#### Technical University of Denmark



### Available fluid codes for turbulence study

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# Available fluid codes for turbulence study

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## Periodic codes (spectral)

- Probably the simplest codes to make
- Easy and fast to develop, a master study
- Easy, fast and compact to run, a bachelor study
- Can use fairly high number of modes on a single CPU: 2048x2048
- Can reach fairly high Reynolds numbers:  $Re(2D) = UL/\mu < 20.000$
- Can fairly easy be parallelized using MPI: linear speedup using 100 CPUs on a 2048x2048 grid
- Note that the domain is infinite with a periodic restriction!



# Periodic codes (spectral)

• Solutions are expanded into Fourier modes (global)

$$\begin{pmatrix} \omega(x, y, t) \\ \psi(x, y, t) \end{pmatrix} = \sum_{m} \sum_{n} \begin{pmatrix} \omega_{mn}(t) \\ \psi_{mn}(t) \end{pmatrix} \exp\left(\frac{2\pi i m x}{L_x}\right) \exp\left(\frac{2\pi i n y}{L_y}\right)$$

• Vorticity equation

$$\frac{\partial \omega}{\partial t} + J(\psi, \omega) = v \nabla^2 \omega \implies \forall (mn) : \frac{\partial \omega_{mn}}{\partial t} + [\psi, \omega]_{mn} = v \nabla^2 \omega_{mn}$$
$$[\psi, \omega]_{mn} = FT \left\{ \frac{\partial \psi}{\partial x} \frac{\partial \omega}{\partial y} - \frac{\partial \psi}{\partial y} \frac{\partial \omega}{\partial x} \right\}_{mn}$$

- Fast Fourier Transformation will take 75 % of computational time
- De-aliasing scheme, zero pad the largest 1/3 of the modes
- The Poisson equation is trivial:  $k^2 \psi_k = \omega_k$



## The Risøs Euler code

Time = 0.0



Time = 95.0



Kuznetsov et al POP 19, 105110 2007

Inverse cascade :





- •1024x1024 points
- •512x512 modes
- •de-aliased removes upper 1/3
- $K_{max} = 340$
- •Taken account for viscosity leave us with approximately 2 decades!

## **Solid boundaries**



Finite difference in x, Fourier expansion in yMultiplication simple, derivatives complex

$$\frac{\partial f_{i}}{\partial x} \Box \frac{f_{i+1}\Delta f_{i-1}}{2dx}$$
$$\frac{\partial^{2} f}{\partial x^{2}} \Box \frac{f_{i+1} - 2f_{i} + f_{i-1}}{(\Delta x)^{2}}$$

Periodic

Banded matrix, solved by Gauss elimination

Poisson equation  

$$\nabla^{2}\phi = \omega \Rightarrow$$

$$\forall k : \frac{\partial^{2}\phi_{k}}{\partial x^{2}} - k^{2}\phi_{k} = \omega_{k} \Rightarrow \qquad \underbrace{A_{k}}_{=} = \frac{1}{\Delta x^{2}} \begin{pmatrix} -1 & 1 & & & & \\ 1 & -2 & 1 & & & \\ & 1 & -2 & 1 & & \\ & & \ddots & & \\ & & & 1 & -2 & 1 & \\ & & & 1 & -2 & 1 & \\ & & & & 1 & -2 & 1 & \\ & & & & 1 & -2 & 1 & \\ & & & & & 1 & -1 \end{pmatrix}$$

## **Diffusion equation**

$$\frac{\partial \omega}{\partial t} = \nabla \cdot (D(\vec{x}, t) \nabla \omega) + \dots \Rightarrow$$

$$(1 - \Delta t \nabla \cdot (D(\vec{x}, t) \nabla)) \omega(t + \Delta t) \Box \omega(t) + \dots$$
Generally gives a complicated matrix, has to be solved by iteration (Petsc)

 $D = D_0$ : Helmholtz equation  $(1 - \Delta t D_0 \nabla^2) \omega(t + \Delta t) = \omega(t)$ 

banded matrix, Gauss elimination possible

# Finite difference, ESEL

- Global model with self-consistent profiles
- Simulation domain include both edge, SOL and limiter shadow regions
- 2D approximation; parallel loss mechanism modeled by a parameterize loss term
- Input; basic plasma parameters
- Test on TCV, JET, ASDEX with reasonable results
- Collisional diffusion coefficients and parallel loss terms from first principal
- It is a very simple 2D model!



