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A study of abnormal occurence reports

Forskningscenter Risø, Roskilde

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A detailed study of failure and occurrence reports	
from five U.S. nuclear reactors. Data concerning the	
frequency of failure causes and multifailure incidents are given.	
Methods of failure classification are discussed.	
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Foreword

Reports are prepared by engineers in U.S. nuclear power plants for a wide range of component failures and similar occurrences. The precise reporting requirements are specified in the U.S. Nuclear Regulatory Commissions Regulatory Guide 1.16. Until 1974, such reports were termed Abnormal Occurrence reports. but since then the term "Abnormal Occurrence reports" has been reserved for those occurrences which have some safety significance. What were earlier termed "Abnormal Occurrences" are now as a general class, termed Reportable Occurrences.

"Abnormal Occurrence Reports", using the pre 1974 definition and data up to and including spring 1974. The data cover a wide range of occurrence types. In particular they give component failure data mostly of relatively unimportant individual component failures, such as miscalibration of a single redundant instrument, but in some cases for failures of some engineering significance. The reports are much less formal than those required for reliability data banks. They give considerably more background information concerning the cause and nature of failures than do reliability data banks; and also much more information concerning consequences and interrelationships between separate failures.

For this reason, the reports provide very valuable information, which is relevant not only to the study of nuclear power plant reliability, but also provides insight into the way failures can occur in many different kinds of process plant.

A STUDY OF ABNORMAL OCCURRENCE REPORTS

Introduction

An earlier study (Rise-M-1742) attempted to evaluate the role of design errors in nuclear power plant reliability. The results of that study showed that design error plays a large role in power plant failure: and the surprising result that an unexpectedly large proportion of failure incidents involve several independent component failures.

Several questions arose as a result of that earlier work. One would expect that the role of design error diminishes for individual plants as they grow older. It was decided to investigate the sequence of abnormal occurrence reports from individual reactors over a number of years.

Another question is the extent to which separate failures in multi-failure incidents contribute significantly to the failure consequence. It is possible that several of the failures within an incident have no direct bearing on the extent of failure consequences. They may play an incidental rather than crucial part in the failure sequence.

The remaining area of interest for this study is the problem of common mode failure. The importance of common mode failure was established earlier, but the only datum obtained was a gross figure for the proportion of failures involving common mode effects. Results of the common mode failure study performed here are published separately (Risz-M-1826).

A major element in motivating this study, was the desire to discover the weak points in existing techniques of failure mode analysis of process plant, and to develop the background information for improving those techniques. There are some types of failure for which no systematic analysis technique exists, for example

- wiring errors involving incorrect interconnections
- "system design" errors in control systems
- mechanical blockage and jamming problems arising from loose parts
- errors in written procedures
- human errors due to confusion between procedures or misinterpretation of operating situation.

All of these problems involve complex common mode effects, and it is important to discover to what extent they are important in practice.

The procedure in this study has been to take individual incident reports, and to classify them according to fixed criteria. The nature of the data prevents one from obtaining good statistical data with known significance, but it is felt that qualitative, and "order of magnitude" conclusions can be drawn from the results.

Choice of data

The data used for this study is abnormal occurrence data submitted to the UNION by operators of light water reactors. The reason for this choice is that the information is readily available, there are consistent criteria for reporting the data (reporting is required by law), and the quality of the reporting is generally excellent. The information differs from that usually available in reliability data banks, in that complete failure incidents are described, often involving several individual component failures.

The choice of reactors for this study was determined by the availability of records for a period of years. Records from the earliest years of reactor operation were however not available to the author. There has been a change in style of reporting over a number of years, and this has to some extent negated the value of the data as a record of "design error" evolution.

Classification of occurrences

For each occurrence report, the date, six month period number (from reactor start up), operating state at the time of occurrence, and method of failure discovery were recorded. Most failures are detected during surveillance testing, some via special inspections, but many are discovered as "actual" failure incidents which interfere with plant operation. In many cases a failed condition existed over a considerable period, but the plant state recorded was nevertheless the plant state at the time the failure was discovered. In virtually all cases it is true that a latent failure, discovered during surveillance or special tests, has existed while the plant was operating.

Each individual component failure was recorded separately for each incident, and in some cases there were several failures contributing to the incident.

- OP Plant operational, generating power.
- SU Plant was in start up phase.
- SD Plant was in shut down phase.
- CS Plant was in cold shut down state.
- RF Plant was shut down for refuelling.

Table 1. Classification of plant states at the time of failure discovery.

- ACT "Actual" incident occurs during normal operation of component.
- SUR Failure discovered during surveillance testing.
- PM Failure discovered during post maintenance testing of the failed component.
- COM Failure discovered during commissioning tests.
- Failure discovered during special inspection, as a result of suspected incipient failure, or as a result of information from other plants.
- Si Failure discovered during start up testing.

Table 2. Classification of "mode of discovery" of failures.

In a study such as this, which is concerned with the cause of failure, it is important to define the term component failure carefully. A failure is deemed to have occurred, if a component is incapable of fulfilling its function, in spite of the fact that inputs such as power supplies, control signals, mechanical support, etc. are within the limits specified for the component. Failures due to incorrect input are judged to be consequent failures, and were recorded for interest, but were excluded from statistical analyses. Failures due to environmental changes were recorded as component failures, unless the environmental changes was a result of some earlier component failure in which case they were classified as consequent failures, and again omitted from statistical analyses.

The degree to which a plant is divided into "components" also affects the number of component failures recorded. In this study, a standard level of div-

ision into components was used, as expressed by table 3. However, where a component was part of a larger component or subsystem, this fact was recorded by opencatenating component and system names.

A 4 10 a			
Amplifier	AM	Motor starter	MS
Annunciaton	AN	Potentiometer	POT
Battery	BŢ	Recorder	REC
Battery charger	BC	Lightning arrester	IA
Cable	CAB	Ground switch	38
Capacitor	CAP	Relay	RE
Circuit breaker	CB	Relay or switch contact	CN
Magnetic clutch	CL	Reset switch	rs
Control switch	CS	Resistor	ret
Coil	co	Signal comparator	COMP
Diode	DI	Pressure switch	PS
Detector	DE	Torque switch	TQS
DC power supply	DC	Temperature switch	TS.
Flow switch	FS	Fuse	Fü
Reater	HG	Generator	Œ
Input module	IM	Heat tracing	HT
Inverter (solidatate)	IN	Test button	SB
Level switch	INT	Thermal overload	OL
Lamp	121P	Transformer	TFMR
Limit switch	LML	Transmitter	THTR
Manual switch	SW	Wire	٧
Meter, guage	GG	Solenoid	SOL
Motor	Ю		

Table 3A. Electrical component coding.

Accumulator	AC	Refrigeration unit	RF
Blower	BL	Sluice gate	SL
Control rod drive	CED	Sump	SP
Control rod	CTR	Tank	TK
Cover plate	COV	Tubing	TUB
Core	COR	Turbine	TURB
Damper	DM	Condenser	COND
Diesel	DIES	Vent	٧T
Expansion joint	XJ.	Well	WL
Filter, strainer	FL	Valve, check	CV
Flexible pipe, hose	FLEX	explosive	EV
Fuel	F	hydraulic	HV
Gas bottle	GB	motorised	MV
Gaskat	GK	pneumatic	AV
Heat exchanger	HEX	relief	RV
Insulation (thermal)	Tins	manual	χv
Ion exchanger	TEX	safety	SV
Noggle	NZ	atop	DV
Orifice	CIR	vacuum relief	VV
Pipe	PP	main steam isolation	MSIV
Pipe Cap	CP	solenoid	ΚV
Pipe Support	CUP	Seal	SL
Pressure vessel	PV	Actuating mechanism	ACT
Pump	PM	-	

Table 38. Mechanical component coding.

Event sequence

The structure of event sequences has a direct bearing on the way in which failure records are interpreted and used in later failure mode analyses. Failures were classified as spontaneous, gradual, misoperation, latent or consequent.

A spontaneous failure is one which occurs at the time of the incident and serves to start the incident. The classification of "gradual" failures was introduced because it was difficult to describe some kinds of initial failures.

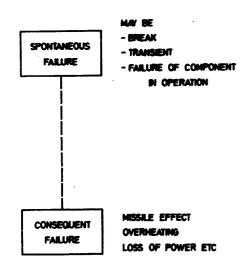


Fig. 1 Event sequence with spontaneous and consequent failures

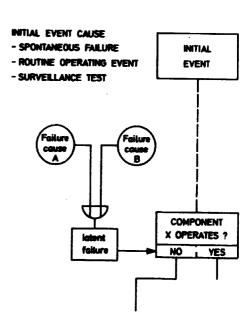


Fig. 2 Event sequence with latent failure

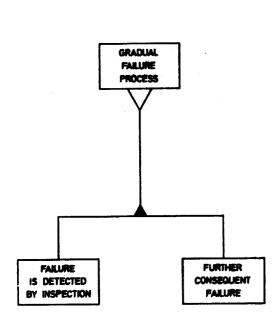
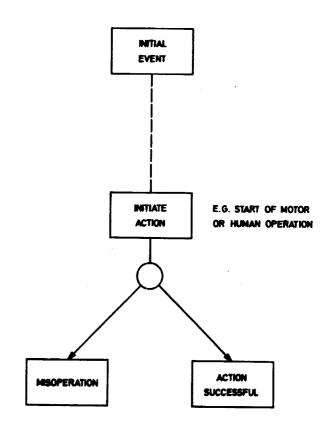


Fig. 3 Alternative failure sequences resulting from gradual failure.



-9-

Fig. 4. Event sequences including misoperation

as spontaneous, for example slow leaks which are detected after they have caused further damage.

Latent failures occur in components which are called on to work intermittently. Such components may exist in a failed state, which is "revealed" when the component is tested or is called on to operate.

Risoperation failures are those which occur when a component or operator is called on to carry out such operation, and which occur while the component or operator is carrying out the operation.

