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## Effect of Infiltration Material on a LSM15/CGO10 Electrochemical Reactor in the Electrochemical Oxidation of Propene

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4 Effect of Infiltration Material on a LSM<sub>15</sub>/CGO<sub>10</sub>  
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8 Electrochemical Reactor in the Electrochemical Oxidation  
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12 of Propene  
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15 Davide Ippolito<sup>a</sup>, Kent Kammer Hansen<sup>a</sup>  
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29 **Abstract**  
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32 The effect of infiltrating on a La<sub>0.85</sub>Sr<sub>0.15</sub>MnO<sub>3</sub>/Ce<sub>0.9</sub>Gd<sub>0.1</sub>O<sub>1.95</sub> 11-layer electrochemical  
33 reactor with CeO<sub>2</sub> and Ce<sub>0.8</sub>Pr<sub>0.2</sub>O<sub>2-δ</sub> was studied in propene oxidation at open circuit  
34 voltage and under polarization as a function of reaction temperature. This work outlined  
35 the importance of catalytic and electrochemical properties of infiltrated material on the  
36 ability to increase propene conversion under polarization with good faradaic efficiency.  
37 Electrochemical impedance spectroscopy (EIS) was used to study the effect of  
38 infiltration material on electrode properties. The infiltration of a mixed ionic and  
39 electronic conductor (MIEC), like Ce<sub>0.8</sub>Pr<sub>0.2</sub>O<sub>2-δ</sub>, increased the electrode performance at  
40 low temperature but decreased the lifetime of the oxygen ion promoters on the  
41 catalyst/electrode surface, reducing the faradaic efficiency of the reaction. The  
42 infiltration of CeO<sub>2</sub> provided high propene conversion at open circuit and high effect of  
43 polarization associated with good faradaic efficiency, especially at low temperature.  
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4 Keywords: LSM, CGO, infiltration, AC impedance, propene oxidation, praseodymium  
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6 doped ceria  
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## 10 11 **Introduction** 12 13 14

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16 Air pollution from stationary and mobile sources has become one of most important  
17 environmental concerns of the last ten years. Stricter legislation on emission control has  
18 been adopted in the US, Europe and also emerging countries, like India and China [1].  
19 Exhaust gases from spark and compression engines contribute to the degradation of air  
20 quality, especially in urban environments. Between these two, Diesel exhausts contain  
21 high levels of NO<sub>x</sub>, volatile organic compounds (VOC) and fine particulate matter (PM)  
22 contributing to respiratory problems and cardiovascular disease [2,3]. Supported metal  
23 catalysts, such as Pt and Pd, are usually employed both for catalytic combustion of  
24 hydrocarbons and NO<sub>x</sub> reduction [4]. They are very active at low temperature but suffer  
25 from high temperature sintering, poisoning from sulphur and their use is limited by high  
26 prices. Alternative catalysts have thus been explored, such as hexaaluminates, single  
27 and doped transition metal oxides and perovskite [5].  
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45 Transition metal perovskites (LaMO<sub>3</sub>) (M=Mn,Co) are possible alternative catalysts to  
46 noble metals in hydrocarbon combustion reactions due to the redox properties of the M  
47 cation, the presence of lattice defects and weakly bonded oxygen at the surface. They  
48 offer good thermal stability in oxygen and steam-rich atmospheres and low cost, but  
49 they currently have lower efficiencies [6,7]. For example, Spinicci et al. studied the  
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4 activity of  $\text{LaMnO}_3$  and  $\text{LaCoO}_3$  towards combustion of VOCs and oxygen surface  
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6 species mobility was identified as a requisite for high catalytic activity [8].  
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9 Catalyst activity can be enhanced by using Electrochemical Promotion of Catalysis  
10 (EPOC). EPOC is based on the control of catalyst work function by applying a potential  
11 or current to an electrocatalyst interfaced with a solid electrolyte. In 1981, for example,  
12 Stoukides and Vayenas [9] demonstrated increased reaction rate and selectivity in  
13 ethylene catalytic oxidation on Ag. This phenomenon has also been studied using  
14 perovskite as a catalyst; Gaillard et al. demonstrated *in situ* control of activity and  
15 selectivity of  $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_{0.8}\text{Fe}_{0.2}\text{O}_3$  for deep oxidation of propene at 450 °C in air by  
16 EPOC [10]. Additionally, Roche et al. presented an electrochemical promotion effect for  
17 the deep oxidation of propane on lanthanum manganite [11]. Furthermore, Tsiakaras et  
18 al. studied the electrocatalytic behaviour of  $\text{La}_{0.6}\text{Sr}_{0.4}\text{Co}_{0.8}\text{Fe}_{0.2}\text{O}_3$  perovskite deposited  
19 on yttria-stabilized zirconia (YSZ) during methane oxidation where oxygen was  
20 electrochemically supplied as  $\text{O}^{2-}$  and found considerable changes in methane  
21 conversion and product selectivity [12]. Finally, Balomenou et al. developed a monolith  
22 electrochemical plate reactor (MEPR) using Pt and Rh dispersed on a YSZ plate to  
23 measure the abatement of simulated and real automotive pollution and achieved  
24 electrochemical promotion in both situations [13].  
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50 The present work studied the possibility of using an 11-layer porous single chamber  
51 electrochemical reactor for the oxidation of propene, a major Diesel exhaust emission  
52 component [14], without precious metal. In this work, the whole reactor was thought of  
53 as a catalytic filter with a porous composite electrode interfaced with a porous  
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electrolyte for Diesel exhaust after-treatment. Ceria is one of the best hydrocarbon oxidation catalysts known, and although ceria-based oxidation catalysts are normally coupled with a precious metal, alumina-supported ceria shows sufficient activity in the oxidation of unburned hydrocarbons in Diesel exhausts without the addition of precious metals [15]. In order to enhance the catalytic activity for a future full-scale application, the effect of  $\text{CeO}_2$  and  $\text{Ce}_{0.8}\text{Pr}_{0.2}\text{O}_{2-\delta}$  impregnation on reactor activity was therefore investigated. The influence of infiltrated material properties on the reactor performance was also investigated. To comply with these objectives, electrochemical impedance spectroscopy (EIS) was employed.

## Experimental

### *Cell preparation*

The 11-layer electrochemical reactor (backbone) was prepared by laminating layers of electrode and electrolyte made by tape casting for a total of 5 single cells. The electrolyte tape was made of  $\text{Ce}_{0.9}\text{Gd}_{0.1}\text{O}_{1.95}$  purchased from Rhodia, while the electrode was made of a 35% weight  $\text{Ce}_{0.9}\text{Gd}_{0.1}\text{O}_{1.95}$  ( $\text{CGO}_{10}$ ) and 65% weight  $\text{La}_{0.85}\text{Sr}_{0.15}\text{MnO}_3$  ( $\text{LSM}_{15}$ ) composite (Haldor Topsoe). Slurries for tape casting were made from metal oxide powder, solvent, binder and carbon as pore former. The slurries were ball milled before tape casting. The cell was then sintered at 1250 °C for 2 h. The average diameter of the cells was 13 mm.

The cells were impregnated using a 1.5 M solution of 20 mol%  $\text{Pr}(\text{NO}_3)_3$  + 80 mol%  $\text{Ce}(\text{NO}_3)_3$  for  $\text{Ce}_{0.8}\text{Pr}_{0.2}\text{O}_{2-\delta}$  ( $\text{CPO}_{20}$ ) infiltration and with a 1.5 M solution of  $\text{Ce}(\text{NO}_3)_3$  for  $\text{CeO}_2$  infiltration with Triton X-100 as surfactant. Solutions were prepared with Millipore water, Triton X-100 (Sigma-Aldrich), Ce nitrate hexahydrate (Alfa Aesar) and Pr nitrate hydrate (Alfa Aesar). Infiltration was carried out in one step by applying vacuum to the cell after application of impregnation solution. After infiltration, the cell was calcined at 600 °C for 2 h. The weight of the cell was measured before infiltration and after calcination to estimate the infiltration loading. The infiltration loading was equivalent to approximately 2.6-2.7% of the weight of the cell. Gold paste with 20% weight carbon was painted on both sides of the electrochemical reactor and used as the current collector. The cell weights were measured without the current collector and the cell areas were approximately 1.429 and 1.409  $\text{cm}^2$  for  $\text{CPO}_{20}$  and  $\text{CeO}_2$  infiltrated cells, respectively.

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9 *Reactor configuration*

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14 **Figure 1 illustrates the reactor configuration.** The sample was mounted in a tubular  
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16 reactor between two alumina tubes with contact between the gold paste and the two Pt  
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18 electrodes used as working and reference/counter electrodes under one atmosphere,  
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20 as reported by Werchmeister et al. [16]. The setup was placed inside a glass tube  
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22 surrounded by a furnace. For the catalytic activity evaluation, a mixture of 10% O<sub>2</sub> (Air  
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24 Liquide; 20% O<sub>2</sub> ± 2% Ar), 1000 ppm propene (Air Liquide; 1% ± 0.02% propene in Ar)  
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26 and Ar to balance **was used** with a total flow rate of 2 L h<sup>-1</sup> controlled by Brooks flow  
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28 meters. Reactants and products were analysed by an on-line Agilent 6890 N gas  
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30 chromatograph connected to the reactor and equipped with Hayesep N and Molsieve  
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32 columns and a thermal conductivity detector. The reaction temperature was monitored  
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34 by two thermocouples: one touching the cell and the other one placed 4 mm over the  
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36 cell. The temperature range of the measurements was 300 °C - 500 °C.  
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4 *Cell structural characterization*  
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9 The 11-layer reactor morphology and infiltrated particle morphology were characterised  
10 with a Zeiss Supra-35 scanning electron microscopy (SEM). In addition,  
11 adsorption/desorption experiments (BET) using Krypton were conducted on the  
12 infiltrated samples to determine the specific surface area (SSA). The samples were  
13 measured in an Autosorp-1-MP before and after catalytic measurements where all the  
14 samples were de-gassed for 3 h under vacuum at 300 °C prior to adsorption. The BET  
15 specific surface areas were calculated from the adsorption isotherm keeping the values  
16 of the relative Krypton pressure ( $p/p_0$ ) between 0.05 and 0.3 for all samples. Finally, X-  
17 ray diffraction (XRD) measurements were carried out with a STOE theta-theta  
18 diffractometer using Cu K $\alpha$  ( $\lambda=1.540 \text{ \AA}$ ) from 20° to 100° and with a 0.05 2 $\theta$  step size.  
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36 *Cell activity characterization*  
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38 The polarisation effect on the cell is characterised by the rate enhancement ratio ( $\rho$ )  
39 defined by:  
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$$\rho = \frac{r}{r_0}$$

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47 where  $r_0$  is the catalytic rate (mol/s) at open circuit voltage (OCV) and  $r$  is the catalytic  
48 rate (mol/s) under polarization  
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55 The faradaic efficiency was thus calculated as:  
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$$\Lambda = \frac{r - r_0}{I}$$



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4 where  $I$  is the current and  $F$  is Faraday's constant.  
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### 10 11 12 13 14 *Cell electrochemical characterization* 15

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19 A potentiostat (Gamry, reference 600 USA) was used to perform chronoamperometry  
20 tests and for recording impedance spectra. The open-circuit voltage of the cell was  
21 stabilised before every measurement. The impedance spectra were recorded at open-  
22 circuit voltage (OCV) and with an anodic bias of +4 V (+ 800 mV/cell) with respect to the  
23 open circuit voltage with an amplitude of 36 mV RMS over the frequency range 0.78  
24 MHz to 5 mHz with 10 points/decade. The chronoamperometry tests were carried out  
25 for 2 h with anodic potentials from +200 mV/cell to 1 V/cell with respect to the open-  
26 circuit voltage with 1 V steps followed by cathodic polarisation using the same  
27 procedure. The ohmic drop was not subtracted in the given potentials. The temperature  
28 range of these measurements was 300 °C - 500 °C.  
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43 The impedance spectra were analysed in ZSimpWin 3.21 software using Complex Non-  
44 Linear Square (CNLS) fitting. The inductance coming from the wiring was subtracted for  
45 every spectrum to perform the fitting. The spectra were validated using the Kramers-  
46 Kronig test for causality and time invariance.  
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53 An equivalent circuit was used containing a serial resistance,  $R_s$ , and a number of RQ  
54 or RG subcircuits. RQ is a resistance  $R$  in parallel with a Constant Phase Element  
55 (CPE). The impedance of a CPE is given by:  
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$$\frac{1}{Z} = Y = Y^0(j\omega)^n$$

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12 where  $Z$  is the impedance,  $Y$  the admittance,  $Y^0$  is the amplitude of the constant phase  
13 element admittance,  $j$  is the imaginary number and  $\omega$  is the frequency.  
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17 The general impedance of the Gerischer element (G) is expressed by:  
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$$Z_G = \frac{1}{Y_0 \sqrt{K_A + i\omega}}$$

27 where  $Y_0$  is the admittance parameter and  $K_A$  is the rate constant parameter.  
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29 The distribution of relaxation times (DRT) analysis was performed using in-house  
30 software based on Schichlein et al. [17]. The visual Hanning filter was used for data  
31 filtering and the filtering values was kept fixed for all analyses.  
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## Result and Discussion

### *Catalyst characterization*

Figures 2 and 3 show the micrographs of  $\text{CeO}_2$  and  $\text{CPO}_{20}$  infiltrated cells, respectively. The good coverage of  $\text{CeO}_2$  and  $\text{CPO}_{20}$  particles on the  $\text{LSM}_{15}\text{-CGO}_{10}$  surfaces was noticeable; the particles were arranged along the walls of the pores without blocking them. The formation of solid solution between Ce and Pr was guaranteed by the exothermicity of Triton X-100 decomposition. Moreover, the XRD recorded on  $\text{CPO}_{20}$  powder and visible in Figure 4 displays nearly all of the characteristic reflections corresponding to the fluorite structure of  $\text{CeO}_2$ . No crystalline phases except the fluorite-type solid solution were detected, suggesting direct solid solution formation.

The  $\text{CPO}_{20}$  particles showed different agglomeration behaviour with respect to  $\text{CeO}_2$ , one that has already been reported by Kharton et al. [18], where a  $\text{Ce}_{0.8}\text{Gd}_{0.18}\text{Pr}_{0.02}\text{O}_{2-\delta}$  composite showed segregated Pr and Gd enriched particles along the grain boundaries. Co-doping with Pr increased the tendency for phase segregation along the grain boundaries of  $\text{Ce}(\text{Gd})\text{O}_{2-\delta}$ . Also in this case, the introduction of  $\text{Pr}^{+4}$  ions could have changed the nucleation properties of  $\text{CeO}_2$  on the  $\text{LSM}_{15}/\text{CGO}_{10}$  composite backbone, giving rise to a diffusion of Pr ions into  $\text{LSM}_{15}$  and  $\text{CGO}_{10}$ . However, the formation of perovskite phases like  $\text{PrMnO}_3$  could not be excluded.