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## Finite difference, ESEL

Interchange model

$$\frac{dn}{dt} + n\Box(\phi) - \Box(Tn) = \Lambda_n$$

$$\frac{dT}{dt} + \frac{2}{3}T\Box(\phi) - \frac{7}{3}T\Box(T) + \frac{2}{3}\frac{T^2}{n}\Box(n) = \Lambda_T$$

$$\frac{d\omega}{dt} + \Box(nT) = \Lambda_{\omega}$$

$$\frac{d}{dt} = \frac{\partial}{\partial t} + \frac{1}{B}b \times \nabla\phi \cdot \nabla$$
$$\frac{1}{B} = 1 + \frac{r_o + \rho_s x}{R_0}$$
$$\Box (B, f) = \frac{\partial B}{\partial x}\frac{\partial f}{\partial y} - \frac{\partial B}{\partial y}\frac{\partial f}{\partial x} \quad \left( = \frac{\rho_s}{R_0}\frac{\partial f}{\partial y} \right)$$

$$\Lambda_{\alpha} = -\frac{\alpha}{\tau_{\Box,\alpha}} + D_{\bot,\alpha} \nabla_{\bot}^{2} \alpha$$

Subsonic advection:

$$\tau_{\Box,n} \Box \tau_{\Box,\omega} \Box \frac{M_{\Box}C_s}{L_p}$$
 ,  $M_{\Box} = 0.5$ 

Spitzer-Harm diffusion:

$$\tau_{\Box,T} \Box \frac{3L_{\rho}^2}{2\chi_{\Box e}}$$

**Collisional SOL limit** 

$$10 < v_e^* = \frac{L_{\rm op}}{\lambda_e} < 80$$



Conditionally averaged density blob structure

PDF of particle density flux

## Direct comparison with experimental results from the TCV-Tokamak, Lausanne: excellent quantitative agreement

Garcia et al. PPCF 48, L1 (2006)

# DTU

## **TCV-ESEL** Comparison

2.0 8 (a) (a) 1.0  $10^3 \overline{\Gamma}(\rho) \, / \, \overline{n}(0) \, \overline{c}_{\mathrm{s}}(0)$ 6 0  $\overline{n}(\rho) / \overline{n}(0)$ 00 00 0 0  $\odot$ 000  $\odot$ 000 0  $\odot$ 0000 2 0.2 TCV TCV  $\bigcirc$ 0 0 ESEL ESEL 0.1 0 0.50 0.75 1.00 1.25 0.00 0.25 0.50 0.75 1.00 1.25 0.00 0.25 ρ ρ 1.5 5 (b) (b) 4  $\Gamma_{rms}(\rho)\,/\,\overline{\Gamma}(\rho)$  $n_{\mathrm{rms}}(\mathfrak{p}) \, / \, \overline{n}(\mathfrak{p})$ 1.0 0 3 0 0 0 0 0 800800000000000000 0 0 0 0 Ö  $\odot$ 0 0 80 2 0.5 1 0.0 0 0.00 0.25 0.50 0.75 1.00 1.25 0.00 0.25 0.50 0.75 1.00 1.25 ρ ρ

Good agreement between experiment and turbulence simulations

Garcia et al. PPCF 48, L1 (2006)

Particle flux profiles

Density profile and relative fluctuations



Fig 4: Particles released inside LCFS, t = 1000



Fig 5: Particles released inside LCFS, t = 2500



Passive particles

$$x(t) = x(0) + \int_0^t v(x, t) dt$$

Summer student S. Boudaux, (2005)

# Solid boundaries - Disk



•Radial points are cosine distributed

•Chebyshev polynomials calculated via cosine transformation

•The Poisson equation decouples in  $\theta,$  a series of banded 1D problem to be solved in r

•r=0 should be a regular point

•As r->0 the grid spacing in  $\theta$  decreases: 1/(2 $\pi$ r)

•Even thought these scales are well below the viscosity scale they are extremely unstable and have to be removed manually (zero pad).



Poisson equation  $\nabla^{2}\phi = \omega \Rightarrow$   $\forall k : \frac{\partial^{2}\phi_{k}}{\partial r^{2}} + r\frac{\partial\phi_{k}}{\partial r} - k^{2}\phi_{k} = r^{2}\omega_{k} \Rightarrow$   $\forall k : \underline{A_{k}} \phi_{k} = \underline{\omega_{k}} + \underline{BC}$ 

$$\begin{pmatrix} \omega(r,\theta,t) \\ \vec{u}(r,\theta,t) \\ \psi(r,\theta,t) \end{pmatrix} = \sum_{m} \sum_{n} \begin{pmatrix} \omega_{mn}(t) \\ \vec{u}_{mn}(t) \\ \psi_{mn}(t) \end{pmatrix} T_{m}(r) \exp(-in\theta)$$

$$r \in [-1:1], \theta \in [0:2\pi]$$

$$T_{n}(x) = \cos(n\cos^{-1}(x)) = \cos(nz)$$

$$T_{0}(x) = 1, \quad T_{1}(x) = x, \quad T_{n+1}(x) = 2xT_{n}(x) - T_{n-1}(x)$$

$$T_{n}(-1) = (-1)^{n}, \quad T_{n}(1) = 1$$

Energy Spectrym: 
$$E(r,n) = \frac{r}{2} \sum_{n} u_n^2(r,t) + v_n^2(r,t)$$

## Spectral versus finite difference



Close-up

Spectral 512

Spectral 1024



FIG. 5.4. Time evolution of the vorticity field for the interaction of a Lamb-dipole with a no-slip wall. The spectral scheme has been used with M = N = 1024 and Re = 2.000. Notice that only a part of the computational domain is displayed.



