



RIMPUFF. Users Guide. Version 20

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RIMPUFF

Users Guide

Version 20

S. Thykier Nielsen and Torben Mikkelsen

**Risø National Laboratory, DK-4000 Roskilde, Denmark
October, 1987**

Risø-M-2673

RIMPUFF
Users Guide
Version 20

S. Thykier-Nielsen and Torben Mikkelsen

Abstract. An operational puff diffusion model, RIMPUFF (Risø Mesoscale PUFF model) has been developed at Risø National Laboratory to provide risk and safety assessments in connection with e.g. nuclear installations. The computer model releases a sequence of puffs with individual pollutant and heat contents, then calculates the time-dependent concentration field, which is provided by the collection of puffs. The puffs are advected through a three-dimensional grid on the basis of a time sequence of measured horizontal wind vectors. The model code is written in standard FORTRAN 77 for a Burroughs B7800 computer. The code also runs on a VAX or a IBM computer. The input data consists of two data files with parameter specifications. In addition, data files with precalculated wind fields and population distribution can be provided. The model outputs for doses, puff positions wind and concentration fields consists of disk files and printed data. Graphical presentation of results is based on a specific program, which creates background maps, wind vector plots, puff plots and isoconcentration contours.

October 1987

Risø National Laboratory, DK-4000 Roskilde, Denmark

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TITLE: Risø Mesoscale PUFFmodel, Version 20

R I M P U F F

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CONTENTS

	Page
1. INTRODUCTION	5
2. RISØ PUFF DIFFUSION MODEL	6
2.1. General characteristics	6
2.2. Present model	7
2.3. Gamma dose model	8
2.4. Wind field calculation	9
2.5. Dispersion Parameters	9
2.6. Dispersion height	10
2.7. Height of the inversion cap	10
2.8. Deposition parameters	11
3. USERS GUIDE	16
3.1. The input data	16
3.2. Flow chart for running RIMPUFF	16
4. Description of the INDATA file	18
4.1. PRIMDA - Namelist	18
4.2. RELDAT - Namelist	24
4.3. STABDA - Namelist	25
4.4. GAMDA - Namelist	29
4.5. DOSDA - Namelist	30
4.6. Example of the INDATA file	32
5. Description of the WINDDA file	34
5.1. WINPAR - Namelist	34
5.2. Wind data record	38
5.3. Example of the WINDDA file	39
6. Description of the BEFDA file	41
7. Description of the output files	43
8. EXAMPLES	45
8.1. Example no. 1	45
8.2. Example no. 2	77
8.2.1. INDATA file	77
8.2.2. WINDDA file	79
8.3. Example no. 3	102

8.3.1. INDATA file	102
8.3.2. WINDDA file	104
8.4. Example no. 4	120
8.4.1. INDATA file	120
8.4.2. WINDDA file	122
8.5. Example no. 5	127
8.5.1. INDATA file	127
8.5.2. WINDDA file	129
8.6. Example no. 6	132
8.6.1. INDATA file	132
8.6.2. WINDDA file	134
8.7. Example no. 7	140
8.7.1. INDATA file	140
8.7.2. WINDDA file	142
REFERENCES	145
INDEX	149

1. INTRODUCTION

The atmospheric diffusion model RIMPUFF is originally implemented on the Risø Burroughs B7800 computer in FORTRAN77 language (B7800 version). The following gives a brief introduction on how to prepare input data and how to run the program. The model outputs are disc files and printed data. Graphical evaluation of the output requires a graphic program which creates background maps, wind vector plots, puff plots and isoconcentration contours. Two program systems are currently available at Risø: PUFFPLOT3 which is based on the Risø Interactive Graphics System (RIGS) and Uniplot which is based on the UNIRAS graphics software package.

2. RISØ PUFF DIFFUSION MODEL

2.1. General characteristics

The shortcomings of a standard plume model can be summarized by its ability to handle non-stationary and non-homogeneous flow- and turbulence situations very poorly. When dispersion is modelled out to distances larger than say 20 km, these shortcomings become progressively more important. The area over which the plume moves is more likely to display significant inhomogeneity, such as, e.g. land-water interfaces. Also, as the advection time of the cloud increases, the probability for temporal changes to occur in the the flow and turbulence fields is more likely.

Standard dispersion modelling of non-homogeneous and non-stationary situations is inhibited by the multitude of characteristics which inhomogeneous and instationary flow situations can take. Flow models to be used to handle many of these situations are also either unreliable, expensive and time consuming, unreliable - or a combination hereof. The quantity and the quality of meteorological data available to drive such a model may also vary greatly from site to site.

The Risø-Mesoscale-PUFF model (RIMPUFF) is designed as a modular system in response to these considerations. The core of the model consists of a bookkeeping algorithm that models a continuous release by a series of consecutively released puffs. At each time step the model advects, diffuses and deposits the individual puffs in accordance with the local meteorological parameter values. Concurrently, it monitors the resulting concentrations in user-specified grid points. The local meteorological parameters and the resulting dispersion parameters are organized in sub-programs, which can readily be changed or modified according to the needs and opportunities in the actual modelling situations.

The puff model is structured such that it handles multiple simultaneous sources and its 3-dimensional monitoring grid can contain several hundreds of puffs. Release points can be located anywhere in the grid and can be specified individual release rates, release times and heat production.

2.2. Present model

In its present form (Dec. 87) for treatment of dispersion over non-homogeneous terrain, RIMPUFF calculates the puffs location on the computer grid by computing their movement during finite time steps, using an interpolated wind field. The latter is based on an objective wind analysis from the available wind measurement stations. Growth of the puffs are computed from simultaneous measurements or specifications of the atmospheric turbulence intensity or/and stability in the dispersion area. The height of the inversion cap (through which pollutants is not assumed to pass) and the source height are specified by the user. Grid spacing for collection of data may vary from meters to kilometers, and time durations for the release can vary from seconds to hours.

A parameter controls the amount of reflection/absorption of the pollutant at the surface. (Total reflection is normally assumed).

The model calculates the concentration at each grid point by summing the contributions from surrounding puffs at each advection step. The grid concentrations/doses can either accumulate or simply be updated with the latest instantaneous value.

The model output consists of individual puff locations and grid concentrations at time intervals specified in the

input data. These data can then optionally be evaluated by an interactive graphic program, which creates background maps, wind-field plots, puffplots and iso-concentration contours.

More detailed information on the RISO puff diffusion model and its use of parameterized puff diffusion can be found in MIK84 and Mik 1987b.

2.3. Gamma dose model

A gamma dose model is included in RIMPUFF. It is based on the semi-infinite cloud model with correction factors given in SLA68. The model calculates the concentration in the centre of each puff and the distance, R, from the puffcentre to each grid point.

The gamma dose in the grid point is then calculated using the following formula:

$$D_{\gamma}(R) = \sum E f(E_{\gamma}) E_{\gamma} 0.2292 GKOR(\sigma, R/\sigma) GKOR1(\sigma, E_{\gamma}) X_{puff}(0,0,0)$$

where

GKOR($\sigma, R/\sigma$) - correction factor for variation of doses with distance. (SLA68, Fig. 7.14)

GKOR1(σ, E_{γ}) - correction factor for variation of doses with photon energy. (SLA68, Fig. 7.14)
This factor is >1 for $E < 0.7$ MeV
and <1 for $E > 0.7$ MeV

R Distance from puff centre to gridpoint.

$f(E_{\gamma})$
 σ Frequency in energy groups.
 $\sqrt{\sigma_{xy} \cdot \sigma_z}$

2.4. Wind field calculation

The mesoscale wind field over a non-homogeneous region is estimated from a network of available observations by the method of objective wind analysis. A $1/r^2$ -weighting function, where r is the distance from the grid point to the measurement station is used here for the interpolation (STA74).

2.5. Dispersion Parameters

Expansion with time of a single instant puff is fundamentally related to the relative diffusion process. In the surface layer, this is most conveniently described as a function of the local turbulence intensities and downwind distance (see e.g., ref. Mik87). Therefore, the optimal data set for driving the model should include turbulence intensities. Alternatively, in the absence of such data, standard plume dispersion information can be used as, e.g. the Pasquill-Turner system or the Karlsruhe-Jülich system. The latter is as an option implemented in the present version of RIMPUFF. These height-dependent dispersion parameters are shown in Table 2.1. The corresponding stability is in the case determined from the Klug/ Manier-system (KLU68, MAN75).

In table 2.1 the σ -curves are described on the form

$$\sigma(x) = a \cdot x^b$$

where x is the downwind distance and a and b are stability-dependent parameters. The formula is applicable for

$$.01 < x < 20 \text{ km}$$

From this equation the sigma-values after a given advection step ΔX and a given local stability are obtained by differentiation as

$$\sigma(X+\Delta X) = (\sigma(x))^{\frac{1}{b+a} \frac{1}{b} \cdot \Delta X)^b$$

2.6. Plume rise

Since the succession of puffs resembles a continuous release, the formulas used to determine the effective source height after plume rise are taken from standard plume models (PS85b).

The final riseheight for each puff is a function of the atmospheric stability and windspeed at the time of release. The windspeed is adjusted to the release height using an exponential, stability dependent profile, shown in Table 2.2.

2.7. Height of the inversion cap

The height of the inversion cap, the mixing height, varies with stability (KLU68). When the stability changes, the final height is changed accordingly, however, it is never allowed to decrease. For a grid with different stability regions and thus different mixing heights the highest value is chosen to apply for all the stability regions.

Neither the final rise height nor the value of σ_z is allowed to exceed the mixing height chosen.

2.8. Deposition parameters .

Dry deposition is calculated using the source depletion concept. The dry deposition parameters are chosen for the individual puffs according to type of isotope, atmospheric stability and wind speed. Typical values, taken from THY82. are shown in Table 2.3.

Wet deposition is calculated using a wet deposition parameter depending on type of isotope and the actual rain intensity, and taking account of the rain duration. The rain intensity is allowed to vary with time and space. Based on the relevant sets of available information a 'rain field' (field of rain intensities) is again calculated using a method of weighted interpolation on a regular grid. A $1/r^2$ weighting function is used in the present study where r is the distance from the grid point to the measurement station.

Table 2.1. Karlsruhe-Jülich diffusion coefficients as function of stability category and height

Height (m)	Stability Category	Diffusion Coefficient			
		Py	Qy	Pz	Qz
50	A	1.503	0.833	0.151	1.219
	B	0.876	0.823	0.127	1.108
	C	0.659	0.807	0.165	0.996
	D	0.640	0.784	0.215	0.885
	E	0.801	0.754	0.264	0.774
	F	1.294	0.718	0.241	0.662
100	A	0.179	1.296	0.051	1.317
	B	0.324	1.025	0.070	1.151
	C	0.466	0.866	0.137	0.985
	D	0.504	0.818	0.265	0.818
	E	0.411	0.882	0.487	0.652
	F	0.253	1.057	0.717	0.486
180	A	0.671	0.903	0.025	1.500
	B	0.415	0.903	0.033	1.320
	C	0.232	0.903	0.104	0.997
	D	0.208	0.903	0.307	0.734
	E	0.345	0.903	0.546	0.557
	F	0.671	0.903	0.484	0.500

The sigma values as function of distance, X, is given as:

$$\sigma_y = p_y x^{q_y}$$

$$\sigma_z = p_y x^{q_y}$$

The formulas are valid for $10 \text{ m} \leq x$ and $x \leq 50 \text{ km}$.

Reference: BUN82.

Table 2.2. Wind speed profile.

Stability	A	B	C	D	E	F
P _u	0.07	0.13	0.21	0.34	0.44	0.44

The wind speed at height h (h > 10 m) is calculated from:

$$u(h) = u_{10} * \left(\frac{h}{10} \right)^{P_u}$$

where u₁₀ is the wind speed at 10 m height.

Reference: PS85b

Table 2.3. Typical values for the dry deposition parameters as a function of stability and wind speed. Based on THY82.

Dry deposition parameter, v_d (m/s)

<u>Stability</u>	A	B	C	D	E	F
Wind speed (m/s)						
$u < 1$	0.4	0.3	0.3	0.2	0.07	0.05
$1 \leq u < 3$	1.0	1.0	1.0	0.7	0.30	0.20
$3 \leq u < 6$	1.0	1.0	1.0	1.0	0.60	0.60
$6 \leq u < 10$	1.0	1.0	1.0	1.0	1.0	0.70
$10 \leq u$	1.0	1.0	1.0	1.0	1.0	1.0

3. USERS GUIDE

3.1. The input data

The input data consist of two data files with the logical names INDATA (FILE 1) and WINDDA (FILE 2) and a file with the population data (if collective doses must be calculated), BEFDA (FILE 8). INDATA contains the necessary simulation parameters to run a puff simulation. The wind fields necessary for advecting the puffs are created according to the parameters and meteorological observation data defined in the WINDDA file.

If the wind field is derived from a flow field model two further input files are needed:

FILE30: Wind speeds in the PUFF grid
FILE31: Wind directions in the PUFF grid.

(For a description of these files see the subroutine LINCOM in VER20/RIMPUFF.)

3.2. Flow chart for running RIMPUFF

Set up parameters	Prepare the grid size for your simulation. Define the lower left corner of the grid in UTM-coordinates. Find the coordinates of the source(s) and the wind observation station(s) in UTM-coordinates.
	Set up the INDATA parameters.

Set up the WINDDA parameters.

Create a file, BEFDA, with population data.

Running
the

Prepare a set of wind observation records.

RIMPUFF code

Create the data files INDATA and WINDDA.

Run RIMPUFF as a batch job.

Obs! 132 chs
output.

Evaluate printer output.

Run the graphical evaluation program.

4. Description of the INDATA file:

The INDATA file contains the parameters essential for the puff simulation and the output of the results. First the different parameters will be explained followed by an example. The parameters are read by the program using the Fortran NAMELIST facility. The INDATA file is divided into five separate parts and must be defined in the following order:

1. PRIMDA
2. RELDAT
3. STABDA
4. GAMDA
5. DOSDA

4.1. PRIMDA - Namelist

The following parameters must be assigned a value:

- TITLE** = '<Text string of max. 72 characters defining of your current problem>'
- ICOLS** = <integer value of number of columns in the concentration grid>
1 < ICOLS < 100
- JROWS** = <integer value of number of rows in the concentration grid>
1 < JROWS < 100

- KPLANS** = <integer value of number of vertical plans in the concentration grid>
1 < KPLANS < 2
- DELX** = <Decimal value of the horizontal grid size (m)>
- DELY** = <Decimal value of the lateral grid size (m)>
- DELZ** = <Decimal value of the vertical grid size (m)>
- KOORD** = <Selector for coordinate system>
KOORD = 0 : Grid units
KOORD = 1 : UTM-coordinates
KOORD = 1 is recommended
- XUTM** = <X coordinate for lower left corner of grid in the UTM - coordinate system. Unit: km>
Only relevant for KOORD = 1 !
- YUTM** = <Y coordinate for lower left corner of grid in the UTM - coordinate system. Unit: km>
Only relevant for KOORD = 1 !
- TDEL** = <Integer value of number of seconds before detection of air and ground concentrations begin>
Concentrations are =0 when T<TDEL
- CHEMIN** = <Decimal value of minimum concentration of interest>
- NTADV** = <Integer value of the number of seconds between each advection step>

TAU = <Integer value of the number of seconds between release of each puff>

TAU must be an integer multiplum of NTADV.

TAU = NTADV is recommended.

Remember that max. number of puff in the grid at any one time must be less than 300.

To obtain resonable computing times the number of puffs must be less than 100.

MAPTIM = <Integer value of the number of seconds between output of concentration- and wind fields to printer and disc>

REFLEC = <Decimal value for the reflection of each puff>

NRELSE = <Integer number of seconds to the stop of all releases>

IDMP = <Index of the i'th position in the concentration matrix for the printer output of concentration data>

$0 < IDMP < ICOLS$

$IDMP = 0 \Rightarrow$ no printer output

JDMP = <Index of the j'th position in the concentration matrix for the printer output of concentration data>

$0 < JDMP < JROWS$

$JDMP = 0 \Rightarrow$ no printer output

KDMP = <Index of the k'th position in the concentration matrix for the printer output of concentration data>

0 < KDMP < KPLANS

ISMODE = <Stability index mode directing the computation of lateral and vertical standard deviation of each puff>

ISMODE	Sigma-Y	Sigma-Z
1	Pasquill Turner (A,B...F)	Pasquill Turner (A,B...F)
2	Pasquill Turner (A,B...F)	Vertical direction deviation
3	Lateral direction deviation	Pasquill Turner (A,B...F)
4	Lateral direction deviation	Vertical direction deviation

PENTPF = .TRUE. or .FALSE.
.TRUE. : Pentafication of puffs
.FALSE.: No pentafication (Default)

SYMPEN = Minimum sigma-xy value for pentafication.
Default value : 300 meters

ROCKET = .TRUE. or .FALSE.
.TRUE. : Exhaust calculations for rocket
(Vandenberg AFB.)
Remember: All values of ZMTAB must be equal (= ZM)
.FALSE.: Normal PUFF calculations.

IBFOPT = Option for calculation of collective doses:
0 : No collective doses
1 : Collective doses from inhalation
2 : Collective doses from gamma doses from deposited material
3 : Collective doses from gamma doses from puffs
4 : Total collective doses
100 : Population distribution in grid
NOTE! Calculation of collective doses or population distribution possible only when KOORD=1 i.e. UTM-coordinates are used.

CALCSY = .TRUE. or .FALSE.
.TRUE. : Calculation of sigma-y values along the X-axis from tracer concentrations in air.
.FALSE.: No calculation of sigma-y (Default)

INPRNT = 'YES' or 'NO'
YES : Logg of input data
NO : No logg of input data

OUTPUT = 'OUTPUT' or 'NOOUTP'
OUTPUT : The concentration in air and the puff position file with the logical name OUTAIR is created on disc. (File 10)
NOOUTP : No air concentration and puff position logg file is created.

OUTMOD = 'INST' or 'DOSE'
INST : The instantaneous concentrations are calculated.
DOSE : The time-integrated concentrations are calculated.

OUTWFD = 'OUTPUT' or 'NOOUTP'
OUTPUT : The windfield file with the logical name
WFIELD is created. (File 12).
NOOUTP : No windfield file is created.

OUTBEF = 'OUTPUT' or 'NOOUTP'
OUTPUT : A file with collective doses is created,
if $1 \leq \text{IBFOPT} \leq 4$. (File 88).
If $\text{IBFOPT} = 100$, a file with the population
distribution is created (File 89).
NOOUTP : No file with collective doses or population
distribution.

ITAPIN = <Selector for output on tape for KfK>
ITAPIN = 0 : NO tape with concentrations
ITAPIN = 1 : Tape with concentration for each
MAPTIM.
The data are written on file 20.

4.2. RELDAT - Namelist

The following parameters must be assigned a value:

PUFPTX = '<Text string of max. 72 characters of your current source specifications>'

NRMULT = No. of sources (≤ 25)

For each source the following should be given:

XSOURC(I) = X-coordinate of source no. I in km in the UTM-coordinate system (or grid-units).

YSOURC(I) = Y-coordinate of source no. I in km in the UTM-coordinate system (or grid-units).

ZSOURC(I) = Z-coordinate of source no. I in grid units.

STRTRL(I) = Start-time of source no. I in seconds

STOPRL(I) = Stop-time of source no. I in seconds

SOURCT(I) = Source strength of source no. I in gram/sec

HEATFX(I) = Heat emission of source no. I in kwatt

Note: $1 \leq I \leq \text{NRMULT}$

ISNAVN = Name of isotope released from all sources.
Max. 6 characters!

ISDCAY = Decay constant in sec⁻¹ for the isotope released.

4.3. STABDA - Namelist

The following parameters must be assigned a value:

STABTX = '<Text string of max. 72 characters of your current stability specifications>'

DTDZ = Potential temperature gradient in deg. Kelvin per meter. If not available, set to zero.
(DTDZ >= 0)

SIGYIN = Initial value of sigma-y in meters.
Must be greater than 1 meter.

SIGZIN = Initial value of sigma-z in meters.
Must be greater than 1 meter.

ZMTAB(I) = Limited mixing depth in meters for stability category I.
 $1 < I < 6$
ZMTAB(I) must be an integer multiple of DELZ.
If not estimated set to zero (0.0).

DSHEAR = Switch for wind direction shear:
DSHEAR = 0 : No wind direction shear
= 1 : Wind direction shear

ALFSHE = Wind direction shear over the height interval from HSHEMI to HSHEMA. Unit: degrees.

HSHEMI = Minimum height in meters for wind shear specification.
The shear below HSHEMI is calculated as a linear extrapolation of the shear between HSHEMI and HSHEMA.

HSHEMA = Maximum height in meters for wind shear specification.
The shear above HSHEMA is calculated as a linear extrapolation of the shear between HSHEMI and HSHEMA.

USH = Switch for wind speed shear:
USH = 0 : No wind speed shear
= 1 : Wind speed shear

USTAR = U^* in meters per sec.

LMOBUK = Monin-Obukov length in meters.

ZROUGH = Roughness length in meters.

DZERO = Zero displacement factor for calculation of wind speed profile. Unit: meters.

DUSDUM = Switch for dump of shear parameters:
DUSDUM = 0 : No dump of shear parameters
= 1 : Dump of shear parameters for each puff, when TOTTIM is an integer multiple of MAPTIM.

DEPMOD = Switch for deposition:
DEPMOD = 0 : No deposition
DEPMOD = 1 : Dry and wet deposition

OUTDEP = 'OUTPUT' or 'NOOUTP'

OUTPUT : The concentration of material deposited on the ground is written on a disc file with the logical name OUTDEP. (File 11)
NOOUTP : No file with concentrations of deposited material.