$\text{CeO}_2$  was found to have a specific area of  $2.43 \text{ m}^2/\text{g}$ .  $\text{CeO}_2$  area is higher than the one of  $\text{CPO}_{20}$  which is equal to  $1.64 \text{ m}^2/\text{g}$ . This is due to the different particle morphologies.

From the SEM micrographs it was possible to observe that the distribution of  $\text{CeO}_2$  particles was more uniform and the adhesion of  $\text{CeO}_2$  on the backbone surface was

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4 more optimal than CPO<sub>20</sub>. Additionally, the infiltration procedure was able to increase  
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6 the specific area of the backbone cell by at least one order of magnitude [19].  
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### 10 11 12 13 *Catalyst activity tests* 14

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16 Figure 5 shows the intrinsic catalytic reaction rate towards propene oxidation measured  
17 at open circuit voltage (OCV). The CeO<sub>2</sub> infiltrated cell showed higher reaction rates  
18 with respect to the CPO<sub>20</sub> infiltrated cell at all temperatures; the conversions of propene  
19 at 400 °C for CeO<sub>2</sub> and CPO<sub>20</sub> infiltrated cells were 46.8% and 37.7%, while at 300 °C  
20 they were 17.8% and 13.5%, respectively. The better activity of CeO<sub>2</sub> at low  
21 temperature could be attributed only partially to the larger specific surface area. The  
22 selectivity towards CO<sub>2</sub> was almost 100% at all temperatures for CeO<sub>2</sub>, but only 91-92%  
23 for the CPO<sub>20</sub> infiltrated cell. Reddy et al. using XPS reported an enrichment of Pr in the  
24 surface region up to 44%, higher than that nominal content of 20% [26]. A partial surface  
25 segregation of Pr forming Pr<sub>6</sub>O<sub>11</sub> could be the reason for the lower activity of CPO<sub>20</sub>.  
26 Pr<sub>6</sub>O<sub>11</sub> is recognised as a good catalyst for methane and CO oxidation due to its high  
27 redox potential, but the catalytic activity of praseodymia seems to be limited by the  
28 difficult reoxidation of Pr<sub>2</sub>O<sub>3</sub> [20]. Pr<sub>6</sub>O<sub>11</sub> could have some activity for propene oxidation,  
29 but it could be relatively inactive compared to ceria due to the high stability of reduced  
30 Pr<sub>2</sub>O<sub>3</sub>. The lower selectivity to CO<sub>2</sub> observed for CPO<sub>20</sub> with CO formation suggested  
31 that oxygen from Pr<sub>6</sub>O<sub>11</sub> was not utilised in the same way as from ceria under the  
32 reaction conditions. Zhao et al. observed a decrease in reaction rate for n-butane  
33 oxidation with the incorporation of Pr<sup>+4</sup> into ceria. This decrease in reaction rate was  
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4 anyway lower than the reaction rate decrease observed for ceria doped with Sm, Gd,  
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6 Nb and Ta [15]. As observed by Zhao et al. for the oxidation of n-butane over ceria and  
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8 Samaria-doped ceria (SDC), the common assumption that doping ceria will increase its  
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10 activity is not always correct [21]. If we compare the reaction rate of the backbone ( $3.88$   
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12  $10^{-8}$  mol  $C_3H_6/(s \times g)$ ) at  $400$  °C as reported in [19], infiltration resulted in a substantial  
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14 increase in reaction rate. The extraction of apparent activation energy was outside the  
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16 scope of this analysis, and observing a slope change in the reaction rate curves due to  
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18 possible diffusion limitations of reactants between  $350$  °C and  $400$  °C is difficult.  
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24 During the application of anodic polarization, being this reactor symmetric, one side  
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26 worked as anode and the other side as a cathode. At the cathodic side molecular  
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28 oxygen was reduced to lattice oxygen, which was then pumped by this anodic voltage  
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30 through the oxygen vacancies of  $CGO_{10}$  to the surface of  $LSM_{15}$ . The pumped oxygen  
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32 lattice on the anodic side can react directly with adsorbed propene to form  $CO_2$  and  $H_2O$   
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34 or recombined to molecular oxygen through oxygen evolution reaction. Figure 6 shows  
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36 the effect of polarisation at  $+4$  V on the infiltrated cells at different reaction  
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38 temperatures, expressed as rate enhancement ratio. It was possible to observe that the  
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40 polarization effect was higher at low temperature for  $CeO_2$  than for  $CPO_{20}$ , but it  
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42 became more prominent on  $CPO_{20}$  with increasing temperature. The  $CeO_2$  infiltrated  
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44 cell reaction enhancement curve strongly flattened at temperatures higher than  $400$  °C  
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46 possibly due to limiting reactant diffusion limitations inside the electrode pores; this  
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48 phenomenon might limit the effect of polarization on propene conversion.  
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57 The rate enhancement ratio behaviour could be attributed to two types of regimes. Ceria  
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59 has very low electronic and ionic conductivity, the latter being only 3% of the total  
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4 conductivity [22]. At low temperature (300-400 °C), some of the oxygen ions thus have  
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6 the opportunity and time to backspillover from CGO<sub>10</sub> on the deposited ceria surfaces  
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8 and act as electronegative promoters of propene oxidation without recombine to form  
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10 molecular oxygen. The increased propene reaction rate on CeO<sub>2</sub> at low temperatures  
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12 could also be due to the contribution of a polarisation-induced double layer established  
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14 between the O<sup>2-</sup> back-spill on ceria surfaces and the O<sub>2</sub> adsorbed from the gas phase.  
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20 On the contrary, CPO<sub>20</sub> has much higher electronic and ionic conductivity, behaving as  
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22 a mixed ionic electronic conductor; the mixed conductivity was able to strongly expand  
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24 the TPB area. This characteristic hindered the possible back-spill of oxygen ions to the  
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26 CPO<sub>20</sub> surfaces because the kinetics of promoter consumption, in the case of CPO<sub>20</sub>,  
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28 might be fast due to the high reactivity of the promoter at the three phase boundaries,  
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30 as suggested by Roche et al. [11]. The O<sup>2-</sup> recombination and following oxygen  
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32 evolution, although the latter contributes to the total current, did not produce any  
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34 increase in propene conversion. Figure 7 shows the behaviour of faradaic efficiency for  
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36 CeO<sub>2</sub> and CPO<sub>20</sub>. It is possible to observe that the two samples showed similar  
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38 efficiency at high temperature (450-500 °C). Below this temperature range CPO<sub>20</sub>  
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40 exhibited a quasi-flat faradaic efficiency with decreasing temperature; CeO<sub>2</sub> instead  
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42 showed a sharp increase with decreasing temperature. The explanation is given in the  
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44 electrochemical characterization section.  
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### *Electrochemical characterization*

Figures 8 and 9 show the Arrhenius plots of polarization resistance ( $R_p$ ) at OCV and under polarisation for CPO<sub>20</sub> and CeO<sub>2</sub> extracted from impedance spectra. CPO<sub>20</sub> infiltration gave a better electrode performance, showing lower polarisation resistance at lower temperatures compared to CeO<sub>2</sub>. This could be attributed to the mixed ionic-electronic conduction behaviour of CPO<sub>20</sub>. CPO<sub>20</sub> infiltration was also able to expand the TPB area and decrease the resistance associated with electrochemical reactions occurring on the surface. The activation energy of the  $R_p$  for CPO<sub>20</sub> was  $0.59 \pm 0.03$  eV, much lower than the activation energy of the CeO<sub>2</sub> infiltrated cell ( $0.97 \pm 0.04$  eV). This meant that the electrode performance for CPO<sub>20</sub> was less susceptible to temperature decreases than for CeO<sub>2</sub>. The activation energy of CeO<sub>2</sub> was close to the value of the backbone cell at OCV ( $0.93 \pm 0.04$  eV) reported in previous study [19]. The infiltration of CeO<sub>2</sub> was thus able to decrease the polarization resistance of the backbone without changing the reaction mechanism. Typical EPOC behaviour was visible in this case where a catalyst with high catalytic performance, like CeO<sub>2</sub>/LSM<sub>15</sub>, is coupled with an electrode with low exchange current at low temperature.

Figure 9 illustrates the Arrhenius plot of the polarization resistance measured at +4 V. At high temperatures (450-500 °C) the decrease of  $R_p$  for CeO<sub>2</sub> upon anodic polarization was found to be very high, reaching resistance values similar to those obtained for CPO<sub>20</sub>. Presumably the polarization response of the backbone became predominant on the infiltrated material polarization response. For this reason, at these temperatures, the faradaic efficiencies for both cells exhibited similar low values. At temperatures below 450 °C, the effect of anodic polarization on CeO<sub>2</sub> polarization resistance drastically

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4 decreased; high  $R_p$  coupled with good enhancement ratio ( $\rho$ ) value caused the sharp  
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6 increase of efficiency observed for  $\text{CeO}_2$ . For  $\text{CPO}_{20}$ , however, the effect of polarization  
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8 decreased with much lower activation energy: low  $R_p$  coupled with low enhancement  
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10 ratio ( $\rho$ ) caused the flattening of the efficiency observed for  $\text{CPO}_{20}$ . The activation  
11  
12 energy value extrapolated at high temperature for  $\text{CPO}_{20}$  curve was  $0.82 \pm 0.03$  eV. The  
13  
14 activation energy extracted for temperatures between  $400^\circ\text{C}$  and  $300^\circ\text{C}$  was  $0.61 \pm$   
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16  $0.01$  eV instead; presumably the effect of mixed conductivity on  $R_p$  became  
17  
18 predominant in this temperature range causing the slope change. The activation energy  
19  
20 of polarization resistance ( $R_p$ ) measured under polarization of  $+4$  V for  $\text{CeO}_2$  was  $1.13 \pm$   
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22  $0.05$  eV; both the infiltrated exhibited an increase of activation energy under anodic  
23  
24 voltage. This change of activation energy could be due to a modification of reaction  
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26 mechanism establishing under polarization.  
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34 In order to obtain high faradaic efficiency it is necessary to reduce the speed of  $\text{O}^{2-}$   
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36 recombination to molecular oxygen and so to increase the promoter lifetime. In the case  
37  
38 of  $\text{CPO}_{20}$  the kinetic of promoter consumption was very high (low  $R_p$ ) also at low  
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40 temperature if compared to  $\text{CeO}_2$ ; this was the cause of low faradaic efficiency.  
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45 Figures 10 and 11 show the impedance spectra of  $\text{CeO}_2$  and  $\text{CPO}_{20}$  infiltrated cells  
46  
47 recorded at OCV and  $+4$  V at  $450^\circ\text{C}$  together with the Bode plot of the imaginary part of  
48  
49 the recorded spectra. At least two depressed arcs were visible in these plots. The  
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51 polarization to  $+4$  V ( $0.8$  mV/cell) strongly affected the impedance responses; a strong  
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53 decrease in resistance was visible for the peak at low frequency for both infiltrated cells,  
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55 as was an increase in characteristic peak frequency. Additionally, the impedance  
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57 spectra under polarisation clearly displayed only two well defined depressed arcs where  
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4 the impedance contribution at medium frequency either disappeared or merged with the  
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6 impedance response at low frequency. Moreover, the inclined line visible at medium  
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8 frequency completely disappeared when polarisation was applied.  
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12 The impedance contribution at high frequencies (Figures 10c and 11c) was differently  
13  
14 affected by polarization depending on the infiltration material. This impedance  
15  
16 contribution at this temperature was likely due to oxygen ion transport from the  
17  
18 electrolyte to the LSM<sub>15</sub> electrode. The peak for the CeO<sub>2</sub> infiltrated cell was not  
19  
20 affected by polarisation and the imaginary part of the spectra recorded under  
21  
22 polarisation completely overlapped with the spectra recorded at OCV. On the contrary,  
23  
24 the high frequency peak of the CPO<sub>20</sub> infiltrated cell showed a small increase in  
25  
26 resistance when polarised at +4 V associated with a peak frequency decrease. This  
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28 meant that, in the case of CPO<sub>20</sub>, it was possible to observe a charge transfer  
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30 contribution even at these high frequencies; the overlapping between oxygen ion  
31  
32 transport and electrode reactions could be due to the mixed conductivity of CPO<sub>20</sub>.  
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42 The distribution of relaxation times (DRT) analysis visible in Figure 12 associated to the  
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44 impedance spectra in oxygen and propene at 450 °C for CeO<sub>2</sub> and CPO<sub>20</sub> showed three  
45  
46 main peaks at high, medium and low frequencies. The peak at medium frequency was  
47  
48 not well resolved and appeared as a shoulder overlapping the main peak at lower  
49  
50 frequencies. The peak at high frequency (10.4 kHz) appeared at the same frequency  
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52 and had similar resistance for both of the infiltration materials, so it was likely  
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54 independent of infiltration material at high temperatures and at OCV. However, this  
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56 effect could be attributed only to the backbone.  
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4 The reconstruction of  $\text{CeO}_2$  impedance spectra through DRT analysis was only possible  
5  
6 using three RQ elements, confirming the presence of a process at medium frequency.  
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8 The DRT analysis for the  $\text{CPO}_{20}$  infiltrated cell showed behaviour typical of a Gerischer  
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10 element at low frequency, as reported by Endler et al. with a single cell using a LSCF  
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12 cathode [23]. The mixed ionic electronic behaviour of  $\text{LSM}_{15}$  usually visible at high  
13  
14 cathodic polarization or low partial pressure of oxygen, associated to superficial oxygen  
15  
16 vacancy formation, was enhanced by  $\text{CPO}_{20}$  infiltration. The Gerischer behaviour  
17  
18 reflected that the overall oxygen reduction reaction on the mixed conducting  $\text{CPO}_{20}$   
19  
20 layers proceeded under the conditions where diffusion of oxygen vacancies in the  
21  
22 electrode and diffusion of adsorbed oxygen species on electrode surface are kinetically  
23  
24 coupled with the electrode exchange reaction between oxygen vacancies and gaseous  
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26 oxygen (charge transfer reaction) at the electrode/gas interface [24].  
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34 Figure 13 and 14 exhibit the DRT analysis of the influence of reaction atmosphere at  
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36  $500\text{ }^\circ\text{C}$  on impedance spectra for the  $\text{CPO}_{20}$  and  $\text{CeO}_2$  infiltrated cell, respectively. From  
37  
38 Figures 13 and 14, the relaxation at high frequency and the shoulder at medium  
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40 frequency were not dependent on reaction atmosphere; these peaks could then be  
41  
42 associated to oxygen ion transport in the electrolyte and across the electrolyte-electrode  
43  
44 interface at TPB. The relaxation at low frequency exhibited an increase in resistance  
45  
46 associated to a frequency decrease when propene was introduced into the reactor. This  
47  
48 behaviour could be due to oxygen dissociation and transport on the  $\text{LSM}_{15}$  surface.  
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50 These suprafacial processes on the electrode were coupled with electrochemical  
51  
52 process, as verified by the effect of polarization on resistance in the low frequency arc  
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54 (Figure 10c and 11c). Propene adsorption on  $\text{LSM}_{15}$  and  $\text{CGO}_{10}$  surfaces decreased the  
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4 rate and interfered with the oxygen exchange reaction on the electrode surface,  
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6 increasing the resistance of the low frequency peak.  
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10 This behaviour was exhibited by the CeO<sub>2</sub> infiltrated cell (Figure 14), as relaxation at  
11 high frequency was not affected by the reaction atmosphere. The relaxation at low  
12 frequency increased resistance and moved to slightly lower frequencies with the  
13 introduction of propene. In the case of CeO<sub>2</sub>, this effect was less pronounced than for  
14 the CPO<sub>20</sub> cell (Figure 13). Zheng Y. et al. studied the effect of oxygen vacancies on the  
15 oxygen reduction reaction (ORR) on La<sub>0.8</sub>Sr<sub>0.2</sub>MnO<sub>3</sub> [25]. After a 3 hours cathodic  
16 polarization at 800 °C, the size of polarization resistance on impedance spectra reduced  
17 significantly because of the *in-situ* generation of oxygen vacancies. The size of low  
18 frequency arc increased slightly with the variation of methane partial pressure at  
19 constant oxygen partial pressure. These changes were more significant than those  
20 before the cathodic polarization but still lower than those generated by oxygen partial  
21 pressure change. This experiment demonstrated that oxygen and methane began to  
22 have a competitive adsorption on *in-situ* generated oxygen vacancies created by  
23 cathodic polarization.  
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45 CeO<sub>2</sub> and CPO<sub>20</sub> are well known oxygen buffers with high oxygen storage/release  
46 capacity (OSC) due to the high mobility of lattice defects, like oxygen vacancies. Reddy  
47 et al. showed that a ceria-praseodymia system exhibited five times higher OSC than a  
48 pure ceria sample [26]. The high OSC of ceria-praseodymia was due to the increased  
49 presence of oxygen vacancies respect to CeO<sub>2</sub> and cooperative Ce<sup>4+</sup>/Ce<sup>3+</sup> and Pr<sup>4+</sup>/Pr<sup>3+</sup>  
50 redox couples. For this characteristic the influence of the adsorption of propene on  
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4 impedance spectra was more pronounced on CPO<sub>20</sub> than on CeO<sub>2</sub>; this effect was  
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6 clearly visible on DRT spectra reported in Figure 13.  
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9 Thus the efficiency towards oxygen storage capacity was a measurement of sensitivity  
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11 of the electrode to the reaction atmosphere change.  
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### 18 *Spectra deconvolution: CPO<sub>20</sub> infiltrated cell*

