Technical University of Denmark



Computational Methods for Model Predictive Control

New Opportunities for Computational Scientists

Jørgensen, John Bagterp; Boiroux, Dimitri; Hovgaard, Tobias Gybel; Halvgaard, Rasmus Fogtmann; Skajaa, Anders; Gade-Nielsen, Nicolai Fog; Standardi, Laura; Sokoler, Leo Emil; Völcker, Carsten; Capolei, Andrea; Frison, Gianluca; Schmidt, Signe; Duun-Henriksen, Anne Katrine

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Computational Methods for Model Predictive Control New Opportunities for Computational Scientists

John Bagterp Jørgensen

Dimitri Boiroux, Tobias Gybel Hovgaard, Rasmus Halvgaard, Anders Skajaa, Nicolai Fog Gade-Nielsen, Laura Standardi, Leo Emil Sokoler, Carsten Völcker, Andrea Capolei, Gianluca Frison, Signe Schmidt, Anne-Katrine Dunn Henriksen **Technical University of Denmark**

> PARA 2012, Finlandia Hall, Helsinki, Finland June 10-13, 2012

DTU Informatics Department of Informatics and Mathematical Modeling

CERE Center for Energy Resources Engineering

DTU

Introduction

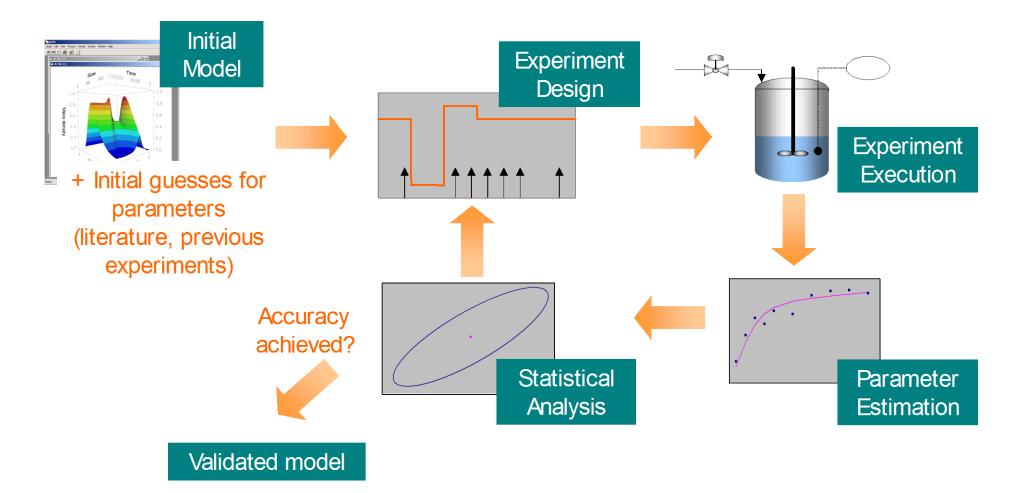
- Model Predictive Control
 - Optimal Experimental Design
 - Parameter Estimation
 - State Estimation
 - Regulation
- Constrained Optimization of Dynamical Systems
- Case Studies
 - The Artificial Pancreas
 - Closed-Loop Oil Reservoir Management
 - Smart Energy Systems



MODEL PREDICTIVE CONTROL

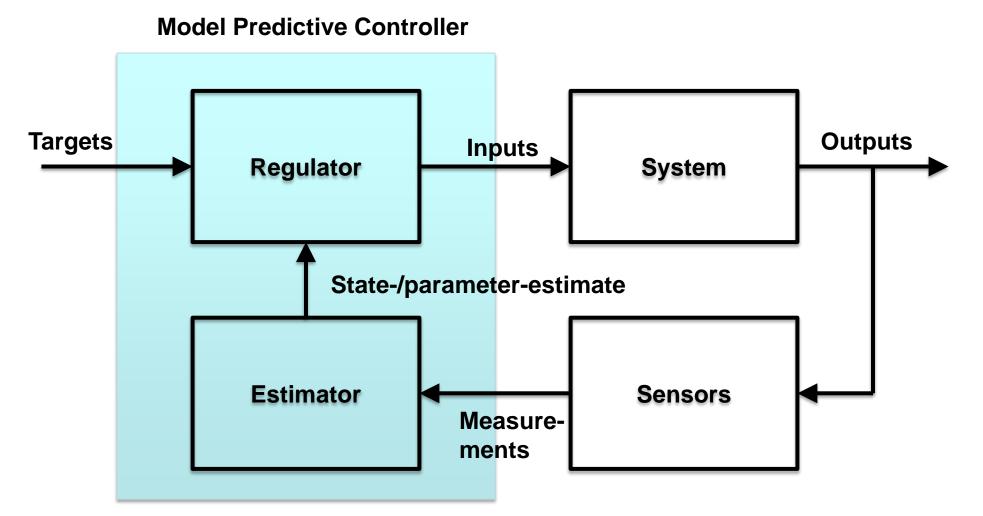


Systematic Model Building



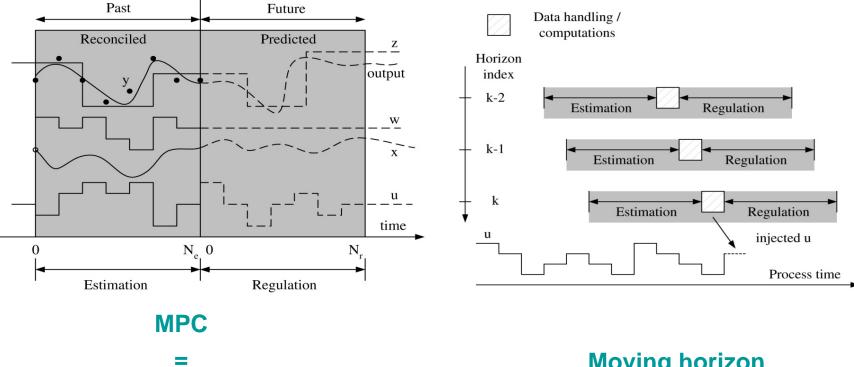


Model Predictive Controller





Model Predictive Control



Estimation + Regulation

Moving horizon implementation

Filtering and Prediction - EKF

$$dx(t) = f(x(t), u(t), \theta)dt + \sigma d\omega(t)$$

$$y(t_k) = g(x(t_k), \theta) + v(t_k)$$
Filtering

$$e_k = y_k - g(\hat{x}_{k|k-1}, \theta) \qquad C_k = \frac{\partial g}{\partial x}(\hat{x}_{k|k-1}, \theta)$$

$$\hat{x}_{k|k} = \hat{x}_{k|k-1} + K_k e_k$$

$$P_{k|k} = P_{k|k-1} - K_k R_{k|k-1} K'_k \qquad C_k = \frac{\partial g}{\partial x}(\hat{x}_{k|k-1}, \theta)$$

$$\frac{e_k = y_k - g(\hat{x}_{k|k-1}, \theta)}{k_{k|k}} \qquad C_k = \frac{\partial g}{\partial x}(\hat{x}_{k|k-1}, \theta)$$

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$$\frac{e_k = y_k - g(\hat{x}_{k|k-1}, \theta)}{k_{k|k-1}} \qquad C_k = \frac{\partial g}{\partial x}(\hat{x}_{k|k-1}, \theta)$$

$$\frac{e_k = g(\hat{x}_k(t), \theta)}{k_{k|k}} \qquad C_k = \frac{\partial g}{\partial x}(\hat{x}_k(t_{k+1}, \theta)}$$

$$\frac{e_k = g(\hat{x}_k(t), \theta)}{k_{k|k}} \qquad C_k = \frac{\partial g}{\partial x}(\hat{x}_k(t_{k+1}, \theta)}$$

$$\frac{e_k = g(\hat{x}_k(t), \theta)}{k_{k|k}} \qquad C_k = \frac{\partial g}{\partial x}(\hat{x}_k(t_{k+1}, \theta)}$$

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$$\frac{e_k = g(\hat{x}_k(t), \theta)}{k_k} \qquad C_k = \frac{\partial g}{\partial x}(\hat{x}_k(t_{k+1}, \theta)}$$



Optimal Control Problem

$$\min \quad \phi = \int_{t_k}^{t_k + T} g(x(t), u(t)) dt \\ s.t. \quad x(t_k) = \hat{x}_{k|k} \\ \dot{x}(t) = f(x(t), u(t)) \qquad t \in [t_k, t_k + T] \\ c(x(t), u(t)) \ge 0 \qquad t \in [t_k, t_k + T]$$

Integrator (Runge-Kutta Methods)

- DOPRI54 (non-stiff systems)
- ESDIRK12 / ESDIRK23 / ESDIRK34 (stiff systems)