VDTAB(I,J)= Dry deposition parameter for stability class I and wind speed interval J.

1 < I < 6
1 < J < 5

The wind speed intervals are (m/s):

J=1 : 0 < Speed < 1
J=2 : 1 < Speed < 3
J=3 : 3 < Speed < 6
J=4 : 6 < Speed < 10
J=5 : 10 < Speed

LDTAB(I) = Wet deposition parameter for precipitation class I.

1 < I < 3

The precipitation classes are (mm/h):

I=1 : 0.01 < Precip. intens. < 1
I=2 : 1 < Precip. intens. < 3
I=3 : 3 < Precip. intens.

**TIMRAI(I) = Duration of precipitation in intensity class I.
In seconds (integer number).**

**Calculation of wind speed and wind direction shear is based on
MIK82.**

4.4. GAMDA - Namelist

The following parameters must be assigned a value:

GAMMOD = Switch for calculation of gamma doses from puffs
GAMMOD = 0 : No gamma doses
 = 1 : Gamma doses from isotope in puffs

OUTGAM = 'OUTPUT' or 'NOOUTP'
OUTPUT : The gamma doses from airborne activity is
 written on a disc file with the logical
 name OUTGAM. (File 14)
NOOUTP : No file with gamma doses from airborne act-
 ivity.

FGAM(I) = Frequency of photons in energy group I.
 $1 < I < 8$
 The energy groups are :

No.	Range (MeV)	Mean (MeV)
1	0.000 - 0.080	0.04
2	0.081 - 0.150	0.12
3	0.151 - 0.250	0.20
4	0.251 - 0.510	0.38
5	0.511 - 0.850	0.68
6	0.851 - 1.330	1.09
7	1.331 - 2.030	1.68
8	2.031 - 3.000	2.53

Note that only one isotope may be considered per calculation and that decay and build-up of daughter products are NOT taken into account!

4.5. DOSDA - Namelist

The following parameters must be assigned a value:

- RADDOS** = Switch for calculation of radiation doses from puffs:
RADDOS = .FALSE. : No radiation doses
 = .TRUE. : Doses from radioactive isotopes in puffs.
- INDOS** = Switch for calculation of inhalation doses from puffs:
INDOS = .FALSE. : No inhalation doses
 = .TRUE. : Doses from inhalation of radioactive isotopes in puffs.
- GAMDEP** = Switch for calculation of gamma doses from deposited radioactive isotopes:
GAMDEP = .FALSE. : No doses from deposited nuclides
 = .TRUE. : Doses from deposited material
- ORGNAM** = '<Text string of max. 8 characters giving the organ to which doses should be calculated>'
- DINHAL** = Dose factor for inhalation: Dose per curie inhaled integrated over a given time after inhalation.
Unit: Rem/ci.
- BRRAT** = Breathing rate, m³/sec
- FLTFAK** = Filtering factor for houses.
Typical values: 0.33 for average Danish house
 1.00 for outdoor stay

- GDISO** = Dose factor for deposited radioactive isotopes.
Unit: Rem/sec/Ci/m²
- DEPSHD** = Shielding factor for gamma doses from deposited
radioactive material
- GAMSHD** = Shielding factor for gamma doses from puffs
- ORGSHD** = Selfshielding factor for the body organ considered
- TDPINT** = Integration time for gamma doses from deposited
activity, sec. The integration starts at the time
when the activity is deposited.
- OUTTOT** = 'OUTPUT' or 'NOOUTP'

OUTPUT : The sum of the 3 dose components:
inhalation, gamma dose from puffs and gamma
from deposited material is written on a
disc file with the logical name **OUTTOT**.
(File 15).

NOOUTP : No file with total doses.

4.6. Example of the INDATA file

```
&PRIMDA
TITLE='RELEASE HOUR 1. IODINE. 500 M GRID ',
ICOLS=81,JROWS=81,KPLANS=1,DELX=500.,DELY=500.,DELZ=100.,
TDEL=0.0,CHEMIN=0.1E-09,NTADV=30,TAU=30,MAPTIM=3600,REFLEC=1.,
NRELSE=3600, IDMP=16, JDMP=34, KDMP=1, ISMODE=1, ITAPIN=0,
KOORD=1, XUTM=437.2609, YUTM=5486.1323,
INPRNT='YES',OUTDAT='OUTPUT',OUTMOD='DOSE',OUTWFD='OUTPUT'
&END
&RELDAT
PUFFTX='SOURCESITE AT XTOWN 20 M ABOVE GROUND ',
NRMULT=1,
XSOURC(1)=457.7609,YSOURC(1)=5506.6323,ZSOURC(1)=0.20,
STRTRL(1)=0,STOPRL(1)=3600,SOURST(1)=277.7777777778,
HEATFX(1)=1.,
&END
&STABDA
STABTX='MIXING HEIGHT VARIES WITH STABILITY .',
DTDZ=0.,ZMTAB(1)=1600.0,ZMTAB(2)=1200.,ZMTAB(3)=800.,
ZMTAB(4)=600.,ZMTAB(5)=300.,ZMTAB(6)=200.,
DSHEAR=0,ALFSHE=0.0,HSHEMI=10.0,HSHEMA=120.0,
USH=0,USTAR=0.265,LMOBUK=70.0,ZROUGH=0.1,DZERO=0.0,
DUSDUM=0,
DEPMOD=1,OUTDEP='OUTPUT',
VDTAB(1,1)=0.010,VDTAB(2,1)=0.010,VDTAB(3,1)=0.010,
VDTAB(4,1)=0.010,VDTAB(5,1)=0.010,VDTAB(6,1)=0.010,
VDTAB(1,2)=0.010,VDTAB(2,2)=0.010,VDTAB(3,2)=0.010,
VDTAB(4,2)=0.010,VDTAB(5,2)=0.010,VDTAB(6,2)=0.010,
VDTAB(1,3)=0.010,VDTAB(2,3)=0.010,VDTAB(3,3)=0.010,
VDTAB(4,3)=0.010,VDTAB(5,3)=0.010,VDTAB(6,3)=0.010,
VDTAB(1,4)=0.010,VDTAB(2,4)=0.010,VDTAB(3,4)=0.010,
VDTAB(4,4)=0.010,VDTAB(5,4)=0.010,VDTAB(6,4)=0.010,
VDTAB(1,5)=0.010,VDTAB(2,5)=0.010,VDTAB(3,5)=0.010,
VDTAB(4,5)=0.010,VDTAB(5,5)=0.010,VDTAB(6,5)=0.010,
```

```
LDTAB(1)=0.000042,LDTAB(2)=0.000106,LDTAB(3)=0.000233,  
TIMRAI(1)=1692,TIMRAI(2)=2628,TIMRAI(3)=2232  
&END  
&GAMDA  
GAMMOD=0,OUTGAM='NOOUTP',  
FGAM(1)=0.0,FGAM(2)=0.0,FGAM(3)=0.0,FGAM(4)=0.0,FGAM(5)=0.0,  
FGAM(6)=1.0,FGAM(7)=0.0,FGAM(8)=0.0  
&END
```

Note: One space is required in the beginning of each line.
Gamma doses are NOT calculated in this example!

5. Description of the WINDDA file

The WINDDA file provides the necessary parameters and wind observation records for a simulation. It is divided in two parts and must be defined in the following order:

1. WINPAR - namelist
2. WIND observation records

The WINPAR namelist assigns values to the parameters used by the wind interpolation routine in RIMPUFF. The wind interpolation record contains information on the stability (Pasquill Turner or standard deviation of the wind direction), the wind direction, the wind speed and precipitation intensity.

5.1. WINPAR - Namelist

The following parameters must be assigned a value:

WINDTLE = '<Text string of max. 72 characters defining of your current winddata set>'

TIME = '<5 character string giving the time of your problem with the format: HH:MM>'

DATE = '<9 character string giving the date of your problem with the format: DD-MMM-YY>'

Example

.... TIME = ' 9:00 ',DATE = '16-OCT-85'

ITSP = <Integer value of averaging time for the wind observations in seconds>

NOTE: MOD(ITSP,NTADV) must be zero!
i.e. ITSP must be an integer multiple of NTADV

NP = <Integer value of the number of wind observation stations>
Max. 10 stations are allowed!

NFX = <The maximum first index in the wind field matrix>
Note: NFX = ICOLS

NFY = <The maximum second index in the wind field matrix>
Note: NFY = JROWS

NSTL = <Integer value of the limit on number of wind stations to be used in interpolation if limiting radius is reached>

NSKIP = <Number of wind record to be skipped before start of wind field calculations>

RTE = <Decimal angle of the wind field matrix rotation from north>

RCH = <Decimal radius in meters (or grid units) within included stations are to be used in interpolation>

HWOBS = >0: <Height (in meters) at which the wind speed is measured>

The same height is used for all stations.

-1: The wind speed is assumed to be measured at puff centre height, i.e. no gradient for wind speed.

K1ST = < 0 : Interpolation performed with defined stations.
0 < K1ST =< NP : Selects the only station from which wind field is exclusively derived.

FLOPLD = **.TRUE.:** Wind speed and -direction from data calculations by a flow field model.
See the subroutine LINCOM in VER20/SPACEPUFF.
Stability data are taken from the WINDDA file.
.FALSE.: All wind field data are taken from the WINDDA-file.

For each wind station the following data must be given:
I denotes the station number (0 < I < NP).

NAMST(I) = '<Max. 6 character station name>'

X(I) = <X coordinate of wind station in km (UTM-grid) or grid units (puff-grid)>

Y(I) = <Y coordinate of wind station in km (UTM-grid) or grid units (puff-grid)>

SSKIP(I) = **.FALSE.:** Use data for station no. I in calculations of stability and windfield. (DEFAULT).
.TRUE. : Skip data for station no. I.
Remember to correct the limits for the stability arrays.

COR(I) = <correction in degrees to the wind direction>

CONFAC(I) = <Height adjustment multiplier of the wind speed to chosen reference height>

Note: If the wind speeds are measured at different heights at each wind station an appropriate reference height should be defined. The same height as the source, if it is elevated, should be chosen.

A(I) = <Alignment angle weight in degrees>

The limits for the stability arrays defining the areas around the station in which the stability data for the station applies should be defined. Note that the first station by definition is the "base" station which determines the stability for the whole puff grid. The stability areas for the following stations are then "patched" in to the areas of the first station.

ISXMIN(I) = <X-coordinate for the lower left corner of the stability area, in meters (UTM) or GDU>

ISXMAX(I) = <X-coordinate for the upper right corner of the stability area, in meters (UTM) or GDU>

ISYMIN(I) = <Y-coordinate for the lower left corner of the stability area, in meters (UTM) or GDU>

ISYMAX(I) = <Y-coordinate for the upper right corner of the stability area, in meters (UTM) or GDU>

5.2. Wind data record (BNF-notation)

```
<wind data record>::=  
<time>  
<Station name>,<Lateral stability>,<Vertical stability>,  
<Wind direction>,<Wind speed>,<Rain intensity>  
.....  
<End Of Wind Record>
```

Where:

```
<time>           ::= 'HH:MM'  
<Station name>  ::= 'XXXXXX' (max. 6 characters)  
<Lateral stability> ::= '<Stability category >' |  
                        <Standard deviation of the horizontal  
                        direction (degrees)>  
<Vertical stability> ::= '<Stability category >' |  
                        <Standard deviation of the vertical  
                        direction (degrees)>  
<Stability category> ::= A|B|C|D|E|F  
<Standard deviation of direction> ::= 0.0 to 99.99 (degrees)  
<End Of Wind Record> ::= 'EOWR' | 'STOP'
```

EOWR = End of wind record for current time step
STOP = End of wind record and wind data file

5.3. Example of the WINDDA file

```
&WINPAR
WNDTLE='WINDDATA: XTOWN , HOUR 2972 ',
TIME=' 08:00 ',DATE='08-MAY-75 ',ITSP=3600 ,
NP=8,NFX=81,NFY=81,NSTL=3,NSKIP=0,
RTE=0.,RCH=250000.,
NAMST(1)='FCIT',X(1)=470.168,Y(1)=5544.385,COR(1)=0.,
CONFAC(1)=1.000,A(1)=0.,ISXMIN(1)=301200,ISXMAX(1)=618000,
ISYMIN(1)=5345000,ISYMAX(1)=5724610,
NAMST(2)='WCIT',X(2)=569.616,Y(2)=5513.247,COR(2)=0.,
CONFAC(2)=1.000,A(2)=0.,ISXMIN(2)=538000,ISXMAX(2)=618000,
ISYMIN(2)=5478201,ISYMAX(2)=5519801,
NAMST(3)='SCIT',X(3)=514.722,Y(3)=5392.38,COR(3)=0.,
CONFAC(3)=1.000,A(3)=0.,ISXMIN(3)=419600,ISXMAX(3)=618000,
ISYMIN(3)=5345001,ISYMAX(3)=5500601,
NAMST(4)='OCIT',X(4)=537.64,Y(4)=5449.926,COR(4)=0.,
CONFAC(4)=1.000,A(4)=0.,ISXMIN(4)=490000,ISXMAX(4)=618000,
ISYMIN(4)=5433401,ISYMAX(4)=5478201,
NAMST(5)='TOWN',X(5)=362.844,Y(5)=5453.358,COR(5)=0.,
CONFAC(5)=1.000,A(5)=0.,ISXMIN(5)=301200,ISXMAX(5)=416400,
ISYMIN(5)=5345001,ISYMAX(5)=5587001,
NAMST(6)='TCIT',X(6)=331.911,Y(6)=5513.559,COR(6)=0.,
CONFAC(6)=1.000,A(6)=0.,ISXMIN(6)=301200,ISXMAX(6)=358800,
ISYMIN(6)=5478201,ISYMAX(6)=5587001,
NAMST(7)='KCIT',X(7)=368.640,Y(7)=5636.773,COR(7)=0.,
CONFAC(7)=1.000,A(7)=0.,ISXMIN(7)=301200,ISXMAX(7)=416400,
ISYMIN(7)=5590201,ISYMAX(7)=5724601,
NAMST(8)='MONT',X(8)=531.374,Y(8)=5683.4,COR(8)=0.,
CONFAC(8)=1.000,A(8)=0.,ISXMIN(8)=522000,ISXMAX(8)=618000,
ISYMIN(8)=5606201,ISYMAX(8)=5724601,
&END
'19:00'
'FCIT','D','D', 50.0, 5.1, 0.180
'WCIT','D','D', 360.0, 3.3, 0.000
```

'SCIT','D','D','D',	40.0,	4.1,	0.000
'OCIT','D','D','D',	60.0,	3.9,	0.000
'TOWN','D','D','D',	40.0,	5.1,	0.090
'TCIT','D','D','D',	60.0,	6.2,	0.180
'KCIT','E','E','E',	20.0,	2.6,	0.180
'MONT','D','D','D',	50.0,	4.1,	0.180
'EOWR'			
'20:00'			
'FCIT','D','D','D',	30.0,	5.6,	0.122
'WCIT','D','D','D',	360.0,	2.8,	0.031
'SCIT','D','D','D',	40.0,	3.1,	0.016
'OCIT','D','D','D',	60.0,	3.4,	0.031
'TOWN','D','D','D',	40.0,	5.1,	0.061
'TCIT','D','D','D',	70.0,	5.1,	0.122
'KCIT','D','D','D',	30.0,	2.6,	0.122
'MONT','D','D','D',	50.0,	4.1,	0.122
'STOP'			

6. Description of the BEFDA file

The BEFDA file provides the population data for 1 by 1 km squares in the UTM-grid. The data are stored in binary form and are read with the following FORTRAN statement:

```
READ(8,END=8008) (INF(I1),I1=1,675)
```

where

```
INF(1)  = XL = X-coordinate of the lower left corner  
          of 25 by 25 km square in the UTM-grid  
INF(2)  = YL = Y-coordinate of the lower left corner  
          of 25 by 25 km square in the UTM-grid  
INF(i1) = Population in a 1 by 1 km square for which  
          the lower left corner has the coordinates  
          XL+(i-1),YL+(j-1) in km.  
i1      = (i-1)*27+(j+1)+1  
          1<= i <= 25  
          1<= j <= 25
```

XL and YL must be an integer multiple of 25.

The BEFDA file must be assigned to File 8 and the specifications must be equivalent to:

(FYSNYREEN) : DIRECTORY ON USERPACK
. DKBF92 : DIRECTORY
. . RIMP : DATA ALTERDATE= 9/19/86 ' 10:52:43 AREAS=1
AREASIZE=1020 BLOCKSIZE=20250
CREATIONDATE= 9/19/86 ' 10:52:43 CRUNCHED
CYCLE=1 FILEORGANIZATION=NOT RESTRICTED
FILETYPE=0 INTMODE=4
LASTACCESSDATE=10/14/86 ' 17:31:07
LASTRECORD=103 (2700 SEGS) MAXRECSIZE=675
MINRECSIZE=0 SAVEFACTOR=0
SECURITY=PRIVATE (I/O)
TIMESTAMP= 9/19/86 ' 10:52:49 UNITS=0
VERSION=0 NO WARNINGS

The following two files, both pertaining to the UTM zone 32 grid are presently available:

DKBF92/85/RIMP.

DKBF92/RIMP.

Both files contain population data for Denmark.

7. Description of the output files

If the 6 output options (OUTDAT='OUTPUT' , OUTDEP='OUTPUT', OUTGAM='OUTPUT', OUTTOT='OUTPUT, OUTWFD='OUTPUT' and OUTBEF='OUTPUT') are specified the following files are created:

1. OUTAIR (FILE10)
 - Concentration in air for each MAPTIM
 - Puff position data for each MAPTIM

2. OUTDEP (FILE11)
 - Concentration on the ground for each MAPTIM
 - Puff position data for each MAPTIM

3. OUTGAM (FILE14)
 - Gammadoses from airborne material for each MAPTIM
 - Puff position data for each MAPTIM

4. WFIELD (FILE12)
 - Position of wind stations
 - Wind velocity field with U and V component for each time step

5. OUTTOT (FILE15)
 - Total radiation doses to individuals for each MAPTIM
 - Puff position data for each MAPTIM

6. OUTBFD (FILE88)
 - Total collective doses for each MAPTIM (1<=IBFOPT<=4)
 - Puff position data for each MAPTIM

7. OUTBFT (FILE89)

- Population distribution in grid. (IBFOPT=100).

Only data for MAPTIM = 1 !!

These data files provide the input for a (computer specific) plotting program, PUFFPLOT.

Output on the printer of the concentration matrix is made if the following parameters are specified in the PRIMDA namelist of the INDATA file:

0< IDMP < ICOLS

0< JDMP < JROWS

0< KDMP < KPLANS

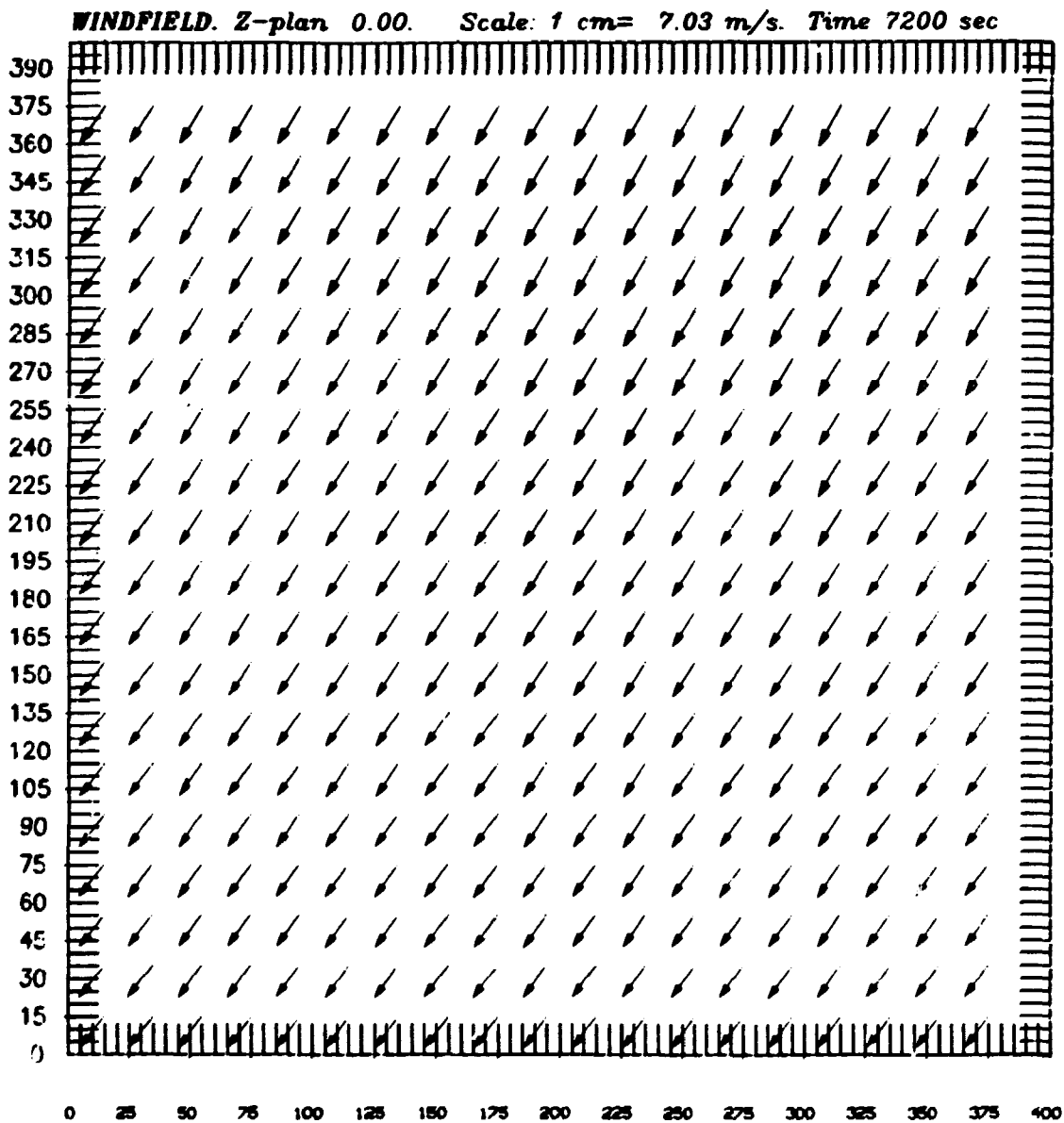
8. EXAMPLES

8.1. Example no. 1

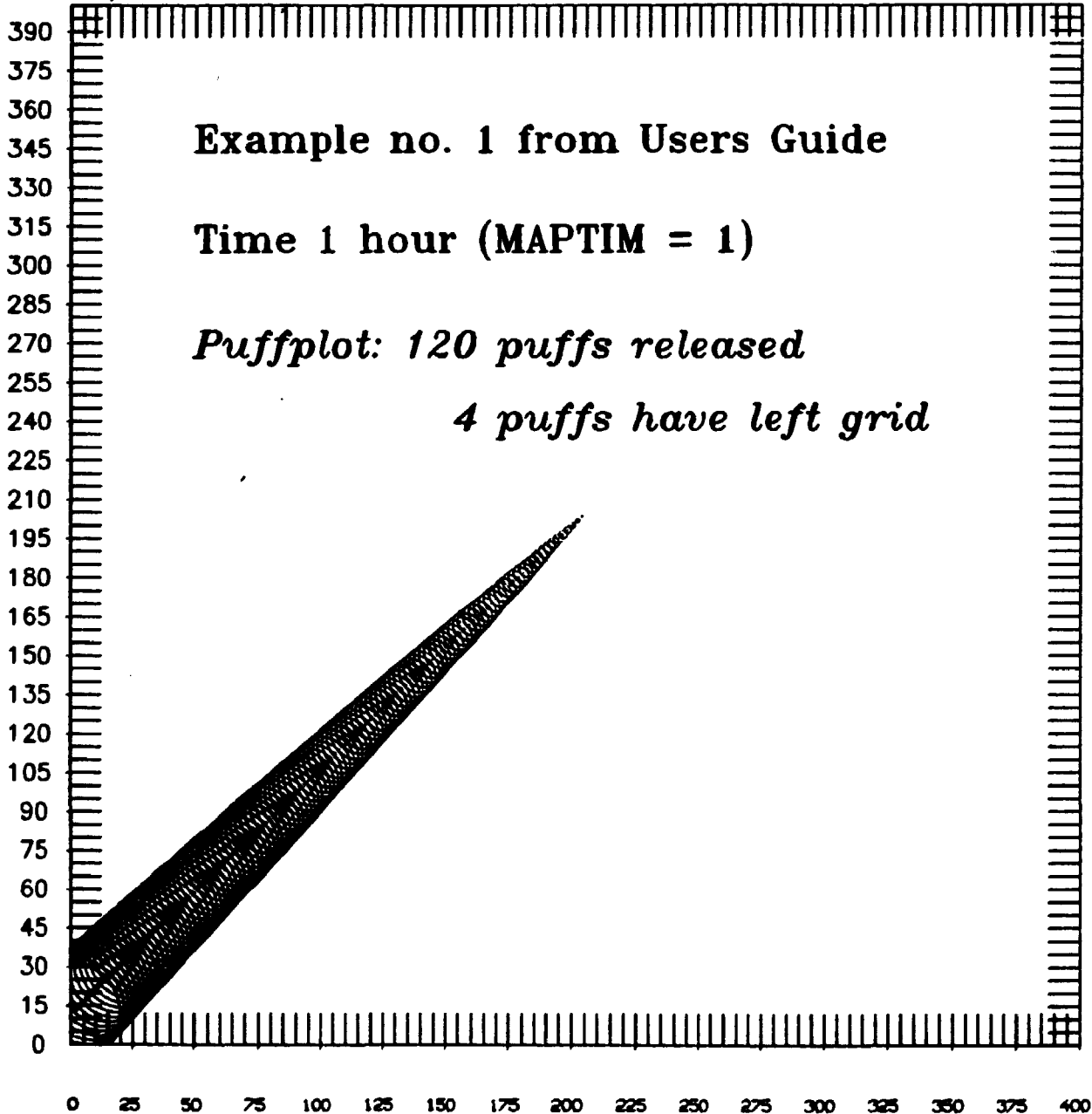
The files INDATA and WINDDA are as given earlier in this paper.
The output is as shown on the following pages.

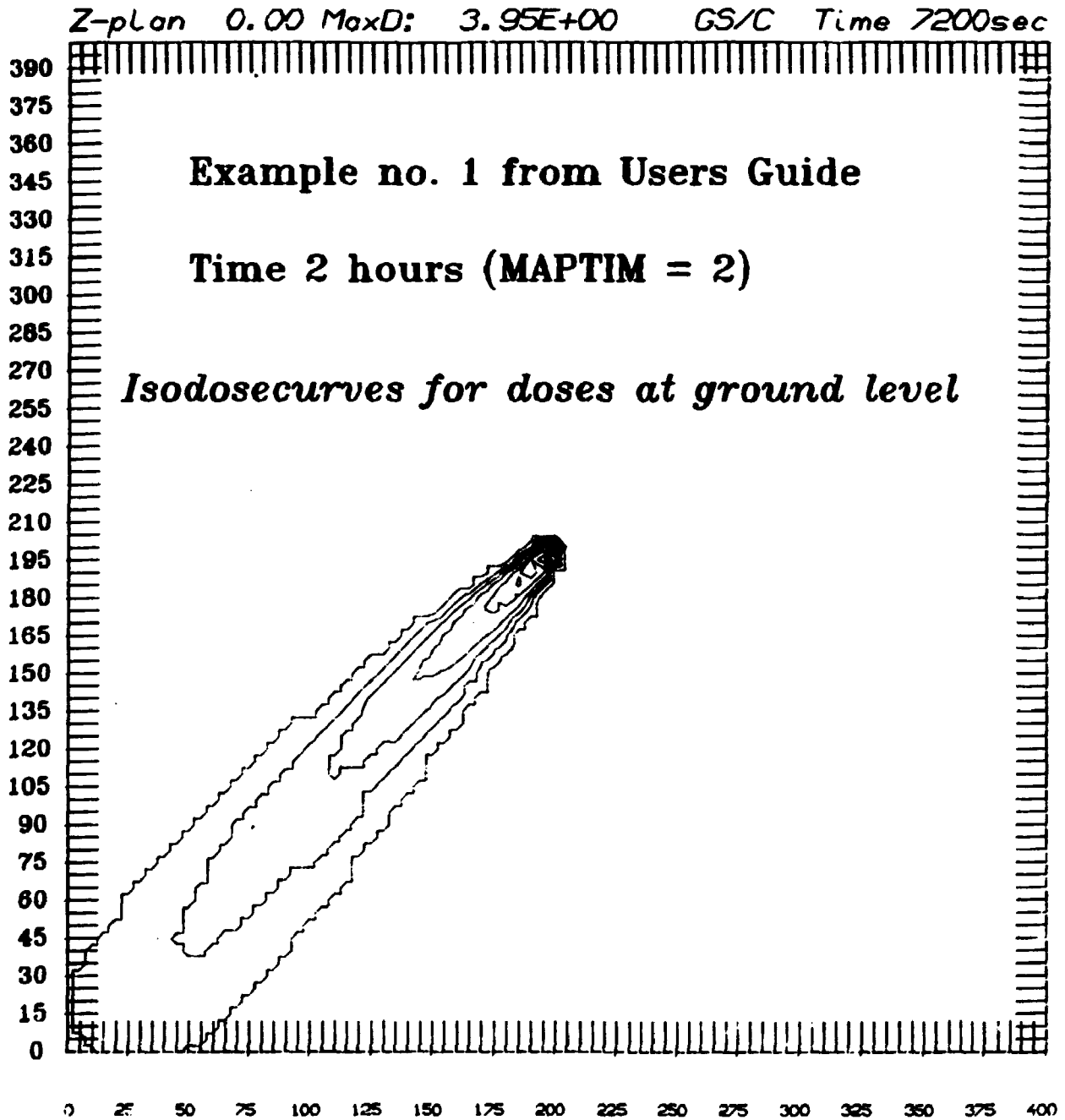
Example no. 1 from Users Guide

Time 2 hours (MAPTIM = 2)



Z-plan 0.00 MaxD: 3.88E+00 GS/C Time 3600sec



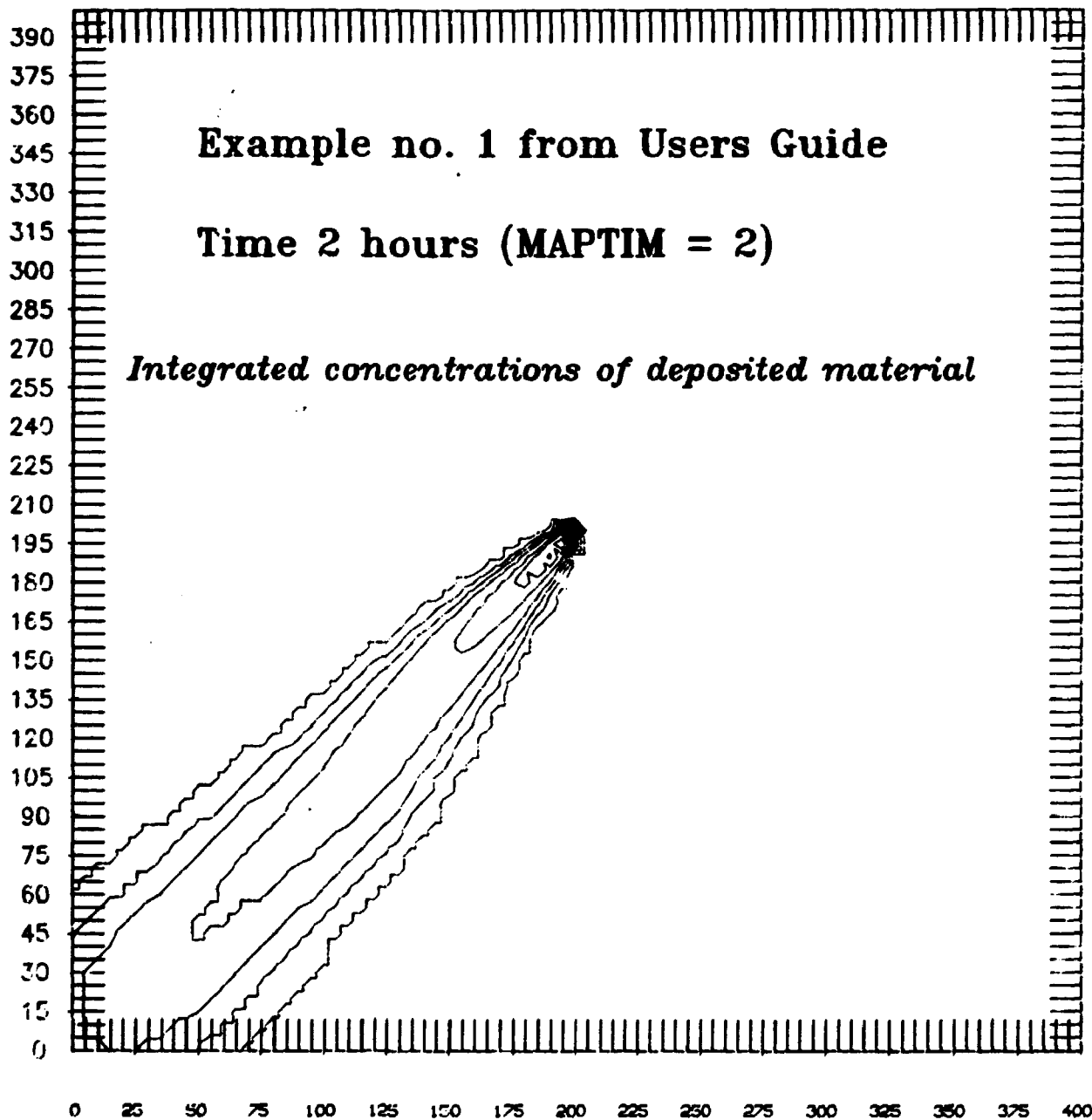


Ground 0.00 MaxD: 5.57E-02 GS/A Time 7200sec

Example no. 1 from Users Guide

Time 2 hours (MAPTIM = 2)

Integrated concentrations of deposited material



RELEASE HOUR 1. IODINE. 500 M GRID

KEY PARAMETER FOR CURRENT RUN:

NRELS = 3600
ICOLS = 51 JRCNS = 31 KPLANS = 1
NTADV = 30 NAPTIM = 3600 TAU = 30
DELX = 500.00 DELY = 500.00 DELZ = 100.00
CHEMIN = 0.1000E-09 REFLEC = 1.00000 TDEL = 0
IDMP = 16 JDMP = 34 KDMP = 1
ISHODE = 1
INPRNT = YES
OUTDAT = OUTPUT OUTMOD = DOSE
CUTWFO = OUTPUT
KFRTAPE= 0 (0 = NO, 1= YES)

* COORDINATES FOR SOURCE AND WINDSTATIONS IN UTM
* LOWER LEFT CORNER IS 437.2609 , 5486.1323 KM

SOURCESITE AT XTQNM 20 M ABOVE GROUND

CURRENT SOURCEDATA : NUMBER OF ACTIVE SOURCES : 1
1 41.00 41.00 0.20 0 3600***** 1.00000000

ZHGT = 20.0

NO GAIN/DCSES FROM PUFFS

FRAME FOR PUFF ADVECTION:
X: 0 => 80 - Y: 0 => 80

THE MIXING LAYER IS LIMITED AT: 1500.00 METERS IN STABILITY CAT 1
THE MIXING LAYER IS LIMITED AT: 1200.00 METERS IN STABILITY CAT 2
THE MIXING LAYER IS LIMITED AT: 800.00 METERS IN STABILITY CAT 3
THE MIXING LAYER IS LIMITED AT: 500.00 METERS IN STABILITY CAT 4
THE MIXING LAYER IS LIMITED AT: 300.00 METERS IN STABILITY CAT 5
THE MIXING LAYER IS LIMITED AT: 200.00 METERS IN STABILITY CAT 6

IN THE CURRENT RUN, THE STABILITY-CLASSES ARE
 CONNECTED TO INTENSITY DATA AS FOLLOWS:
 STABILITY CLASS NO.: 1 2 3 4 5 6
 INTENSITY DATA : 0.42 0.34 0.26 0.17 0.09 0.04

MIXING HEIGHT VARIES WITH STABILITY -

IN THE CURRENT RUN, THE POTENTIAL TEMPERATURE
 GRADIENT IS SET TO: 0.0030

NO WIND SHEAR

DEPOSITION PARAMETERS

DRY DEPOSITION PARAMETER, VD (M/S)

WINDSPEED (M/S)	A	E	C	D	E	F
1 <= U < 1	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02
1 <= U < 3	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02
3 <= U < 6	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02
6 <= U < 10	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02
10 <= U	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02

WASH-OUT COEFFICIENT

PRECIPITATION (MM/H)	LD(S-1)	TIME(SEC)
1 <= P < 1	4.20E-05	1692
1 <= P < 3	1.06E-04	2525
3 <= P	2.33E-04	2232

OUTDEP = OUTPUT
 =====

WIND PARAMETER DUMP

WINDDATA: XTOWN, HOUR 2972

TIME = 00:00 DATE = 08-MAY-75 ITSP = 3600 SEC
 MFX = 0 MFX = 01 MFX = 01
 MSTL = 3 MSHR = 0 K1ST = 0
 RTE = 0.0 (REG. 3 RCH = 500.0 (6-U.))

NAME	X GU	Y GU	CDR DEC	CONFAC	ALIGN DEG	ISXMIN GU	ISYMAX GU	ISYMIN GU	ISYMAX GU
CU11	264.0	116.5	0	1.0	0.0	100	100	100	100
CU12	264.0	117.5	0	1.0	0.0	100	100	100	100
CU13	264.0	118.5	0	1.0	0.0	100	100	100	100
CU14	264.0	119.5	0	1.0	0.0	100	100	100	100
CU15	264.0	120.5	0	1.0	0.0	100	100	100	100
CU16	264.0	121.5	0	1.0	0.0	100	100	100	100
CU17	264.0	122.5	0	1.0	0.0	100	100	100	100
CU18	264.0	123.5	0	1.0	0.0	100	100	100	100
CU19	264.0	124.5	0	1.0	0.0	100	100	100	100
CU20	264.0	125.5	0	1.0	0.0	100	100	100	100

1. The first part of the document discusses the general principles of the law of nations, which are derived from the natural law of God. It states that the law of nations is not a separate body of law, but rather a part of the natural law that applies to all nations and individuals.

2. The second part of the document discusses the law of nations as it applies to the relations between nations. It states that the law of nations is based on the principle of reciprocity, and that nations are bound to treat each other as they would wish to be treated.

3. The third part of the document discusses the law of nations as it applies to the relations between nations and individuals. It states that the law of nations is based on the principle of justice, and that individuals are bound to treat nations as they would wish to be treated.

4. The fourth part of the document discusses the law of nations as it applies to the relations between nations and the Church. It states that the law of nations is based on the principle of charity, and that the Church is bound to treat nations as they would wish to be treated.

5. The fifth part of the document discusses the law of nations as it applies to the relations between nations and the State. It states that the law of nations is based on the principle of authority, and that the State is bound to treat nations as they would wish to be treated.

6. The sixth part of the document discusses the law of nations as it applies to the relations between nations and the individual. It states that the law of nations is based on the principle of responsibility, and that the individual is bound to treat nations as they would wish to be treated.

7. The seventh part of the document discusses the law of nations as it applies to the relations between nations and the world. It states that the law of nations is based on the principle of peace, and that the world is bound to treat nations as they would wish to be treated.

8. The eighth part of the document discusses the law of nations as it applies to the relations between nations and the future. It states that the law of nations is based on the principle of hope, and that the future is bound to treat nations as they would wish to be treated.

9. The ninth part of the document discusses the law of nations as it applies to the relations between nations and the past. It states that the law of nations is based on the principle of memory, and that the past is bound to treat nations as they would wish to be treated.

10. The tenth part of the document discusses the law of nations as it applies to the relations between nations and the present. It states that the law of nations is based on the principle of reality, and that the present is bound to treat nations as they would wish to be treated.

STABILITY INDEX AIRRAY (J=1-64)

11. The eleventh part of the document discusses the law of nations as it applies to the relations between nations and the future. It states that the law of nations is based on the principle of hope, and that the future is bound to treat nations as they would wish to be treated.

12. The twelfth part of the document discusses the law of nations as it applies to the relations between nations and the past. It states that the law of nations is based on the principle of memory, and that the past is bound to treat nations as they would wish to be treated.

13. The thirteenth part of the document discusses the law of nations as it applies to the relations between nations and the present. It states that the law of nations is based on the principle of reality, and that the present is bound to treat nations as they would wish to be treated.

14. The fourteenth part of the document discusses the law of nations as it applies to the relations between nations and the future. It states that the law of nations is based on the principle of hope, and that the future is bound to treat nations as they would wish to be treated.

15. The fifteenth part of the document discusses the law of nations as it applies to the relations between nations and the past. It states that the law of nations is based on the principle of memory, and that the past is bound to treat nations as they would wish to be treated.

16. The sixteenth part of the document discusses the law of nations as it applies to the relations between nations and the present. It states that the law of nations is based on the principle of reality, and that the present is bound to treat nations as they would wish to be treated.

17. The seventeenth part of the document discusses the law of nations as it applies to the relations between nations and the future. It states that the law of nations is based on the principle of hope, and that the future is bound to treat nations as they would wish to be treated.

18. The eighteenth part of the document discusses the law of nations as it applies to the relations between nations and the past. It states that the law of nations is based on the principle of memory, and that the past is bound to treat nations as they would wish to be treated.

19. The nineteenth part of the document discusses the law of nations as it applies to the relations between nations and the present. It states that the law of nations is based on the principle of reality, and that the present is bound to treat nations as they would wish to be treated.