FIG. 5.6. A close-up of vorticity contours for runs with the same parameters as in Figure 5.4 at T = 4.0 and Re = 2.000. Top: Spectral scheme. Middle: Arakawa scheme using an equidistant radial grid. Bottom: Anakawa scheme using cosine distributed nadial grid points. Left resolution 512 and right resolution 1024. The dot in each frame locates the position where the time development is compared; see Figure 5.7.

(V. Naulin and A.H. Nielsen 25, 104–126 SIAM J. SCI. COMPUT 2003)

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### (V. Naulin and A.H. Nielsen 25, 104–126 SIAM J. SCI. COMPUT 2003)

## **Spectral versus finite difference**

Solve the vorticity equation with solid boundaries in annulus geometry

$$\frac{\partial \omega}{\partial t} + \left[ \omega, \psi \right] = v \nabla^2 \omega, \quad \nabla^2 \psi = -\omega, \quad \vec{u} \mid_{\partial D} = 0$$

We used a spectral code (Chebyshev-Fourier expansion) and finite difference code (cosine distributed radial points). A Lamb dipole

$$\omega = \begin{cases} \frac{2\lambda U}{J_0(\lambda R)} J_1(\lambda r) \cos(\theta) & , r \le R \\ 0 & , r > R \end{cases}$$

was used as initial condition and let it interact with the outer wall for different Reynolds numbers, Re=UL/v.

## Conclusion:

- Spectral schemes are more accurate than FD using the same resolution BUT
- Using the same computer power we can obtain similar results for the two different schemes

FIG. 5.10. Integrated error calculated from (5.2) versus resolution for the FDc scheme. Reynolds number: 200 (solid line), 1.000 (dotted line), 2.000 (dashed line), 4.000 (dashed-dotted line).

FIG. 5.9. Integrated error calculated from (5.2) versus resolution for the spectral scheme. Reynolds number: 200 (solid line), 1.000 (dotted line), 2.000 (dashed line), 4.000 (dashed-dotted line)









Spectral

resolution

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# DIESEL

- Global version of "ESEL"
- Covers the full toroidal domain

$$\frac{\partial n^{i}}{\partial t} + \left\{\phi, n^{i}\right\} = \mu_{n} \nabla_{\perp}^{2} n^{i} + C_{s} \nabla_{\square} n$$
$$\frac{\partial \omega^{i}}{\partial t} + \left\{\phi^{i}, \omega^{i}\right\} = \left\{\frac{1}{B}, n^{i}\right\} + \mu_{\omega} \nabla_{\perp}^{2} \omega^{i} + V_{A} \nabla_{\square} \omega$$
$$\omega = \frac{1}{B} \nabla_{\perp}^{2} \phi \quad , \quad B(r, \theta) = \frac{B_{0}}{1 + \frac{x}{R} \cos \theta}$$

$$\begin{split} c_{s} \nabla_{\Box} n^{i} &= \begin{cases} \frac{C_{s}}{L_{\Box}} \left( n^{i+1}(r, \theta + \Delta \theta) - n^{i}(r, \theta) \right) & \text{if } n^{i} \geq n^{i+1} \\ \frac{C_{s}}{L_{\Box}} \left( n^{i-1}(r, \theta - \Delta \theta) - n^{i}(r, \theta) \right) & \text{otherwise} \end{cases} \\ c_{s} \nabla_{\Box} \omega^{i} &= \begin{cases} \frac{C_{s}}{L_{\Box}} \left( \omega^{i+1}(r, \theta + \Delta \theta) - \omega^{i}(r, \theta) \right) & \text{if } |\omega^{i}| \geq |\omega^{i+1} \\ \frac{C_{s}}{L_{\Box}} \left( \omega^{i-1}(r, \theta - \Delta \theta) - \omega^{i}(r, \theta) \right) & \text{otherwise} \end{cases} \\ \Delta \theta &= \frac{2\pi}{qn_{\text{drift}}} \end{cases} \\ \hline \text{Normalisation[4], space and time } \mathbf{x} \rightarrow \frac{X}{a}, t \rightarrow \gamma t \\ \hline \text{Interchange growth rate: } \gamma &= \sqrt{\frac{2}{aR}} c_{s} \\ \hline c_{s} \text{ in normalized unites : } c_{s} \rightarrow \sqrt{\frac{R}{2a}} \end{split}$$

## DIESEL

□ Global model using full toroidal geometry on closed magnetic field lines □ Model, at present, based on a simple interchange model, see e.g. [1,2] □  $n_{drift}$  2-D drift planes each covering the full cross section of the torus □ In the above equations  $i \in [1;n_{drift}]$  and denotes the particular drift plane □ Parallel numerical code, based on spectral expansion of the solutions □ Scale linearly at least upto 100 CPU using 1024x2048 pr. drift plane □ Estimated maximum number of CPU is above 1.000!? (to be tested) □ The drift planes are separated toroidally by  $L_0 = 2\pi R/n_{drift}$ □ Parallel velocitites are parameterized using  $c_s$  and  $V_A$ □ q enters in the two parallel terms:



