system of equations obtained from the batch reactor balance (Equation (IV. 2.5)) and from the proposed kinetics for the enzymatic reactions (Equations (IV. 2.1) - (IV. 2.4)) was solved using a Fortran program with integration by the LSODE code (Livermore Solver for Ordinary Differential Equations) based on Adams backward differentiation formulæ methods, to predict the profile of the dye concentrations versus time in the batch reactor. The initial concentrations of the dyes and first guesses of the parameters values were fed to the program. This program was combined with an optimization algorithm to estimate the kinetic constants of the proposed model by minimizing the difference between the predicted time courses and the ones obtained experimentally. The function to minimize between both time courses was the sum of squared relative residuals and was calculated as in Equation (IV. 2.6).

$$F = \sum_1^n \left| \frac{C_{calc} - C_{exp}}{C_{exp}} \right|^2 \quad (\text{IV. 2.6})$$

where  $C_{calc}$  is the concentration calculated using the model equation,  $C_{exp}$  is the experimental concentration and  $n$  is the total number of experimental and calculated points. The function was minimized through an optimization loop based on an adaptive random search algorithm that varies the values of the kinetic constants until a global minimum within the optimization criterion is achieved (Salcedo et al., 1990; Salcedo, 1992). This procedure was repeated for each dye present in the mixture.

### IV. 2.5 Results and Discussion

#### IV 2.5.1 Degradation of dye mixture

Laccase-mediator systems (LMS) were already described in some works for degradation processes of single reactive textile dyes (Mechichi et al., 2006; Murugesan et al., 2007; Peralta-Zamora et al., 2003). As real industrial effluents often contain several dyes, in this work three reactive textile dyes were mixed in order to evaluate the applicability of these processes to a real situation and submitted to commercial laccase catalyzed degradation. The

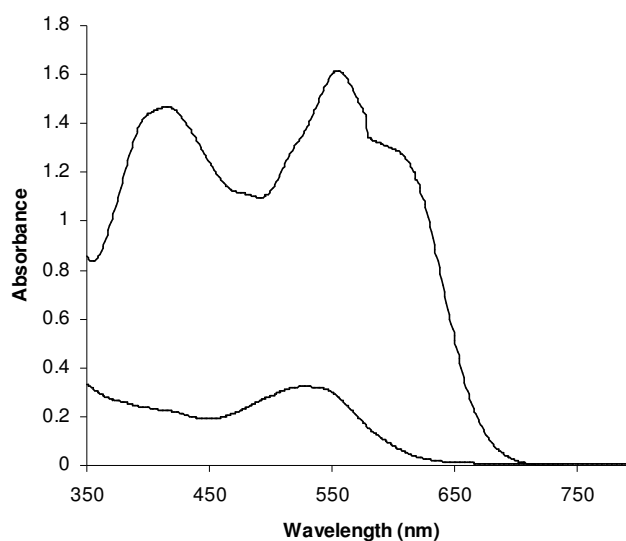
degradation of simulated effluents was already tested by other methods, such as ozonation (Sarayu et al., 2007), flocculation (Kang et al., 2007) and photodegradation (Zainal et al., 2006).

The decolourization of the dye mixture was evaluated by the percentage of absorbance reduction at the maximum absorbance wavelength of each dye present in the mixture as well as by the total colour removal based on all the visible spectrum. These results are presented in Table IV. 2.1 and show that significantly high amounts of colour were removed in both cases, at the maximum absorbance wavelength of each dye (above 76 % at 416 nm, above 71 % at 542 nm and above 89 % at 598 nm) and based on all the visible spectrum range, i.e., on the area under the curve (above 84 %). Figure IV. 2.1 represents the UV-visible absorbance spectrum of the mixed dyes before and after treatment and confirms the obtained results. Peaks in UV-visible region significantly decreased in the treated mixture. These results validate the applicability of the laccase catalyzed degradation method for the treatment of mixed dyes.

**Table IV. 2.1** - Dye mixture decolourization (%) based on the absorbance peak at maximum absorbance wavelength of each dye present in the mixture and on the area integration over all dye spectrum range.

[mixture] (mg/L)	% Decolourization			Area
	RY15 416 nm	RR239 542 nm	RB5 598 nm	
125	76.92 ± 0.10	78.44 ± 0.59	89.60 ± 0.43	85.01 ± 1.41
100	78.54 ± 0.48	77.42 ± 1.15	90.91 ± 0.26	84.10 ± 2.82
85	82.59 ± 0.62	76.26 ± 1.06	90.51 ± 0.05	87.49 ± 0.05
75	81.89 ± 0.19	71.90 ± 1.12	91.73 ± 0.23	88.33 ± 0.99
50	77.89 ± 0.78	68.23 ± 1.17	90.51 ± 0.36	90.55 ± 1.83

\*standard deviation



**Figure IV. 2.1** - Absorption spectrum of dye mixture before (a) and after (b) decolourization by commercial laccase at 125 mg/L.

The decolourization of dyes in the mixture is a relatively fast process, although to a lesser extent than when each dye is alone in solution (data not shown). This is probably due to some reasons: to the competition between several compounds for the active sites of the enzyme; to the enzyme deactivation; to the products of the polymerization that can provide unacceptable colour levels in effluents. According to Zille et al. (2005), the enzyme laccase can polymerize the reaction products obtained during the batch degradation processes with azo dyes. As the dye mixture degradation can have more reaction products than the single dyes one, probably this may affect the extent of the degradation.

#### **IV. 2.5.2 Kinetic modelling and estimation of kinetic constants**

In a previous work (Cristóvão et al., 2008) a kinetic model to simulate the decolourization of five individual reactive textile dyes in a batch reactor by a commercial laccase formulation was proposed. It was the first study on the determination of kinetic parameters of these reactions from the entire time course data. To our knowledge there is no study about the kinetics of degradation of a mixture of dyes.

Thus, as far as we are aware, since in this work the kinetics of degradation of a mixture of dyes by commercial laccase is investigated, this is the first study of the kinetics of these reactions and the first in which the kinetic constants of the enzymatic mixed dye decolourization are determined from the entire time course data.

In order to enable the comparison with the results of the individual dyes degradation, the kinetics of the dyes mixture degradation was studied at the maximum absorbance wavelength of each dye present in the mixture (416 nm, 542 nm and 598 nm). The proposed models to simulate the degradation of each dye in the mixture were the same proposed before to simulate the single dyes degradation.

At the wavelengths corresponding to the peaks of RB5 and of RY15, it was observed that the concentration almost do not decrease in the beginning, as seen in the individual degradations (Cristóvão et al., 2008). This period probably corresponds to an activation time of the laccase-mediator system. So, the kinetic model for the degradation of these dyes incorporates an exponential term to take into account this induction time. All the three dyes degradations were not complete, i.e., the dyes concentrations decrease along time until reaching a plateau where no more dye is degraded. In contrast, the degradation of the individual RR239 dye was complete, so, this dye exhibits a different behaviour when present in a mixture.

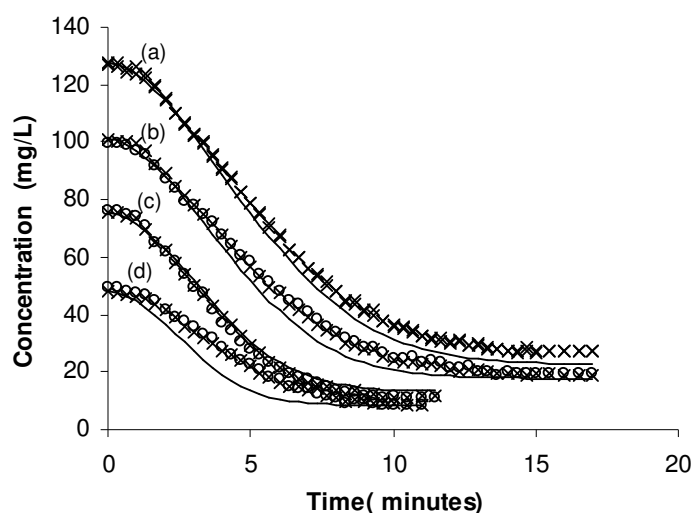
A program using the LSODE code to solve the differential equation of the batch reactor balance (Equation (IV. 2.5)) considering the proposed kinetics of enzymatic degradation of each dye present in the mixture (Equation (IV. 2.4) for RY15 and RB5 and Equation (IV. 2.2) for RR239) was combined with an optimization program (Salcedo et al., 1990; Salcedo, 1992) to obtain the theoretical time courses. As in the single dyes degradation case, the kinetic

constants were estimated by minimizing the difference between the predicted time courses and the experimentally obtained ones. The algorithm developed adjusts automatically the kinetic constants so that the output response (predicted by the model) and the input values (experimental data) are as close as possible according to the objective function (Equation (IV. 2.6)). This process was repeated while the relative errors between the estimated and the experimental values decreased.

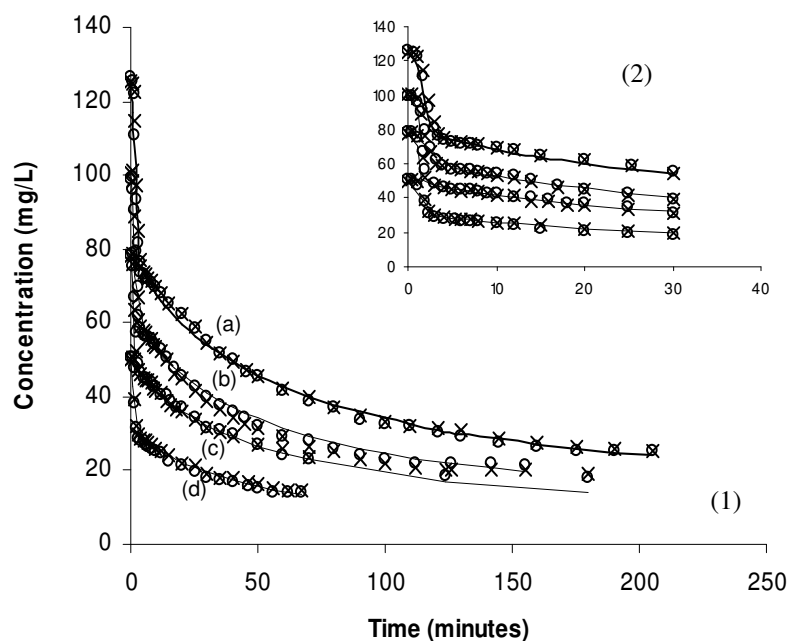
The obtained kinetic constants for each dye kinetic model are shown in Table IV. 2.2 and were used to draw the continuous lines in Figures IV. 2.2 – IV. 2.4, that represent the behaviour of each dye degradation when present in a mixture.

**Table IV. 2.2** – Proposed model, kinetic data and average sum of squared relative residuals (SSRR) of RY15, RR239 and RB5 degradation by commercial laccase when mixed together.

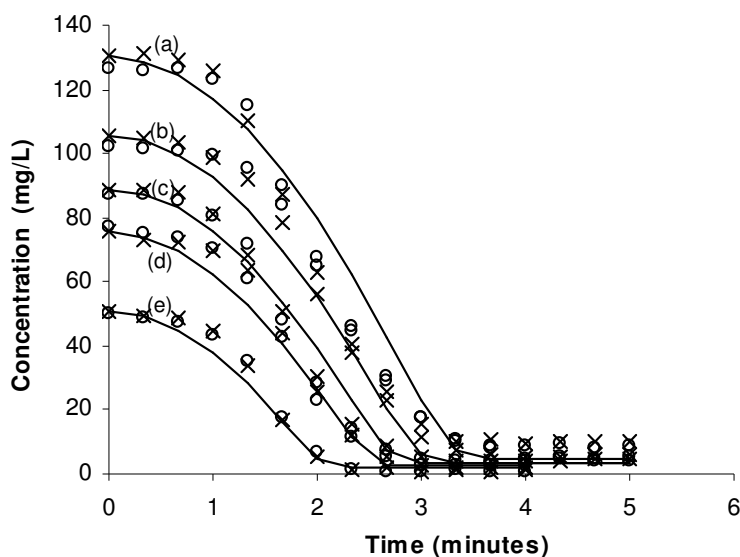
	<b>RY15 (416 nm)</b>	<b>RR239 (542 nm)</b>	<b>RB5 (598 nm)</b>
<b>Kinetic equation</b>	(IV. 2.4)	(IV. 2.2)	(IV. 2.4)
<b><math>v_{max}</math> (mg/g.min)</b>	5.534	4.450	152.370
<b><math>K_{MS}</math> (mg/L)</b>	8.636	743.18	0.795
<b><math>K_{MP}</math> (mg/L)</b>	67.200	22.9	100.000
<b><math>K_{eq}</math></b>	4.700	3.200	28.000
<b><math>k</math> (min<sup>-1</sup>)</b>	0.497	-	0.049
<b>SSRR/n</b>	$2.760 \times 10^{-2}$	$1.900 \times 10^{-3}$	0.183



**Figure IV. 2.2** – Comparison of experimental (× run 1; o run 2) and simulated (continuous line) time courses of RY15 degradation in a mixture of three dyes by commercial laccase under different dye initial concentrations: (a) 127.7 mg/L and 126.9 mg/L; (b) 101.1 mg/L and 99.5 mg/L; (c) 75.4 mg/L and 75.9 mg/L; (d) 48.2 mg/L and 49.8 mg/L.



**Figure IV. 2.3** – Comparison of experimental ( $\times$  run 1;  $\circ$  run 2) and simulated (continuous line) time courses of RR239 degradation in a mixture of three dyes by commercial laccase under different dye initial concentrations: (a) 125.1 mg/L and 126.3 mg/L; (b) 100.5 mg/L and 99.1 mg/L; (c) 78.0 mg/L and 78.20 mg/L; (d) 50.0 mg/L and 50.4 mg/L. (2) Scale amplification of (1).



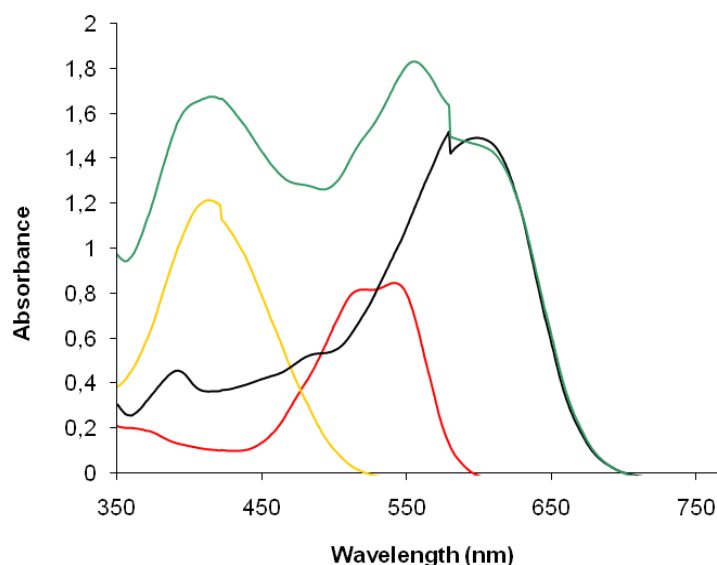
**Figure IV. 2.4** - Comparison of experimental ( $\times$  run 1;  $\circ$  run 2) and simulated (continuous line) time courses of RB5 degradation in a mixture of three dyes by commercial laccase under different dye initial concentrations: (a) 130.3 mg/L and 126.2 mg/L; (b) 105.5 mg/L and 101.9 mg/L; (c) 88.9 mg/L and 87.1 mg/L; (d) 75.5 mg/L and 76.8 mg/L; (e) 50.6 mg/L and 50.3 mg/L.



According to Cristóvão et al. (2008), in this reaction of dye catalyzed degradation by commercial laccase, the  $K_{MS}$  constant is the equilibrium constant of the enzyme-mediator/substrate complex decomposition. So, it is a measure of the enzyme-mediator system affinity to the substrate. The lesser the value of  $K_{MS}$ , the larger is the affinity of the enzyme-mediator system to the substrate. Comparing the  $K_{MS}$  values of each dye of the mixture (Table IV. 2.2), the laccase-mediator system affinities for the dyes decrease according to the following order: RB5 > RY15 > RR239, as when they are not mixed. A larger dyes degradation time corresponds to a more difficult decolourization (less affinity of the laccase-mediator system for the dye), thus the conclusion about the laccase-mediator system affinities for the dyes is easy to confirm in Figures IV. 2.2 – IV. 2.4, by the time that each dye takes to reach the equilibrium. The rates of the dyes degradation in the mixture can also be assessed by the value of  $v_{max}$  – the theoretical maximum velocity. According to the values of  $v_{max}$  shown in Table IV. 2.2 for each dye present in the mixture, the degradation rate decreases in the following order: RB5 > RY15 > RR239, in agreement with the previous observation.

It is also possible to evaluate the activation rate of the laccase-mediator system on the RB5 and RY15 dyes degradations by the  $k$  values presented in Table IV. 2.2. According to the displayed results, the activation of the laccase-mediator system is faster in the RY15 than in the RB5 degradation, contrarily to what was observed when dealing with the individual dyes (Cristóvão et al., 2008).

For the RR239 degradation, a different behaviour was observed, which had never occurred before. The concentration decreases almost instantly in the first minutes and then decreases slowly, showing a kind of elbow, as can be observed from Figure IV. 2.3. Looking at the spectrum of the single dyes and of their mixture, presented in Figure IV. 2.5, it is possible to conclude that at 542 nm (maximum absorbance wavelength of RR239) the mixture absorbance is the sum of RR239 and RB5 absorbances, representing approximately 46 % and 54 % of each, respectively. So, during the degradation at 542 nm, it is observed first the degradation of RB5 dye, that is faster than the degradation of the RR239 (corresponding to the sharp decolourization in the first few minutes) and only after that, the degradation of the RR239 dye is observed. Therefore, to simulate the RR239 decolourization, it is necessary to take into account that initially the decolourization of the RB5 is also present. Then, this initial decolourization is simulated with the decolourization of the RB5 and of the RR239 at 542 nm. The RB5 decolourization at 542 nm was simulated taking into account that the RB5 absorbance at 542 nm is 66% of the absorbance at 598 nm (Figure IV. 2.5), whose kinetic parameters are known.



**Figure IV. 2.5** - Absorption spectrum of singles dyes (RY15 (–), RR239 (–), RB5 (–)) and of the dyes mixture (–) before degradation by commercial laccase.

In order to evaluate the adequacy of the proposed models for the kinetics of dye decolourization by commercial laccase when present in a dyes mixture, the time courses calculated by the kinetic models were compared with the experimental ones. These comparisons for RY15, RR239 and RB5 degradations are displayed in Figures IV. 2.2 – IV. 2.4, respectively. In order to avoid the overloading of the respective graphs, only four different concentrations are presented for the RY15 and RR239 cases.

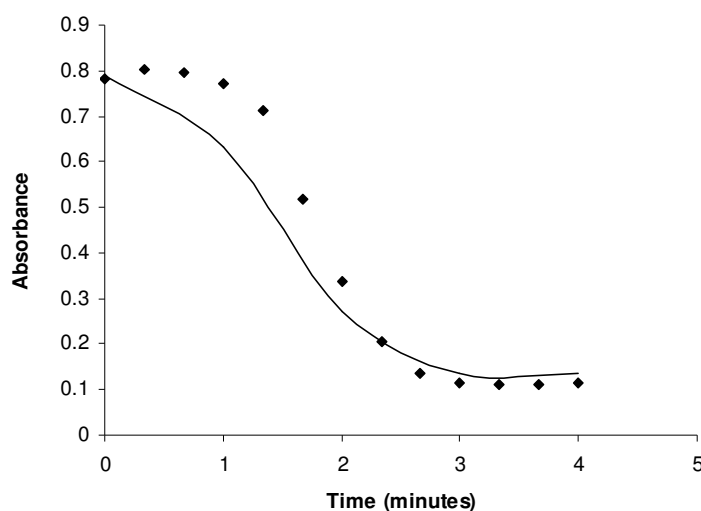
The proposed models seem to exhibit some systematic quantitative deviations, probably due to the subtraction of the turbidity induced by the enzyme support, since apparent colour is not very reproducible (Cristóvão et al., 2008). Nonetheless, the close correspondence of the experimental data with the simulated values under different substrate concentrations seems to demonstrate that the proposed mathematical models are able to describe with remarkable accuracy the RY15, RR239 and RB5 laccase catalyzed degradations when they are mixed.

In this context, it is possible to conclude that the models can also be applied when the commercial laccase is used for the degradation of mixtures of reactive dyes, although the values of the kinetic constants are different of those obtained when dealing with the single dyes degradation systems.

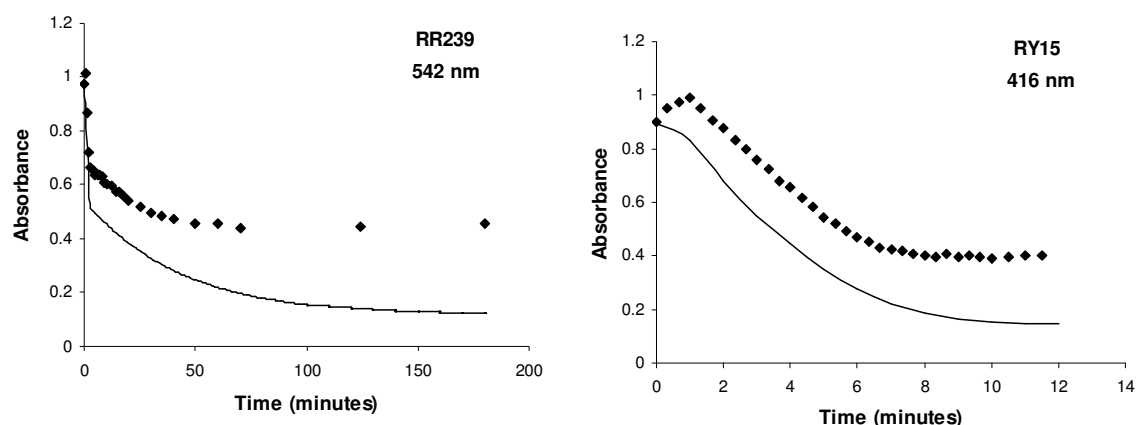
Comparing the kinetic constants values of the single dyes decolourization models (Cristóvão et al., 2008) with the ones of the decolourization of the same dyes when present in a mixture (this work), it is clear that they are very different and that probably it is not possible to simulate the degradation of the single dyes with the kinetic parameters obtained for the degradation of the dyes in a mixture and vice versa. When mixed, the RB5 and RR239 dyes present a higher degradation rate ( $v_{max}$ ), while the RY15 dye presents a lower velocity of

degradation than when they are separated. The laccase-mediator system affinity for the RB5 dye is the highest in the degradation of the single dyes, but it presents more affinity to RY15 and RR239 dyes when they are mixed. It is also possible to compare the activation rates of the laccase-mediator system in the dyes degradation in both situations. So, in the RB5 degradation case, this activation rate is greater when it is alone in solution, contrarily to what happens to the RY15 dye. The degradation of the RR239 dye does not present laccase-mediator system activation in both cases studied. Furthermore, RB5 is the only dye that fits the same kinetic model in both situations. The degradations of single dye solutions of RY15 and RR239 are complete, contrarily to what happens when they are in a mixture.

In order to assess the ability of the models developed for the single dyes in the prediction of the degradation of a mixture of dyes, the time responses of each dye predicted by the individual models were evaluated and summed for each of the characteristic wavelengths. The comparison of these predictions with the actual results shows that the models are able to reproduce the general qualitative behaviour. Nonetheless, when the quantitative results are compared the predictions are far from reasonable. The best case is observed when dealing with the black dye (RB5) where the experimental results observed at the respective wavelength (598 nm) are close to the sum of the predictions of the three dyes mixed at the same wavelength is displayed in Figure IV. 2.6. As referred to above, the results for the other two wavelengths, characteristic for the RY15 and RR239 dyes, is worse, even if qualitatively correct, as shown in Figure IV. 2.7.



**Figure IV. 2.6** – Simulation of the mixture degradation with commercial laccase at the maximum wavelength of RB5 (◆) with the kinetic model of the single dye degradation (continuous line).



**Figure IV. 2.7** – Simulation of the mixture degradation with commercial laccase at the maximum wavelength of RR239 (◆) and of RY15 (◆) with the kinetic models of the singles dye degradation (continuous lines).

## IV. 2.6 Conclusions

The degradation of a mixture of reactive dyes, simulating a real textile effluent, catalyzed by commercial laccase, was tested. The good results of decolourization as measured by the percentage of absorbance reduction at the maximum absorbance wavelength of each dye present in the mixture (above 76 % at 416 nm, above 71 % at 542 nm and above 89 % at 598 nm) and by the total colour removal based in all the visible spectrum (above 84 %), indicates the possibility of implementing this technique for the treatment of textile dyeing wastewaters.

A kinetic model to simulate the decolourization by commercial laccase of each of the three reactive textile dyes mixed in a batch reactor was proposed. The kinetic parameters estimation was performed by minimization of the sum of the squared relative residuals between the experimental and the predicted time courses. The good agreement between the experimental and simulated results validates the applicability of the proposed models in predicting the kinetic behaviour of mixed reactive dyes degradation by commercial laccase. These kinetic models provide a useful tool for the design and optimization of textile effluents treatment, using this process.

Comparing the kinetic models and the kinetic constants values, it is possible to conclude that a single reactive dye degradation catalyzed by commercial laccase and the same dye degradation but mixed with other reactive dyes present different behaviours.

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## **Part IV. 3** Treatment and kinetic modelling of a simulated dye house effluent by enzymatic catalysis\*

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*\*based on: Cristóvão, R.O., Tavares, A.P.M., Loureiro, J.M., Boaventura, R.A.R., Macedo, E.A., 2009. Treatment and kinetic modelling of a simulated dye house effluent by enzymatic catalysis. Bioresource Technology, 100, 6236-6242.*





## **IV. 3 Treatment and kinetic modelling of a simulated dye house effluent by enzymatic catalysis**

### **IV. 3.1 Abstract**

Biocatalytic treatment of a synthetic dye house effluent, simulating a textile wastewater containing various reactive dyestuffs (Reactive Yellow 15, Reactive Red 239 and Reactive Black 5) and auxiliary chemicals, was investigated in a batch reactor using a commercial laccase. A high decolourization (above 86 %) was achieved at the maximum wavelength of Reactive Black 5. The decolourization at the other dyes wavelengths (above 63 % for RY15 and around 41 % for RR239) and the total decolourization based on all the visible spectrum (around 55 %) were not so good, being somewhat lower than in the case of a mixture of the dyes (above 89 % for RB5, 77 % for RY15, 68 % for RR239 and above 84 % for total decolourization). Even so, these results suggest the applicability of this method to treat textile dyeing wastewaters. Kinetic models were developed to simulate the synthetic effluent decolourisation by commercial laccase. The kinetic constants of the models were estimated by minimizing the difference between the predicted and the experimental time courses. The close correlation between the experimental data and the simulated values seems to demonstrate that the models are able to describe with remarkable accuracy the simulated effluent degradation. Water quality parameters such as TOC, COD, BOD<sub>5</sub> and toxicity were found to be under the maximum permissible discharge limits for textile industries wastewaters.

### **IV. 3.2 Introduction**

Large amounts of dyes are annually produced and applied in many different industries, including the textile, cosmetic, paper, leather, pharmaceutical and food industries. The textile industry accounts for two-thirds of the total dyestuff market (Asad et al., 2007). A large proportion of reactive azo dyes is consumed due to the actual high demand for cotton fabrics with brilliant colours. A significant fraction of the dye is hydrolysed and released into the environment with the rejected dye baths or wash waters. The effluents from reactive dye baths have highly coloured streams and contain unutilized, hydrolysed dyes, as well as salts, sizing agents and auxiliary chemicals (Alaton et al., 2002). These effluents are of great priority once they are toxic for several organisms and a threat to ecosystems. They block out the sunlight and thus reduce photosynthesis and dissolved oxygen concentration (Aksu, 2005). Taking into account the new strict rules for the protection of the environment which are implemented by most countries around the world, measures have to be taken by the textile industry. The organic nature of a textile wastewater can be addressed in terms of classical parameters such as BOD<sub>5</sub>, COD and TOC.

Some physical and chemical treatments are effective, but their limitations render them unattractive. These include excessive usage of chemicals, accumulation of concentrated sludge with obvious disposal problems, expensive plant requirements, high operational costs and sensitivity to variations in the wastewater input (Aksu, 2005). Enzymatic degradation is viewed as one alternative. Laccase (benzendiol:oxygen oxidoreductase, EC 1.10.3.2) and laccase-producing fungi were studied in the oxidation of textile dyes (Ramsay and Nguyen, 2002; Soares et al., 2002; Tavares et al., 2008, 2009a,b). Studies showed that the range of substrate specificity of laccases can be extended to non-phenolic substrates by addition of redox mediators (Tavares et al., 2008, 2009a,b). The degradation of simulated effluents was already tested by other methods, such as nanofiltration (Avlonitis et al., 2008), photocatalysis (Arslan et al., 2000) and electrochemical oxidation (López-Grimau and Gutiérrez, 2006). Limited data are available on the action of laccase over simulated real effluent degradation but it is important to evaluate the feasibility of this method to treat real textile effluents. In a preliminary work, we studied the effects of several operating conditions (pH, temperature and enzyme mass) on separated dyes degradation (Tavares et al., 2009a). After that we studied the applicability of the laccase degradation method for the treatment of a mixture of three dyes (Cristóvão et al., 2009). An understanding of the kinetics of enzyme systems is essential for the design of efficient reactors to carry out industrial processes as well as for optimization and control purposes. There are some works that report the values of kinetic constants of enzymatic dye degradation (Almansa et al., 2004; Moldes and Sanroman, 2006), but to our knowledge, apart from our previous studies (Cristóvão et al., 2008, 2009), there was no other study that determined the kinetic constants of enzymatic dye degradation from the entire time course data.

In the present work, commercial laccase was used for an experimental and modelling study on the degradation of a simulated real effluent, containing a mixture of three reactive textile dyes and other auxiliary chemicals, in the perspective of an industrial application of the process. Besides these studies, to investigate the environmental impact of this process, the total organic carbon (TOC), the chemical oxygen demand (COD), the biochemical oxygen demand (BOD<sub>5</sub>) and the toxicity of the simulated effluent were evaluated, before and after treatment.

## **IV. 3.3 Materials and Methods**

### **IV. 3.3.1 Chemicals and enzyme**

Textile dyes: Reactive Black 5 (Remazol Black B), Reactive Yellow 15 (Remazol Yellow GR) and Reactive Red 239 (Remazol Brilliant Red 3BS) were kindly provided by DyStar (Portugal) and were used for degradation experiments without any further purification.

Enzyme: Commercial laccase formulation (DeniLite II S; 120 U/g) from genetically modified *Aspergillus* was kindly provided by Novozymes (Denmark). This formulation is used for

indigo dye decolourization in denim finishing operations and includes a buffer and an enzyme–mediator.

#### **IV. 3.3.2 Simulated real effluent preparation**

To mimic the effluent produced by typical textile industries using reactive dyes, a synthetic dye effluent was prepared. This simulated effluent was used in biodegradation experiments to evaluate the effect of the presence of dyeing auxiliary chemicals and salts on the biodegradation performance. Its preparation involved a first step where a dye bath with the three reactive textile dyes was simulated based on a standard exhaust procedure of non mercerised cotton as suggested by the dye supplier: 50 g/L of NaCl were dissolved in warm tap water and 1.0 g/L of each of the auxiliaries Sera Wet C-AS (anionic wetting agent), Sera Lube M-CF (a non-ionic nature crease inhibitor and lubricant agent) and Sera Quest M-PP (anionic sequestrant) were added. The desired amount of a mixture of three reactive textile dyes (from 50 mg/L to 125 mg/L, with equal proportions of each dye) was then carefully dissolved at 60 °C for 20 min. 2 g/L of NaOH and 10 g/L of Na<sub>2</sub>CO<sub>3</sub> were added and the solution was maintained at constant temperature for 1 h more. Taking into account the dyeing process and the following rinse and softening baths steps industrially used, an estimated dilution of the dye bath in the final effluent by a factor of eight was considered fair. Using this hypothesis, the prepared dye bath was then accurately diluted and neutralized for use in biotreatment experiments.

The complex effluent was employed since industrial effluents usually contain a mixture of dyes derivating from the baths of different machines. Moreover all the dyes were dissolved in saline solution since textile effluents are usually characterised by high salt concentrations. This solution fed to the reactor was also previously hydrolysed to simulate dye bath conditions used in the textile industry.

#### **IV. 3.3.3 Simulated effluent decolourization kinetics**

The conditions used in this work were exactly the same used to study the degradation kinetics of the dye mixture by commercial laccase (Cristóvão et al., 2009). To compare the kinetic constants of the dye mixture degradation reaction with the ones of the simulated effluent degradation, the degradation kinetics were studied at the same wavelengths.

So, to study the kinetic behaviour of the simulated effluent, five different concentrations of the dyes (from 50 mg/L to 125 mg/L) and 432 U/L of commercial laccase were incubated in 50 mL Erlenmeyer flasks at 35 °C with phosphate buffer (50 mM/pH 7.0) under stirring. For each assay duplicate runs were made.

After withdrawing samples at 0h, degradation was started by the addition of laccase. Samples were withdrawn at certain time intervals and subsequently analyzed by UV–visible spectrophotometry.

#### IV. 3.3.4 Determination of simulated effluent degradation

Since the degradation of a simulated effluent containing a mixture of three dyes is to be studied, it seems appropriated to study not only the degradation as the percentage of absorbance reduction at the maximum absorbance wavelength of each dye, but also the total colour removal based on the residual absorbance over all the visible spectrum.

The simulated effluent degradation by commercial laccase was determined by monitoring the decrease in the absorbance peak at the maximum absorbance wavelength of each dye, Reactive Yellow 15 (416 nm), Reactive Red 239 (542 nm) and Reactive Black 5 (598 nm), as well as by calculating the total area under the plot, by integration of the absorbance between 350 and 800 nm (Thermo model UV1, UV–visible spectrophotometer). Percent decolourization was calculated as  $(A_i - A_f)/A_i \times 100$ , where  $A_i$  is the initial absorbance at a given wavelength or the total area under the initial spectrum and  $A_f$  is the final absorbance of the dye or the total area under the final spectrum.

#### IV. 3.3.5 Determination of dyes concentrations

Dyes concentrations were calculated from calibration curves by reading the absorbance of the samples at the maximum absorbance wavelength of each dye present in the effluent. UV–visible spectrophotometer (Thermo model UV1) was used in all the experiments. By measuring the amount of the substrate remaining overtime it is possible to obtain the concentration vs. time plot which is known as time course. Equilibrium was considered to be achieved when no significant changes in the concentration were detected.

### IV. 3.4 Kinetic modelling: optimization and simulation

#### IV. 3.4.1 Kinetic models

Most kinetic studies of laccase catalyzed reactions involved the application of the Michaelis–Menten kinetic model (Gianfreda et al., 1998; Hofer and Schlosser, 1999; Ryan et al., 2003; Xu, 2001). According to Cristóvão et al. (2009), the kinetics of the laccase catalyzed degradation of a mixture of dyes can be described by the following equations based on Michaelis–Menten equation:

$$v = \frac{v_{max} [S]}{K_{MS} + [S]} \quad (\text{IV. 3.1})$$

$$v = \frac{v_{max} \left( [S] - \frac{[P]}{K_{eq}} \right)}{K_{MS} \left( 1 + \frac{[P]}{K_{MP}} \right) + [S]} \quad (\text{IV. 3.2})$$

$$v = \frac{v_{max} [S]}{K_{MS} + [S]} (1 - e^{-kt}) \quad (\text{IV. 3.3})$$

$$v = \frac{v_{max} \left( [S] - \frac{[P]}{K_{eq}} \right)}{K_{MS} \left( 1 + \frac{[P]}{K_{MP}} \right) + [S]} (1 - e^{-kt}) \quad (\text{IV. 3.4})$$

where  $v$  is the reaction rate,  $v_{max}$  is the maximum reaction rate,  $K_{eq}$  is the equilibrium constant of the catalytic reaction,  $K_{MS}$  and  $K_{MP}$  are the Michaelis–Menten constants for the substrate and for the product, respectively,  $[S]$  and  $[P]$  are concentrations of the substrate and the product, respectively,  $k$  is the rate constant of the activation period of the laccase–mediator system and  $t$  is time. Since these models are valid for the degradation of a mixture of dyes: RY15 (Equation (IV. 3.4)), RR239 (Equation (IV. 3.2)) and RB5 (Equation (IV. 3.4)) (Cristóvão et al., 2009), we tried to use the same models to describe the kinetics of the degradation of the simulated effluent.

#### IV. 3.4.2 Batch reactor balance

The differential equation obtained from the mass balance to the batch reactor is given by Equation (IV. 3.5):

$$-\frac{d[S]}{dt} = v \cdot W_E \cdot \frac{1}{V_L} \quad (\text{IV. 3.5})$$

where  $W_E$  is the enzyme mass and  $V_L$  is the volume of the reactor.

#### IV. 3.4.3 Estimation of the reaction kinetics and kinetic constants

As in previous works (Cristóvão et al., 2008, 2009), the system of equations obtained from the batch reactor balance (Equation (IV. 3.5)) and from the proposed kinetics for the enzymatic reactions (Equations (IV. 3.1) – (IV. 3.4)) was solved using a Fortran program with integration by the LSODE code (Livermore Solver for Ordinary Differential Equations) based on Adams backward differentiation formulae methods, to predict the profile of the effluent

concentrations versus time in the batch reactor. The initial concentrations of the effluent and first guesses of the parameters values were fed to the program. This program was combined with an optimization algorithm to estimate the kinetic constants of the proposed model by minimizing the difference between the predicted time courses and the ones obtained experimentally. The function to minimize between both time courses was the sum of squared relative residuals and was calculated as in Equation (IV. 3.6):

$$F = \sum_1^n \left| \frac{C_{calc} - C_{exp}}{C_{exp}} \right|^2 \quad (IV. 3.6)$$

where  $C_{calc}$  is the concentration calculated using the model equation,  $C_{exp}$  is the experimental concentration and  $n$  is the total number of experimental and calculated points. The function was minimized through an optimization loop based on an adaptive random search algorithm that varies the values of the kinetic constants until a global minimum within the optimization criterion is achieved (Salcedo et al., 1990; Salcedo, 1992). This procedure was repeated for each dye present in the effluent.

### IV. 3.5 Analytical methods

The routine analysis of conventional wastewater parameters are necessary in order to monitor the quality of effluents and to decide its further reuse or discharge. So, water quality analyses such as TOC, COD and BOD were made.

#### IV. 3.5.1 Total organic carbon

Following the reduction in TOC it is possible to evaluate the mineralization of the simulated effluent. The TOC was determined by catalytic oxidation followed by quantification of the  $\text{CO}_2$  formed through infra-red spectrometry, as described in Method No. 5310 of the Standard Methods for the Examination of Water and Wastewater (APHA, AWWA, WEF, 1998). For that, a Shimadzu 5000A TOC analyser was used. TOC values reported represent the average of at least two measurements; in most cases each sample was injected three times, validation being performed by the apparatus only if the coefficient of variation (CV) is smaller than 2 %.

#### IV. 3.5.2 Chemical oxygen demand

COD is often used as a measurement of pollutants in wastewater and natural waters. COD was determined by colourimetric measurement after closed reflux digestion (APHA, AWWA, WEF, 1998), carried out in a MERCK spectroquant, model TR 420.

### IV. 3.5.3 Biochemical oxygen demand

The BOD is used to determine the relative oxygen requirements for the biodegradation of wastewaters effluents and polluted waters. BOD<sub>5</sub> (biochemical oxygen demand in a 5-days test period at 20 °C) was quantified by the dilutions method (APHA, AWWA, WEF, 1998). The concentration of dissolved oxygen was measured with a Crison O<sub>2</sub> meter electrode, model oxi45.

### IV. 3.5.4 Toxicity

The toxicity of simulated effluent was determined using the bioluminescent bacterium *Vibrio fischeri* before and after the decolourization, by measuring the reduction of light production due to interactions between bacteria and toxic compounds (Dutka et al., 1991). The test is standardized for water and effluent samples (ISO 11348-3, 1998), but the toxicity assessment of colourful and turbid samples with this method is complicated or impossible due to the interferences in the measurement. According to Lappalainen et al. (1999, 2001) the toxicity of that highly colourful samples can be measured with kinetic Flash method using, also, the luminescent *V. fischeri*. In this method, each sample acts as a reference for itself.

The toxicity of the simulated effluent was evaluated by this bioluminescence test in Toxicity Analyzer Microtox 2055, according to the Microtox acute toxicity basic test procedure. All samples were serially diluted in 2 % w/v NaCl, and each assay was performed in duplicate at pH 7.0, 15 °C. Sodium chloride (2 % w/v) was used as the negative control. For colour correction the bacteria were dispensed into the sample and the signal was recorded continuously. The maximum signal received after immediately dispensing was compared to the signal after an incubation period. The sample concentrations that inhibited 20 % and 50 % of the light output (EC<sub>20</sub> and EC<sub>50</sub>, respectively) were determined after a 5 and 15 min. exposure times. Phenol was used as the positive control with EC<sub>20</sub> ranging from 3 to 6 mg/L and EC<sub>50</sub> from 13 to 26 mg/L.

## IV. 3.6 Results and Discussion

### IV. 3.6.1 Degradation of the simulated effluent

A simulated effluent containing three reactive textile dyes, salts and dyeing auxiliary chemicals was used in equilibrium and kinetic experiments, in order to evaluate the applicability of the degradation process of textile effluents by commercial laccase to a real situation. An artificial reactive dye bath was prepared due to three reasons: firstly, it enables research to be carried out in the absence of a local source of effluent; secondly, simulated effluents have a constant composition and, hence, enable the effect of treatment to be more readily understood; and thirdly, from the practical point of view it is of utmost importance to assess the treatment

performance of the selected treatment systems in the presence of several dye assisting chemicals since reactive dyes are always found in the form of an “exhausted” dye bath formulation.

The degradation of the simulated real effluent by commercial laccase was evaluated by the percentage of absorbance reduction at the maximum absorbance wavelength of each dye present in the effluent as well as by the total colour removal based on all the visible spectrum. These results are presented in Table IV. 3.1 and show that the degradation is more pronounced at the RB5 maximum wavelength. At this wavelength decolourization above 86 % was observed. At the maximum wavelength of RY15 it was also observed a good decolourization (above 63 %), but at 542 nm (corresponding to RR239) a worse decolourization was observed: only around 41 %. The total degradation based on all the visible spectrum range presented values in order of 55 %. These decolourizations were lower than those obtained with the mixture of dyes only (above 89 % for RB5, 77 % for RY15, 68 % for RR239 and above 84 % for total decolourization) (Cristóvão et al., 2009) due to the presence of salts and auxiliary chemicals. Probably happens one or more of the following things: the formation of strong chemical bonds with the species involved in the degradation process, the creation of products during the process or even because of enzyme deactivation.

**Table IV. 3.1** – Simulated effluent degradation (%) based on the absorbance peak at maximum wavelength of each dye present in the effluent and on the area integration over all spectrum range.

[effluent] (mg/L)	% Degradation			Area
	RY15 416 nm	RR239 542 nm	RB5 598 nm	
125	64.96 ± 1.74*	39.92 ± 0.69	86.41 ± 0.50	59.57 ± 0.72
100	63.38 ± 0.59	42.90 ± 0.05	87.36 ± 0.04	60.53 ± 0.35
85	63.84 ± 0.98	41.66 ± 0.13	87.65 ± 0.28	55.09 ± 0.24
75	64.86 ± 0.22	40.82 ± 1.36	87.45 ± 0.70	54.29 ± 2.27
50	63.82 ± 0.17	42.04 ± 0.34	87.33 ± 0.16	49.99 ± 0.50

\*Standard deviation

The laccase catalyzed degradation showed to be an interesting treatment method for a mixture of dyes but its performance is a little worse when treating real textile dyeing effluents. Nonetheless, the presented results show that this method could be used for treating textile dyeing wastewaters, particularly as a polishing process for water recycling.

#### IV. 3.6.2 Kinetic modelling and estimation of kinetic constants

In previous works, kinetic models to simulate the decolourization of individual reactive textile dyes (Cristóvão et al., 2008) and of a dye mixture (Cristóvão et al., 2009) in batch reactors by commercial laccase formulation containing a specific mediator were proposed. In this work, the kinetics of degradation of a simulated effluent is investigated, using the same models previously established as above mentioned. It was the first study on the determination



of kinetic parameters of these reactions from the entire time course data. To our knowledge there is no study about the kinetics of degradation of a simulated textile effluent.

The kinetics of the simulated effluent degradation was studied at the maximum wavelength of each dye in the effluent, in order to enable the comparison with the results of the dye mixture degradation. The kinetic constants of the proposed models were estimated by comparing the experimental time courses with the predicted ones for each wavelength studied.

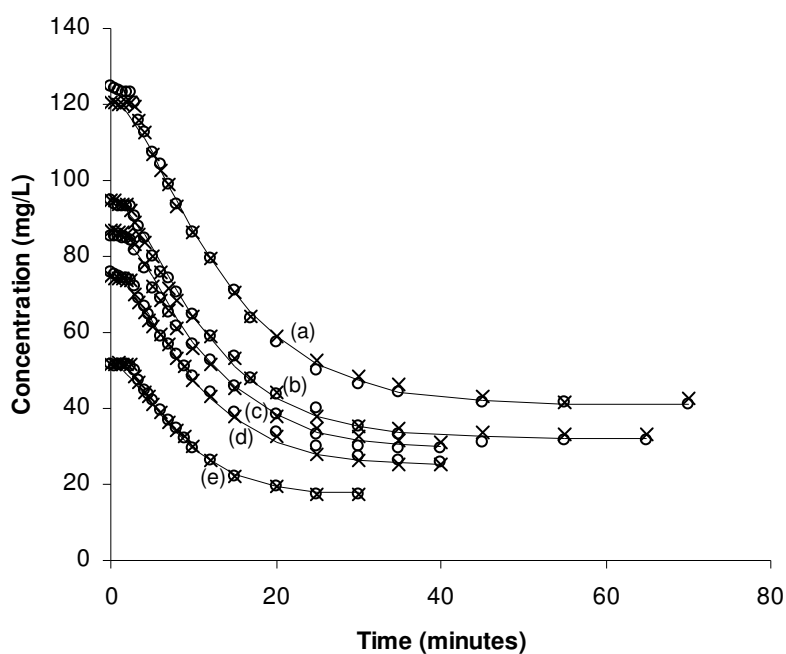
Experimental time courses were obtained in duplicate at five different initial effluent concentrations for each wavelength. It was observed for all the wavelengths studied that initially the concentration almost do not decrease, which probably corresponds to the activation time of the laccase–mediator system. However these initial periods vary depending on the wavelength, being more (598 nm) or less (416 nm) pronounced. Then, the kinetic models must present an exponential term to predict these induction times. These reactions are not complete at any of the wavelengths. The concentrations decreased along time until reaching a plateau where no more effluent was degraded. However, at the wavelength corresponding to the RB5 the reaction was almost complete, which is in accordance with the degradation observed (above 86 %). Comparing these results with the ones obtained for the dye mixture (Cristóvão et al., 2009), it was possible to observe that the degradations exhibit similar behaviours at 416 nm and at 598 nm. At 542 nm the behaviour is a little different. This was probably due to the presence of other substances in the effluent.

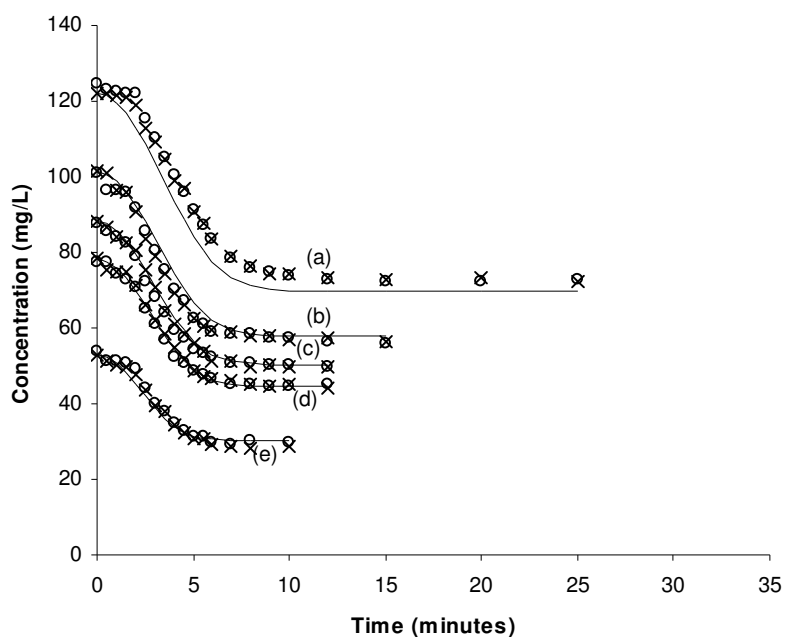
As in the other cases, a program using the LSODE code to solve the differential equation of the batch reactor balance (Equation (IV. 3.5)) considering the proposed kinetics for the enzymatic degradation of the simulated effluent at the wavelengths of each dye in the effluent (Equation (IV. 3.4) for all the wavelengths) was combined with an optimization program (Salcedo et al., 1990; Salcedo, 1992) to obtain the theoretical time courses. The kinetic constants were estimated by minimizing the difference between the predicted time courses and the experimentally obtained ones. The developed algorithm adjusts automatically the kinetic constants so that the output response (predicted by the model) and the input values (experimental data) are as close as possible according to the objective function (Equation (IV. 3.6)). This process was repeated while the relative errors between the estimated and the experimental values decreased.

The obtained kinetic constants for the kinetic models at each wavelength are shown in Table IV. 3.2 and were used to draw the continuous lines in Figures IV. 3.1 – IV. 3.3, that represent the behaviour of the effluent degradations at each wavelength.

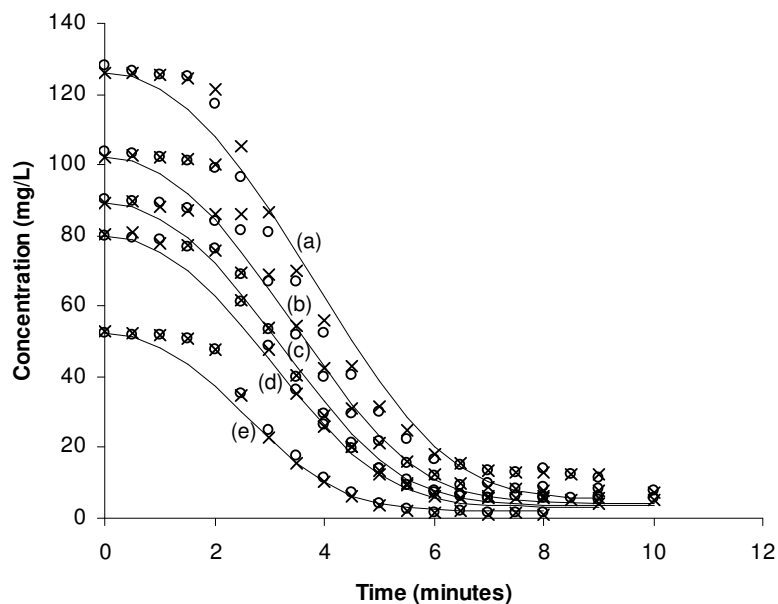
**Table IV. 3.2** - Proposed model, kinetic data and average sum of squared relative residuals (SSRR) of RY15, RR239 and RB5 degradation by commercial laccase when in a simulated effluent.

	<b>RY15 (416 nm)</b>	<b>RR239 (542 nm)</b>	<b>RB5 (598 nm)</b>
<b>Kinetic equation</b>	(IV. 3.4)	(IV. 3.4)	(IV. 3.4)
<b><math>v_{max}</math> (mg/g.min)</b>	10.0	19.7	58.0
<b><math>K_{MS}</math> (mg/L)</b>	10.0	8.1	7.0
<b><math>K_{MP}</math> (mg/L)</b>	2.43	372.3	49.0
<b><math>K_{eq}</math></b>	1.95	0.752	23.2
<b><math>k</math> (min<sup>-1</sup>)</b>	0.044	0.075	0.050
<b>SSRR/n</b>	$6.90 \times 10^{-4}$	$1.14 \times 10^{-3}$	$8.19 \times 10^{-2}$

**Figure IV. 3.1** - Comparison of experimental (x, run 1; o run 2) and simulated (continuous line) time courses of RY15 degradation in a simulated effluent by commercial laccase under different initial concentrations: (a) 120.5 mg/L and 124.7 mg/L; (b) 94.7 mg/L and 94.8 mg/L; (c) 86.8 mg/L and 85.4 mg/L; (d) 74.6 mg/L and 75.5 mg/L; (e) 51.4 mg/L and 51.5 mg/L.



**Figure IV. 3.2** - Comparison of experimental (x, run 1; o run 2) and simulated (continuous line) time courses of RR239 degradation in a simulated effluent by commercial laccase under different initial concentrations: (a) 122.2 mg/L and 124.9 mg/L; (b) 101.3 mg/L and 101.1 mg/L; (c) 88.1 mg/L and 87.8 mg/L; (d) 78.3 mg/L and 77.4 mg/L; (e) 53.0 mg/L and 53.6 mg/L.



**Figure IV. 3.3** - Comparison of experimental (x, run 1; o run 2) and simulated (continuous line) time courses of RB5 degradation in a simulated effluent by commercial laccase under different initial concentrations: (a) 126.2 mg/L and 128.1 mg/L; (b) 102.2 mg/L and 103.6 mg/L; (c) 89.3 mg/L and 90.0 mg/L; (d) 79.9 mg/L and 80.2 mg/L; (e) 52.5 mg/L and 52.7 mg/L.

According to Cristóvão et al. (2008), the  $K_{MS}$  constant of the proposed model is the equilibrium constant of the enzyme–mediator/substrate complex decomposition. It measures the enzyme–mediator system affinity to the substrate. The lesser the value of  $K_{MS}$ , the larger is the affinity of the enzyme–mediator system to the substrate. Comparing the  $K_{MS}$  values of each dye in the effluent (Table IV. 3.2), the laccase–mediator system affinities for the dyes decrease according to the following order: RB5 > RR239 > RY15. This result is easy to confirm in Figures IV. 3.1 – IV. 3.3 by the time that each dye takes to reach the equilibrium. A larger dyes degradation time corresponds to a more difficult decolourization (less affinity of the laccase–mediator system for the dye). In the previous cases of single and mixture of dyes (Cristóvão et al., 2008, 2009), the RR239 was always the slower dye. In this case, this dye reached the equilibrium faster, however it was not so degraded: it continues to be the least degraded. The degradation of each dye and its affinity to the laccase–mediator system depends on the redox potentials of each substance (Tavares et al., 2009b). The RR239 is the dye with the highest redox potential, thus being the more difficult to degrade.

The rates of the dyes degradation in the effluent can also be assessed by the value of  $v_{max}$  – the theoretical maximum velocity. According to the values of  $v_{max}$  presented in the Table IV. 3.2 for each dye in the effluent, the degradation rate decreases in the following order: RB5 > RR239 > RY15, which is in a good agreement with the conclusions obtained with the other parameters.

This study also enables to evaluate the activation rate of the laccase–mediator system by the  $k$  values presented in Table IV. 3.2. According to the results, the activation of the laccase–mediator system decreases according to the following order: RR239 > RB5 > RY15.

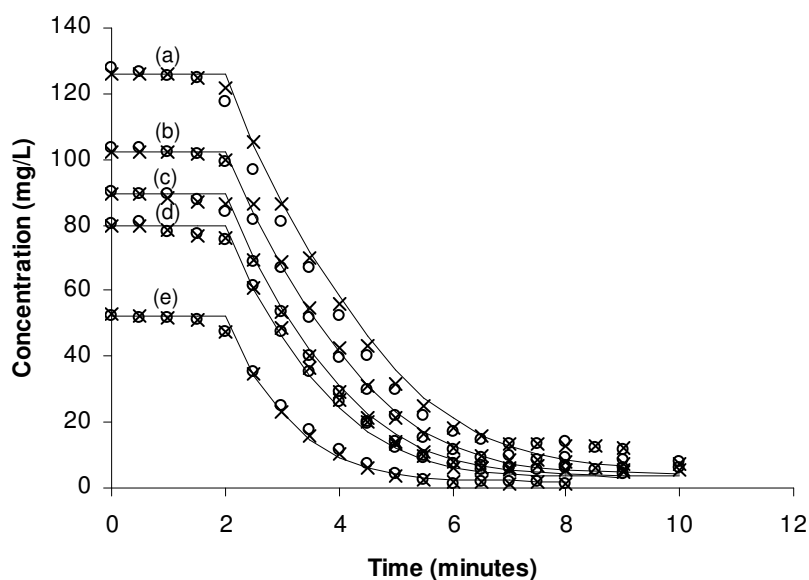
In order to evaluate the adequacy of the proposed models for the kinetics of the simulated effluent decolourization by commercial laccase, the time courses calculated by the kinetic models were compared with the experimental ones. These comparisons at the wavelengths of RY15, RR239 and RB5 are displayed in Figures IV. 3.1 – IV. 3.3, respectively. The close correspondence of the experimental data with the simulated values under different effluent concentrations seems to demonstrate that the proposed mathematical models are able to describe with remarkable accuracy the RY15, RR239 and RB5 laccase catalyzed degradations when they are present in a simulated textile effluent. These kinetic models provide an emergent tool to simulation and design of enzymatic bioreactors as for optimization of the process.

Nonetheless, the correspondence between both time courses for RB5 wavelength seems to be not as good as for the other wavelengths. This led us to try a new model for this case, this time with a static period for the activation time of the laccase–mediator system, during which the initial concentration does not change:

$$v = C_0[H(t) - H(t - t_0)] + \frac{V_{max} \left( [S] - \frac{[P]}{K_{eq}} \right)}{K_{MS} \left( 1 + \frac{[P]}{K_{MP}} \right) + [S]} H(t - t_0) \quad (\text{IV. 3.7})$$

where  $C_0$  corresponds to the initial concentration,  $H(t)$  is the Heaviside step function with values of 0 for  $t < 0$  and 1 for  $t \geq 0$  and  $t_0$  corresponds to the time at which the concentration starts to decrease.

By observation of the experimental behaviour the concentration almost does not vary up to 2 min., so it was assumed that  $t_0$  corresponds to 2 min.. The kinetic constants of the model were estimated by minimizing the difference between the experimental time courses and the ones predicted by the model from 2 min. to the end. The obtained kinetic constants for this kinetic model were  $v_{max} = 11.887$  mg/g.min,  $K_{MS} = 21.31$  mg/L,  $K_{MP} = 108.71$  mg/L and  $K_{eq} = 22.57$  with an average sum of squared relative residuals of  $9.366 \times 10^{-2}$ . Despite of having a slightly larger error, we found important to show this new result as it seems to better follow the initial behaviour at this wavelength and seems to be qualitatively more appropriate to describe the system behaviour. The comparison between the experimental time courses and the ones predicted by this new model is presented in Figure IV. 3.4.



**Figure IV. 3.4** - Comparison of experimental (x, run 1; o run 2) and simulated (continuous line) time courses by a new kinetic model with a static initial period of RB5 degradation in a simulated effluent by commercial laccase under different initial concentrations: (a) 126.2 mg/L and 128.1 mg/L; (b) 102.2 mg/L and 103.6 mg/L; (c) 89.3 mg/L and 90.0 mg/L; (d) 79.9 mg/L and 80.2 mg/L; (e) 52.5 mg/L and 52.7 mg/L

By these results, it was possible to conclude that the models can, probably, be also applied to the decolourization of a real effluent by commercial laccase; however attention must be paid to the values of the kinetic constants that vary with the system studied.

Comparing the kinetic constants values of the dye mixture degradation models (Cristóvão et al., 2009) with the ones of the simulated effluent degradation containing the same dyes studied, they are different and probably it is not possible to simulate the degradation of the simulated effluent with the kinetic parameters obtained for the degradation of the dye mixture and vice versa. When in a simulated effluent, with other auxiliary chemicals and salts, the RY15 and RR239 dyes present a higher degradation rate ( $v_{max}$ ), while the RB5 dye presents a lower degradation rate than when in a simple mixture of the dyes. The laccase–mediator system affinity for the RR239 dye is highest when present in the simulated effluent, but it presents more affinity to RY15 and RB5 dyes when they are in the simple mixture. It is also possible to compare the activation rates of the laccase–mediator system in the degradation of both systems. In the RB5 degradation case, the activation rate is equal in both situations, when present in a simple mixture or when in a simulated effluent. Relatively to the RY15 degradation, the activation rate is greater when it is present in the simple mixture. The degradation of the RR239 dye does not present laccase–mediator system activation when present in a mixture of dyes. Furthermore, the RR239 is the only dye that does not fit the same kinetic model in both situations.

In order to assess the ability of the models developed for the dye mixture in the prediction of the simulated effluent degradation, the time responses of each dye predicted by the models of the mixture were evaluated for each of the characteristic wavelengths for the simulated effluent. The comparison of these predictions with the actual results reveals that, in the case of RB5 and RY15 the models are able to reproduce the general qualitative behaviour. However, when the quantitative results are compared the predictions are far from reasonable. For the RR239 the models are different in both cases, so this simulation does not make sense.

#### **IV. 3.6.3 Environmental analysis**

To simulate the dye bath conditions used in the textile industry, the solution fed to the reactor was previously hydrolysed. After hydrolysis, the environmental parameters average values of the dye bath effluent were in the order of:  $BOD_5 = 17\text{mg O}_2/\text{L}$ ,  $COD = 394\text{ mg O}_2/\text{L}$  and  $TOC = 75\text{ mg/L}$ . For the toxicity, since the relationship between  $EC_{20}$  and  $EC_{50}$  is not linear we decided to give both values presenting two toxic designations (Backhaus et al., 1997). The values obtained were  $EC_{20} = 42\text{ mg/L}$  and  $EC_{50} = 64\text{ mg/L}$ , after 5 min. of exposure and  $EC_{20} = 28\text{ mg/L}$  and  $EC_{50} = 56\text{ mg/L}$ , after 15 min. of exposure. The initial solution was almost non-toxic. It was only possible to determine the  $EC_{20}$  and  $EC_{50}$  values for effluent concentrations of  $125\text{ mg/L}$ . For concentrations lesser than that, it was not possible to determine the toxicity since it was not detected.

The final values of water quality analysis obtained after the laccase catalyzed degradation of the simulated reactive dye bath wastewater were:  $BOD_5 = 1338 \text{ mg O}_2/\text{L}$ ,  $COD = 3383 \text{ mg O}_2/\text{L}$ ,  $TOC = 957 \text{ mg/L}$  and  $COD/BOD_5 = 2.53$  (defined here as the specific biodegradability of the effluent in question). Regarding toxicity, only values after 5 min. of exposure time were possible to obtain and only the  $EC_{50}$  value was possible to get:  $EC_{50} = 4.7 \text{ mg/L}$ . All the other values give results of high toxicity, even for only 5 % of the effluent. In the Flash method, the sample is used as a reference for itself, and the light output must be recorded immediately after all the bacteria contact the sample. The light output of the bacteria was reduced immediately after contact with the sample, and no actual peak value can be measured due to the extreme toxicity.

A reduction in the studied values was expected, since the treatment method is based on an oxidation. However, the simulated effluent has a high degree of complexity since it is a mixture of auxiliaries, salts, surfactants, degradation products and unknown components of refractory pollutants. So, the high toxicity to the luminescent bacteria, the high TOC, COD and  $BOD_5$  could be explained as a result of some unknown products produced during the treatment process. However the results were well above of those expected. So we decided to investigate this and consider only the solution of enzyme (only with buffer and enzyme). After the same analysis, the following values were obtained for this enzyme solution:  $BOD_5 = 1300 \text{ mg O}_2/\text{L}$ ,  $COD = 3341 \text{ mg O}_2/\text{L}$  and  $TOC = 875 \text{ mg/L}$ . Relatively to the toxicity, one more time it was only possible to obtain the  $EC_{50}$  value for 5 min. of exposure:  $EC_{50} = 5.4 \text{ mg/L}$ , a very high toxicity value. By these results and comparing with the simulated effluent ones after treatment, it was possible to conclude that they are of the same order of magnitude, leading to say that it is the enzyme that contributes to the increase of these analytical parameters. Subtracting the values corresponding to the enzyme, the values of the treated simulated effluent are similar or slightly higher than the initial values, which could be due to the complexity of the treated effluent. Besides that, these values are below the maximum permitted discharge values of textile industries wastewaters in Portugal ( $BOD_5 = 40 \text{ mgO}_2/\text{L}$ ,  $COD = 150 \text{ mgO}_2/\text{L}$ ). A possible solution to solve the environmental problem caused by the enzyme in the effluent will be studied and reported in the future, namely the immobilization of the enzyme. If this problem can be overcome, it seems possible to conclude that the treatment of textile wastewaters by commercial laccase is probably a good treatment method to implement in textile industries.

### **IV. 3.7 Conclusions**

The decolourization of a simulated wastewater containing salts and auxiliary chemicals was carried out effectively by laccase catalyzed degradation (around 55 % total decolourization, 86 % RB5, 63 % RY15 and 41 % RR239) showing that it would be a good potential candidate for treatment of real textile wastewaters.

The good consistency between experimental and predicted data proved that the proposed models could successfully simulate the kinetic behaviour of these reactions in batch reactors. These kinetic models provide an emergent tool to simulation and design of enzymatic bioreactors.

The water quality analyses showed values below the maximum permissible discharge values of textile industrial wastewaters.

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## **Part V**

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### **Immobilization**



*In this part of the thesis the study of the immobilization of commercial laccase (DeniLite II S) into coconut fiber by physical adsorption is presented. The typical characteristics of immobilized enzymes are evaluated and its implementation in the degradation of dyes is checked.*



# **Part V** Immobilization of commercial laccase onto green coconut fiber by adsorption and its application for reactive textile dyes degradation

V. 1 Abstract

V. 2 Introduction

V. 3 Materials and Methods

V. 4 Results and Discussion

V. 5 Conclusions

V. 6 References





## **V Immobilization of commercial laccase onto green coconut fiber by adsorption and its application for reactive textile dyes degradation**

### **V. 1 Abstract**

An effort has been made to find a cheaper, easily available and simple alternative for the immobilization and subsequent utilization at large scale of commercially available enzymes in textile wastewater treatment. Commercial laccase DeniLite II S was immobilized for the first time on an agroindustrial residue, green coconut fiber, by physical adsorption. The effect of the immobilization conditions (enzyme concentration, contact time and pH value) on the properties of the biocatalyst was determined. Then, the immobilized enzyme characterization in the optimized conditions was performed and kinetic parameters were obtained. Thermal and operational stabilities were improved comparing with the free commercial laccase showing its potential for continuous applications. Finally, the performance of immobilized laccase for the continuous degradation of various reactive textile dyes and of a mixture of them in batch reactors was evaluated, for application in continuous mode at industrial level. In these experiments, two phenomena were observed: decolourization of the solutions due to dyes adsorption on the support and degradation due to the enzyme action. A high decolourization percentage of practically all dyes was obtained in the first two cycles, showing the suitability of the immobilized commercial laccase for continuous colour removal from textile industrial effluents. An effective dye mixture decolourization (about 50 % of total decolourization in all visible spectra) by the immobilized enzyme was also observed. All these results confirm the initial idea of commercial laccase immobilized on coconut fiber as a promising biocatalyst for industrial applications.

### **V. 2 Introduction**

A large number of synthetic dyes are being increasingly used in the textile, paper, pharmaceutical, cosmetics and food industries. Over  $7 \times 10^5$  tonnes of approximately 100,000 different dyes and pigments are produced annually worldwide, of which about 50,000 tonnes are discharged into the environment (Lewis, 1999; Slokar and Marechal, 1998). These compounds cause serious environmental pollution. Most of them are toxic, mutagenic and carcinogenic. Moreover, they are unusually resistant to degradation due to their complex structure and synthetic origin. Colour can be removed from effluents by chemical and physical methods including adsorption, coagulation-flocculation, ion-exchange, oxidation and electrochemical methods (Anjaneyulu et al., 2005; Forgacs et al., 2004). However these methods have financial and methodological disadvantages. They are also time-consuming and

mostly are ineffective. Alternatively, dye decolourization using microbial enzymes has received great attention in recent years due to its efficient application (Casas et al., 2007; Champagne and Ramsay, 2005; Couto et al., 2006). Laccase-based decolourization treatments are potentially advantageous to bioremediation technologies since the enzyme is produced in larger amounts. Laccase (p-diphenol oxidase, EC 1.10.3.2) catalyzes the oxidation of phenolic compounds and aromatic amines and accepts a broad range of substrates (Claus, 2004; Thurston, 1994). The number of substrates can further be extended by using laccase in combination with mediators (Husain and Husain, 2008; Tavares et al., 2008).

One of the main drawbacks of using free enzymes to detoxify waste streams is their instability towards thermal and pH denaturation, non-reusability, proteolysis, inactivation by inhibitors. The immobilization of enzymes to water-insoluble supports can increase their operational stability and durability and can provide easy separation of the product from reaction media and easy recovery of the enzyme. Furthermore, enzyme immobilization would allow the reuse of the enzyme and thus decrease the cost of industrial applications and allow the control of the process. Therefore, many efforts have been made to immobilize laccase from various sources (Cao, 2005; Durán et al., 2002), but most of the immobilized enzyme preparations either use commercially available enzyme or expensive supports, which increase the cost of the processes (Akhtar et al., 2005a,b).

Several techniques may be applied to immobilize enzymes on solid supports. They are mainly based on chemical and physical mechanisms (Durán et al., 2002). Therefore, it is hardly surprising that there is no general universally applicable method of enzyme immobilization. The main task is to select a suitable carrier, condition (pH, temperature and nature of medium) and enzyme itself (source, nature and purity) to design an immobilized biocatalyst. The selected method should meet both the catalytic needs (expressed in productivity, space-time yield, stability and selectivity) and the non-catalytic needs (e.g. separation, control, down-streaming process) that are required by a given application. As a result, an immobilized enzyme can be labelled as "robust, when both the catalytic and the non-catalytic functions can meet the requirements of a specific application (Bornscheuer, 2003; Dyal et al., 2003).

Laccase, immobilized on several supports, has been evaluated for the elimination of pollutants such as phenols, but few studies have investigated dye decolourization (Durán and Esposito, 2000; Durán et al., 2002). Dye decolourization using laccase immobilized on imidazol-modified silica gel (Peralta-Zamora et al., 2003) or silanized alumina particles (Zille et al., 2003) occurred mainly by adsorption and to a lesser extent, by enzymatic decolourization. More recently, Champagne and Ramsay (2007) demonstrated that laccase immobilized on controlled porosity carrier glass beads using APTES-glutaraldehyde decolourized a single anthraquinone dye mainly by enzymatic degradation.

An effort has been made to find a cheaper and easily available alternative for the immobilization and subsequent utilization at large scale of commercially available enzymes. Thus, green coconut fiber was used as support for laccase immobilization. To our knowledge,

no reports on laccase immobilization by physical adsorption on green coconut fiber have been published. Among the various immobilization techniques, the physical adsorption on the basis of bioaffinity may be a good choice for enzyme immobilization, as this process can immobilize enzyme directly from crude homogenate and thus avoid the high cost of purification. It saves time and labour since it is a simple operation, no further treatment of the support is needed and supports can be reused after desorption of the inactivated enzyme, thus reducing the final price and generating fewer residues (Alonso-Morales et al., 2004; Sari et al., 2006). The ease of immobilization, lack of chemical modification and enhancement in stability are some of the advantages offered by the adsorption procedures (Akhtar et al., 2005a,b; Kulshrestha and Husain, 2006). Besides the mentioned advantages offered by the bioaffinity-based procedures, there is an additional benefit, such as proper orientation of enzyme on the support (Khan et al., 2005; Mislovicova et al., 2000). These supports provide high yield and stable immobilization of enzymes. However, this technique possesses disadvantages, such as low linking energy between enzyme and support, which may cause enzyme desorption in presence of the substrate or when it is exposed to variations on temperature, pH and ionic strength. Nevertheless, immobilization by adsorption is one of the most used techniques in the attainment of insoluble biocatalysts (Kennedy et al., 1988).

The first objective of this study was to immobilize the commercial laccase by adsorption on green coconut fiber and to determine the effect of the immobilization conditions (enzyme concentration, contact time and pH value) on the properties of the biocatalyst. The second objective was to evaluate the performance of immobilized laccase regarding the continuous degradation of various reactive textile dyes and of a mixture of them in batch reactors.

## **V. 3 Materials and Methods**

### **V. 3.1 Chemicals and enzyme**

Textile Dyes: Reactive Black 5 (RB5) (Remazol Black B), Reactive Blue 114 (RB114) (Levafix Brilliant Blue E-BRA), Reactive Yellow 15 (RY15) (Remazol Yellow GR), Reactive Yellow 176 (RY176) (Remazol Yellow 3RS), Reactive Red 239 (RR239) (Remazol Brilliant Red 3BS) and Reactive Red 180 (RR180) (Remazol Brilliant Red F3B) were kindly provided by DyStar (Portugal) and were used for degradation experiments without any further purification.

Enzyme: Commercial laccase formulation (DeniLite II S; 120 U/g) from genetically modified *Aspergillus* was kindly provided by Novozymes. This formulation is used for indigo dye decolourization in denim finishing operations and includes a buffer and an enzyme mediator.

Support: Green coconut fiber was kindly donated by Embrapa Agroindústria Tropical, Ceará State, Brazil. It was cut and sieved to obtain particles between 32 and 35 mesh and then washed with distilled water and dried at 60 °C before being used as immobilization matrix.

### V. 3.2 Immobilization procedures

To optimize the enzyme immobilization conditions by adsorption technique, 0.15 g of green coconut fiber were incubated in syringes with 1.5 mL of laccase solution containing 0.08-2.6 g/mL of enzyme at room temperature and varying pH from 4.0 to 9.0. The syringes with the solutions were stirred on a rotational shaker TECNAL, model TE-165 (Figure V. 1). At the optimized conditions of pH and enzyme concentration, the effect of contact time was evaluated in the range 30 min. – 8 h. The solutions were also stirred on the rotational shaker. After immobilization, the support was separated by filtration and washed three times with 0.1 M of phosphate buffer (pH = 7.0). The supernatant was kept for enzyme activity measurements. The immobilized enzyme activity was measured as described below. For each assay duplicate or triplicate runs were made.

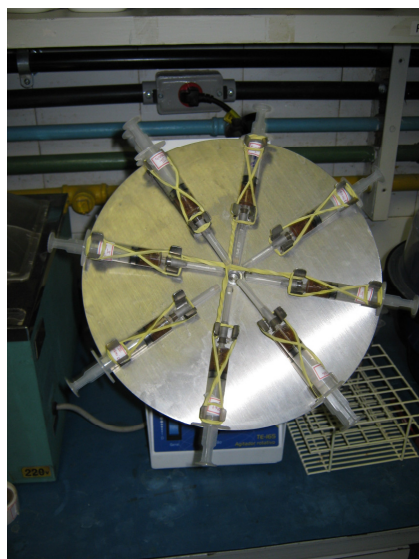


Figure V. 1 – Rotational shaker with syringes.

### V. 3.3 Measurements of activity of free and immobilized laccase

The free laccase activity was assayed spectrophotometrically (Thermo Electron, model UV1 spectrophotometer) with ABTS as substrate (0.4 mM) in 0.05 mM citrate/0.1 mM phosphate buffer at pH 4.5. To measure the laccase activity, 0.1 mL of the incubated enzyme solution was added to 1.9 mL of the ABTS solution at 40 °C (Ander and Messner, 1998). The change in absorbance at 420 nm ( $\epsilon = 36 \times 10^3 \text{ M}^{-1} \cdot \text{cm}^{-1}$ ) was recorded for 30 s and the catalytic activity was determined by measuring the slope of the initial linear portion of the kinetic curve. One unit (U) was defined as the amount of enzyme that oxidized 1  $\mu\text{mol}$  of ABTS per min. and the activities were expressed in U/L.

The immobilized laccase activity was assayed by incubating 0.1 g of support in 7.0 mL of the same citrate–phosphate buffer with 2.5 mL of ABTS (0.4 mM) at 40 °C. The change in absorbance was monitored every minute, over a 4 min. period, by withdrawing 2 mL of the

solution. After measurement, the solution was turned back to the reactor. The absorbance at 420 nm ( $\epsilon = 36 \times 10^3 \text{ M}^{-1} \cdot \text{cm}^{-1}$ ) was measured as before. The final activity of immobilized laccase was expressed in U/kg .

Immobilization yield (%) is defined as the difference between enzyme activity in the supernatant before and after immobilization divided by the enzyme activity in the supernatant before immobilization.

The recovery activity (%) of the immobilized enzyme is defined as the ratio between the activity of the immobilized enzyme and the activity of a similar amount of the free enzyme.

### V. 3.4 Thermal stability of free and immobilized laccase

The thermal inactivation of the free and immobilized laccase was investigated by incubating the free and immobilized enzyme in phosphate (100 mM) buffer pH 7.0 at 60 °C. For this purpose 0.1 g of immobilized enzyme or free laccase (550 U/L) were incubated in a water bath with temperature control. In certain time intervals consecutive aliquots were taken up to complete inactivation. The initial activities were compared with the residual activities. The thermal parameters were calculated according to the simplified deactivation model proposed by Henley and Sadana (1985) referenced by Arroyo et al. (1999):

$$A = (1 - \alpha) \cdot e^{-kt} + \alpha \quad (\text{V. 1})$$

where  $A$  is the residual enzyme activity,  $\alpha$  is the ratio of specific activity  $E_i/E$  to the different states (see Equation V. 2),  $k$  the thermal inactivation parameter and  $t$  the time. Thermal parameters were estimated by fitting the experimental data to Equation (V. 1) using a nonlinear regression code (MicroCal Origin software v.3.01 (SPSS Inc., Northampton, USA).



Biocatalyst half-life ( $t_{1/2}$ ) was calculated from Equation V. 1, using the estimated parameters ( $k$  and  $\alpha$ ) and making  $A$  equal to 0.5. In this work, stabilization factor ( $F$ ) was considered as the ratio of immobilized enzyme's half-lives to soluble enzyme half-life.

### V. 3.5 Operational stability of immobilized laccase

Operational stability of the immobilized laccase was assessed by incubating 0.1 g of the immobilized laccase with 2.5 mL of ABTS (4 mM) in 7 mL of citrate–phosphate buffer pH 7.0 at room temperature and under moderate mixing. 16 cycles of operational stability were carried out. At each cycle, a sample was withdrawn in 1 min. intervals, absorbance was measured and then it was returned to reactor (initial reaction rate measurements). Afterwards, the reaction was stopped to the substrate removal. Then the immobilized enzyme was collected by filtration,

washed twice with phosphate buffer 100 mM pH 7.0 and resuspended in a fresh substrate solution to begin the next cycle. For each assay duplicate runs were made.

### V. 3.6 Determination of kinetic parameters

The Michaelis–Menten kinetic parameters  $K_M$  and  $v_{max}$  of free and immobilized laccase were determined by measuring the laccase activity using ABTS as substrate over a 0.1-1.5 mM range of initial concentrations. The parameter values were obtained by non-linear curve fitting of the plot of reaction rate versus substrate concentration using the MicroCal Origin software v.3.01 (SPSS Inc., Northampton, USA).

### V. 3.7 Degradation of Reactive dyes by immobilized laccase

A solution of single reactive dye (50 mg/L) (RB5, RB114, RR180, RR239, RY15 or RY176) or a mixture of three dyes 50 mg/L (RB5, RY15 and RR239) was continuously orbital stirred (240 rpm) with 0.4 g of support immobilized with laccase (0.067 g/mL of laccase per g support) in phosphate buffer solution pH 7.0, final volume of 25 mL at 35 °C (Figure V. 2). Three cycles of dye degradation were carried out. Between each cycle, the support was washed three times with phosphate buffer pH 7.0, 100 mM. Dye decolourization was determined by monitoring the decrease in the absorbance peak at the maximum wavelength for each dye: RY15 (416 nm), RR239 (542 nm), RB114 (593 nm), RB5 (579 nm), RR180 (540 nm) and RY176 (421 nm). UV-visible spectrophotometer (Thermo, model UV1) was used in all experiments. Decolourization is reported as: % decolourization =  $(A_i - A_f)/A_i \times 100$ , where  $A_i$  is the initial absorbance or total area from the initial spectrum and  $A_f$  is the final absorbance or total area from the final spectrum. A control with support alone (without enzyme immobilization) was carried out at the same conditions in order to determine the dye adsorption by the support. For each assay duplicate runs were made.

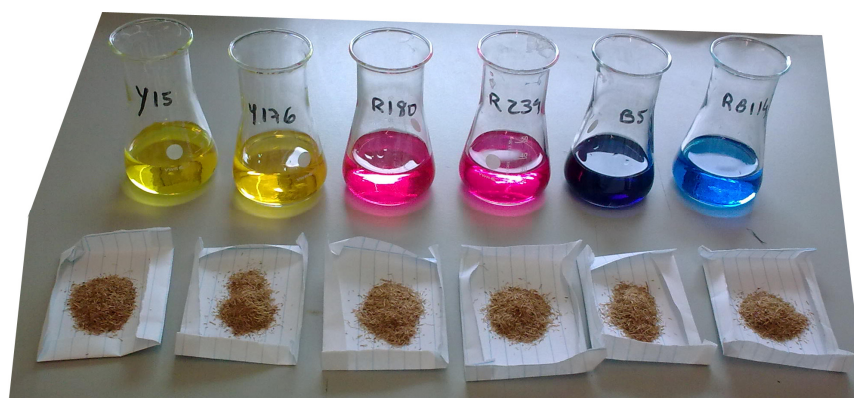


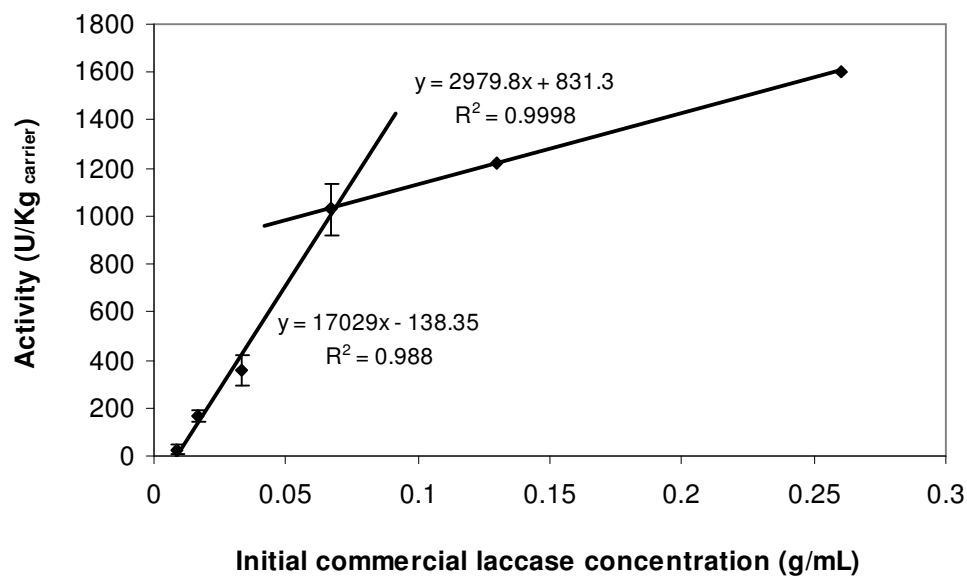
Figure V. 2 – Initial dyes solutions and the coconut fiber.

## V. 4 Results and Discussion

### V. 4.1 Immobilization of commercial laccase on green coconut fiber by adsorption

In this study the immobilization of commercial laccase using a simple, effective and inexpensive process for the degradation of reactive textile dyes was studied. The effect of enzyme concentration, pH and contact time between enzyme solution and coconut fiber on the activity of immobilized commercial laccase was studied and optimized.

In order to determine the optimum commercial laccase concentration to be immobilized, several experiments with the same amount of carrier and buffer were performed with initial enzyme concentrations ranging from 0.008 to 0.26 g/mL at room temperature. Contact time between the enzyme and the coconut fiber and pH were set at 3h30min. and 7.0, respectively. The results are presented in Figure V. 3.



**Figure V. 3** – Influence of initial enzyme concentration on the activity of the immobilized commercial laccase on coconut fiber by adsorption at pH 7.0 and 3h30min. of contact time.

It can be seen that the activity of the immobilized laccase increases with the enzyme concentration, however not always in a linear way. Two slopes are observed, with the first one, for lower enzyme concentrations until 0.067 g/mL, steeper than the second one. According to the literature (Arroyo et al., 1999; Blanco et al., 2004) enzyme adsorption is not restricted to a monolayer on the support, and adsorption of secondary layers has been reported. Thus, the first slope possibly corresponds to the formation of a monolayer of enzyme, while the second slope corresponds to the binding of enzymes on top of the monolayer. A control experiment with fiber

without enzyme was also performed and no activity was found when only the fiber was used as catalyst.

Recovered activity and immobilization yield were calculated, and results are listed in Table V. 1. Recovered activity was maximum at the point of change of slope (0.067 g/mL), from which begins to decrease (in a non-regular way). The maximum recovered activity at this point suggests that probably at this concentration the enzyme molecules are immobilized at close proximity to each other covering the entire support surface, thus preventing the enzyme deactivation. In other words, when enzyme load was increased, more enzyme molecules were immobilized and less area on the support is available for laccase to spread itself, which may prevent loss in activity (de Oliveira et al., 2000). Above this concentration, probably a second layer of commercial laccase was adsorbed on the first layer. Although more molecules were immobilized on coconut fiber, not all of them were available to the substrate, causing decrease in recovered activity. Coconut fiber surface does not have a porous structure, and it has a low surface area. This poor surface area limits the number of enzyme molecules to be immobilized, facilitating the multilayer adsorption of enzymes (Brígida et al., 2007). Immobilization yield increases until an enzyme concentration of 0.033 g/mL, point from which starts to slowly decrease (in a more regular way). With these results and taking into account the both values of recovered activity and immobilization yield, the commercial laccase concentration of 0.067 g/mL was selected to continue the studies, since it is the concentration that offers the best relationship among the values of recovered activity and immobilization yield. From this enzyme concentration (where the slope changes), no increase in recovered activity or immobilization yield is observed, so there is no point on using higher initial enzyme concentrations.

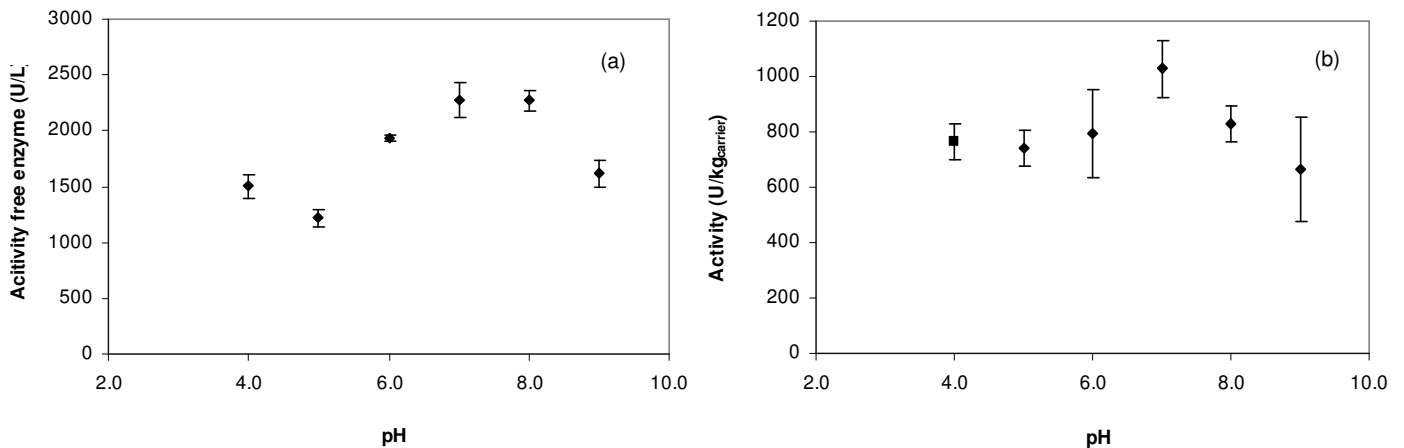
**Table V. 1** – Influence of initial enzyme concentration on recovered activity and immobilization yield.

Enzyme concentration (g/mL)	Recovered activity (%)	Immobilization yield (%)
0.008	11.0	3.3
0.017	4.2	43.3
0.033	6.7	45.2
0.067	12.0	37.5
0.13	7.4	37.2
0.26	9.6	23.3

The effect of pH was studied at pH values from 4.0 to 9.0. Enzyme concentration and contact time between the support and the enzyme solution were set at 0.067 g/mL and 3h30min., respectively. The pH profiles of the free and the immobilized laccase are shown in Figure V. 4. It can be clearly observed from Figure V. 4 b) that a maximum of immobilized enzyme activity is reached at about pH 7.0, and for values lower or higher than 7.0 the activity decreases. This optimum range is very similar to that observed for the soluble laccase (Figure V. 4 a)) indicating that the immobilization procedure on green coconut fiber does not affect the



enzyme charge, which has also been reported in other studies (Kara et al., 2005; Wang et al., 2008). Subtle changes in the activity/pH profiles have been reported on the immobilization of enzymes to charged supports (Al-Adhami et al., 2002; Leontievsky et al., 2001).



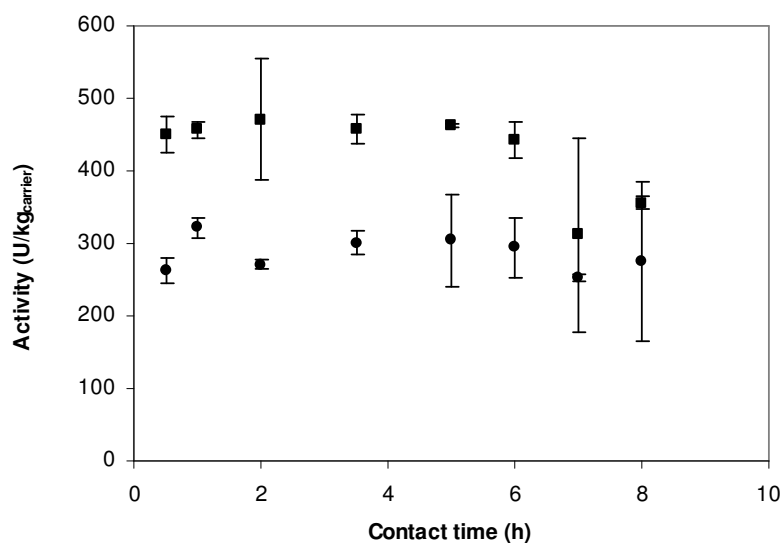
**Figure V. 4** – Effect of pH of the solution a) on initial commercial laccase activity and b) on the activity of the immobilized commercial laccase on coconut fiber by adsorption at 0.067 g/mL of enzyme and 3h30min. of contact time.

Immobilization parameters, recovered activity and immobilization yield, were calculated for all the range of pH studied. Table V. 2 shows that immobilization yield and recovered activity were dependent on the pH of adsorption. Interactions between the molecule and its environment influence the structure of an enzyme molecule and these interactions are pH-dependent (Geluk et al., 1992). The best result for recovered activity (45.7 %) was achieved at pH 5.0, value from which it starts to decrease. On the other hand, immobilization at pH 7.0 significantly improved the amount of immobilized enzyme (37.5 %). The commercial laccase immobilization at pH 5.0 results in a high decrease in the immobilization yield. Thus, pH 7.0 was chosen to continue the studies of optimization, as it represents the value where more enzyme was immobilized and, despite of having a lower recovered activity, it corresponds to the highest activity of immobilized enzyme (Figure V. 4 b)).

**Table V. 2** – Influence of pH of the solution on recovered activity and immobilization yield.

pH	Recovered activity (%)	Immobilization yield (%)
4.0	31.9	10.8
5.0	45.7	13.3
6.0	24.5	16.8
7.0	12.0	37.5
8.0	18.2	20.1
9.0	14.0	29.4

Finally, the influence of contact time between coconut fiber and commercial laccase solution was evaluated at pH 7.0 and two different enzyme concentrations: 0.033 g/mL and 0.067 g/mL. The results are shown in Figure V. 5. Similar contact time profiles were achieved for both enzyme concentrations studied. It was observed that commercial laccase immobilized activity increases as time increased until 3h30min.. From 3h30min. till 5/6 hours no significant changes in immobilized laccase activity were observed, but after this time the activity tends to fall. Probably for longer contact times some enzyme desorption takes place or the enzyme starts to adsorb at the second monolayer ceasing to have so available enzymes to react with the substrate.



**Figure V. 5** – Effect of contact time on the activity of the immobilized commercial laccase on coconut fiber by adsorption at pH 7.0 and at ● 0.033 g/mL and ■ 0.067 g/mL of enzyme.

These results can be confirmed by the recovered activity and immobilization yield presented in Table V. 3. In both cases immobilization yield increased with the increase of contact time once more till 5/6 hours, showing that there is no need to leave the support and the enzyme solution in contact for longer periods. By the recovered activity that increases till 3h30min. and then starts to decrease, it is possible to conclude that there is no advantage in leaving the enzyme solution in contact with the coconut fiber for longer times, since it does not promote the immobilization. Although more molecules were immobilized on coconut fiber, not all of them were available to the substrate, causing a decrease in recovered activity. So, this is a way to avoid the formation of the second monolayer and the loss of enzyme activity.

**Table V. 3** – Influence of contact time on recovered activity and immobilization yield for 0.033 g/mL and 0.067 g/mL of enzyme.

Contact time (h)	Recovered activity (%)		Immobilization yield (%)	
	0.033 g/mL	0.067 g/mL	0.033 g/mL	0.067 g/mL
0.5	5.3	4.4	37.8	31.9
1.0	6.7	3.8	36.0	37.0
2.0	3.6	3.3	57.3	44.7
3.5	5.1	3.5	44.2	40.2
5.0	3.4	2.6	68.8	55.4
6.0	4.4	2.2	50.6	61.8
7.0	2.5	1.6	75.1	59.9
8.0	2.9	3.5	70.8	31.8

## V. 4.2 Immobilized enzyme properties

### V. 4.2.1 Thermal stability

The thermal stability is one of the most important features concerning the application of the biocatalyst. Immobilization of an enzyme to a support often limits its freedom to undergo drastic conformational changes and thus results in increased stability towards denaturation (Al-Adhami et al., 2002; Leontievsky et al., 2001).

Thermal stability experiments were carried out with free and immobilized enzyme, which were incubated at 60 °C. The immobilized enzyme was obtained by contacting 0.067 g/mL of a commercial laccase solution of pH 7.0 with the coconut fiber for 3h30min.. The thermal deactivation model (Equation V. 1) was fitted to experimental data (Figure V. 6) and the model parameters are listed in Table V. 4, for free and immobilized enzyme.

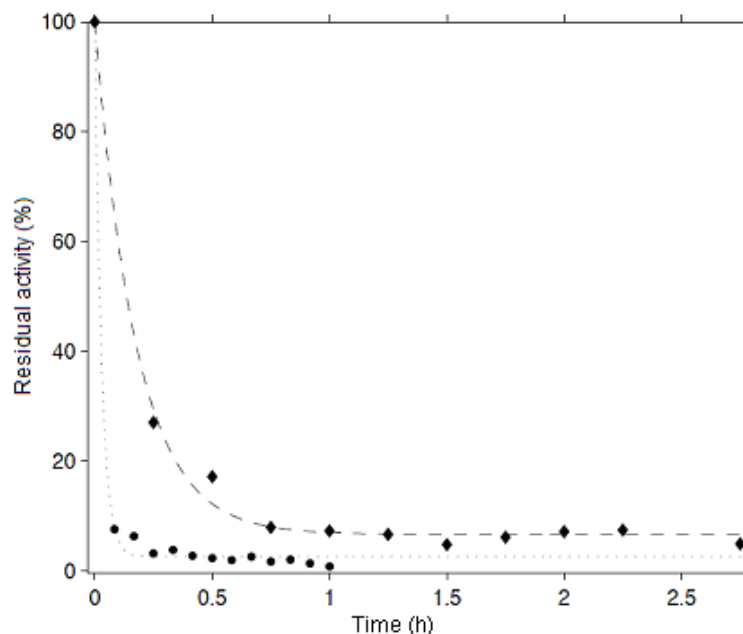
**Table V. 4** – Kinetic parameters of thermal deactivation at 60°C of free commercial laccase and immobilized by adsorption on coconut fiber.

Enzyme	k (h <sup>-1</sup> )	$\alpha$	t <sub>1/2</sub> (h)	F	R <sup>2</sup>
free	34.8	0.026	0.02	1.0	0.998
immobilized	5.64	0.067	0.14	6.6	0.995

As it can be seen from the results in Table V. 4, the  $\alpha$  values are quite small, indicating that possibly these can be discarded. Therefore it is possible the use of simple exponential decay model, that states the final activity of the enzyme as zero, as reported by many authors on their researches (Longo and Combes, 1999; Santos et al., 2007). However, the final activity

of the enzyme observed is very small but not zero, then the correct formula to use is the Equation V. 1, used in this work.

Figure V. 6 show that commercial laccase immobilization led to a significant stabilizing effect towards heat denaturation at 60 °C. The immobilized laccase was inactivated at a much slower rate than that of the free form under the same conditions. After 5 minutes of incubation at 60 °C the free enzyme shows a percentage of deactivation that the immobilized one shows only after 1 hour of incubation.



**Figure V. 6** – Thermal stability of (●) free and (◆) immobilized commercial laccase obtained by adsorption at 60 °C.

These results can be confirmed by the kinetic parameters of thermal deactivation presented in Table V. 4. The half-life time ( $t_{1/2}$ ) is the period of time that takes for a substance undergoing decay to decrease by half. The free enzyme has a half-life of 0.02 h whereas the value for the immobilized one is 0.14 h, 6.6 times higher. This means that the free enzyme lost 50 % of the initial activity 6.6 times earlier than the immobilized one. This 6.6 value is exactly the stabilization factor ( $F$ ) which shows that the immobilization of commercial laccase on coconut fiber promoted an improvement on thermal stability, as immobilized commercial laccase is more stable than the free one at 60 °C. The increased stability of immobilized laccase was due to the restricted conformational mobility of the molecules following immobilization. Other authors obtained similar results when immobilizing laccase on other supports (Arica et al., 2009; D'Annibale et al., 2000; Leontievsky et al., 2001). The increased resistance to thermal denaturation of laccase arising from immobilization would be an advantage for its industrial application due to the high temperatures used in the industrial processes (Berrio et al., 2007; D'Annibale et al., 1999).

#### V. 4.2.2 Operational stability

The reusability of the commercial laccase immobilized on coconut fiber by adsorption was studied by cycles of ABTS oxidation due to its importance for industry to reduce the processing costs. From the results shown in Figure V. 7, it was possible to observe that, despite only (weak) physical bonds were involved, the operational stability of this system was good, losing only about 30 % of the initial enzyme activity after 5 cycles of reaction and 45 % after 13 cycles. After that little activity loss was determined. Successful reuse of various immobilized laccase systems has been reported by other investigators (Davis and Burns, 1992). Some of these works present better operational stabilities than the verified in our study due to the immobilization method used. The physical adsorption is known for having only weak bonds involved and, probably, the most pronounced loss of activity is due to enzyme leaching during washings. Nevertheless, the achieved values are good results and commercial laccase immobilized in coconut fiber by adsorption can be considered a good choice of insoluble biocatalyst to be used in continuous reactions studies.

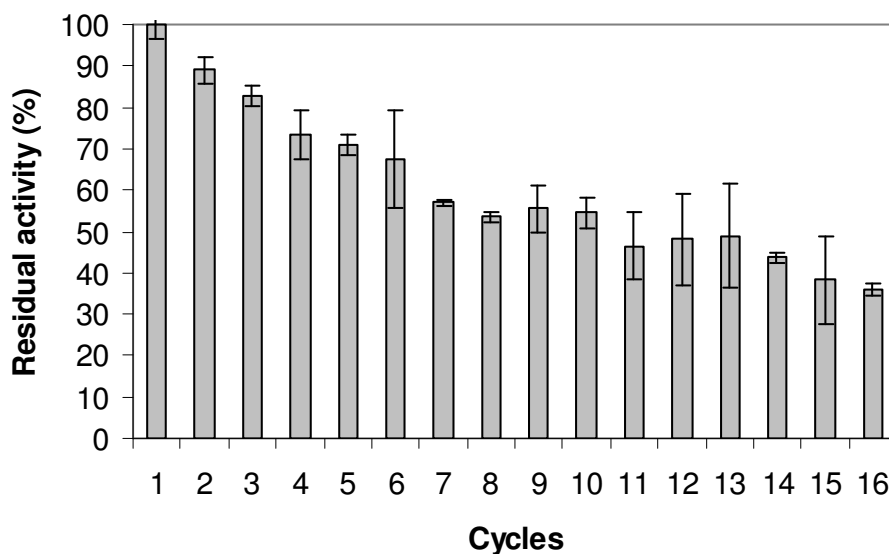


Figure V. 7 – Operational stability of commercial laccase immobilized on coconut fiber by adsorption.

#### V. 4.2.3 Kinetic properties

The free and the immobilized commercial laccase exhibited a normal behaviour of an enzyme reaction with ABTS as substrate. Thus, the kinetic parameters were calculated according to the classical Michaelis-Menten equation:

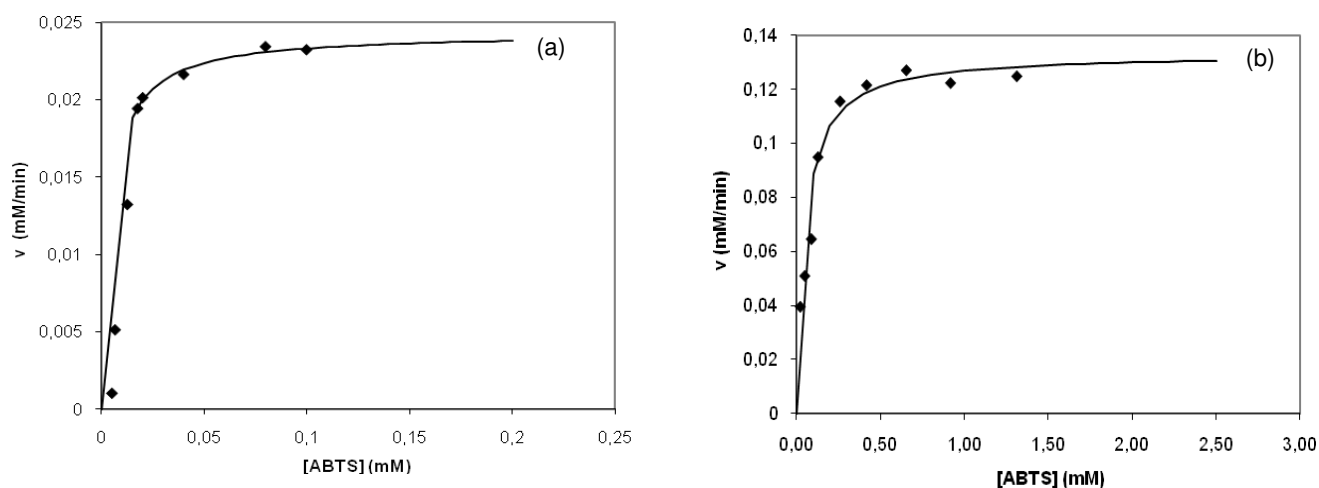
$$v = \frac{v_{max} [S]}{K_M + [S]} \quad (V. 3)$$

where  $v$  is the velocity of the reaction (mM/min),  $v_{max}$  is the maximum velocity (mM/min),  $K_M$  is the Michaelis-Menten constant and  $[S]$  is the ABTS concentration (mM).

The Michaelis-Menten parameters  $v_{max}$  and  $K_M$  were obtained by non-linear fitting of reaction rate versus substrate concentration using the MicroCal Origin software v.3.01 (SPSS Inc., Northampton, USA). It was tried to use the same initial enzyme activities in both studied cases. Table V. 5 shows the kinetic constants determined and Figure V. 8 shows the initial reaction rate of increasing concentrations of ABTS for free and immobilized commercial laccase. The solid line represents the fit of Michaelis-Menten model to experimental data.  $K_M$  value is most useful in proving the ability of an enzyme to bind its substrate (Yu et al., 2001). The lesser the value of  $K_M$ , the higher is the affinity for the substrate. An increase in the  $K_M$  value for the reaction of ABTS with the immobilized laccase was observed. The same results have been reported by other researchers (D'Annibale et al., 1999, 2000; Wang et al., 2008), indicating a lower affinity for the substrate caused by diffusional limitations and decreased enzyme flexibility after immobilization. Moreover, diffusional limitations are less significant in coconut fiber, as immobilization occurs on the surface due to the absence of porous. Diffusional substrate limitations (Davis and Burns, 1992), substrate partitioning, protein conformational changes (Gottschalk and Jaenicke, 1991) and decreased protein flexibility (Clark, 1994) have been associated with the decrease in the enzymatic properties after immobilization. However, the  $v_{max}$  value of the immobilized enzyme increased compared to the free enzyme, probably because of the adsorption by the support: the local concentration increases, increasing the reaction rate.

**Table V. 5** – Kinetic parameters of free and immobilized commercial laccase by adsorption on coconut fiber.

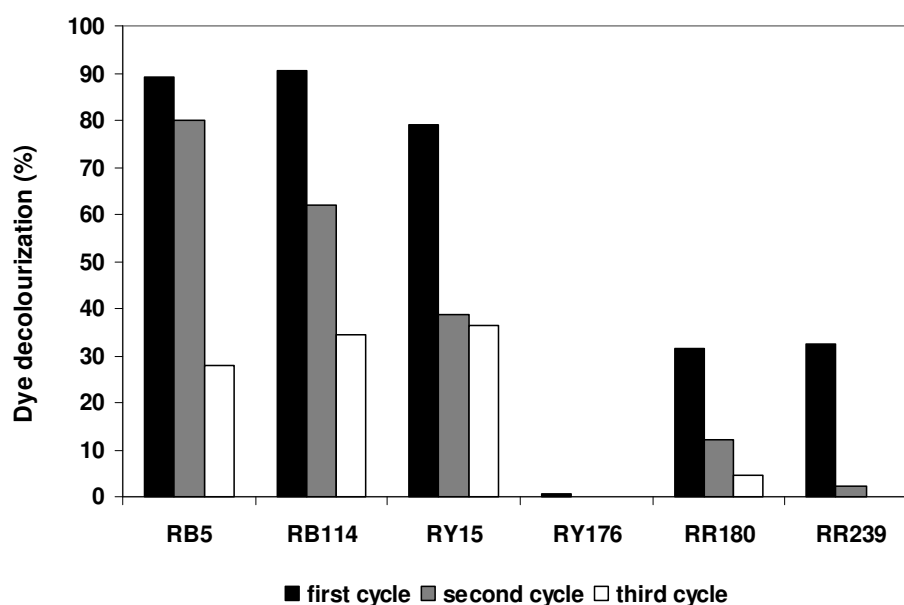
Enzyme	$K_M$ (mM)	$v_{max}$ (mM.min <sup>-1</sup> )
free	0.0044	0.024
immobilized	0.0501	0.133



**Figure V. 8** – Initial reaction rates for different concentrations of ABTS a) with free and b) with immobilized commercial laccase on coconut fiber. The solid line represents the fit of Michaelis-Menten model to experimental data.

#### V. 4.3 Dye decolourization by immobilized laccase

Decolourization of RB5, RB114, RR180, RR239, RY176 and RY15 were achieved in a batch reactor with commercial laccase immobilized on coconut fiber (Figure V. 9) for three cycles of reaction.



**Figure V. 9** – Degradation of RB5, RB114, RR180, RR239, RY176 and RY15 in a batch reactor by commercial laccase immobilized on coconut fiber for three cycles of reaction.

A high decolourization percentage of RB5, RB114 and RY15 were obtained in the first cycle, 90 %, 90 % and 80 %, respectively. For RR180 and RR239 a moderate degradation of 30

% was observed. No significant reduction of colour was observed for RY176. The second cycle presented a good degradation for both RB5 (80 %) and RB114 (62 %), whilst RY15 shows a significant decrease on the decolourization (39 %). A poor degradation for the third cycle was observed. This tendency can be explained, when compared to ABTS oxidation cycles (Figure V. 7), by the laccase mediator. It is known that no mediator is necessary for ABTS reaction with laccase. However, for most dyes and other phenolic compounds, a mediator is necessary to complete the catalytic cycle with laccase (Husain and Husain, 2008; Tavares et al., 2008, 2009a). The laccase used in this study is a commercial formulation which includes a mediator. The mediator probably is not being reoxidised, as occurs in a system with free enzyme. Thus, after some time there is no longer available mediator to oxidize the dyes. Additionally, the difference of dye decolourization percentage among the different dyes can be explained mainly due to the different molecular structure of the dyes and different potential redox as observed in an earlier study with free laccase (Tavares et al., 2009a).

When immobilized enzymes are used in decolourization studies the evaluation of the adsorption capacity of the support is necessary. Generally, the colour removal is the result of both enzymatic and adsorption processes. When an operation is carried out batchwise, the overall extent of decolourization is strongly affected by the physical removal of the dye from the liquid phase. Thus, another point that should be considered in this study is the colour removal by the adsorption on the support. Many dye decolourization tests carried out with immobilized laccase have showed that support adsorption presents a significant contribution to the colour degradation (Kandelbauer et al., 2004; Peralta-Zamora et al., 2003; Zille et al., 2003). In order to verify this tendency, a control experiment with dyes and support alone was carried out. The adsorption of the dye by the support surface was around 40 % for RB114, 48 % for RY15, 23 % for RB5, 4 % for RY176, 7 % for RR180 and no adsorption for RR239 was detected. These results show that, depending on the dye, in the first cycle of the reaction with immobilized laccase, a percentage of colour removal was due to adsorption of the dyes by the support. In the next cycles, partial saturation of the support occurred and the contribution of laccase increased. Using the supported laccase in experiments that involve the consecutive addition of several dye samples the catalytic effect of the enzyme is evidenced, maybe due to the progressive saturation of the active free-sites of the support. This was observed by Peralta-Zamora et al. (2003) applying consecutive feeds to a batch system loaded with immobilized laccases. Since the enzyme is only active in the presence of a mediator, they observed that, in the absence of the mediator, the extent of decolourization in the consecutive dye additions decreased as adsorption approached equilibrium; on the contrary, in the presence of the mediator, the extent of decolourization during each cycle remained constant up to eight dye additions. Comparing with dyes degradation (90 % for RB5, 90 % for RB114, 93 % for RY15, 96 % for RR239, 93 % for RR180 and 0 % for RY176) by free laccase (Cristóvão et al., 2008; Tavares et al., 2009b), at the same conditions of dye concentration, temperature and agitation, a considerable difference was observed. A decreased in all dyes degradation was observed



taking into account only the degradation by the immobilized laccase. This might be attributed to the diffusional limitations and the loss of laccase activity during the immobilization process.

As most industrial effluents contains a mixture of dyes, this part of the study is important in order to validate the applicability of the process. To our knowledge there is no study on degradation of a mixture of dyes by an immobilize laccase. The Table V. 6 shows the decolourization of a mixture of three dyes, RY15, RR239 and RB5, by the immobilized laccase and by the adsorption. The degradation of the mixture was obtained from both corresponding wavelength of each dye and the integration of the area of the all visible spectrum.

**Table V. 6** - Dye mixture degradation (%) by immobilized laccase based on the absorbance peak at maximum absorbance wavelength of each dye present in the mixture and on the area under all dye absorbance spectrum range. It was taked into account the percentage of adsorption and of enzymatic activity.

$\lambda$ (nm)	Total dye degradation (%)	Adsorption by the coconut fiber (%)	Dye degradation by the immobilized enzyme (%)
416	58	13	45
542	51	1.7	49
579	79	16	63
Area under all spectrum	54	0	54

When compared with a single dye, a decrease in dye degradation of the mixture was observed. This probably occurs due to the competition between several compounds for the active sites of the enzyme. Comparing the decolouration with free laccase (Cristóvão et al., 2009), at the same conditions of dye concentration, temperature and agitation, a considerable difference was also observed, a decrease in total decolouration of the mixture about 36 %, from 90 % (free enzyme) to 54 % (immobilized enzyme), was obtained with immobilized enzyme. This might be also attributed to the diffusional limitations and the loss of laccase activity during the immobilization process.

## V. 5 Conclusions

Green coconut fiber was successfully used to immobilize commercial laccase by adsorption in the optimized conditions. A high decolourization percentage of practically all reactive textile dyes in the first two cycles and a good dye mixture decolourization by the immobilized enzyme were obtained. Despite the observed dye degradations are not higher than

those observed with free enzyme, the laccase immobilization allows enzyme reuse (with high operational stabilities) and has been shown to improve its stability, which could be a potential advantage in wastewater treatment. In addition, immobilization on green coconut fiber by adsorption of commercial laccase DeniLite II S is a simple and inexpensive method with an easily available support. This work may provide a basis for the development of suitable biocatalysts for continuous colour removal from various industrial effluents at large scale.

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## **Part VI**

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# Supercritical Carbon Dioxide Media



*In part VI the degradation of the reactive textile dyes by commercial laccase in supercritical carbon dioxide media is investigated. The operational conditions are optimized by experimental design combined with response surface methodology.*





## **Part VI** Optimization of laccase catalyzed degradation of reactive textile dyes in supercritical carbon dioxide media by response surface methodology\*

VI. 1 Abstract

VI. 2 Introduction

VI. 3 Materials and Methods

VI. 4 Results and Discussion

VI. 5 Conclusions

VI. 6 References

*\*based on: Cristóvão, R., Amaral, P., Tavares, A., Coelho, M., Cammarota, M., Loureiro, J., Boaventura, R., Macedo, E., Pessoa, F., 2010. Optimization of laccase catalyzed degradation of reactive textile dyes in supercritical carbon dioxide media by response surface methodology. Reaction Kinetics, Mechanisms and Catalysis, 99, 311-323*



## **VI Optimization of laccase catalyzed degradation of reactive textile dyes in supercritical carbon dioxide media by response surface methodology**

### **VI. 1 Abstract**

In this work, the laccase catalyzed degradation of reactive textile dyes was studied in supercritical carbon dioxide media. A two level Box–Behnken factorial design with two factors and response surface methodology (RSM) were performed to investigate and optimize the effects of pressure and temperature on reactive red 239 (RR239), reactive yellow 15 (RY15) and reactive black 5 (RB5) dye degradations by commercial laccase in supercritical carbon dioxide media. Mathematical models were developed for each dye showing the effect of each factor and their interactions on colour removal. Pressure and the interaction between temperature and pressure were the main factors affecting the decolourization. The optimum conditions for RB5 and RY15 were found to be high pressure values (>120 bar), whilst temperature presented low effect on their degradation at these pressures. For RR239, both variables influenced the decolourization and the optimum conditions appear to be at low values of pressure and high values of temperature.

### **VI. 2 Introduction**

The use of supercritical fluids as nonaqueous solvents for enzyme-catalyzed reactions has been an innovative area of research for the last times (Cantone et al., 2007; Habulin et al., 2008a; Hammond et al., 1985; Palocci et al., 2008; Randolph et al., 1985). Many substrates as well as many reaction products have low solubility in water, making biocatalyzed reactions difficult to employ in aqueous phase. By using enzymes in nonaqueous solvents, it is possible to overcome this barrier, but their uses in organic solvents have been limited by relatively low catalytic activity observed when compared to reactions in water (Celia et al., 2005). Therefore, in addition to ongoing research in solvent free systems, synthesis in supercritical fluids can be potentially preferred as a new alternative to enzyme catalyzed reactions.

The ability to manipulate the physical properties of the solvent by simply changing the pressure or temperature is unique to supercritical systems (Erickson et al., 1990; Nakamura et al., 1990). Therefore, supercritical fluids are attractive media to perform and, more importantly, control biocatalytic reactions.

Actually, an increasing number of works was reported on the basic studies relating to supercritical fluid dyeing (SFD) such as dyes solubility measurements (Kim et al., 2006). The use of dyes in supercritical media has been directed as a new concept of dyeing to replace the

traditional wet dyeing process (Jun et al., 2004; Montero et al., 2000). The traditional dyeing processes cause environmental problems such as water pollution due to the inevitable use of an excess amount of water and the discharge of unfixed dyes and various chemical additives. However, few studies about the treatment of textile effluents in supercritical fluids have been published. Conventional methods of textile wastewater treatment include adsorption, coagulation/flocculation, electrochemical methods, membrane separation, ozonation and biological oxidation. The disadvantages of some of these treatments are the potential toxicity of dyes and their degradation products, especially the suspected carcinogenicity of potential intermediate products. Supercritical treatment shows to be a promising clean technology for efficient decontamination of many aqueous organic wastes like textile wastes. The oxidation of organic compounds contained in aqueous waste effluents is carried out in supercritical water. Future applications are also foreseen in supercritical CO<sub>2</sub> oxidation to treat contaminated effluents (Schmieder and Abeln, 1999).

In enzymatic catalysis, the supercritical fluid carbon dioxide has been used in benefit of making the enzyme reactions greener, because of being a natural, unregulated solvent, with low cost and low toxicity, non-flammability and high availability (Braker and Mossman, 1980; Habulin et al., 2008a). Apart from being non-toxic, easily available and cheap, many enzymes proven to be stable and active in it (Primo et al., 2007). Besides, carbon dioxide offers possibilities to reduce the reactor volumes to a great extent and to accelerate enzymatic processes (Hauthal, 2001). The gaslike diffusivities and low viscosities enhance mass transfer rates of reactants to the active sites on enzymes dispersed in supercritical fluids. Reactions which are limited by the rates of diffusion, rather than intrinsic kinetics, will proceed faster in supercritical fluids than in liquids (Cantone et al., 2007).

Many industrial applications are hindered by the obstacle that high-pressure equipment can be quite costly. Despite this difficulty, the attraction of combining natural catalysts with green solvents has been the driving force behind a growing body of literature concerning the stability, activity, and specificity of enzymes in supercritical carbon dioxide (Martym et al., 1990).

Recent studies have shown that fungi or their enzymes are able to decolourize and detoxify industrial dyes (Amaral et al., 2004; Cristóvão et al., 2008; Romero et al., 2006; Tavares et al., 2008). Enzyme methods applied in dye degradation have low energy costs, are easy to control and have low impact on ecosystems. Laccase (benzendiol:oxygen oxidoreductase, EC 1.10.3.2) has been studied in the oxidation of textile dyes. Studies have shown that the range of substrate specificity of laccases can be extended to non-phenolic substrates by the addition of redox mediators (Tauber et al., 2005; Tavares et al., 2009a). Although the enzymatic treatment presents good results in concern with dye decolourization (above 90% degradation), toxic dye degradation products can be formed (Tauber et al., 2005). These products can also be more toxic than the pollutant. In order to avoid this, the treatment with supercritical carbon dioxide was studied as an alternative solvent for enzymatic synthesis,

as it is known to leave no residues in the products and to be easy to separate of the unreacted substances (Celebi et al., 2007; Habulin et al., 2008b; Palocci et al., 2008).

In this study parameters such as temperature and pressure were examined to optimize the reactive textile dye degradation in supercritical medium. For this purpose, a two-level Box–Behnken full factorial design coupled with RSM was employed to maximize the decolourization of three reactive textile dyes, reactive black 5 (RB5), reactive yellow 15 (RY15) and reactive red 239 (RR239) by commercial laccase in supercritical carbon dioxide medium.

## **VI. 3 Materials and Methods**

### **VI. 3.1 Chemicals and enzyme**

Textile dyes: Reactive yellow 15 (Remazol Yellow GR), reactive red 239 (Remazol Brilliant Red 3BS) and reactive black 5 (Remazol Black B) were kindly provided by DyStar (Porto, Portugal).

Enzyme: Commercial laccase formulation (DeniLite II S; 120 U/g) from genetically modified *Aspergillus* was kindly provided by Novozymes (Germany). This formulation is used for indigo dye decolourization in denim finishing operations and includes a buffer and an enzyme mediator.

### **VI. 3.2 Factorial design for dye decolourization in supercritical media**

The response surface methodology (RSM) is a collection of statistical and mathematical techniques useful for developing, improving and optimizing processes. Additionally, the factors that influence the experiments are identified, optimized and possible synergic or antagonistic interactions that may exist between factors can be evaluated (Box et al., 1978). The accuracy of the models generated is evaluated by the coefficient of determination  $R^2$ . RSM is a multivariate technique that mathematically fits the experimental domain studied in the theoretical design through a response function.

A  $2^2$  Box–Behnken full factorial design, including one replicate at the central point, was carried out in order to study the factors (temperature and pressure) that influence the decolourization of reactive textile dyes by commercial laccase in supercritical carbon dioxide media (Table VI. 1). The factors temperature and pressure were chosen since they are known to be important parameters for synthesis of chemical compounds in supercritical carbon dioxide medium (Hartmann et al., 2001; Lin et al., 2006; Razei et al., 2007), and once the other parameters such as pH and enzyme concentration had been optimized in aqueous medium and we wanted to use the same values. On the basis of preliminary experiments, the values of temperature and pressure were defined taking into consideration the dyes degradation by enzyme laccase in aqueous medium (Cristóvão et al., 2008; Tavares et al., 2009b). Therefore, the ranges of temperature and pressure were: 30 to 50 °C and 60 to 120 bar, respectively. It is

important to point out that carbon dioxide is a near critical fluid at 30 °C and 60 bar, once its critical temperature and pressure are 31 °C and 73.8 bar, respectively.

This design establish both linear and quadratic models determining their accuracies by comparing lacks of fit of model predictions to experimental points with experimental error estimated from replicates at the central point. Table VI. 1 gives the range and the levels of the variables investigated and the experimental design. The experimental Box–Behnken design, analysis of variance (ANOVA) and 3D response surface were carried out using the software Statistica v.5.1 (Statsoft Inc.). Equation VI. 1 describes the regression model of the present system, which includes the interaction term:

$$\hat{Y} = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_{12} x_1 x_2 \quad (\text{VI. 1})$$

where  $\hat{Y}$  is the predicted response, i.e. the colour removal;  $x_1$  and  $x_2$  are the coded levels of the independent factors pressure and temperature, respectively. The regression coefficients are:  $\beta_0$  the intercept term;  $\beta_1$  and  $\beta_2$  the coefficients for linear effects and  $\beta_{12}$  the coefficient for interaction effects. The model evaluates the effect of each independent factor on the response.

### VI. 3.3 Dye decolourization experiments

The laccase catalyzed degradation of reactive black 5, reactive yellow 15 and reactive red 239 was performed in a supercritical fluid medium batch reactor. The system consisted of a high-pressure syringe pump, a reactor, a controller unit and an adjustable flow rate restrictor. Experiments were carried out with 50 mg/L of each dye and 432 U/L of commercial laccase dissolved in 40 mL of phosphate buffer (50 mM, pH = 7.0) with a total volume of 50 mL. Cooled carbon dioxide was fed into the high-pressure reactor, pressurized at the desired target pressure by the syringe pump and heated to the reaction temperature, with a stirring rate of 320 rpm. This step was quite fast, so the conversion degree was ignored during it. The experiments lasted for 2 hours after the temperature and pressure were stable. The starting point of the reaction was assumed to be when both the pressure and temperature of the system reached the abovementioned values. The conditions were chosen by the previously optimum conditions determined by the studies in aqueous medium (Cristóvão et al., 2008; Tavares et al., 2009b).

### VI. 3.4 Determination of dye decolourization

Dye decolourization by laccase was determined by monitoring the decrease in the absorbance peak at the maximum wavelength (peak) for each dye: reactive yellow 15 (416 nm), reactive red 239 (542 nm) and reactive black 5 (579 nm). A UV-visible spectrophotometer (Hach DR/4000 UV) was used in all experiments. Decolourization is reported as: % decolourization =  $(A_i - A_f)/A_i \times 100$ , where  $A_i$  is the initial absorbance and  $A_f$  is the final absorbance.

## VI. 4 Results and Discussion

### VI. 4.1 Experimental design

In order to optimize the dye degradation conditions, Box–Behnken full factorial design with two factors (pressure and temperature) was chosen. The levels of the factors and the results from the 5 experiments for each dye are presented in Table VI. 1. The dye decolourization results calculated by the models (Equations VI. 2 – VI. 4), at each experimental point, are also presented in Table VI. 1. The optimum operating conditions for each dye can be predicted from the second-order polynomial function.

Using the experimental data, the second order polynomial model was fitted to decolourization results of RB5, RR239 and RY15 and obtained in terms of coded factors:

$$\hat{Y}\hat{y}(\text{RB5}) = 49.2 + 0.16x_1 - 0.10x_2 + 0.003x_1x_2 \quad (\text{VI. 2})$$

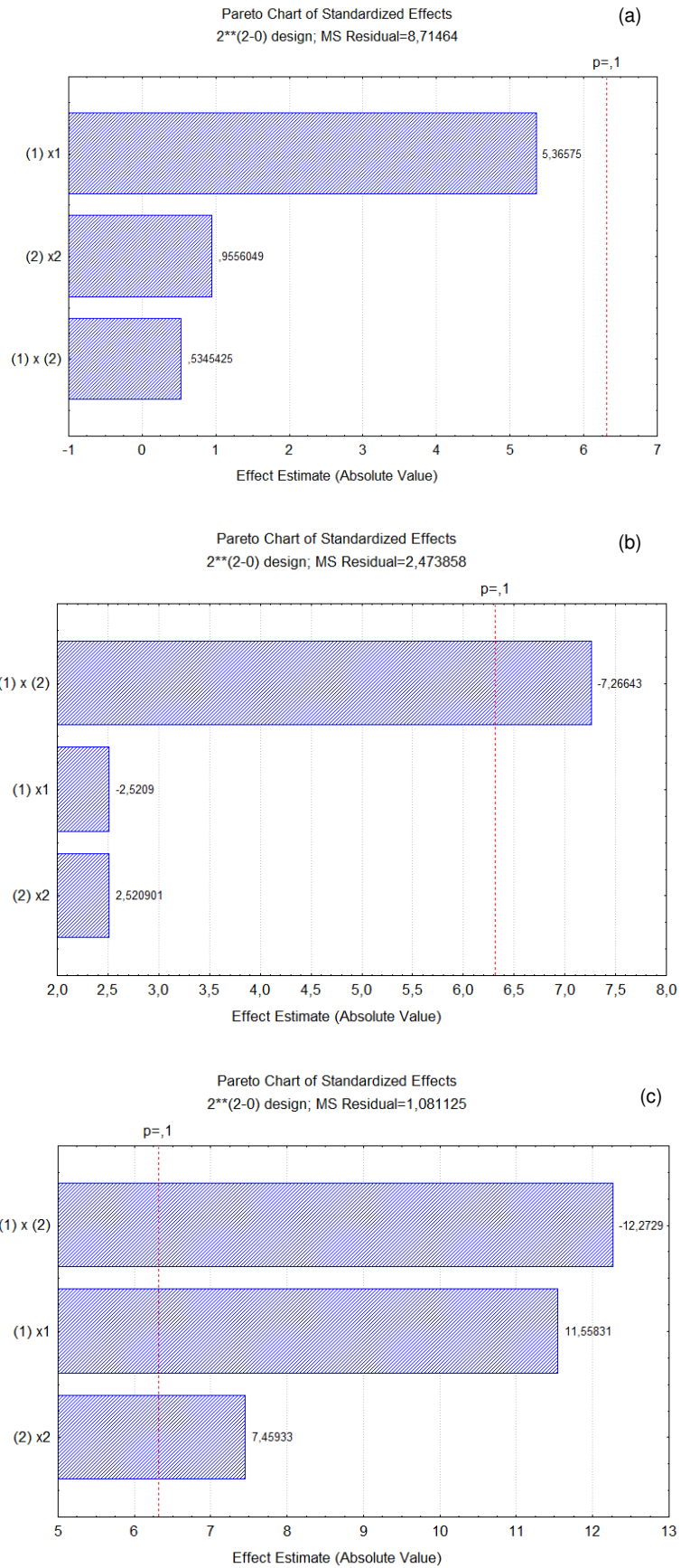
$$\hat{Y}\hat{y}(\text{RR239}) = 64.5 + 0.70x_1 + 1.91x_2 - 0.019x_1x_2 \quad (\text{VI. 3})$$

$$\hat{Y}\hat{y}(\text{RY15}) = 42.5 + 1.05x_1 + 2.30x_2 - 0.021x_1x_2 \quad (\text{VI. 4})$$

**Table VI. 1** – Comparison between experimental data and calculated values for RB5, RR239 and RY15 decolourization.

Runs	Factors		Dye degradation (%)					
	$x_1$ pressure (bar)	$x_2$ temperature (°C)	RB5		RR239		RY15	
			Actual Value	Calculated Value	Actual Value	Calculated Value	Actual Value	Calculated Value
1	60	30	59.94	60.60	0	0.35	51.54	51.30
2	60	50	61.19	61.85	15.39	15.75	72.05	71.82
3	120	30	74.21	74.87	7.46	7.82	76.31	76.08
4	120	50	78.61	79.27	0	0.35	71.31	71.08
5	90	40	71.79	69.15	7.47	6.07	66.64	67.57

The Pareto chart displays the statistically relevant effect of each factor on the response and it is a practical mode to view the results. These are sorted from the largest to the smallest, and the effects to the right of the divisor line are considered statistically significant. From Figure VI. 1, it is possible to observe that there is no significant effect for RB5, all the effects are to the left of the divisor line corresponding to a  $p$  value of 0.1. For RR239 the only significant effect was the interaction between both factors (pressure and temperature), but for RY15 all the factors were significant, although the temperature had a much smaller influence.