20. The twentieth part of the document discusses the law of nations as it applies to the relations between nations and the future. It states that the law of nations is based on the principle of hope, and that the future is bound to treat nations as they would wish to be treated.


```

TIMESTEP NO = 1
OBSERVATION TIME: 15:00
STATION DIRECTION VELOCITY STABILITY RAIN
(CM/H)
FCIT 360. 3.1 0 0.18
WCIT 50. 4.1 0 0.00
OCIT 40. 3.9 0 0.00
TCIT 60. 5.2 0 0.18
MCIT 60. 6.2 0 0.18
MONT 50. 4.1 0 0.18

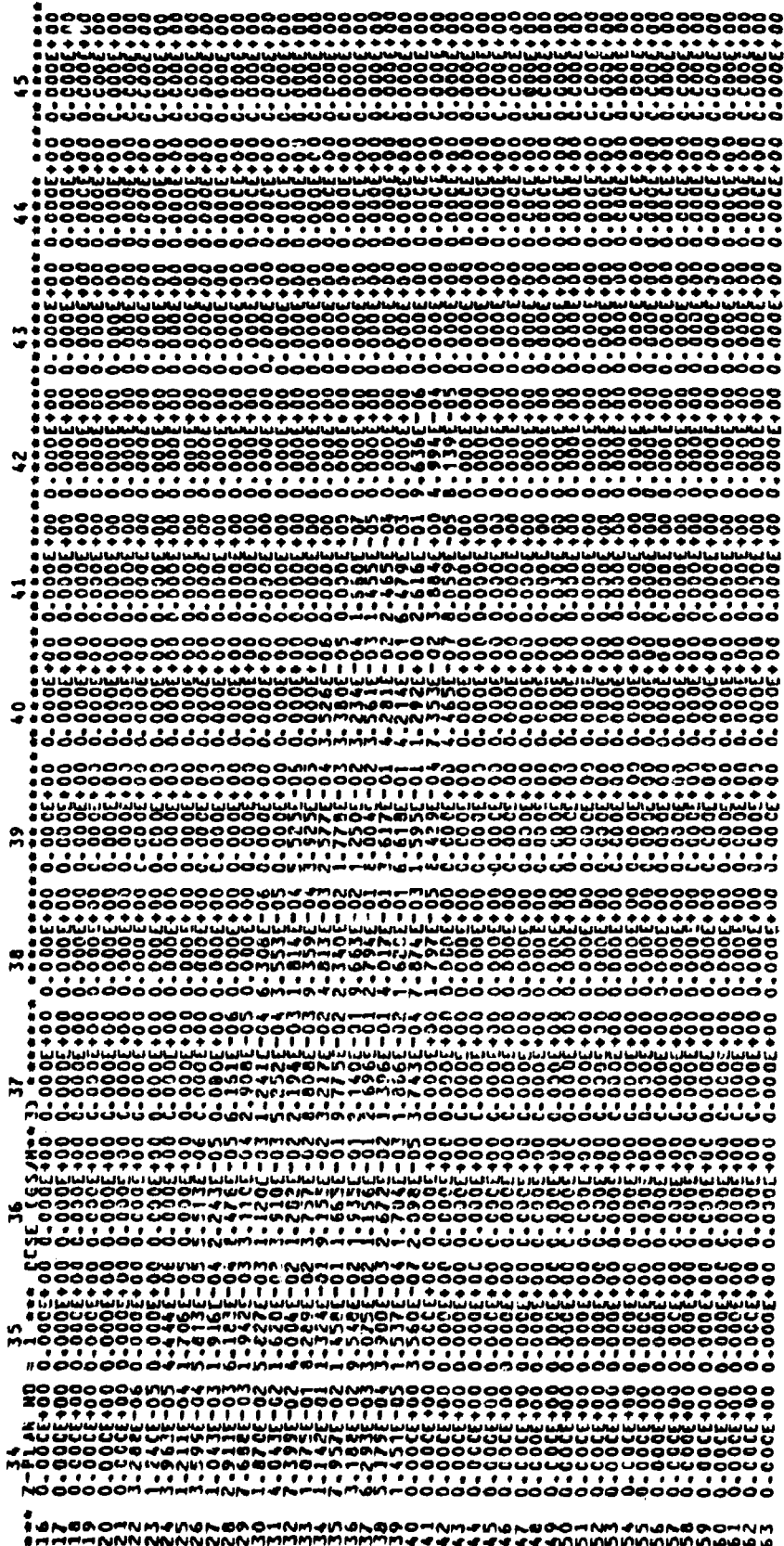
STATION U V RAIN
(CM/H)
FCIT -3.9 -1.3 0.18
WCIT -2.6 -1.1 0.00
OCIT -1.3 -2.0 0.00
TCIT -2.9 -2.1 0.18
MCIT -1.1 -2.6 0.18
MONT -1.1 -2.6 0.18

```

* TIMESTEP NO. 1 : ZM = 800.0 => ZMG = 6

=====
>>> WIND-DIRECTION AT SOURCE: 47-317749955
>>> AT TIME 3 30 SEC

=====
3600 SEC - AFTER START OF RELEASE
T0V - 120 PUFFS RELEASED AND 4 HAVE LEFT THE GRID
=====




```

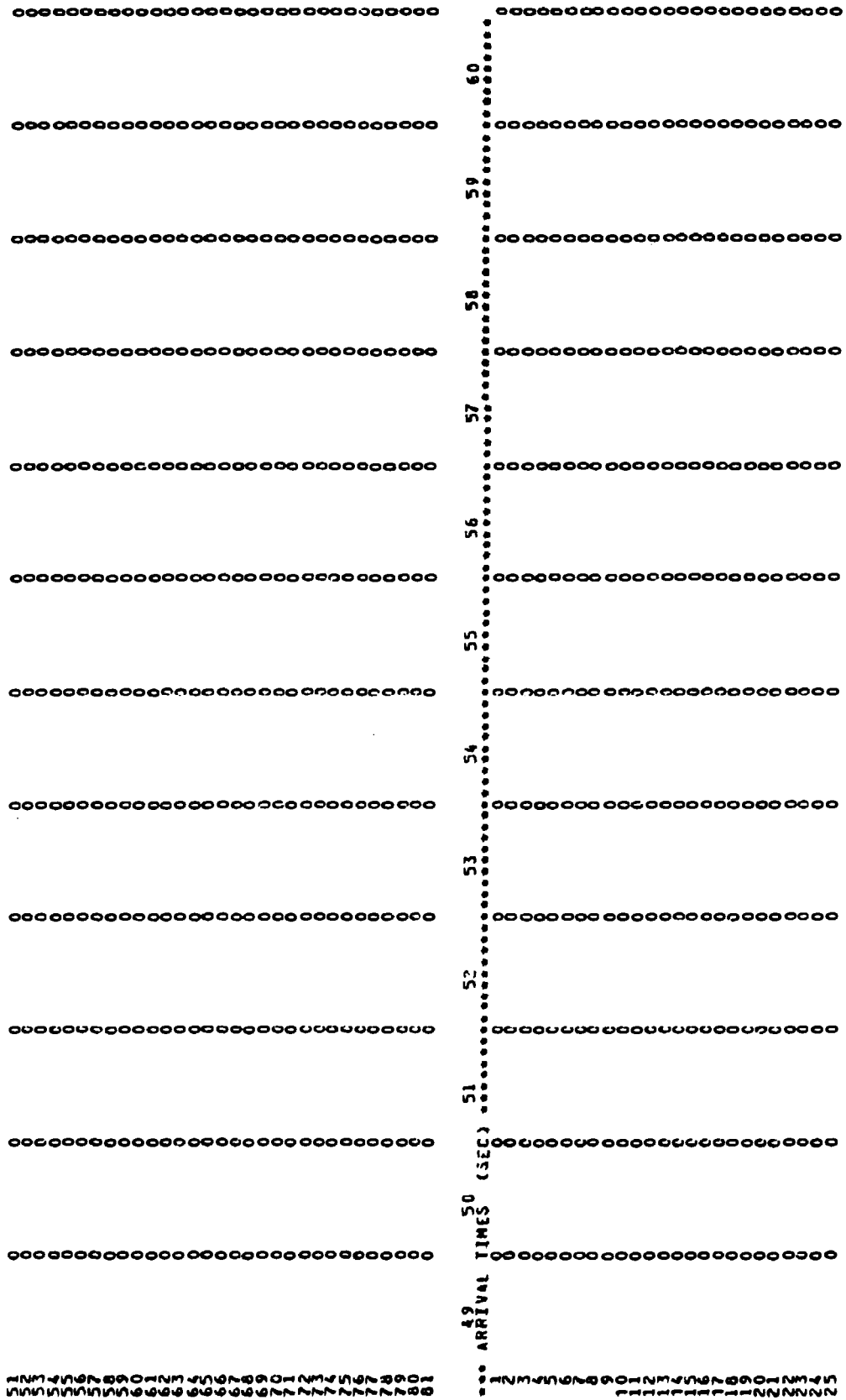
TIMESTEP NO = 2
OBSERVATION TIME = 20:00

STATION   STATION   DIRECTION   VELOCITY   STABILITY   RAIN
          (M/S)   (DIR)       (M/S)      (TYP)       (MM/H)
FCIT      30.0     30.0       5.6         0           0.0
MCIT      40.0     40.0       5.6         0           0.0
OCIT      60.0     60.0       5.6         0           0.0
TCMK      40.0     40.0       5.6         0           0.0
TCIT      70.0     70.0       5.6         0           0.0
MCMI      30.0     30.0       5.6         0           0.0

STATION   (M/S)   (M/S)   (M/S)   (M/H)
FCIT      30.0     30.0     5.6     0.0
MCIT      40.0     40.0     5.6     0.0
OCIT      60.0     60.0     5.6     0.0
TCMK      40.0     40.0     5.6     0.0
TCIT      70.0     70.0     5.6     0.0
MCMI      30.0     30.0     5.6     0.0

* TIMESTEP NO. 2 * ZM = 600.0 => ZMS = 6

```

8.2. Example no. 2

The files INDATA and WINDDA are as shown below:

8.2.1. INDATA file

```
&PRIMDA
TITLE='DEMO 1. DRY AND WET DEPOSITION ',
ICOLS=100,JROWS=64,KPLANS=1,DELX=500.,DELY=500.,DELZ=30.,
TDEL=0.0,CHEMIN=0.1E-15,NTADV=60,TAU=60,MAPTIM=900,REFLEC=1.,
NRELSE=9999,IDMP=1,JDMP=26,KDMP=1,ISMODE=1,ITAPIN=0,
KOORD=0,XUTM=332.7609,YUTM=5381.6323,
INPRNT='YES',OUTDAT='OUTPUT',OUTMOD='DOSE',OUTWFD='NOOUTP'
INPRNT='YES',OUTDAT='OUTPUT',OUTMOD='DOSE',OUTWFD='NOOUTP'
&END
&RELDAT
PUFPTX='SOURCEHEIGHT=100 METERS, SOURCESTRENGTH=1/3600',
NRMULT=1,
XSOURC(1)=0.0,YSOURC(1)=32.0,ZSOURC(1)=3.3333,
STRTRL(1)=0,STOPRL(1)=3600,SOURST(1)=277.77777778,HEATFX(1)=0.,
&END
&STABDA
STABTX='MIXING HEIGHT VARIES WITH STABILITY .',
DTDZ=0.,ZMTAB(1)=1620.0,ZMTAB(2)=1200.,ZMTAB(3)=810.,
ZMTAB(4)=570.,ZMTAB(5)=330.,ZMTAB(6)=210.,
DSHEAR=0,ALFSHE=-5.0,HSHEMI=0.0,HSHEMA=200.0,
USH=0,USTAR=0.1397,LMOBUK=44.64,ZROUGH=0.1,DZERO=0.0,
DUSDUM=0,
DEPMOD=1,OUTDEP='OUTPUT',
VDTAB(1,1)=0.010,VDTAB(2,1)=0.010,VDTAB(3,1)=0.010,
VDTAB(4,1)=0.010,VDTAB(5,1)=0.010,VDTAB(6,1)=0.010,
VDTAB(1,2)=0.010,VDTAB(2,2)=0.010,VDTAB(3,2)=0.010,
VDTAB(4,2)=0.010,VDTAB(5,2)=0.010,VDTAB(6,2)=0.010,
VDTAB(1,3)=0.010,VDTAB(2,3)=0.010,VDTAB(3,3)=0.010,
```

VDTAB(4,3)=0.010,VDTAB(5,3)=0.010,VDTAB(6,3)=0.010,
VDTAB(1,4)=0.010,VDTAB(2,4)=0.010,VDTAB(3,4)=0.010,
VDTAB(4,4)=0.010,VDTAB(5,4)=0.010,VDTAB(6,4)=0.010,
VDTAB(1,5)=0.010,VDTAB(2,5)=0.010,VDTAB(3,5)=0.010,
VDTAB(4,5)=0.010,VDTAB(5,5)=0.010,VDTAB(6,5)=0.010,
LDTAB(1)=0.000042,LDTAB(2)=0.000106,LDTAB(3)=0.000233,
TIMRAI(1)=1692,TIMRAI(2)=2628,TIMRAI(3)=2232
&END

8.2.2. WINDDA file

```
&WINPAR
WNTLE='WINDDATA (CONSTANT WIND) FOR KFK-INTERCOMP. TEST',
TIME=' 12:00',DATE='25-MAR-85',ITSP=1800,
NP=1,NFX=100,NFY=64,NSTL=1,NSKIP=0,
RTE=0.,RCH=100.,
NAMST(1)='RIS',X(1)=0.,Y(1)=32.,COR(1)=0.,CONFAC(1)=1.0000,
A(1)=0.,ISXMIN(1)=1,ISXMAX(1)=100,ISYMIN(1)=1,ISYMAX(1)=64,
&END
' 12:00 '
'RIS','D','D',270.,5.00,0.0
'EOWR'
' 12:30 '
'RIS','D','D',270.,5.00,0.0
'EOWR'
' 13:00 '
'RIS','D','D',270.,5.00,0.0
'EOWR'
' 13:30 '
'RIS','D','D',270.,5.00,2.0
'EOWR'
' 14:00 '
'RIS','D','D',270.,5.00,0.0
'EOWR'
' 14:30 '
'RIS','D','D',270.,5.00,0.0
'EOWR'
' 15:00 '
'RIS','D','D',270.,5.00,0.0
'EOWR'
' 15:30 '
'RIS','D','D',270.,5.00,0.0
'EOWR'
' 16:00 '
```

'RIS', 'D', 'D', 270., 5.00, 0.0

'EOWR'

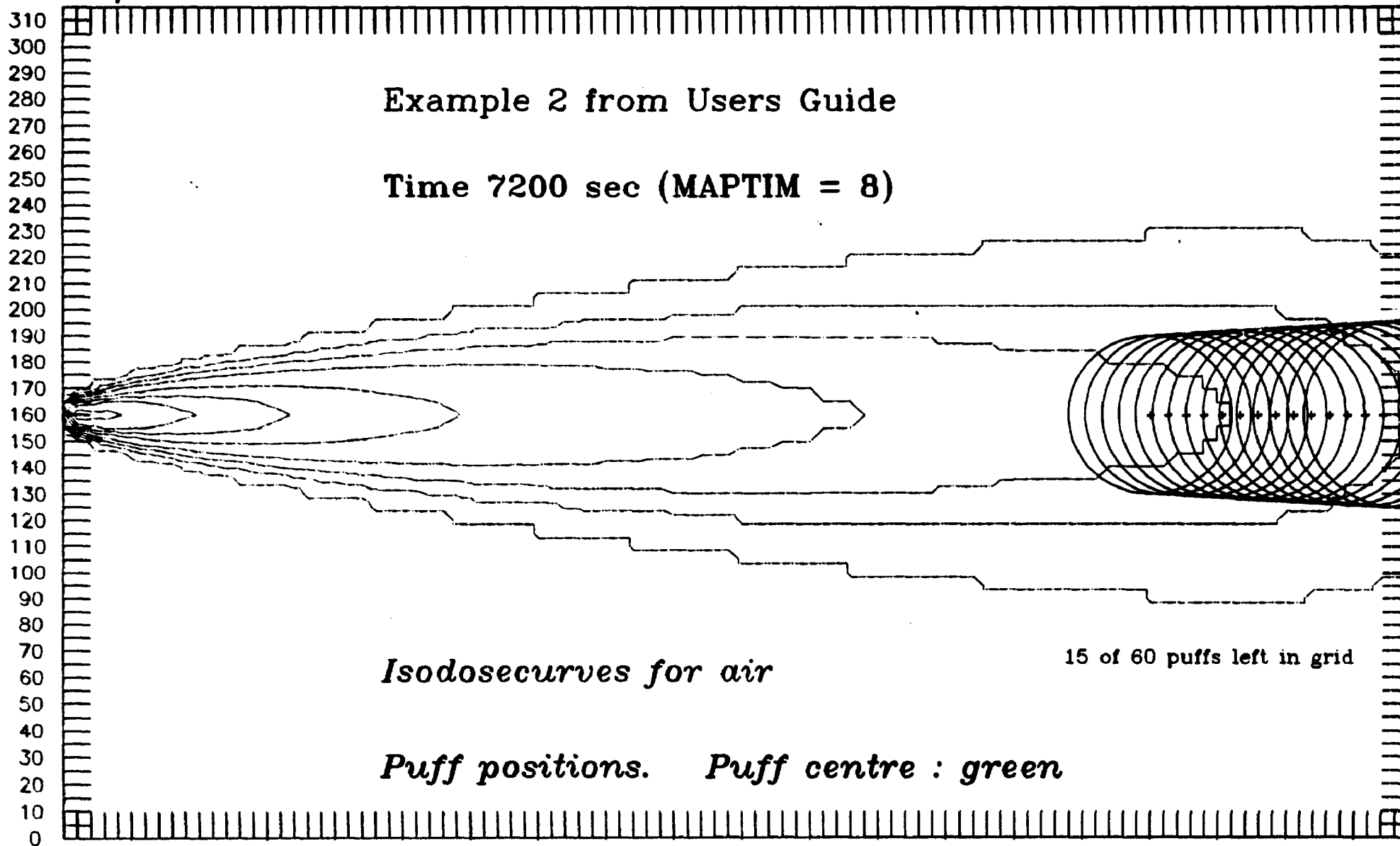
' 16:30 '

'RIS', 'D', 'D', 270., 5.00, 0.0

'STOP'

The output from this example is shown on the following pages.

Z-plan 0.00 MaxD: 6.86E-01 GS/C Different times



Ground 0.00 MaxD: 6.86E-03 GS/A Different times

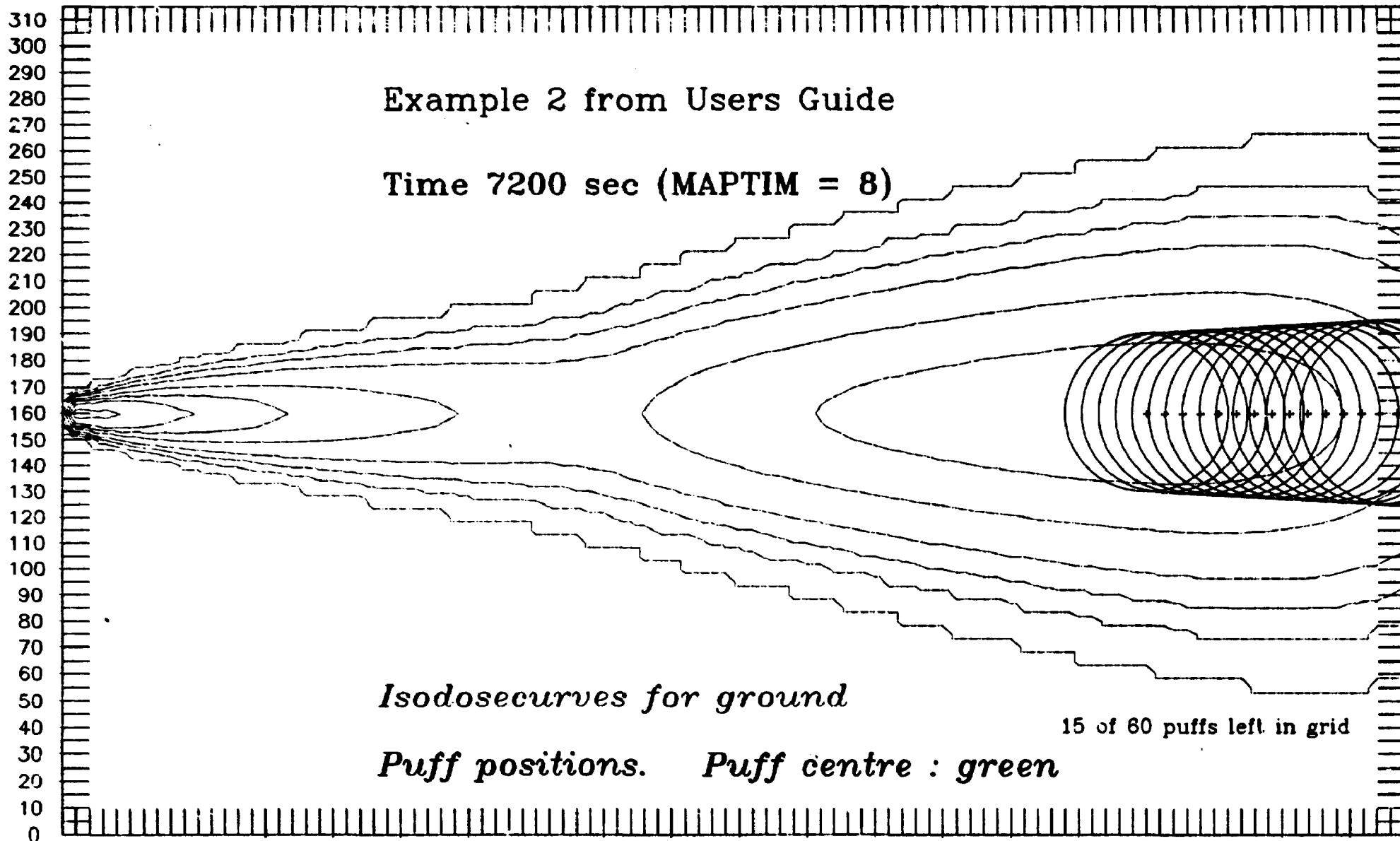
Example 2 from Users Guide

Time 7200 sec (MAPTIM = 8)

Isodosecurves for ground

Puff positions. Puff centre : green

15 of 80 puffs left in grid



0 25 50 75 100 125 150 175 200 225 250 275 300 325 350 375 400 425 450 475

QUEUE: 0
ORIGINATING LSN: 51 MCS: 1
PRIORITY: 30
USERCODE: FYSNYREEN.
CHARGECODE: 1025601.