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21 The spectra were modelled using R(RQ)(RQ)(RQ) and R(RQ)(RQ)G as equivalent  
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23 circuits at OCV for CeO<sub>2</sub> and CPO<sub>20</sub> [19]. In this case, the Gerischer element (G) was  
24  
25 used to account for the mixed ionic and electronic behaviour of CPO<sub>20</sub>.  
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30 The simulation of the CPO<sub>20</sub> infiltrated cell was made using two models. The first model  
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32 with two CPE elements and one Gerischer element was used at temperatures between  
33  
34 500 °C and 400 °C. The second model with three CPE elements was used at  
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36 temperatures below 400 °C. As reported by Fagg et al. [27], at temperatures close to  
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38 350 °C the total conductivity in air for a Ce<sub>0.8</sub>Pr<sub>0.2</sub>O<sub>2-δ</sub> system showed decreased  
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40 activation energy as the conductivity became predominantly electronic through the  
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42 reoxidation of Pr<sup>3+</sup> to Pr<sup>4+</sup> with decreasing of oxygen vacancies. The evaluation of the  
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44 model was based on fitting residuals, accepting the lowest residual as the most reliable  
45  
46 fitting. The choice of model was thus based on reaction temperature and was able to  
47  
48 take into account the change in ionic conductivity of CPO<sub>20</sub>. The high frequency  
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50 process observed in the spectra (ARC1) had activation energy of 0.78 ± 0.06 eV. The  
51  
52 arc closed completely at high frequency when the temperature reached 300 °C. The  
53  
54 near equivalent capacitance lay between 2.04 × 10<sup>-8</sup> F/cm<sup>2</sup> and 2.8 × 10<sup>-8</sup> F/cm<sup>2</sup> and was  
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4 independent of temperature between 500 °C and 350 °C. The independence from  
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6 temperature and gas phase shift (Figure 13) attributed this arc to the migration of  
7  
8 oxygen ions from the electrolyte to the LSM<sub>15</sub>/CGO<sub>10</sub> electrode  
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12 At 300 °C an increase in the capacitance to  $7.5 \times 10^{-8}$  F/cm<sup>2</sup> was observed. This  
13  
14 behaviour could have been due to the overlap of the electrolyte grain boundaries  
15  
16 response with the oxygen ion migration. This was not clearly visible in the DRT analysis  
17  
18 likely due to the time constants overlap, but it was confirmed by the full closing of the  
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20 arc at 300 °C. The extraction of the activation energy for this high frequency process  
21  
22 was performed using the resistance values obtained at temperatures above 300 °C. The  
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24 high frequency arc (ARC 1) was slightly influenced by polarisation at +4 V, an increase  
25  
26 in arc resistance for temperatures below 500 °C and a small increase in activation  
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28 energy ( $0.86 \pm 0.1$  eV) were observed. At the same time the near equivalent  
29  
30 capacitance increased to  $3.2-4.1 \times 10^{-8}$  F/cm<sup>2</sup>.  
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38 The process belonging to the medium frequency region (ARC 2) had an activation  
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40 energy of  $0.58 \pm 0.1$  eV and a near equivalent capacitance that increased with  
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42 temperature from  $2.2 \times 10^{-4}$  F/cm<sup>2</sup> at 300 °C to  $5 \times 10^{-4}$  F/cm<sup>2</sup> at 500 °C. This arc  
43  
44 showed a slight dependence on reaction atmosphere and due to the increase of  
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46 capacitance with the temperature, this arc could be correlated to the adsorption,  
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48 diffusion or charge transfer at or near the three-phase boundary (i.e., increasing  
49  
50 temperature will increase the TPB zone and thereby increase the associated  
51  
52 capacitance). This part of the spectrum was fitted with a CPE element having n-values  
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54 between 0.45 and 0.53 depending on the temperature. The slope of this arc, the ratio of  
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56  $-Z''$  and  $Z'$ , calculated from the Nyquist plot increased with increasing temperature from  
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4 0.25 to 0.5. The distorted shape of the medium frequency arc was explained by the  
5 porous structure of the electrode. For an electrode-process described by an R-CPE  
6 parallel circuit, the impedance response in a porous electrode will be approximated by  
7 the square root of the impedance of the R-CPE element [28]:  
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$$Z_{R-CPE,porous} = \sqrt{Z_{R-CPE}}$$

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18 In Figure 10b, the application of +4 V was able to strongly affect ARC 2 and ARC 3,  
19 reducing them to a single process/arc. In this case it was possible to observe from the  
20 Nyquist plot in Figure 10b two well separated arcs over the entire spectra. The low  
21 frequency arc was associated to a two orders of magnitude increase in peak  
22 characteristic frequency and to a near equivalent capacitance of  $4.9-9.4 \cdot 10^{-5} \text{ F/cm}^2$ , but  
23 the dependence on temperature was not clear. The capacitance increased with  
24 decreasing temperature until 400 °C, and then decreased again at 350 °C and 300 °C.  
25 The polarisation decreased capacitance by one order of magnitude with respect to  
26 OCV. The second arc clearly lost its characteristic slope during polarisation. In this  
27 case, the n-value of the CPE used was between 0.59 and 0.64. The new arc formed  
28 under polarization had an activation energy of  $0.59 \pm 0.07 \text{ eV}$ , similar to the value  
29 obtained at OCV. We could therefore argue that the polarisation only affected the third  
30 arc. ARC 3 was modelled using two different elements. At temperatures of 350 °C and  
31 300 °C, an RQ element was used to simulate this arc. The spectra for both  
32 temperatures did not close at lower frequencies, complicating the fitting. This arc was  
33 strongly influenced by reaction atmosphere, had an activation energy of  $0.79 \pm 0.06 \text{ eV}$   
34 and a near equivalent capacitance of  $2.6-2.8 \times 10^{-3} \text{ F/cm}^2$ . At temperatures between 400  
35 °C and 500 °C, an RG element was used to simulate the spectra. Such an impedance  
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4 response has been argued to arise in both mixed electronic and ionic conductors, such  
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6 as LaSrCoO<sub>3</sub>, and in LSM/YSZ when cathodically polarised. This characteristic was not  
7  
8 visible on CeO<sub>2</sub> infiltrated cell spectra, so it was possible that this behaviour was a result  
9  
10 of CPO<sub>20</sub> infiltration where oxygen ion diffusion through CPO<sub>20</sub> was coupled with oxygen  
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12 ion discharge at the extended TPB.  
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17 In mixed ionic electronic conductor cathodes, oxygen ion diffusion is argued to occur  
18  
19 primarily along bulk paths, giving high capacitance values near 1 F/cm<sup>2</sup> [29]. In this  
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21 study, the capacitance was found to be 1.1×10<sup>-3</sup> F/cm<sup>2</sup> at 500 °C and increased to  
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23 3.5×10<sup>-3</sup> F/cm<sup>2</sup> at 400 °C. These values were far from values found by Adler [29] (1  
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25 F/cm<sup>2</sup>). A value of 100 μF was also found by Hjalmarsson et al. using LaCoNiO<sub>3</sub>-  
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27 CeGdO and attributed to oxygen transport confined to the electrode surface rather than  
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29 the bulk [30]. Oxygen ion diffusion could follow two different paths: along the electrode  
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31 surface (LSM<sub>15</sub>) or along bulk paths (CPO<sub>20</sub>). The activation of the resistance,  $R_G$ ,  
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33 associated to a Gerischer element was found to be 0.44 ± 0.05 eV.  
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#### 43 *Spectra deconvolution: CeO<sub>2</sub> infiltrated cell*

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46 The spectra of the CeO<sub>2</sub> infiltrated cell were modelled using 3 CPE elements in series  
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48 with a resistance R(RQ)(RQ)(RQ) for all temperatures. The spectra at 350 °C and 300  
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50 °C recorded at OCV also did not close at low frequencies. The first process at high  
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52 frequencies visible in DRT analysis of Figure 12 was associated to the first arc (ARC 1).  
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54 The activation energy of this arc was 1.14 ± 0.15 eV at OCV and was surprisingly higher  
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56 than the value obtained for the CPO<sub>20</sub> cell. The difference in ARC 1 resistance between  
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4 CeO<sub>2</sub> and CPO<sub>20</sub> cells is mainly visible for temperatures between 400 °C and 300 °C  
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6 and not for higher temperatures. This behaviour is confirmed by DRT analysis of Figure  
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9 12, Figure 13 and 14 where the two cells show a similar resistance for the relaxation  
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11 contribution at high frequency.  
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15 The application of +4 V polarisation had no effect on the resistance of this arc with an  
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17 observed activation energy of  $1.13 \pm 0.08$  eV. It was thus possible to infer that also this  
18  
19 part of the spectra could be influenced by the infiltration material especially at medium-  
20  
21 low temperature and could contain overlapping processes. This overlap would  
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23 complicate separation of two close relaxation times belonging to the infiltrated material  
24  
25 and the backbone.  
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30 As verified for CPO<sub>20</sub>, the near equivalent capacitance of this arc was almost unaffected  
31  
32 by temperature both at OCV and at +4 V (values between  $4.5$  and  $4.7 \times 10^{-8}$  F/cm<sup>2</sup>). At  
33  
34 300 °C, where the first arc was fully closed on the high frequency side, the capacitance  
35  
36 dropped to  $2.9 \times 10^{-8}$  F/cm<sup>2</sup>. At this temperature it was possible to measure the  
37  
38 electrolyte grain boundaries contribution to conductivity. Additionally, this arc was not  
39  
40 affected by reaction atmosphere. Analysing its characteristics, this arc was attributed to  
41  
42 the migration of oxygen ions from the electrolyte to the LSM<sub>15</sub>/CGO<sub>10</sub> electrode.  
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48 As observed for CPO<sub>20</sub>, the polarization effect for the CeO<sub>2</sub> infiltrated cell was also  
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50 visible on the second/third arc (ARC 2-ARC 3) and associated to a strong decrease in  
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52 resistance and increased peak frequency (Figure 11c and 11b). This part of the  
53  
54 spectrum was modelled with two RQ at OCV. For ARC 2 (Figure 11a), n-values used  
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56 for the fitting ranged from 0.49 to 0.68 and the activation energy was  $0.79 \pm 0.03$  eV.  
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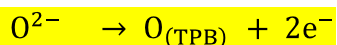