Consequent failures are those which occur as a direct result of some

S	Spontaneous
G	Gradual
L	Latent
M	Misoperation
С	Consequent

Table 4. Classification of failures according to how they are triggered.

Further classification of "consequent" failures is possible - input failures (I) (command failures), overload or stress failures (secondary failures) (O), and direct effect failures (D). Such classification is often made in failure mode analysis studies. But such classification was made only for common mode failures, in this study.

Mymbolic description of the different kinds of failure are shown in fig. 1 to 4 (see Rise Report Rise-M-1743). For each of the different kinds of failure, a different model is required to describe failure probability.

As a result of the study, some of the initial ideas on classification of failures were revised, and these ideas, which were not used in the study itself, are given in Appendix 1.

One of the important objectives of this study was to observe the number of failure events occurring in actual failure sequences. For this purpose, failures detected by testing were ignored. Also, several failures occurring within similar components due to a common mode effect, were treated as single failures. Consequent failures which were certain to occur, given earlier failures, in the sequence were ignored. But consequent failures which involved some probability factor, such as destruction of components by impinging steam jets, were counted as separate failures.

Common mode and coupled failures

As part of the study of multiple failures, a study was made of common mode and complet failures in similar plant components. The results of this study are presented in a separate report.

Failure cause

The objective in this study has been to come as close as possible to the original cause of failure. Failure causes are classified at two levels, as shown in table 4. The second level of classification is much less certain than the first. In the case of operator and maintenance errors, the subclassification was completely experimental.

To maintain consistency of cause classification it is important to have clear criteria. An error was considered a design error if it was explicitly described as such in the abnormal occurrence report, if it was one of a long series of similar failures with very high failure rate, or if the design was modified as a result of the failure. A similar criterion was used for classifying procedural errors. Failures were classed as operator errors if this was explicitly stated in the abnormal occurrence report, and similarly for maintenance and installation errors. (This can lead to underestimation of operator errors).

Random component failures were recorded in those cases where a simple standard mechanism of component failure was involved e.g. bearing leakage, shorting of a relay coil stc., and in which no excessive grouping of failures of a similar kind occurred.

In some cases, more than one cause of component failure could be discovered. In other cases, it was difficult to judge between two alternative failure causes. In these cases, fractional contributions to failure classes were recorded, an equal fraction to each contributing cause.

In many cases, the same kind of failure occurred in the same component several times in the course of a few years. These cases were counted as single failures in determining relative importance of different failure causes (though all incidents were counted in determining common mode failure proportions). If one does not count failure causes in this way, then some frequently occurring failure types come to dominate the distribution of causes. The proportion of design error failures, in particular, becomes inflated.

######################################	- <u>1</u> 2-		
Cause		Cause subclass	
C Random component failure	×	Mechanical	
C Random component failure D Design error	E	Electrical	
D Design error	U	Problem unknown at design time	To the state of th
	C	Complex system interactions	
	. 1	Interdisciplinary problems	
	٥	Oversight	
	ĸ	Communication problems	1
	z	Calculation, sizing problems	
	S	Component selection problem	
O Operator error	0	Omission	
	x	Unnecessary extra operation	İ
	¥	Wrong target of operation	and the second
- 유명의 - 弘祖 구성	E	Error in amount of operation	ì
	8	Error in operation sequence	
	P	Wrong procedure used	P
	J	Judgement of quantity	
	С	Communication problem	
	R	Lack of recognition of danger	1
		situation	1
	н	Misrecognition of danger situation	P
			4

Table 4. Coding for causes of failure.

	Cause		Cause subclass
M	Maintenance error Installation error	A	Adjustment (of instruments, switches)
		o	Omission of step in installation, repair
		P	Positioning of component
		H	Misuse of component, handling problem
		В	activation of other equipment not under repair
		С	Choice of component to install, repair
		1	Interchange of two components, cables etc.
		Q	Quality of join
P	Procedure error	0	Omission of subprocedure
		С	Extra control, checking required
		М	Procedure open to misinterpretation
		U	Effect unknown before failure
		¥	Procedure wrong
r	Fabrication fault		

Table 4. Continued.

Cause unknown

Date

Abnormal occurrence reports from five reactors were classified for reactors with start up dates in 1962, 1963, 1967, 1969, and 1970. Abnormal occurrence reports were generally available to the author only from the later years of reactor operation (from 1969 operat).

Both the number and character of abnormal occurrences varied greatly from reactor to reactor. The variation could have arisen from the different quantity and type of equipment at the reactor plant, as well as differences in reliability of components. However, it was hoped that by concentrating on the proportion of occurrences of different types, meaningful conclusions could be drawn.

As can be seen from fig. 7 not too such significance can be attached to the actual numbers of abnormal occurrence reports for successive years.

In addition to abnormal occurrence reports, some "unusual event" reports were included in the analysis, where the reports concern safety related or pressure boundary equipment (see USAEC safety guide 13.2. for definition of abnormal occurrence, unusual event).

There may be some omissions of abnormal occurrence reports for the reactors studied, though where possible records were checked against semiannual operating reports. On the assumption that omissions are randomly distributed, the effect on proportions of failure types should not be too important.

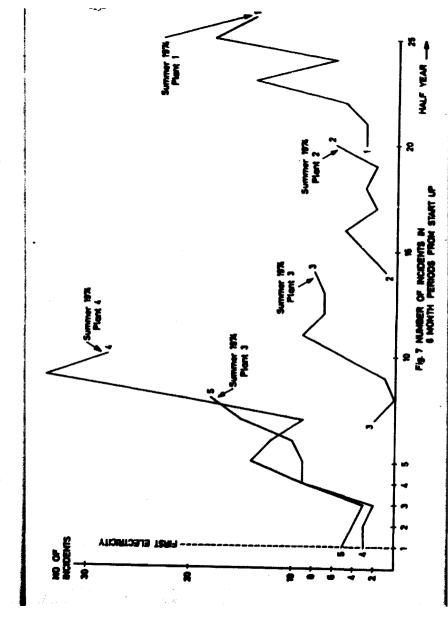
In all there were 67, 24, 33, 141, 75 abnormal occurrences for the respective reactors.

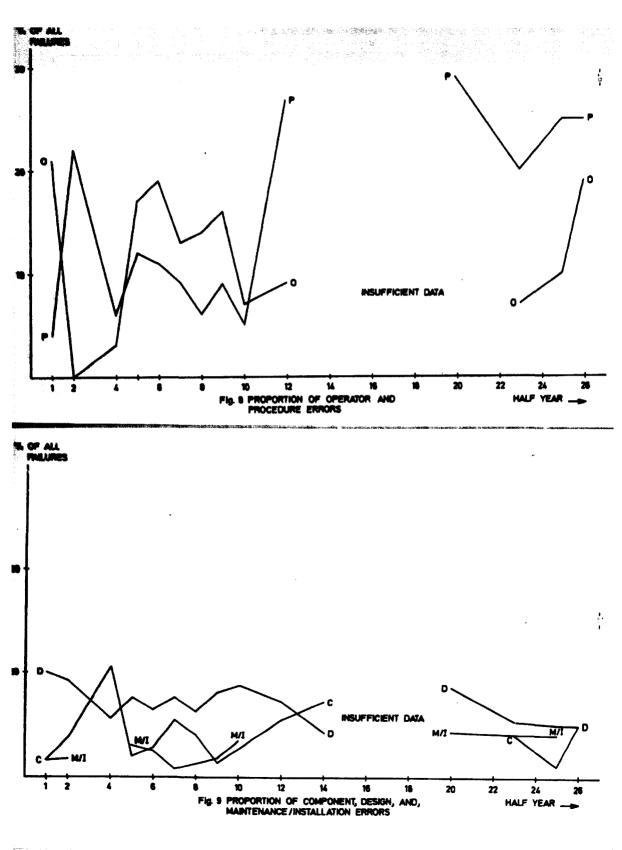
Causes of failure

Fig. 8 and 9 show how the various causes of failure behave as plants grow older. No significant trends can be detected, the proportion of failures due to respective causes seem if anything more or less constant. But such more data would be required, before trends could be detected beneath the random variations in the data. As has been observed in earlier studies, design error seems to be the dominant cause of failure, followed by random component failure.

Table 5 gives the numbers of failures attributed to particular cause classes, for each of the reactors studied. The pattern is more or less constant, appart from an unusually high proportion of failures attributed to mintenance errors, for one of the older reactors, and a complete lack of reported operator errors for one reactor.

The classification of secondary causes for design, operator, procedure, and maintenance errors are shown in tables 6 to 9. The classifications here are experimental, and should be regarded as indicative rather than definite. Such classifications can be used as a guide to qualitative studies of failure causes.





e,								
Reactor	Design error	Random component failure	Operator error	Error in procedure	Maintenance or installation error	Fabrication error	Cause of failure unknown or unrecorded	Number of individual lailures reported
1	37 %	11 %	10 %	18 %	16 %	1 %	7 %	8 2
2	14	11	11	11	<u>36</u>	o	18	28
3	48	<u>31</u>	<u>o</u>	7	5	0	10	42
4	34	17	1,2	9	10	0	17	174
5	34	23	19	7	6	3	7	96
ALL	35 %	18 %	12 %	10 %	12 %	1 %	12 %	422

Table 5. Cause classes for component failures.

		9
s	Component selection	14
0	Oversight	17
U	Error due to effect unknown at	
	design time	25
z	Sizing, dimensioning error	13
С	Error due to lack of recognition of	
	complex system interactions	7
K	Error due to communication problems	1
?	Error with cause unknown or unrecorded	22
Table	6. Design error secondary causes	
	(Based on 147 occurrences)	

% of error

0	Omission of a step, operation or procedure (reason for omission	
	unknown)	49
P	Wrong procedure used	16
R	lack of recognition of situation	7
M	Misrecognition of situation	2
8	Error in operation sequence	4
٧	Operation applied to wrong target component	. 4
J	Error of judgement of amount	2
С	Error due to communications problems, lack of communication	4
E	Error in amount of adjustment	2
7	Error due to unknown cause	9

Table 7. Secondary causes of operator errors.

(Based on 77 occurrences)

		%
0	Error due to omission of step or procedure	5
U	Error due to omission, because effect was unknown at the time the procedure was defined	10
H	Procedure was open to misinterpretation, unclear	7
F	Wrong test frequency specified	2
v	Wrong procedure specified	2
c	Extra control required - procedure does not contain sufficient cross checks	6
?	Error with unknown cause	14

Table 8. Secondary causes of errors in procedures.

(Based on 44 occurrences)

		*
A	Problems with adjustment of instruments, limit, torque switches etc.	22
¥	From operation carried out, or right operation carried out wrongly, due to lack of knowledge or expertise	16
В	Spurious activation of other equipment while carrying out tests or repair	9
I	Interchange of two cables	6
υ,0	Omination of operation, due either to oversight or to ignorance of requirement	6
P	Error positioning component	3
Q	Problems of quality in soldering, welding	3
R	Error due to lack of recognition of situation	3
С	Error in choice of which component to repair	3
s	Breach of safety regulations	3
7	Error due to unidentified causes	25

Table 9. Secondary causes of installation and maintenance errors.

· (Based on 49 occurrences)

It is possible to make some qualitative comments on the results.

A large proportion of design errors involve effects which were unknown before failure occurred. Many failures of this type occur repeatedly, the same component sometimes being repaired several times before the failure is correctly diagnosed. Such incidents underline the value of abnormal occurrence reporting.

Another large group of design errors involve inappropriate choice, of materials, or especially, of instruments. Problems of this kind can be reduced by qualification testing and standardisation, activities which are receiving a great deal of attention from nuclear engineers.

By far the largest proportion of operator errors involve omission or oversight, involving just a single type of plant operations. By their nature, such errors are relatively easy to forsee, and analyse, even in the cases where several components are affected in a common mode fashion. More serious are the errors due to lack of recognition of dangerous situations, misrecognition, application of inappropriate procedures or application of correct procedures to the wrong component. Among installation and maintenance errors, difficulties in adjusting limit switches and torque switches are outstanding.

Some types of failure are difficult to account for in failure analysis. It is difficult to identify all of the failures of this kind, but the following provides a list of errors which occurred, but for which no systematic failure analysis procedure exists (as yet).

Loose parts jamming	5
electrial circuit omissions or miswiring	5
omission of essential procedural steps,	
or incorrect steps	3
human decision errors with wide ranging effects	3
established trip levels inappropriate	6
water hammer effects	3

Also, there were some instances of problems present special difficulties in failure mode analysis.

common dependence of several components on one service supply or environment

Haltifailure incidents

In this study, as in the previous one, the number of multiple failure incidents was high when compared with expectation. At the level of consequence represented by abnormal occurrence reports, there are still a significant matter of 4, 5, 6, and 7 fold failure incidents (fig. 8).

This pattern holds true in spite of the fact that

- a) failures to several components of the same type, due to the same cause, have been treated as single failures.
- failures which are a direct consequence of earlier failures, are not counted in arriving at the number of independent failures.
- c) failures which do not contribute significantly to the consequences of the incident have been ignored.

Examining the nature of the multiple failure incidents reveals several distinct types,

- blowdown incidents, in which steem is released, causing defects in surrounding components to be revealed, in some cases, and causing a large variety of safety components to be activated.
- multiple human errors. It is clear that in some of these incidents there is coupling between the errors. Once one human being has made an error, others tend to perpetuate it. However, the nature and degree of interdependence of these errors is difficult to determine.
- because of the way that these data are classified, if single component fails to work because its design is inappropriate and its operating procedure is incorrect, the result is counted as a double failure. This "classification effect" is significant in raising the number of 2 and 3 fold failures. It does not contribute significantly to the number of 4, 5, 6 fold failures etc.

By far the largest proportion of failure types in the saltiple failure incidents are latent failures revealed during special incident conditions, or revealed when anfety equipment is activated.

NO. OF INCIDENTS NO. OF FAILURES

Fig. 6 HISTOGRAM OF MULTIPL PALLIFIC INCIDENTS PER INCIDENT

Conclusions

Conclusions as to the meaning and importance of the kind of results given here have been presented before (Riss-M-1742). The additional data collected here serve merely to reinforce those conclusions which are

- That design and other human errors are responsible for a significant number of failures and abnormal occurrences.
- Some "design error" type failures cannot be accounted for in traditional types of reliability analysis.
- 5) Improvement in particular component reliability performance, in testing, and in standardisation, should be valuable in improving plant reliability, because a small number of component types are responsible for a large proportion of failures.
- 4) Multiple failure incidents play an unexpectedly large role in abnormal occurrences. Records of interrelationships between failures would be a useful addition to failure statistics data bases.

In addition to these remarks, some conclusions can be offered concerning the type of classification study attempted here.

It would be useful to obtain some standardization of the terms used in classifying different types of failure, according to the way in which failures reveal themselves, the plant state at the time of occurrence and/or discovery, and the triggering mechanism of the failure. The classification used here is self consistent, but is different from schemes used elsewhere.

The classification of primary causes of failure seems acceptable, and is similar to that use by the USAEC (s.g. OOE-OS-OO1, 1974). However the method of classification used here, attributing a failure to a single class, or using fractions to represent degree of responsibility for a particular cause, is messy. Accepting that a failure may have several causes, and that the percentages of failures due to different causes may total to more than loos, seems preferable. But if this method of classification is accepted, some definition must be made of how important and unusual an effect must be, before it is accepted as a contributing cause of failure.

The classification of different failure causes into secondary categories was not particularly successful. Often there was insufficient information in the abnormal occurrence reports to make classification precise. And the cat-

egories used here often overlapped. The information in such classification should not be used to derive percentages to which different causes are responsible for failures. The information might be used to perform clustering studies, with the hope of finding more clearly identifiable types of failure.

Uncertainty as to cause of failure should not be used as an excuse for assigning two causes to a particular failure. Instead, if there are several clearly alternative causes, this fact should be recorded explicitly (e.g. A/B means either cause A or cause B is involved, C & D/E means either cause C and E are together responsible, or cause E is responsible). Failure for which causes are unknown, should be recorded separately. Only in this way is it possible to interpret the meaning of failure cause data.

A revised system of classifying different failures according to event sequences, is given in appendix 1.

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Appendix 1. Classification of failure events

Classification of the different kind of failure events which can enter into event sequences is useful and important, because it indicates the relevance of particular pieces of failure data to different reliability calculation models. In fact, as reliability models become more complex, more complex failure classifications are required. The scheme introduced here is therefore just a particular example of a range of possible schemes which differ in level of detail.

The first distinction is made between failures which are caused by some external event or process, and those which arise with no apparent cause or for which the failure cause is an inherent property of the component. This second group is the one which has been called "random component failure" earlier in this note. These are called spontaneous failures here. Examples are the normal forms of bearing failure, relay contact failure etc., for which no specific cause can be described, or which cannot be prevented in normal engineering practice.

Examples of typical causes in the first group of failures are design and installation errors, extreme environmental conditions, misoperation by an operator etc.

A distinction which is equally important for obtaining a reliability model of failure consequences is whether the effects follow instantaneously from the failure, or whether the effects are gradual (e.g. slow leakage of some valuable material).

When components operate intermittently or only occasionally (such as safety systems) or with intermittent load (such as many pneumatic orhydraulic systems) a third distinction becomes important - whether the effects of the failure remain latent, or whether the consequences show themselves immediately. In the case of a latent failure, a failure event occurs at some time. The component is reduced to a state in which it cannot operate according to specifications. When the component is called upon to operate (the failure is triggered), a "failure to operate" occurs.

The definitions of the various failure types are illustrated in fig. 7.

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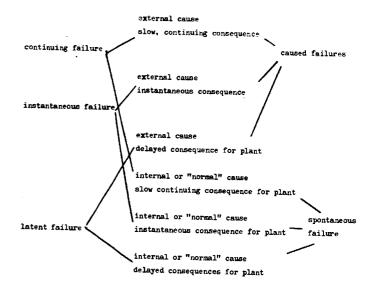


Fig. 7. Definitions of failure classes.

For latent failures, the stage at which the failure is discovered becomes important, especially for systems in which automatic continuous testing and periodic testing is performed.

A latent failure may remain hidden due to the fact that the particular type of error is not exercized or triggered by the test inputs applied. These failures are called "untriggered". Equally, a failure may be triggered, but its effects may not be indicated because the failure alarm outputs and test measurements performed, are inadequate. These failures are called unmonitored. (See fig. 8).

50	age at which failure pho	enomenon occurs	
kind of failure involved	continuous operation	during stand-by	on activation
latent		latent failure	failure to operate
			failure on demand
imediate	failure in operation	active failure	misoperation

Table 10. Terms used in describing latent and immediate failure sequences.

A useful distinction in judging the effectiveness of testing, is that between actual failures and failures found under test. For actual failures consequences occur which affect the operation of the plant. The following relation is true.

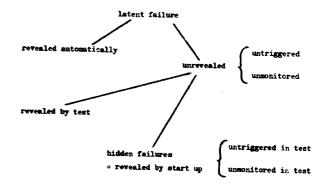


Fig. 8. Types of latent failure.

Actual failures = hidden failures

- + failures in operation
- + active failures
- + misoperations, not under test

Finally, it is useful, in classifying multiple failure sequences, to indicate whether a failure was initial (initiated the sequence), contributory (independent, but triggered as a result of the initial failure, or increasing the consequences of the initial failure), or consequent (caused by the initial failure).

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128	AO	Nov 5	a.	OF	ACT											8			Bindfrical less rejection valve tecting Transiest Manual trip
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141	AO	Jan 15 - 73	5		ACT		M/O	Safe					A			M		And the second s	rege muico atour aperatir.♪ radiation averibye.