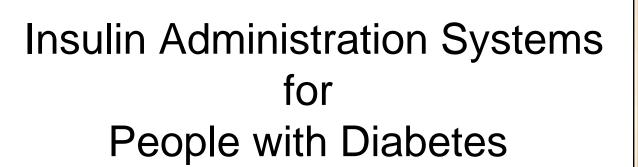
Sensitivities

• Forward, Adjoint

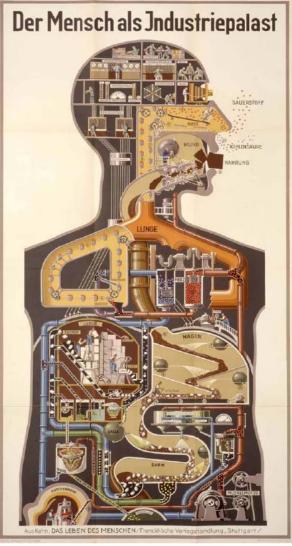
Optimization

- SQP
- Single-shooting
- Multiple-shooting

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The Artificial Pancreas

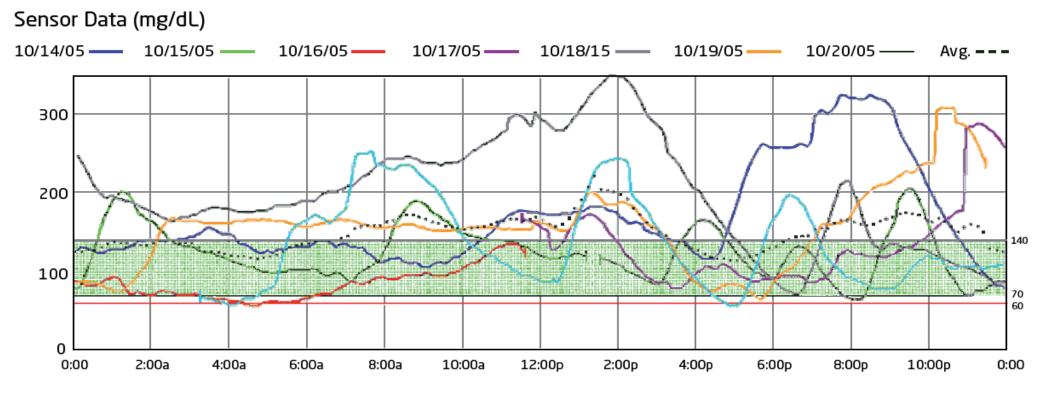


Blood glucose control



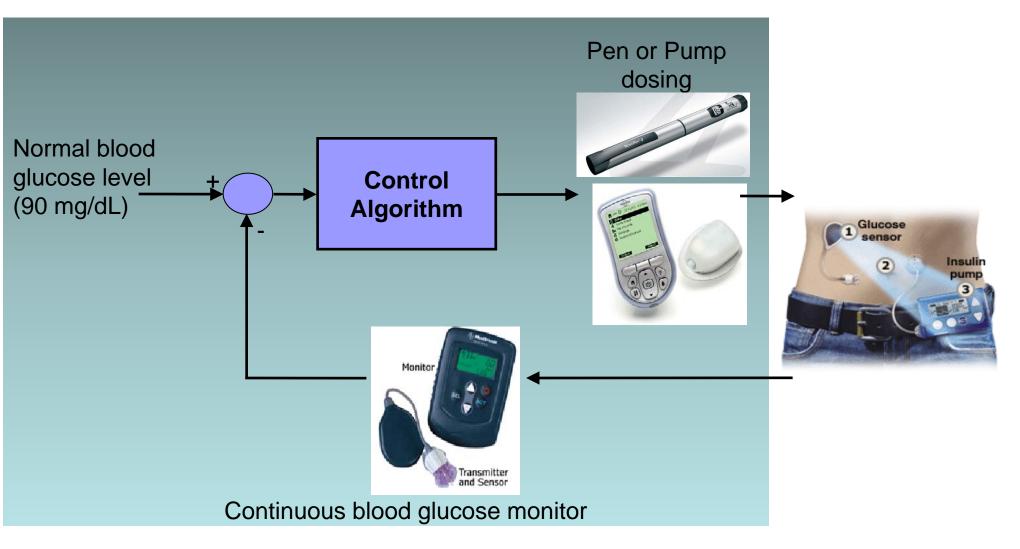
The blood glucose must stay within certain upper and lower bounds!

- Too low: coma (immediate effect)
- Too high: blindness and other long-term effects



Insulin Administration Systems

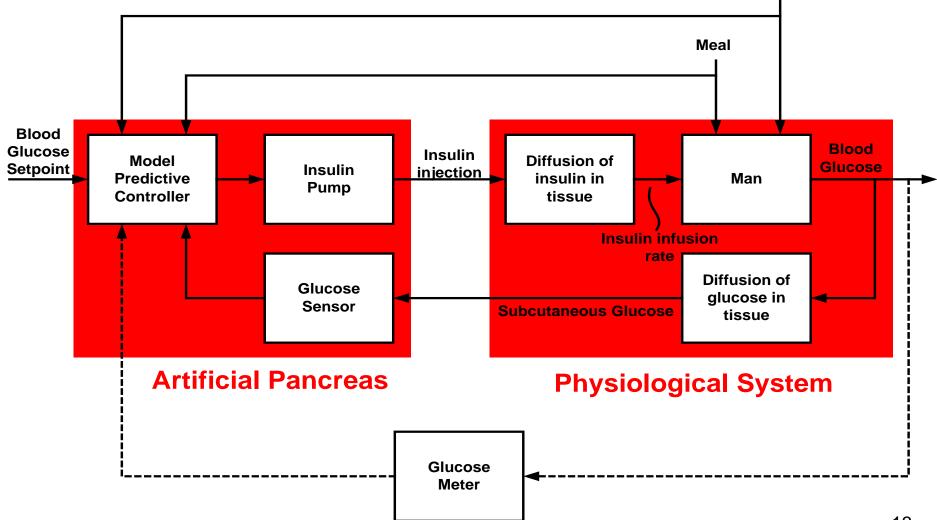


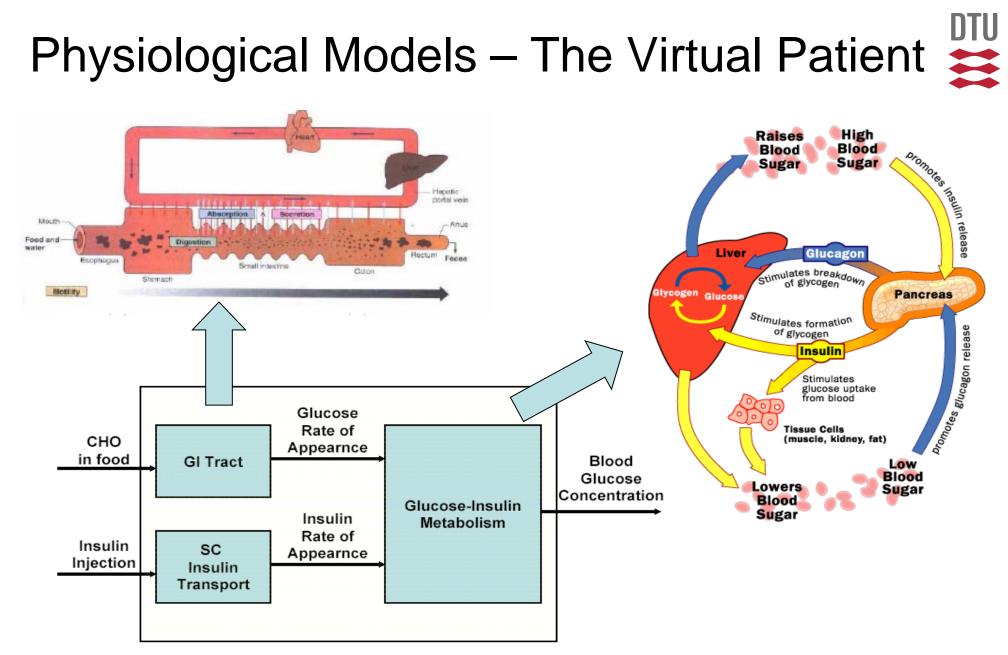




Physical activity / exercise

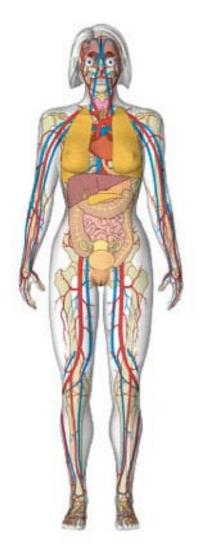
Systems Diagram

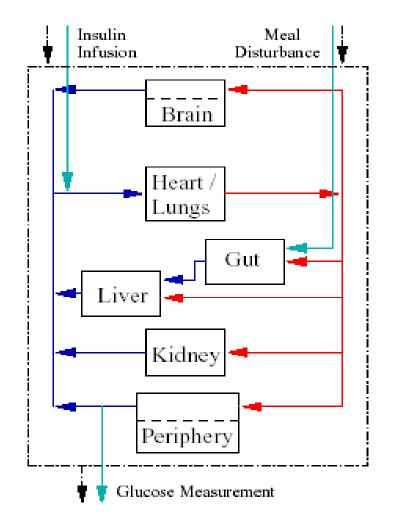




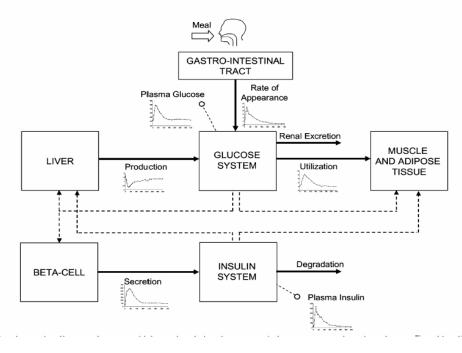
DTU

Physiological Models – A Compartment Model





The Cobelli Model – and the Virtual Clinic



- Developed by
 - University of Virginia
 - University of Padova
 - Juvenile Diabetes Research Foundation
- 30 virtual patients in the version that we have a license to
- The full version including 300 patients approved to substitute animal tests by FDA

user_interface							
Load Scenario							
Enter scenario ASCI file (.scn)							
- Common Scenario							
Simulation Parameters							
Open loop basal [U/hr] 0.8 End of commutation / start of regulation (min) 0							
start of closed loop [min] 0 length of simulation [min] 1440 clear scenario							
Single Meal							
enter amount of carbohydrates [g] 60 timing [min] 60 create Meal							
enter amount of insulin bolus [U] 4 duration [min] 15							
Note: Meal boluses will only be delivered during open loop control							
Multiple Meals breakfast (7am) lunch (noon) snack (4pm) dinner (6pm) snack (11pm)							
Carbs (g) 45 70 5 80 5 create 1 day							
bolus [U] 3 4.7 0 5.3 0 create 1 week							
Note: Meal boluses will only be delivered during open loop control							
Select Subject							
adulf#average							
Add all Remove all							
Children Children							
Adults All							
v							
Choose outcome measures							
Choose hardware define metabolic test Run Simulation							

Clinical Trials

- Gastric emptying trials (left)
- Clinical trials collecting data for modeling (right)







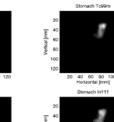
Original Tc99m

20 40 60 80 10 Horizontal (mm)

Original In111

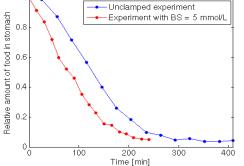
Horizontal (mm)





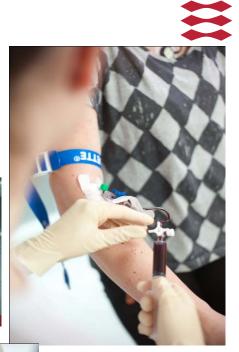








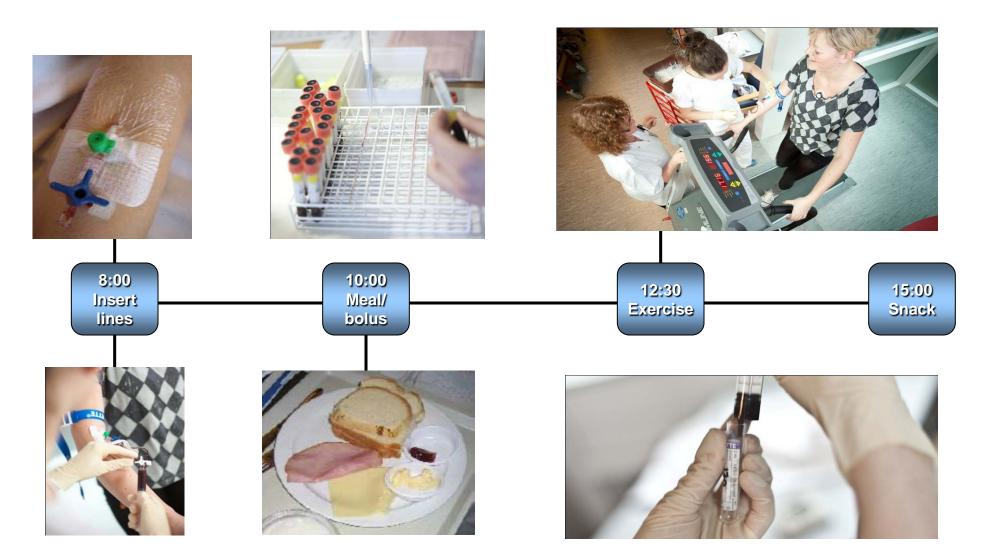




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Example of a Clinical Experiment

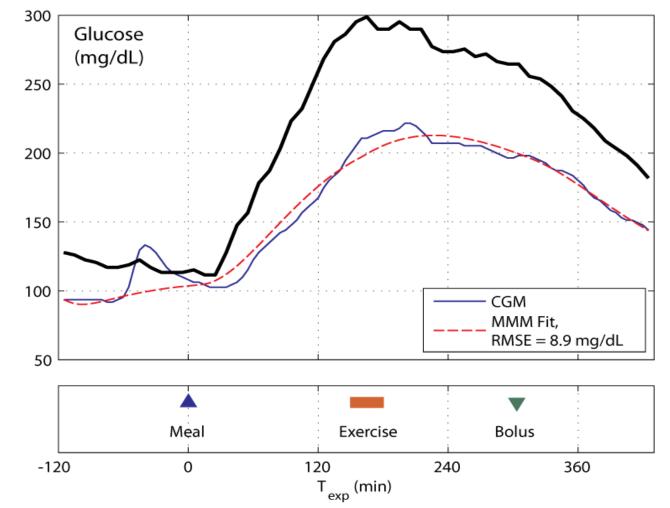


Identification Results

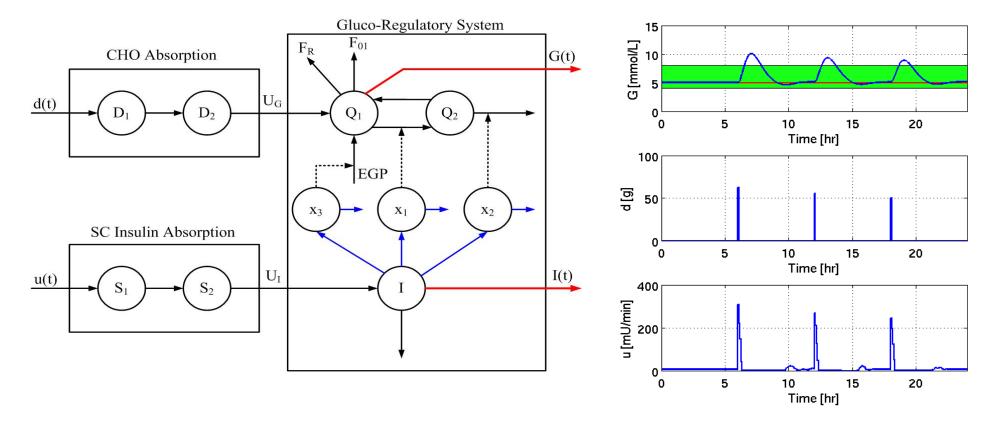
- Representative model fit
- Very accurate model fit

• Note:

Model is fit to the CGM signal. The intravenous glucose concentration is also shown (thick line) for comparison



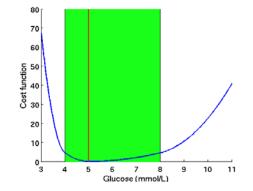
The DTU Type 1 Diabetes Model **#**



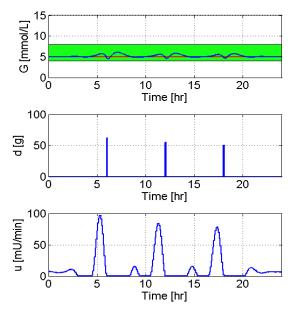
$$d\boldsymbol{x}(t) = f(\boldsymbol{x}(t), \boldsymbol{u}(t), \boldsymbol{d}(t))dt + \sigma d\boldsymbol{\omega}(t)$$
$$\boldsymbol{y}(t_k) = g(\boldsymbol{x}(t_k)) + \boldsymbol{v}(t_k)$$