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4 The near equivalent capacitance increased from  $1.3 \text{ to } 2.1 \times 10^{-4} \text{ F/cm}^2$  with increasing  
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6 temperature. In addition, this arc was also affected by the infiltration material. The two  
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8 modelled arcs visible at OCV merged into one when the cell was polarized at +4 V  
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10 (Figure 11b). The activation energy measured at +4 V was  $1.11 \pm 0.06 \text{ eV}$  with only one  
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12 arc observable at this voltage, and contrary to  $\text{CPO}_{20}$ , this activation energy likely  
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14 belonged to a different process. The near equivalent capacitance increased from  $5.2 \times$   
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16  $10^{-5} \text{ F/cm}^2$  at  $300 \text{ }^\circ\text{C}$  to  $8 \times 10^{-5} \text{ F/cm}^2$  at  $500 \text{ }^\circ\text{C}$ . The polarization, as observed for  
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18  $\text{CPO}_{20}$ , was able to decrease the capacitance by one order of magnitude. The  
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20 temperature dependence, the polarisation effect and the insensitivity to atmosphere  
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22 (Figure 14) assigned this arc to the charge transfer near or at the TPB.  
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30 The third arc (ARC 3) was only modelled and visible at OCV. This arc was affected by  
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32 reaction atmosphere, as shown in the DRT analysis of Figure 14, and by temperature  
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34 with an activation energy of  $0.98 \pm 0.04 \text{ eV}$ . The near equivalent capacitance strongly  
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36 increased with temperature from  $8.6 \times 10^{-5} \text{ F/cm}^2$  at  $300 \text{ }^\circ\text{C}$  to  $5.7 \times 10^{-4} \text{ F/cm}^2$  at  $500$   
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38  $^\circ\text{C}$ . This process was thus related to the adsorption and dissociation of oxygen, as well  
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40 as electrode reaction, on the catalyst/electrode surface.  
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45 For both infiltrated material, ARC 1 was attributed to oxygen ion transport between the  
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47 electrolyte and LSM and to grain boundary conductivity; these processes were not  
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49 faradaic. The strong resistance decrease upon polarization of ARC 2 and ARC 3  
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51 indicated that medium and high frequency part of the spectra contained a charge  
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53 transfer contribution following the Butler-Volmer equation. This behaviour did not  
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55 exclude the possibility that chemical/physical processes could contribute to the total  
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57 resistance; these processes, if associated to an electrochemical process, can exhibit  
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4 the general Butler-Volmer behaviour [31]. According to C.J. Borja, [32] ARC 2 could be  
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6 tentatively attributed to the charge transfer reaction taking place at the three phase  
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8 boundaries:  
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16 The oxygen formed at TPB could undergo different reactions: it could recombine to form  
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18 molecular oxygen, react with adsorbed propene giving rise to an increase of reaction  
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20 rate or migrate over the entire gas-exposed catalyst electrode surface establishing an  
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22 effective double layer able to increase the reaction rate above the faradaic limit (EPOC).  
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27 The ARC 3 was the most affected by introduction of propene in the gas mixture as also  
28  
29 reported by Butlel with Pt/YSZ system [33]. Propene was strongly adsorbed on  
30  
31 electrode surface; it is possible to argue that the introduction of propene could interfere  
32  
33 with a process involving biatomic oxygen or dissociated oxygen on the surface.  
34  
35 Kaloyannis et al. [34] reported a competitive adsorption mechanism of dissociative  
36  
37 chemisorbed oxygen and propylene during electrochemical promotion studies with  
38  
39 stronger binding of propylene than oxygen on the Pt catalyst surface. As illustrated  
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41 before, the sensitivity to propene introduction was dependent on infiltrated material and  
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43 especially on its oxygen vacancies mobility.  
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50 Upon applying positive potential the increase in catalyst work function is obtained  
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52 primarily by the increase in the coverage of the backspillover oxide ions  $O^{\square}$ ; the effects  
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54 should be to enhance the reactivity of surface oxygen species coming from the gas  
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56 phase and changing the adsorption strength of the adsorbates like oxygen and propene.  
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59 The effect of polarization on impedance spectra in this work was visible at medium and  
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4 low frequency associated to one order of magnitude decrease of both resistance and  
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6 capacitance; the impedance spectra recorded under polarization did not show any new  
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8 semicircle with high capacitance ( $> 200 \mu\text{F}/\text{cm}^2$ ) as reported by Vayenas et al. [35] and  
9  
10 attributed to backspillover oxygen semicircle. In this work EPOC behavior was not  
11  
12 visible, probably due to the fast reaction of oxygen ions with another oxygen or with  
13  
14 propene; the short lifetime of the oxygen ions hindered the possibility to the effective  
15  
16 double layer formation between the catalyst and the gas phase. Kambolis et al. [36] did  
17  
18 not observe EPOC in propane oxidation on LSCF/GDC electrode but it was observed  
19  
20 on Pt infiltrated LSCF/GDC electrode, especially at low temperature (267 °C). The  
21  
22 impregnation of Pt had two effects: increase the reaction rate towards propane oxidation  
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24 at OCV and also the electrode polarization resistance ( $R_p$ ) measured at OCV. These  
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26 two combined effects gave rise to EPOC behavior.  
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## 37 **Conclusions**

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41 The catalytic activity of a  $\text{CeO}_2$  infiltrated cell in propene oxidation was shown to be  
42  
43 superior to a  $\text{CPO}_{20}$  system. The performance in terms of polarization effect on propene  
44  
45 oxidation was strongly influenced by electrochemical and electrical properties of the  
46  
47 infiltrated material.  $\text{CeO}_2$  infiltrated cell exhibited high electrode resistance if compared  
48  
49 to  $\text{CPO}_{20}$ . The activity of  $\text{CeO}_2$  in propene oxidation was highly influenced by  
50  
51 polarization, especially at low temperatures, and displayed good faradaic efficiency. The  
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53 low electrode resistance of  $\text{CPO}_{20}$ , instead, was detrimental to obtain good faradaic  
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4 efficiency at low temperature, likely due to the short lifetime of oxygen ion promoters  
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6 given by mixed conductivity of  $\text{CPO}_{20}$ .  
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10 Impedance spectra exhibited three main features belonging to oxygen ion  
11 migration/grain boundary conductivity, charge transfer reaction of oxygen ion and  $\text{O}_2$   
12 adsorption/dissociation on the electrode surface. The spectra recorded under anodic  
13  
14 polarization showed a strong decrease of resistance and capacitance at medium-low  
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16 frequency range while the contribution at high frequency was unaffected.  
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23 The introduction of propene in the reaction atmosphere affected the low frequency  
24 contribution on impedance spectra;  $\text{CPO}_{20}$  was affected on a major extent, probably due  
25 to the higher oxygen vacancies mobility compared to  $\text{CeO}_2$ . EPOC behaviour was not  
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27 visible for both the infiltrated cells; the backspillover of oxygen ions was hindered by the  
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29 high reactivity of the oxygen promoter at the TPB.  
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7 Captions  
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13 **Fig. 1:** Scheme of the reactor configuration.  
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16 **Fig. 2:** SEM micrograph of a CeO<sub>2</sub> infiltrated cell.  
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20 **Fig. 3:** SEM micrograph of a CPO<sub>20</sub> infiltrated cell.  
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23 **Fig. 4 :** XRD powder pattern of CPO<sub>20</sub> powder.  
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26 **Fig. 5:** Reaction rate for propene oxidation as a function of temperature in 1000 ppm  
27 C<sub>3</sub>H<sub>6</sub> and 10% O<sub>2</sub> at 2 L/h.  
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32 **Fig. 6:** Rate enhancement ratios of CeO<sub>2</sub> and CPO<sub>20</sub> infiltrated cells as a function of  
33 temperature.  
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38 **Fig. 7 :** Faradaic efficiency of CeO<sub>2</sub> and CPO<sub>20</sub> infiltrated cells versus temperature.  
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41 **Fig. 8:** Arrhenius plots of polarisation resistance ( $R_p$ ) at OCV for CeO<sub>2</sub> and CPO<sub>20</sub>  
42 infiltrated cells.  
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47 **Fig. 9:** Arrhenius plots of polarization resistance ( $R_p$ ) at +4 V for CeO<sub>2</sub> and CPO<sub>20</sub>  
48 infiltrated cells.  
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53 **Fig. 10:** Nyquist plots of impedance spectra of a CPO<sub>20</sub> infiltrated cell recorded at a)  
54 OCV, b) +4 V and c) Bode plot of impedance spectra at 450 °C and OCV with 10% O<sub>2</sub>  
55 and 1000 ppm C<sub>3</sub>H<sub>6</sub> at 2 L/h.  
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4 **Fig. 11:** Nyquist plots of impedance spectra of a CeO<sub>2</sub> infiltrated cell recorded at a)  
5 OCV, b) +4 V and c) Bode plot of the impedance spectra as a function of frequency at  
6  
7 450 °C and OCV with 10% O<sub>2</sub> and 1000 ppm C<sub>3</sub>H<sub>6</sub> at 2 L/h.  
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12 **Fig. 12:** Distribution of relaxation times (DRT) for CeO<sub>2</sub> and CPO<sub>20</sub> spectra recorded at  
13 450 °C and OCV with 10% O<sub>2</sub> and 1000 ppm C<sub>3</sub>H<sub>6</sub> at 2 L/h.  
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18 **Fig. 13:** Distribution of relaxation times (DRT) in the CPO<sub>20</sub> spectra recorded at 500 °C  
19 and OCV with 10% O<sub>2</sub> and 10% O<sub>2</sub> + 1000 ppm C<sub>3</sub>H<sub>6</sub> at 2 L/h.  
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24 **Fig. 14 :** Distribution of relaxation times (DRT) in the CeO<sub>2</sub> spectra recorded at 500 °C  
25 and OCV with 10% O<sub>2</sub> and 10% O<sub>2</sub> + 1000 ppm C<sub>3</sub>H<sub>6</sub> at 2 L/h.  
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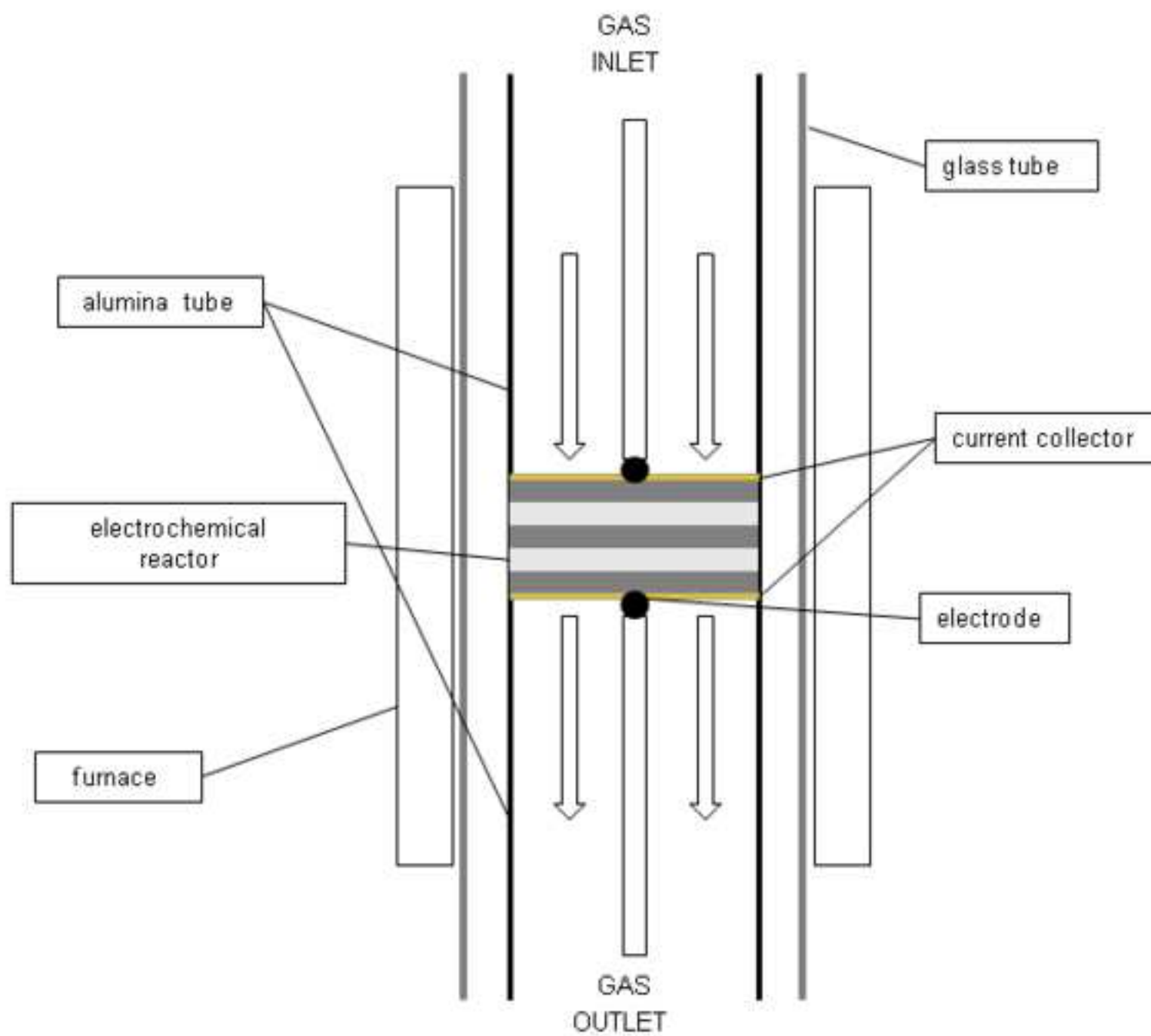


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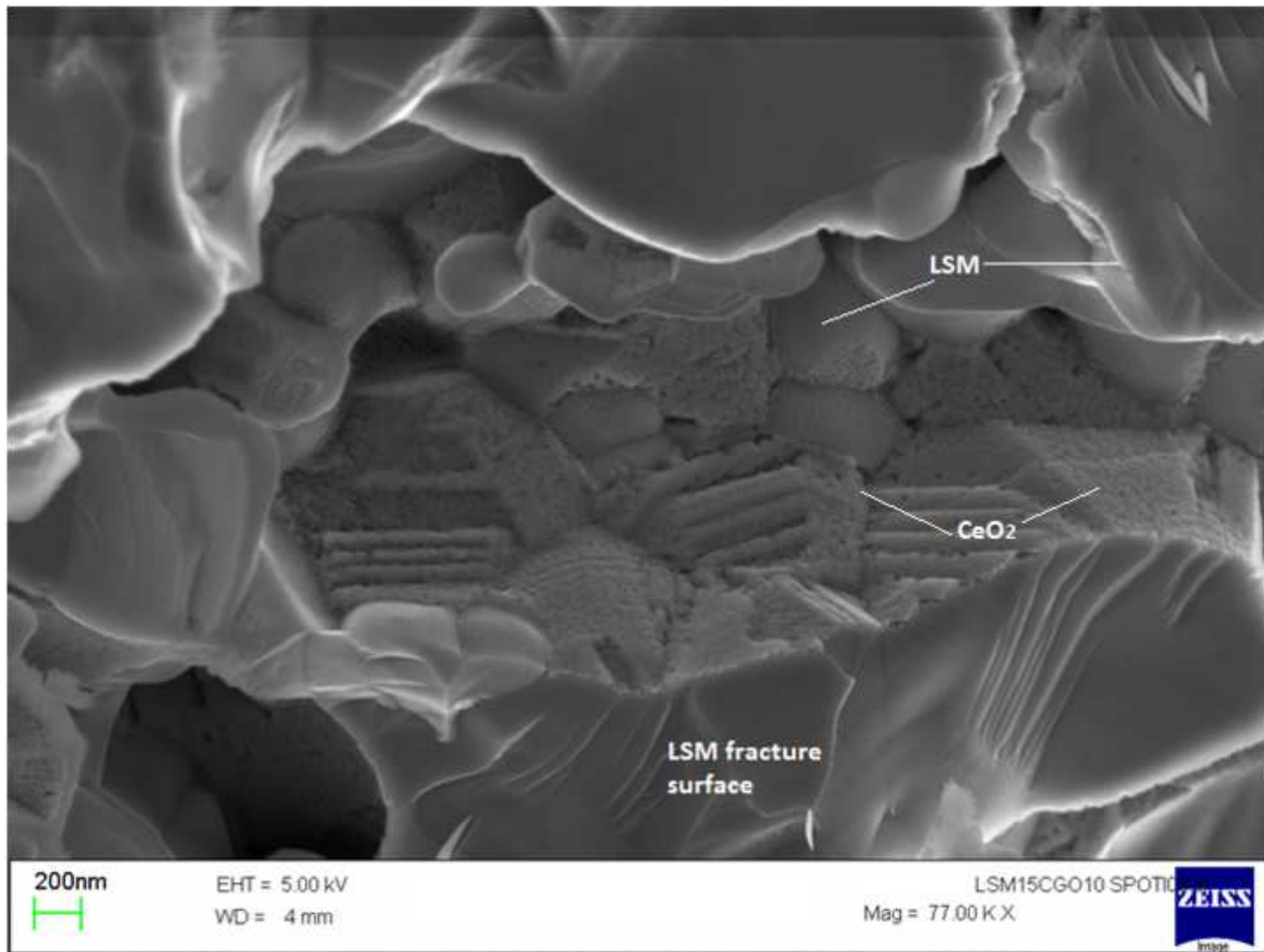


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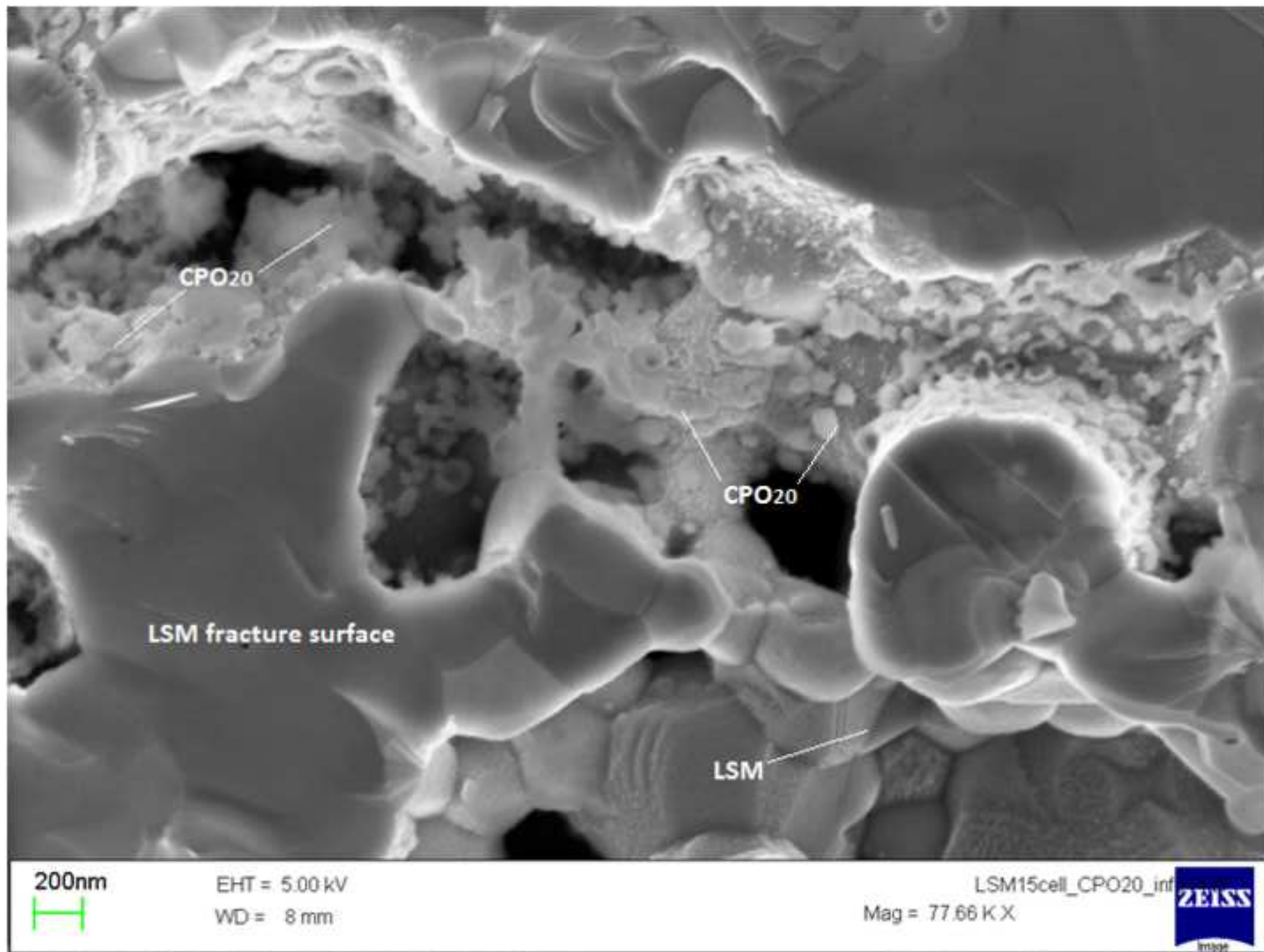


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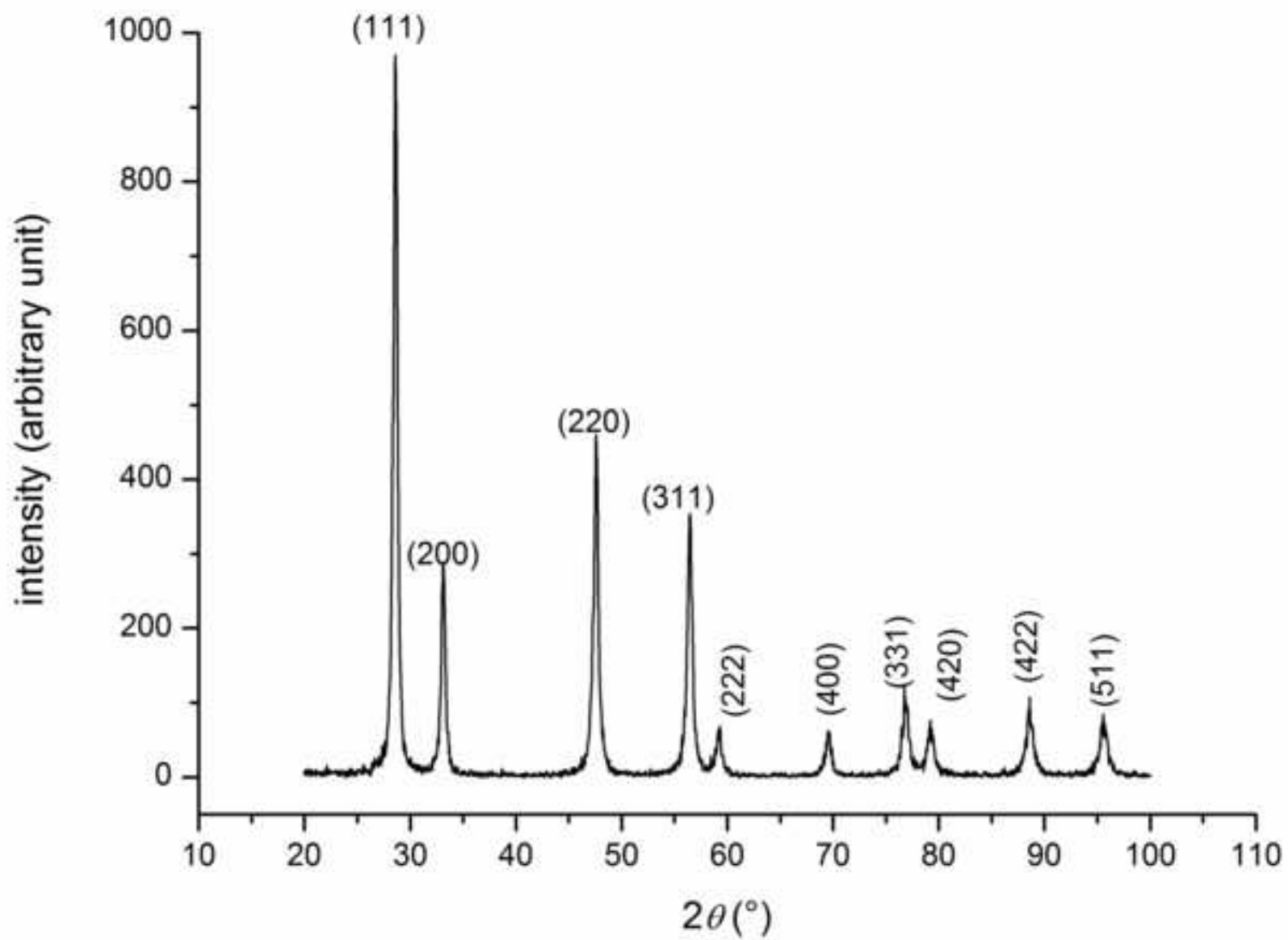


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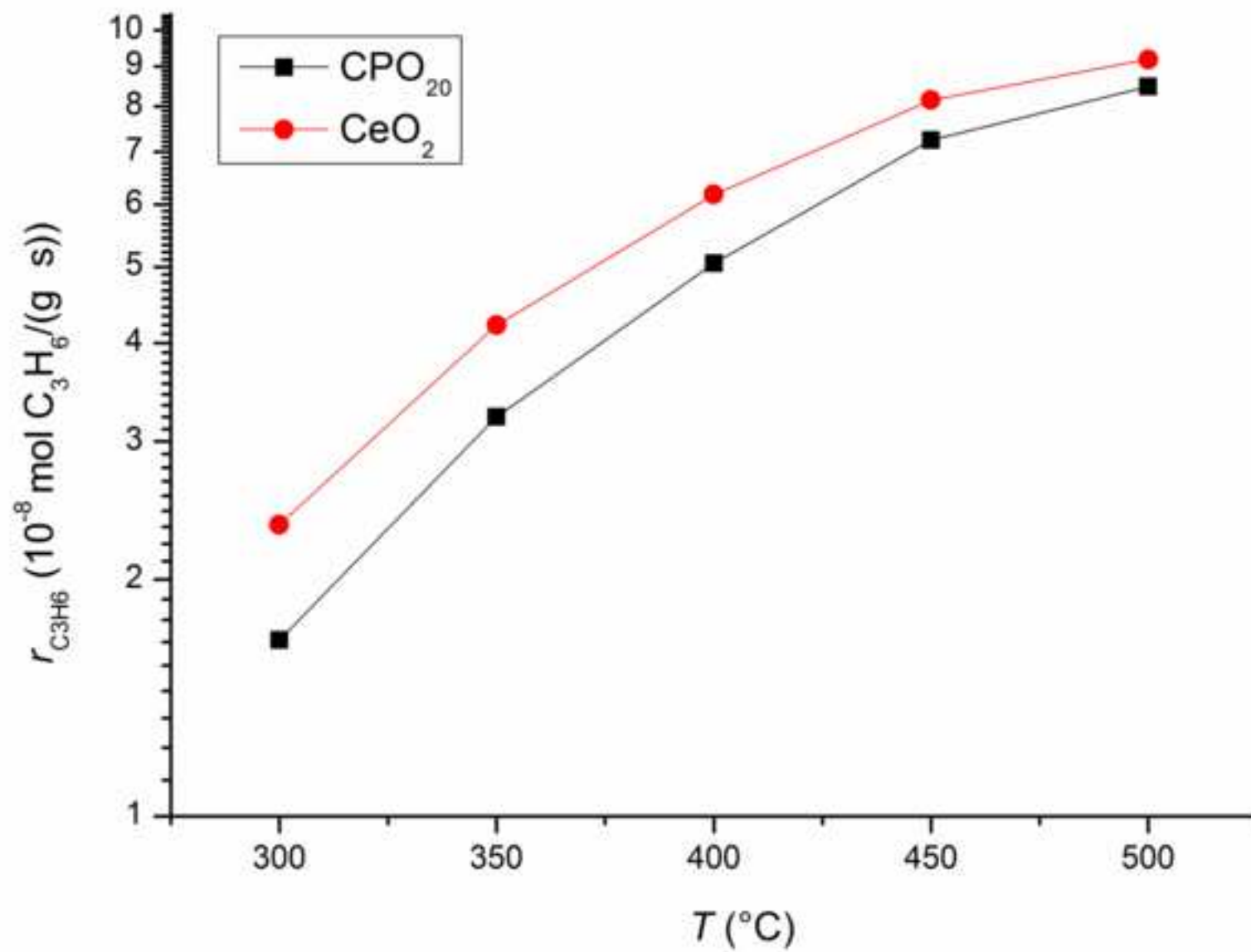