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DOCKET NUMBER	OCCURRE ICE NUMBER	DATE	SIX MONTH PRRIOT TO.	OPERAL CONTRACTOR OF PLANT.	DISCOVERY TYPE	SPRIOUS	೦೩ ೮ ವಿ.	CAUSE STROMAGE	COMPONENT TYTE	FAILURE MODE	CATTORN WORKING	RECOMBLE MESSESSIONS	DONNOL NALE REFECT	JONNORMAN AREN DED	HOMEOTHONON HIGH NO MON	IAPENI, SPOIDASEUS	INMEDIALS REPORTED TO THE PROPERTY OF THE PROP	INTELA	rachana . d
1 8 6	AO	Jun 6 - 73	6		ACT		O P D M ?	C X B	XV. C.EC XV.P C.EC	5 .			r	3	i.	M L L S L	CMF		Went valves open on contain vent pressure measurement Valves were not on drawing
197 212		Jun 73			ACT SIR		đ		RPS AC							C			Turbise trip did for lead to reactor trip immediately, but from high pressure / sec. later. Set point calculation error - too low
225		Aug 23 July 10			ACT ACT		O F	0	usio CS. BL	h			Ą	all	4,	M M			-y relase 1: 19 Wi Spring alignenties in over current protector
226	AO	July 10	6		ACT		D O M		CB. PM. ECC				y	all 3 or		L M L	CMF		All circuit brookers type westinghouse DB-80 replaced omitted testing of S-by S C testing after replacement. Overcurrent setting not adjusted -2 spurious trips.

DOCKET SUMMERS	OCCURRENT Winds	30 m						100 mg 2 mg	21 21 22 21	i vina seri	And the second second	**************************************	* * * * * * * * * * * * * * * * * * *				
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294	AC			-3	\$774			F.B.	1	LCCE					1		Several 1 in gents it steam generator = fuel strates
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DOCKET NUMBER	COURAGE HUMMER	מאמ	12. Mark 18 18. S. Land	1 등 등 등 4 km () - 4	PLE STEN 1:	C.764 H.863	JASES.	CAGED TIP DALL	COMESTABLE TO C	AACCONS MODES.	PALLSON MOTOR OFF	Martin Amerikan Martin Amerikan	5,8844 5,8844	308 C18 4.4	REPORT TO A SECTION OF THE SECTION O	18 18 18 18 18 18 18 18 18 18 18 18 18 1	LMMs. CALC RMPR.CALC	10 mm - 10 mm	rae auntino (
1	72 ~ AG			OP	ACT	11	a	;;>	xv c	¥	CRK		¥		N	(O			Same valve as in 133, - water freezing prack
176	72-1	Feb 73			SI	* *	a	F J	W RL RHR W.RI BL				¥	2	N N			of the second	Sommon sir em it breaker bod ies for circuit breakers give SME potential
191	73-1	Feb73		OP	SUR	1	C		DI RE RPS		₩?	c:	*				D.		Light diods in meter relay ernatic Meter relays are being replaced
100		Mer73 Mer73		OP	SUR	12 12	0 P 0 P	1	PT GEN		Loos	cı				i.	R	C	Loose pot an generator regulator Surveillance testing omitted, procedure revised

A SANCTON OF THE PROPERTY OF T	NOVETA	ACCURA MICE NUMBER		**C	0x33,	2018.1 388.5% C 14	1.000 F. 1.0	A.1.8	AMMITTEL STOKE	seal incoment	acck audine	NATIONAL COURSE	भट्टा फाटक अवदेश स्थ	J.BJXX	108.00.40.40 A6.55.035.0	3000 - 3000 3000 - 3000	S. JENNYCHOAS Zonatal	T ASKOLI STOPHANE FTMSLERWS	. 联合. 1 / 3 是 . 5 / 3 / 3 / 3 / 3 / 3 / 3 / 3 / 3 / 3 /	DELCTRIBATION -
		A0 73-4	Feb73	11	0F	ACT		۵	М	ξ V		LK, JAM	ÇI				1.1	18.	C	Same as AO 7)
A CONTRACTOR OF THE PROPERTY O	224	NO 73-5 NO 73-7		12		ACT		a 0		MV ©		CR)	7.				ω 1	I P	I G	Sampling line isolation valve 270 ⁹ crack around seat Let down valve opened too
								P	Ü	RV. C		LK						۲٦	Ç	slowly - causing relief valv To blow, then leaked, due to - procedural error minor LOCA, radicactivity release
	225	3-6	Tune 7 3 -			ACT		D		AV. COD CLEA	LANT V							. CK		purification line torn - overtorqueing - fit torque switch - Minor LOC A, release radicactivity
•		0			⊖ P	ACT		D	0	Boit		BRK COP		¥	44	l	S 8e	i	1	Overstressed hold down bolts on steam gen

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		NOWER	ii.va	83.K. 90.5. 0 PMF 100.5. 0.0.	Company of the second of the s	PI CORP (C.S.	288 Be 2	€.*!@	0 4 356. 279 4 13	Selection of the select	PATCHE VICE	MISSE MISSE	PER STANTED	1. (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	70% C1% 137	\$ \$40° 0°; 3008 * 538°;	. A.18 %; - 14 China Service	ANN CONTRACTOR		. : . • •
		NO 73-1		12	OF	ACT		ŭ		មន្តិ: !			<i>.</i> :	÷		¥	. 1	3	ŀ	Motor control centra jower supply failure
		k0 73-9	Det73	7.3	4 F	SUP		M. D.	u			iay.	()		i virta de la composito de la	i v	> ;	· I -	-	Viltage sensing relay covers too tight Too low ontant pressure Fost maintenance test did not detect incident
	253	3-1 10 3-1	De c73	13		ACT		D	(3)	MY.		20.2	91	7.	>:	**	. ~	1.		Paditactive waste tank valve leaked Same as Alms
1	257	3-1:		13	#	SUR		¢	M.	MS:7	4	JAM	_{::}				<u>.</u>	3		
1		•	Jan7≒	13				Ç.	М					¥	:	:	3	1	i	wy ymin beathro failed
		4-2			CP	ACT			×	F.				¥				ŭ,	С	Two flow sensor lines frozen
		10- 14-1	Jan74	13	The state of the s			M. G.	<u></u>	Pi.,				***	7.	Я		£3.		Same as Al-7∂∂

Several components/several causes

DOCKET	OCCURRENCE NUMBER	DATE	SIX NOWIH	OF PLANT OF PLANT	DISSOVERY DV >	SPRIOUS:	ጋሉ ወ.አት.	CAUSE SPECIALS	COMPONENT TYPE	FASTURE MODE	SAIDDER MODERATOR	ANTONERW MATERIAL	COMMON Nova SPENIS	DOMEROPE LUC A SUECISSO	SOFT STATES	(ATEST) GPOLASED	* 6.33.58.5.21.13. 85.53.8 * 6.7.41.3. 73.8 8.	18 18 4. 18 18 18 18 18 18 18 18 18 18 18 18 18 1	SEA POSTOS
263	NO 74-3	Fan74	13	OP	ACT		et ?		PM. RHR				Y	V)	Y	S	1	Ĭ	Total loss of external power- ice, relay problem Service water pum,s failed on automatic, worked on manual
284	4-4		14		ACT		?		SV. FL. GAS		LK					S	6		Filter fíre spray valve leaked
291	4-5	lar74	14	cs	ACT		M ,	M	MV.		JAM					٦.	₽	Ç	Overtightened letdown valve packing
292	9-6	l .	14	H	SUR		С	M	V		BLK					5	G	;	Check valve .
31.2	74 6	lay74	14	OP	ACT		۵	0	BEN		CIR FIRE		Y	6	2	5	I	O	Transformer winding short + fire Both generators affected by design error.
313	A0 74-1	Apr74	14	OP	ACT		c	M	SV SL.		CRC LK					S	G	I	Leaking seal on vol.control
320	A0 74-1	May 74	14	OP	SUR		D	0	PS		rif	•	Y	4	2	L	P	1 .	Power switch set points drift 'set points too near limit'

DOCATI NUMBER OCCURRENCE	14.18 513 // / : :	0.85v	. 1	50 % 0	CAUCH CHOCALD	30803838	BOOM ENTERS	CALIFORNIA WITH THE	KITTMODIA KATUUTEE	COMMU B. EMPROT	70 3 (0.55 - 5.7) A 5.7 ± 7.7 ± 7.8	#150 50 #500 #150 #5 * 5 #500	JATENIZ SPORTATO IT I	1896-015 - 1996-1981 1898-835 - 1995-19	(4.5), 1.5, 1307 (0.5), 1.5, 1.5, 1.5	ka na area.
324 AO 77-1	74	3 €		0 0	М	MSIV		JAM					. 1	ρ. β.	O ::	One trip unit

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		NUMERIC	XC VC		0. 17. 1. 1. 19.17 0. 17.18.	115 K. 1888 . 1888	SEN FOULT	TYD	COMPLEX OF BEINE	at at in and mod	সংগ্ৰেম উদ্ভাৱিক	CONTRACTOR SHOOT A	APTEMBLE WESTAMESTA	を *** *** *** *** *** *** *** *** *** *	787, 5, 18 771, 510, 1800	원 동작공학자 소리 한 10 일 : #일	5. 03408-15. 3. 03408-15.	I HAVE TO SEED OF A SEED O		EL WOLLD
	13.		April	,	E	e e l	1.5	ay E	. o		nit	,								
	97		7/7/7		u	ACT	T	ETP				-					is a	:	I	External transient caused trip. pf normal power
										COND							<u> </u>	-		Condenser failed
	113							м.	A	Ÿ	j.						1.	P		Safety valve opened early
								ΟР	NP									:		Operator failed to recognise BV open
1										٧	C	JAM					-		1	- this caused condenser failur
1				İ			İ	H									1	1		condensate return valve
]	1		thermal overhead trip -
1												ĺ	1				İ	1	ĺ	Jammed wedge, high dosing
1					ı								1				1	1		torgue switch.
I	ă î.							1	Lack	l							1			Lack of procedure for this kind of intident
1							1	D	1	INST		Į				1]	1	E	Lack of power to Peactor Fress
I			L										1					1	i	water level instruments
1	53		Apr7	1 1) DE	SUR		÷	Ε	Fuse	oc.					l			1	Offgas isolation valve
1								_	١		l						1			instruments fuse.
	61			1 10		ACT	i	ם	s	c.				Y	ALL					Lack of monitor light Stainless steel control rod
1				*`	"	1]	_	,	Γ.			l	ľ	Ann	l"	-		1	Collower rivets. Followers
1								l						l						removed. Everdose to investi-
	. 1																			sating engineer.
	67		Sept	14	6			¢			TAM									Condensate return valve again

	I	عدد	e of	roc	ANS			Sef	etv.	சூர்க்	<u> </u>	,	<u>a </u>	N 16	<u>-7</u>			,		2 of 3
BOCKET WINNER		WHER	DATE	SIX MONTH PERIOD SO.	OFERN LINE OF PARTY OF	DISCOVERY TYPE	SERIOGSE	CAUSE	CAUSE : GACIASS	COMPONER TYPE	FAILURE MODE	FAILURE MECHANING	RECOVERY NEATHWAY ISM	SORMON SULE	COMPOSESCE A PERCITAGO	SONFOL FOLE CONCEQUENCE	CLOSKVINOIS ZINGLYT	HMALDIA 15/1 REVEA 15/1/1011/14	-80 118 180: /TYTINT	TWO INTERCLON
7	•		22 Je r72	14	KC	sua		ж			Drin	Wate		В			L	R		Low vacuum sensor - water accumu-
: 1	8		LOJuly7 P hil iar72		op op	SUR SUR		t MT	1	en en										lation Generator voltage drop - Oil in distributor of propane generator
•	*		17Apr72 13 Apr	19 18	OP	SUR		M ?	1	CEN CEN		MAT								Solenoid fuel stop valve short Oil in solenoid
11	5		26Jan 73	19	OP	ACT		OP	٥								,			Radwaste concentrator valve left open - oversight
112	3		2 Oct72					7												Baffle damage Loss of power to emergency con- denser condensate return valve,
12	3		10 00 cy73	20	СP	ACT		N		eal.							М			Shaft seals leaked when deminer- aliser pump was stopped ~ motor failure due to arcing.
1.3			JU173		OP	РМ		7		EER		ĺ								Failed to start
1.1			3Aug73 680Y73		MT OP	SUR SUR		H E	,	S T	a	Dri f		×			L L	R R		Cranking limiter contr.lresistor
										9										open circuit prevented generator start.
								1												

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RCXXXI		NUMBER	Zá v e	(1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	(1, 20) (1, 20) (1, 20)	(A) (A) (A) (A) (A) (A) (A) (A) (A) (A)	1.125 李通教	in the second		in a second	হ'লে⇔ প্ৰান্ত হ'	.संस्थानक भूति १८५७ - १,	Marin Marina AMMAR FA	्र सुक्त देव कार्य			· · · · · · · · · · · · · · · · · · ·	COMPANY CONTRACTOR		
14	T		.6Jec74	21	J¥	J .∵T		ε.												loss of office power, more town 12
14	9		2Jan?4	21	∋₽	ACT		24		₽S.	ч			3			j.	:		nre ise to flood Opring in syltob fallet - press
15	- 1		:6Fe 674	21	OP	SP/P		E		WR FPS	Ţ	ENEAL		3.4	,	3			l	nnemer vecim relief velve. Fequest for lesses nomege by regulatury
1	77			21.	IJ₽	AC		ж		TLCS SL PM	î.	¥		H			77.	-		Mescup system pump soul lessage
16	- 1			21	JF.	SUR				CL RFS	F	ELX		S				÷		Folson injection waige blockage
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	ونولو	20	ap.	SUP		×		PM.	<u> </u>	L.E		3		ļ	_	<u>.</u>		Liss of priming water in generator
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92	epc?l	20	Ģ₽	SUR											-	7-	1	Added Operation cours ocumber to
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BOCKET HPAREA	Course N. S. Hunged	#:#		SIX MONITH PERIOD VO.	08.884.35.3 C.C.C. 08. PIANT	DISCOVERY TY A	nek toua?	AUDK.	Auge Stailate	ORIONARE TYPE	A HONEY MENE	A LOSS MONBALLS	RECOVERY MECHANISM	NORMALE PART	OM CONTACT.	ነው ነገ <mark>፡፡ መ</mark> መ ነው ነገር መመ	LASTERS.	4階階点 48-74 RBMA 78-11-19-11-1	কুল্ম নিজ্ঞানীয়ে কুল্ম কুল্ম কুল্ম কুল্ম কুল্ম কুল্ম কুল্ম কুল্ম কুল্ম কুল্ম কুল্ম কুল্ম কুল্ম কুল্ম কুল্ম কুল	४ वदा र १६४ का ११ १४
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	ſ	'	[· · · ·	"	1		- OF		٦	Ü	~~			1.3	'		Y	٤	P	1	Valve open timings not in accordance with safety spec.
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225	Ŧ			•	7.7	SUF] :		À.							1			lesign of usplation valve lever
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230		l pr	74	25				:		34			1.							Invertés control rod pins
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		May 74	 	RF	SUR	• ;	:	Ä		L.	ī.K					i v			Bolts needed tightening on valve
237	V O 11	May 74	25	RF	SUR		Ü	s	PS		រិកព្រំ	l CI	¥	٠.	Y	í			flenge New switches - temp problem
238	•	May 74 May 74		1E3	PM PM		D P	; M	CR ∶		TIM		Y Y	A	Y inst		9	i .	Timing problems again Start up check omitted
244 250		Apr 74 May 74	1	RF SU	SUR ACT		D 0	E	arge		Warp	: 58				i č	9 1	ŀ	Cotait target warp Raised reactor power extra 10% over
257	0 15	June?4	26	or	sur		P	O M	PM			đ‡				÷] 	instructions revised procedures Fuel pump - snsft key day tank empty
260		June7)	l	OP	SUR		Þ	?	BL.C			CE					p.	•	Suntainment blower had too high flow
265		June?4		HB SD	SUR		C	M	CF RPS	ļ, 	TIM		Y	,	À	1.		İ	Centrel rod timing again
269		June7	i				0		ES. RPS Fuel		STK	R				i.	Ħ		Scromm dum; tank level switch Choose wrong fuel bundle for test S

	V. 17.				,	,	,	,	,							,	,		
	Contract of the second of the	ME	1. 人名英格勒	Lobbins Comment of the Comment of th	Control of the contro	Spri) ** ** ** ** ** ** ** ** ** ** ** ** **	""。 · · · · · · · · · · · · · · · · · · ·	\$ 10 JAC	AF 1. AF 1. T. ₹4	* ************************************	ACTION ASSOCIATION	사 보기(점 본) (점 보기)	N.		7,47 5	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
270	019	Jun 74		32	ACT.				PM				ï	All	Ý	2		-	regradation of cultvaterleas.
									JF RPS										Trains pump (Monthe) flooded
285	2 7	auy†=	à6	31	ACE		:		Œ		- AM	la l	·	L.	ï	Ŀ] ;	Towali not withdraw ariwea
	72. 6	July ?	26	as	AUT		ř	ij	HPO IR		JAX	3E				1	7.		Seven loose parts in all retrieved.
	13. 9	June 74	26	SE	ACT		3	м	RPS		BPX		7	·		1		Ç	Newstrop ತಂಪಾಂಕರ ಕರ್ನಳೇ ಸ್ಥಾ =
							i.	7											teryllium oxude scattered through plant
290	1050	July ?	26	af	AUT.		Î	٥	Fost			Ξ	Y			ε	:	;	Post incident system valved out
593	arro	Fuly 7	26	ЯF	ACT		<i>j</i>	L.	BOLT BAFFI			:	Ÿ	,	Y	3	:	;	Badfle solts troke DMF
	1061		26				i,		COFE							у.			Failure to report UE 10
	r 055	Tuly74	26	59	ACT.			R	4 7.	ĺ		31	:		ř	1	} :	?	Dminter to test valves - subsystem
304	<u> </u>	July74	26	RF	ACT		g		RE.	-	CIP OH	÷	ï	,	5	ā		-	after reyair Lifetime problem with relay coil - isolation valve trip.
311	023	Bept 74	2€	JF.	SUR		<u>.</u>	Q	EM. EARCE		¥	<i>:</i> :				٤	7	:	nmergency lock test equipment

	No.							,—,						,	·,		,	,	 _			
		MUNICE HE SEE				A STATE OF THE STA	**************************************	4010 OCC	SZKISL	\$17. 4 0	- 19 July (\$12.80)	 (4) (4) (5) (3) (3) (3) 	PALLONE MOUS	क्षा अध्यक्ष क्षा अध्यक्ष	Security of the second	* : ख़िस २९ 'चीक्रमणि	・・・ さいかい (新)() () () () () () () () () () () () ()	URLAND ROOM Statement OF No.	2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2	JWK-Lini History	40 - A 4 - A	1 af 26
50	-3	19						Oy:	ter	Cree	k un	it l	Bi/R									
55		AO	Det	. 69	1	ا ا	Sti	Str		ם	U	FL. CR. RPS		BLK.		v	26	Y	Ţ,	Ь	c	First of a series of problems with control rod filter mesh
59		AO	Sep	. 69	()	SU	ទ ប		?	ł	AM.										Major transient, MSIV shut etc.
ľ		-	Ter	1.70	1	1	SU	SU		I		MSIV		LK		Y	3	Y	L	P	С	MSIV valves linking across seat due to excessive hanger strain
۱"		AO	ia z	70	1	ı		SUR		С	н	PS RPS		LK	51							Swage lock fitting leak
										0										c		Operator tightening fitting + scram
										D	С	W. ECC				Y	2	Y	L	R	С	Both condensers disabled
100			Tu l	. 70		2	OP	SUR		D		PS. RAC							L	R	С	Reset level of trip
1								l	1	P		L							L	R	i	New operating procedure
111	Ð	AO	Fee). 27 !0		2	OP	ACT		D		CAM.		bsc					L	R	С	Turbine control cam design problem • trip
										С	M	IV. CURB		BLK					L	P	С	Dirt in valve
1									l	С	Į	LTHA	1	MIS					L	C	С	Leakage
										P	0								I.	R	С	New procedure privilestal

DOCIGET	OCCURRENCE NUMBER	DATE	SIX NONTH PERIOD YO.	OFERNING CHAIR	DISCOVERY INTE	SER 10230	್ತಾರ್ಬ್ ಮ	SAUSE SUBSTALI	COMPONENT IN SE	FALLURA MODE	FAILUNG MECHANICA	RECOVERY MODIFY SUP	CONNOCT VOLE	COMPOSES IN A PPECPS D	CONCENTRATION	iateni/ Spontaneo: 1	INMEDIATION REVEATED/YOUSE	INTERAC SOUTERS CLOS	75% (471) (44) 2 af 20
•.		Sep. 2: 70	2	OP	BCR		м	M	MV		BRK					L	R	С	Bypass valve linkage rod broken - someone stood on it
114	40	Nov.7	3	SD	SUR		7		κv		LK		Y	2	?	L	R	c	Torms Exygen sample valve leak
117	AO	Dec . 70	3		SUR		1	A	AV		ADJ JAM		Y	2	Y	L	R	с	Vacuum breaker block valves jamming
135	UE	May 71	4		SUR		С	E	RT. RE		CIR					i. C	R	С	Resistor overhested + burn + broke + jammed timer relay
138	AO	Jun. 71			SUR		c	м	PS.		LOO:					L	R	С	•
139	UZ	Jun. 71	4		СТ		?		PP							s	G	ī	Collapscof package boiler flue
140	A0	Jun. 7	1 4		BUR		D	С	PM. CS		73		Y	2	Y	L	R	C	Water hammer/vibration in core spray
148	AO	Aug. 7	4	OP	СТ		D		TK. RD		OVP					s	G	С	Excess demand for rod waste storage while tank maintenance in progress
		Aug.2	4	OP	SUR		С	и	XV. RS RPS		lk					s	G	С	-
		July (4	OP	UR		c,	M	RV .025		JAM					L	R	c	•
		lag.1	1	OP	SUR		c	M	RE. CR. RPS		JAM					L	R	c	Dump tank (CR, water hold up level alarm relay binding

	WORKS.	THE .	· 1000年代 100	1977 - 1987 - 1987 - 1988 - 19	Section of the sectio	SDRIC	يجيمة المر	AUS A.D	TORENCE TO TE	ALCH BELLA	क्रायात्र ४० वस्ता प	HELLOWER Y THURSDAY	- 849	1995年美術教の第二	5. \$ 4. \$ 6. \$ 6. \$ 6. \$ 6. \$ 6. \$ 6. \$ 6	7 55 50 E	*************************************	Andrew Comments	
309	20	Sep.7	٠	OP	5UR		מ	\$	RT. RE. RHR		CIR		Ā	Ħ	N	L.	£.	С	Same as earlier relay failure - see 50-210-135
193	A.O	Dec. 7	5	SD	SUR		ם	U	ms IV LK		LK		Ÿ	4	23	L	₽	C	Same as earlier MSIV leakage
253	20	10v. 7	5	OP	ACT		0	O.	MS IV		JAM BRK					L	Þ	ū	Failure to equalise pressure across valves breakag - linkage bmack - failure to
154	NO.	Nov.7	5	SD	ACT		D,P	n	MV. RHIR		LK-		"	3	24	L	c c	Ċ	close oil leak to motor + burn out
	A 0	dov.7	7	ор	ACT		D? I.D		Hyd PP. AS		BRK					5	I	İ	Led to water hammer Air supply pipe rupture + loss of air + scrams + manual scram Other compressor could take over only after manual valve closed
157	10	Dec.7	5				?		CO RW		BI.K					s	G	I	Blockage of concentrator + plant outage +
									TK. RW								C		Excess activity in tank
	1				1		D		l								L		Lack of spare concentrator
159	20	Dec.7	5	OP	SUR ACT				SW PM TK.	EN			Y	4	2	CI	R	С	Empty fuel oil tank due to pump switch problem
								C P	M 0							E.			Added to check list
					1			D								L			New annunciator added

MUNICAL	OCCURRENCE NUMBER		DATE	DIX NOWTH PSH (OD IX).	OF ENALTHS POTATE.	DISCOVERN INSE	auk lous?	CAULE	CAUSE SURCIALS	COMPONENT TYPE.	PATIONE MODE	PATLURE MECHANICS	RECOVERY RECOGNICA	TOM NOWNO	COMPONEUTS ASSECTED	DONUS NOW.	latent/ Spoteaneous	NMEDIA DA / REVEA LE D/ COSCESS.	ANTEAU JOSEPHORORY	TERRATECIA 4 af 20
-,		Jas						I	А	PA		LOO					L.	R	С	Failure 3/4" vent line *
								ם	0	PН					Ì		L	R	С	orderly shut down
										PP							s	c	C	Due to poor pipe hanger installation, pipe hanger extra needed
164	۸٥	Dec	. 71	5	OP	ACT		D		SL CR	I			Y	2	Y	L	Ř	С	LOCA Failure to insert fully- seal leakage
167	40	Jar	.72	5	OP	ACT		٥	P								S	I	С	Shut down generator 1 a core apray 2
					1									¥	2 0	1881	aila	<u>. s</u> y	stem	<u>.</u>
					ı			Р	C								L			New procedure
168	NO	Ja	. 72	5	OP	ACT		0	5								S	I	I	Loss of buss power
								D	С								L			Extra circuitry to prevent problem
				•	1	1	•	P	0	1		1					L			Extra tagging procedure
																				Many plant subway terms but power
169		rei	. 72	5	OP	ACT		0	W,					Y	sev sys	eral tems	dis tri	simi P	lar	Operator removed 125 V S DC power + load drop
								D7		PH FW		osc						н		Feedwater pump scoop tube jammed

	7 0	205 1 09	104	182	180 246	177	176	173	
		AS							
		L ay	ľ	ay	pr.	ar.	Þr.	ar.	
		72	**	7.7	72	72	72	72	
		6	*9	6	6	5	5	5	· 医二甲基磺胺
And the second s	op	OP.			OP	ગ્ર		ାମ	10.7 m 10.7 m 20
	ΣI	ACT.		SUR	ACT	SUR		SUR	18.3 23.7 5.4 (18.3)
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	ი ი ა z	00	-	Ç,≓	ε			σ	A MAN TO STANK AND THE STANK A
	APF	uel	,3 ,	D# C SV	MO W	BY GEN	SM Sk eks	ES PR PPS	E # Constant March
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		COR IRT	STR	CIR CRE	CIR	£		DIRT	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
	Andrews and the second								a the Property of the Section Sec
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	A STATE OF THE STA			4		2			
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			16			L		L	क्षेत्रक्रित
		×		p P	R	9		ņ	1.00 mg
		-	-		^	c		c	
	S New procedure Baffles removed after Monticello incident	Fuel mundle misoriented - four people dhecked % &	bushings	Oracking in two seat		Two patteries had bad rells	Rod waste outside rank activity again	Scram fump volume level switch arain of 115	5 af 20

DOCKET	TO COMMENCE	NUMBER	20.00		SIX MOSCE.	04 91A17	DIRCOVES: THE	arriou	SAUGE.	CAUCIE STETTALC	COMPONENT IN 135.	FAILURE WATE	TARGON MODERNOS	RECOVERY MICO SECTION	JOHNON YOUR JOHNON YOUR	TUMPONESS, L. Ale PROFESS	3. 1.48(1) 3. 1.48(1) 3. 1.48(1)	JACKNEZ ARONZADELIJ	MEDISA SE REPURA DE LA TODOS SE	(1947) - 2 BB (1968) (1977) - 2 BB (1968)	TEV +1951TV- 6 af 2 0
196			Jan.	,	6	SD	ACT		С	E	ROT.		CIR DH					s	ī	1	Relay overheating
*			Jun.	, 4	6	SD	ACT				PP. ESWS		BRK LK HYD2					L	F	c	Rubber expansion joint hroke on pump start
							SUR		?		15 I V		LK					L	R	С	MSIV leakage again
190	1		Fun.	1	6	OP	ACT		D	S	rs.		i.r					s	I	1	Turhine cooling water tower temp, switch lost its gas charge
201	^	٥	7a1.7	14	6	OP	ACT		ຄ		PK. RW							L	R	۲	Outside waste tank again - high activity
263	^	0	lug.	1	6	OP	SUR		С	Ħ	PS.		LOOS					L	R	С	Loose nut - loss of torque in torque tube of PS
204	^	0	lug.	1	6	OP	ACT		С	E	re. Cs		DIRT					t.	R	c	Containment spray pump circuit breaker open circuit ? dirt
1		_							P	0			L								Added to check procedures
207	^		mg.	1	6	SD	ACT		С	m	GG RHR		BTK					"	R	С	Failure of containment isolation condensers
									1, D	0	SNUE GG	BER	NISS					L	R	c	Hissing snubber + full scale reading - sticking
									Р		rv		PAM					t	R	С	 motor valve too tight on meat