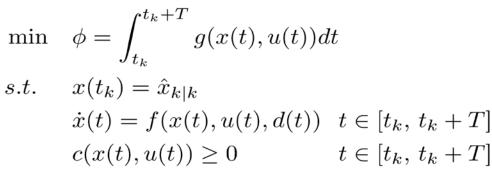
20

Insulin Administration Strategies

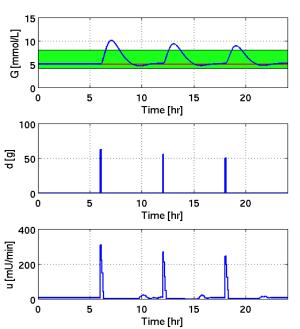


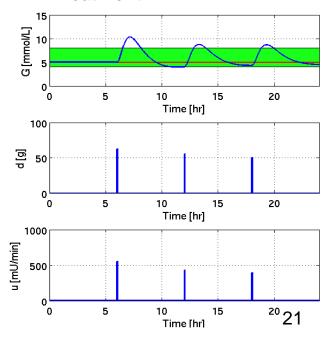
NMPC Pre-meal Insulin Allowed





NMPC No Pre-meal Insulin



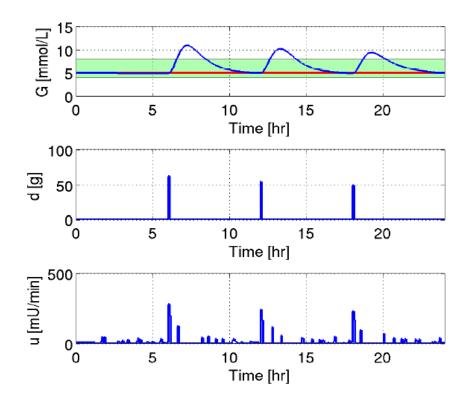
MDI (Pen Based) Insulin Treatment 

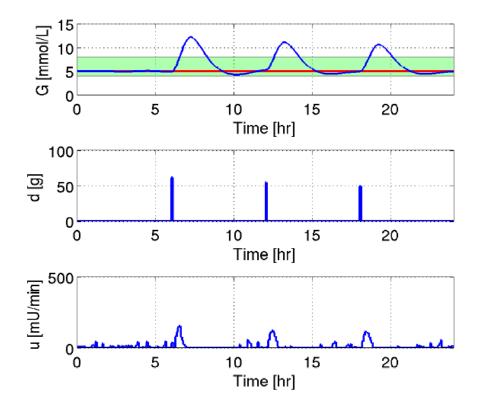


Closed-Loop Studies by NMPC

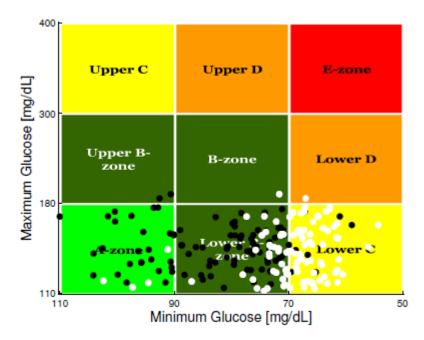
Meals announced at meal-time

Meals not announced

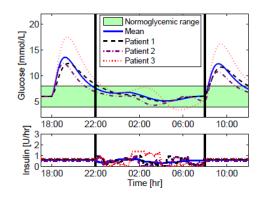


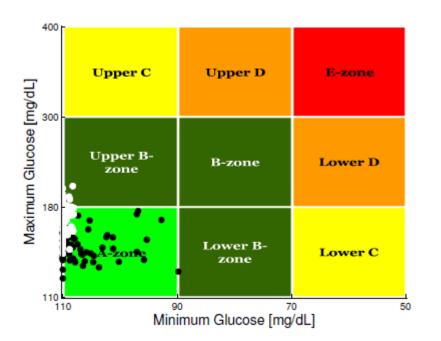


Overnight Stabilization – A Cohort

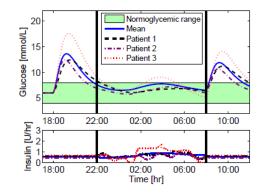


(a) Insulin sensitivity increases by 30%





(b) Insulin sensitivity decreases by 30%





Clinical Closed Loop Studies



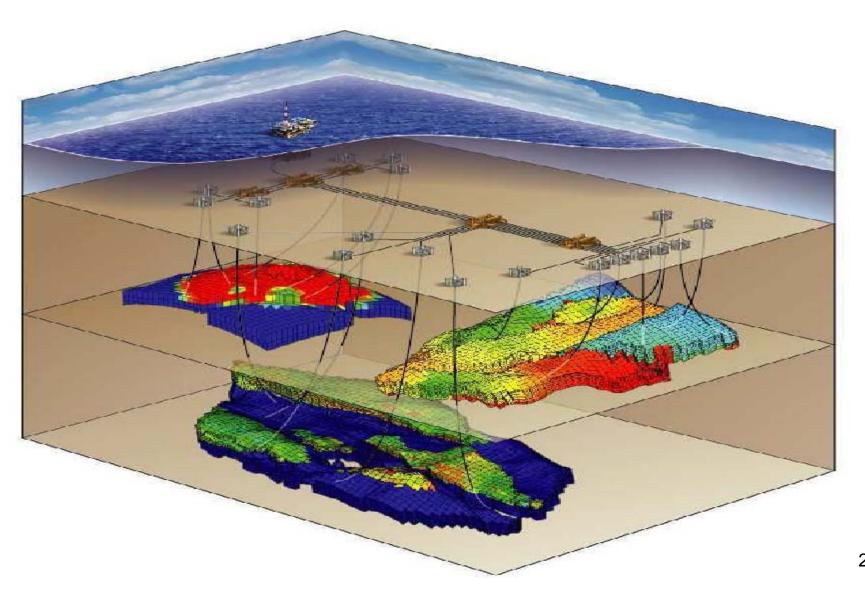
nt	History Chart	Syster				
4:39-1	0 06:20	10,601	0,400	0,400	04:30:16	CGM Value
4:44:1	0 06:25	10,712	0,400	0,400	04:44:16	CONT VIDEN
4:49:1	0 06:30	10,712	0,375	0,375	04-50:01	F 40
4:54:1	0 06:35	10,268	0,375	0,375	04:54:16	5,43
4:59:1	0 06:40	10,323	0,375	0,375	04:59:16	01.0
6.14:1	0 06:45	10,489	0,350	0,350	05:04:19	
5:09:1		10,656	0,350	0,350	05:09:16	Comment table
6:14:1	0 06:55	10,601	0,350	0,350	05:14:16	SALEN IN CONTR.
6.19-1	0 07:00	10,545	0,350	0,350	05:19:36	
6.14:1	0 07:05	10,434	0,350	0,350	05:24:16	
6.29-1		9,657	0,350	0,350	05:29:16	
6.341	0 07:15	0,000	0,350	0,350	05:34:19	
6:39:1	0 07:20	7,604	0,350	0,350	05:39:16	
6:44:1	0 07:25	7,381	0,350	0,350	05:44:16	
6:49:1	0 07:30	7,770	0,250	0,250	05:49:32	
5:54:1	0 07:35	B,270	0,250	0,250	05:54:16	
6:59:1	0 07:40	8,436	0,250	0,250	05:50:16	
6:04:1	0 07:45	8,103	0,200	0,200	06:04:19	
6.09-1	0 07:50	B,603	0,200	0,200	06:00:16	
6141	0 07.55	7,825	0,200	0,200	06:14:16	
6193	0 05:00	7,881	0,200	0,200	06:19:54	13-
6243	0 06/05	7,100	0,200	0,200	00:24:16	12-
6 29 1	0 08.10	6,216	0,200	0,200	06:29:16	2.23
6.341	0 08.15	5,495	0,150	0,150	05/34/23	10-
6.39.1	0 06:20	0,000	0,150	0,150	06:39:16	5
644.1	0 08:25	5,328	0,150	0,150	99/44/16	§ a-
6491	0 08:30	5,439	0,100	0,100	06:49:18	
6.54.1	0 08:35					8 4. W
0.59.0	0 06:40					Th.
7/04:1	0 06(45					and a free of the second
7,09.1	0 08:50					3 4-
7141	0 08:55				1	
7.19.1	00.60 0	1		1		2-
0.24(1	0 09:05					
m 29 (1	0 09.10					0.41111111
0.343	0 0915					00:00
0.39 1	0 09.20					
0,440	0 09.25					11 (V-5
0491	0 09.30				-	*:





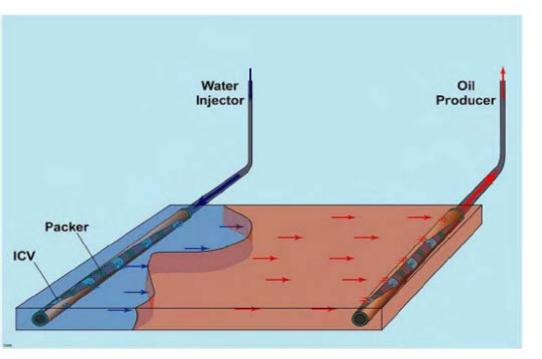
MODEL PREDICTIVE CONTROL FOR MANAGEMENT OF OIL RESERVOIRS

An Offshore Oil Reservoir



DTU

Mathematical Model



$$\frac{d}{dt}g(x(t)) = f(x(t), u(t))$$

The mass conservation of water and oil

$$\frac{\partial}{\partial t} C_w(P_w, S_w) = -\nabla \cdot \mathbf{F}_w(P_w, S_w) + Q_w$$
$$\frac{\partial}{\partial t} C_o(P_o, S_o) = -\nabla \cdot \mathbf{F}_o(P_o, S_o) + Q_o$$

The mass concentrations

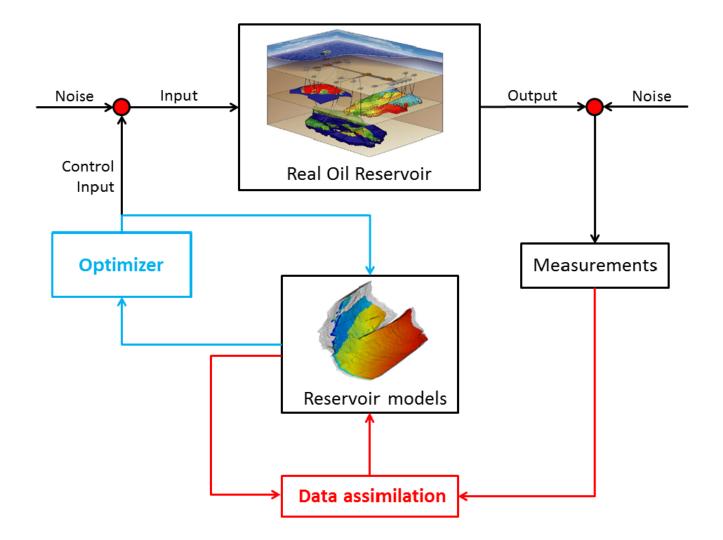
$$C_w = \phi \rho_w(P_w) S_w$$
$$C_o = \phi \rho_o(P_o) S_o$$

Fluxes through the porous medium

$$\mathbf{F}_w = \rho_w(P_w)\mathbf{u}_w(P_w, S_w)$$
$$\mathbf{F}_o = \rho_o(P_o)\mathbf{u}_o(P_o, S_o)$$



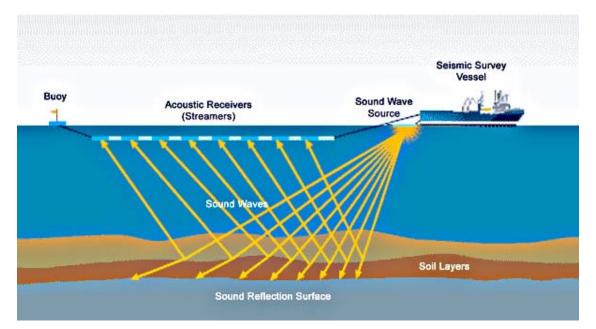
Closed-Loop Reservoir Management

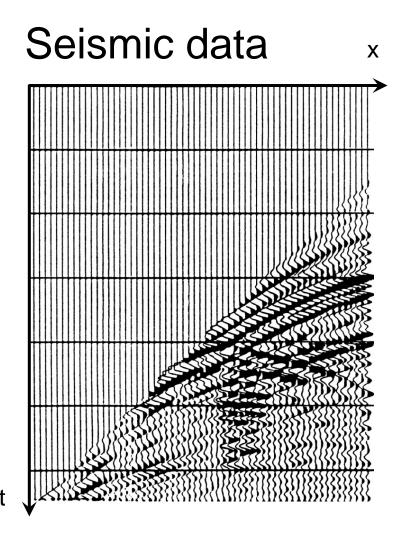


Applied Seismology: Subsurface Imaging



Experimental setup



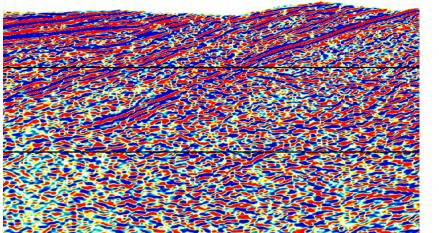


The Computational Challenge: Integrated Inversion of Seismic and Production Data

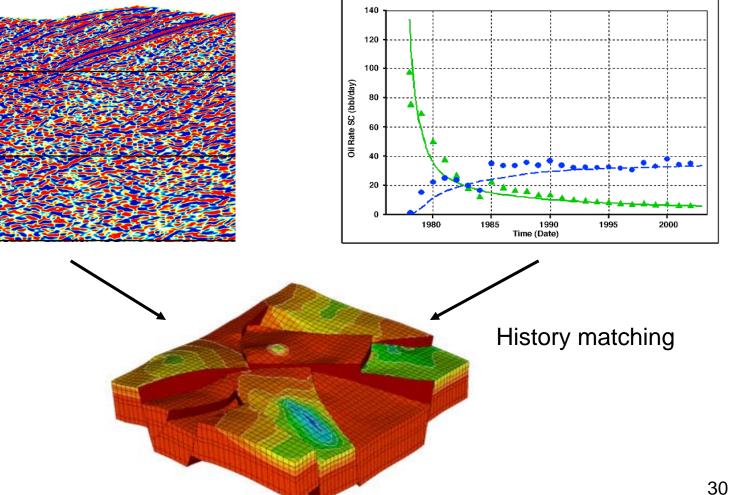
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Seismic data