18:25:24 BOT 2765 (FYSNYREEN)OBJECT/VER8K3/R/RIMPUFF ON USERPACK.
CODE COMPILED: OCT 28, 1985 12:58:32 BY FORTRAN77 36.120
TASK TYPE: COROUTINE(CALL)

PRIORITY: 30
USERCODE: FYSNYREEN.
CHARGECODE: 1025601.

18:25:34 2765 STACK EXTENDED FROM 688 TO 879 WORDS.
18:25:38 2765 STACK EXTENDED FROM 878 TO 985 WORDS.

18:50:42 EOT 2765 (FYSNYREEN)OBJECT/VER8K3/R/RIMPUFF ON USERPACK.

PROCESSOR TIME: 00:23:02.232 USERCODE: FYSNYREEN.
I/O TIME: 00:00:08.670 CHARGECODE: 1025601.
READYQ TIME: 00:00:36.110 LINES PRINTED: 2142.
INITPBIT TIME: 00:00:04.556 AVERAGE MEMORY USAGE: CODE=5544, DATA=244095
OTHERPBIT TIME: 00:00:04.429 MEMORY INTEGRAL: CODE=7711.846, DATA=339512.636
ELAPSED TIME: 00:25:08.312 DATA & CODE ALLOWED IN & OCCUPIED: GLOBAL.
INITIAL PBITS: 1704, OTHER PBITS: 1062.

18:50:43 EOJ 9851 DEMC4A.
PROCESSOR TIME: 00:00:00.073
I/O TIME: 00:00:00.159
READYQ TIME: 00:00:00.015
INITPBIT TIME: 00:00:00.030
OTHERPBIT TIME: 00:00:00.002
ELAPSED TIME: 00:25:09.541

USERCODE: FYSNYREEN.
CHARGECODE: 1025601.
AVERAGE MEMORY USAGE: CODE=41, DATA=995
MEMORY INTEGRAL: CODE=0.010, DATA=0.237
DATA & CODE ALLOWED IN & OCCUPIED: GLOBAL.
INITIAL PBITS: 27, OTHER PBITS: 1.

SOURCEHEIGHT=100 METERS, SOURCESTRENGTH=1/3600

CURRENT SOURCE DATA : NUMBER OF ACTIVE SOURCES : 1
1 0.00 32.00 3.33 0 3600***** 0.00000000

ZHGT = 99.999

DEMO 1. DRY AND WET DEPOSITION

KEY PARAMETER FOR CURRENT RUN:

NRELSE = 9999

ICOLS = 100 JROWS = 64 KPLANS = 1

NTADV = 60 MAPTIM = 900 TAU = 60

DELX = 500.00 DELY = 500.00 DELZ = 30.00

CHEMIN = 0.1000E-15 REFLEC = 1.00000 TDEL = 0

IDMP = 1 JDMP = 25 KDMP = 1

ISMODE = 1

INFRNT = YES

OUTDAT = OUTPUT OUTMOD = DISE

OUTWFD = NOGUTP
KFXTAPE = 0 (0 = NO, 1 = YES)

* COORDINATES FOR SOURCE AND WINDSTATIONS IN GRID-UNITS (GDU)

THE MIXING LAYER IS LIMITED AT: 1520.00 METERS IN STABILITY CAT. 1

THE MIXING LAYER IS LIMITED AT:	1200.00 METERS IN STABILITY CAT	2
THE MIXING LAYER IS LIMITED AT:	810.00 METERS IN STABILITY CAT	3
THE MIXING LAYER IS LIMITED AT:	570.00 METERS IN STABILITY CAT	4
THE MIXING LAYER IS LIMITED AT:	330.00 METERS IN STABILITY CAT	5
THE MIXING LAYER IS LIMITED AT:	210.00 METERS IN STABILITY CAT	6

IN THE CURRENT RUN, THE STABILITY-CLASSES ARE
 CONNECTED TO INTENSITY DATA AS FOLLOWS:
 STABILITY CLASS NO.: 1 2 3 4 5 6
 INTENSITY DATA : 0.42 0.34 0.26 0.17 0.09 0.04

MIXING HEIGHT VARIES WITH STABILITY .

IN THE CURRENT RUN, THE POTENTIAL TEMPERATURE
 GRADIENT IS SET TO: 0.0000

NO WIND SHEAR

DEPOSITION PARAMETERS

		DRY DEPOSITION PARAMETER, VD (M/S)					
WINDSPEED (M/S)		A	B	C	D	E	F
1	U < 1	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02
3	1 <= U < 3	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02
6	3 <= U < 6	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02
10	6 <= U < 10	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02
10	10 <= U	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02	1.0E-02

WASH-OUT COEFFICIENT

PRECIPITATION (MM/H)		LD(S-1)	TIME(SEC)
1	P < 1	4.20E-05	1692
3	1 <= P <= 3	1.06E-04	2928
3	3 < P	2.33E-04	2232

OUTDEP = OUTPUT

FRAME FOR PUFF ADVECTION:
 X: 0 => 99 - Y: 0 => 63

THE MIXING LAYER IS LIMITED AT: 1520.00 METERS IN STABILITY CAT 1

WIND PARAMETER DUMP

WINDJATA (CONSTANT WIND) FOR KFK-INTERCOMP. TEST

TIME = 12:0 DATE = 25-MAR-65 ITSP = 1000 SEC

NP = 1 NFX = 100 NFY = 64

MSL = 1 MSKIP = 0 K1ST = 0

RTE = 0.0 (DEG.) RCH = 100.0 (G.U.)

NAME	X	Y	CON	CONFAC	ALIGN	ISXMIN	ISXMAX	ISYMIN	ISYMAX
	GU	GU	DEG	DEG	GU	GU	GU	GU	GU
KFK	0.0	32.0	0.	1.0	0.0	1	100	1	54

TIMESTEP NO = 1

OBSERVATION TIME: 12:0

STATION	DIRECTION (DEG.)	VELOCITY (M/S)	STABILITY (-Y) (-Z)		RAIN (MM/H)
KFK	270.	5.0	0	0	0.00

STATION	U (M/S)	V (M/S)	RAIN (MM/H)
KFK	5.0	0.0	0.00

* TIMESTEP NO. 1 : ZH = 570.0 => ZMG = 19

=> (1.3126525113 , 32.0) DISTANCE: 656.32625566
 => U= 10.938770928 V= 0.0

900 SEC. AFTER START OF RELEASE
 TOT. 15 PUFFS RELEASED AND 0 HAVE LEFT THE GRID

	26	27	28	29	30	31	32	33	34	35	36	37
1	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.183E-11	4.507E-07	4.080E-04	4.040E-03	4.080E-04	4.507E-07	5.183E-11	0.000E+00
2	0.000E+00	0.000E+00	0.000E+00	1.222E-11	1.827E-08	2.979E-05	1.768E-02	1.712E-01	1.768E-02	2.979E-05	1.827E-08	1.222E-11
3	0.000E+00	0.000E+00	2.632E-12	1.348E-09	7.901E-07	3.140E-04	2.363E-02	1.348E-01	2.363E-02	3.140E-04	7.801E-07	1.348E-09
4	0.000E+00	5.531E-13	1.472E-10	4.022E-08	9.440E-06	1.079E-03	3.295E-02	1.472E-01	3.295E-02	1.079E-03	9.440E-06	4.022E-08
5	5.645E-14	2.087E-11	3.249E-09	4.743E-07	4.846E-05	2.351E-03	3.140E-02	3.249E-01	3.140E-02	2.351E-03	4.846E-05	4.743E-07
6	3.487E-12	3.593E-10	3.536E-08	2.857E-06	1.482E-04	3.557E-03	2.876E-02	3.593E-01	2.876E-02	3.557E-03	1.482E-04	2.857E-06
7	4.981E-11	3.543E-09	2.233E-07	1.073E-05	3.175E-04	4.594E-03	2.568E-02	4.981E-01	2.568E-02	4.594E-03	3.175E-04	1.073E-05
8	4.433E-10	2.235E-08	9.398E-07	2.871E-05	5.405E-04	4.523E-03	2.210E-02	4.433E-01	2.210E-02	5.405E-04	5.232E-03	5.405E-04
9	2.708E-09	9.872E-08	2.883E-06	6.000E-05	7.791E-04	5.515E-03	1.888E-02	2.708E-01	1.888E-02	5.515E-03	7.791E-04	6.000E-05
10	1.212E-08	3.279E-07	6.942E-06	1.042E-04	9.991E-04	5.507E-03	1.597E-02	1.212E-01	1.597E-02	5.507E-03	9.991E-04	1.042E-04
11	4.186E-08	8.660E-07	1.383E-05	1.575E-04	1.173E-03	5.278E-03	1.341E-02	4.186E-01	1.341E-02	5.278E-03	1.173E-03	1.575E-04
12	1.167E-07	1.897E-06	2.371E-05	2.231E-04	1.287E-03	4.904E-03	1.119E-02	1.167E-01	1.119E-02	4.904E-03	1.287E-03	2.371E-04
13	2.707E-07	3.558E-06	3.593E-05	3.640E-04	1.337E-03	4.438E-03	9.276E-03	2.707E-01	9.276E-03	4.438E-03	1.337E-03	3.593E-05
14	5.367E-07	5.848E-06	4.909E-05	3.033E-04	1.325E-03	3.920E-03	7.617E-03	5.367E-01	7.617E-03	3.920E-03	1.325E-03	3.033E-04
15	9.248E-07	8.560E-06	6.126E-05	3.271E-04	1.258E-03	3.379E-03	6.177E-03	9.248E-01	6.177E-03	3.379E-03	1.258E-03	3.271E-04
16	1.400E-06	1.126E-05	7.030E-05	3.312E-04	1.145E-03	2.834E-03	4.923E-03	1.400E-01	4.923E-03	2.834E-03	1.145E-03	3.312E-04
17	1.871E-06	1.333E-05	7.429E-05	3.142E-04	9.955E-04	2.301E-03	3.829E-03	1.871E-01	3.829E-03	2.301E-03	9.955E-04	3.142E-04
18	2.205E-06	1.425E-05	7.192E-05	2.795E-04	8.200E-04	1.791E-03	2.876E-03	2.205E-01	2.876E-03	1.791E-03	8.200E-04	2.795E-04
19	2.276E-06	1.357E-05	6.338E-05	2.230E-04	6.323E-04	1.318E-03	2.056E-03	2.276E-01	2.056E-03	1.318E-03	6.323E-04	2.276E-04
20	2.041E-06	1.140E-05	5.000E-05	1.708E-04	4.490E-04	9.018E-04	1.374E-03	1.533E-01	1.374E-03	9.018E-04	4.490E-04	1.708E-04
21	1.570E-06	8.344E-06	3.487E-05	1.138E-04	2.880E-04	5.619E-04	8.409E-04	1.570E-01	8.409E-04	5.619E-04	2.880E-04	1.138E-04
22	1.024E-06	5.237E-06	2.108E-05	6.650E-05	1.635E-04	3.120E-04	4.604E-04	1.024E-01	4.604E-04	3.120E-04	1.635E-04	6.650E-05
23	5.594E-07	2.780E-06	1.082E-05	3.346E-05	8.049E-05	1.511E-04	2.206E-04	5.594E-01	2.206E-04	1.511E-04	8.049E-05	3.346E-05
24	2.530E-07	1.231E-06	4.722E-06	1.425E-05	3.374E-05	6.255E-05	9.066E-05	2.530E-01	9.066E-05	6.255E-05	3.374E-05	1.425E-05
25	9.375E-08	4.494E-07	1.699E-06	5.058E-06	1.184E-05	2.176E-05	3.137E-05	3.544E-01	3.137E-05	2.176E-05	1.184E-05	5.058E-06
26	2.821E-08	1.338E-07	5.008E-07	1.477E-06	3.430E-06	6.267E-06	8.999E-06	2.821E-01	8.999E-06	6.267E-06	3.430E-06	1.477E-06
27	6.844E-09	3.223E-08	1.198E-07	3.511E-07	8.110E-07	1.475E-06	2.113E-06	6.844E-01	2.113E-06	1.475E-06	8.110E-07	3.511E-07
28	1.330E-09	6.234E-09	2.306E-08	6.732E-08	1.549E-07	2.811E-07	4.019E-07	1.330E-01	4.019E-07	2.811E-07	1.549E-07	6.732E-08
29	2.060E-10	9.629E-10	3.552E-09	1.034E-08	2.375E-08	4.301E-08	6.143E-08	2.060E-01	6.143E-08	4.301E-08	2.375E-08	1.034E-08
30	2.536E-11	1.183E-10	4.357E-10	1.266E-09	2.904E-09	5.254E-09	7.500E-09	2.536E-01	7.500E-09	5.254E-09	2.904E-09	1.266E-09
31	2.474E-12	1.153E-11	4.242E-11	1.232E-10	2.822E-10	5.103E-10	7.281E-10	2.474E-01	7.281E-10	5.103E-10	2.822E-10	1.232E-10
32	1.902E-13	8.855E-13	3.272E-12	9.494E-12	2.174E-11	3.930E-11	5.606E-11	1.902E-01	5.606E-11	3.930E-11	2.174E-11	9.494E-12
33	1.163E-14	5.416E-14	1.990E-13	5.770E-13	1.321E-12	2.386E-12	3.403E-12	1.163E-01	3.403E-12	2.386E-12	1.321E-12	5.770E-13
34	0.000E+00	0.000E+00	9.605E-15	2.785E-14	6.376E-14	1.152E-13	1.643E-13	0.000E+00	1.643E-13	1.152E-13	6.376E-14	2.785E-14
35	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
36	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
37	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
38	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
39	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
40	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
41	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
42	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
43	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
44	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
45	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
46	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
47	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
48	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
49	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00

180 SEC. AFTER START OF RELEASE
 TOT. 30 PUFFS RELEASED AND 0 HAVE LEFT THE GRID

	26	27	28	29	30	31	32	33	34	35	36	37
1	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.078E-01	9.040E-07	8.162E-04	8.081E-03	8.162E-04	9.040E-07	1.078E-01	0.000E+00
2	0.000E+00	0.000E+00	0.000E+00	2.664E-11	3.831E-01	6.052E-07	3.541E-04	3.742E-01	3.541E-04	6.052E-07	3.831E-01	6.664E-11
3	0.000E+00	0.000E+00	6.093E-12	2.981E-09	1.666E-01	1.588E-04	4.850E-02	2.742E-01	4.850E-02	1.588E-04	1.666E-01	2.981E-09
4	0.000E+00	1.366E-12	3.464E-10	9.065E-08	2.086E-01	3.020E-03	6.920E-02	3.886E-01	6.920E-02	3.020E-03	2.086E-01	9.065E-08
5	1.506E-13	5.283E-11	7.812E-09	1.096E-06	1.086E-01	1.086E-04	6.814E-02	1.689E-01	6.814E-02	1.086E-04	1.086E-01	1.096E-06
6	9.642E-12	9.335E-10	8.741E-08	6.796E-06	3.427E-01	8.066E-03	6.442E-02	1.336E-01	6.442E-02	8.066E-03	3.427E-01	6.796E-06
7	1.421E-10	3.250E-08	5.549E-06	2.642E-05	1.346E-01	1.079E-02	5.340E-02	8.729E-01	5.340E-02	1.079E-02	1.346E-01	2.642E-05
8	1.314E-09	6.229E-07	8.003E-06	7.348E-05	1.108E-01	1.079E-02	5.340E-02	8.729E-01	5.340E-02	1.079E-02	1.108E-01	7.348E-05
9	8.406E-09	2.878E-06	2.003E-05	1.605E-04	2.027E-01	4.408E-02	4.766E-02	4.408E-01	4.766E-02	4.408E-01	2.027E-01	1.605E-04
10	3.971E-08	1.008E-06	8.029E-05	2.932E-04	2.732E-01	1.477E-02	4.234E-02	6.052E-01	4.234E-02	6.052E-01	2.732E-01	2.932E-04
11	1.464E-07	6.829E-06	4.289E-05	4.690E-04	3.394E-01	1.498E-02	3.758E-02	5.134E-01	3.758E-02	5.134E-01	3.394E-01	4.690E-04
12	4.404E-07	2.655E-06	8.870E-05	6.781E-04	3.971E-01	4.811E-02	3.339E-02	4.399E-01	3.339E-02	4.399E-01	3.971E-01	6.781E-04
13	1.111E-06	1.355E-05	1.292E-04	9.069E-04	4.441E-01	1.441E-02	2.972E-02	3.799E-01	2.972E-02	3.799E-01	4.441E-01	9.069E-04
14	2.474E-06	4.469E-05	1.939E-04	1.141E-03	5.209E-01	3.555E-02	2.652E-02	3.301E-01	2.652E-02	3.301E-01	5.209E-01	1.141E-03
15	4.874E-06	8.942E-05	3.573E-04	1.577E-03	5.266E-01	1.172E-02	1.909E-02	2.344E-01	1.172E-02	2.344E-01	5.266E-01	1.577E-03
16	8.716E-06	6.942E-05	4.496E-04	1.761E-03	5.201E-01	1.247E-02	2.126E-02	2.344E-01	1.247E-02	2.344E-01	5.201E-01	1.761E-03
17	1.437E-05	8.942E-05	4.496E-04	1.761E-03	5.201E-01	1.247E-02	2.126E-02	2.344E-01	1.247E-02	2.344E-01	5.201E-01	1.761E-03
18	2.205E-05	1.121E-04	5.411E-04	1.915E-03	5.258E-01	1.098E-02	1.718E-02	1.999E-01	1.098E-02	1.999E-01	5.258E-01	1.915E-03
19	3.202E-05	1.556E-04	8.309E-04	2.038E-03	5.187E-01	9.244E-03	1.534E-02	1.558E-01	9.244E-03	1.558E-02	5.187E-01	2.038E-03
20	4.405E-05	1.955E-04	1.146E-03	2.288E-03	5.066E-01	8.141E-03	1.394E-02	1.558E-01	8.141E-03	1.394E-02	5.066E-01	2.288E-03
21	5.600E-05	2.343E-04	1.695E-03	2.186E-03	4.905E-01	8.141E-03	1.257E-02	1.616E-01	8.141E-03	1.257E-02	4.905E-01	2.186E-03
22	7.360E-05	2.731E-04	2.393E-03	2.214E-03	4.749E-01	8.141E-03	1.134E-02	1.616E-01	8.141E-03	1.134E-02	4.749E-01	2.214E-03
23	9.013E-05	3.100E-04	3.049E-03	2.214E-03	4.492E-01	7.749E-03	1.022E-02	1.133E-01	7.749E-03	1.022E-02	4.492E-01	2.214E-03
24	1.070E-04	3.437E-04	3.303E-03	2.188E-03	4.254E-01	6.879E-03	9.199E-03	1.011E-01	6.879E-03	9.199E-03	4.254E-01	2.188E-03
25	1.237E-04	3.729E-04	3.673E-03	2.140E-03	4.003E-01	6.292E-03	8.270E-03	9.088E-01	6.292E-03	8.270E-03	4.003E-01	2.140E-03
26	1.533E-04	4.146E-04	4.756E-03	1.993E-03	3.747E-01	5.734E-03	7.419E-03	8.087E-01	5.734E-03	7.419E-03	3.747E-01	1.993E-03
27	1.654E-04	4.250E-04	4.963E-03	1.886E-03	3.537E-01	5.203E-03	6.639E-03	7.292E-01	5.203E-03	6.639E-03	3.537E-01	1.886E-03
28	1.744E-04	4.301E-04	5.131E-03	1.773E-03	3.293E-01	4.703E-03	5.920E-03	6.395E-01	4.703E-03	5.920E-03	3.293E-01	1.773E-03
29	1.806E-04	4.273E-04	5.248E-03	1.650E-03	3.068E-01	4.223E-03	5.257E-03	5.657E-01	4.223E-03	5.257E-03	3.068E-01	1.650E-03
30	1.831E-04	4.175E-04	5.333E-03	1.519E-03	2.803E-01	3.771E-03	4.645E-03	4.980E-01	3.771E-03	4.645E-03	2.803E-01	1.519E-03
31	1.818E-04	4.010E-04	5.383E-03	1.382E-03	2.403E-01	3.343E-03	4.078E-03	4.378E-01	3.343E-03	4.078E-03	2.403E-01	1.382E-03
32	1.767E-04	3.781E-04	5.245E-03	1.240E-03	2.143E-01	2.938E-03	3.553E-03	3.786E-01	2.938E-03	3.553E-03	2.143E-01	1.240E-03
33	1.675E-04	3.493E-04	4.933E-03	1.095E-03	1.888E-01	2.555E-03	3.065E-03	3.258E-01	2.555E-03	3.065E-03	1.888E-01	1.095E-03
34	1.555E-04	3.156E-04	4.573E-03	9.504E-04	1.641E-01	1.955E-03	2.614E-03	2.771E-01	1.955E-03	2.614E-03	1.641E-01	9.504E-04
35	1.400E-04	2.780E-04	4.199E-03	8.077E-04	1.417E-01	1.544E-03	2.197E-03	2.324E-01	1.544E-03	2.197E-03	1.417E-01	8.077E-04
36	1.223E-04	2.380E-04	3.819E-03	6.698E-04	1.157E-01	1.146E-03	1.815E-03	1.916E-01	1.146E-03	1.815E-03	1.157E-01	6.698E-04
37	1.032E-04	1.974E-04	3.409E-03	5.400E-04	9.699E-02	8.288E-04	1.575E-03	1.321E-01	8.288E-04	1.575E-03	9.699E-02	5.400E-04
38	8.375E-05	1.579E-04	2.706E-03	4.214E-04	7.699E-02	6.828E-04	1.157E-03	1.033E-01	6.828E-04	1.157E-03	7.699E-02	4.214E-04
39	6.524E-05	1.213E-04	2.055E-03	3.169E-04	6.444E-02	5.600E-04	8.852E-04	8.852E-01	5.600E-04	8.852E-01	6.444E-02	3.169E-04
40	4.852E-05	9.220E-05	1.499E-03	2.288E-04	5.186E-02	4.444E-04	6.546E-04	6.871E-01	4.444E-04	6.871E-01	5.186E-02	2.288E-04
41	3.433E-05	6.251E-05	1.033E-03	1.578E-04	3.186E-02	3.186E-04	4.657E-04	4.882E-01	3.186E-04	4.882E-01	3.186E-02	1.578E-04
42	2.304E-05	4.159E-05	6.836E-04	1.033E-04	1.844E-02	1.794E-04	3.171E-04	3.322E-01	1.794E-04	3.322E-01	1.844E-02	1.033E-04
43	1.461E-05	2.599E-05	4.236E-04	6.445E-05	1.108E-02	9.757E-05	2.059E-04	2.155E-01	9.757E-05	2.155E-01	1.108E-02	6.445E-05
44	8.730E-06	1.555E-05	2.517E-04	3.790E-05	6.800E-02	6.467E-05	7.406E-05	7.406E-01	6.467E-05	7.406E-01	6.800E-02	3.790E-05
45	4.598E-06	8.687E-06	1.411E-04	2.099E-05	4.484E-02	4.484E-05	4.075E-05	4.259E-01	4.484E-05	4.259E-01	4.484E-02	2.099E-05
46	2.520E-06	4.553E-06	7.365E-05	1.092E-05	2.484E-02	2.484E-05	2.108E-05	2.203E-01	2.484E-05	2.203E-01	2.484E-02	1.092E-05
47	1.271E-06	2.333E-06	3.603E-05	5.324E-06	1.220E-02	1.220E-05	1.023E-05	1.058E-01	1.023E-05	1.058E-01	1.220E-02	5.324E-06
48	5.840E-07	1.023E-06	1.644E-05	2.427E-06	6.264E-02	6.264E-05	4.642E-06	4.848E-01	4.642E-06	4.848E-01	6.264E-02	2.427E-06
49												

TIMESTEP NO = 6

OBSERVATION TIME: 14:3

STATION	DIRECTION (DEG.)	VELOCITY (M/S)	STABILITY (-Y) (-Z)		RAIN (MM/H)
KFK	270.	5.0	0	0	0.00

STATION	U (M/S)	V (M/S)	RAIN (MM/H)
KFK	5.0	0.0	0.00

* TIMESTEP NO. 6 : ZH = 570.0 => ZMG = 19

8.3. Example no. 3

The files INDATA and WINDDA for external gamma dose calculations are as shown below:

8.3.1. INDATA file

```
&PRIMDA
TITLE='PROBLEM 1. NO DEPOSITION ',
ICOLS=25,JROWS=25,KPLANS=1,DELX=500.,DELY=500.,DELZ=30.,
TDEL=0.0,CHEMIN=0.1E-15,NTADV=20,TAU=20,MAPTIM=900,REFLEC=1.,
NRELSE=3600,IDMP=1,JDMP=6,KDMP=1,ISMODE=1,ITAPIN=0,
KOORD=0,XUTM=332.7609,YUTM=5381.6323,
INPRNT='YES',OUTDAT='NOOUTP',OUTMOD='DOSE',OUTWFD='NOOUTP'
&END
&RELDAT
PUFFTX='SOURCEHEIGHT=10 METERS, SOURCESTRENGTH= 1',
NRMULT=1,
XSOURC(1)=0.0,YSOURC(1)=12.0,ZSOURC(1)=0.33333,
STRTRL(1)=0,STOPRL(1)=3600,SOURST(1)=1.0,HEATFX(1)=0.,
&END
&STABDA
STABTX='MIXING HEIGHT VARIES WITH STABILITY .',
DTDZ=0.,ZMTAB(1)=0.0,ZMTAB(2)=0.,ZMTAB(3)=0.,
ZMTAB(4)=0.,ZMTAB(5)=0.,ZMTAB(6)=0.,
DSHEAR=0,ALFSHE=-5.0,HSHEMI=0.0,HSHEMA=200.0,
USH=0,USTAR=0.1397,LMOBUK=44.64,ZROUGH=0.1,DZERO=0.0,
DUSDUM=0,
DEPMOD=0,OUTDEP='NOOUTP',
VDTAB(1,1)=0.010,VDTAB(2,1)=0.010,VDTAB(3,1)=0.010,
VDTAB(4,1)=0.010,VDTAB(5,1)=0.010,VDTAB(6,1)=0.010,
VDTAB(1,2)=0.010,VDTAB(2,2)=0.010,VDTAB(3,2)=0.010,
VDTAB(4,2)=0.010,VDTAB(5,2)=0.010,VDTAB(6,2)=0.010,
VDTAB(1,3)=0.010,VDTAB(2,3)=0.010,VDTAB(3,3)=0.010,
```



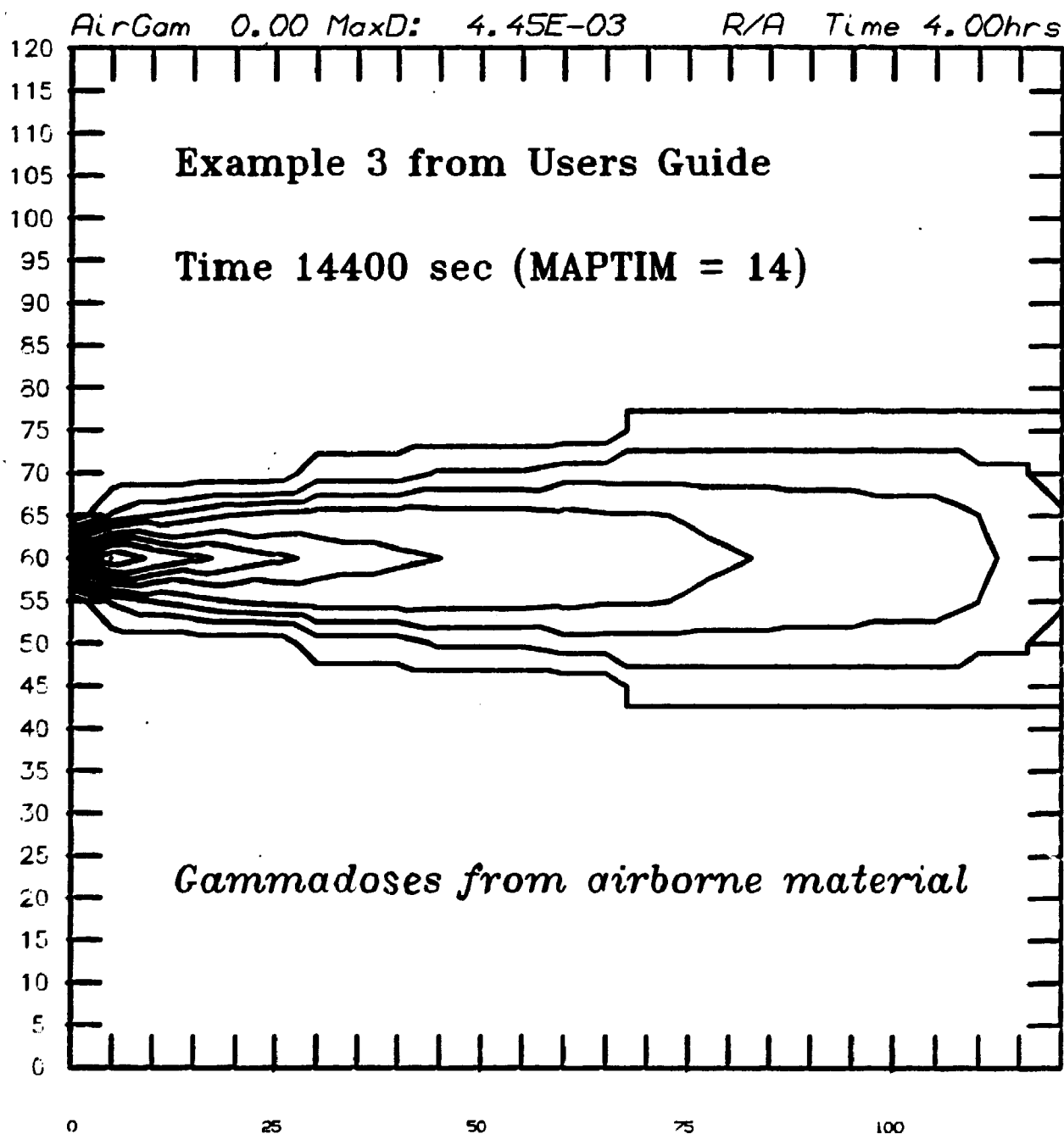
```
VDTAB(4,3)=0.010,VDTAB(5,3)=0.010,VDTAB(6,3)=0.010,  
VDTAB(1,4)=0.010,VDTAB(2,4)=0.010,VDTAB(3,4)=0.010,  
VDTAB(4,4)=0.010,VDTAB(5,4)=0.010,VDTAB(6,4)=0.010,  
VDTAB(1,5)=0.010,VDTAB(2,5)=0.010,VDTAB(3,5)=0.010,  
VDTAB(4,5)=0.010,VDTAB(5,5)=0.010,VDTAB(6,5)=0.010,  
LDTAB(1)=0.000042,LDTAB(2)=0.000106,LDTAB(3)=0.000233,  
TIMRAI(1)=1692,TIMRAI(2)=2628,TIMRAI(3)=2232  
&END  
&GAMDA  
GAMMOD=1,OUTGAM='OUTPUT',  
FGAM(1)=0.0,FGAM(2)=0.0,FGAM(3)=0.0,FGAM(4)=0.0,FGAM(5)=0.0,  
FGAM(6)=1.0,FGAM(7)=0.0,FGAM(8)=0.0  
&END
```

Note: One space is required in the beginning of each line.

8.3.2. WINDDA file

```
&WINPAR
WNTLE='WINDDATA (CONSTANT WIND) FOR GAMMA DOSES TEST',
TIME=' 12:00 ',DATE='21-JUN-84 ',ITSP=14400,
NP=1,NFX=25,NFY=25,NSTL=1,NSKIP=0,
RTE=0.,RCH=100.,
NAMST(1)='RIS',X(1)=1.,Y(1)=12.,COR(1)=0.,CONFAC(1)=1.0000,
A(1)=0.,ISXMIN(1)=1,ISXMAX(1)=25,ISYMIN(1)=1,ISYMAX(1)=25,
&END
' 12:00 '
'RIS','D','D',270.,5.0,0
'STOP'
```

The output from this example is shown on the following pages.



GAMMADOSES. NO DEPOSITION

KEY PARAMETER FOR CURRENT RUN:

NRELS = 3600
ICOLS = 25 IROWS = 25 KPLANS = 1
NTADM = 20 NAFIM = 900 TAU = 20
DELX = 500.00 DELY = 500.00 DELZ = 30.00
CHEMIN = 0.100E-15 REFLEC = 1.00000 TDEL = 0
IDMP = 1 JDMP = 6 KJMP = 1

ISMODE = 1

INPRNT = YES

CUTDAT = OUTPUT OUTNO = 000E

OUTWFO = NOOUTP
KFRTAPE = 0 (0 = NO, 1 = YES)

* COORDINATES FOR SOURCE AND WINDSTATIONS IN GRID-UNITS (GDU)

SOURCEHEIGHT=10 METERS, SOURCESTRENGTH= 1

CURRENT SOURCE DATA : NUMBER OF ACTIVE SOURCES : 1
1 0.00 12.00 0.33 0 3600 1.000000000 0.000000000
ZMGT = 9.999999999

IN THE CURRENT RUN, THE STABILITY-CLASSES ARE
CONNECTED TO INTENSITY DATA AS FOLLOWS:
STABILITY CLASS NC: 1 2 3 4 5 6
INTENSITY DATA : 0.42 0.34 0.26 0.17 0.09 0.04

MIXING HEIGHT VARIES WITH STABILITY .

IN THE CURRENT RUN, THE POTENTIAL TEMPERATURE
GRADIENT IS SET TO: 0.0000

NO WIND SHEAR

NO DEPOSITION

EXTERNAL CANALUSES FROM PUFFS
FREQUENCIES IN ENERGY GROUPS
0.00 0.00 0.00 0.00 0.00 0.00

FRAME FOR PUFF ADVECTION:
X: 0 => 24 . Y : 0 => 24

NO FINAL MIXING-DEPTH IS SPECIFIED.

THE MIXING LAYER IS LIMITED AT:	0.00 METERS IN STABILITY CAT	1
THE MIXING LAYER IS LIMITED AT:	0.00 METERS IN STABILITY CAT	2
THE MIXING LAYER IS LIMITED AT:	0.00 METERS IN STABILITY CAT	3
THE MIXING LAYER IS LIMITED AT:	0.00 METERS IN STABILITY CAT	4
THE MIXING LAYER IS LIMITED AT:	0.00 METERS IN STABILITY CAT	5
THE MIXING LAYER IS LIMITED AT:	0.00 METERS IN STABILITY CAT	6

WIND PARAMETER DUMP

WINDATA (CONSTANT WIND) FOR GAMMA D0SES TEST

TIME = 12:0 DATE = 21-JUN-34 ITSP = 14400 SEC
NP = 1 NFX = 25 NFY = 25
NSTL = 1 NSHIP = C K1ST = 0
RTE = 0.0 (SEG.) AC1 = 100.0 (C.U.)

NAME	X GU	Y GU	CBF SEG	CONFAC	ALIEJ SEG	ISXMIN GU	ISXMAX GU	ISYMIN GU	ISYMAX GU
KFK	1.0	12.0	0.	1.0	0.0	1	25	1	25

TIMESTEP NO = 1
OBSERVATION TIME: 12:00
STATION DIRECTION VELOCITY RAIN
(DEG) (M/S) (CM/H)
KFK 270.0 5.0 0.00

STATION	U	V	RAI
(M/S)	(M/S)	(M/S)	
KFK	5.0	0.0	0.00

* TIMESTEP NO. 1 : ZM = 0.0 => ZMG = 0

8.4. Example no. 4

The files INDATA and WINDDA for calculations of integrated air-concentrations with wind shear are shown below:

8.4.1. INDATA file

```
&PRIMDA
TITLE='KFK-MODELCOMPARISON JAN. 1985: EXPERIMENT 1. SHEAR',
ICOLS=100,JROWS=64,KPLANS=1,DELX=300.,DELY=300.,DELZ=30.,
TDEL=0.0,CHEMIN=0.1E-15,NTADV=10,TAU=10,MAPTIM=600,REFLEC=1.,
NRELSE=9999, IDMP=1,JDMP=24,KDMP=1, ISMODE=4,ITAPIN=0,
KOORD=0,XUTM= 0.,YUTM=0.,
INPRNT='YES',OUTDAT='OUTPUT',OUTMOD='DOSE',OUTWFD='NOOUTP'
&END
&RELDAT
PUFPTX='SOURCEHEIGHT=100 METERS, SOURCESTRENGTH=1/3600',
NRMULT=1,
XSOURC(1)=0.00 ,YSOURC(1)=31.0,ZSOURC(1)=0.33333333333,
STRTRL(1)=0,STOPRL(1)=3600,SOURST(1)=2.7777777778,HEATFX(1)=0.,
&END
&STABDA
STABTX='MIXING HEIGHT IS INFINITE',
DTDZ=0.,ZMTAB(1)=0.,ZMTAB(2)=0.,ZMTAB(3)=0.,ZMTAB(4)=0.,
ZMTAB(5)= 0.,ZMTAB(6)=0.,
DSHEAR=1,ALFSHE=45.0,HSHEMI=1.0,HSHEMA=201.0,
USH=1,USTAR=0.265,LMOBUK=70.0,ZROUGH=1.2,DZERO=0.0,
DUSDUM=0,
DEP:IOD=0,OUTDEP='NOOUTP',
VDTAB(1,1)=0.010,VDTAB(2,1)=0.010,VDTAB(3,1)=0.010,
VDTAB(4,1)=0.010,VDTAB(5,1)=0.010,VDTAB(6,1)=0.010,
VDTAB(1,2)=0.010,VDTAB(2,2)=0.010,VDTAB(3,2)=0.010,
VDTAB(4,2)=0.010,VDTAB(5,2)=0.010,VDTAB(6,2)=0.010,
VDTAB(1,3)=0.010,VDTAB(2,3)=0.010,VDTAB(3,3)=0.010,
```

```
VDTAB(4,3)=0.010,VDTAB(5,3)=0.010,VDTAB(6,3)=0.010,  
VDTAB(1,4)=0.010,VDTAB(2,4)=0.010,VDTAB(3,4)=0.010,  
VDTAB(4,4)=0.010,VDTAB(5,4)=0.010,VDTAB(6,4)=0.010,  
VDTAB(1,5)=0.010,VDTAB(2,5)=0.010,VDTAB(3,5)=0.010,  
VDTAB(4,5)=0.010,VDTAB(5,5)=0.010,VDTAB(6,5)=0.010,  
LDTAB(1)=0.000042,LDTAB(2)=0.000106,LDTAB(3)=0.000233,  
TIMRAI(1)=1692,TIMRAI(2)=2628,TIMRAI(3)=2232  
&END  
&GAMDA  
GAMMOD=0,OUTGAM='NOOUTP',  
FGAM(1)=0.0,FGAM(2)=0.0,FGAM(3)=0.0,FGAM(4)=0.0,FGAM(5)=0.0,  
FGAM(6)=1.0,FGAM(7)=0.0,FGAM(8)=0.0  
&END
```

Note: One space is required in the beginning of each line.

8.4.2. WINDDA file

```
&WINPAR
WNDTLE='WINDDATA KFK EXPERIMENT NO. 1 ',
TIME=' 12:10',DATE='14-FEB-85',ITSP=600,
NP=1,NFX=100,NFY=64,NSTL=1,NSKIP=0,
RTE=0.,RCH=100.,
NAMST(1)='KFK',X(1)=1.,Y(1)=32.,COR(1)=0.,CONFAC(1)=1.0000,
A(1)=0.,ISXMIN(1)=1,ISXMAX(1)=100,ISYMIN(1)=1,ISYMAX(1)=64,
&END
' 12:10'
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 12:20'
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 12:30'
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 12:40'
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 12:50'
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 13:00'
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 13:10'
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 13:20'
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 13:30'
```

'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 13:40 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 13:50 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 14:00 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 14:10 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 14:20 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 14:30 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 14:40 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 14:50 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 15:00 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 15:10 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 15:20 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 15:30 '

'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 15:40 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 15:50 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 16:00 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 16:10 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 16:20 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 16:30 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 16:40 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 16:50 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 17:00 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 17:10 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 17:20 '
'KFK',2.6,2.3,270,1.8779,0.0
'EOWR'
' 17:30 '

'KFK',2.6,2.3,270,1.8779,0.0

'EOWR'

' 17:40 '

'KFK',2.6,2.3,270,1.8779,0.0

'EOWR'

' 17:50 '

'KFK',2.6,2.3,270,1.8779,0.0

'EOWR'

' 18:00 '

'KFK',2.6,2.3,270,1.8779,0.0

'EOWR'

' 18:10 '

'KFK',2.6,2.3,270,1.8779,0.0

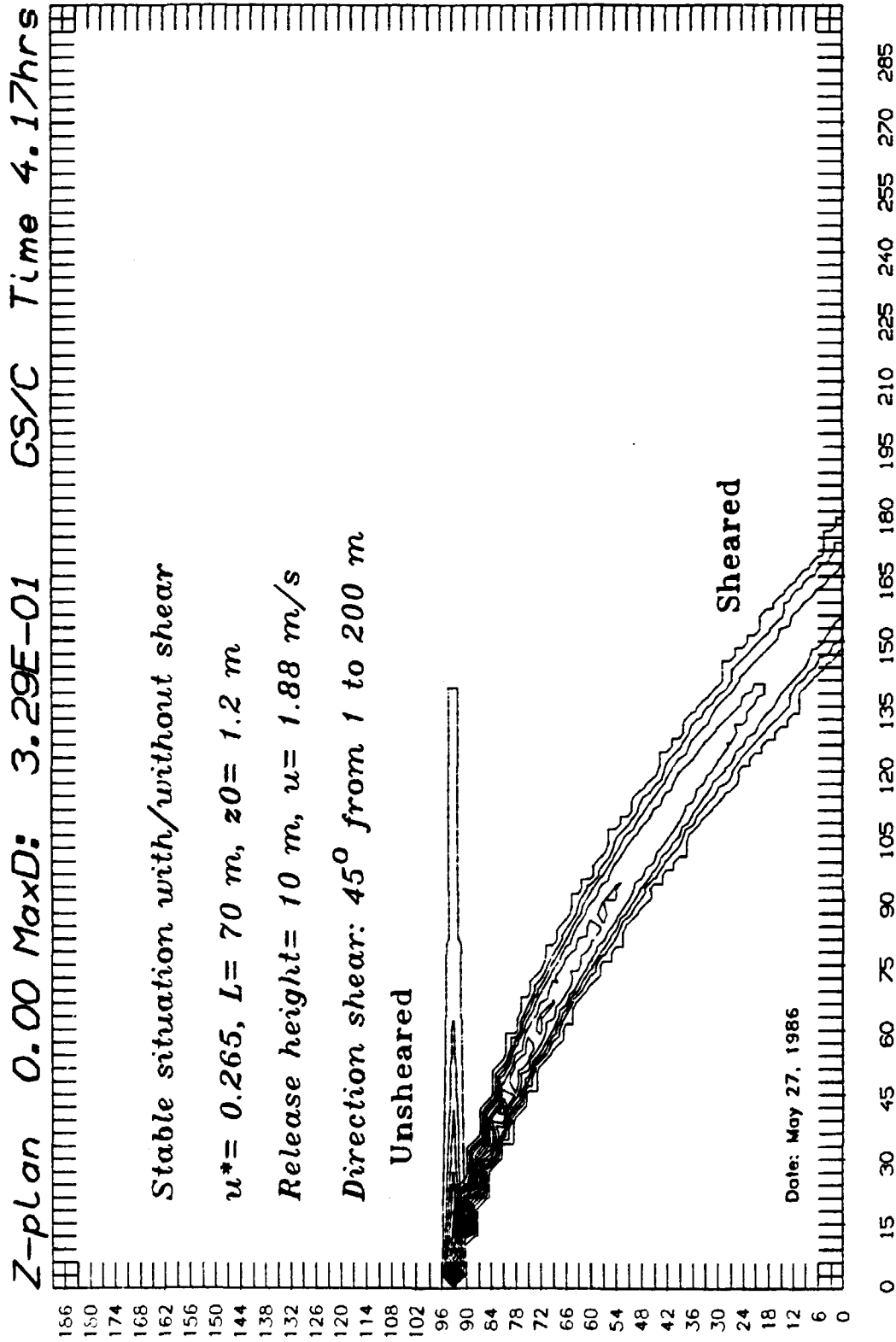
'EOWR'

' 18:20 '

'KFK',2.6,2.3,270,1.8779,0.0

'STOP'





Example no. 4: Air concentrations at ground level.