		5. 4			· · · · · · · · · · · · · · · · · · ·	-at	e ege da e e e e e		A TO ME TO THE TOTAL THE T	A Company of the Comp	ત ્રાપ્ટ જે ત ્રાહ્ય કે હથ	in the second se		新山大学 1757 新山大学 1757				a- 1114 1 af 2 0
		Sep. 7	6	OP	ACT.		ļ	RE A.S	Fight Browning (Spins Sp	Loss SCRI	7				U)	I		Scram fue to 1905e wire • multiple leakage in clemnit valves
21.5	20	Sep. 7				5	77	SL. SL. Pm		L.F		ï		7	13 (3)			Ligitî montepî system pump packing leak - maintepance
						Đ	۵	LCS W. PM		CIP				eliteratura de la facto de la facto de la facto de la facto de la facto de la facto de la facto de la facto de				Racking our directit breaker preventing other pump starting
	•	35 4.7	7			P 11		Mi. ₽S		CIR		*				R	đ.	Interchange of asolation condenser pressure switch lines
222 228	Ľ	Dec.7	1	OP OP	SUR	Б С		so P₽.		COR		}**	4, Œ	<u> </u>	5		c :	Release of rad waste
							c ,v	POW"							* 1			

		DATE:	10 NO NEW HERE	0758A	saki vanoseld	5270 1 HJB	SAUS).	CHYSERS TRAYO	COMPONENT TOTAL	FASSURE WORK	SATUME MEGHANING	ACTIVIZATION AND AND COM	COMMON TO A	COMPOSE C.C.	30 8 38 6 52 50 8 40 68 - 50 8 8 60	IADKAYZ PONZAS OCC	MRVEA TECH COURS	INCLINE) POROPEINE,	1507 (A. 1920) (1224) 8 af 20
227	2	Dec. 29	7	OĐ.	ACT		0/0		P							5	t	1	Operator opened door of relay cabinet - scram
							D	Ħ	RV.		EK BLX					×	ş	c	Electromatic relief valve failed to reseat (?why did it open) see below
							đ		RV		BRR		Y	4	¥	L			LOCA Rroken parts on 4 relief valves
							c	Ħ	KV.		LOOS	,				L	R	С	Rissing parts problem
							с	Ħ	ВМ		BRIT					L	R	с	Mode switch broken, prevented switch to start up mode - MSIV closure
						İ	С	77	MSIV		DIRI	,				L	R	С	MSIV failed to close
eninger Kabupatèn Kabupatèn							D	c	NV.		JAM					L			Pailure of isolation condenser, condensate return valve to open
135	~	100.73	7	œ	ACT		D	0	PGS		M.K					L	R	С	Stock gas sample line frose
236	**	73 73	7	C\$	ACT		,	7								5			Personnel overexposure in clean up after blow- down
237		100.73	7	æ	ACT		c	5.	EN.		EIR					L	R	c	Failed open circuit
Account and a second a second and a second and a second and a second and a second and a second and a second and a second and a second and a second a																			

							4 7 2 2 2 2			A STATEMENT AND A STATEMENT OF THE STATE	n profita		A CANADA CANADA CONTRACTOR OF A CANADA CANADA CANADA CANADA CANADA CANADA CANADA CANADA CANADA CANADA CANADA C				- A -18 - 18 - 18 - 18 - 18 - 18 - 18 - 18 - 18			9 af 20
	**		.73	F.c	(JeP	ACT		ų li	F								eg.	I W	3-4 K.	Operator started feed pum with too low feed temp, 5 other convirences
		Perc	.71	\$ in		SI		£2		RE. PPS RUS				7	2	¥	ī	B	<u>.</u>	Circuit breaker ranked ou problem again
251	200	·	.73	ð	cs	sz: a		D.	9	RU.		JAM					L	Þ	đ	Isolation condenser condensate valbe jam agai
252	340	101	.71	5	st	SUR		Э		act.		JAM			5	:•	1.	P	Ċ.	Cilde pin for solenoid cocked, jammed - remade with stronger weld
	**	e-	.73	ė				?	;	V		L¥					S	I	I	Chromated water leaked fr trick tank valve + radio- activity release
26 3	-	۴,	73	5		SUR		D.	5	w		LF		?			s	ı	I	Vacuum relief valve leak
249	140	١,	73	•		SUR		7	1	SI	•	E.X		ij		•	L	R	c	As in 1971
XI)		-	73	ŧ		SUR		?		SL.		L.F		7			1	Ą	٢	Manhole seal in containme leaked
	30 20	۳	m. 7			SUR		0	0 P 0	GEN				Y	2	Y	L	P	C	Did not set up generators for synchronization
	3-1		un. 73	e		ACT		o	0											Omitted to take coolant sample
	3.	1	un. 73	9		SUR		C	Ε	RE. CS		DH CIB					i	9	-	
	1							Ċ	Е	1.5	1	Loos					:.	þ	-	

المعتبي الم				1											-				
POCKET WUNNESS		u w	14.1、10.1 KGH 14.1、10.1 r>14.1 KGH 14.	0 53A - 1 4 6 6 6 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	PINCONER PEC-	SINH DEPT	CA USO	TOWEDHET BERKE	ରି ବଳ । ଏହିଲିଆନିଆନିଆନ୍ତ୍ରିୟ	ROW SHOUTE	*A.1.39*g. WENDERS	L'ORDON LEASTON	2018/8/10 PERSE. \$48.5% 11	1943 (44 4 V	AUDERTANO:	NATEMBY SPONEASE OUR	TO STABLEST VERSE	861 (686) 48 7 9 3 (98	152179394365 10 af 2 0
33	73-1		8	OP	кст		?		GEN		GOD					\$	I	I	Light ning wrecked transformer +no fuel transfer pump
203	20 73-1	Jul. 5 73	۰		SUR		С		sl. Ms IV Re.		LK. Tim					L	R	С	Desh pot seal leak * timing error
302 309	ر ب-در	As1.7	8	OР	ACT		С	•	CS SL. CV PH		e.K					ន	I	1	Leak 5 gpm see LOCA
305	þ	Pal . 7.		CS OP	SI		P D	0 \$	SH				Å	6	¥	L	R	С	Shock absorber seal failure
	-	ing . 7.	•				D		TR. RW Cond	ent 1						L S	R	C I	Excess radioactivity in outside waste tank again
714 714	3	ng . 7:]		SUR		D	Ū	GEN MO		N N		7			L	5.	С	
31.9	3		8	\$D	ACT		M D	^	72. F 72.11				Å	2	Y	L	R	С	Noth power busses out - setting of transfer relay Noth generators out
							,	0											

	The Co	ala.						····	,					,					
DOCKLIN NUMBER	OCCURRE. CA. NUMBER	DACE	SIX MOLTE PERIOD TO	OFERALLO COME. OF PLAS.	DIRCOVERS TYPE	SERIOUS:	CAUSE	CAUSE FTANASE	COMPOSES SYSTE	ATLURE MODE	PATITION MECHANICS	RELOVERS NECTALIZA	JOHNOL MAIN REFERI	COMPONEDC A POPENED	SOLAN TECHOO FOOL TO AROUS	IACENIZ GIONDANECTO	IMMEDIALAZ KIVEA 1207 TAROAL	18.11.25.17. JOHN BEN 19.40.	11. markini.k. 11 af 20
320	73- 20		8	SD	ACT		?		RE. MV.		-					L	R	с	New condensate return valve
	73- 21		8	S D	SUR		D	s	RHR SL. SH		LK		Y	21	Y	Ľ	R	c	Snubber seals again
	73- 22		8	cs	SUR		?		MSIV		ΓK					L	R	С	
330 350	NO 73-	Det.73	9		SUR		С	М	PS. ADS		STK					L	R	С	
331	23 23- 23-	Sep.73	8		SUR		?		MSIV		W E.K					L	R	с	See above
332	24 73-	Sep.73	8		SUR		?		RE.							L	R	с	
335	25				SUR		D		RHR MSIV SL	,	ľĸ		Y	2	Y	L	R	С	2 more MSIV's leaking - but this time through
337	10	Det.73	9	ΟÞ	ACT		0	P								s	Ī	I	stem packing
349	73- 26						0 0	000			1	tri	of p os - inc	1	[5 5	I I I	0 0	
							O P	0								S L	I R	c c	
	<u></u>							<u> </u>		l			L_			<u> </u>	I		
DOCKIST NUMBER	OCCURRENCE NUMBER	DATE	SIX MONTH PERIOD NO.	OFSEALING FIRES	DISCOVERY IN A	SERIOUS?	OA COS.	CAUSE SURCIACI	COMPONENT DUE	FAILURE MODE	SPINATURE MENTAR	RELIDERY YESTER TEST	COMMON ROLE	COMPONENTS ANTECESO	CONTRACT NOTE	IATENT/ SECURATEOTO	EMMSID CALLEZ/ ARVEM FRIEZ/COTT.	INITIALU JON FIFTISE	15.1783.0105 12 af 2 0
339		Det.73	t —	OP	SUR		c,	н	RV.		COR					5	ī	I	
342	.0	Det. 73	9	ОР	ACT		c	м	HE.		СK					G	 		Radiation release, closed cooling water system leak
							D	U								L			14,500 gal,
346	10		9	OP	SUR		P D	S	SII.		LK			1		L			Rergen Patterson arrestor again
363	90	9ec. 73	1		SUR		?		PS. RPS		brif		Y	4	Y	L	R	С	ĺ
365 366	2	Jan.8 Jan.4	9	OP OP	SUR	l	? C,	0	rs. C Ps.		brif brif		Y	2	Y	L	R	С	
							D, P				VD.T				* 				
367 368	74-3	Jan.13	9	cs cs	SUR		D C	S	BH		Lĸ					L	R	С	Bergen Patterson snubber again Valve packing back again
369	1	Jan. 22	1	SD	лст		n	J	THEF	i						I.	R	c	as Sep. 73 Operator used too much
370	4-7		9	Str	ACT		2		NO2		brit					1.	R	_	NO2 - misjudged amount left - delivery date
1	1 '	1	1	1	1	1	li .	i	RP5		1	1	11		1		1	1	