Seismic inversion



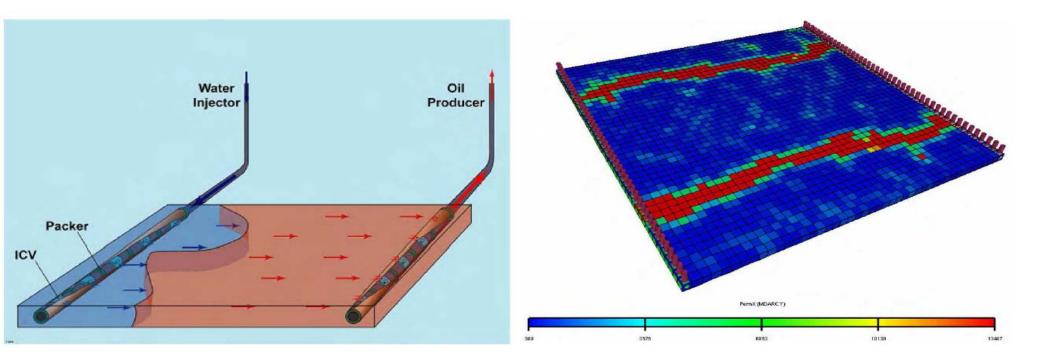
Oil production data





History Matching (State and Parameter Est) + Seismic Data

=> Permeability Field





Optimization Problem

$$\min_{\substack{[x(t),u(t)]_{t_0}^{t_f}}} \int_{t_0}^{t_f} J(x(t),u(t))dt$$
s.t.
$$\frac{d}{dt}g(x(t)) = f(x(t),u(t))$$

$$x(t_0) = x_0$$

$$u_{min} \le u(t) \le u_{max}$$

$$- u_{min}^{\Delta} \le \frac{d}{dt}u(t) \le u_{max}$$

- Single-Shooting and SQP
- ESDIRK methods tailored for this problem
- Gradients computed by the adjoint method

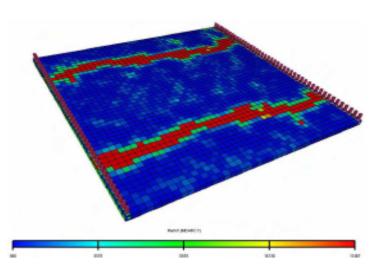


Objective Function is the Net Present Value

$$NPV = \sum_{k=0}^{N-1} \left[\frac{h_k}{(1-d)^{t_k/\tau}} \left(\sum_{j=1}^{N_{pro}} \left[r_{op} Q_{k,j}^{op} - r_{wp} Q_{k,j}^{wp} \right] - \sum_{j=1}^{N_{inj}} r_{wi} Q_{k,j}^{wi} \right) \right]$$

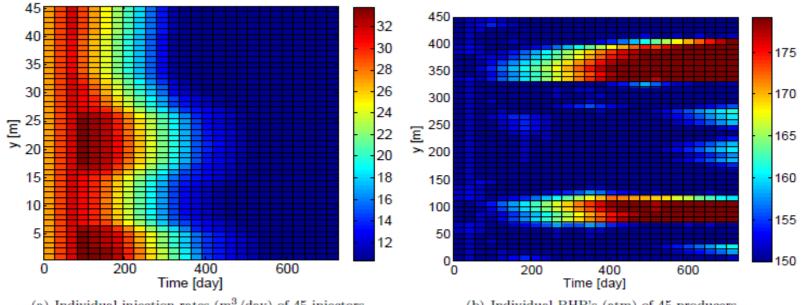
Adjust the injectors and producers by taking the oil price, the water injection cost and the water separation cost into account.

- Rate constrained injector on the left.
- BHP constrained producer to the right.
- 2×45 individually controllable sections.
- Max. 2 PV's injected over two years.
- Injection rates and BHP's are updated once a month.





Optimal Oil Field Development - MVs

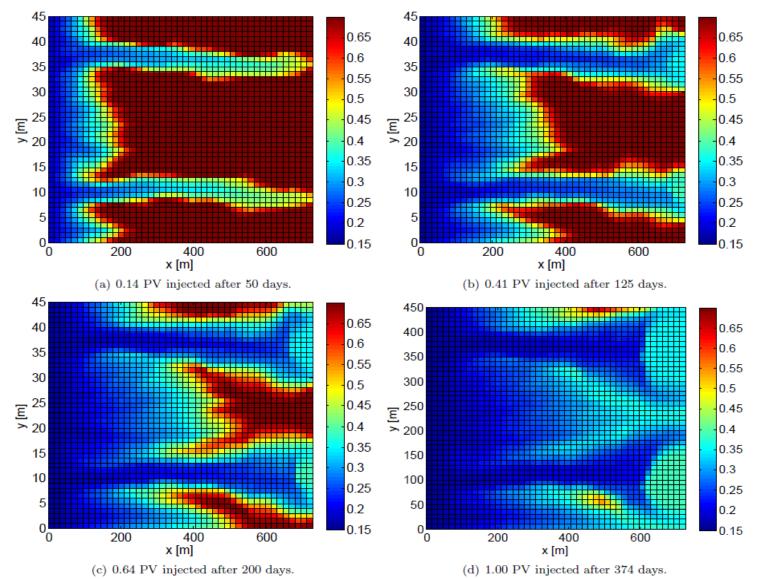


(a) Individual injection rates (m³/day) of 45 injectors.

(b) Individual BHP's (atm) of 45 producers.



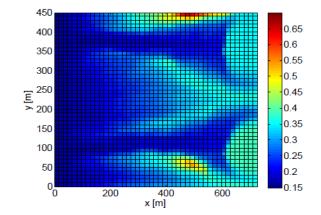
Optimal Oil Field Development - CVs



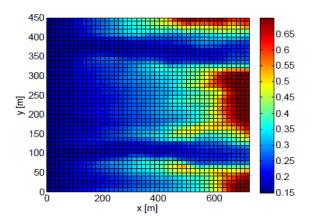


Oil Field Development Using NMPC

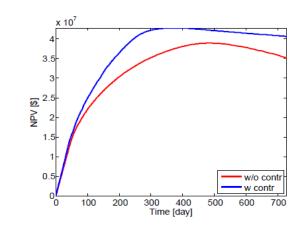
With control strategy, 374 days:



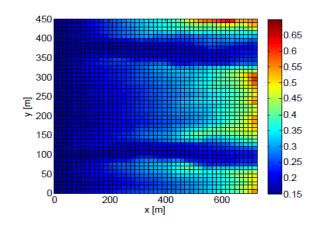
No control strategy, 374 days:



Net present value over 2 years:



No control strategy, 484 days:

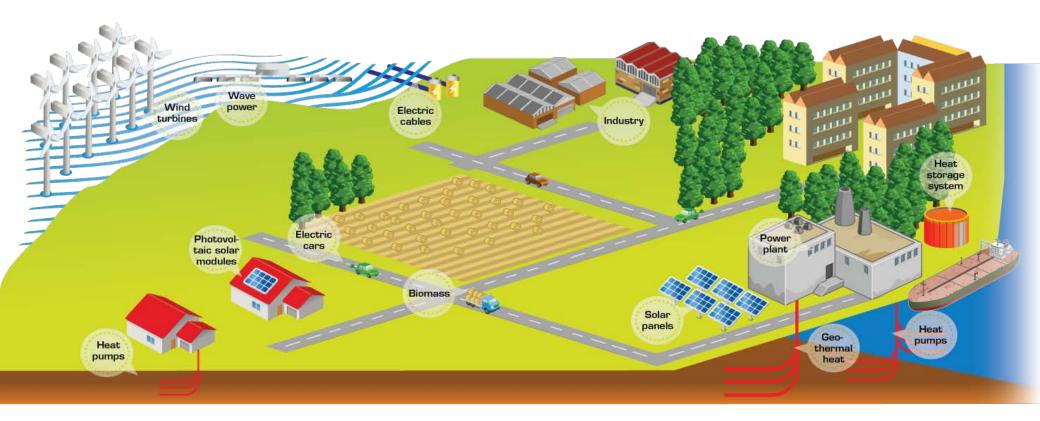




MODEL PREDICTIVE CONTROL OF SMART ENERGY SYSTEMS

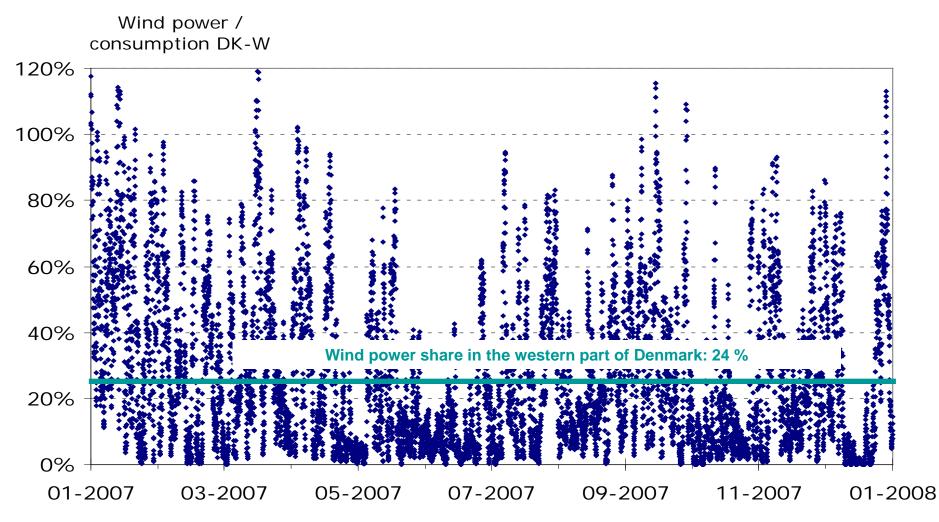


Smart Energy Systems



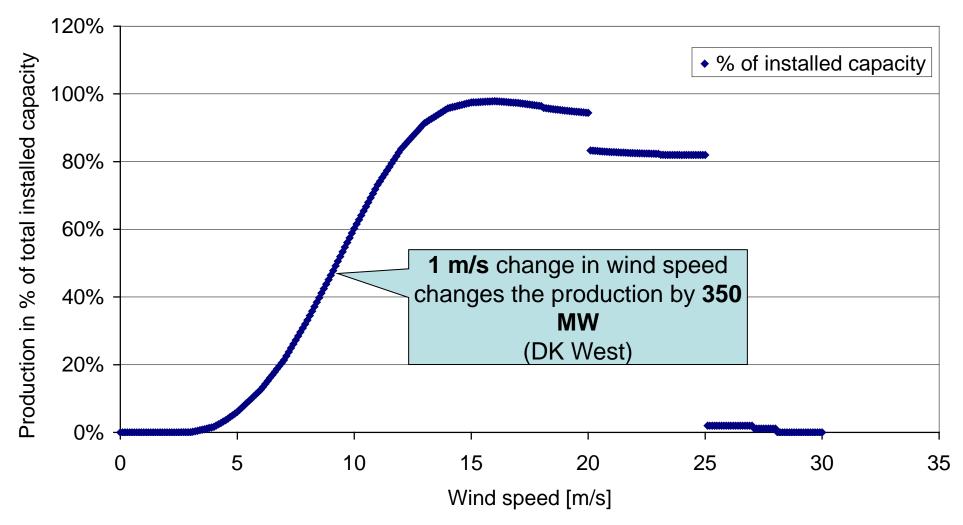


Wind Power

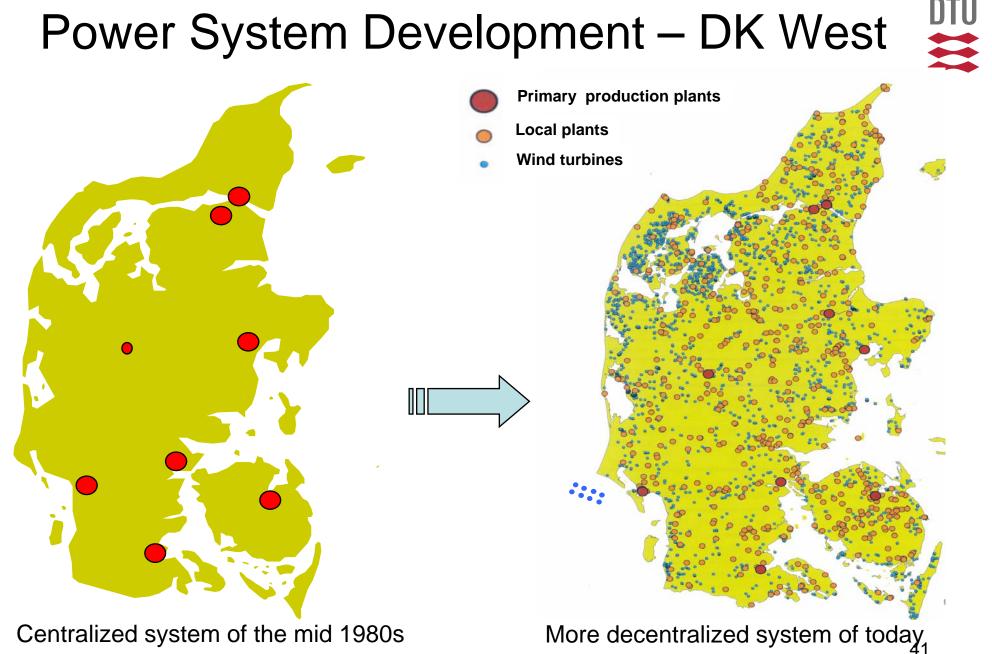




Wind Power Production and Imbalances

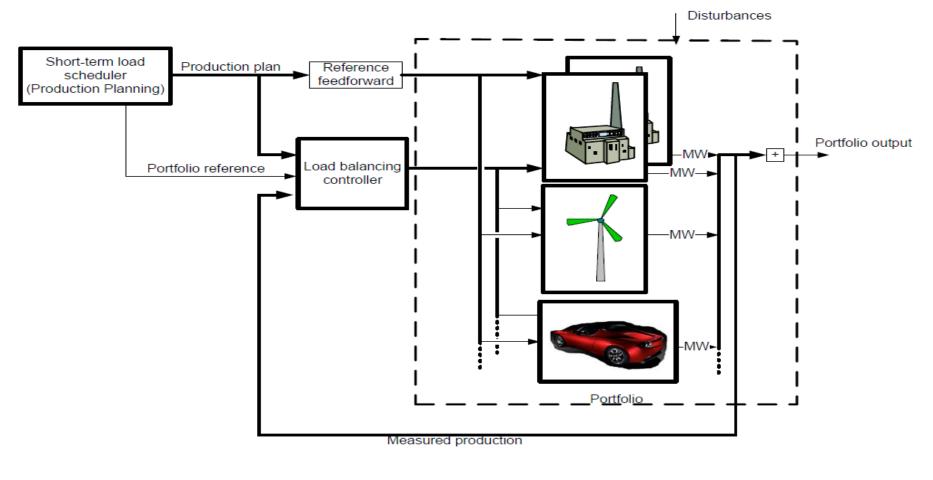


Power System Development – DK West





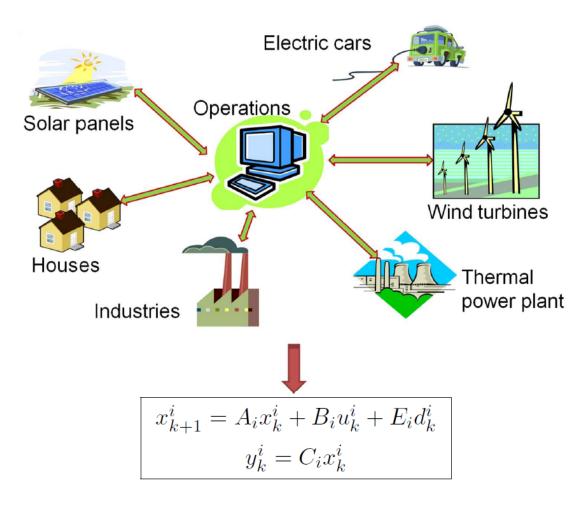
Load Balancing Controller







Models of Energy Components



Controllable Power Generators

Each controllable power generator has an allowable operating range

 $u_{\min} \le u_k \le u_{\max}$

and limits on how fast you can change the desired production

 $\Delta u_{\min} \le \Delta u_k \le \Delta u_{\max}$

The unit production cost for power plant #i is: c_i . Therefore, the total production cost over a given period is

$$\phi = \sum_{k=0}^{N-1} \sum_{i=1}^{n_u} c_i(u_k)_i = \sum_{k=0}^{N-1} c'u_k$$

MPC for Economic Power Portfolio Optimization

The portfolio power generation problem can be stated as

$$\min_{\{u_k\}_{k=0}^{N-1}} \phi = \sum_{k=0}^{N-1} c' u_k s.t. \qquad x_{k+1} = A x_k + B u_k + E d_k \quad k = 0, 1, \dots, N-1 y_k = C x_k \qquad k = 1, 2, \dots, N \\ u_{\min} \le u_k \le u_{\max} \qquad k = 0, 1, \dots, N-1 \\ \Delta u_{\min} \le \Delta u_k \le \Delta u_{\max} \qquad k = 0, 1, \dots, N-1 \\ y_k \ge r_k \qquad k = 1, 2, \dots, N$$

The parameters for this problem are

- Initial state, x_0 , and previous decision, u_{-1}
- Predicted loads on non-controllable generators (e.g. wind speed on wind turbines): $\{d_k\}_{k=0}^{N-1}$
- Predicted power demand: $\{r_k\}_{k=1}^N$

DTU

Soft Economic MPC

It may not always be possible to meet the power demand. Therefore, we relax the MPC problem

$$\min_{\{u_k, v_{k+1}\}_{k=0}^{N-1}} \phi = \sum_{k=1}^{N} \rho v_k + \sum_{k=0}^{N-1} c'_k u_k$$
s.t.
$$x_{k+1} = Ax_k + Bu_k + Ed_k \quad k = 0, 1, \dots, N-1$$

$$y_k = Cx_k \quad k = 1, 2, \dots, N$$

$$u_{\min} \le u_k \le u_{\max} \quad k = 0, 1, \dots, N-1$$

$$\Delta u_{\min} \le \Delta u_k \le \Delta u_{\max} \quad k = 0, 1, \dots, N-1$$

$$y_k \ge r_k - v_k \quad k = 1, 2, \dots, N$$

$$v_k \ge 0 \quad k = 1, 2, \dots, N$$

by introduction of the slack variables, v_k . ρ is selected sufficiently large, such that the power demand is met whenever possible.

Simple Test Example

Power Generator #1: Slow and Cheap

$$Y_{1}(s) = \frac{1}{(\tau_{1}s+1)^{3}} U_{1}(s) \qquad \tau_{1} = 20 \qquad c_{1} = 1$$
$$0 \le u_{k} \le 10$$
$$-1 \le \Delta u_{k} \le 1$$

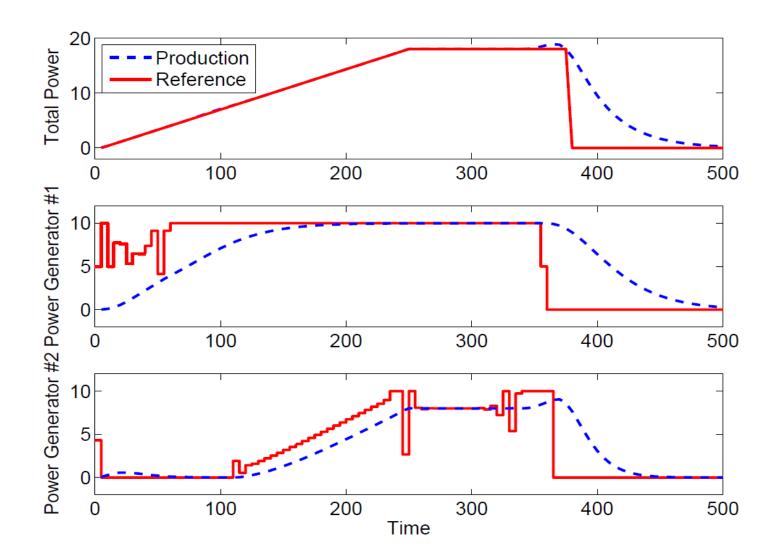
Power Generator #2: Fast and Expensive

$$Y_{2}(s) = \frac{1}{(\tau_{2}s+1)^{3}} U_{2}(s) \qquad \tau_{2} = 10 \qquad c_{2} = 2$$
$$0 \le u_{k} \le 10$$
$$-3 \le \Delta u_{k} \le 3$$

Total production: $Y(s) = Y_1(s) + Y_2(s)$ Penalty for producing less than sold: $\rho = 1.0 \cdot 10^5$

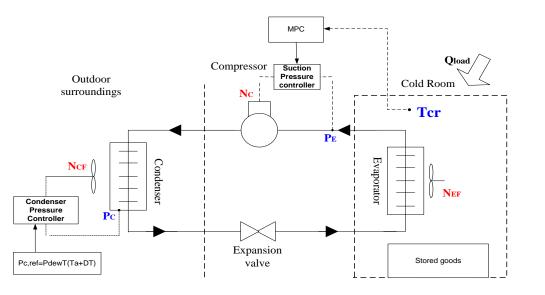
Optimal Production Profiles







Cooling Houses – A Flexible Consumer



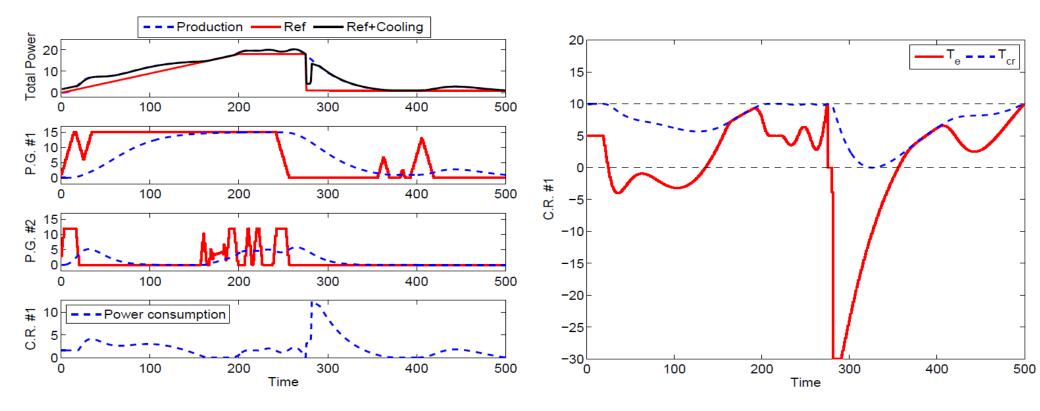
Cooling system used in refrigerators and cooling houses



- <u>Motivation:</u>
- Refrigeration and air-conditioning consume substantial amounts of energy.
- E.g. up to 80% of energy consumed by supermarkets goes to refrigeration.
- <u>Methods:</u>
- Economic MPC: Minimize the cost of cooling subject to temperature limits
- Predictions of weather, energy prices and load profiles.
- Implementation on industrial hardware.



Power Management 2 Power Plants and 1 Cooling House

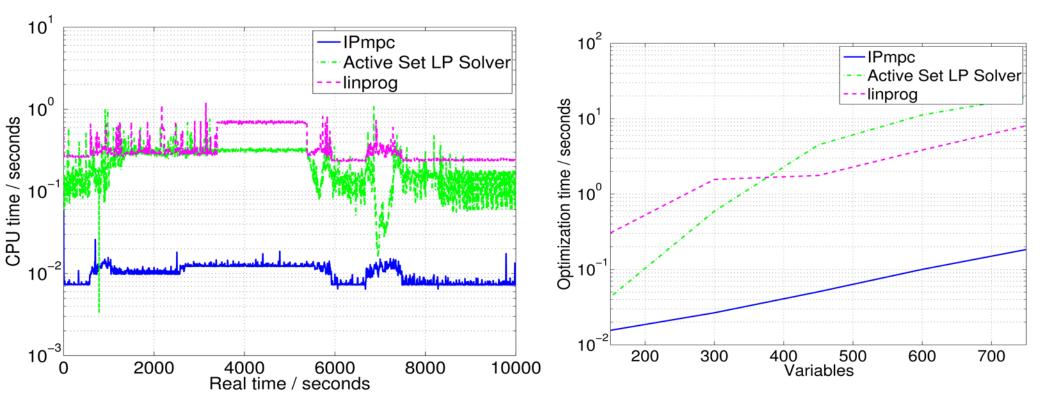


- Economic Optimizing MPC
- Minimize power consumption and costs without lowering the cooling quality
- Load shifting utilizing the thermal capacity of the cooling house

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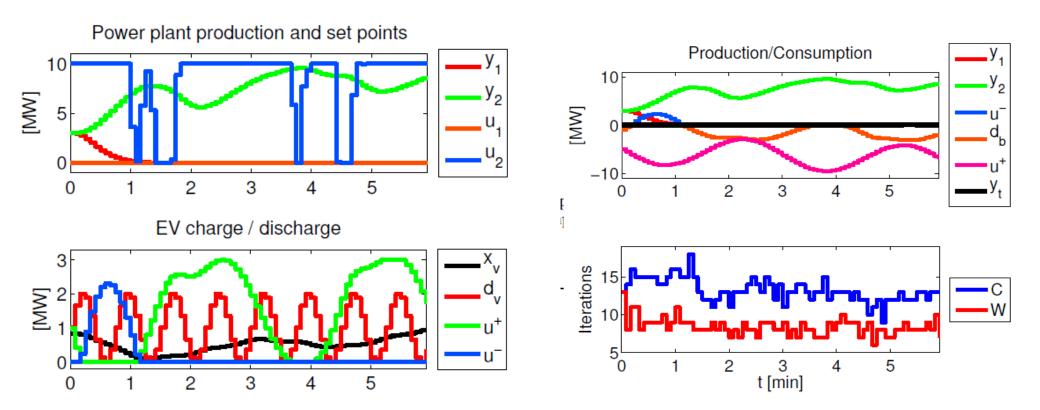


Online Computing Time Tailored Primal-Dual Interior Point Algorithm



Warm Start Interior Point Methods





Accelerating LP Algorithms with GPUs

- Interior Point Methods are used for solving $min \phi = g'x$ mathematical optimization problems eg: s.t. Ax = b
- Basic direct algorithm:
 - While not converged
 - Form Hessian matrix: H = A' D A
 - Factorize Hessian: *L* = *chol*(*H*)
 - Compute affine step
 - Compute corrector step
 - Take step
 - Compute residuals
- The main workload is the formation of the Hessian followed by the factorization.
- GPUs are very good at matrix-multiplication.

s.t. Ax = b $x \ge 0$



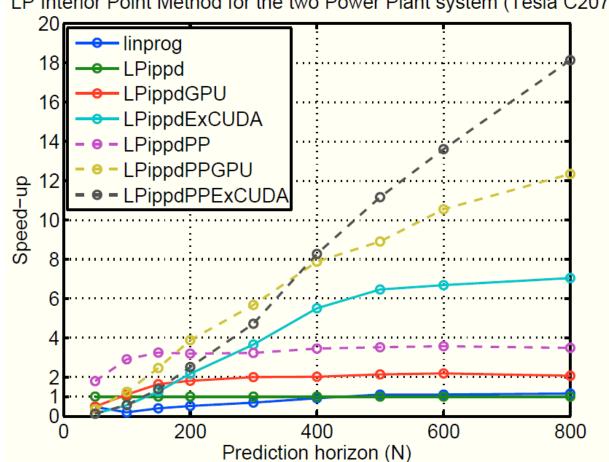
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Implementation Details

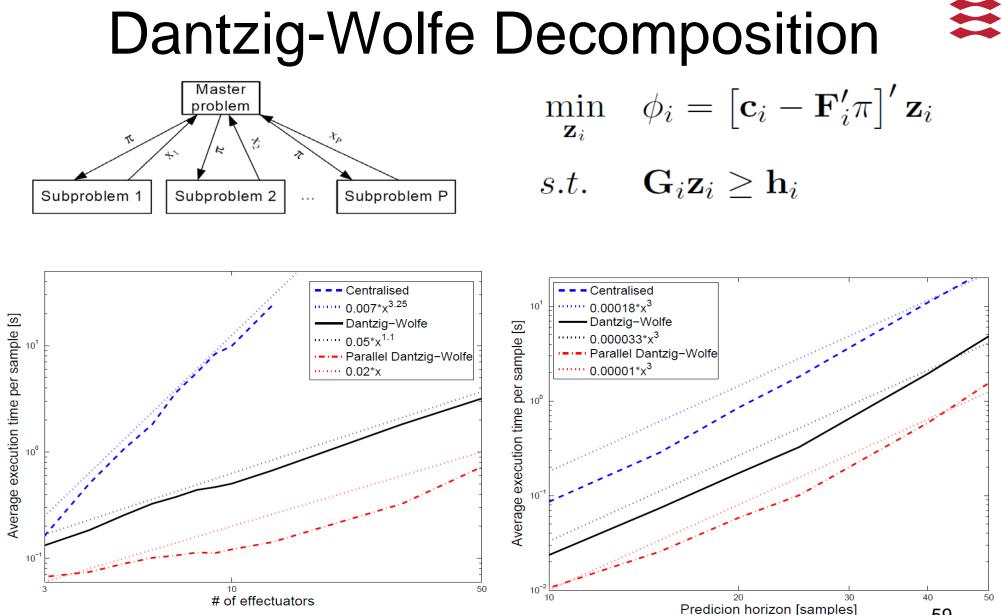
- MATLAB CPU implementation as reference: LPippd
- MATLAB GPU implementation (MATLAB R2011b): LPippdGPU
- C + CUDA implementation: LPippdExCUDA
 - Uses available libraries for standard operations.
 - CUBLAS used for matrix operations.
 - MAGMA used for Cholesky factorization.
 - CUDA kernels implemented for additional operations such as computing step lengths.