8.5. Example no. 5

The files INDATA and WINDDA for calculations of integrated concentrations of a fictive radioactive isotope with a half-life of 1 hour is shown below.

The data is the same as in example 2 except for the isotope data.

8.5.1. INDATA file

```
&PRIMDA
TITLE='DEMO 1. DRY AND WET DEPOSITION ',
ICOLS=100,JROWS=64,KPLANS=1,DELX=300.,DELY=300.,DELZ=30.,
TDEL=0.0,CHEMIN=0.1E-15,NTADV=60,TAU=60,MAPTIM=900,REFLEC=1.,
NRELSE=9999,IDMP=1,JDMP=26,KDMP=1,ISMODE=1,ITAPIN=0,
KOORD=0,XUTM=332.7609,YUTM=5381.6323,
INPRNT='YES',OUTDAT='OUTPUT',OUTMOD='DOSE',OUTWFD='NOOUTP'
&END
&RELDAT
PUFCTX='SOURCEHEIGHT=100 METERS, SOURCESTRENGTH=1/3600',
NRMULT=1,
XSOURC(1)=0.0,YSOURC(1)=32.0,ZSOURC(1)=3.3333,
STRTRL(1)=0,STOPRL(1)=3600,SOURST(1)=277.77777778,HEATFX(1)=0.,
ISNAVN(1)='FIKTIV',ISDCAY(1)=1.9254088E-4
&END
&STABDA
STABTX='MIXING HEIGHT VARIES WITH STABILITY .',
DTDZ=0.,ZMTAB(1)=1620.0,ZMTAB(2)=1200.,ZMTAB(3)=810.,
ZMTAB(4)=570.,ZMTAB(5)=330.,ZMTAB(6)=210.,
SIGYIN=1.,SIGZIN=1.0,
DSHEAR=0,ALFSHE=-5.0,HSHEMI=0.0,HSHEMA=200.0,
USH=0,USTAR=0.1397,LMOBUK=44.64,ZROUGH=0.1,DZERO=0.0,
DUSDUM=0,
DEPMOD=1,OUTDEP='OUTPUT',
```

```
VDTAB(1,1)=0.010,VDTAB(2,1)=0.010,VDTAB(3,1)=0.010,  
VDTAB(4,1)=0.010,VDTAB(5,1)=0.010,VDTAB(6,1)=0.010,  
VDTAB(1,2)=0.010,VDTAB(2,2)=0.010,VDTAB(3,2)=0.010,  
VDTAB(4,2)=0.010,VDTAB(5,2)=0.010,VDTAB(6,2)=0.010,  
VDTAB(1,3)=0.010,VDTAB(2,3)=0.010,VDTAB(3,3)=0.010,  
VDTAB(4,3)=0.010,VDTAB(5,3)=0.010,VDTAB(6,3)=0.010,  
VDTAB(1,4)=0.010,VDTAB(2,4)=0.010,VDTAB(3,4)=0.010,  
VDTAB(4,4)=0.010,VDTAB(5,4)=0.010,VDTAB(6,4)=0.010,  
VDTAB(1,5)=0.010,VDTAB(2,5)=0.010,VDTAB(3,5)=0.010,  
VDTAB(4,5)=0.010,VDTAB(5,5)=0.010,VDTAB(6,5)=0.010,  
LDTAB(1)=0.000042,LDTAB(2)=0.000106,LDTAB(3)=0.000233,  
TIMRAI(1)=1692,TIMRAI(2)=2628,TIMRAI(3)=2232  
&END
```

Note: One space is required in the beginning of each line.

8.5.2. WINDDA file

&WINPAR

WNTLE='WINDDATA (CONSTANT WIND) FOR KFK-INTERCOMP. TEST',
TIME=' 12:00 ',DATE=' 25-MAR-85 ',ITSP=1800,
NP=1,NFX=100,NFY=64,NSTL=1,NSKIP=0,
RTE=0.,RCH=100.,HWOBS=100.,
NAMST(1)='KFK',X(1)=0.,Y(1)=32.,COR(1)=0.,CONFAC(1)=1.0000,
A(1)=0.,ISXMIN(1)=1,ISXMAX(1)=100,ISYMIN(1)=1,ISYMAX(1)=64,
&END

' 12:00 '

'KFK','D','D',270.,5.00,0.0

'EOWR'

' 12:30 '

'KFK','D','D',270.,5.00,0.0

'EOWR'

' 13:00 '

'KFK','D','D',270.,5.00,0.0

'EOWR'

' 13:30 '

'KFK','D','D',270.,5.00,2.0

'EOWR'

' 14:00 '

'KFK','D','D',270.,5.00,0.0

'EOWR'

' 14:30 '

'KFK','D','D',270.,5.00,0.0

'EOWR'

' 15:00 '

'KFK','D','D',270.,5.00,0.0

'EOWR'

' 15:30 '

'KFK','D','D',270.,5.00,0.0

'EOWR'

' 16:00 '

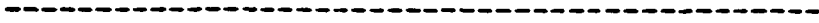
'KFK', 'D', 'D', 270., 5.00, 0.0

'EOWR'

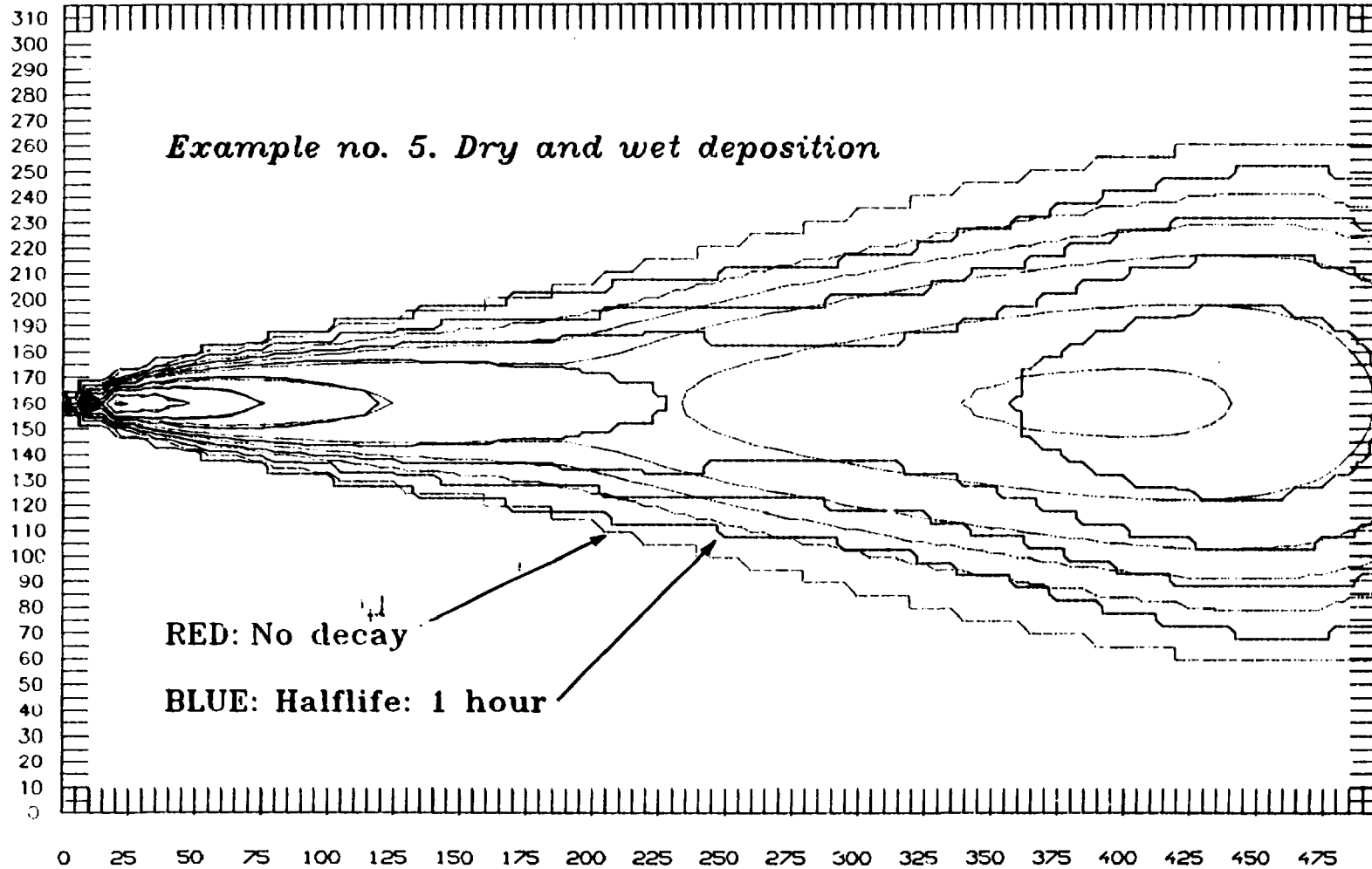
' 16:30'

'KFK', 'D', 'D', 270., 5.00, 0.0

'STOP'



Ground 0.00 MaxD: 9.46E-03 GS/A Time 3.00hrs



Example no. 5: Concentrations of deposited material

8.6. Example no. 6

The files INDATA and WINDDA for calculations of total individual and collective doses from a release of Iodine 131.

8.6.1. INDATA file

```
&PRIMDA
TITLE='RINGHALS: IODINE DOSES TO BONE MARROW: LAESQ',
ICOLS=100,JROWS=100,KPLANS=1,DELX=4000.,DELY=4000.,DELZ=30.,
TOEL=0.0,CHEMIN=0.1E-15,NTADV=60,TAU=60,MAPTIM=900,REFLEC=1.,
NRELSE=10860,ICMP= 10,JDMP=34,KDMP=1,ISMODE=1,ITAPIN=0,
KOORD=1,XUTM=400.0000,YUTM=6030.0000,IBFOPT=4,
INPRNT='YES',OUTDAT='NOOUTP',OUTMOD='DOSE',OUTWFD='NOOUTP',
OUTBEP='OUTPUT'
&END
&RELDAT
PUFCTX='SOURCEHEIGHT=100 METERS, SOURCESTRENGTH=5.865E+7 CI',
NRMULT=1,
XSOURC(1)=690.0,YSOURC(1)=6200.0,ZSOURC(1)=3.333333333,
STRTRL(1)=0,STOPRL(1)=10800,SOURST(1)=5430.55555556,
HEATFX(1)=0.,
ISNAVN(1)='J 131 ',ISDCAY(1)=9.941E-7
&END
&STABDA
STABTX='MIXING HEIGHT VARIES WITH STABILITY .',
DTDZ=0.,ZMTAB(1)=1020.0,ZMTAB(2)=1020.,ZMTAB(3)=1020.,
ZMTAB(4)=1020.,ZMTAB(5)=510.,ZMTAB(6)=210.,
SIGYIN=1.,SIGZIN=1.0,
DSHEAR=0,ALFSHE=-5.0,HSHEMI=0.0,HSHEMA=200.0,
USH=0,USTAR=0.1397,LMOBUK=44.64,ZROUGH=0.1,DZERO=0.0,
DUSDUM=0,
DEPMOD=1,OUTDEP='NOOUTP',
VDTAB(1,1)=0.010,VDTAB(2,1)=0.010,VDTAB(3,1)=0.010,
```

```
VDTAB(4,1)=0.010,VDTAB(5,1)=0.010,VDTAB(6,1)=0.0005,  
VDTAB(1,2)=0.010,VDTAB(2,2)=0.010,VDTAB(3,2)=0.010,  
VDTAB(4,2)=0.010,VDTAB(5,2)=0.010,VDTAB(6,2)=0.002,  
VDTAB(1,3)=0.010,VDTAB(2,3)=0.010,VDTAB(3,3)=0.010,  
VDTAB(4,3)=0.010,VDTAB(5,3)=0.010,VDTAB(6,3)=0.004,  
VDTAB(1,4)=0.010,VDTAB(2,4)=0.010,VDTAB(3,4)=0.010,  
VDTAB(4,4)=0.010,VDTAB(5,4)=0.010,VDTAB(6,4)=0.007,  
VDTAB(1,5)=0.010,VDTAB(2,5)=0.010,VDTAB(3,5)=0.010,  
VDTAB(4,5)=0.010,VDTAB(5,5)=0.010,VDTAB(6,5)=0.010,  
LDTAB(1)=0.000100,LDTAB(2)=0.000350,LDTAB(3)=0.000350,  
TIMRAI(1)=3600,TIMRAI(2)=3600,TIMRAI(3)=3600  
&END  
&GAMDA  
GAMMOD=1,OUTGAM='NOOUTP',  
FGAM(1)=0.0262,FGAM(2)=0.0,FGAM(3)=0.0027,  
FGAM(4)=0.8787,FGAM(5)=0.0929,  
FGAM(6)=0.0,FGAM(7)=0.0,FGAM(8)=0.0  
&END  
&DOSDA  
RADDOS=.TRUE.,INDOS=.TRUE.,GAMDEP=.TRUE.,  
ORGNAM='AK. MARV',DINHAL=150.0,BRRAT=3.5E-4,FLTPAK=1.0,  
GDISO=1.59358E-3,DEPSHD=0.798,GAMSHD=1.0,ORGSHD=0.483,  
TDPINT=99900,OUTTOT='OUTPUT'  
&END
```

8.6.2. WINDDA file

```
&WINPAR
WNTLE='WINDDATA (CONSTANT WIND) FOR LAESQ CALC.',
TIME=' 0:00 ',DATE='29-SEP-86 ',ITSP=900,
NP=1,NFX=100,NFY=100,NSTL=2,NSKIP=0,
RTE=0.,RCH=100.,HWOBS=100.,
NAMST(1)='RIS',X(1)=693.85,Y(1)=6176.65,COR(1)=0.,CONFAC(1)=1.,
A(1)=0.,ISXMIN(1)=390000,ISXMAX(1)=842000,
ISYMIN(1)=600000,ISYMAX(1)=6500000,
&END
' 0:00 '
'RIS','F','F',90.,4.00,0.0
'EOWR'
' 00:15 '
'RIS','D','D',90.,5.00,0.0
'EOWR'
' 00:30 '
'RIS','F','F',90.,4.00,0.0
'EOWR'
' 00:45 '
'RIS','F','F',90.,4.00,0.0
'EOWR'
' 01:00 '
'RIS','F','F',90.,4.00,0.0
'EOWR'
' 01:15 '
'RIS','F','F',90.,4.00,0.0
'EOWR'
' 01:30 '
'RIS','F','F',90.,4.00,0.0
'EOWR'
' 1:45 '
'RIS','F','F',90.,4.00,0.0
'EOWR'
```


' 02:00 '
'RIS', 'D', 'D', 90., 4.00, 0.0
'EOWR'
' 02:15 '
'RIS', 'F', 'F', 90., 4.00, 0.0
'EOWR'
' 02:30 '
'RIS', 'F', 'F', 90., 4.00, 0.0
'EOWR'
' 02:45 '
'RIS', 'F', 'F', 90., 4.00, 0.0
'EOWR'
' 03:00 '
'RIS', 'F', 'F', 90., 4.00, 0.0
'EOWR'
' 03:15 '
'RIS', 'F', 'F', 90., 4.00, 0.0
'EOWR'
' 03:30 '
'RIS', 'F', 'F', 90., 4.00, 0.0
'EOWR'
' 03:45 '
'RIS', 'F', 'F', 90., 4.00, 1.0
'EOWR'
' 04:00 '
'RIS', 'F', 'F', 90., 4.00, 1.0
'EOWR'
' 04:15 '
'RIS', 'F', 'F', 90., 4.00, 1.0
'EOWR'
' 04:30 '
'RIS', 'F', 'F', 90., 4.00, 1.0
'EOWR'
' 04:45 '
'RIS', 'F', 'F', 90., 4.00, 1.0
'EOWR'

' 05:00 '

'RIS','D','D',90.,4.00,1.0

'EOWR'

' 05:15 '

'RIS','F','F',90.,4.00,1.0

'EOWR'

' 05:30 '

'RIS','F','F',90.,4.00,1.0

'EOWR'

' 05:45 '

'RIS','F','F',90.,4.00,1.0

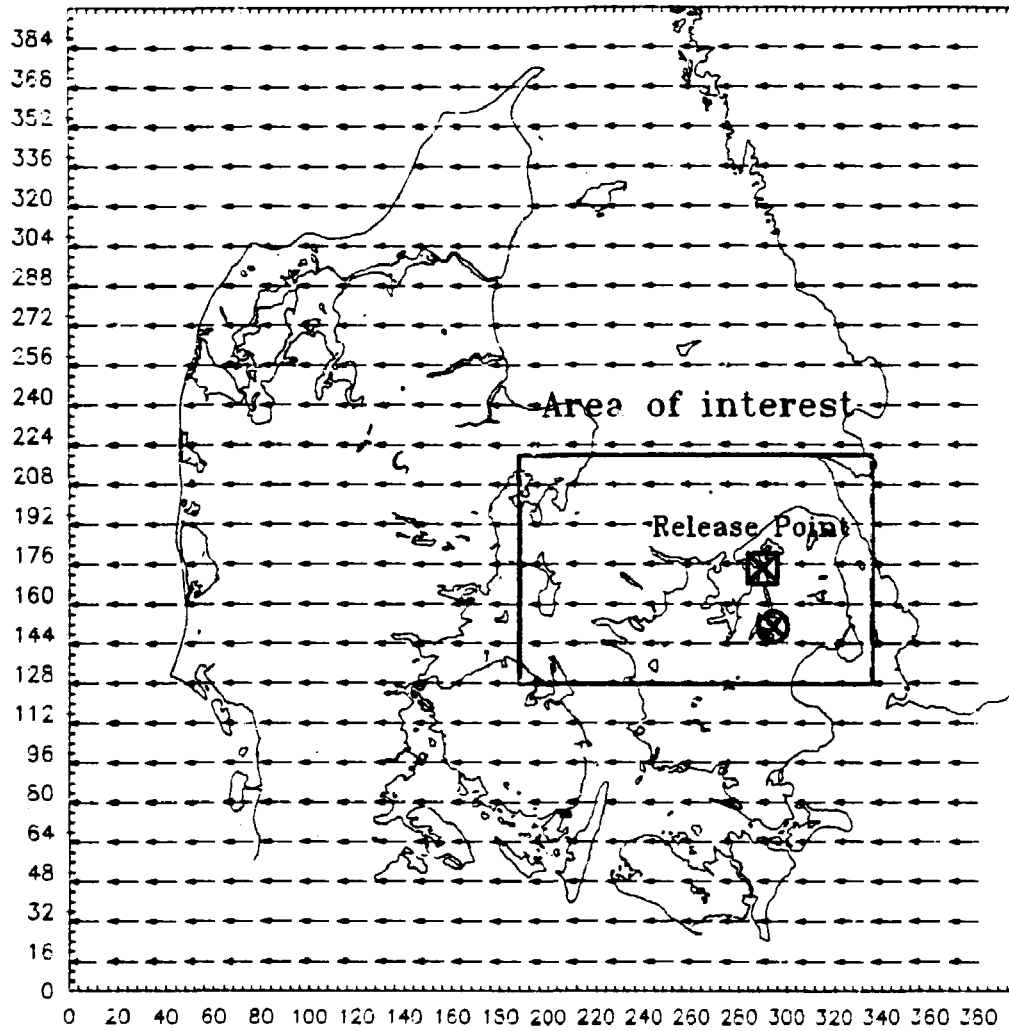
'EOWR'

' 06:00 '

'RIS','F','F',90.,4.00,1.0

'STOP'

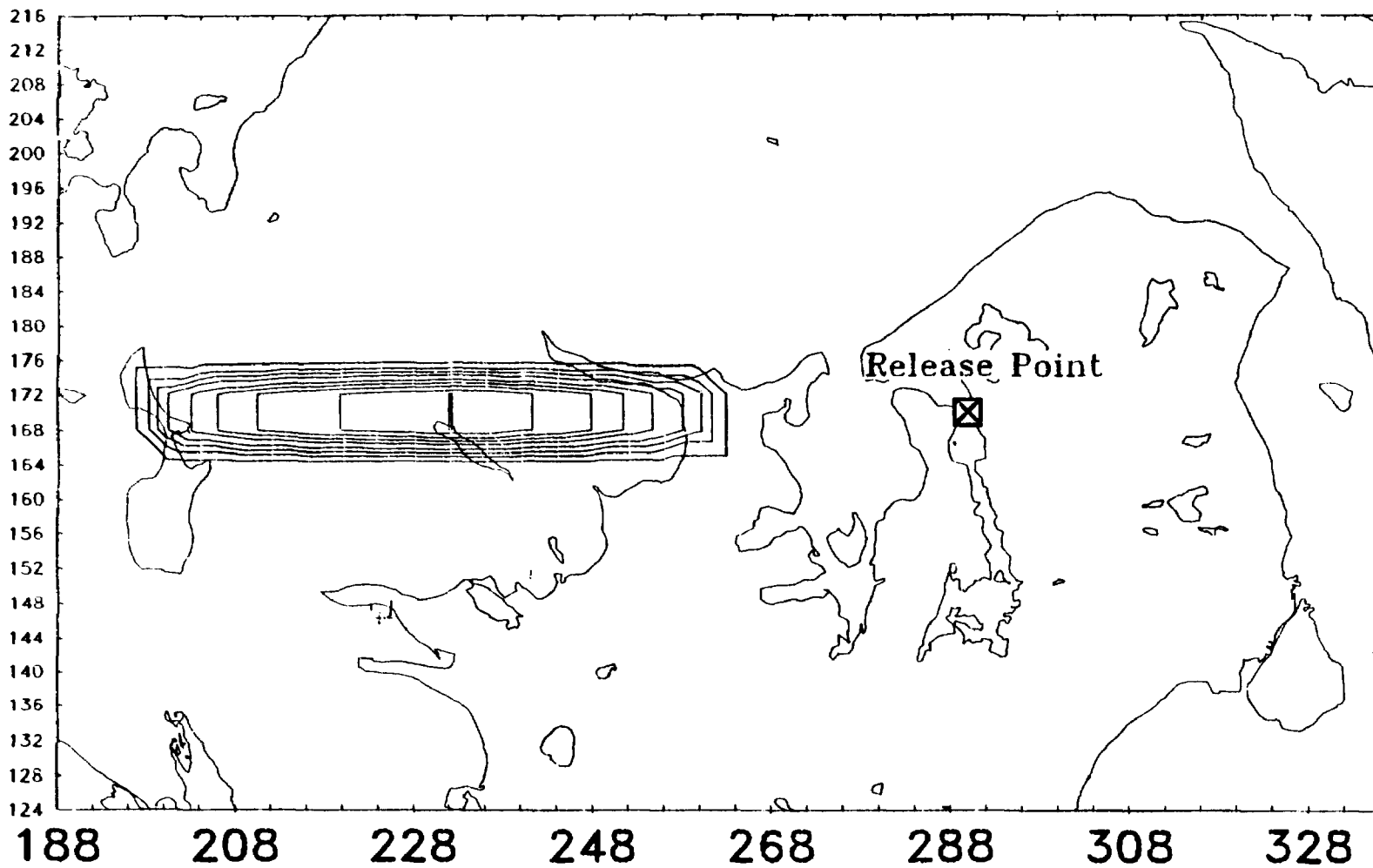
WINDFIELD. TotDos 0.00. Scale: 1 cm= 7.73 m/s. Time 50 sec



Example no. 6: Wind field

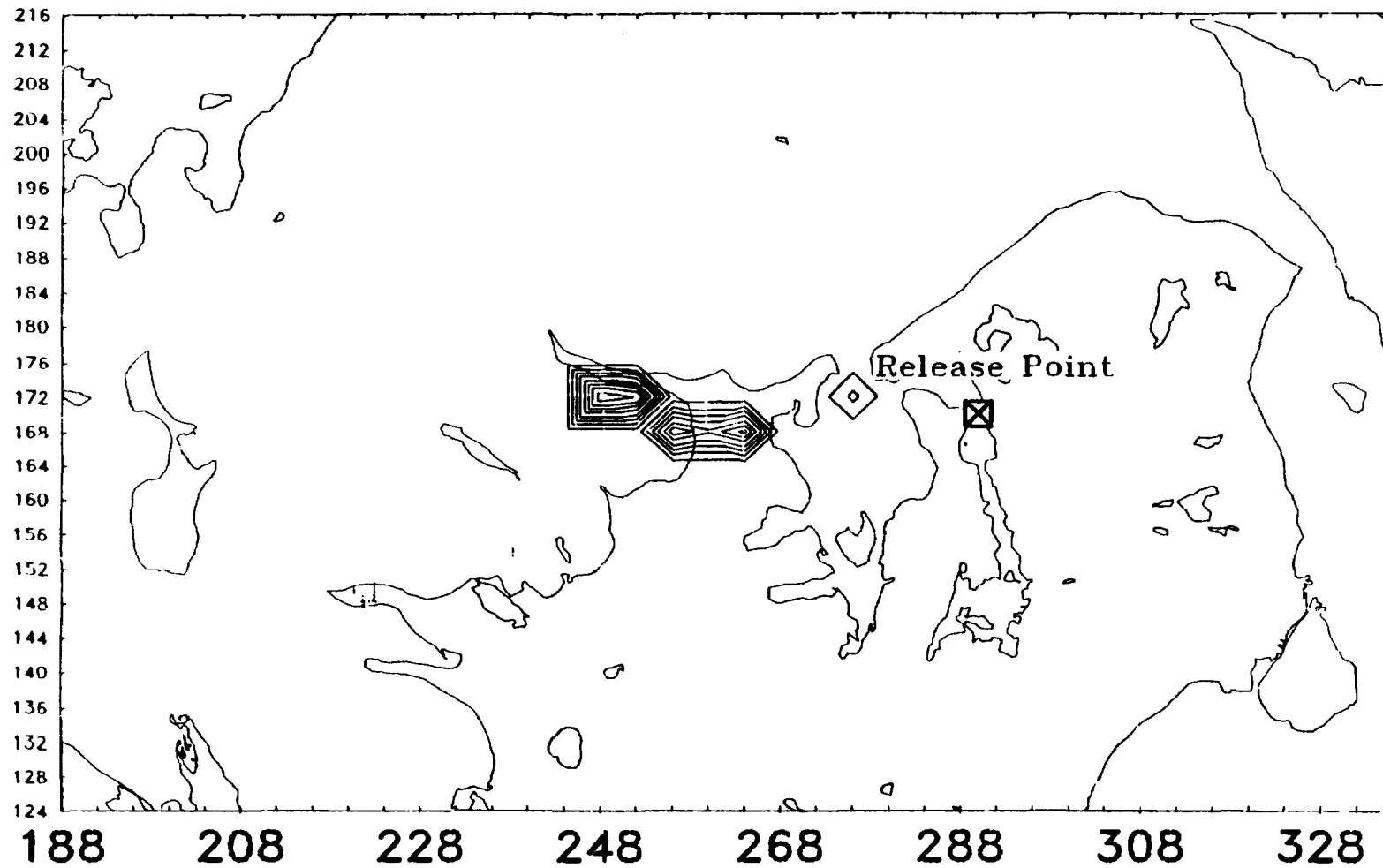
The area of interest for the dose calculations is shown

TotDos 0.00 MaxD: 1.91E+00 R/A Time 6.25hrs



Example no. 6: Total doses to individuals

BefDos 0.00 MaxD: 1.82E+02 ManR Time 6.25hrs



Example no. 6: Collective doses.

8.7. Example no. 7

The files INDATA and WINDDA for calculations of a release of HCl in complex terrain. Pentafication of puffs is in effect.

8.7.1. INDATA file

```
&PRIMDA
TITLE='VANDENBERG AFB. SHUTTLE SITE: 100 M',
ICOLS=50,JROWS=80,KPLANS=1,DELX=500.,DELY=500.,DELZ=50.,
TDEL=0.0,CHEMIN=1.0E-16,NTADV=20,TAU=20,MAPTIM=900,REFLEC=0.,
NRELSE=9999,IDMP=7,JDMP=38,KDMP=1,ISMODE=3,ITAPIN=0,
KCOORD=1,XUTM= 714.1090386,YUTM=3809.792283,
INPRNT='YES',OUTDAT='OUTPUT',OUTMOD='DOSE',OUTWFD='OUTPUT',
PENTPF=.TRUE.,SYMPEN= 600.,ROCKET=.FALSE.
&END
&RELDAT
PUFPTX='SOURCEHEIGHT=100 METERS, SOURCE= 2. TON HCL PR. S',
NRMULT=1,
XSOURC(1)=718.0495114 ,YSOURC(1)=3829.16345807,ZSOURC(1)=2.000,
STRTRL(1)=0,STOPRL(1)=20,SOURST(1)=2.05E9,HEATFX(1)=0.,
ISNAVN(1)='OTHER ',ISDCAY(1)=1.0000E-30
&END
&STABDA
STABTX='MIXING HEIGHT IS 1000 M',
DTDZ=0.,ZMTAB(1)=1000.,ZMTAB(2)=1000.,ZMTAB(3)=1000.,
ZMTAB(4)=1000.,ZMTAB(5)=1000.,ZMTAB(6)=1000.,
DSHEAR=0,ALFSHE=45.0,HSHEMI=1.0,HSHEMA=201.0,
USH=0,USTAR=0.265,LMOBUK=70.0,ZROUGH=1.2,DZERO=0.0,
DUSDUM=0,
DEPMOD=0,OUTDEP='NOOUTP',
VDTAB(1,1)=0.010,VDTAB(2,1)=0.010,VDTAB(3,1)=0.010,
VDTAB(4,1)=0.010,VDTAB(5,1)=0.010,VDTAB(6,1)=0.010,
VDTAB(1,2)=0.010,VDTAB(2,2)=0.010,VDTAB(3,2)=0.010,
```

```
VDTAB(4,2)=0.010,VDTAB(5,2)=0.010,VDTAB(6,2)=0.010,
VDTAB(1,3)=0.010,VDTAB(2,3)=0.010,VDTAB(3,3)=0.010,
VDTAB(4,3)=0.010,VDTAB(5,3)=0.010,VDTAB(6,3)=0.010,
VDTAB(1,4)=0.010,VDTAB(2,4)=0.010,VDTAB(3,4)=0.010,
VDTAB(4,4)=0.010,VDTAB(5,4)=0.010,VDTAB(6,4)=0.010,
VDTAB(1,5)=0.010,VDTAB(2,5)=0.010,VDTAB(3,5)=0.010,
VDTAB(4,5)=0.010,VDTAB(5,5)=0.010,VDTAB(6,5)=0.010,
LDTAB(1)=0.000042,LDTAB(2)=0.000106,LDTAB(3)=0.000233,
TIMRAI(1)=1692,TIMRAI(2)=2628,TIMRAI(3)=2232,
SIGYIN=100.,SIGZIN=100.
&END
&GAMDA
GAMMOD=0,OUTGAM='NOOUTP',
FGAM(1)=0.0,FGAM(2)=0.0,FGAM(3)=0.0,FGAM(4)=0.0,FGAM(5)=0.0,
FGAM(6)=1.0,FGAM(7)=0.0,FGAM(8)=0.0
&END
&DOSDA
RADDOS=.FALSE.,INDOS=.FALSE.,GAMDEP=.FALSE.,
ORGNAM='COMM.DEQ',DINHAL=20715.0,BRRAT=3.5E-4,PLTFAK=0.404,
GDISO=3.04480E-3,DEPSHD=0.160,GAMSHD=0.73,ORGSHD=0.53103,
TDPINT=31536000,OUTTOT='NOOUTP'
&END
```

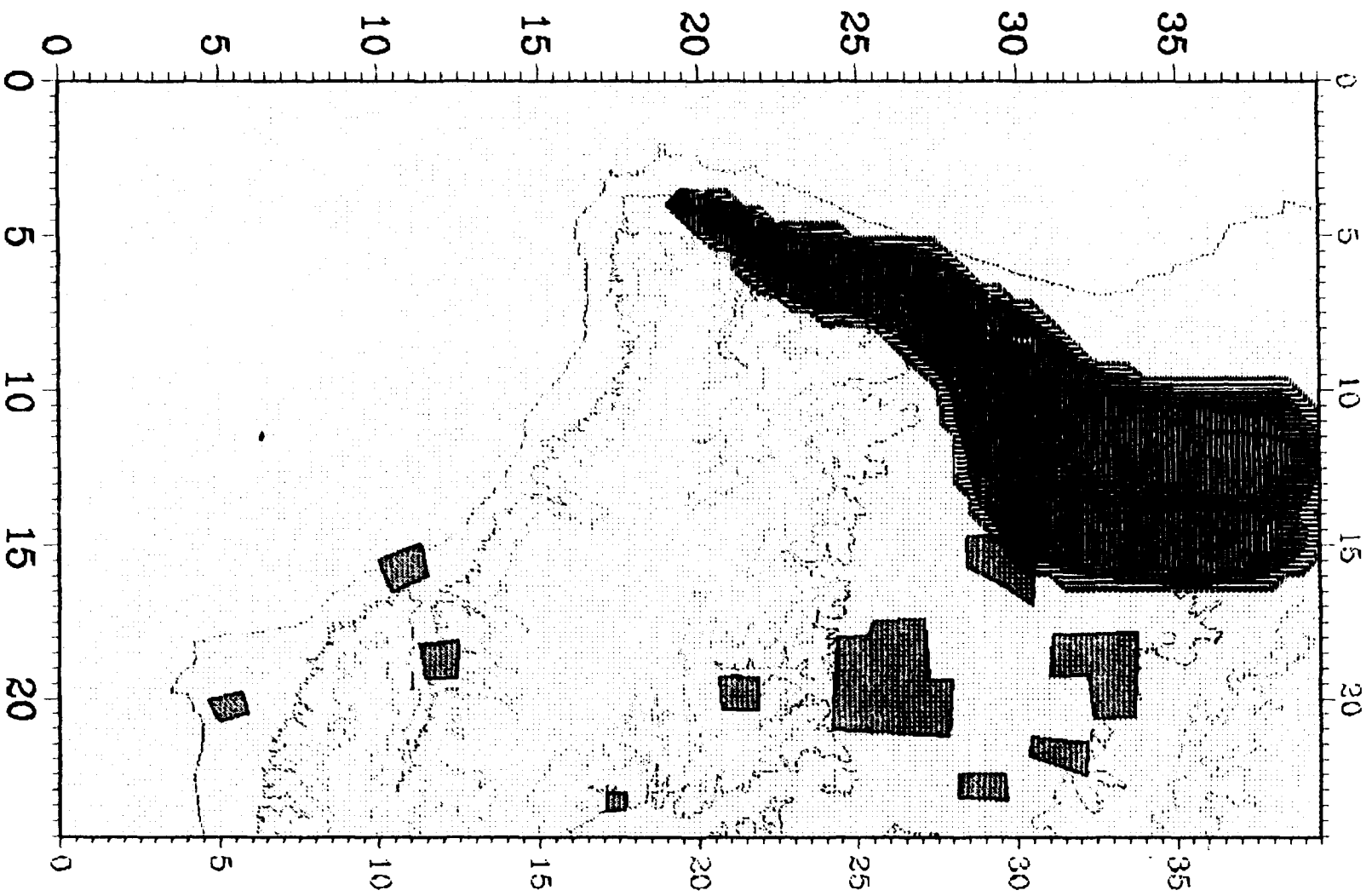
8.7.2. WINDDA file

&WINPAR

WNTLE='WINDDATA FOR VANDENBERG AFB.: CASE 11A',
TIME=' 12:00 ',DATE=' 1984.07.14 ',ITSP=14400,
NP=11,NFX=50,NFY=80,NSTL=1,NSKIP=0,
RTE=4.0,RCH=100000.,HWOBS=16.4,FLOFLD=.FALSE.,
NAMST(1)='009',X(1)=724.907,Y(1)=3837.914,COR(1)=0.,
CONFAC(1)=1.0000,A(1)=0.,ISXMIN(1)=714109,ISXMAX(1)=738609,
ISYMIN(1)=3837763,ISYMAX(1)=3840763,
NAMST(2)='014',X(2)=727.377,Y(2)=3831.980,COR(2)=0.,
CONFAC(2)=1.0000,A(2)=0.,ISXMIN(2)=725550,ISXMAX(2)=738609,
ISYMIN(2)=3809792,ISYMAX(2)=3834817,
NAMST(3)='052',X(3)=721.414,Y(3)=3845.626,COR(3)=0.,
CONFAC(3)=1.0000,A(3)=0.,ISXMIN(3)=719640,ISXMAX(3)=738609,
ISYMIN(3)=3840763,ISYMAX(3)=3849292,
NAMST(4)='054',X(4)=721.532,Y(4)=3835.508,COR(4)=0.,
CONFAC(4)=1.0000,A(4)=0.,ISXMIN(4)=714109,ISXMAX(4)=738609,
ISYMIN(4)=3834817,ISYMAX(4)=3837763,
NAMST(5)='055',X(5)=721.086,Y(5)=3829.540,COR(5)=0.,
CONFAC(5)=0.6000,A(5)=0.,ISXMIN(5)=719640,ISXMAX(5)=722550,
ISYMIN(5)=3809792,ISYMAX(5)=3834817,
NAMST(6)='056',X(6)=724.126,Y(6)=3828.984,COR(6)=0.,
CONFAC(6)=1.0000,A(6)=0.,ISXMIN(6)=722550,ISXMAX(6)=725500,
ISYMIN(6)=3809792,ISYMAX(6)=3831270,
NAMST(7)='101',X(7)=723.736,Y(7)=3832.041,COR(7)=0.,
CONFAC(7)=1.0000,A(7)=0.,ISXMIN(7)=722560,ISXMAX(7)=725550,
ISYMIN(7)=3831270,ISYMAX(7)=3834817,
NAMST(8)='102',X(8)=719.063,Y(8)=3848.291,COR(8)=0.,
CONFAC(8)=1.0000,A(8)=0.,ISXMIN(8)=714109,ISXMAX(8)=719640,
ISYMIN(8)=3840763,ISYMAX(8)=3849292,
NAMST(9)='200',X(9)=718.252,Y(9)=3831.792,COR(9)=0.,
CONFAC(9)=1.0000,A(9)=0.,ISXMIN(9)=714109,ISXMAX(9)=719640,
ISYMIN(9)=3831270,ISYMAX(9)=3834817,
NAMST(10)='300',X(10)=719.640,Y(10)=3834.692,COR(10)=0.,


```
CONFAC(10)=1.0000,A(10)=0.,ISXMIN(10)=719640,ISXMAX(10)=719640,  
ISYMIN(10)=3834817,ISYMAX(10)=3834817,  
NAMST(11)='301',X(11)=717.581,Y(11)=3828.803,COR(11)=0.,  
CONFAC(11)=1.0000,A(11)=0.,ISXMIN(11)=714109,ISXMAX(11)=719640,  
ISYMIN(11)=3809792,ISYMAX(11)=3831270,  
&END  
' 00:40'  
'009', 29.7,'E', 266, 1.5, 0.0  
'014', 17.2,'E', 137, 2.7, 0.0  
'052', 8.5,'E', 180, 0.3, 0.0  
'054', 11.7,'E', 276, 0.6, 0.0  
'055', 5.5,'E', 127, 2.5, 0.0  
'056', 3.1,'E', 129, 4.6, 0.0  
'101', 15.6,'E', 69, 0.5, 0.0  
'102', 10.3,'E', 174, 1.1, 0.0  
'200', 32.4,'E', 240, 1.3, 0.0  
'300', 38.6,'E', 191, 1.7, 0.0  
'301', 25.9,'E', 210, 1.3, 0.0  
'STOP'
```

The output from this example is shown on the following pages.



Output from example no. 7

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INDEX

	Pages
ALFSHE	25
BEFDA	16,17,41,42
BRRAT	30
CALCSY	22
CHEMIN	19
CONFAC	37
COR	36
DATE	34
DELX	19
DELY	19
DELZ	19
DEPMOD	27
DEPSHD	31
DINHAL	30
DOSDA	18
DSHEAR	25
DTDZ	25
DUSDUM	26
DZERO	26
FGAM	29
FLTFAK	30
GAMDA	18
GAMDEP	30
GAMMOD	29
GAMSHD	31
GDISO	31
HEATFX	24
HSHEMI	25,26
IBFOPT	22
ICOLS	18
IDMP	20
INDATA	16,17,18

INDOS	30
INPRNT	22
ISDCAY	24
ISMODE	21
ISXMAX	37
ISXMIN	37
ISYMAX	37
ISYMIN	37
ITAPIN	23
ITSP	35
JDMP	20
JROWS	18
KDMP	21
KOORD	19
KPLANS	19
K1ST	36
LDTAB	27
LMOBUK	26
MAPTIM	20
NAMST	36
NFX	35
NFY	35
NP	35
NRELSE	20
NRMULT	24
NSKIP	35
NSTL	35
NTADV	19,20
ORGNAM	30
ORGSHD	31
OUTAIR	43
OUTBEF	23
OUTBFD	43
OUTBFT	44
OUTDEP	27,43
OUTGAM	29,43

OUTMOD	22
OUTPUT	22
OUTTOT	31
OUTWFD	23
PENTPF	21
PRIMDA	18
PUFFTX	24
RADDOS	30
RCH	35
REFLEC	20
RELDAT	18
ROCKET	21
RTE	35
SIGYIN	25
SIGZIN	25
SOURCT	24
SSKIP	36
STABDA	18
STABTX	25
STOPRL	24
STRTRL	24
SYMPEN	21
TAU	20
TDEL	19
TDPINT	31
TIME	34
TIMRAI	28
TITLE	18
USH	26
USTAR	26
VDTAB	27
WFIELD	43
WINDDA	16, 17
WINPAR	34
WNTLE	34
XSOURC	24

XUTM	19
YSOURC	24
YUTM	19
ZMTAB	25
ZROUGH	26
ZSOURC	24

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