**Figure VI. 1** – Pareto chart of standardized effects for 2<sup>2</sup> Box-Behnken factorial design for (a) RB5, (b) RR239 and (c) RY15 degradation. (1) pressure; (2) temperature.



The statistical significance of the polynomial model for the experimental responses (Table VI. 1) was evaluated by analysis of variance (ANOVA). According to the ANOVA results (Table VI. 2), the models present high determination coefficients ( $R^2$ ): 0.937, 0.985 and 0.997 for the degradation of RB5, RR239 and RY15, respectively. These results indicate that the accuracy of fitting of the polynomial models was good. The values of adjusted determination coefficients  $R^2_{adj}$  are also high to advocate for high significances of the models. The results showed that the experimental values were significantly in agreement with the calculated values and also suggested that the models (Equations VI. 2 – VI. 4) were satisfactory and accurate (Figure VI. 2).

**Table VI. 2** – Analysis of variance (ANOVA) for the fitted quadratic polynomial models of RB5, RR239 and RY15 decolourization.

Source	Sum of squares (SS)			df <sup>a</sup>	Mean Square (MS)			F-value			p-value		
	RB5	RR239	RY15		RB5	RR239	RY15	RB5	RR239	RY15	RB5	RR239	RY15
$x_1$	250.9	15.7	144.4	1	250.9	15.7	144.4	28.8	6.35	133.5	0.117	0.24	0.055
$x_2$	7.96	15.7	60.2	1	7.96	15.7	60.2	0.913	6.35	55.6	0.514	0.24	0.085
$x_1$ by $x_2$	2.49	130.6	162.8	1	2.49	130.6	162.8	0.286	52.8	150.5	0.687	0.087	0.052
<b>Error</b>	8.71	2.47	1.08	1	8.71	2.47	1.08						
<b>Total SS</b>	270.1	164.5	368.5	4									

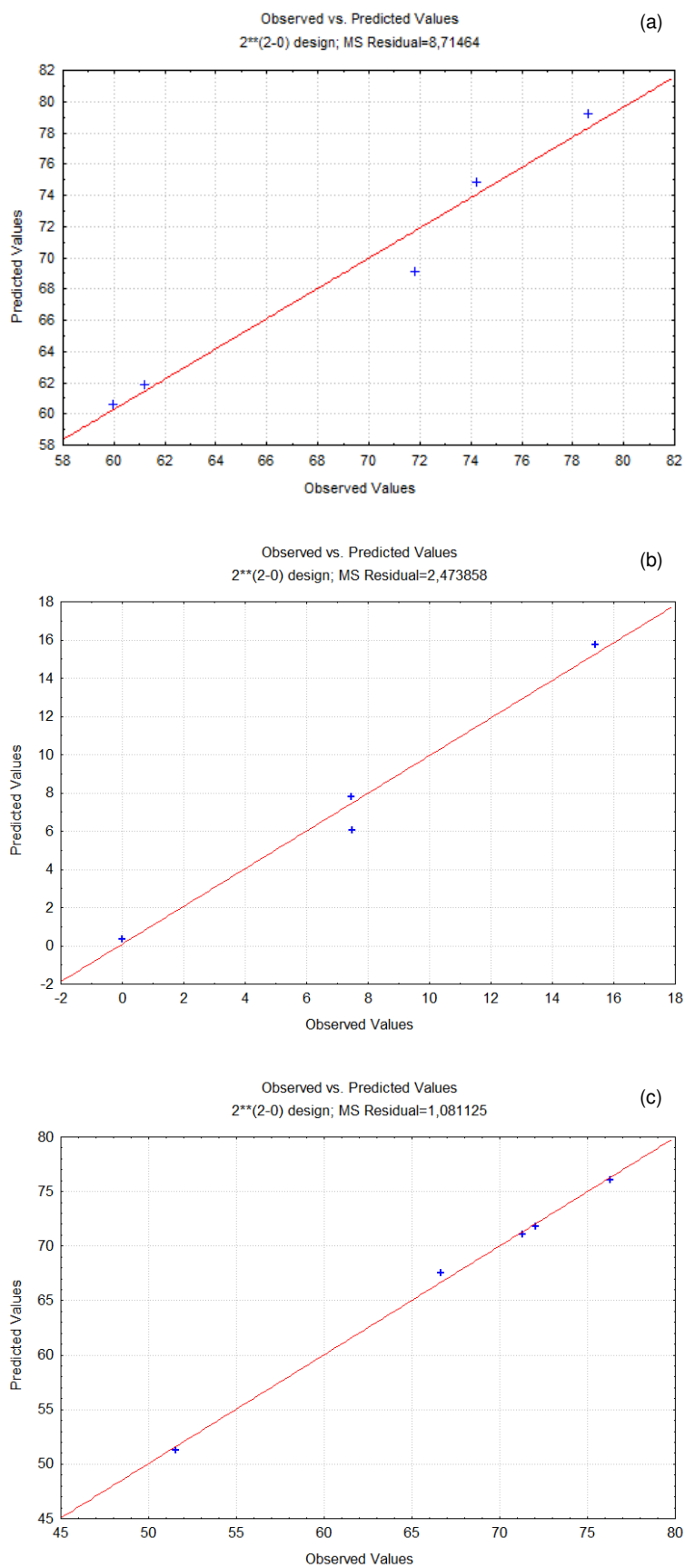
df<sup>a</sup>: degrees of freedom

RB5:  $R^2 = 0.938$ ;  $R^2_{adj} = 0.871$

RR239:  $R^2 = 0.985$ ;  $R^2_{adj} = 0.940$

RY15:  $R^2 = 0.997$ ;  $R^2_{adj} = 0.988$

The significance of each coefficient was determined through a  $p$  value test, considering 90 % of confidence, in which low  $p$  values ( $p < 0.1$ ) indicate a high significance of the corresponding coefficient. It was possible to observe by the analysis of variance (Table VI. 2) that the interaction between both factors and the pressure were the factors that influenced most the degradations, since they presented the lowest values of  $p$ . The variable temperature was shown to be almost statistically insignificant.



**Figure VI. 2** – Observed vs predicted values in the degradation of (a) RB5, (b) RR239 and (c) RY15 in supercritical carbon dioxide. + observed; – predicted.

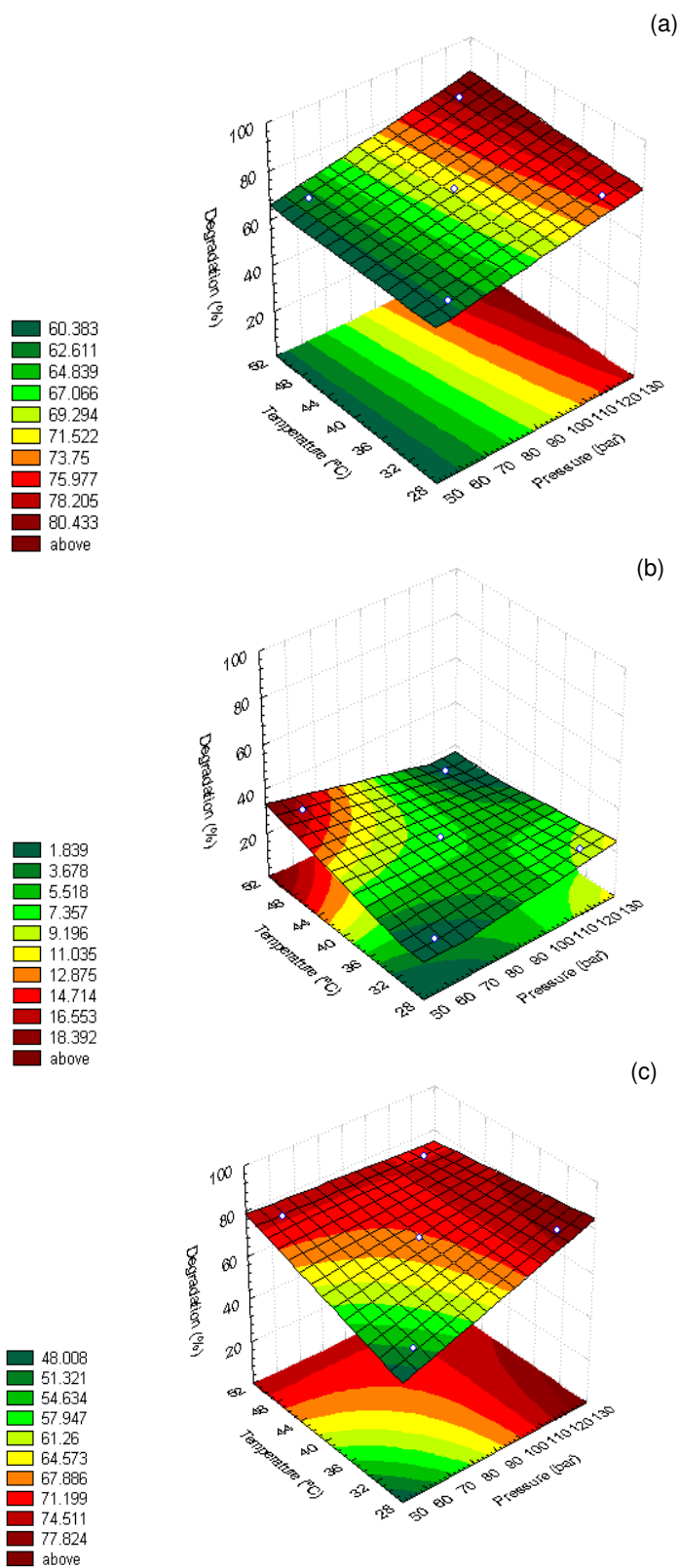
Using RSM, the effects of the independent factors (pressure and temperature) and their interaction on the dyes decolourization are represented, the response can be predicted and the optimum values of decolourization can be determined. The response surface plots (Figure VI. 3) show the decolourization in supercritical medium of RB5, RR239 and RY15 as function of the two factors.

Figure VI. 3a represents the response surface for RB5 decolourization. The surface plot shows the increase in dye degradation with increasing pressure values. The plot clearly shows that the decolourization of this dye in supercritical carbon dioxide was sensitive to small pressure variations. The temperature slightly influenced the decolourization. This influence is a little clearer for higher values of pressure. So, the degradation (>80 %) seems to increase with the increase of both factors.

The response surface plot of RR239 degradation is presented in Figure VI. 3b. From the results, it can be observed that this dye does not present a very consistent behaviour. At low pressures it seems that the degradation increases with the increase of temperature but for high pressures, despite being less pronounced, the opposite happens. So, it seems that the maximum decolourization of RR239 (>15 %) is given by the increase of temperature and by the decrease of pressure. However, it should be considered that it is not possible to work at temperatures much higher than that studied, because it can deactivate the enzyme. Nevertheless, it does not seem possible to attain large percentages of degradation of this dye with this method. From previous studies in aqueous medium, the red dye was also the most difficult dye to degrade (Cristóvão et al., 2008). The degradation of each dye depends on the redox potentials of each substance (Tavares et al., 2009a). The RR239 is the dye with the highest redox potential, thus being the most difficult dye to degrade.

Finally, the response surface plot of RY15 degradation is presented in Figure VI. 3c. For this dye it is evident that the degradation increases with the increase of pressure and temperature. The degradation is low for low values of both variables. But at low pressures, when the temperature increases, the dye degradation starts to increase as well, and the same happens at low temperatures when the pressure increases, leading to degradations above 76%. At high pressures the temperature influences almost nothing the dye degradation and vice versa. For this dye the variables present almost the same influence in the degradation, despite pressure being the variable that influences a little more.

By Figure VI. 3 it is possible to observe that the response surface plots of all the three dyes were very different, which we think that could be explained by the structure and by the redox potential of each dye. The dyes present very different structures, with many different bonds, what influences each dye degradation by the laccase-mediator system. After studying the potential redox of the enzyme and of each dye studied (Tavares et al., 2009a), it is possible to conclude that the degradation is strongly influenced by the potential redox of each substance, leading to the different response surface plots. The lesser the value of the redox potential of the dye, the larger is the degradation by the enzyme laccase.



**Figure VI. 3** - Response surface plot for decolourization of (a) RB5 (b) RR239 and (c) RY15 in supercritical carbon dioxide as a function of pressure and temperature.

The results presented show that pressure was the most relevant factor for the decolourization of the three dyes in supercritical medium. As is known supercritical fluids are compressible. A small change in pressure is accompanied by a dramatic change in density, thus altering the physical properties of the supercritical fluid. Since the properties of the fluid may modulate the enzyme properties suspended therein, the effect of pressure on enzyme-catalyzed reactions in supercritical fluids is probably an important factor (Mesiano et al., 1999). Ikushima et al. (1995) reported that pressure could induce modification of both structure and function of enzyme particles leading to a change in the enzyme activity. The interactions between carbon dioxide and enzyme molecules, in the near critical region, are increased and enabled to stimulate conformational changes in the enzyme, even though their role during the catalytic step is not yet well understood.

DeniLite II S is a commercial laccase with great potential to decolourize textile dyes. There are few studies regarding the use of this enzyme on the treatment of effluents containing dyes, especially with reactive dyes (Cristóvão et al., 2008; Soares et al., 2002; Tavares et al., 2009b). Some reports of the literature show the chemical treatment of textile wastewater by supercritical water oxidation (Sogut and Akgun, 2007). However, to our knowledge, this is the first work on dyes degradation by commercial laccase in supercritical carbon dioxide medium. The enzymatic reactions in supercritical carbon dioxide are attractive due to its low toxicity and cost, as well as its environmental friendliness, among other characteristics (Braker and Mossman, 1980). Other advantage of using a supercritical fluid is that its physical properties can be manipulated by merely changing the temperature or pressure of the reaction system. However, the results obtained showed that a higher degradation is achieved most often when the pressure is increased. It is known that high pressure equipment can be quite costly, hindering many industrial applications. While there are examples that clearly demonstrate that the use of supercritical carbon dioxide can be advantageous, one must still realize that there are certain economic issues that may prevent the implementation of this method in some processes. So, for technical application of supercritical fluids the benefits gained must be carefully weighed against the higher costs of supercritical process technology. This balancing will limit economic and beneficial applications. In this study, apart of high pressure being preferred, the results of degradation seem to be lower than those obtained in aqueous medium, despite of being studied in a shorter reaction period (3 h against 24 h in literature) (Cristóvão et al., 2008; Tavares et al., 2009b). So, it seems that for the reactive textile dye degradation by commercial laccase, it is preferable to work in aqueous medium instead of working in supercritical conditions, since it is cheaper and more efficient.

## **VI. 5 Conclusions**

Commercial laccase (DeniLite II S) was tested for decolourization of reactive textile dyes in supercritical carbon dioxide medium. The Box–Behnken statistical experimental design

and response surface methodology were found to be efficient tools to optimize these reactions conditions. The optimum conditions for RB5 and RY15 in the range studied were found to be high pressure values (>120 bar), whilst temperature presented a reduced effect on their degradation at these pressures. For RR239 both variables (pressure and temperature) influenced the decolourization and, despite of having a strange behaviour, the optimum conditions in this range appear to be at low values of pressure and high values of temperature.

Pressure was the factor that influenced most the dyes degradation, probably due to the fact that a small change in pressure causes dramatic variations in the density of supercritical fluids, altering their physical properties. So, pressure may have the capacity of induce modification on both the structure and function of enzyme particles leading to a change in the enzyme activity.

Despite the use of supercritical carbon dioxide present many advantages, probably it is not the best technique for this process. This method implies the use of high pressures which makes the equipment cost quite expensive and the degradation results obtained are not better than those obtained in aqueous medium. Therefore, it seems that the benefits of using a supercritical fluid do not outweigh the disadvantages founded.

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## **Part VII**

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### Conclusions and Future Work



## VII. 1 Conclusions

The aim of this thesis was the study of the reactive textile dyes degradation by laccase, the optimization of operative conditions and the kinetic modelling of the process.

The best working conditions for the catalysis of the six reactive textile dyes studied (reactive black 5, reactive blue 114, reactive yellow 15, reactive yellow 176, reactive red 239 and reactive red 180) by laccase (DeniLite II Base) were established by testing five traditional mediators (ABTS, VA, HBT, NHA and TEMPO), the mediator concentrations, temperature and pH. Laccase without mediator did not decolourize any dye during the incubation time, demonstrating that these reactive dyes were not primary substrates for laccase. When a redox mediator was introduced, there was already degradation of dyes whose extension depends on the dye and on the mediator. ABTS was the most effective mediator leading to higher decolourization. The optimum temperature and pH values were 35 °C and 5.0, respectively, for maximum decolourization (above 70 %) of reactive black 5, reactive blue 114 and reactive yellow 15. For reactive red 239 the optimum conditions were found to be 40 °C and pH 4.5 (above 56 % decolourization). Reactive yellow 176 and reactive red 180 were not decolourized at any of these conditions. Three level Box-Behnken factorial design with three factors (pH, temperature and enzyme concentration) combined with response surface methodology was applied to optimize dyes degradation with commercial laccase (DeniLite II S). pH proved to be the principal factor that affects the decolourization of all dyes. The mathematical models developed estimate a degradation equal or above 90 % for all reactive dyes with the exception of reactive yellow 176, that was not degraded. A comparison between dye decolourization by absorbance reduction at the maximum absorbance wavelength and total colour removal based on the overall spectrum was made, showing that the second was less efficient, probably due to the degradation products formed during the decolourization of some of the dyes. These results are very promising and reveal the potential of laccase mediator system for reactive dye decolourization since it has been reported that these dyes are only 10% (on average) removed by conventional treatments.

The large variation in the decolourization percentage of the six different reactive dyes by laccase-mediator system can be explained by voltammetric studies. The voltammetric measurements showed a remarkably good linear correlation between the percentage of decolourization of each dye and the respective anodic peak potential: the efficiency of decolourization by laccase increases with decreasing dye oxidation potential. It was thus demonstrated that the redox potential differences between the biocatalysts and the dyes are a relevant preliminary tool to predict the decolourization capacity of oxidative and reductive biocatalysts.

The sequential decolourization of the reactive textile dyes by laccase mediator system during seven cycles demonstrated that the treatment with laccase can be used over a long

period, proving the feasibility of biological catalysts and their reuse in reactive dyes degradation. Thus, laccase mediator systems may be applied for the treatment of textile dyeing effluents.

As real industrial effluents often contain several mixtures of unfixed and hydrolyzed dyes, as well as salts, sizing agents and auxiliary chemicals, the degradation by commercial laccase of a mixture of three reactive dyes (reactive black 5, reactive yellow 15 and reactive red 239) and of a synthetic dye house effluent, simulating a real textile wastewater, containing the three dyes, salts and auxiliary chemicals were tested in the previously optimized conditions in a batch reactor, in order to evaluate the applicability of this method to a real situation.

A high decolourization of the simulated textile effluent was achieved at the maximum wavelength of reactive black 5 (above 86 %). The decolourization at the other dyes wavelengths (above 63 % for reactive yellow 15 and around 41 % for reactive red 239) and the total decolourization based on all the visible spectrum (around 55 %) were not so good, being somewhat lower than in the case of the mixture of the dyes (above 89 % for RB5, 77 % for RY15, 68 % for RR239 and above 84 % for total decolourization) which, in turn, is already lower than the degradation of each of these dyes. This is probably due to the competition between several compounds for the active sites of the enzyme, to the formation of strong chemical bonds with the species involved in the degradation process, to the enzyme deactivation or to the polymerization of the reaction products that can provide unacceptable colour levels in effluents. Even so, the good results of decolourization as measured by the percentage of absorbance reduction at the maximum absorbance wavelength of each dye and by the total colour removal based in all the visible spectrum indicate the possibility of implementing this technique for textile wastewater treatment.

The water quality analysis (total organic carbon, chemical oxygen demand, biochemical oxygen demand and toxicity) showed that values below the maximum permissible discharge limits for textile industrial wastewaters are achieved if the degradation is carried out with immobilized commercial laccase.