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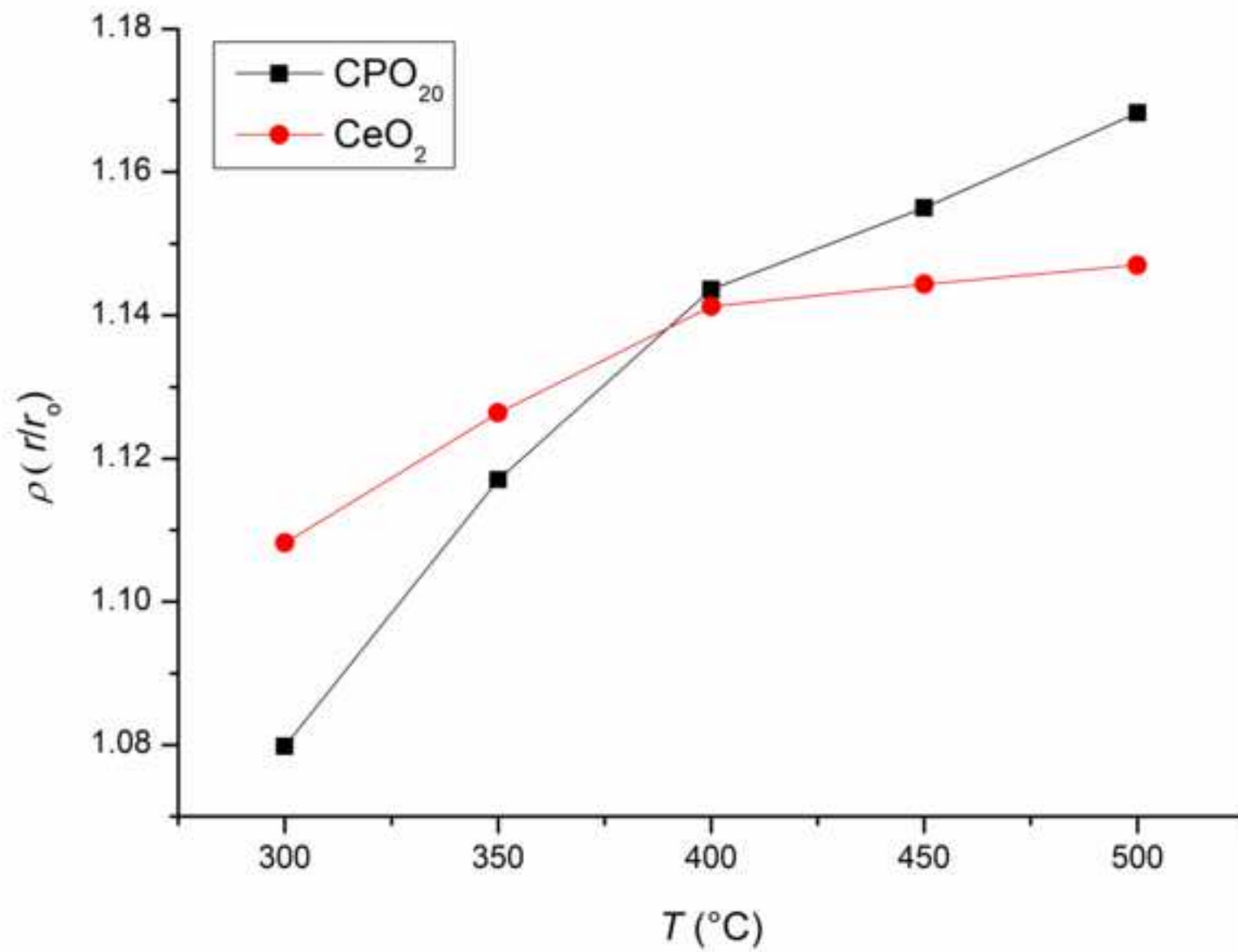


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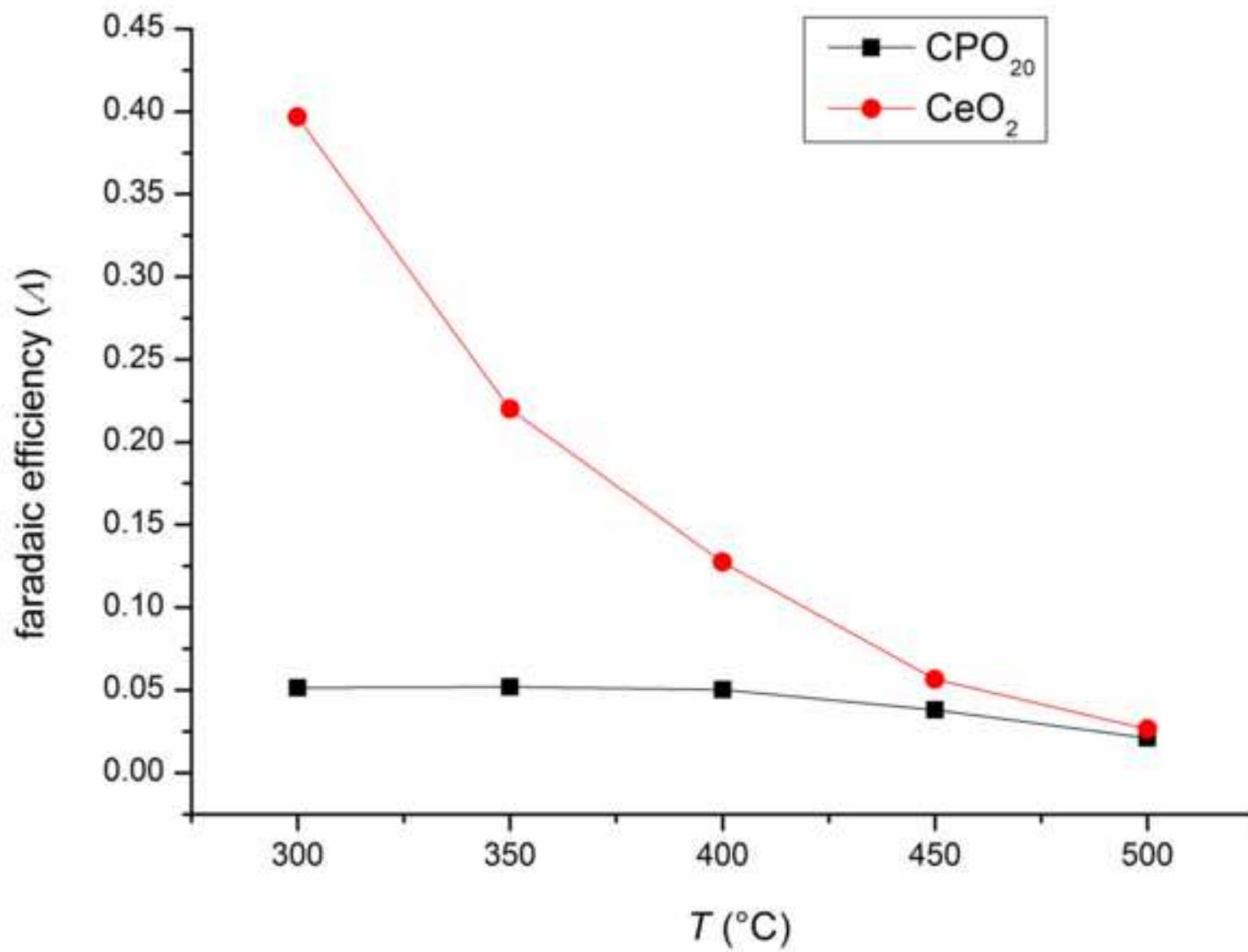




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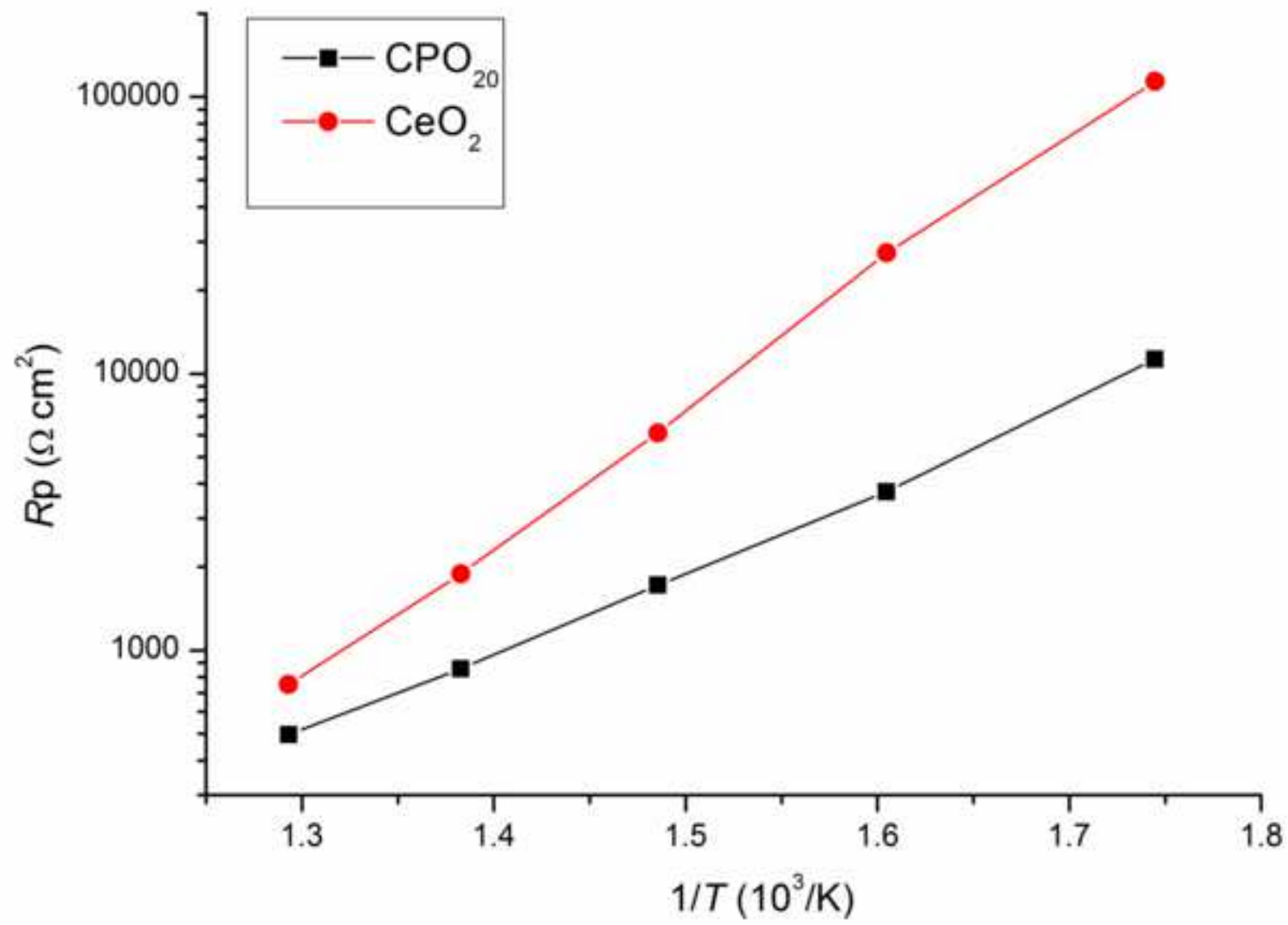


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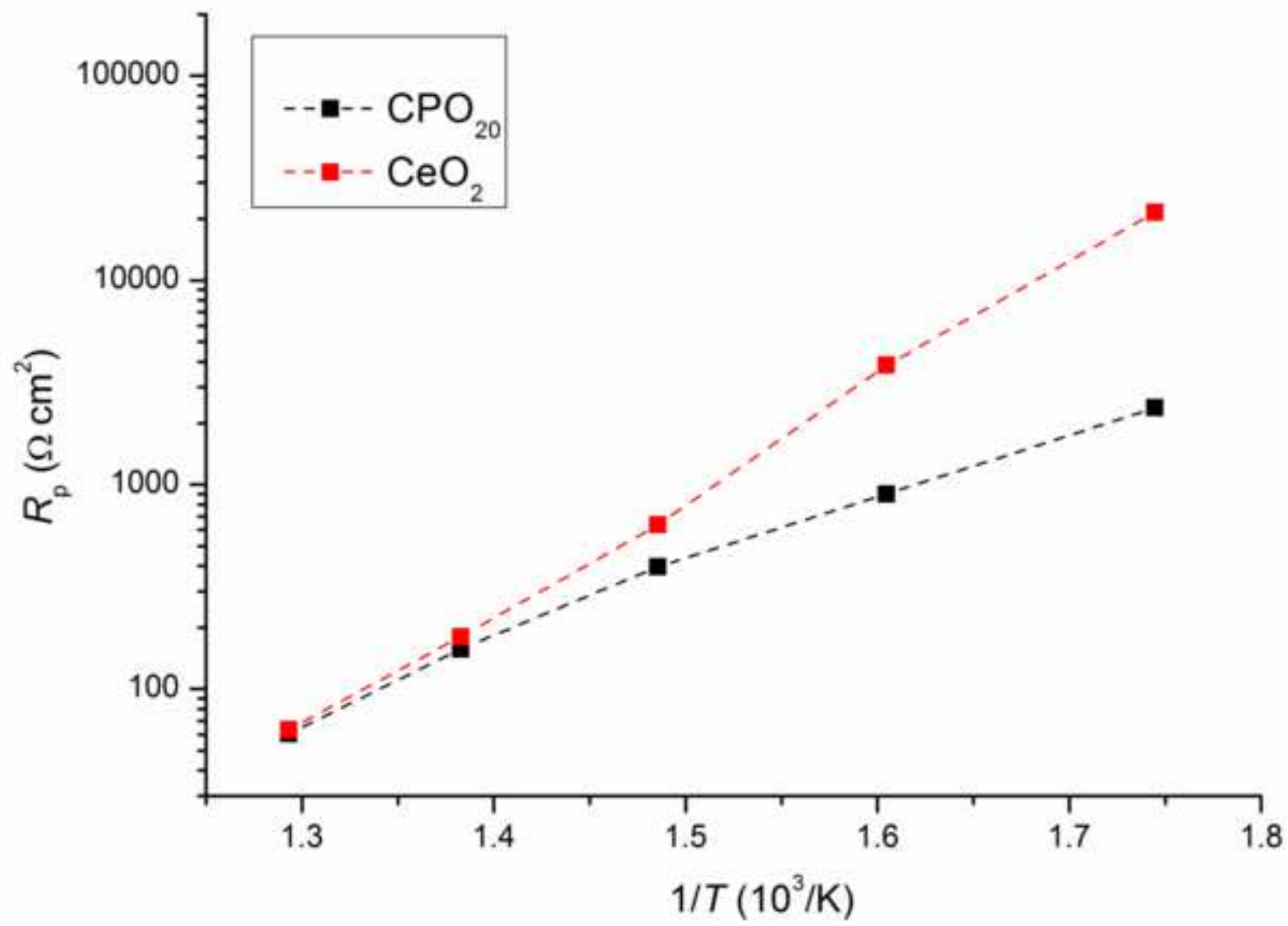


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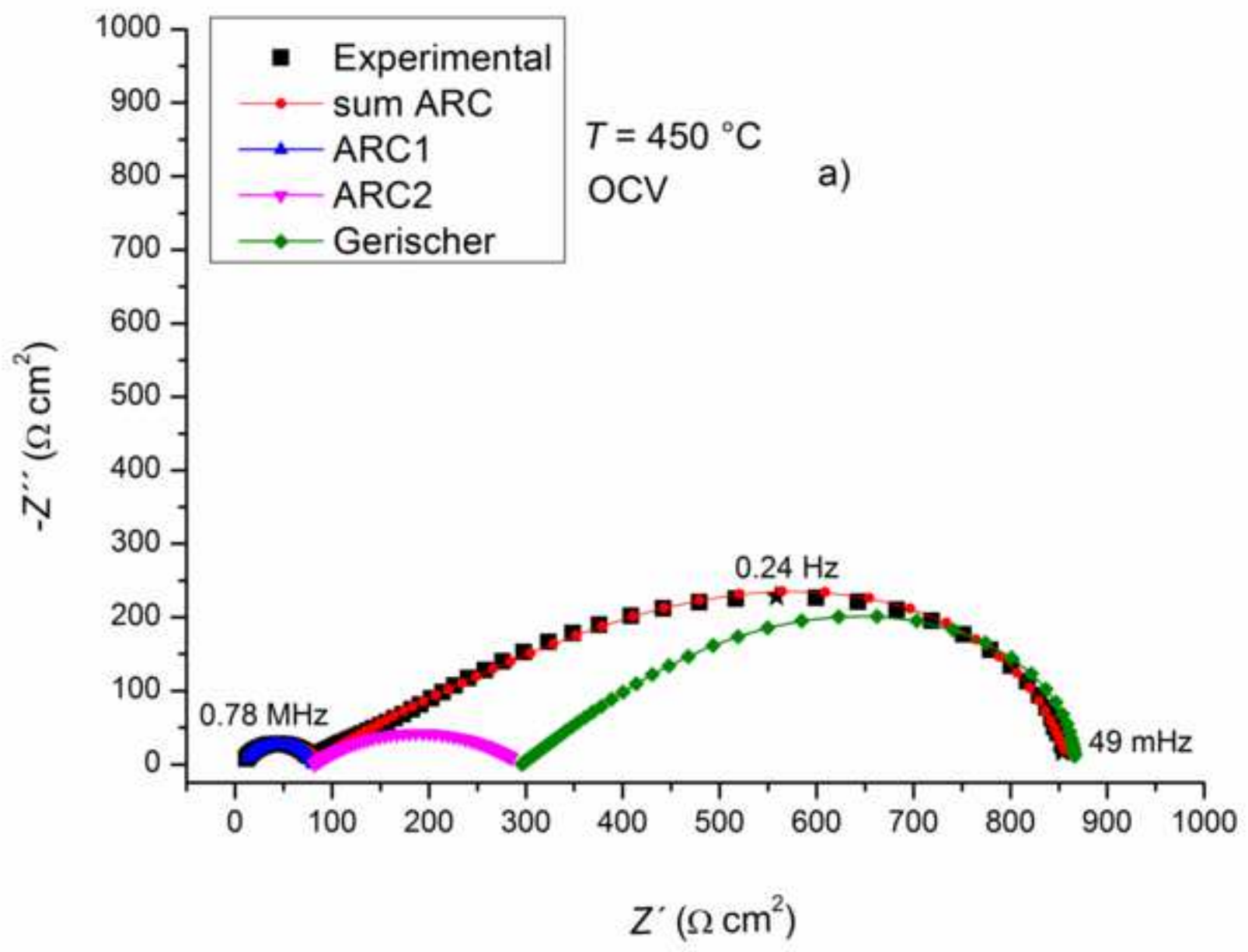


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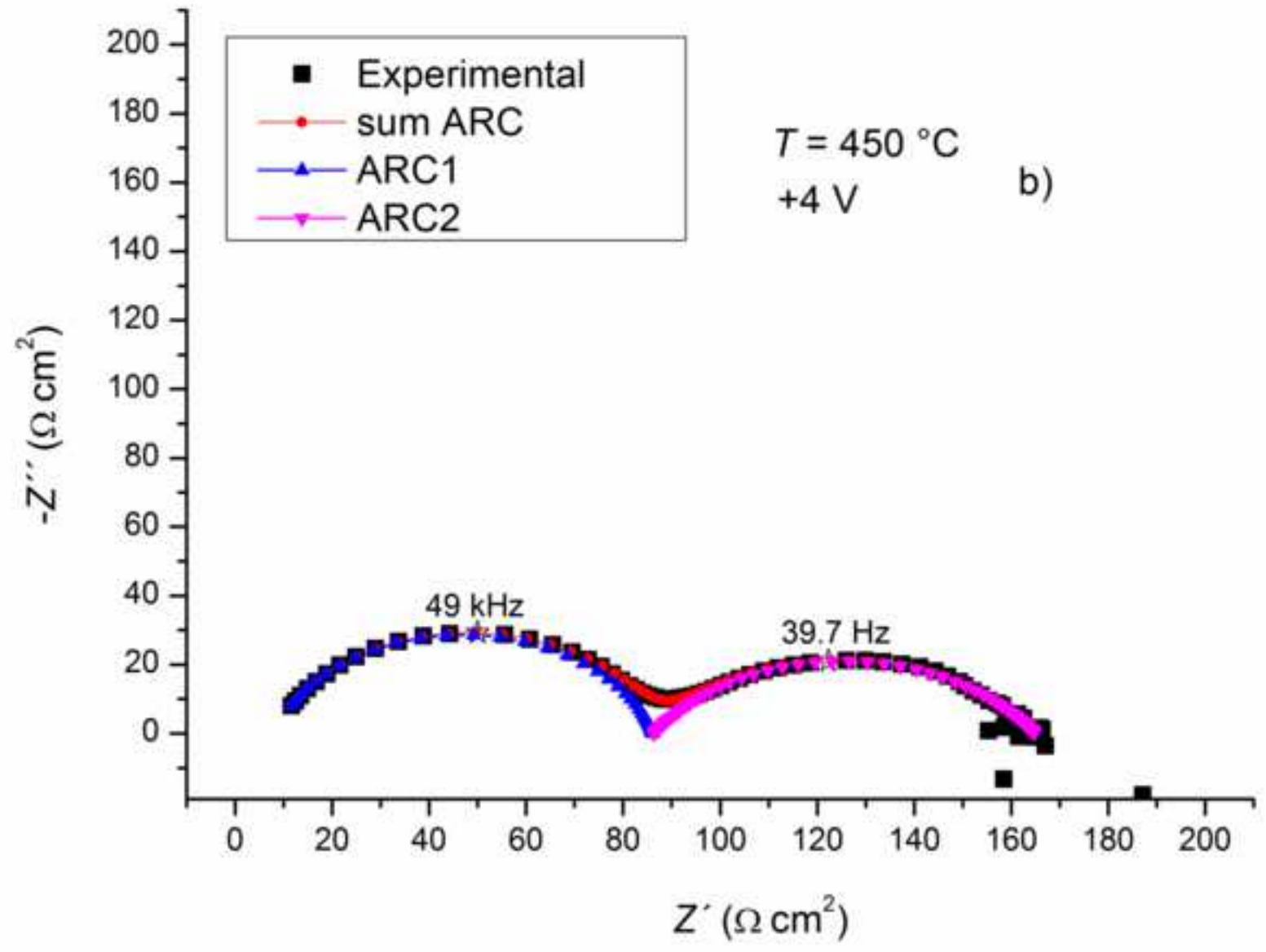


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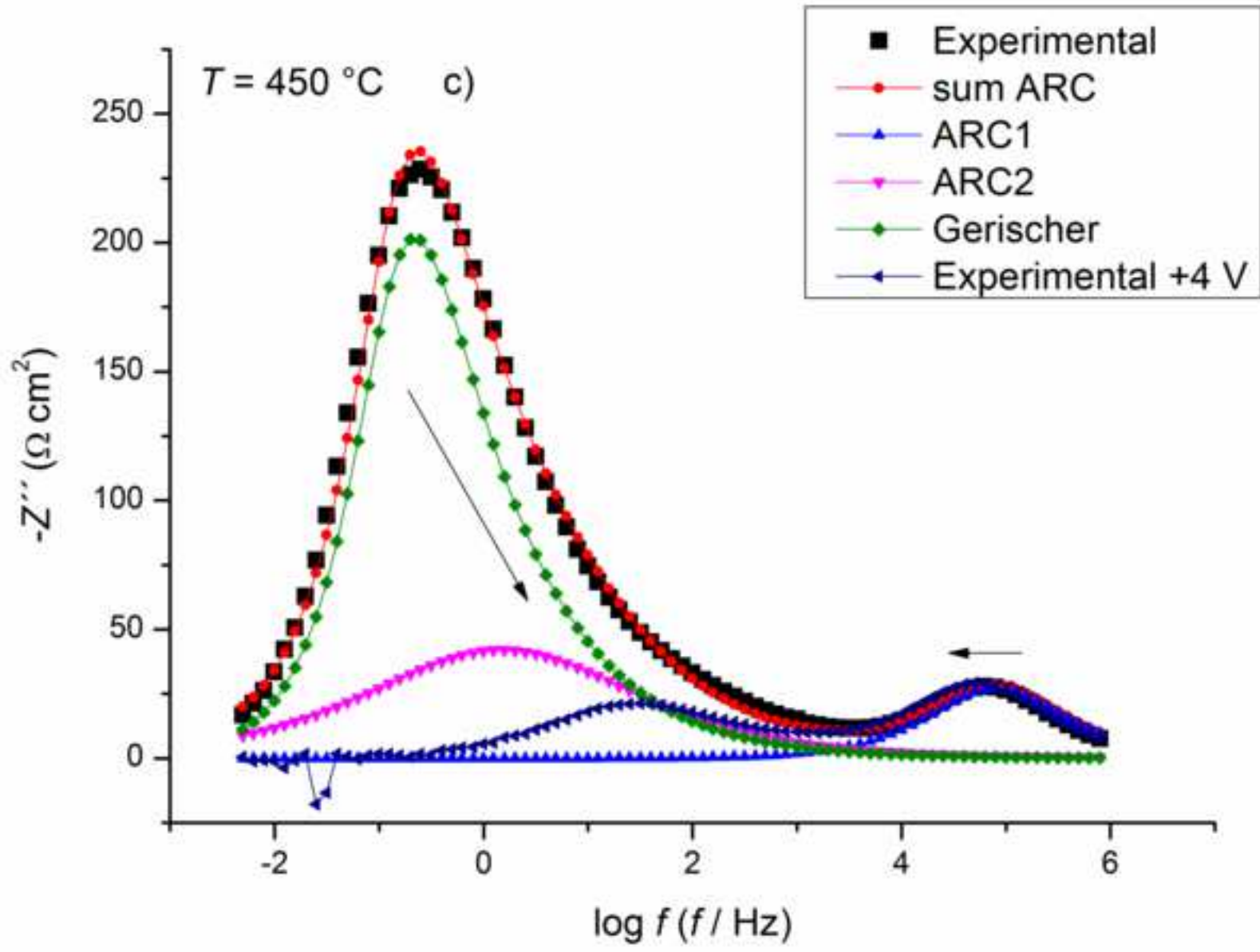


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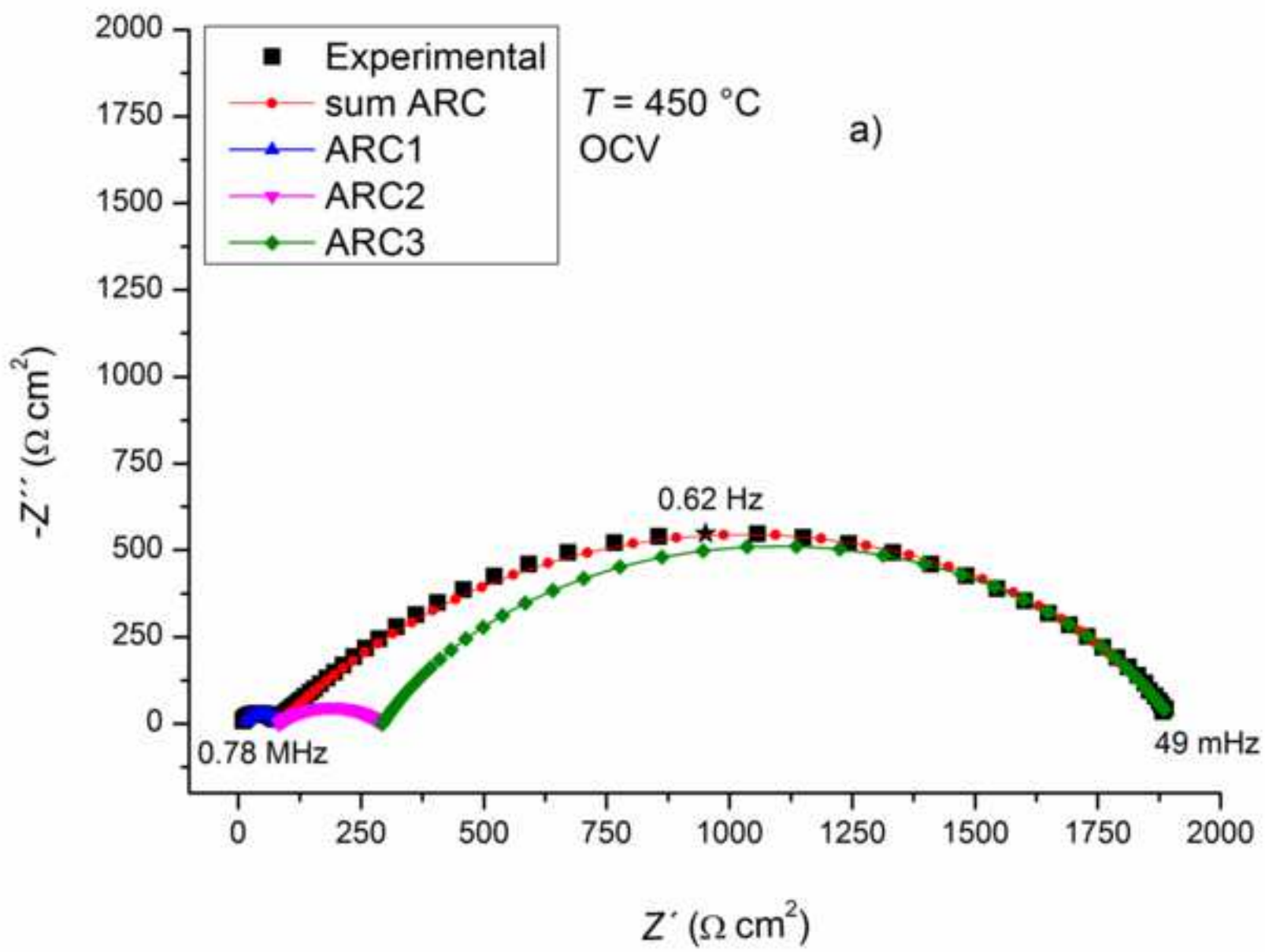