	44	,																	
DOCKET NUMBER	DCCURRE LOR NUMBER	Date	51X NO.1H PRETOT 10.	Dribbutti - Chhai Dribbutti	presentation of the	SERIO'.:	عزمت هن	SALACTOR TO PED AC	COMPOSITION OF THE	BCON RELITYS	FAILURE MEGRADIUS	MONUMENT MECHANISM	STEERS STORY	1400 do 4V 1400 do do	बार्डस्ट ^{स्ट्र} टनस्ट अस्टार १८५सटा	CTE 40 MOTORIO E CONTRACTORIO E CONT	PREMISON OF BASEA	2907 14. 1808 ?d.≴*1€*	CELOTRIPOTON 13 af 20
378	73- 31		9	ОР	ACT		М	I	χ.				Y	2	Y	s	I	I	Loss of DC power
379	73- 32		9		SUR		a	U	KV. MSIV		STK DIRT					L	R	С	Overtravel - pr. transient
380		0v.21 73	9		ACT		?		RE. ADS.		рн					5	G	Į	
185	73	Dec. 73	9	OP	SUR		I		NH.							į.	R	C	Poor sedered contact
188	14	lov.73			ACT		D		rı.		rin					ſ.	R	c	
								l	HE. RHR										
350	10	Dec. 73	9	OP	ACT		D	٥	PP. RW		BRK					S	G	Ċ	Radioactivity release after pipe freeze - than
400	74-8	Jan.17	9	нѕ	SUR		?		ri. RHR		orif TIM	È	Y	3	Y	L	R	C	
403	74-4	San. 22	9	нѕ	SUR		D,		KV. MSIV		STK					E.	R	С	
407	4-9	Van.31	,	ОР	SUR		P D	s	PS.		prif	t	Y	2	¥	L	R	С	As 73-39
408	4-	eb.8	9	OР	SUR		D		es.				ĭ.	2	Y	L	R	Ç.	As 73-30 - these are
	10								ľ										Barkdale PS's
																			_
	<u> </u>	<u> </u>		<u> </u>	<u> </u>			<u> </u>							<u> </u>				

DOCKET	OCCURRENCE NUMBER		DATE	SIX MONTH FERTOL (1).	OLERANDO IN ALE.	DISCOVER: 1:15	STR 10CC:	CA D.A.E.	CAUSE SUNTAINS	COMPONETY TYPE	FAILURE MOUE	PAILURE MESSANIOS	RECOVERY SECTIONSES	JOHNON MULLI Be FECT	COMPONENT.	COMPANIE (COMPANIE)	IACENT/ SPOTTANEOT	INMEDIACE REVENIENT COLES.	1M:1A:7 30M:8[40]?8	1820 - 1811 - 14 af 20
415	74-	reb	.15	9	OP	SUR		D	s	νv		5TK		Y	4	Ÿ	7.	R	c	
	79- 14													¥	2	Y				
419	74-	reb	.28	9	ОP	SUR								Y	4	ŭ				As 74-11 & 74-14
420	74-			9	As	4-11								Y	4	Y				As 74-11
	74- 2		λs	for	74	1,		74-	b ,	74-	0									
425	4-	reb	-18	9	OP	ACT		11	В								r			Cleanup system isolation valve inoperatable
								?		ív.							м			- Manual trip 'blunder' failed to close
428	7-	ta r	.7	9	S D	act		?		SW.							Ĺ	R	c	Loss of electrical power on two husses
129	4-	a.r	. 8	9				ח	s	P SH				¥	7	ч	L	R	С	As 74-3
130	4-	lar	.9	9	Сs	ACT		D	7	εG.		STK					L	R	ď	Gauge sticking -
								0	0								s	ī	٦	Omitted to check recorder

роски т Кижев	NONSER NONSER	DATE	5.00 40,843 5.00 40,843	CARL CONTROL O	TIT TOVERS TYPE	SHOING	Alexandria Alexandria	CAUCE SOFTALE	ent landouner	BLOW BALLEA	CONTRACTOR CONTRACTOR	RATENSIAN LANGUER	Same same	adit basada Antaria	10 8 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	DATENTA PROGRAMMONA	MANAGE STATE	40 Tubu 8 TM 7 M 1 TM	раниргуу. 15 af 20
431	74- 20	Mer.l	9	RS	SUR		I, P		SL. MSIV		LK		Y	4	Y	L	R	С	Leaking because seal was cut to install, instead of dismantling
	74- 21	Mar.1	9	OP	ACT		?		XV. PG							5	ı	I	Rypass valve open
	74- 22	Mar.1	9	OP	SUR		D		DS. C		Dri	t	Y		13	L	R	С	As 74-1
449		Mar.l	9	OP	SUR		D	s	FS. RHR		Dri	t	ň	2	Y	L	R	С	
156 168	74- 25	Apr.9	10	OP	SUR		?		W. C		TK		Å	2	Y	Ե	R	с	
57, 540	74- 24	Apr.	10	OP	ACT		0	o	FL. OGS							5	1	1	Omitted to measure off gas filter activity
660	74- 26		10				С		PM. ESW							L			Emergency service water pump failed to operate
	74- 29	Apr.1	10	Ber	en :	Patt	E SOT	sho	ck a	b s oı	ber	aga	in Y	3	Y				
676	74- 28	Apr.1	10	RS	SUR		Ħ	1	LS MV. CS							L	R	С	
684	74- 29		10	RS	SUR		D		PS. ADS		Dri	t	Y	2	Y	L	R	с	

DOCKET NOVEER	OCCURRENCE NUMBER	DATE	SIX MONTH PERIOR TO.	OF PIANS	DISCOVERT INTE	SER ICTES	CAUSE	CAUSE SPROTASE	GERT CHIEFLOGMOD	FAILURE MODE	FAILURE MOCHANION	RECOVERY MECHANICA	COMMON NOTE BRYBOT	COMPONY LE	CONTOCT POLE	IATENE/ SPOSTATEOTI	TWEDELTS/	INITIALS SOMERI POT ONE	12.1 B1/(1.0) 16 af 20
486		Apr. 24	10	R5	SUR		c		MV. ADS,		CRK					L	R	c	Crack in butterfly valve disc
500 509	74- 30	tay 14	10	r.p	SUR		11		PS. TURE		Drii	t				L	Ð	С	
	74- 33	lay 21	10	RF	SUR		P		TI. ADS		TIM		Y	2	Y	L	R	С	7 seconds extra delay on ADS
	74- 52	lay 21	10	RF	SUR		?		PS. CS		CIR					L	R	С	Merc#oid pressure switch failed open
	74- 31		10		Ber	en 1	atte	rsor					Y	2	Y	L	R	С	
512 548	74-	28	10	RF			C		PEN		LK					S	1	I	Leakage in instrument penetration (LOCA-minor) (0.02 gal/nr.)
520		125	30	SU	ACT		D	iod,		Ps. CS			Y	2	Y	7,	R	С	Reset trip point
							D												Several switches on one alarm
1	l			1			0									t		'	Operator did not reset
529	74- 35	Ju1.5	10	SU	SUR		D	S		PS.			Y	4	Y	L	R	C	Barksdale switches, As 74-1
	36	July	10	ספ	SUR		D	ន		PS. RPS						I,	R	С	Another Barksdale switch
545	74	July	10		SUR		D	0		w. c			47	2	Y	Ľ	R	C	Activation of main line drain isolation valves omitted

DOCKET	ОССЕКВЕТЕ ИОМЕКЯ	36.25	NOT WORTH	SEAS	piacovnak inte	RENIOUT:	CAUSE	STATE SET BEST	SOMBOTES : PERF	AILURE MODE	HATEURE MECHANICAL	HELLOVERY MICHAEL LOM	CONSOL 1 L. S. BHEDDE	COMPOUNTIE	STREET NOTE:	ia tentz Pionakonu	immed la . 27 Revente . 2300	1987 (A1808) 1988 (A1808)	JENTRIPHION 17 af 20
8 8	8 2	ă	48	ે ઠં	id.	<u> </u>	5	5	Ď,	₹.	4.	32	7 5 1 5	00.4	(i e	15 Å	M H	48	17 81 20
546	74- 37		10										Y	4	Y				Barksdale switches again. As 74-1
552	74- 40		B 10	rgen	Pat	ters	n a	ain						1					
557	74- 30	July 74	10				D.	s	HV MSI	,	TIM					L	R	с	New activation design on these valves
558	74- 39	July 14	10	R₽	SUR		D	Z	PS.	Dri	t		Y	4	Y	L	R	С	
559			10	OΡ	SUR		D	5					Y	2	Y	L	R	С	Barksdale switches again as 74-1
560			10										Y	4	Y				Ditto
564		Aug.8	10		ACT		?		PM. RPS										
566	74- 44	Aug.9	10	λs	74-		В	rks	ale	SWİ	che	•		ì,					
568		Aug. 2	10											1					
582	1	Aug. 26	10	OP	SUF		D	s,	w.		MAL		Y		N	L	R	С	Teflon 'growth' in
588	74- 47		B 10	rgen	Pat	ters	n s	· -	C abs	rbe	8			2					hinge
5 96	74- 48	Sep.	10	ОP	ACT		1									5	1	ī	Scram - load rejection
	-	25					D	z	RHR				Y	2	Y	L	R	С	Both heat removal system.

DOCYST NUMBER	OCCURRA OE WUNDER	DATE	SIX ONCH	0: 5544 - 173 - 174 - 1 0: 1748	DISCOVERY TATE	Serious:	CAUZE	CAUGS: SUHT. ASS	SEMI DIEMONIOS	FAILURE MODE	TATEMENT OF SALLON	NO CORRY MEDIAN CON	JOHNOR MODE APPEND	COM POSSILS A N - E 2 PEO	3000 10 1000 3000 10 1000	IATANI/ JPONEMEDIN	IMPODIATELY RETEALED/10001		DEFORMAN, 10% 18 af 20
597 599	74- 49 74- 50		11 11		ale ACT	swi	ch a		CB MV. C		BLK			1		L	P	С	
602 603	74~ 52 74~ 55		11 11		ale SUR	swi(ch a	gain	PM. CS					1		L	R	С	