Mathematical models based on Michaelis-Menten equation were developed to simulate the kinetics of commercial laccase decolourization of the separated reactive dyes, of their mixture and of the simulated effluent in a batch reactor. The unusual kinetic behaviour of some of these reactions suggests that the kinetic model must consider the activation of the laccase mediator system. Kinetic constants were determined by minimizing the difference between the time courses predicted by the model and the experimental ones. The close correlation between the predicted and the experimental results seems to support the reliability of the established models. Thus with the knowledge of these models it is possible to predict the system performance under different operating conditions, reactor design, scale-up, optimization and control of the system. In principle, the models can be applied whenever the commercial laccase is used in the degradation of reactive dyes (from an effluent with only one reactive dye up to a real effluent). But the fact that the behaviour of the commercial laccase changes with the colour of the dye and with the effluent composition indicates that they should be used with care.

In order to perform the treatment of textile effluents by enzymatic catalysis at large-scale and to obtain an effluent with parameters below the legal discharge limits the immobilization of commercial laccase by physical adsorption into coconut fiber was also studied. The immobilization conditions (enzyme concentration, contact time and pH) were optimized obtaining an immobilized enzyme with thermal and operational stabilities improved when compared with the free commercial laccase. Despite the degradations of practically all reactive dyes and of their mixture in batch reactors are lower than those obtained by the free enzyme, the decolourizations achieved, the enzyme reuse and the improvement in stability indicate the potential of the immobilized enzyme for continuous applications in the wastewater treatment of textile industries.

The laccase catalyzed degradation of the reactive dyes was also tested in supercritical carbon dioxide media as a promising clean technology. The effect of pressure and temperature in the system were investigated using the experimental design and the response surface methodology. Pressure was the most relevant factor. The results obtained showed that a higher degradation is achieved most often when the pressure is increased, turning it in an expensive process. Since the results in supercritical media are not so good as those found in aqueous solution, despite its advantages, it seems preferable to perform reactive dyes degradation by commercial laccase in aqueous medium, since it is a cheaper and more efficient method.

In summary, it was demonstrated that the laccase catalyzed system is an efficient method for the decolourization of reactive textile dyes containing wastewaters (the most difficult to degrade dyes), although further studies are recommended for implementing a continuous system. The results obtained for this enzymatic treatment of industrial textile dye effluent and respective kinetic models could be the bases for a wide range of other similar dyes, suggesting its suitability for larger scale applications. Moreover, compared to the common and often expensive physical or chemical ways for dye effluent remediation, the biodegradation by the use of commercial laccase appears to be an attractive alternative.

## **VII. 2 Future Work**

The work described in the present thesis allowed to retrieve important information about the use of laccase in textile applications. Significant steps forward are possible and efforts are already being made in that direction.

Studies of simulated textile effluent degradation with the immobilized laccase should be performed in batch reactor to understand the impact of salts and auxiliary chemicals on the decolourization. The best conditions for effective degradation should be determined and environmental parameters must be also evaluated.

Studies of immobilization should be more thorough regarding the enzyme reuse in a continuous mode. Possibly, the immobilization of the pure laccase (DeniLite II Base) and the subsequent addition of a mediator, which is re-oxidized during the process will be needed to get a good degradation for a longer period of time. Different and more efficient immobilization supports and techniques should also be investigated to improve immobilized laccase dye decolourization.

Based on batch reactor results, studies carried out in a continuous reactor with immobilized enzyme should be made. For this, an experimental set-up that includes a continuous fixed bed reactor can be created. Several parameters must be considered and optimized, e.g., flow-rate, immobilized enzyme activity and temperature.

The decolourization of a real effluent from a textile industry in the continuous reactor with immobilized laccase should be evaluated in order to examine the effectiveness of the method to a more complex system. The effect of real textile wastewater components on the enzymatic degradation may be different, so it is recommended that the kinetic behaviour of these reactions should also be characterized and modelled. Comparing the kinetics of the simulated and real effluents may help to identify other components and the knowledge of its behaviour over time will allow to develop better strategies in order to maintain long term enzyme stability. Once a kinetic model is obtained, an enzyme reactor can be sized, allowing the development of a pilot treatment plant to apply in a textile industry.

Further study should consider different and less polluting mediators such as the natural mediators produced by laccase in natural environment during lignin degradation (acetosyringone, syringaldehyde, etc.).

Studies should be performed in order to understand the laccase mediated degradation mechanism of dyes. Experiments will be needed to evaluate the products formed during the enzymatic degradation of the effluent and to analyze their interference in the process. Further studies should be performed in order to find a possible method for reaction products removal.

It is also interesting to investigate the effect of known inhibitors of laccase catalyzed degradation of dyes. There is much to study about any possible inhibitions by other products used in textile processing, dyeing and finishing.

This type of study could also be extended to other classes of dyes (basic, direct, acid, etc.) often present in effluents from textile industries.

## **Appendices**

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## Appendix A – Dyes Safety Data Sheets

### A1 – Remazol Black B

#### I – Product Information

Product name: Remazol Black B 133 % gran

Composition:

Dangerous component: C.I. Reactive Black 5

Content: 70-80 %

EC Number: 241-164-5

#### II – Physico-Chemical properties

Physical state: granulated

Colour: black

Odour: odourless

Ignition temperature: > 240 °C

Bulk density: about 600 kg/m<sup>3</sup>

Water solubility: > 100 g/L (25°C)

pH value: about 4.5 (10 g/L)

water

Combustibility index: BZ1 – does not enter into combustion

#### III – Stability and Reactivity

Thermal decomposition: > 190 °C

Dangerous reactions:

Tendency to blow the dust: non-flammable

#### IV – Toxicological information

Acute oral toxicity: DL50 > 2.000 mg/kg (vole)

Effect of skin irritation: not irritating (rabbit)

Irritating to eyes: not irritating (rabbit eye)

#### V – Ecological information

Biodegradability: 10-25 % (static test)

Toxicity to fish: CL50 > 100 mg/L (48h, Brachydanio rerio)

Toxicity to bacteria: > 1.000 mg/L (fermentation tube test)

#### VI – Standards

Danger symbol: Xn (harmful)

R42/43: may cause sensitization by inhalation and skin contact

S22: not breathe dust

S24: avoid skin contact

S37: use appropriate gloves

## A2 – Remazol Yellow GR

### I – Product Information

Product name: Remazol Yellow GR 133 % gran

Composition:

C.I. Reactive Yellow 15

### II – Physico-Chemical properties

Physical state: granulated

Colour: dark yellow

Odour: odourless

Melting temperature: > 250 °C

Ignition temperature: from 240 °C

Bulk density: about 833 kg/m<sup>3</sup>

Water solubility: 80 g/L (20 °C)

pH value: about 5.5 (50 g/L

water

Combustibility index: BZ1 not enter into combustion

### III – Stability and Reactivity

Thermal decomposition: > 260 °C

Dangerous reactions: in the case of organic powders, should be counted, as a rule, with dust explosion

### IV – Toxicological information

Acute oral toxicity: DL50 > 2.000 mg/kg (vole)

Effect of skin irritation: not irritating (rabbit)

Irritating to eyes: not irritating (rabbit eye)

### V – Ecological information

Physico-chemical elimination: 10-25 % (precipitation of iron sulphate)

Biodegradability: 10-25 % (static test)

Toxicity to fish: CL50 = 500 mg/L (48h, *Leuciscus idus*)

Toxicity to bacteria: CEO > 500 mg/L (biological sludge)

COD: 630 mg/g

BOD<sub>5</sub>: 70 mg/g

### VI – Standards

S22: not breathe dust

## A3 – Remazol Yellow 3RS

### I – Product Information

Product name: Remazol Yellow 3RS 133 % gran

Composition:

C.I. Reactive Yellow 176

### II – Physico-Chemical properties

Physical state: granulated

Colour: red to brown

Odour: odourless

Ignition temperature: from 270 °C

Bulk density: 400-500 kg/m<sup>3</sup>

Water solubility: 50 g/L (20 °C)

pH value: about 7.0 (25 °C, 10 g/L)

Combustibility index: BZ3 localized burning without spread

### III – Stability and Reactivity

Thermal decomposition: > 150 °C

Dangerous reactions: in the case of organic powders, should be counted, as a rule, with dust explosion

### IV – Toxicological information

Acute oral toxicity: DL50 > 2.000 mg/kg (vole)

Effect of skin irritation: not irritating (rabbit)

Irritating to eyes: not irritating (rabbit eye)

### V – Ecological information

Toxicity to fish: CL50: 500 – 1.000 mg/L (96h, Leuciscus idus)

Toxicity to bacteria: CE10: 1.000 mg/L (activated sludge bacteria)

### VI – Standards

S22: not breathe dust

## A4 – Remazol Brilliant Red 3BS

### I – Product Information

Product name: Remazol Brilliant Red 3BS gran

Composition:

C.I. Reactive Red 239

### II – Physico-Chemical properties

Physical state: granulated

Colour: dark brown

Odour: odourless

Melting temperature: 240 °C

Bulk density: about 494 kg/m<sup>3</sup>

Water solubility: 100 g/L (20°C)

pH value: about 5.5 (25 °C, 10 g/L)

Combustibility index: BZ1 not enter into combustion

### III – Stability and Reactivity

Thermal decomposition: > 250 °C

Dangerous reactions: in the case of organic powders, should be counted, as a rule, with dust explosion

### IV – Toxicological information

Acute oral toxicity: DL50 > 2.000 mg/kg (vole)

Acute dermal toxicity: DL50 > 2.000 mg/kg (vole)

Effect of skin irritation: not irritating (rabbit)

Irritating to eyes: not irritating (rabbit eye)

### V – Ecological information

Biodegradability: 50-100 % (static method)

Toxicity to fish: CL50 > 500 mg/L (96 h, Brachydanio rerio)

Toxicity to daphnias: CL50: 10 - 100 mg/L (Daphnia magna)

Toxicity to bacteria: IC50 > 100 mg/L (biological sludge)

### VI – Standards

S22: not breathe dust

## A5 – Remazol Brilliant Red F3B

### I – Product Information

Product name: Remazol Brilliant Red F3B gran

Composition:

C.I. Reactive Red 180

### II – Physico-Chemical properties

Physical state: granulated

Colour: red

Odour: odourless

Ignition temperature: from 280 °C

Bulk density: about 494 kg/m<sup>3</sup>

Water solubility: > 10 g/L (20 °C)

pH value: 4.5 - 5.0 (25 °C, 10 g/L)

Combustibility index: BZ1 not enter into combustion

### III – Stability and Reactivity

Thermal decomposition: > 350 °C

Dangerous reactions: in the case of organic powders, should be counted, as a rule, with dust explosion

### IV – Toxicological information

Acute oral toxicity: DL50 > 5.000 mg/kg (vole)

Effect of skin irritation: not irritating (rabbit)

Irritating to eyes: not irritating (rabbit eye)

### V – Ecological information

Biodegradability: < 20 % (static method)

Toxicity to fish: CL50: 100 - 500 mg/L (96 h, Cyprinus carpio)

Toxicity to bacteria: CEO > 2.000 mg/L (inhibition of respiration of activated sludge organisms)

### VI – Standards

S22: not breathe dust

## A6 – Levafix Brilliant Blue E-BRA

### I – Product Information

Product name: Levafix Brilliant Blue E-BRA gran

Composition:

Dangerous component: C.I. Reactive Blue 114

Content: 65-75 %

CAS Number: 72139-17-4

### II – Physico-Chemical properties

Physical state: granulated

Colour: blue

Odour: odourless

Bulk density: 350 - 450 kg/m<sup>3</sup>

Water solubility: 40 g/L (25 °C)

pH value: 5.0 – 7.0 (100 g/L)  
water

### III – Stability and Reactivity

Thermal decomposition: > 230 °C

Dangerous reactions: explosive in powder form

### IV – Toxicological information

Acute oral toxicity: DL50 > 5.000 mg/kg (vole)

Effect of skin irritation: not irritating (rabbit)

Irritating to eyes: not irritating (rabbit eye)

### V – Ecological information

Biodegradability: 10-25 % (Zahn-Wellens test)

Toxicity to fish: CL50 > 100 mg/L (48h, *Leuciscus idus*)

Toxicity to bacteria: > 100 mg/L (inhibition of respiration of activated sludge organisms)

COD: 1.150 mg/g

BOD<sub>5</sub>: < 5 mg/L

### VI – Standards

Danger symbol: Xn (harmful)

R42/43: may cause sensitization by inhalation and skin contact

S22: not breathe dust

S24: avoid skin contact

S37: use appropriate gloves

## Appendix B – Enzymes Data Sheets

### B1 – DeniLite II Base

#### I – Description

DeniLite II Base is a highly concentrated laccase (EC 1.10.3.2) produced by submerged fermentation of a genetically modified *Aspergillus* microorganism.

#### II – Product Properties

DeniLite II Base is a beige granulated product available with a standard strength of 800 LAMU/g. Product colour may vary from batch to batch. Colour intensity is not an indication of product strength. The enzyme activity of DeniLite II Base is declared in LAMU (Laccase Units).

DeniLite II Base is a non-food-grade product intended for technical applications only.

#### III – Application

DeniLite II Base should be formulated together with DeniLite II Assist. The combined product is used for the decolourisation of indigo in denim processing applications. A ready-to-use formulation will contain DeniLite II Base, DeniLite II Assist and suitable buffer salts to target pH 4.5 during washing. The end-user formulation should be made as a solid product and not exposed to water or other liquids prior to use. The final product offers the following benefits:

- Creation of new looks, new fashions and finishes (e.g. grey cast/antique finishes)
- Enhancement of denim abrasion – overall reduction in processing time
- Maximum strength retention at high abrasion levels (e.g. destruct finishes)
- Clean-up of backstaining and improved garment contrast
- Easily controllable and reproducible dye decolourisation process

Suggested process conditions are:

- Liquor/garment ratio: 4:1 – 20:1 (optimum 5:1 – 10:1)
- Treatment time: 10 – 30 min.
- pH: 4.0 – 5.5
- Temperature: 60-70 °C
- Afterwash: Rinse

#### IV – Safety

Enzymes are proteins and inhalation of dust or aerosols may induce sensitization and may cause allergic reactions in sensitized individuals. Some enzymes may irritate the skin, eyes and mucous membranes upon prolonged contact.

#### V – Storage

Enzymes gradually lose activity over time depending on storage temperature. Cool conditions are recommended. Close container after partial use to protect from humidity.

When stored in closed containers at 25 °C, the product will maintain its declared activity for at least three months. Extended storage and/or adverse conditions, including higher temperatures, may lead to a higher dosage requirement.

## B2 – DeniLite II S

### I – Description

DeniLite II S is a laccase (EC 1.10.3.2) produced by submerged fermentation of a genetically modified *Aspergillus* microorganism.

### II – Product Properties

DeniLite II S is light grey powder product available in the following standard strength: 120 LAMU/g. Colour intensity is not an indication of product strength. The enzyme activity of DeniLite II S is declared in LAMU (Laccase Units).

DeniLite II Base is a non-food-grade product intended for technical applications only.

### III – Application

DeniLite II S is a ready-to-use product for indigo dye decolourisation in denim finishing operations. DeniLite II S is used when the following is sought:

- Creation of new looks, new fashions and finishes
- Enhancement of denim abrasion, allowing for a very fast denim abrasion process
- Denim finishing with optimum fabric strength retention
- Easily controllable and reproducible dye decolourisation process

DeniLite II S is a fully formulated product including buffer and an enzyme mediator, and needs no further formulation. The phosphate adipic acid buffering system in DeniLite II S ensures a pH of 4-5 during washing. The product contains no water and it is essential that the product is not mixed with water before use.

Suggested process conditions are:

- DeniLite II S: 0.5 – 2 % of weight of garment
- Liquor/garment ratio: 4:1 – 20:1 (optimum 5:1 – 10:1)
- Treatment time: 10 – 30 min.
- pH: 4.0 – 5.5
- Temperature: 60-70 °C
- Afterwash: Rinse

### IV – Safety

Enzymes are proteins and inhalation of dust or aerosols may induce sensitization and may cause allergic reactions in sensitized individuals. Some enzymes may irritate the skin, eyes and mucous membranes upon prolonged contact.

### V – Storage

Enzymes gradually lose activity over time depending on storage temperature. Cool conditions are recommended. Close container after partial use to protect from humidity.

When stored in closed containers at 25 °C, the product will maintain its declared activity for at least three months. Extended storage and/or adverse conditions, including higher temperatures, may lead to a higher dosage requirement.



## Appendix C – Mediators Safety Data sheets

### C1 – ABTS

#### I – Product Information

Product name: 2,2' - Azino-bis(3-ethylbenzothiazoline-6-sulfonic acid) diammonium salt  
CAS Number: 30931-67-0  
EC Number: 250-396-6  
Linear Formula:  $C_{18}H_{24}N_6O_6S_4$   
Molecular Weight: 548.68

#### II – Safety

Personal protective equipment: dust mask type N95 (US), eyeshields, gloves  
Hazard Codes: Xi (Irritant)  
Risk Statements: 36/37/38 (Irritating to eyes, respiratory system and skin)  
Safety Statements: 26-36 (In case of contact with eyes, rinse immediately with plenty of water and seek medical advice. Wear suitable protective clothing)

### C2 – HBT

#### I – Product Information

Product name: 1-Hydroxybenzotriazole hydrate  
CAS Number: 123333-53-9  
EC Number: 219-989-7  
Linear Formula:  $C_6H_5N_3O \cdot xH_2O$   
Molecular Weight: 135.12 (anhydrous basis)

#### II – Safety

Hazard Codes: F (Highly flammable)  
Risk Statements: 5-11 (Heating may cause explosion; highly flammable)  
Safety Statements: 15-16-35 (Keep away from heat; keep away from ignition sources – no smoking; this material and its container must be safely disposed)

### C3 – VA

#### I – Product Information

Product name: Violuric acid  
CAS Number: 87-39-8  
EC Number: 201-741-4  
Linear Formula:  $C_4H_3N_3O_4$   
Molecular Weight: 171.1

#### II – Safety

Hazard Codes: Xi (Irritant)  
Risk Statements: 36/37/38 (Irritating to eyes, respiratory system and skin)  
Safety Statements: 26-36 (In case of contact with eyes, rinse immediately with plenty of water and seek medical advice. Wear suitable protective clothing)

**C4 – TEMPO****I – Product Information**

Product name: 2,2,6,6 – Tetramethyl-1-piperidinyloxy, free radical  
CAS Number: 2564-83-2  
EC Number: 219-888-8  
Linear Formula: C<sub>9</sub>H<sub>18</sub>NO  
Molecular Weight: 156.25

**II – Safety**

Personal protective equipment: Eyeshields, faceshields, full-face particle respirator type N100 (US), gloves, respirator cartridge type N100 (US), type P1 (EN143) respirator filter, type P3 (EN 143) respirator cartridges

Hazard Codes: C (Corrosive)

Risk Statements: 34 (Causes burns)

Safety Statements: 26-36/37/39-45 (In case of contact with eyes, rinse immediately with plenty of water and seek medical advice. Wear clothing, gloves and appropriate protective devices for eyes and face. In case of accident or sickness, seek medical help immediately; if possible, show the label)

## Appendix D – Textile processing auxiliaries

### D1 – Sera Lube M-CF

#### I - Function

Crease inhibitor and lubricant for dyeing and scouring processes.

#### II – Properties

Has lubricating properties.

Prevents crease formation in dyeing of fabrics made of acrylic, wool, wool blends, polyamide, silk and cellulosic knit goods.

Prevents crease formation during milling wool-containing fabrics.

Reduces milling of wool blends during dyeing.

Does not foam and may therefore be used on all dyeing machines including jets.

Shows good compatibility with anionic and cationic dyestuffs.

Does not retard dyes.

Avoids moiré in beam dyeing machines.

Prevents channelling of dye liquor in dyeing of hanks and raw stock.

#### III – Amounts required

1 – 2 % in dyeing processes

1,000 kg IBC / 120 kg drum

#### IV – Appearance

Almost colourless

Viscous liquid

#### V – Ionic nature

Nonionic

### D2 – Sera Quest M-PP

#### I - Function

Sequestrant with dispersing, soil suspending and buffering ability for scouring, bleaching and dyeing of textile material.

#### II – Properties

Has sequestering ability for calcium, magnesium and heavy metal ions in a wide pH range.

Improves the removal of soil, mineral contaminations as well as heavy metal ions, sizes and yarn lubricants in scouring processes; aids in pretreating the fabrics for subsequent bleaching or dyeing.

Prevents the agglomeration of dispersions and emulsions.

Stabilises dyebaths when dyeing natural and synthetic fibers.

Improves the fastness to rubbing when soaping dyeings and prints, also the wet fastness when soaping reactive dyeings and prints.

**III – Amounts required**

0.5 – 2.0 g/L for washing  
0.5 – 1.0 g/L for preparation and dyeing

1,100 kg IBC / 120 kg drum

**IV – Appearance**

Yellowish liquid

**V – Ionic nature**

Anionic

**D3 – Sera Wet C-AS****I - Function**

Low-foaming rapid wetting and deaerating agent for pre-treatment and dyeing processes of cotton and synthetic fibers.

**II – Properties**

Provides rapid wetting over a wide temperature range  
Does not impair the solubility of water soluble dyes  
Improves dye penetration  
Does not foam  
Promotes high liquor pick-up  
Stable in alkaline solution up to 30 g/L caustic soda  
APEO-free

**III – Amounts required**

1.0 – 4.0 g/L in preparation and dyeing

950 kg IBC / 110/120 kg drum

**IV – Appearance**

Clear, colourless to slightly yellowish liquid

**V – Ionic nature**

Anionic