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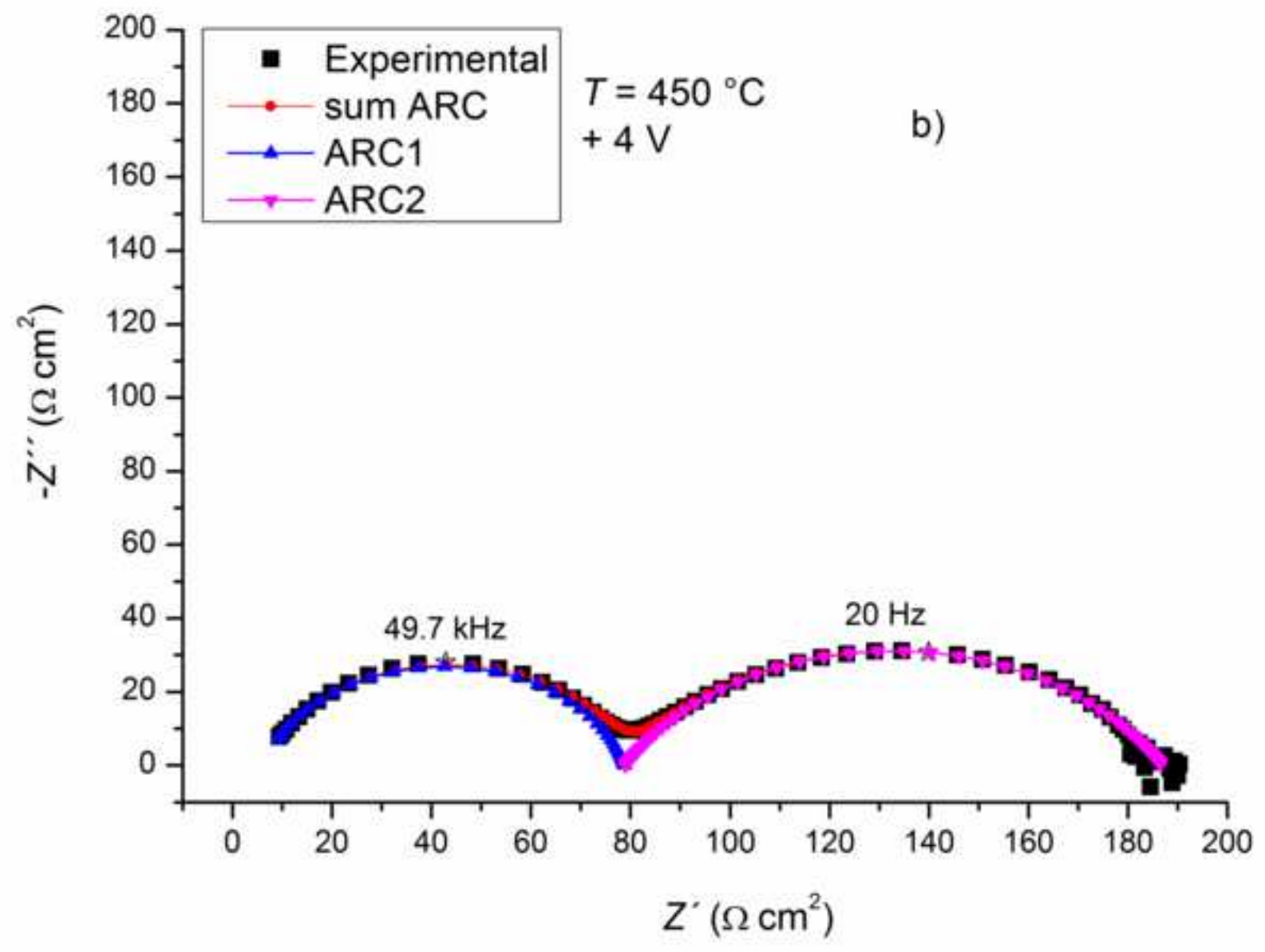


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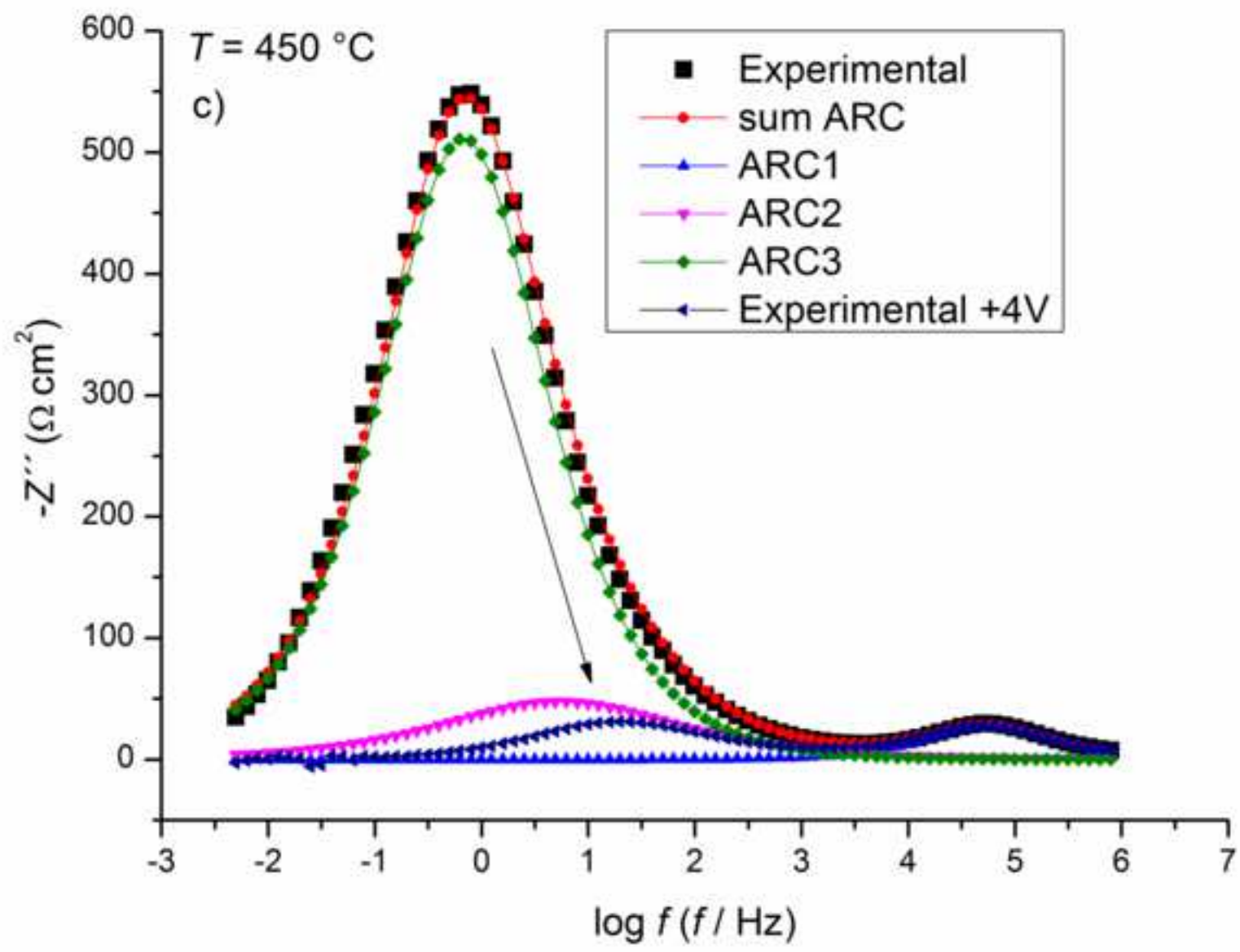




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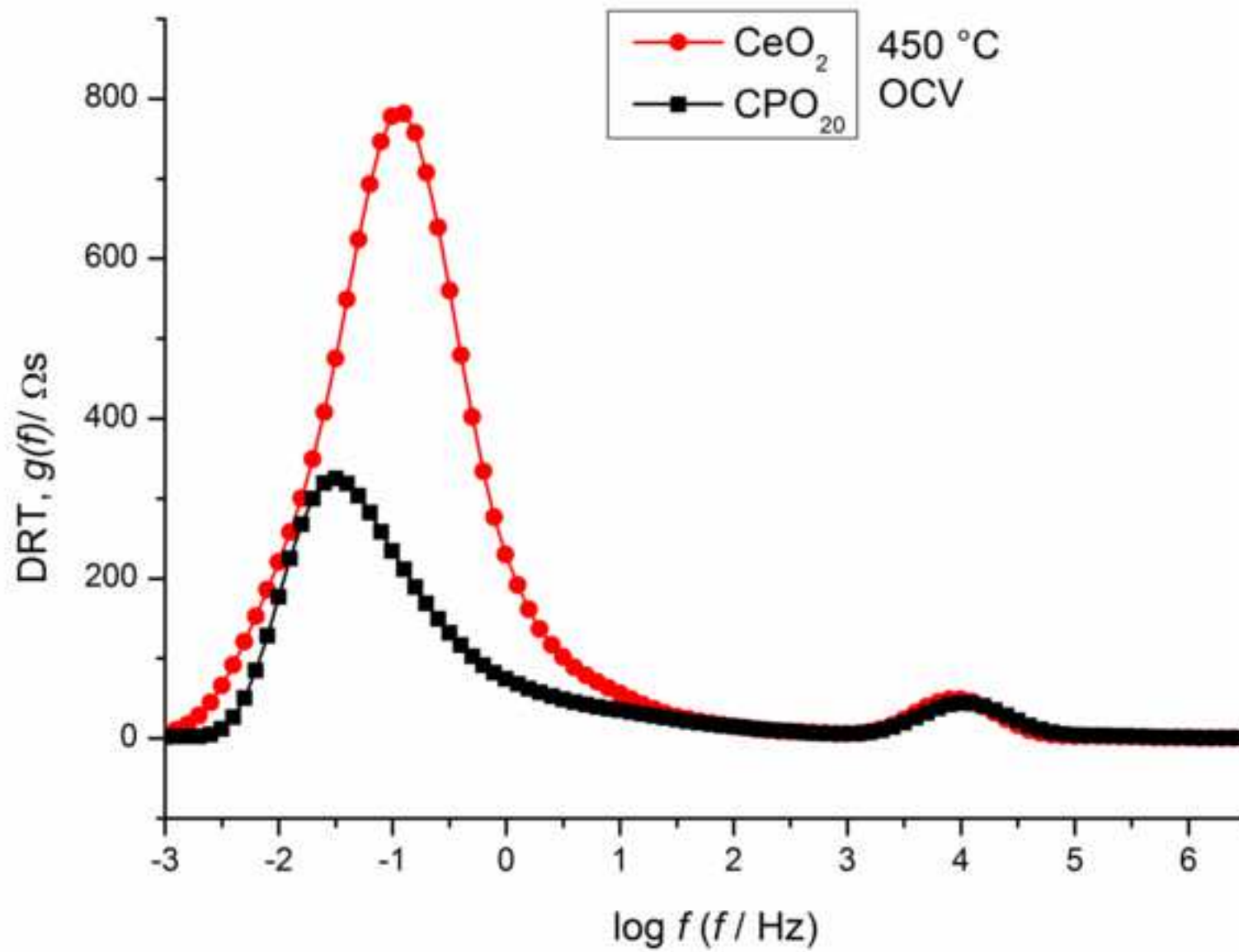


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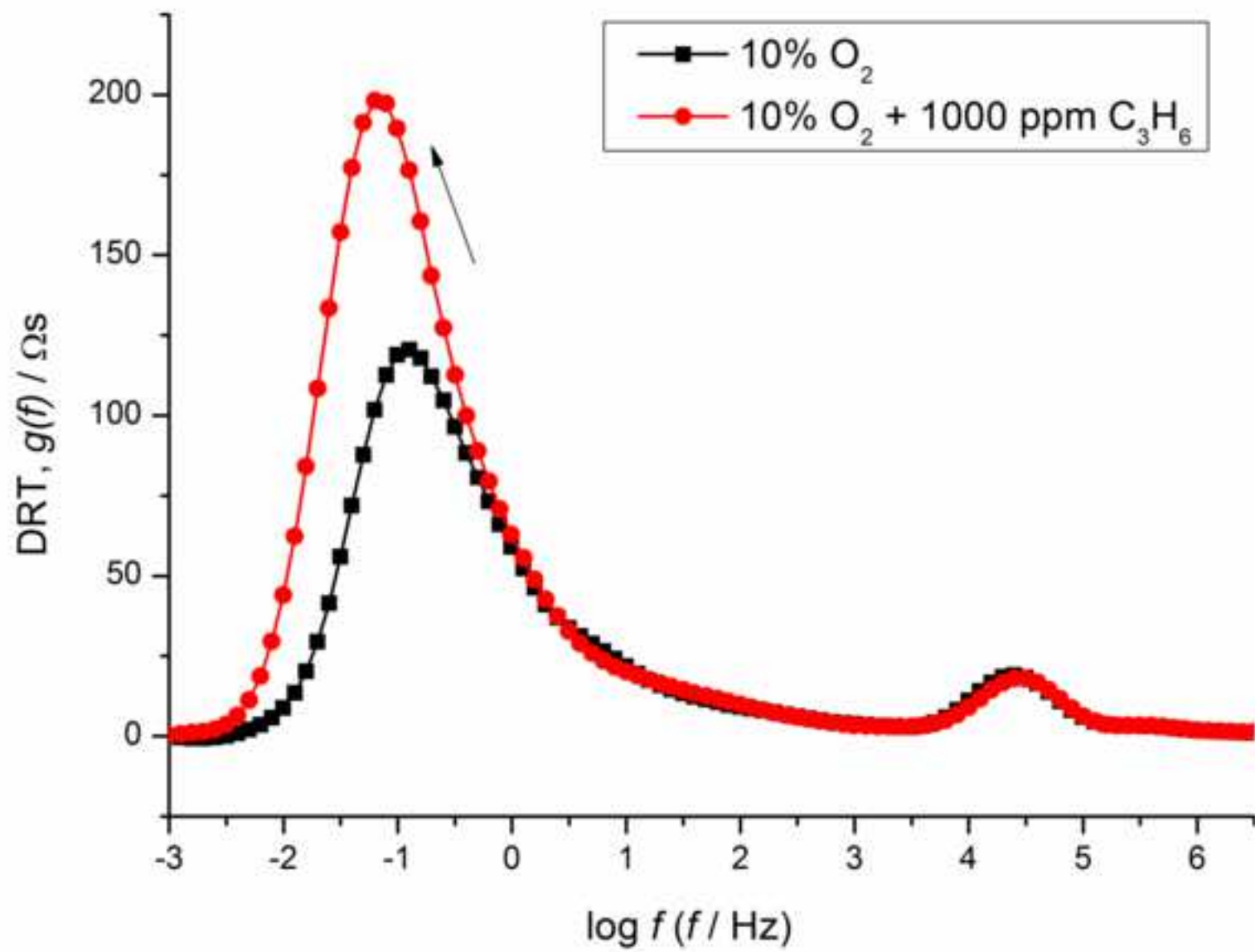


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