Speed-Up with GPU



LP Interior Point Method for the two Power Plant system (Tesla C2070)



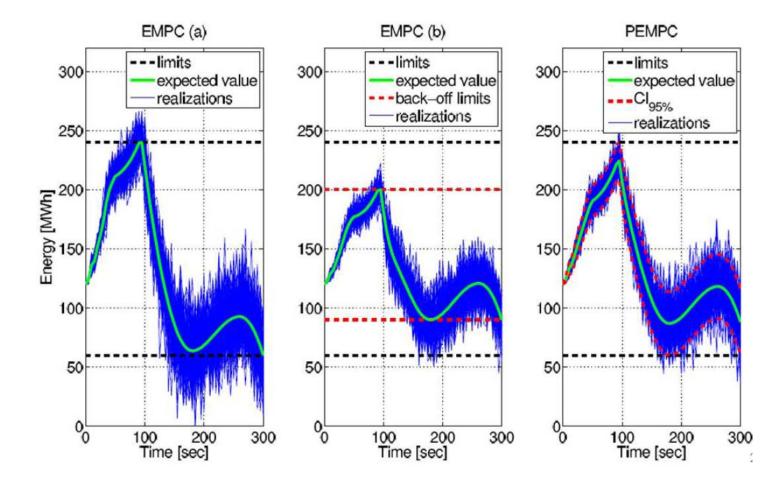
Uncertainty

Smart energy systems are subject to uncertainty:

- Demand / Price / Weather
- Uncertainty on g and $b \implies \mathsf{LP}$ $\min_{x} \mathbf{g}^{T} x$ $s.t \ Ax \ge \mathbf{b} \qquad j = 1, ..., m$ $x \in \Re^{n}$
- Uncertainty on g, A and b with Gaussian distribution \implies SOCP $\min_{x} \mathbf{g}^{T} x$ $\min_{x} g^{T} x$
- $s.t \quad \mathbf{A}_{[j,:]} x \ge \mathbf{b}_j \qquad j = 1, ..., m \implies s.t \quad Ax \ge b \qquad j = 1, ..., m \\ x \in \Re^n \qquad \qquad x \succeq_{K^n} 0$



Uncertainty Scenarios



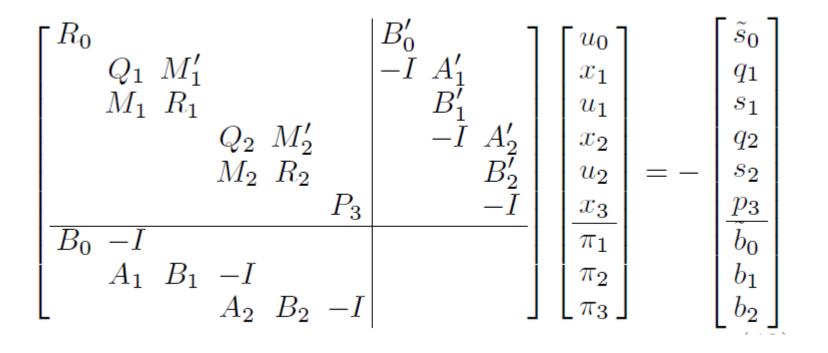


The Extended LQ Problem

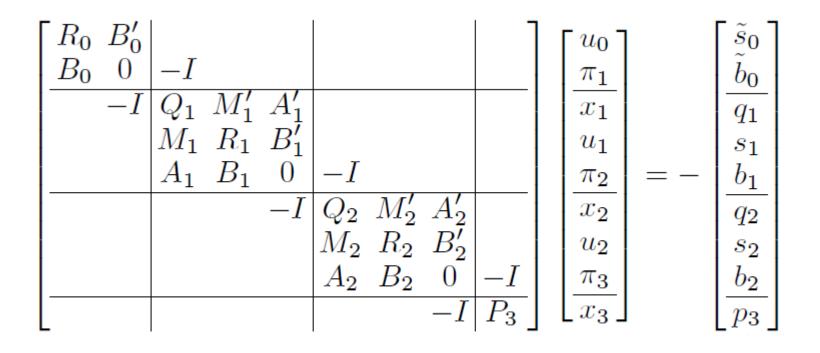
$$\min_{\substack{\{u_k, x_{k+1}\}_{k=0}^{N-1}}} \phi = \sum_{k=0}^{N-1} l_k(x_k, u_k) + l_N(x_N)$$

s.t. $x_{k+1} = A_k x_k + B_k u_k + b_k \quad k \in \mathcal{N}$
with $\mathcal{N} = \{0, 1, \dots, N-1\}$ and stage costs defined by
 $l_k(x_k, u_k) = \frac{1}{2} \begin{bmatrix} x_k \\ u_k \end{bmatrix}' \begin{bmatrix} Q_k & M'_k \\ M_k & R_k \end{bmatrix} \begin{bmatrix} x_k \\ u_k \end{bmatrix} + \begin{bmatrix} q_k \\ s_k \end{bmatrix}' \begin{bmatrix} x_k \\ u_k \end{bmatrix} + \rho_k$
 $l_N(x_N) = \frac{1}{2} x'_N P_N x_N + p'_N x_N + \gamma_N$

KKT System for the Extended LQ Problem

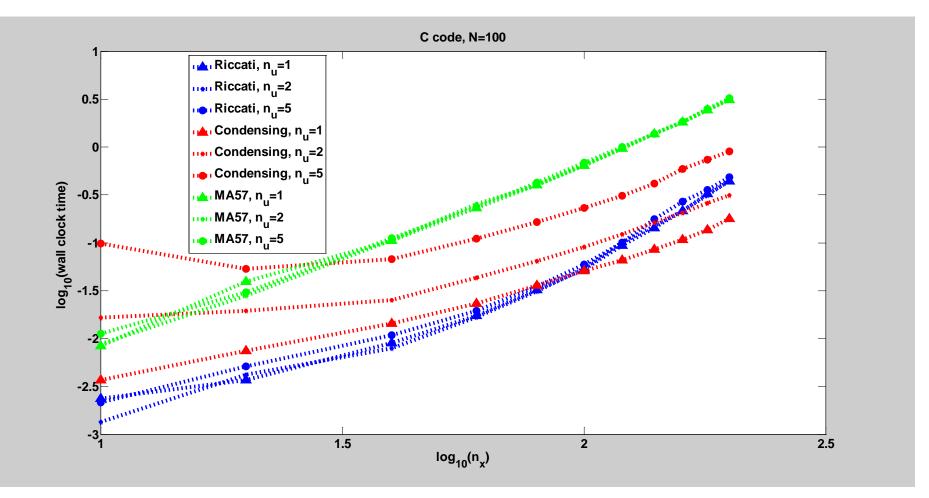


KKT System for the Extended LQ Problem



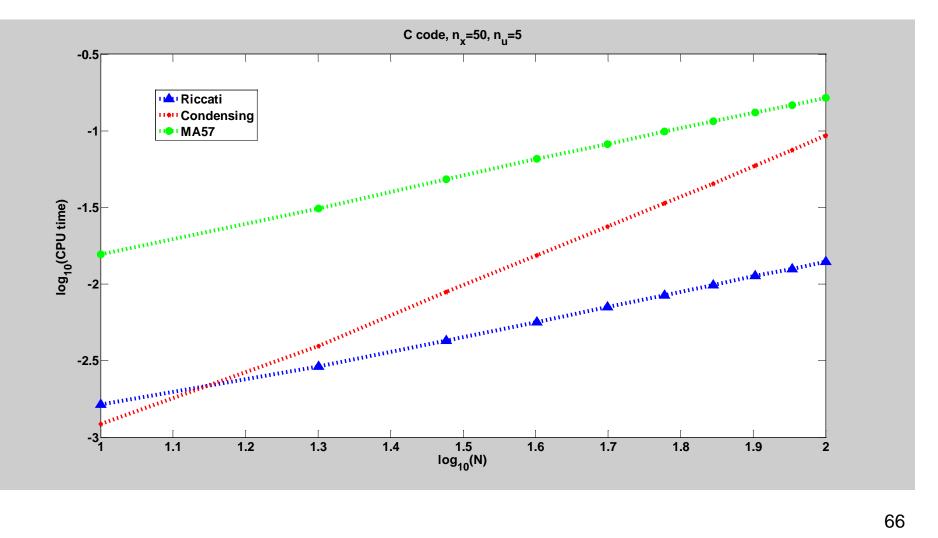


Numerical Results





Numerical Results



Summary



- There is a need for HPC software supporting MPC
 - QP, LP, SOCP algorithms
 - ODE/PDE solvers equipped with sensitivity computing abilities (adjoints)
 - SQP / NLP algorithms
 - Efficient direct sparse and iterative methods for KKT systems (even when they are ill-conditioned)
- The number of potential applications is very large



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